ELECTRONIC INDUSTRIES - RADIO-TELEVISION



Control Room

Core Materials
for Small Tempsformer

October

1953

STATION & STUDIO
EQUIPMENT
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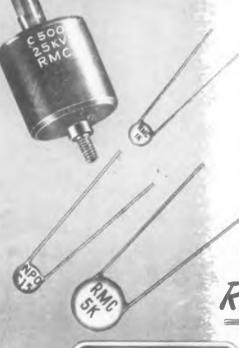
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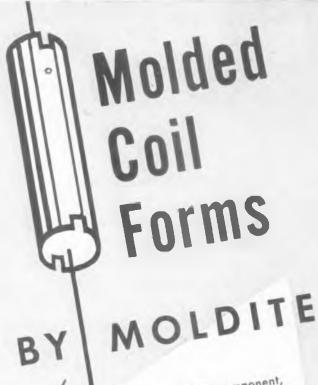
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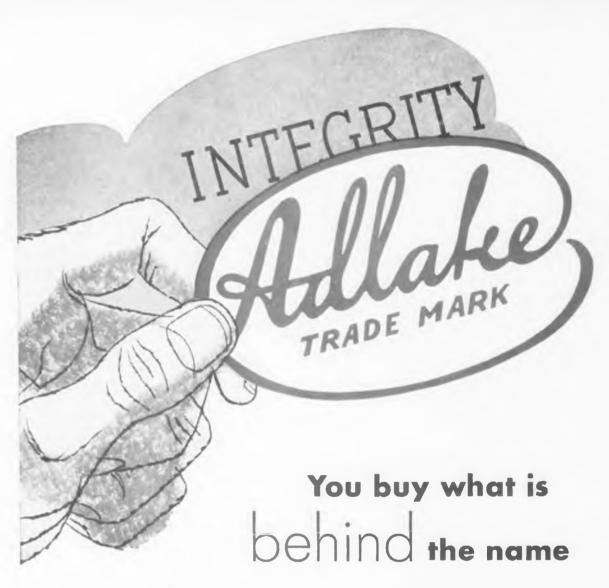
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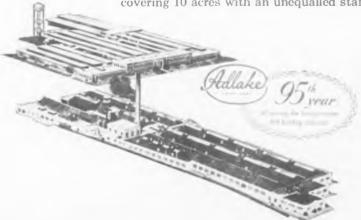
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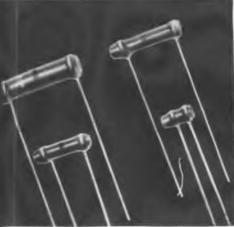
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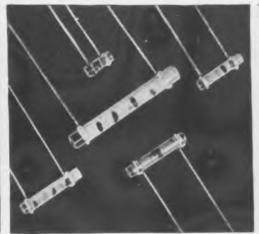
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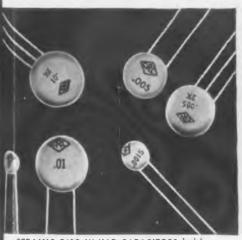
BC HI-KAP TUBULAR CERAMIC CAPACI-TORS available from 1 mmf to 10,000 mmf. Ideal for use in r.f. by-pass and audio-coupling applications. For details, write for Bulletin 42-3.



TUBULAR CERAMIC CAPACITORS — Type TCZ show no capacitance change over wide temperature range. Type TCN spe-cial ceramic body varies capacitance with temperature. Write for Bulletin 42-18.



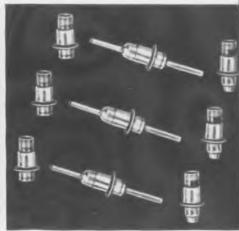
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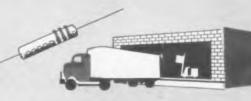
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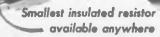
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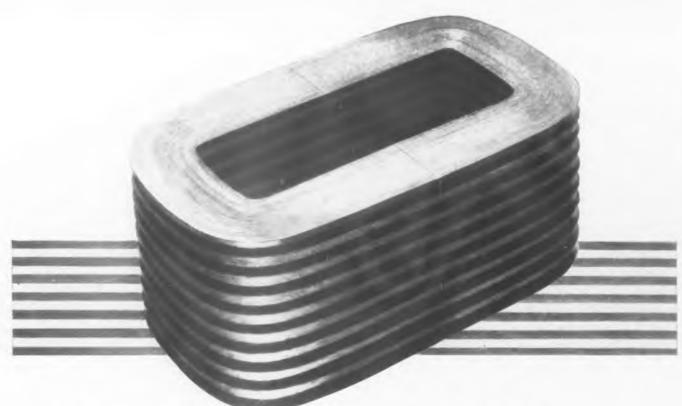
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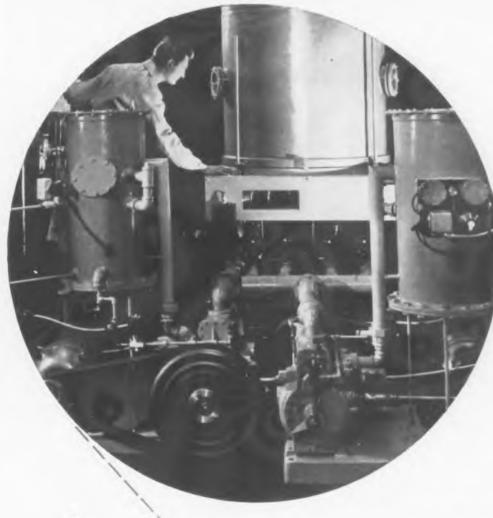
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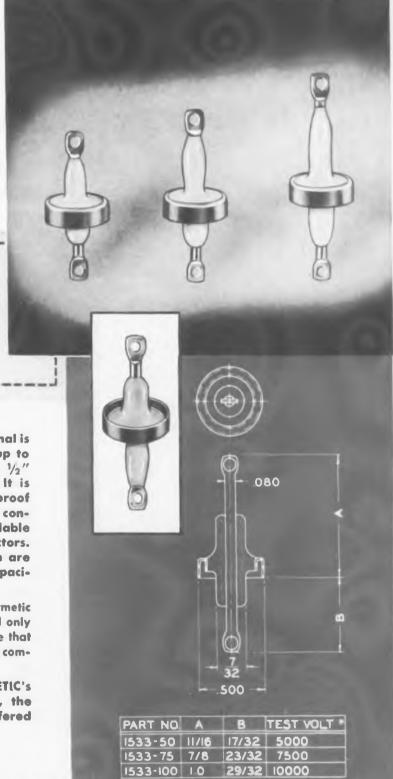
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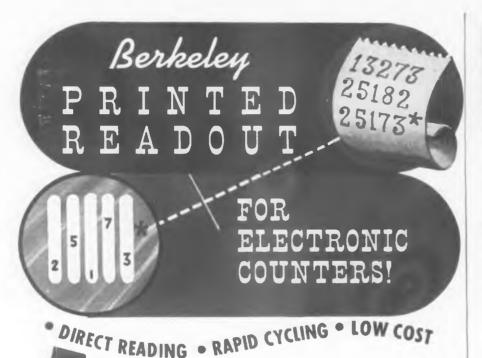
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DIGITAL RECORDER... Series 1550 is composed of a Readout unit and a Printing Recorder. The first unit consists of a bank of readout decimal counting units essentially paralleling the totalizing function of the basic counting instrument from which they operate, and a selecting relay matrix to channel information from the counting circuit to the Printing Recorder. This second unit presents a sequence of total counts in direct reading digital form on a standard adding machine tape.

A COMPLETE SYSTEM... of Electronic Counter and Digital Recorder then consists of three elements: a suitable electronic counting device, Readout unit, and Printing Recorder. The latter two elements comprise the complete Digital Recorder. Under certain conditions a special modification of the system will permit original count information to be channeled directly into the Readout unit, thus eliminating the need for a separate electronic counter.

SPECIFICATIONS . . . Minimum counting period determined by the characteristics of the basic counting instrument. Maximum cycling rate: 1 printout every ³4 second. Indicating capacities 3, 4, 5 or 6 columns. Readout Unit—20³4" x 10³2" x 15" cabinet, wt. 60 lbs., standard 19" relay rack panel. Printing Recorder—7³2" x 8³4" x 14³2" cabinet, wt. 20 lbs. Price, Digital Recorder, Model 1553 (3-column), \$1050; Model 1554 (4-column), \$1125; Model 1555 (5-column), \$1200; Model 1556 (6-column), \$1275, f.o.b. factory.

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"DIRECT READING DIGITAL PRESENTATION OF INFORMATION"



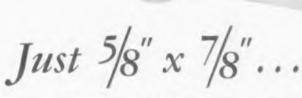
"PREVIEW TV" is the name given a special TV set which, installed in public places operates by a special patented device for a few minutes at the beginning of a program giving a preview of that program without charge, thereupon turning itself off, lighting up a sign which instructs the user to deposit a coin to see the remainder of the program. Large blocks of motels have been signed up for installation of this new TV entertainment device.

WAVE CONTOURS may now be studied by a gage which is submerged deep in the ocean and feeds a sensitive magnetic amplifier which responds to powers of less than 10⁻¹² watt. Left alone for days or weeks at a time, the instrument records faithfully the slightest disturbances on the surface. The magnetic amplifier operates by changing very small do into a variation of ac which is shown on a cathode ray tube to reproduce the contours of the ocean waves.

INDICATIONS are that the size of TV tubes is going to stay up, but that 30 in. will be the largest for home use. After all, cabinets to house picture tubes larger than this will not pass through doorways in the average home! We hear that many tube makers are disposing of their 16 and 17 in. tubes at very low prices. Does this mean that these will soon join the 10-in. tube in the limbo of the past?

WORLD'S LARGEST TRAIN communication system is claimed by the Pennsylvania Railroad, Presently installed over 2000 miles of line from the eastern seaboard to Chicago and St. Louis, the company plans to increase its present \$9,000,000 investment and extend the radio-and-wire network over more of its system. Greater efficiency and increased safety result from the rapid communication between crewmen, flagmen and station control operators. Statistical breakdown on units in service: Two-way telephone equipment on 916 locomotives, 230 freight train cabin cars, and 122 wayside towers, as well as 25 walkie-talkies for portable use.

(Continued on page 24)



yet the rating of this Mallory Tantalum Capacitor is 120 mfd at 15 volts for operation from -60° C. to $+125^{\circ}$ C. It will operate at 12 volts up to $+200^{\circ}$ C.

Developed for the Armed Forces subminiaturization program, Mallory Tantalum Capacitors now are available in a wide range of sizes and ratings.

They offer you the advantages of:

Compactness

Continuous performance over a temperature range of -60° C. to $+200^{\circ}$ C.

High resistance to shock and vibration

Proof against thermal shock from -60° C. to $\pm 200^{\circ}$ C. without damage

Double sealing for absolute protection under all operating conditions

Now that Mallory Tantalum Capacitors are available in quantity, check their advantages for your equipment. Don't hesitate to consult Mallory on any problem involving the application of capacitors, the development of special types or the simplification of related circuits.

Get complete information...

Write for your copy of the Technical Information Bulletin on the Mallory Tantalum Capacitor. It is complete with sizes, mounting arrangements, surge voltages and performance curves.



SERVING INDUSTRY WITH THESE PRODUCTS:

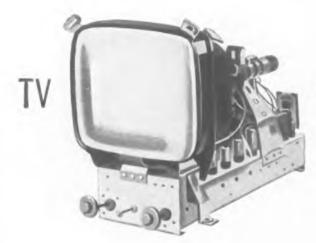
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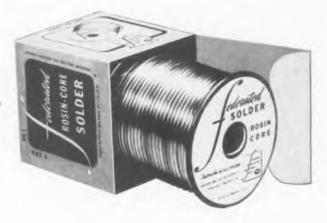


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For any soldering job that demands freedom from corrosion and conductive flux residue... for ease of working and unequalled consistency... there is nothing better than Federated Rosin Core Solder.

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Federated Rosin Core Solder is a quality product that is unsurpassed for the permanence of the bond it produces... for the consistently easier soldering job it does! Look for it in 1. 5, 20, 25, and 50-pound sizes on the familiar orange and black metal spool. Listed by Underwriters' Laboratories Inc.

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THE NEW

RAYTHEON

TYPE CK628

LOW MICROPHONIC SUBMINIATURE TRIODE

OF A UNIQUE DESIGN*

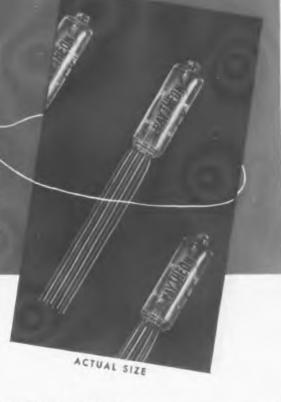
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MICROPHONIC NOISE OUTPUT - NOT MORE THAN 2.5 MILLIVOLTS across plate resistor of 10,000 ohms with applied vibrational acceleration of 15 G at 40 cycles per second.



- *The low microphonics result from Raytheon's advanced design - not from tube selection.

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TELE-TECH . October 1952

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with experience in

RADAR OR ELECTRONICS

Hughes Research and Development Laboratories, one of the nation's large electronics organizations, is now creating a number of new openings in an important phase of its operation.



Here is what one of these positions offers you:

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Hughes Research and Development Laboratories is located in Southern California. We are presently engaged in the development of advanced radar devices, electronic computers and guided missiles.

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The positions are for men who will serve as technical advisors to the companies and government agencies purchasing Hughes equipment. Your specific job would be to help insure the successful operation of our equipment in the field.

3. THE TRAINING

Upon joining our organization,

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4. WHERE YOU WORK

After your period of training (at full pay), you may (1) remain with the company Laboratories in Southern California in an instruction or administrative capacity, (2) become the Hughes representative at a company where our equipment is being installed, or (3) be the Hughes representative at a military base in this country—

or overseas (single men only). Compensation is made for traveling and for moving household effects, and married men keep their families with them at all times.

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You will gain all-around experience that will increase your value to the company as it further expands in the field of electronics. The next few years are certain to see a large-scale commercial employment of electronic systems—and your training in the most advanced electronic techniques now will qualify you for even more important positions then.

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If you are under thirty-five years of age, and if you have an E. E. or Physics degree, with some experience in radar or electronics,

write to:

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RESEARCH AND DEVELOPMENT LABORATORIES

Engineering Personnel Department

CULVER CITY, LOS ANGELES COUNTY, CALIFORNIA

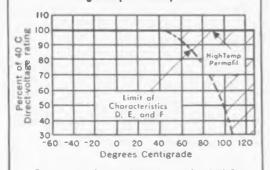
Assurance is required that relocation of the applicant will not cause disruption of an urgent military project.

Reduce space and weight requirements as much as 80%...



G-E Permafil d-c capacitors designed to operate in high ambients—up to 125 C—without derating

Why you gain by using Permafil capacitors for high-temperature operation



Comparison of operating voltages for JAN-C-25 characteristics D (vegetable oil), E (mineral oil), and F (synthetic insulating liquids) with Permafil impregnated capacitors crosshatched area reveals advantages of Permafil over other impregnants in the high-temperature range above 40 C.

For ambient temperatures above 40 C, most liquid-filled paper-dielectric capacitors require considerable derating. This increases both space and weight requirements.

G-E Permafil capacitors, however, operate in high ambients—up to 125 C—for 10,000 hours, at full rated voltage. They average about $\frac{1}{25}$ the size and weight of liquid-filled capacitors that will operate at 125 C—a saving of 80%. They're suitable for all blocking, by-pass, filtering, and many coupling and timing applications.

Permafil capacitors stand up in elevated temperatures because the paper dielectric is impregnated with a *solid* plastic compound that retains its electrical stability at *both* high and low temperatures. And since the impregnant is a solid, it can't leak. With proper derating or where short life characteristics are permissible, Permafil capacitors can be used in temperatures as high as 150 C. They can also be used in high altitudes and where extreme cold is encountered. Other characteristics include high insulation resistance and comparatively constant capacitance with temperature changes.

G-E Permafil capacitors can be obtained in case styles CP53 and CP61, as covered by specification JAN-C-25—in ratings of .05 to 1.0 muf, 400 volts DC. They are housed in metallic containers and hermetically sealed with G-E long-life all-silicone bushings.

For full information on Permafil capacitors, see your local G-E representative. Or write Section 407-310. Ask for Bulletin GEC-811. General Electric Company, Schenectady 5, New York.

GENERAL ELECTRIC



Sylvania provides highest quality electronic components for radio, television and other electronic equipment . . . at lowest prices.

New plant facilities and improved methods now enable Sylvania to provide you with highest quality electronic components for every need . . . when you need them.

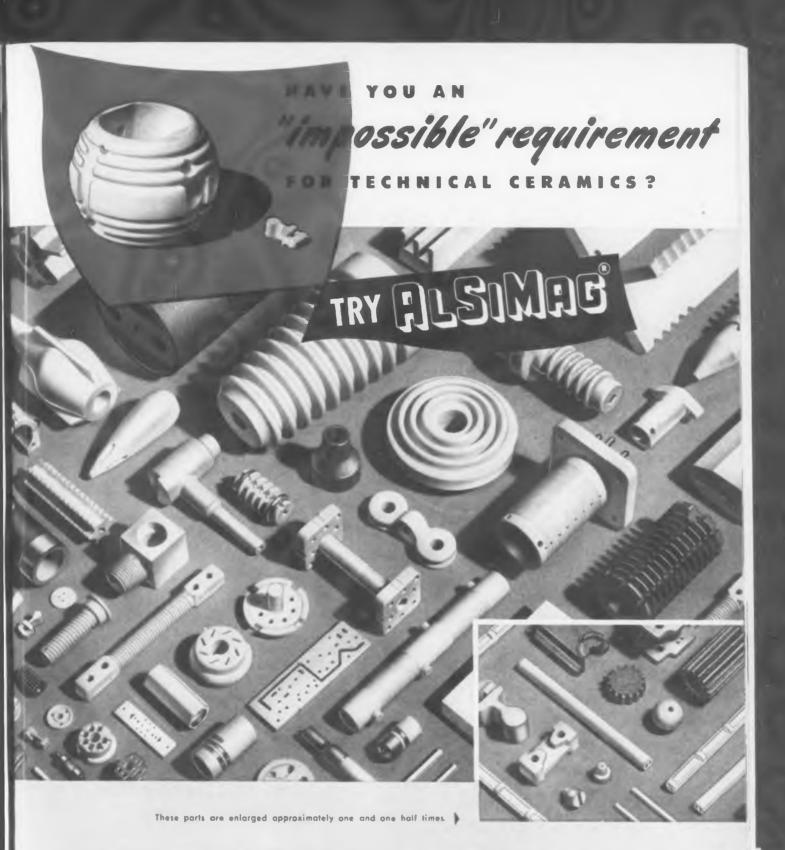
Typical examples of Sylvania components in-

clude hundreds of diversified items such as: Terminal Strips and Boards; JAN Sockets; Radio Tube, Cathode Ray Tube and Power Tube Sockets; Fuse Holders; Plugs and Connectors.

To be sure of the finest possible quality . . . put your component problems up to Sylvania. We welcome your inquiries addressed to: Sylvania Electric Products Inc., Dept. A-1111, Warren, Pa.



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Many people are kind enough to say we're the first to try for any "impossible" technical ceramic. It's probably true that we've made more different sizes, types and shapes than anybody.

Through cooperation, and a little give and take on both sides, we've been able to make a lot of "impossible"

ceramics. If you have an "impossible" requirement, let us know. We might be able to work it out with you. Anyway, we'd be caught trying.

We don't make a thing but technical ceramics. We've been doing it for over fifty years. It might pay you to give us first crack at anything in technical ceramics.

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TELE-TIPS

(Continued from page 16)

GERMANIUM, wonder metal of the 4-year-old transistor, was first predicted by the Russian chemist Dmitri Mendeleff, in 1871, who described its probable properties while compiling his famous "periodic table of the elements,"-although he never lived to see the actual metal. Fifteen years later, Clemens Winkler, a German, actually discovered a piece and named it for the Latin designation of his native land. Then nothing much happened for 62 years, until the telephone people discovered that germanium worked like the cat-whiskers in early crystal sets, except a whole lot better. Most germanium is found in chimneys as a waste from the smeltering of lead, titanium, and zinc. The Eagle-Picher Co., which didn't realize for years what precious stuff was going up its flues, is the leading producer of germanium in the U.S.

UNDERWATER SOUND EQUIP-MENT is receiving accentuated attention. The Navy reports that the number of West Coast manufacturers producing these equipments has doubled within the last year. At the Navy Electronics Laboratory on Point Loma, San Diego, Cal., a multi-million dollar annual research and development program is being carried out by a staff of over 1000 scientists, engineers, and technicians. The success of its program depends greatly upon the ability and willingness of West Coast manufacturers of electronic equipments to produce development models and equipments from NEL designs as required by the Navy's materiel Bureaus.

"ELECTRONIC COP"-a simple radar-like device that sends out a beam of 5-in. radio waves and picks up their echoes from moving objects, is being used to detect automobiles, as well as pedestrians, approaching the main entrance of the General Electric Research Laboratory at Schenectady, N.Y. Approach of a car causes a bell to ring, warning a guard whose attention may have been temporarily diverted, as by a telephone call. A person walking is detected at about 100 ft., an automobile produces an effect several hundred feet away. Though the system differs from radar used to reveal the presence of ships and airplanes, mainly in the fact that its waves are sent out continually rather than in brief pulses, it does embody principles used in the wartime proximity fuse. The vehicle-approach alarm system was developed by William C. White, C. Luther Andrews and Hiram S. Lasher of the Laboratory. The system sends out radio waves which are only 5 in, long and behave much like light waves. Some of these waves may be echoed back to the transmitter by an object in the beam. If the object is stationary nothing happens. But if it is moving, the returning waves successively go in and out of step with those being sent out, causing the alarm to operate.

TINY CAPACITOR—At the recent Manchester, England, radio-TV exhibition among the components shown was what the British claimed to be the smallest capacitor in the world. This is ¹16 in. in diameter and is wound round with paper on which there is a metal coating a millionth of a millimeter thick—a dimension which can only be measured by electrical resistance or by light.

PITY THE POOR SCOTS who have a television station but can't see TV in the town alongside the station! It seems that there is no electric power in Shott 'O Kirk in Scotland where the Scottish TV transmitter is located. Perhaps there's a fortune for someone who can make a good cheap battery-operated TV set for export— or for portable domestic use!

THE WHITE HOUSE, as reconstructed, is now completely protected against lightning, using halfinch lightning conductor cable leading to half-inch copper ground rods 10 ft. long. The George E. Thompson Co., Minneapolis, Minn., which made the installation, recommends that all radio and TV antennas be provided with arresters grounded through similar heavy conductors, as was done for the White House. Since 1885 the Federal Government has been protecting its buildings from lightning. That year an installation was made on the Washington Monument after it had been struck twice.

SALESMAN'S PRAYER—"O Lord, help me to Remember that Humility is still the Hallmark of the Successful Salesman—that the Seller is Always Servant to the Buyer—that Arrogance Costs as many orders as Ignorance of the Line—that I have Too Short a Memory ever to Tell a Lie—and that the Buyer has Too Long a Memory ever to Forget a Wrong!"—Posted in waiting room outside the office of A. J. Schmitt, president of the multi-million dollar American Phenolic Corp., Chicago.



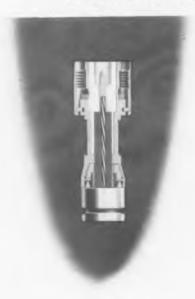
high heat resistance... low loss...

Designed for extreme heat conditions, such as are encountered in modern aircraft, Teflon dielectric performs satisfactorily in temperatures as high as 500° F. Use of Teflon as dielectric in RF cables is an outstanding achievment of the skilled research team at Amphenol.

In addition to the important feature of high heat resistance, Teflon has electrical characteristics which exceed those of Polyethylene. Teflon is the *one* satisfactory cable for use, not only in aircraft, jet engines or guided missiles, but in covered electronic equipment or any application where temperatures might run over 185 F.

TEFLON

POLYTETRAFLUOROETHYLENI



for insulation in cables & connectors

Expert engineering, highest quality materials and stringent continuous inspection make Amphenol cables the very best that can be had anywhere! Uniform quality and maximum performance from every foot of Amphenol cable is assured by constant checking and testing. Every shipment of cable is accompanied by a notarized affidavit certifying the guaranteed construction of the cable.

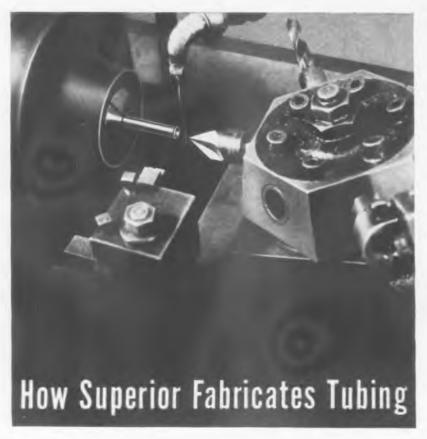
Amphenol also manufactures a comprehensive line of RF Connectors with Teflon inserts for high voltage or extreme heat applications.

Write for this free literature describing Amphenol Teflon cable. Address Dept. 13D



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It's a job we like to do and know how to do. But there's more to the story than simple production of fabricated or semi-finished parts, or even top-quality tubing in any analysis and many sizes. The rest of the story is our willingness, desire and ability to work closely with customers' development engineers and product designers. Frequently we are able to materially assist in design of parts, selection of analysis, and development of processes. Many times we have been able to suggest minor changes in shape or method to effect major economies in assembly time and product cost.

If you are a manufacturer or an experimenter in electronics and have a need for a tubular part of any kind, check with us. We can probably help by giving you quantity production of the parts you need. Write Superior Tube Company, 2508 Germantown Ave., Norristown, Pennsylvania.



Cut and Annealed. Extensive cutting equipment, hand cutting jigs, electronically controlled annealers and other equipment, much of it developed within our own organization results in high speed, precision production of parts.



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Expanded. Here is a part almost ready for delivery. Simple as it looks, it may well have been the subject of a score of operations and at every stage the prime consideration has been the *quality* of the finished part.

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NICKEL ALLOYS FOR OXIDE-COATED CATHODES: This reprint describes the manufacturing of the cathode sleeve from the refining of the base metal. Includes the action of the small percentage impurities upon the vapor pressure, sublimation rate of the nickel base; also future trends of cathode materials are evaluated.



SUPERIOR TUBE COMPANY • Electronic products for export through Driver-Harris Company, Harrison, New Jersey • Harrison 6-4800

National Engineering Research finds the economical solution

The problem:

to insulate a 5 kilovolt, 1500 ampere bus bar installation

Recently I-T-E Circuit Breaker Company of Philadelphia had the problem of *completely* insulating 5 kilovolt, 1500 ampere 3 phase bus bar units for an Atomic Energy Commission installation. It was simple enough to insulate the bus bars with oval Phenolite tubing. But, to completely insulate the bus supports and expansion joints was a real problem. I-T-E's engineers showed us what they wanted postformed Phenolite insulating covers and drawn deeper than anything we had ever attempted. Our engineers tackled the problem.

The solution:

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Perhaps your problem doesn't involve the insulation of 5 KV, 1500 ampere bus bars. But maybe you have an insulating problem where National can give you some real help in solving how to do your certain job economically. Write us, our engineering service is immediately available.

National Laminated Plastics nationally known—nationally accepted

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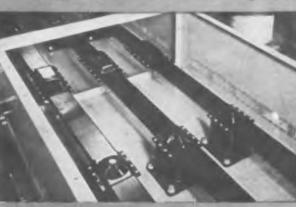
Phonolite postformed expansion joint cover.



Expansion joint with and without Phenolite insulating covers



Bus support with and without Phenalite Insulating covers.



Completed installation, showing Phenolite insulation for his



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The IBM card punch receives the data from the Telecordex, punches it and continues the cycle.

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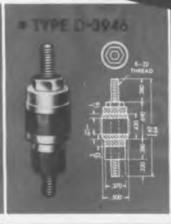
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TYPES



3	PART NO.	D-3342	D-3346	D-3350	D-3349
D-7mmu Hoat Dis	A	1 1/32	1 19/32	21/32	33/14
	В	.490	5/8	15/16	3/4
	C	3/8	.490	11/16	1/16
E 21-	D	.095	.095	.130	.130
1	E	3/16	1/4	3/8	1/4
144	F	3/16	3/8	3/8	5/16
	G	1/2	7/8	1 15/32	27/16
7E SUDEACE	Н	1/16	3/32	1/8	1/8
AZE SURFACE ETALLIZED SURFACE	J	3/32	1/8	1/8	1/8
					-

THREADED STUD TYPES

PART NO.	D-3856	D-3857	D-3962	D-3638
A	17/32	151/64	215/32	215/32
В	.490	5/8	15/16	15/16
C	3/8	.490	11/16	11/16
D	1/16	1/14	.055	1/16
E	1/4	1/4	3/8	3/8
F	3/16	3/8	3/8	3/8
G	1/2	7/0	1 15/32	1 15/32
Н	1/16	3/32	1/8	1/0
J	3/32	1/8	1/8	1/8
K	6-32	6-32	8-32	10-32



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9 standard terminal designs fit every mounting need

20,000-Volt Molded Ceramic Capacitors

Molded in moisture resistant, non-flammable thermosetting plastic, these new Sprague Type 700C Ceramic Capacitors offer exceptional reliability and economy as filters for TV receivers and C-R instrument high-voltage supplies. Standard capacitance is 500 mmf. and the units are conservatively rated for operation at 20,000 volts d-c. Write on letterhead for Engineering Bulletin 606.



Extended Capacitance Ranges for Precision Circuitry

These new Sprague-Herlec Precision Tubular Ceramic Capacitors make it possible to control the capacitance tolerance of exacting 500, 1000 and 1500 V. d-c precision circuits within $\pm 1\%$. Temperature coefficient tolerances may be reduced to as little as ± 10 parts in a million!

A logical development of the design first popularized in Sprague-Herlec cup ceramics, they greatly extend the capacitance range available to designers. "Q" and capacitance stability are high and the units have excellent retrace characteristics. Hermetically sealed in metal tubes, they operate over the range from -55°C. to +85°C. Bulletin 607 sent on letterhead request to Sprague etric Company, 233 Marshall St., North Adams, Mass. or to the wholly and Sprague subsidiary, The Herlec Corp., 422 N. 5th St., Milwaukee 3, Wis.

WORLD'S LARGEST

SPRAGUE CA

CAPACITOR MANUFACTURER

TELE-TECH

& ELECTRONIC INDUSTRIES - RADIO-TELEVISION

O. H. CALDWELL, Editorial Director * M. CLEMENTS, Publisher * 480 Lexington Ave., New York (17) N. Y.

Engineers Must Learn How to Sell —

Both Themselves and Engineering Ideas!

Engineers are a modest lot. We are prone to let our work speak for itself without realizing that, by the time it speaks in a language that is readily understood, the authorship may have been forgotten. There is little wonder that the major credit often rebounds to the producer or the seller rather than to the creator of a new product. Far too often success is not achieved and excellent conceptions are never fully developed because we have failed to recognize the need to sell the idea itself, its potential for good, or the research necessary to apply it.

Far too generally accepted in the profession is the idea that selling is something for which one has to be specifically suited, and that selling is somehow incompatible with engineering. Selling is a universal human tool wherever man deals with man. From the time we are born, we are constantly engaged in selling. A baby's cry in the night is his way of selling the idea that it is time for feeding, and if you don't buy the idea, you don't sleep. This may be an effective way for an infant to sell his needs, but considerable more maturity is required as our social contacts become more complex.

Emotional Maturity Needed

It is not unreasonable to expect engineers to develop an emotional maturity equal to that of anyone engaged in selling as a profession. I am afraid it is our failure to recognize this that often makes us poor salesmen, rather than our inability to present facts in a logical manner. What we have to present can be scientifically unimpeachable, but unless it is understood, our efforts will be ineffective. We need, therefore, to develop an understanding of the other fellow and an ingenuity of presentation which will help him to understand our goal and share our desire to see such goals achieved.

To be honest we have to admit that one of our greatest failings as engineers has been our propensity to examine the details, leaving far too little time to be broadly objective in our planning. If, in addition to the time spent in solving our immediate problems, we would find time to show more enthusiasm for the ultimate objectives, there should be an enhancement of both the economic and social standing of our profession.

Selling is communication, and this is where engineers in the past have been lamentably weak: we have mastered the *science* but not the *art* of communication.

Tune To the Other Fellow's Wavelength

When, on the other hand, an engineer does have the ability to communicate his ideas to others clearly, he becomes a marked man. I saw a striking example of this not so long ago. It was at an important management meeting in which an engineer was called on to give a progress report to men who, for the most part, had not met this engineer before. In fifteen minutes he told, in a simple way to men who were not engineers, what he was doing, with such clarity and conviction that he at once became a man marked for a future. He had something to sell and he sold it. To do this he first had to be able to put himself in the place of his audience in order to appreciate its interest and point of view, then make his presentation accordingly. Often we get better results by tuning our transmitter to the other fellow's receiver rather than by assuming he will tune to our wavelength.

Let me add that retuning our transmitter is not always the easiest job in the world. The wavelengths on which we must transmit are numerous if communication in the true sense is to be established.

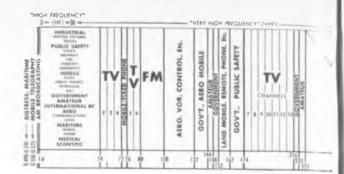
Wider acceptance of engineering philosophy, and a more complete realization of its goals, depend in large measure on salesmanship of the right kind.

Engineering has something to sell; let's sell it!

A guest editorial by E. Finley Carter, Vice-president Sylvania Electric Products, Inc., New York, abstracted from his remarks before the Western Convention, IRE, Long Beach, Calif., with the hearty concurrence of the Editors of Tele-Tech.

RADARSCOPE

Revealing Important Advances Throughout the Spectrum of Radio, TV and Tele Communications



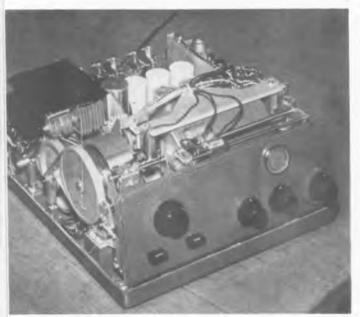
MILITARY PROCUREMENT

SIGNAL CORPS PROCUREMENT REORGANIZED

-Signal Corps Supply Agency, Philadelphia, has reorganized its procurement setup, effective now, reflecting changes in requirements and progress in equipment production. A major change was the elimination of the "Contract Division" and establishment of an Awards Division and a Production Division. The Awards Division takes over former Contract Division responsibilities; the Production Division is designed to expedite and monitor production and delivery of equipment now being manufactured. The new organization also transfers administration of all contractual matters to the Signal Corps regional offices in New York, Chicago, Los Angeles and Ft. Monmouth, New Jersey. This is a major procurement reorganization affecting Signal Corps procurement of electronics, as well as other items. Reorganization chart and details are given on a following page.

NEW HORIZON

SUPERCOLD TECHNOLOGY—Already industry is shipping liquid oxygen (-297°F.) in tank cars, and new supercold techniques are finding everyday uses. In communications, a potential possibility is the use of



New automatic telephone recorder offered by Bell System operates from 110 volt ac supply, and costs \$15 for installation plus \$12.50/month. In operation, subscriber makes one-minute "talk out" record on magnetic drum. In subscriber's absence announcement is played to caller, after which a 28-second period is provided for the caller to leave a message. Recording drum can accommodate 20 consecutive messages. Beep tone is sounded at the start and disconnect finish of the 28-second period. Since equipment is attached directly to the telephone line, receiver is not taken off hook during exchange of messages

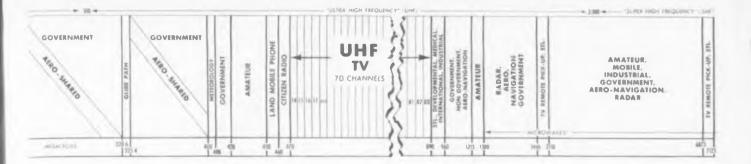
refrigerated crystals to pick up radio signals too faint to be detected by a heated tube. This possibility is suggested by the superconductivity of a number of metals and crystals at extremely low temperatures. When the atoms are either "stopped in their tracks" or their motions ordered to conform with each other, by such low temperatures, internal friction among them is largely eliminated, and current flows easily. Moreover. undesirable electrical signals due to thermal motion of the atoms are suppressed and the crystal is thus more sensitive as a detector. Since communication and control processes usually involve low energy levels, elimination of thermal noise makes possible more delicate measurements and detection. The radio industry is already acquainted with some of the benefits of low temperatures, through its use of refrigerated traps for achieving a vacuum. Vapors driven out of metal tube elements in the process of manufacture will collect on a cold surface faster than they could be removed by pumping; liquid helium traps may be suitable for rapid evacuation during the production of high-performance tubes.

SUPPLIES

STEEL MAKING FACILITIES added to the capacity of the country's steel making plants during 1951 can make enough steel for 1,000,000 television sets, 1,000,000 autos, 800,000 refrigerators, 10,000 freight cars, 1 aircraft carrier, two heavy cruisers, 500 tanks, 3000 six-room houses, 10,000 aircraft, and 500,000 half-inch steel shelves. Even after making all these things 6000 tons will be left over. Reading figures like this makes us wonder why TV and Radio steel allocations have to be cut down. It makes us wonder perhaps that some of the cut-backs in Radio Electronic production are not more for appearances sake than dictated by necessity.

TV MOTION PICTURES

COOPERATION FEUD! It is interesting to note that while the motion-picture industry is bitterly opposed to the release of recent-vintage feature films for TV broadcast use, (vis-a-vis the current struggle with the government on the release of 16mm stock ordinarily for use by armed forces, churches, hospitals and schools), yet continually declining box-office receipts have led to an arrangement between the movie and the radio-TV industries whereby each will plug the other's wares. Radio and television broadcasts include daily listings of current motion pictures as well as movie-personality shorts and interviews. The theaters boost TV programs in film trailers, and mention radio-TV's part in their regular program mailings and posters.



TELEVISION X-RAYS

SCANNING X-RAY SYSTEM developed by Prof. R. J. Moon of the University of Chicago is capable of producing an image which will show the wrinkles in the skin of a finger, as well as outline the bone structure. Scanning arrangement permits exposure to 0.01% of amount of X-rays required by standard apparatus for equivalent picture. The device's suitability for photographic recording of moving objects suggests studies of high-speed mechanical equipment. Operation of the tube at 53,000 v., 30 to 50 ma, depends on an electron beam from a TV-type scanning gun striking a tungsten target which emits X-rays. These rays pass out of the tube through a small hole in a metal shield, through the object being examined, and on to a crystal of calcium fluoride. The crystal in turn transforms the X-ray pattern into a pattern of bursts of ultraviolet rays which are picked up by a photomultiplier tube. The amplified impulses go to a picture tube, enlarging the image.

MANPOWER

ENGINEER SHORTAGE will get worse next year, warns ex-President Herbert Hoover, himself a distinguished engineer who did much to guide radio development in the 1921-1929 period. "We do not have enough engineers in incubation to carry on the nation's work," says he. "We need 60,000 new technologists a year to supply national needs. Our engineering graduates have dropped from 50,000 in 1950 to 38,000 in 1951. And the students in training indicate less than 30,000 next year." Mr. Hoover adds that one reason for the drop is that a young mechanic with three years of training, during which he is paid, can earn more take-home pay after taxes than a young engineer with six years of training and three years more of experience.

RADAR

RADIO INTERFERENCE aboard Navy vessels is caused by radar systems 56.3% of the time, according to engineering reports covering the investigation of 217 interference complaints. The next two major offenders are radio transmitters, 15.6%, and motor-generator sets for radio equipment, 11.5%. Statistically broken down another way, 88.5% of the complaints are attributed to radio and electronic sources, 10.1% to electrical equipment, and 1.4% to interior communications. Suggested methods for reducing the interference to radio reception are: 1) Utilize shielding offered by bulkheads by using separate wireways for electronic and electrical equipment; 2) Isolate high level and low level leads; 3) Orient antennas for minimum coupling; 4) Shield antenna leadins; 5) Replace dc motors with ac motors where possible.

COMPUTERS

MAN BEATS MACHINE! And it's a good thing too. considering the almost human qualities being attributed to electronic computers. Winner and still champion is Electronic Computer Corp. prexy Dr. Samuel Lubkin Runner-up is Dr. Lubkin's non-sentient brainchild, the 240-tube digital computer Elecom 100. The contest centered on a game of Nim, which requires several piles of marbles. Each player must remove one or more marbles from one pile only. The player who picks the last marble off the table wins the game. Explains the victor, "The machine removes the number of marbles which leaves a combination placing it in a winning position. Once it achieves this position, it can't lose. But the machine doesn't think. It just does as it was told, and since I know what it will do, I don't let it get in a winning position." With due respect to Dr. Lubkin's victory, it should be noted that one of TELE-TECH's editors, as well as several other engineers, succumbed to the "brainless" machine in the contest of Nim-



Engineers designing new UHF television installations are showing increasing interest in the use of waveguide for transmission purposes. Experimental test set-up at Allen B. DuMont Labs, shows standard 5.75 x 11.5 in, guide with two right-angle bends which do not affect tine's operation. Favorable comparison with slightly less expensive coax points up the following: 1) Extremely low attenuation of 0.05 to 0.1 db/100 ft., 2) excellent vswr of about 1.01, 3) no reflections from faulty center conductor, and 4) no spurious modes above 750 MC

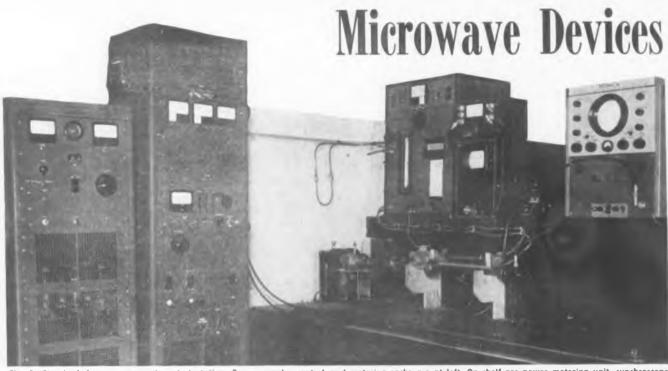


Fig. 1: Standard Amperex magnetron test station. Power supply, control and metering racks are at left. On shelf are power metering unit, synchroscope, r-f monitor and spectrum analyzer. Mounted above bench are magnetron under test, waveguide components, slotted section, wavemeter, and water load

By MARKUS NOW OGRODZKI,

Amperex Electronic Corp.
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THE quantity testing of magnetron oscillators frequently presents special problems in microwave instrumentation. Commercially available instruments designed for laboratory-type measurements at microwave frequencies are, in many cases, not suitable for speedy and economical operation by semiskilled personnel and do not always lend themselves to quantity testing procedures. On the other hand, the comparatively high cost of a magnetron tube, even in quantity production, prohibits the lowering of accuracy standards on the production test station and the consequent danger of decreasing the percentage production yield by the unnecessary rejection of salable tubes.

Two qualities of most magnetron oscillators make it possible to simplify the measuring instruments appreciably on the test station without sacrificing the accuracy of results. These are the inherently high power levels generated by the magnetron and the comparatively narrow frequency band which is of interest for most magnetron types. The high power levels propagated along the microwave transmission line on the test station make it possible to employ relatively large quantities of r-f power for measurement purposes without upsetting the accuracy of output-power measurements. The relatively narrow bandwidths encountered in magnetron testing permit, on the other hand, the construction of comparatively simple apparatus designed specifically for a given magnetron test station, without the complications in design and execution arising from the broadbanding attempts usual in laboratory-type instruments.

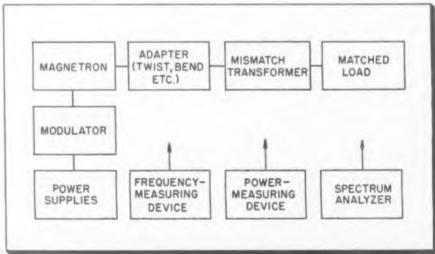
A photograph of the standard Amperex magnetron test station is shown in Fig. 1. A block diagram showing the elements of a magne-

tron test station is presented in Fig. 2. The connections of the power- and frequency-measuring instruments to the magnetron output transmission line have purposely been omitted. The interest in this article is focused on microwave devices, i.e., devices designed either to measure magnetron properties in the microwave region of the spectrum or activated by the microwave power output of the magnetron under test.

Visual Indication Wavemeter

A cavity wavemeter, well suited to production measurements of magnetron resonant frequencies, has been developed for the $X_{\rm B}$ band (6250-6700 Mc). Pictured in Fig. 3, it consists of a cylindrical cavity system

Fig. 2: Elements of a typical magnetron test station, measuring instruments to output line omitted



for Magnetron Production Testing

Economical measuring devices take advantage of two magnetron properties: high power and narrow bandwidth. Neon bulb indicator employed in wavemeters and power monitors for X-band and S-band systems

of conventional design placed in the transmission line ahead of the water load and operating as a transmission-type wavemeter. The cavity, designed for operation in the TEo11 mode, is coupled to a section of RG-50 U waveguide. Instead of the conventional crystal diode and milliammeter combination, a neon bulb is coupled to the output of the wavemeter. As a result, an indicating system without inertia is obtained, so that a flicker of the neon bulb can be observed whenever the cavity is momentarily tuned to the magnetron output frequency as the micrometer head spindle is moved, however rapidly this may be done by the operator. A sketch of the system is shown in Fig. 4.

Principal Advantage

The main advantage of the device, as pointed out above, lies in the fact that it obviates the necessity for slowly "hunting" for resonance by the operator, a drawback of circuits using a meter as an indicating device. Another advantage is the ruggedness of a neon bulb as compared with a crystal diode from the standpoint of burnout, and the low replacement cost of the neon bulb. By tuning the wavemeter for maximum

brightness of the neon bulb glow, a frequency measurement accurate to within 1 Mc can be obtained, which is adequate for this application. A similar instrument was developed for X-band operation, using RG-52 U waveguide.

R-F Output Sampling

The high power levels generated by the magnetron oscillator can be used to advantage whenever a sample of the energy is required, particularly for injection to the spectrum analyzer. The usual method, which makes use of a directional coupler, appears unnecessarily costly and complicated in test setups utilizing a water load for the matched transmission-line termination. A simple method found adequate in Sband (3000 Mc) work is the placement of an N-type connector with an antenna probe extending into the waveguide approximately one-quarter guide wavelength from the water load end plate, as sketched in Fig. 5a. The r-f power extracted in this fashion from the water load certainly does not detract from the accuracy of power measurements when average power levels of the order of 300 watts or more are involved, and the pick-up probe does not disturb the match of the load, whose voltage standing-wave ratio (vswr) remains less than 1.05:1.

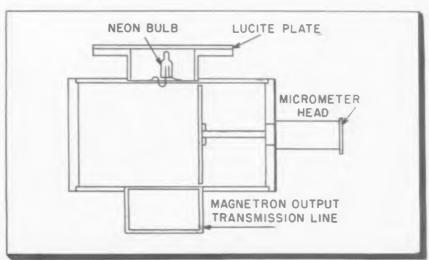
A variation of the method described above is shown in Fig. 5b. where the water-carrying glass tube in the load has been made to extend through the bottom wall of the waveguide, so that a standard waveguide flange could be brazed to the end of the water load section. An attenuating disk is then clamped between this flange and a standard waveguide-to-coaxial transition, the diameter of the coupling hole d being used to determine the amount of microwave power available at the output of the transition. This design has been used in the 6300 MC range. and, again, the error in measured power is of the order of 0.5%, while the match of the entire system at the magnetron output terminals is 1.05: 1 in vswr.

High-Dispersion Wavemeters

For frequency-difference measurements, viz., measurements of magnetron r-f spectrum bandwidth and magnetron pulling figure, wavemeters of comparatively high dispersion may be required. Laboratory instruments of this type are costly and, particularly in the case of longer wavelengths (say, 10 cm), not always readily available. Use can be made, however, of the comparatively narrow frequency band of operation needed, and conventional cavity wavemeters can be designed to operate over a limited range without recourse to complicated mode-sup-(Continued on page 110)

Fig. 3 (1) Visual Indication wavemeter, Note neon bulb in center of standard flange. Fig. 4: (r) Sketch of cavity wavemeter with visual indicator





The WJZ-TV Auxiliary

Emergency broadcast antenna atop Empire State Building uses four tor assemblies to obtain good pattern circularity. Skewed arrange-

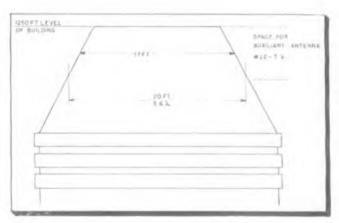


Fig. 1: Top of Empire State Building Is frustum of cone

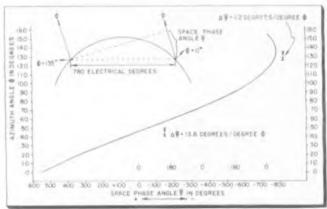
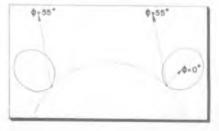


fig. 2: Plot of computed space phase angle and azimuth angle

By JOHN PRESTON, Director of Engineering Facilities and General Services, American Broadcasting Co., 30 Rockefeller Plaza, New York, N.Y.

THE achievement of a good degree of horizontal pattern circularity from a TV broadcast transmitting antenna is not particularly difficult when the antenna radiating elements can be mounted on or made a part of a supporting structure which is of small cross-section in terms of wavelengths at the operating frequency. For example, a simple turnstile type antenna mounted on a slender supporting pole is capable of producing a horizontal radiation pattern in which the total variation from maximum to minimum does not exceed approximately 3 db. As the support structure cross-section is increased in size, the pattern circularity problem rapidly becomes formidable, particularly if one confines his consideration to the more conventional types of radiating element configurations. To further illustrate, the supporting structure for the WJZ-TV main Empire State antenna is only

Fig. 3: Pattern of radially outward beam



wavelength in cross-section, and even this small cross-section, we have found recently, poses serious pattern circularity problems. These pattern problems are currently under intensive investigation.

Design Problem

ABC was fortunate in securing rights to erect a permanent auxiliary TV antenna for emergency operation at the very uppermost location on the Empire State Building. We were, however, faced with a vexing antenna design problem from the point of view of horizontal pattern circularity.

Fig. 1 shows the upper part of the Empire State Building—the frustum of the cone—and the space which was available for the WJZ-TV auxiliary antenna. At this location, the building cone is approximately 17 ft. in diameter, slightly over three wavelengths at WJZ's channel 7 operating frequency. The approximate diametric distance between the radiating centers of antenna elements which might be placed around this cone is about 20 ft. or 3.6 wavelengths, as shown on the sketch.

To explore the principles of design of this auxiliary antenna, let us assume that four antenna radiating elements will be uniformly spaced around the periphery of the cone, and that all four elements will be fed electrically in phase.

The more critical factors affecting pattern circularity will now be considered. The sketch on the upper left corner of Fig. 2, a plan view of a sector of the cone, shows the relative position of two of the four radiating elements-at the points marked z = 0 and z = 135. The elements are physically separated by approximately 780 electrical degrees. As the azimuth direction ; is varied, the relative lengths of the paths from the widely separated adjacent radiating elements to distant points do not remain equal but rather vary with ... The difference in these path lengths gives rise to a phase angle which we

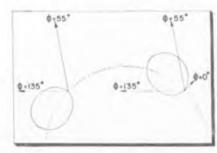


Fig. 4: Skewing element patterns around the supporting structure prevents deep nulls

will call space phase angle 2, as shown on the sketch. The field intensity at a distant point results from the vector combination of the fields from the adjacent radiating elements, which fields differ in phase at the distant point by the amount of the space

Antenna

asymmetrical corner reflecment prevents deep nulls

phase angle. The graph on the lower right portion of Fig. 2 is a plot of the computed space phase angle, along the abscissa, against azimuth angle \$, along the ordinate.

It may be seen from this curve that the space phase angle varies quite rapidly with azimuth angle through most of the sector from $\phi = 0$, to p = 135. For example, in the vicinity of $\phi = 40^{\circ}$, the space phase angle is varying approximately 13.6 '/ degree of azimuth. The auxiliary abscissa scale indicates the effective magnitude of the space phase angle variation. The phase angle goes through four excursions between 0' and 180 over an azimuth sector of only 70 This is the villain which has heretofore resulted in severe horizontal pattern nulls. It is only on the nose of this curve, in the vicinity of z=135 that the space phase angle variation is small—about 1.2° / degree of azimuth.

In practice it is necessary that we let the radiation patterns of adjacent antenna elements overlap, otherwise nulls in the horizontal pattern of the array would result due to absence of any field from either element in some azimuth directions. If the element patterns are beamed radially outward as illustrated in Fig. 3, the pattern overlap will occur in azimuth regions, for example in the vicinity of \$\div = 55\div \div \text{, where the space phase}

angle varies rapidly. Severe pattern nulls will of course result from the rapid excursions of the space phase angle between 0 and 180° in such azimuth regions.

The Skew Principle

If the element patterns are skewed around the supporting structure in pinwheel fashion as shown in Fig. 4. the overlap of adjacent patterns can be made to occur in azimuth regions where the space phase angle variation with azimuth is small. In the case illustrated, the pattern overlap occurs in the vicinity of $\phi = 135$ where space phase variation of only 1.2 degree of a was found. The large space phase variation in the vicinity of $\Rightarrow = 55$, for example, is now harmless since only one radiating element contributes a significant field in this direction. It is by use of this skew principle that deep nulls in the horizontal pattern of the array can be avoided. It was on this principle that the design of the WJZ-TV auxiliary antenna was based.

The WJZ-TV array now atop Empire State consists of four asymmetrical corner reflector antenna assemblies skewed around the cone as outlined in Fig. 5. The radiating element in each antenna is a coaxial half-wave dipole projecting outward at an angle of approximately 80 from a tangent to the cone. This is



Fig. 6: Front view of corner reflector with coaxial dipole minimizing lightning danger

referred to as the angle of skew. The asymmetrical corner reflectors serve not only to achieve the required horizontal shape of the skewed individual patterns but also to minimize excessive high angle radiation and thereby increase the horizontal power gain of the array. The elements are driven in phase. Through this design, power gain of unity and horizontal pattern circularity of ± 3 db have been achieved in spite of the three wavelengths diameter of the mounting circle.

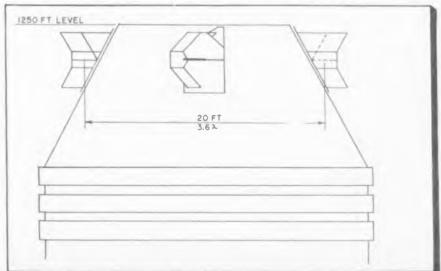
Figs. 6 and 7 show front and rear views of one of the corner reflectors and dipole elements. It should be noted that the folded type of coaxial dipole tends to minimize danger of lightning damage to the antenna and feedline insulators.

Development of this array was undertaken through cooperation of the Andrew Corp. and the American Broadcasting Co., and was carried out under supervision of M. W. Scheldorf of the Andrew organization.

Fig. 7: Rear view of one antenna assembly



Fig. 5: WJZ-TV array consists of four corner reflector assemblies skewed around cone



Core Materials for Small

Extremely thin strips of new Hipersil reduces weight and losses of transformers for airborne electronic equipment. Special grooving technique increases mechanical rigidity

By C. C. HORSTMAN Specialty Transformer Dept. B estinghouse Electric Corp. Sharon, Penna.

Forces during World War II and since, and especially during the present period of rearmament, have greatly accelerated the improvement of characteristics and reduction in size of small transformers and other iron-cored components. With the rapid advances in the science of electronic equipment, transformer development had to keep pace. This not only involved the development of new magnetic materials, but also new methods of utilization. During World War II there was a great acceleration of the development of high-frequency transformers and of thin-gauge Hipersil cores !

The rapid advances in core material and the increasing strictness of core-material specifications have been based on grain-oriented silicon steel and wound Hipersil cores. The original development of Hipersil* was directed toward obtaining a

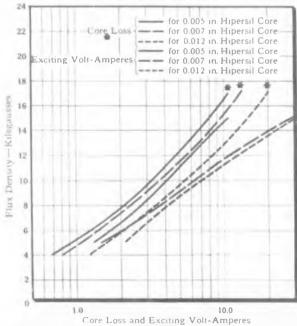
core material with increased permeability and lower hysteresis loss in order to achieve a balanced, economical design of a power or distribution transformer. The permeability was increased at operating inductions by raising the "knee" of the saturation curve. This was achieved by the process of obtaining preferred orientation.

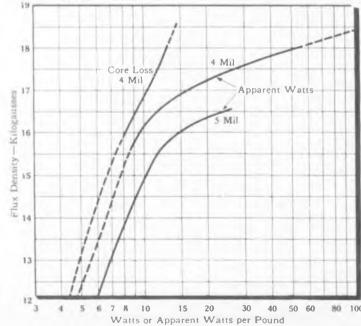
Directions of Magnetization

A single crystal of silicon steel consists of a body-centered, cubic structure. Since it is a cube, there are three possible directions of magnetization: (1) along the cube edge, (2) along the cube-face diagonal, and (3) along the cubic diagonal. The easiest direction of magnetization is along the shortest path. or edge, of the cube, and the aim in orienting the crystal structure is to obtain as many of the cube edges in one direction as possible. Grain orientation is obtained by control of the rolling and heat-treating processes, and, very importantly, maintaining high purity of the silicon steel. The rolling process sets up certain strains in the crystal lattice. By controlling the rolling reductions, the strains are such that when recrystallization on subsequent heat treatment occurs, most of the cube edges lie in the rolling direction. By this means, the "knee" of the saturation curve is raised considerably. Oriented steel has low loss and high permeability in the direction of rolling. It, therefore, requires fewer ampere turns to obtain a given flux density in the material. This has given the transformer designer a wonderful tool with which to reduce cost, size, or obtain better performance.

Designers of airborne electrical apparatus commonly employ 400 cycles, instead of 60 cycles, to help with their everlasting problem of reducing weight. This demands a core material possessing high per-meability and low loss at this frequency. This led to the development of methods of orienting the grain of strip thinner than the 29-gauge (14 mils) commonly used in power-frequency transformers. As the gauge of silicon steel is reduced, although the permeability decreases and the hysteresis loss increases, the eddy loss decreases up to a point more than enough to offset them. The first step in this direction was the crea-

Fig. 1: (1) Comparison of 7- and 5-mil Hipersil with 12-mil material. Fig. 2: (r) Core loss and exciting energy of 4- and 5-mil Hipersil cores





Transformers

magnetic amplifiers and and temperature stability

tion of seven-mil thick oriented Hipersil cores during the early years of World War II. Continued work in this field brought a five-mil oriented steel, which, when made into the Hipersil core, gave the best balance of magnetic performance with economy of design. The fivemil Hipersil core has been the standard for obtaining minimum size and weight in 400-cycle transformers since 1945 and is being used in most of the airborne components being built by the military today. The curves of Fig. 1 illustrate the improvement in weight and size characteristics that can be obtained by using the five-mil Hipersil core in standard 400-cycle power components

With the emphasis on miniaturization, a program was started three years ago to obtain a superior core material that would enable the transformer designer to make his components still smaller and lighter. The limitation with the standard oriented Hipersil cores in working them at high induction in small components has always been excit-ing current. If the transformer is worked at much above an operating induction of 15 kilogausses at 400 cycles, the exciting current becomes so large in comparison with the load current that the regulation is so poor as to make the transformer no longer operable. Recognizing this, the U.S. Navy Bureau of Aeronautics initiated a program of development for a superior magnetic material and core that would eliminate this exciting current limitation. Out of this has come a new type of Hipersil material possessing a very high permeability at high operating flux density. Cores made from this material have been developed through a cooperative research program with Armco Steel Corp., Westinghouse, and the Navy Bureau of Aeronautics.

The new material is four mils thick and has such a high degree of orientation that the minimum dc permeability is 1800 at a magnetizing force of 10 oersteds. Some samples have had a permeability as high as 1860. Theoretically the best



Fig. 3: Transformer at left, using 4-mil Hipersil, is 15% smaller than similar 5-mil unit



Fig. 4: Typical group of airborne, hermetically-sealed transformers using 4- and 5-mil Hipersil cores

permeability of pure single crystal under these conditions is 2015, but because of the slight impurities in the steel the best possible due to orientation is 1940. Core loss and exciting volt-ampere characteristics of four-mil Hipersil cores are shown in Fig. 2, and show their advantages at flux densities of over 17,000 gausses. The reduction of size and weight of 400-cycle transformers possible with the four-mil material is shown in Fig. 3.

Four-Mil Cores

As an example of what can be done with the new four-mil cores, during the past year a certain airborne electronic equipment was redesigned, using four-mil cores for transformers and other components. The resultant weight saving on the iron-cored components was 40%. This saving, of course, cannot be

credited solely to the four-mil Hipersil core. Some is due to redesign and new performance specifications made possible by the use of this new four-mil material. The four-mil cores will have a distinct place in the development of miniaturized, high-temperature-rise transformers for airborne equipment. Some of these are shown in Fig. 4.

One of the most interesting and rapid developments of magnetic materials has been in that used for pulse transformers. These are used in radar equipment to transmit square voltage waves of short duration and high frequency. These last from a fraction of a microsecond up to several microseconds. The transformer must be capable of transmitting these steep front waves with great fidelity. The core material in a pulse transformer is the key to its performance, and, in or-

CORE MATERIALS (Continued)

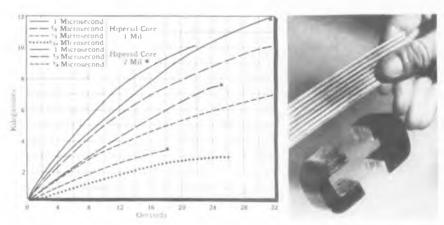


Fig. 5: (1) Comparison of effective permeability of 2- and 1-mil Hipersil cores. Fig. 6: (1) Extremely stable type-C core and a strip of the ribbed Hipersil steel from which it was wound

der that the transformer be made even reasonably small, the core material must have high permeability and low losses over a wide frequency range. In this type of transformer small size is essential for high fidelity.

For pulse transformers during World War II, Hipersil cores were developed and orientation achieved in material as thin as two mils without seriously affecting hysteresis loss. It was decided quite early in the development that thinness of gauge, high de permeability, and low coercive force were the three criteria of performance for the core material. With advances in radar equipment, pulse lengths became shorter and shorter. This meant that, to achieve the ultimate in design performance in the pulse transformer, the material had to be thinner and still retain the high permeability characterized by oriented silicon steels. The purpose of the development that followed was to obtain good orientation in one-mil thick material. The one-mil steel is now being used regularly in some of the advanced radar and allied electronic equipments.

Core for Short Pulses

The figure of merit for a transformer core material of this type is the effective permeability with high rates of change of flux with respect to time. The definite superiority of the one-mil core for the very short pulse lengths is shown in Fig. 5.

As advances in the electronic art call for high-permeability cores for higher and higher frequencies, the material will have to be rolled thinner than one mil. Samples have already been prepared experimentally down to as low as one eighth mil thick, although at these thick-

nesses there is a considerable sacrifice with respect to coercive force and hysteresis loss. However, the development of the magnetic material can be counted on to keep pace with progress in electronic equipment.

To utilize these extremely thin materials effectively in transformer cores. it is necessary to make a wound-type core. The material is slit into a narrow ribbon, wound on a mandrel of required window dimensions, annealed as a unit, and then impregnated solidly with a plastic or resin compound to bind the laminations together. The wound core is then cut into two pieces to allow assembly with formwound coils, and the core halves butted together with a low-reluctance joint. This is the most economical way to handle thin-gauge materials. Space factors, the ratio of the volume of core iron to the volume of core space, are high-90% for five-mil cores and as high as 89% for one-mil cores, which are much higher than an equivalent stacked core using the same gauge materials. Another advantage of the wound and cut type-C core is that the finished core in the transformer is in exactly the form in which it was annealed. This is an important factor in obtaining the ultimate in quality from these highly-oriented materials. The core is easy to assemble in the transformer coil and saves many man-hours in assembly time.

In 1951 another important development was made in the construction of wound type-C cores, especially in regard to the use of thin magnetic materials. Small lengthwise grooves placed in the strip of material as it is wound into a core add a great deal of stiffness. See Fig. 6. The resulting core is more

stable mechanically and better in performance. The added strength in the core legs due to grooving contributes greatly to the core performance in the transformer in that it is much more stable during temperature cycles. This improvement has resulted in much better production performance for both core building and transformer building with these thin-gauge materials.

The development in thin-gauge, oriented materials has not been entirely confined to silicon steels. Recently, much work has been done in the development of oriented nickel alloys, particularly for magneticamplifier application. The orientation of these alloys differs from that of silicon steel in that a cube face is in the plane of the sheet, making one cube edge parallel to the direction of rolling and another normal to the direction of rolling. This results in a very square hysteresis loop as illustrated in Fig. 7. These square loops are desirable in magnetic-amplifier application. Depending on the power range, the design engineer applies either the oriented silicon or the oriented nickel alloy.

Perhaps one of the most interesting developments of the past year has been the development of small, ultrathin gauge cores for high-frequency magnetic amplifiers or "flip-flop" magnetic components in computer applications. See Fig. 8. This development has both military and commercial significance. Here is a

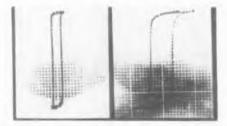


Fig. 7: Square hysteresis loops for (1) 2-mil Hypersil and (1) 2-mil Orthonik nickel-steel

case where the circuit development had reached a point where there was no available magnetic material thin enough to reverse its magnetization with the rapidity required. Armoo Research Labs. in a short space of time succeeded in rolling 3% silicon alloy, 50% nickel alloy, and 79-4 Permalloy down to thicknesses as thin as one-eighth mil. It is truly remarkable that even in these ultra-thin gauges the important magnetic properties of high permeability and low coercive force are retained.

Pilot production cores of this ul-(Continued on page 90)

Q-Meter Correction Chart for

Q Voltmeter Loading

Nomograph corrects errors introduced by shunting effect of vtvm input resistance

By RAYMOND LAFFERTY, National Broadcasting Co. RCA Building, Radio City, New York, N.Y.

THIS nomograph is concerned exclusively with the shunting effect of the vacuum tube voltmeter input resistance that is connected directly across the Q capacitor. Note the basic Q-meter circuit of Fig. 1. This resistance, in parallel with the tuning capacitance, acts to lower the circuit Q as read by the Q voltmeter, thus reducing the measured, or apparent Q, from the true Q of the coil.

The voltmeter input resistance may be measured in the following way: A differential voltmeter of high input resistance can be connected to the Q capacitance terminals and the Q voltmeter alternately connected and disconnected. The increase in voltage when the Q voltmeter is disconnected, is related to the input resistance of the Q voltmeter as follows:

$$R = \frac{Q^2 + 50 \triangle EQ}{50 \triangle E \omega C} \text{ ohms}$$

where Q measured Q with Q voltmeter connected

 ΔE increase in voltage when Q voltmeter is disconnected

C Q capacitance

and w 2nf

The finite input resistance of the differential voltmeter affects only the sensitivity of the measurement.

Another method of measuring the input resistance of the Q voltmeter, simpler perhaps than the previous method, consists of constructing an identical Q voltmeter circuit, substituting a spare voltmeter tube in the Q-meter itself, and measuring the actual Q voltmeter tube in the external circuit by connecting it in parallel with the Q capacitor.

Once the input resistance of the Q voltmeter is measured, other values required for the chart can be obtained directly from the Q-meter.

Example: If the input resistance of the Q voltmeter measures 0.38 megohms at 29 mc, the $F_{\rm mc}R_{\rm meg}$ product equals 11. Assume we have tuned a coil to resonance with 60 muf of capacitance and the apparent Q (Q₁) measures 190. For this particular case we lay a straight-edge on the nomograph between 60 muf and the $f_{\rm mc}R_{\rm meg}$ product of 11. Noting where this line intercepts the reference line, we pivot about

this point and rotate the straightedge to let it pass through a Q_a of 190. The ratio of Q_a/Q_a can be read as 0.95. Thus, the corrected Q equals 100 0.95 or 200.

Fig. 2. is an approximate curve of the f. R... product as measured for the Q-meter used by the author. It is not necessarily representative of other Q-meters.

At low frequencies the input resistance consists mainly of a 100 megohm grid resistor in parallel with a resistance that represents the structual losses within the voltmeter tube. At high frequencies the input resistance is predominately due to transit time loss.

It is important to note that the loading produced by the Q voltmeter is only one of several sources of error. At high frequencies corrections are in order for the internal series impedance of the Q-meter. Then too, the presence of distributed capacitance across the inductor results in an error that requires correction at all frequencies when small values of tuning capacitance are used. A chart for the correction of Q-meter error introduced by distributed capacitance will appear in the next issue of Tele-Tech. When multiple corrections are necessary, they should be made in the order listed above, using the partially corrected values of Q and inductance in succeeding steps.

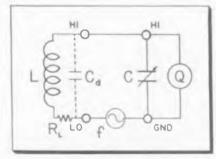
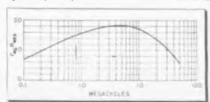
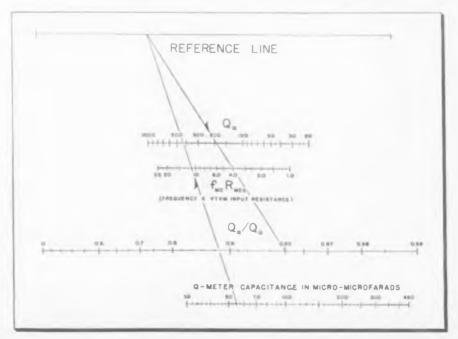


Fig. 1: (above) Basic circuit of Q-meter

(right) Correction chart for loading error

Fig. 2: (below) Curve of measured f. R.





Calibration of Commercial

Service offered to manufacturers certifies overall linearity and attenuator ratio measurements to 2% from 10 kc to 300 mc

By CLARENCE C. COOK National Bureau of Standards Washington, D.C.

BECAUSE of lack of uniformity of the various calibrating methods employed by different manufacturers, it has been necessary to provide an accurate calibration service for commercial field-strength meters to serve as a standard of comparison. For the past 20 years or so this service has been maintained by the National Bureau of Standards and has been available for general use. The original range of calibration was approximately 200 to 1600 kc. About 1946 this range was raised to the upper limit of 20 Mc and later to 30 Mc. More recently', after extensive research and development, calibration of sets covering the FM and TV bands was made possible with the inclusion of VHF calibrations from 30 to 300 Mc. The lower frequency limit was extended to 10 KC. The purpose of this article is to give a general picture of the calibrating procedure employed at the Bureau at the present time.

The field-strength meters dealt with in this article can be divided into two general classes: VLF to HF sets having a frequency range between 10 kc and 30 Mc, and VHF sets whose range falls within the frequency band 30 to 300 Mc. Calibration of a field-strength meter usually consists of three steps: measurement of the antenna coefficient at specified frequencies, measurement of the relative attenuator ratios, and the determination of the overall linear-

ity of the set. Upon request, other tests may be made, such as frequency calibration, stability, bandwidth measurements, and effects of request supply changes.

power supply changes.

VLF to HF sets usually employ a shielded, unbalanced, tuned-loop antenna located immediately above the instrument's case. The attenuator may be entirely in the i-f circuit of the set or it may consist of a section in the r-f circuit as well. Attenuators generally provide step ratios and employ resistive or capacitive elements. VHF field-strength meters use a dipole antenna adjusted to approximately one-half wavelength and supported by a tripod. The antenna is connected to the set through an r-f transmission line 20 to 30 ft. long. The attenuator is of the same types as found in VLF to HF sets.

No Internal Adjustments

It is the policy of the Bureau to make no repairs or internal adjustments on field-strength meters received for calibration. Each set is given a preliminary test to determine its operating condition and to detect any obvious faults which would make a calibration impracticable.

An accurate calibration requires a power source of constant voltage to operate the field-strength meter. If the power supply included with the set is not sufficiently constant, a regulated external supply is used. However, external connecting wires when used, must be positioned to cause no observable distortion or r-f pickup.

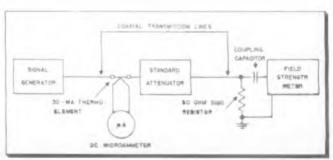
Before a calibration is begun, all equipment to be used is energized

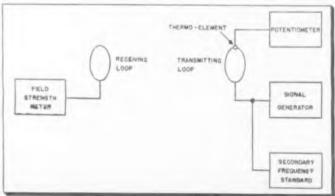
for at least one hour to reach stable operating conditions. The field-strength set is adjusted for normal gain during all tests. On most sets this is accomplished by means of an internal calibrating oscillator, whose output may be coupled into the antenna circuit.

Because of nonlinearity of dynamic characteristics of vacuum tubes and meter movements, it is necessary to determine the relationship between output indications of different values. For calibrating purposes a particular reading of the output indicator is used as a reference for all other readings.

In determining the overall linearity a stable r-f signal generator and a precision standard attenuator are required. A standard signal generator having an unbalanced output and an internal impedance of the order of 50 ohms is used. The attenuator is a 50-ohm, unbalanced, precision standard employing lowinductance resistive elements with a range of 100 db adjustable in 0.01-db increments. A 30-ma r-f vacuum thermo-element in the attenuator input serves as a means of monitoring the generator output and also protects the attenuator from overload. The output of the thermo-element is measured with a dc microammeter. The attenuator is terminated by a 50-ohm disc resistor. The r-f voltage developed across this resistor is loosely coupled to the input of the field-strength meter. Coaxial transmission lines are used between the different pieces of equipment. Fig. 1 shows the arrangement of the equipment during calibration.

Fig. 1: (1) Equipment set-up for determining linearity and attenuator ratios, VLF to HF. Fig. 2: (1) Antonna coefficient measurement using field-standard method, VLF to HF range





Field-Strength Meters

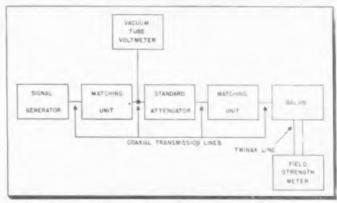


Fig. 3: (1) Arrangement used to determine overall linearity and attenuator ratios in VNF range uses balun and voltmeter monitor

After allowing the equipment sufficient time to become stable and having adjusted the power supply to its proper value, the field-strength meter is adjusted to normal gain. The signal generator and fieldstrength meter are tuned to an arbitrary frequency, usually about 550 κc. The generator output is adjusted for full-scale deflection on the output indicator of the field-strength meter. The output indicator reading, standard attenuator setting and thermo-element output are observed. Maintaining constant output from the signal generator, the standard attenuator is readjusted to give a slightly lower output reading on the field-strength meter, covering the range of the output meter scale in several small steps. Readings of the output indicator and standard attenuator are observed for each step. The corrections for nonlinearit, are computed from the data as follows:

Corrected reading for actual reading of $X = (V_c/V_x)$ CAL where

CAL = Reading on the output indicator which is assumed correct

V_r = Voltage ratio corresponding to the standard attenuator setting required to give a reading of CAL on the output indicator

V_x = Voltage ratio corresponding to the standard attenuator setting required to give a reading of X on the output indicator.

Voltage ratios are obtained from a previous calibration of the standard attenuator.

All attenuator steps are measured relative to one position (usually marked CAL on the instrument) which is assumed to be correct. The equipment and its arrangement used

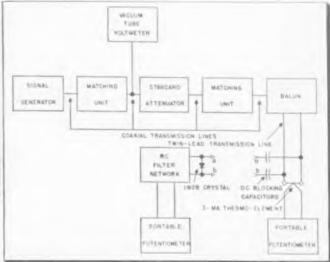


Fig. 4: (r) Calibrating crystal voltmeter used with standard antenna

in the measurement of the attenuator ratios are the same as used in the linearity test. With the attenuator on the field-strength meter on its highest position, the output of the signal generator is adjusted to give a reference reading on the output indicator of the field-strength meter. The output indicator reading, standard attenuator setting, and thermoelement output are observed. Maintaining constant output from the signal generator, the attenuator on the field-strength meter is set to each succeeding step and the standard attenuator readjusted to give the reference reading on the output indicator. Readings are observed for each step of the attenuator.

The relative attenuator rations are computed as follows:

Corrected ratio of attenuator step

$$X\!=\!\!\frac{V_{\rm c}}{V}{\rm times}$$
 CAL where

CAL = Value of the attenuator step CAL which is assumed correct

V = Voltage ratio corresponding to the standard attenuator setting required on the CAL position

 $V_x = V$ oltage ratio corresponding to the standard attenuator setting required on step X.

Antenna Coefficients

There are two general methods² of determining antenna coefficients of field-strength meters: the standard-field method and the standard-antenna method. In the standard-field method the field strength at the receiver is calculated from the dimen-

sions of the transmitting antenna, its current and current distribution, effects of the ground, and distance to the receiving antenna. In the standard-antenna method the field strength is determined from the voltage induced in a standard receiving antenna and the dimensions of this antenna. The standard-antenna method was originally used in the measurement of antenna coefficients of VLF to HF field-strength meters. However, this method was abandoned in favor of the more convenient and equally accurate standard-field method is used now.

Balanced Transmitting Loop

The present setup employs a oneturn, eight-inch diameter, fine-wire. balanced transmitting loop which is mounted in the penthouse on the roof of the Bureau's Radio Building. The antenna is energized by a standard signal generator (85 кс to 40 мс) having a 20-ohm unbalanced output. Special transformers convert this to a 20-ohm balanced output. A portable generator (10 to 100 KC) is used below 85 kc. The frequency of the generator is monitored by a secondary frequency standard having frequency intervals of 10, 25, 100 or 1000 KC. The resulting beat note is maintained within ±200 cycles by aural monitoring. The generator is connected to the loop input through a balanced twinax line. Radiation from this line is negligible over the frequency range used. The antenna current is measured by means of H 100-ma r-f vacuum thermo-element mounted in the loop center. A pre-

FIELD-STRENGTH METERS (Continued)

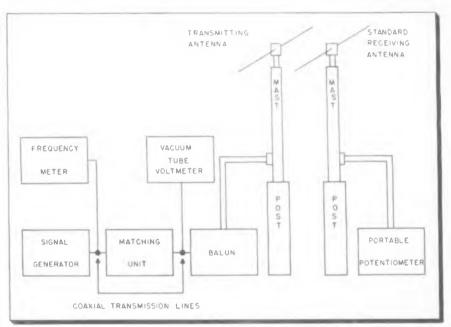


Fig. 5: Measuring antenna coefficient in the VHF range using the standard-antenna method

cision potentiometer measures the dc output of the thermo-element.

All antenna coefficients are measured using an antenna current of 100 ma. The quasi-static magnetic field is utilized. The field-strength is determined by the size of the transmitting and receiving loops, loop current and distance between loops. The equivalent free-space electric field strengths are computed from the following formula:

$$\mathbf{E} = \frac{60\pi \text{ N } \mathbf{r}_1^2 \text{ I}}{(\mathbf{d}^2 + \mathbf{r}_1^2 + \mathbf{r}_2^2)^{3/2}} \mathbf{1} + \left(\frac{2\pi \text{ d}}{\lambda}\right)^2$$

where

E = RMS field strength, $\mu\nu/m$ N = Number of turns in trans-

mitting loop

Transmitting loop current,

µa, rms

 $r_1 = Radius$ of transmitting loop, meters; $r_1 < .02\lambda$

r = Radius of receiving loop, meters

d = Distance between loop centers, meters; d > 10r₁

1 = Wavelength, meters.

The validity of determining antenna coefficients in a quasi-static field in terms of a radiation electric field was confirmed experimentally.

With the equipment connected as in Fig. 2 the field-strength meter loop is properly spaced and the axis aligned with the transmitting loop axis. The generator is tuned to the desired frequency and the output adjusted to give the value of thermo-element output determined by a dc calibration of the thermo-element for 100-ma loop current. The field-strength meter is tuned to the generator frequency and adjusted to

normal gain as before. With the attenuator set so as to give an on-scale reading, the output meter reading attenuator setting and frequency are observed. This is repeated at different frequencies in the range to be covered. The antenna coefficient for a typical make of field-strength meter is computed as follows:

$$K = F'M \cdot E/A$$

where

K = Antenna coefficient

F = Frequency, KC

M = Output meter reading

E = Field strength, $\mu\nu/m$

A = Attenuator setting

Corrected values of output meter reading and attenuator ratios as determined in the two previous tests are used in the computations. The frequency factor, F, was added in the above equation arbitrarily to make the antenna coefficient, K, tend to be independent of frequency.

Calibration from 30 to 300 MC

Certification of VHF field-strength meters is a relatively recent feature of the Bureau's calibration service. It was made possible only after extensive development work on VHF field-strength standards. 1 This work was thoroughly checked by comparison of results obtained from the standard-field method and the standard-antenna method in actual propagation tests at 50, 100, 200 and 325 Mc. The results obtained by the two methods agreed within ±5% at the three lower frequencies and within =10% at 325 Mc. The standard-antenna method was selected as

being the more suitable in regards to accuracy and practicability.

The same general principles apply to linearity tests of VHF fieldstrength meters as are used in the calibration of VLF to HF instruments. However, the higher frequencies make the problem more difficult because connections must be carefully shielded to minimize radiation and impedance matching between the various test components must be rather precise to prevent high losses. The generator used for this purpose is a standard signal generator (40-400 Mc) having an unbalanced 50ohm output and maximum power of about 5 watts. The range 30 to 40 MC is covered by use of a generator similar to the one used on VLF to HF calibrations. The generator output is attenuated by standard mutual-inductance piston attenuator. The dial is calibrated in 0.01-db increments. A broad-band balanced transformer or balun converts from unbalanced to balanced output. This output is applied directly to the antenna input of the field-strength meter by means of the twinax line supplied with the instrument. An impedance matching unit is used on each side of the piston attenuator, Output of the generator is monitored by a high-frequency vacuum-tube voltmeter Coaxial transmission lines are used to connect the various components of the setup.

For the linearity test the equipment is connected as shown in Fig. 3. The generator is set to an arbitrary frequency, usually 100 mc, and the field-strength meter is tuned to this frequency. Except for the use of the piston attenuator, balun, and the voltmeter monitor instead of the decade attenuator and thermo-element monitor, the test procedure and computations for VHF linearity tests are identical to VLF to HF tests.

Measurements of the relative attenuator ratios on VHF field-strength meters are made in the same manner as on VLF to HF sets except for modifications specified in the preceding test of overall linearity. The equipment is connected as in the linearity test (Fig. 3). This applies only to attenuators in the i-f circuit, however. R-F attenuators are calibrated by making antenna coefficient measurements on each attenuator step. This precedure is covered in a later section.

The determination of antenna coefficients of VHF field-strength meters necessitated the location of a field site which would be free of radio interference over the VHF range and would consist of level ground having no large objects nearby which might

(Continued on page 96)

Signal Corps Procurement Changed

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Contracting Division Shuffled; Regional Offices to completely administer all contracts

THE Signal Corps Supply Agency in Philadelphia, Pa., from where nearly all Signal Corps procurement is done, has effected a major reorganization of the Procurement Group.

The important changes resulting from the reorganization include the activation of a Production Division and an Awards Division in lieu of the former Contracting Division; creation of an Economics Branch in which activities relative to pricing and financial matters are combined; and concentration of responsibilities pertaining to Government Furnished Property and Facilities in a newly organized Property Branch.

Division evidences the increasing emphasis placed upon securing prompt delivery of equipment to

along both commodity and functional lines with a view towards obtaining the benefits of both types of systems in the placement of con-

Under a new policy, Regional Offices will completely administer all contracts within their respective geographical areas except those covering crystals, batteries and certain selected equipments. Officers located in the Regional Offices will henceforth assume complete responsibility.

Letters are being issued to all Signal Corps contractors holding open orders advising them of the nature of the change and informing them of the transfer of contract administration and includes appropriate instructions

sponsibilities as at press time, is shown in the accompanying chart.

PRODUCTION DIV. AWARDS DIVISION Establishment of the Production RADIO BRANCH TELEPHONE & TELETYPE BRANCH the Government. MAJ P S DAVIS, Chief Est 165 M E TAYLOR Chief Ext 643 The Awards Division is organized **PURCHASES BRANCH** CONTROLLED ITEMS BRANCH SIGNAL CORPS REGIONAL OFFICES RESPONSIBLE FOR COMPLETE ADMINISTRATION OF SIGNAL CORPS CONTRACTS EXCEPT THOSE FOR Contracting CRYSTALS, BATTERIES AND CERTAIN SELECTED EQUIPMENTS NEW YORK CHICAGO LT COL E P BOYNTON. CO LT. COL L V. GERMAIN. CO. PHOTOGRAPHIC CENTER PROCHREMENT OFFICE The new organization and its re-LARORATORY LOS ANGELES PROCUREMENT OFFICE IT COL J & BURKE Compiled by Lt. Col. Stanley Gerstin, Consulting Editor, TELE-TECH; Vice President & General Manager, Caldwell-Clements Manuals Corp.



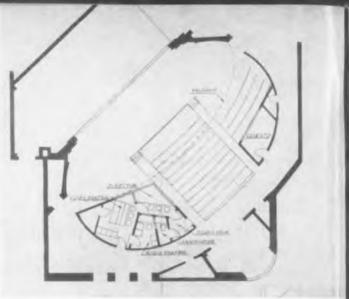


Fig. 1: (1) Early WARD control room has director, audio and video men in one room. Production problems result from high noise levels, possible confusion, and difficult audio monitoring. Fig. 2: (r) New TV studio plan shows split control booth, separating directing, audio and video functions

Television Control

Split arrangement segregates directing, video and audio functions to in undisturbed atmosphere. Application of plan to large, medium and

By R. D. CHIPP
Director of Engineering
DuMont Television Network
515 Madison Ave., New York, N.Y.

THE arrangement of equipment in Studio Control Rooms and Master Control Rooms is generally determined by two broad factors: (1) the equipment selected, and (2) the program requirements. As these vary, so will the control room layout vary. At the same time, some degree of standardization is highly desirable. It is proposed to discuss several facets of this basic problem. First, the growth and development of what we refer to as the DuMont Standard Control Room will be described. Next, it will be shown how

this applies in different ways to three different types of TV broadcasting stations.

Consider some of the qualities which a studio control room should have:

- (a) Visibility of monitors
- (b) Visibility of staging area
- (c) Aural communication between members of production and technical staffs
- (d) Visual communication between members of production and technical staffs
- (e) Equipment location for ease of operation
- (f) Equipment location for ease of maintenance
- (g) Easy access to the studio area Logically, a control room should, if possible, combine these qualities,

consistent with equipment budgets and minimum personnel requirements.

The fundamental functions that take place in a control room are audio, video, and direction. In early control rooms, these three functions were generally placed together. A frequent arrangement consisted of a console in the front row, at which video control technicians and the audio control operator were seated. A raised desk in the rear was used by the program director and the technical director or switcher. Although there were variations of this arrangement, they were alike in that all functions were located in a single space.

Undivided Control Room

Fig. 1 shows the control room of Studio A at WABD. In this particular arrangement the program director and the audio man were in the rear row, and the video control operators and switcher were in the front row. Technically, this set-up is quite satisfactory. However, from the production standpoint there are disadvantages. Among these are:

(a) High ambient noise, consisting of a mixture of program audio, talk on intercom, talk on outside telephones, talk between personnel in the course of their duties.

(b) Confusion in the event of equipment trouble, with increased

Fig. 3: Split arrangement of Ambassador Theatre TV control room, layout shown in Fig. 2





Fig. 4: Photograph taken from audio section of Ambassador studio. Announce booth is on left, director's section and staging area ahead. Division of control functions allows undisturbed work

Room Layout

provide efficient operation small studios illustrated

chance for personnel errors.

(c) Difficult audio monitoring.

Several years ago when first converting the Ambassador Theatre in New York into a TV studio, what was called a split control booth was developed. Fig. 2 shows a floor plan of this theatre. Note that the audio, video and direction functions previously mentioned are separately divided. In addition, an announce booth has been added.

The peculiar shape of this particular control room is caused by the existing structure of the theatre, and it did complicate the design considerably. The section in the front contains the program director and the switcher only. In front of them are camera monitors, preview monitors, and line monitors. Directly in back of the switcher is a separate booth containing the audio operator. To the right of the audio

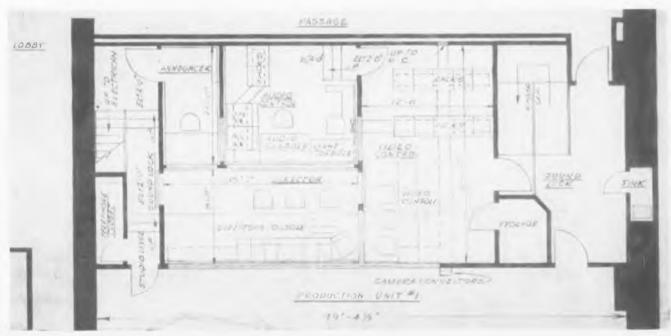
operator is the announce booth, and to his left is the video control section. These spaces are connected by doors which are normally kept closed.

Glass windows permit the audio operator to see the announce booth on his right, the video control booth on his left, and the monitors in the director's room in front of him. He also has an excellent view of the acting area. The announcer, likewise, can see the audio operator on his left, the camera monitors and the acting area. The director, of course, has a full view of the acting area and the monitors.

The video control operators, who normally concentrate on the camera control units, do not necessarily need to view the studio, although it can be helpful at times. For example, on one occasion an accident on stage caused several lights on a set to go out. The operator quickly checked the studio by turning his head, before making any unnecessary camera adjustments and calling the camera operator on the intercom.

This arrangement has proved to be extremely satisfactory. The production staff, as well as the technicians, have found that this segregation has permitted smoother, more trouble-free operation. In the event of camera trouble, the director does not hear instructions passed from video control to camera. Likewise, the director does not hear conversations between studio control and master control, checking levels or line difficulties. The audio man can set his speaker volume as high as necessary for proper monitoring

Fig. 5: Standard control room as it would be laid out where no constructional limitations exist. Director and switcher are in front, audio in rear



TV CONTROL ROOM (Continued)

without disturbing other members of the team. The director and switcher have audio monitoring facilities that can be adjusted to suit their need and can work in a relatively undisturbed atmosphere.

The split arrangement at the Ambassador studio is shown in Fig. 3. The director's booth is in foreground, announce booth left rear, audio control center rear, and video control right rear.

Fig. 4 shows a photograph taken from the audio section showing the announce booth on the left, the director's section and staging area ahead. Note the director's monitors.

Minimum Equipment

This type of layout requires minimum added equipment in the form of video and audio monitoring. Du-Mont camera control units have two standard video outputs, one of which is fed to the switcher, the other of which is fed to the added camera monitor in the production section of the booth. Audio speakers, with separate monitor amplifiers and gain controls, are placed in the video control section and the production section of the booth. This scheme was quite successful, and was developed further in the planning for the new 67th St. studios in New York.

Fig. 5 shows this standard control room as it can be laid out where

there are no construction restrictions. The same general arrangement has been followed: the director and switcher in the front, the audio and announcer in the rear, and the video control section on the side. The production and video section are two feet above studio level, and the announce and audio section are four feet above studio level. Adherence to this arrangement in all new studios has been attempted, although certain modifications appear to be desirable at certain type stations.

Dual Studio

Fig. 6 shows how this same layout has been adapted to a dual studio set-up. Here space requirements forced the elimination of the announce booth on this floor level. It has been placed on a second level overlooking the studio. This type of control room layout is primarily designed for use in a station that is a network origination center and presumes a rather elaborate master control and projection room. Individual film cameras, the new Du-Mont film scanners, and other program sources will be fed directly to the studio control room. Film scanners or projectors will be started and stopped, slides will be changed. remotes will be cued and switched from the console in the production section of this studio.

A control room of this kind may be adapted to a station of smaller size, having two live studios, and using network and film. For this purpose plans for the new Hotel Raleigh studios at the DuMont station WTTG in Washington will be examined.

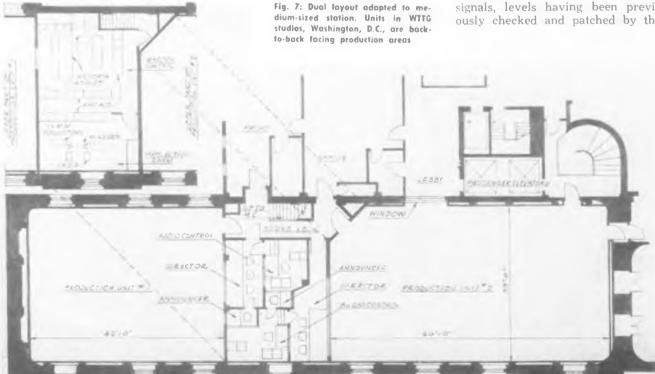
Network Feeds

In general, such a station combines a great deal of network feeds and film programs, with local live programs that do not require extensive rehearsal. Fig. 7 shows how units on the lower floor of the two-story structure are placed back to back as in the case of the dual arrangement in the New York studios. The basic change to the standard control room is that master control and studio video control are combined.

Such a plan still provides the proper segregation of the three functions, audio, video and production, and yet, at the same time, permits a variety of programming without the need for additional personnel.

Network to Live Program

Assume that a live program is immediately followed by a commercial film spot and then a network feed. At the conclusion of the live show the projector audio will appear on the studio console, and the video operator in master control will turn in his chair and handle the film camera controls. At the conclusion of the spot, network audio and video signals, levels having been previously checked and patched by the



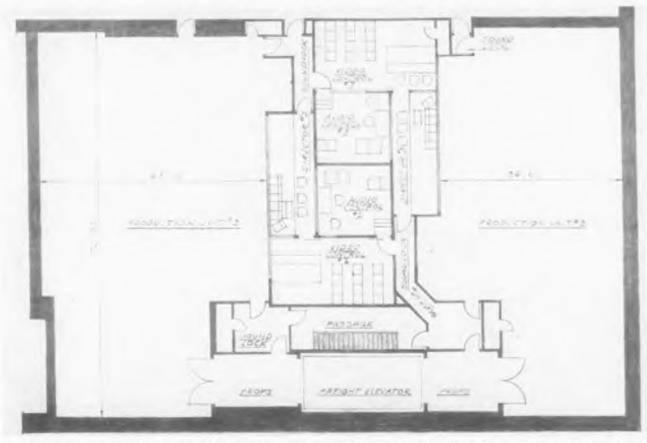


Fig. 6: Standard layout adapted to dual studio set-up. This type of control room is primarily for a station that is network origination center

technical supervisor, will feed directly through the master control section and be monitored at that point. This frees the switcher and audio man for another rehearsal or other duties.

Small Station

Now, finally, let us consider the type of station that depends on network feeds and film only for its program material. In this case it seems desirable to combine all operating functions at a master control point provided the arrangement allows for proper expansion at the time studios may be added.

Thus, although film and network can be easily handled at a common point, a separate studio control is highly desirable, particularly if live programs and rehearsals of any degree of complexity are contemplated.

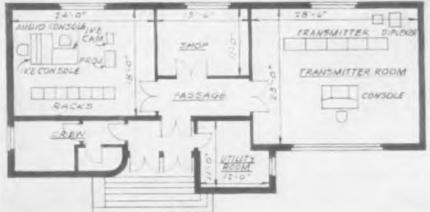
Original Transmitter Plant

Fig. 8 shows a floor plan of the original WDTV, Pittsburgh, transmitter plant, constructed in 1948. One man at the film console handled all video control and switching. Remote controls on the DuMont flying spot scanner, line amplifier and stabilizing amplifier are brought out at the film console. Thus all shading controls, gain and pedestal controls, slide change buttons and video switching controls are placed for ease of operation. Film monitors in the console are in front of the operator, and scanner and line monitors are rack mounted on his right. The audio console, directly in front of the video console, contained audio feeds from turntables, network, film and announce booth. The audio operator faced the rack mounted video monitors. The only additional technician needed to supply complete programming was the projectionist. A fourth technician remained on duty at the transmitter console, and a fifth man had overall supervision and was free for relief or to fit in where needed in an emergency.

Three Examples Covered

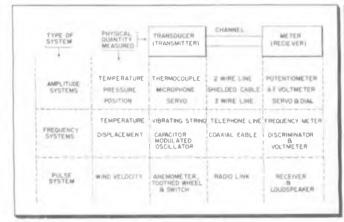
Three examples of control room layouts and some of the associated problems have been covered. Many arrangements can be designed to suit the needs of any particular station, and these needs will of course, vary with the type of equipment used and the type of programming desired. Based on broad and varied experience at DuMont, it is believed that these three basic layouts constitute an efficient use of space, equipment, and manpower.

Fig. 8: Floor plan of original WDTV transmitter plant, Pittsburgh, shows small station layout



Telemetering and Direct Frequency

Communications engineering techniques applied to remote measurement systems. Comparative evaluations made of operation, accuracy and time of AM and FM instruments



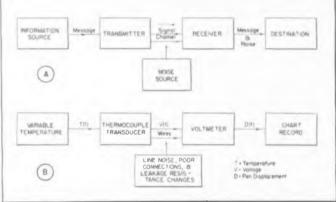


Table 1: (I) Examples of instrument systems for remote measurements. Fig. 1: (a) Elements of electrical and (b) instrument communication systems

By PAUL M. ERLANDSON Southwest Research Institute 8500 Culebra Road San Antonio, Texas

MORE and more, problems of instrumentation concern themselves with communications over large distances. Manufacturing plants may be controlled wholly or partly from central points where the results of many measurements are available. In guided missile test flights or in operation of nuclear reactors, remote measurements are absolute necessities.

The great majority of communications systems are electrical and have the elements shown in Fig. 1A. The message from the information source is converted into a signal by the transmitter. The signal is sent along a channel to the receiver, which converts the signal to a message acceptable at the destination.

These elements may be compared with those of a typical instrument communication system, as shown in Fig. 1B. The information source is some system where the temperature. T(t), varies with time. The message introduced into the transmitter or transducer is therefore a time-varying physical quantity. The transducer, a thermocouple, changes temperature variations into voltage variations, V(t), which constitute the electrical signal.

The signal is transmitted over a channel, which in the illustration may consist of ordinary wires. Electrical noise is unavoidably introduced into the channel by poor connections, nearby wires carrying other voltages, variable line leakage, changes in line resistance due to temperature, etc.

Both signal and noise reach the receiver, in this case a voltmeter which is part of a chart recorder. The signal is converted into a message which is displacement, D(t), of the chart recorder pen as a function of time. Each displacement of course corresponds to a certain temperature, depending on the errors introduced by noise, etc. The final destination of the information is the chart.

The process illustrated is actually communication between two machines—yet it is governed by the same laws as, say, telephone communication between two persons. Many of the practices and ideas of communication engineering are found to be of increasing value in instrumentation as the latter becomes more complex.

In radio and TV, signals in which the carrier frequency is varied or modulated have been found to be more useful for many purposes than signals in which the carrier amplitude is modulated. Advantages have also been found for signals where the carrier is turned on and off at intervals or pulse modulated. The principal reason for such benefits in

FM and PM is that most channel noise disturbances between the transmitter and the receiver are variations in amplitude, and this noise can be effectively suppressed by receiver of FM and pulse signals. Fig. 2 presents typical examples of MA, FM, and PM signals for the transmission of a message which might consist of four different values of the pressure of a gas. There are other modulation systems, but those shown are the principal types.

Five Basic Systems

In the language of instrument engineers, basic systems of telemetering are sometimes classified into five systems: Current, Voltage, Frequency, Impulse, and Position. In a review of these types of instruments. it has seemed impossible to justify this many categories. It is suggested that the most general categories are three in number: Amplitude Systems, Frequency Systems, and Pulse Systems. Subdivisions of Amplitude Systems could include current, voltage, or position as pertinent. This suggestion is open to discussion of such matters as phase systems, which find the least in common between instrument and communications practices.

Before listing factors of importance in this evaluation, it is of interest to introduce several ideas from communication engineering practice.

The channel in most instrument

Measurement

PART ONE
OF TWO PARTS

systems, very often consists of ordinary wires. It has not been too expensive to use separate wires for each measurement. Thus, this element has been given little consideration in the design of transducers or receivers or meters. As the distances over which instruments must communicate grow, channel considerations become more important. Even over short distances, transmission of a large number of measurement messages may benefit from channel design beyond ordinary wires.

Channel Time Inexpensive

In wire or radio communications, channel time has always been relatively expensive. Thus, it is not surprising that much time and effort has been devoted to development of systems which can transmit the maximum amount of information during the shortest possible time over the least expensive channel. Recent advances in communication theory have shown that more messages can be sent over a given channel in a given time if each message does not need to be absolutely correct. This theory, which is statistical in nature, may be expected to influence instrumentation in time.

To evaluate overall systems, then, we must take account of the following factors:

1. Overall Measurement Accuracy: This factor, expressed in percent of the measured value (not in percent of full-scale instrument reading) may be evaluated in terms of the

value of the measurement. It may not be as important as time or reliability in some cases.

2. Measurement Time: This factor is primarily important in relation to use of the measurement for control purposes and in relation to the speed of the process being measured. If a given measurement can be made fast enough, the transducer might be arranged to send a signal each time a prearranged change occurs in the quantity being measured, rather than at regular intervals. This might save channel time as well as recording chart space.

3. Measurement Reliability: This is measured as the percent of total measurements which are actually within the desired limits of accuracy. In systems where data are averaged, 100% reliability may not be necessary. "Fail Safe" is a consideration.

4. Message Presentation: This is evaluated in terms of operator skill and effort necessary to obtain and interpret the output data or message. An instrument which indicates the square of a current value may be less useful than another which reads current directly. A device which requires adjustment of controls and observation of a null indicator may be less satisfactory than an automatic device, particularly for control or recording purposes. Quantitatively, these properties can be evaluated in terms of the labor costs they incur and the contribution of human errors toward reducing accuracy and measurement reliability and increasing measurement time.

5. Cost: This factor is determined quantitatively by the actual value of the measurements and the time over which they can be made under original specifications of the above quantities. Included here is the cost of maintaining and checking accuracy, which involves performance under adverse operating conditions: the frequency that recalibration is required, the difficulty of recalibration, and the availability of calibration standards. Since cost is usually inversely proportional to size and weight, the latter are classified here.

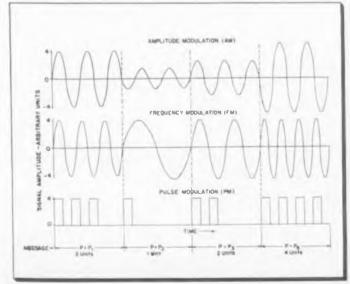
To correlate and simplify the results of the foregoing, it will be easier to speak of an instrument communication system as composed of a transducer, a channel, and a meter—remembering that the transducer serves as a transmitter and the meter as a receiver. Table I lists examples of amplitude, frequency, and pulse systems used for remote measurements. An attempt has been made to secure a variety of combinations of elements, and not to represent any particular advantages or disadvantages of a given system.

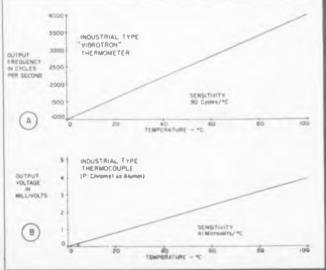
Type of Modulation Used

The type of modulation to be used in any system depends primarily on available transducers and meters. Most of those available use AM, probably because so many convenient meters and recording devices are available. It is quite likely that the lack of transducers using FM and PM systems is due to a previous scarcity of meters for converting FM and PM signals directly into meter readings.

Southwest Research Institute has devoted considerable attention to FM transducers. One of these is the (Continued on page 86)

Fig. 2: (1) AM, FM and PM signals for four values of pressure. Fig. 3: (r) Comparison of (a) frequency and (b) amplitude transducer characteristics





CUES for BROADCASTERS

Practical ways of improving station operation and efficiency

Conelrad Alarm

JAMES F. LAWRENCE, Jr., Chief Engineer, KMGM, Culver City, Calif

THE circuit operates with any receiver using Avc. Plate and filament voltages can be taken from the receiver or from a separate source. Operation is as follows: negative Avc voltage applied to the grid of the first section of the 6SN7 reduces the current through R, to a very low value. In this condition, the voltage across the potentiometer is nearly equal to the B supply voltage, a portion of which is applied to the second grid. This positive voltage on the grid tends to counteract the bias voltage developed across the cathode bias resistor R. and allows sufficient plate current to flow to just hold in the relay. If the carrier of the station to which the receiver is tuned is cut, the Avc voltage will be removed from the grid of the first section of the 6SN7 which will draw plate current and in turn cause the voltage across the potentiometer to decrease because of the increased IR drop across R. The voltage on the grid of the second section will no longer be high enough to balance out the cathode bias voltage and the plate current will be reduced, allowing the relay to open, completing the bell circuit and at the same time opening the cathode circuit so that restoration of the Avc will not stop the alarm bell until the reset button has been pressed.

\$\$\$ FOR YOUR IDEAS

Readers are invited to contribute their own suggestions which should be short und include photographs or rough sketches. Typewritten, double-spaced text is preferred. Our usual rates will be paid for material used.

Voice Video

BOB HOLT, Chief Engineer, KATE. Albert Lea, Minn.

Here is a guidance and fails to attract attention at special based as sta-ERE is a gimmick that never cial events in which broadcast stations frequently find themselves involved. The observer sees and hears his own voice repeated by depressing a button and speaking into a mike in an unattended device. A tape puller is required with three heads and an oscilloscope-if desired. Our Presto works very nicely by switching around the heads and setting the puller upside down on the edge of a table out of sight of the viewers. The reels are removed, and one is used as a weighted pulley for the bottom of a continuous loop of tape. The recordable time and delay depends on the length of the loop.

The display seen by the viewer is a "magie" box with only a speaker grille and the face of the scope showing. He speaks into a conveniently located mike while holding the "press to talk" switch. Upon releas-

ing the button his voice comes back over the speaker and can be seen on the scope. The machine is set to record and runs continuously without attention. A small sign with instructions is helpful.

Rejuvenating Old Discs by Applying Lubricant

H. BROOKS, WKLX, Lexington, Ky

Some old records were acquired to be used on one of the WKLX record shows. Some of the discs dated back as far as 1920, and had been treated rather badly, so the noise level was very high. We used the following process to reduce the surface noise to a level at which the discs could be used.

First, we washed the discs with warm water and mild soap, and rinsed thoroughly. After drying with a lint-free towel the surface noise was found to be considerably lower. But, still too high for broadcast use. Then we cleaned the discs with carbon tetrachloride and anplied a liberal coat of vaseline. After removing the excess vaseline and playing through once to remove the lubricant from the grooves the surface noise was found to be sufficiently low. Application of a lubricant to the disc is used only in extreme cases but a good washing is helpful any time and does not damage the disc. Discs treated with a lubricant must be protected from dust.

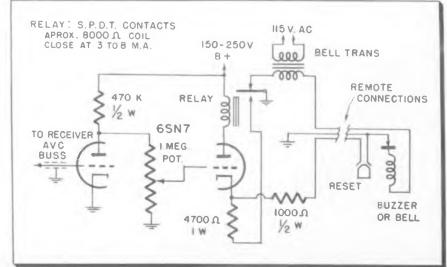
Cuing Instantaneous Recordings

RAY WILLARD, WISL, Mount Carmel, Pa.

To provide a foolproof means of cuing an instantaneous recording without "back-tracking" or counting grooves from a certain spot on the disc, we use a method that has proved satisfactory here at WISL. Because instantaneous recordings are usually made on a soft surface and must be discarded because of break-down of the grooves due to back tracking, this method greatly lengthens the life of a record by eliminating the necessity for cuing.

Before beginning the spot announcement, modulate the disc with a 1,000 cycle tone for a few moments and follow this with two turns of silence on the disc and then im-

Another variation of a Conelrad alarm using easily available radio receiver



mediately begin whatever is to be recorded. Do this at the start of each cut and once a habit is established it provides a simple and easy method for the control room operator to cue a recording prior to placing it on the air. It is only necessary to play the recording on audition to the spot between the end of the tone and the beginning of the intelligence, stop the disc and let the pick-up rest at this point until air time.

Disc Reverberation

J. B. STRAUGHN, 107 Woodbridge Ave., Silver Spring, Md.

A simple way of introducing a variable amount of reverberation into music and speech coming from a disc is to mount a second pickup wired in parallel with the main pickup and place its stylus behind the main stylus. Depending on the displacement between the two styli the re-echo will be long or short.

If desired, a number of pickup mounting holes can be drilled in the top of the turntable mounting and used to provide a variable degree of delay according to the type of program in use. This type of delay is suitable for all types of recorded programs.

Pad Storage

CECIL TANKERSLEY, Chief Engineer, WMOG, Brunswick, Georgia

HERE is an excellent way to keep pads safely and know the exact impedance and loss of each. Remove the tops from a number of discarded metal tubes, clean out the inside of the base, and remove all leads to the prongs. Tubes with at least pins 1, 2, 7 and 8 intact should be used, and all connections should be made to these pins to standardize the setup.

Construct pads from resistors of the proper value for the desired impedance and solder the input to one set of pins, say 1 and 8, and the output to the other set of pins 2 and 7, then crimp the top of the tube back in place. Paste a gummed label showing the db loss and impedance on the outside of the tube shell, and there is a handy pad that can be handled and stored without fear of resistors being torn loose.

A number of these pads can be made up for future use. One shorting pad should be included with connections from 1 to 8, and 2 to 7. For use, mount two octal sockets on a strip, with binding posts at each end. Connect the input of the first socket to pins 1 and 8, and the output pins 2 and 7 of the first socket to 1 and 8 of the second socket and pins 2 and 7 of the second socket to the output binding posts. You now can easily set up various values of loss and impedance. If only one pad is needed, the shorting pad may be placed in the extra socket.

Sump Pump Switch

LLEWELLYN JONES, Chief Engineer, WSBA, York, Pa.

THIS idea is a little out of the broadcast line, but we have been troubled by water seeping into our basement. On two occasions, the switch on the sump pump failed to operate due to rust and corrosion in the switch. As a result our basement was flooded. The damage: three motors shorted and a transformer waterlogged. To prevent additional mishaps of this kind, an emergency control was connected across the regular start-and-stop switch. Relay A is energized when the water level rises to contact AA. Contact AA is an aluminum rod mounted on an insulator extending about four inches from the bottom of the well. When the water reaches the height of contact BB, also an aluminum rod, relay B closes, holds through its own contacts and relay A contacts. The pump runs until the water level falls below contacts AA, thus de-energizing a relay A, releasing relay B, and stopping the pump. (Ed. Note: owing to danger of high voltage line being exposed the aluminum rods should be run inside larger plastic tubes for insulation.)

Cleaning Tape Recorder Mechanism

HAROLD H. NEWBY, Chief Engineer, KAKE, Wichita, Kan.

ENGINEERING maintenance men at KAKE have found that cotton tipped swabs such as "Q TIPS" are very convenient for cleaning tape recorder heads, drive pucks and idlers. They are readily available at almost any drug store. The swab may be dipped in whatever cleaning fluid one prefers and the excess flipped off. We find this much more satisfactory than trying to use a piece of cloth wrapped around a stick or screwdriver blade.

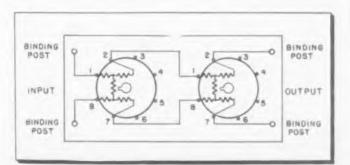
Remote Control for Studio Amplifiers

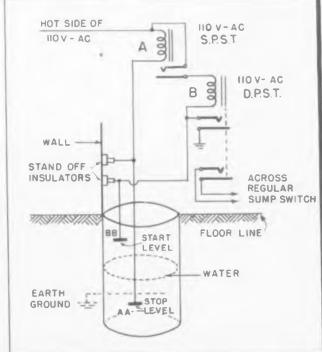
R. S. HOUSTON, Chief Engineer, KNBZ, La Junta, Colo.

In cases where the only engineering staff is at the transmitter, leaving the studios completely in the hands of relatively non-technical personnel, there arise times when it is impossible to obtain the desired circuit setup for special (Continued on page 84)

Failure-proof automatic sump-pump switch makes use of water conduction ->>

Metal tube cases make sturdy plug-in pads





Second Detector S/N Improvement

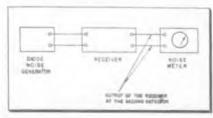
Consideration of division of noise into ac and dc components in pulse radar linear receivers eliminates errors in calculating noise figures

By LEONARD S. SCHWARTZ Hazeltine Electronics Corp. 58-25 Little Neck Parkway Little Neck, N.Y.

THE specification of receiver sensitivity is intended to insure desired performance, but this performance may not be attainable within the limitations set by "the state of the art." All too often this fact is discovered the hard way—by constructing the receiver and finding that it does not and cannot be made to meet performance requirements. A much more economical way of discovery would be to examine the design itself, in advance of construction, to see whether or not it is practicable.

A criterion of practicability is the noise figure of the receiver because it is known that, granted the "state of the art," a certain noise figure is the best attainable. Since the sensitivity and the noise figure are intimately related, it should be possible to find the latter knowing the former. In the past the only valid, though uneconomical, method of finding the receiver noise figure was to construct the receiver and make measurements. There is a frequently used method of calculating noise figure from the specification which defines sensitivity in terms of a signal-tonoise indication on an oscilloscope. but this method yields erroneous results because it overlooks the division of noise into dc and ac components in the output of the second detector. The key to the valid assignment of receiver noise figure rests upon the proper understanding of the action of the second detector with regard to this noise division. It is the purpose of this paper to

Fig. 1: Installation for measuring receiver noise figure. Meter reads receiver noise with zero output from noise generator. Generator output is increased until meter reading is doubled, so output equals noise of receiver



show that such understanding leads to a definition of noise figure that meets the test of experimental results. The discussion is confined to pulse radar types of linear receivers and to signals as large or larger than average peak noise. The noise as well as the signal is assumed large enough to cause the second detector to operate in its linear region.

Second Detector Operation

A linear detector with zero fixed bias is specified by the relations: I(t) = 0, V(t) < 0, and $I(t) = \alpha V(t)$ V(t) > 0, where V(t) is the input voltage, I(t) is the output current, and α is the constant of detection. If the signal at the input to the detector consists solely of noise and if the detector has unit load impedance, the following relations apply:

$$V_{GC} = \frac{(V_{n+f}(t))^2}{\sqrt{2\nu}}$$

$$(V_{GC}^2)^{\frac{1}{2}} = \frac{1}{\nu} \left(2 - \frac{\nu}{2}\right)^{\frac{1}{2}} |V_{n+f}(t)|^2 + \frac{1}{\nu}$$

$$= \frac{1}{\sqrt{-2\nu}} |V_{n+f}(t)|^2 + \frac{1}{\nu}$$
(2)

where $V_{\rm dc}$ is the dc noise voltage at the output of the second detector, $(V_{\rm n}^2)^{\rm dc}$ is the rms low frequency noise voltage at the output of the second detector, and $\overline{[V_{\rm nf}(t)]^2}^{\rm dc}$ is the rms noise voltage at the output of the i-f amplifier or, what is the same thing, at the input to the second detector. The quantity a can, to good approximation, be taken as unity, so it will be dropped from further discussion.

Comparison of Eqs. (1) and (2) shows that the dc component of noise is twice the rms low frequency component. This fact is determined solely from analysis of the Fourier content of the signal and does not arise from consideration of time constants in the output of the detector. In practice the RC load in the output of the detector has a time constant large compared to the period of variation of the i-f components of the input noise signal, but small compared to the period of variation of its envelope. The i-f components of the noise signal in the output will, consequently, be shunted to ground; the dc components in Eq. (1) will fix the bias level on the diode; and the

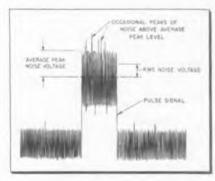


Fig. 2: Oscilloscope presentation of noise and signal. Average peak and rms noise are shown

capacitive coupled output will consist solely of the ac component of the noise given by Eq. (2).

For a pulse signal, if the duty cycle is small, the dc level in the output of the second detector can be neglected, and essentially the entire output signal, excluding i-f energy, is low frequency ac. The signal-tonoise ratio, as viewed on an oscilloscope connected to the output of the second detector, is conveniently expressed in terms of the ratio of pulse signal amplitude plus average peak noise (sometimes called tangential noise) to average peak noise. Symbolically, $N = (V_s + V'_{ac}) / V_{ac}$ where $\stackrel{\wedge}{V}_s$ represents the peak amplitude of the signal (the height of the pulse in the present study, V'_{ac} the average height of the peaks of the noise on top of the pulse, and $\overset{\wedge}{V_{\rm ac}}$ the average height of the peaks of the noise on the base line.

With the aid of this definition and Eqs. (1) and (2), an expression can be derived for the ratio of the signalto-rms noise ratio at the input to the second detector, to the signal-torms noise ratio at the output. This ratio of two ratios is greater than one and represents an effective improvement in signal-to-noise ratio when read on an oscilloscope, a device which is sensitive to the ac components of the output noise only. That is, the improvement in signalto-noise ratio is a consequence of the division of the rectified noise into dc and ac components. The expression for this ratio, termed the

(Continued on page 102)



Fig. 1: Agent set with coded information plate queries storage drum to find seat availability

By CRAIG ANDREWS Teleregister Corp. 157 Chambers St. New York 7, N.Y.

In the early part of July this year, a totally automatic "Magnetronic Reservisor" was put into operation at the American Airlines' reservation office at LaGuardia Field in New York. It represents eight years of joint development by the airline and The Teleregister Corp., the manufacturer, during which the combined outlay went to about a half million dollars.

Before this time, sales agents who carried on business over telephones checked a large board with placards indicating open flight space. Not only was this board, at its best, many minutes behind the sales, but it was very hard to read from the agents' desks. This board showed availa-

"Reservisor"—

A memory drum-computer which checks seat availability on 10,000 airplane flights in a few seconds

bility for only three to five days in advance, and many sales after that period had to go through more paper work and interoffice phone calls.

The Reservisor now presents to an agent, within a few seconds, the immediate ability to check availability, and to sell or cancel, one to four seats of any eight flights at a time in certain combinations from a total of 1000 flights per day for a ten day advance period.

The unit used by the agent, the agent set, Fig. 1, resembles a small desk adding machine. With each agent set there are 46 plates that slide into the set with the flight information written on them. On each plate there are 64 flights, and an operator may see 16 of these with no movement of the plate. The bottom of the plate is coded with slot combinations to enable each plate to pick out one small portion of the stored information from the storage drum. The agent never knows the exact number of available seats in a flight but only that there are enough or not enough seats to make the transaction

The input information from these agent sets is a date, a seat number, the plate coding, and the type of call. This information is locked up in relays as the electronic elements process the call. It should be noted that only one call may be processed at a time, so only one agent set may be connected at a time. To do this each set asks a seeker if it may ask a question. If no other set is connected at this time, the set is connected. If

another call is being processed, it must wait its turn to get an answer. With this system, it takes an average of one second to process a call.

In the control position, there is a set that enables the master agent to read the exact number of open seats left in a flight and where the flight is stored on the drum, or its "address."

Remote from the main installation are other agent sets that may perform the same functions as the local agent sets. These sets operate over a telephone pair and, therefore, may be located as far as is desired from the main storage point.

Two Digital Units

The electronic computer actually is composed of two identical digital units with the same information fed to each and the answers compared for accuracy in the cross-checking unit, Fig. 2. Not only are the answers checked (2), but timing between the two units (1) in several places is also checked. This is done to give a high degree of reliability in the answers. If a disagreement between the two units occurs, a teletype printer will print the input information and the subdivision of the equipment which caused the error. This duplication in equipment makes it possible to leave one unit in service while the other is undergoing major repairs.

The drum storage, 28 in. in length and 20 in. in diameter, is divided into (Continued on page 108)

Fig. 2: Cross-checking unit compares outputs

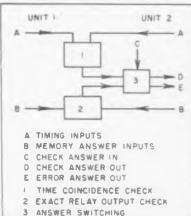
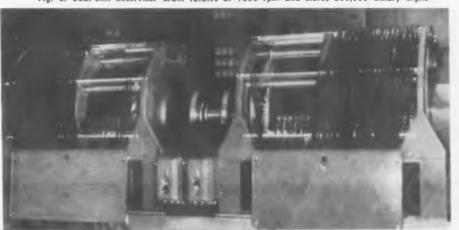


Fig. 3: Dual-unit Reservisor drum rotates at 1200 rpm and stores 200,000 binary digits



Flush-Mounted Antennas

Zero-drag types developed for jet fighters and Functions include distance measuring, communica-

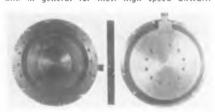
With the advent of high speed jet airplanes, the design of zerodrag, flush-mounted antennas became a necessity, and is today a basic consideration in making these installations. Presented here are representative types currently being used on military aircraft or being developed for use in the near future. With the exception of the DME Pancake and ODR antennas, which were evolved by private manufacturers, all of the units were developed at

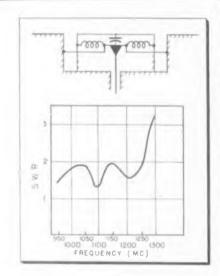
the Wright Air Development Center, Ohio. Their functions include distance measuring, communications, landing approach, interrogation and navigation.

The operating frequencies of the various antennas described here range from 100 Mc for the Biconic Command antenna to 1250 Mc for the Distance Measuring Pancake antenna. The coaxial feed lines are either 50 or 52 ohms, and antenna weights run from 8 oz. to 8 lbs.

Antenna AT-234/APX is a distance measuring equipment antenna and is for use with Radar Set AN APN-34 or similar frequency equipments.
It is the latest standard flush mounted antenna for these equipments. It operates over the frequency range 950-1250 MC, is vertically polarized, and uses 52 ohm RG-8/U or similar cable for connecting the antenna to the equipment. This antenna is gasket-scaled to prevent moisture collection. Antenna AT-234/APX was designed for use on bomber, cargo, fighter and in apparat. This antenna is gasket-sealed to and in general for most high speed aircraft.

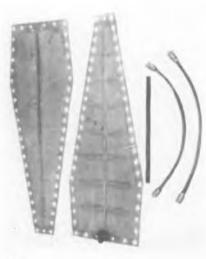
DME PANCAKE ANTENNA

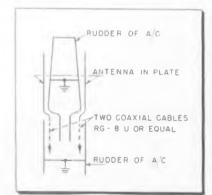




VHF HOMING ANTENNA

Dragless antenna (flush-mounted VHF Homing panels) for use with the AM/ARA-8 VHF Homing Equipment in conjunction with AN/ARC-3

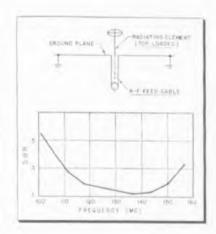




was developed in June 1945. The development of this antenna was necessitated by require-ments for a low-drag article for installation on the jet type aircraft. The operating frequency of this antenna is from 120 MC to 144 MC and normally has vertical polarization. It was designed to operate with a 50 ohm type coaxial cable. The antenna panels are used in pairs. Each panel weighs 1 lb. Dimensions are: overall length, 21 in.; overall width, approximately 0.5 in.; overall depth, 12 in.; length of element, 21 In.; and width of element, 0.101 In.

PICKAY ANTENNA

The Pickax communication antenna is designed for use with the AN ARC-3 equipment. The development of this antenna in Oct. 1944 was



necessary because of the large aerodynamic drag figure of its predecessors resulting in decreased speed and maneuverability of the air-craft. The operating frequency of this built-in antenna is from approximately 100 to 156 MC,



normally has a vertical polarization and em ploys a 50 ohm coaxial type cable. This antenna, described in USAF Specification No. X-7122, or one of similar configuration. Is used on all Air Force aircraft of the jet series. This flush-mounted, 24 oz. antenna has the following dimensions: overall length, 13.5 in.; overall width, 2.5 in.; overall depth, 15.5 in.; length of element, 13.5 in.; and width of ele ment, 2.5 in.

The Pickax antenna is shown mounted on the vertical stabilizer. In operation, this VHF unit is covered with a close-fitting cap.

for Military Aircraft

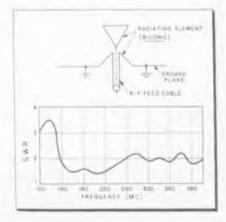
high speed bombers cover 100 to 1250 MC range. tions, landing approach, navigation and interrogation

BICONIC COMMAND ANTENNA

This zero-drag antenna was designed for operation with the Interim equipment AN ARC-13 or its successor. This antenna was developed in the



early part of 1946 to satisfy the requirements of a broadband antenna covering the frequency range of 100 to 400 MC and could be used with the following current equipments: VMF Command Equipment, IFF Equipment, and UHF



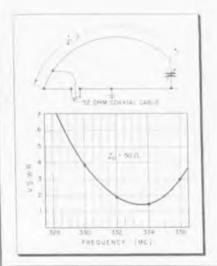
Command Equipment. The antenna was designed to operate satisfactorily inside the normal contours of jet pircraft with 50 ohm coaxial cable. It is described in USAF Specifications No. X-7074 and No. X-7172. The 55 oz. unit has the following dimensions: overall length, 15 in.; overall width, 2.5 in.; overall depth, 21.5 in. (forward-aft); length of element, 15 in.; and width of element, 2.5 in.

ODR ANTENNA

For a picture and description of the operating characteristics of the ODR antenna, turn to page 111

GLIDE PATH ANTENNA

Antenna AT-(XA-113) ARN is for use with Glide Path Receiver AN ARN-5 and R-322 ARN-18 and is in the experimental category. Requirements for dragless flush mounted antennas for high speed aircraft necessitated unusual shapes to fit the aircraft structures. The curved bath tub shape was the radical design necessary for high speed aircraft. The operating frequency is 329 rhrough 335 MC and is horizontally polarized. RG-8, U or similar \$2 ohm coble is utilized in connecting the antenna to the AN ARN-5 receiver through a balun. Unit is described in

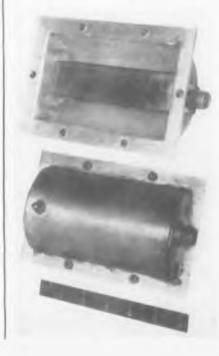


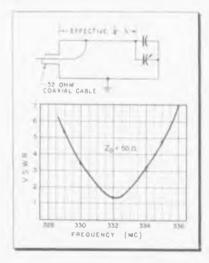


USAF Specification No. X-7196, and is particularly suitable for F-80 type airplanes. This antenna weighs 12 oz. and has the following dimensions: overall length, 7.75 in.; overall width, 4 in.; overall width, and width of element, 8.24 in.; and width of element, 1.75 in.

BATH TUB ANTENNA

Antenna AT-{XA-106}/ARN-5A is for use with Glide Path Receiver R-89 () ARN-5A or R-332/ARN-18 and is in the experimental category. It





is generally similar in application and design to the AT-(XA-113)/ARN. The operating frequency is 329 through 335 MC, herizontally polarized. For connecting Antenna AT-(XA-106)/ARN-5A to the receiver, 52 ohm, RG-8/U cable is utilized. A balun is required for connection to Receiver R-89 ()/ARN-5A. Depending on the mounting surface, the B ez. unit has zero drag. Its dimensions are: overall length, 6.75 h.; overall width, 4.25 in.; overall length, 2.25 in.; length of element, 4-29/32 in.; and width of element, 1.25 in.

High-Power

Linear amplifier delivers 15 kw with over 23 db gain in 470-890 mc band. Demountable cathode-filament assembly permits inexpensive replacement

SEVERAL high-power klystrons have been produced and are seeing service in the 1000 Mc region. These include the V-25 operated at 1036 Mc by the National Bureau of Standards on Cheyenne Mountain, Colo., and delivering 5 kw, and the X-16 which forms a part of the General Electric TV transmitter announced last year.

By extending and refining the techniques utilized in those tubes, Varian Associates, San Carlos, Calif., has developed the V-42 (Fig. 1) which delivers 15 kw with at least 23 db gain over the UHF TV band and is 30% efficient. Bandwidth of the tube is 6 Mc between the 1 db points. Tuning means are included to permit adjustment at least 4' either side of the factoryestablished center frequency. This is accomplished by stretching or compressing the individual resonators, using the locking nuts visible on the side adjusting studs in Fig. 1.

Electrical specifications for the V-42 include a dc beam voltage of 17 kv maximum at 3 amp between cathode and catcher; a dc bombarder voltage of 2400 v. at 0.5 amp between cathode and filament; and an ac filament voltage of 7 v. at 35 amp. The electron beam is collected in a water-cooled catcher requiring a 10-gpm flow at 50 psi while the cathode-filament assembly is cooled by forced air. Having a length of 50 in., the tube weighs 150 lb. without the 100-lb. beam-focussing magnets.

Like the earlier tubes, the V-42 has a demountable cathode-filament assembly designed to permit inexpensive replacement. A cross-section (Fig. 2) through this assembly shows its construction, based on rigid shock- and vibration-insensitive concentric cylinders. The filament is a flat spiral of pure tungsten located behind the dished circular tantalum cathode. The bombarder voltage established between filament and cathode produces electron bombardment of the cathode—in the na-

Fig. 1: Varian's V-42 klystron may be tuned to 4% of factory-set frequency by compressing or stretching resonators with locking nuts

ture of diode operation—heating the tantalum to an emitting temperature. Cathodes of this type give long trouble-free service limited generally only by failure of the filament from evaporation of the tungsten.

This factor is made even more favorable by operating the filament with enough undervoltage to limit temperatures to a point where operating life expectancies of over 10,000 hours can be attained. Upon failure, these tubes can be returned to the factory for economical replacement of parts or of the entire cathode structure. Tantalum cathodes have the advantage that they do not lose their emissivity by poisoning when tubes are exposed to air during such overhaul operations.

Inherent Advantages

In general, klystrons have a number of inherent advantages for application to services of this kind. Due to configuration, the cathode is located outside of the r-f field and far from it by comparison with conventional negative-grid electron tubes. This makes it relatively easy to develop the large-scale source of electrons required for high-power operation and, at the same time, permits use of an ac filament without creating hum difficulties in the signal regions. Also, since current drain from the power supply is independent of r-f level, a regulated or low-impedance source is not required to accommodate modulation peaks. Power-supply ripple presents the most likely problem of spurious modulation, but even the most simple filtering will carry this down better than 60 db below the

Linearity in a klystron is also a point of advantage. Output varies with input as a Bessel function of the first order and first kind. Consequently, output voltage across the load rises to a maximum and then as excitation increases, falls again—eventually to zero. The first portion of this curve is used as show in Fig. 3. For low levels, the curve

UHF Klystron

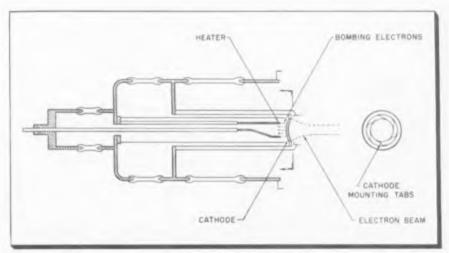


Fig. 2: Cross-section shows demountable cathode structure. Hatched areas are Kovar, clear areas glass

is extremely linear and does not deviate appreciably until about 80% of maximum power. Thus the TV picture signal is undistorted throughout the video region up to the black level. The remaining part of the curve up to full power is used by synchronizing pulses and the nonlinearity is easily accommodated by predistortion or stretching in video circuits ahead of the klystron stages.

No Partition Noise

From a random noise point of view, there is no partition noise to contend with because there are no grids. In physical and electrical arrangement, these klystrons constitute complete final amplifiers in-cluding their own integral tank circuits.

Both safety and water-supply considerations are furthered by the arrangement of the 10 gpm, recirculating collector cooling system in the V-42. The collector is insulated from the body of the tube by a glass seal so that current lost to the drift tube and reaching the collector can be metered. Because the cathode is operated below dc ground potential, both the collector and tube body are at ground. Besides giving maximum protection to operating personnel, this arrangement obviates electrolysis and insulation difficulties.

Fig. 4 shows the physical configuration of a cascade klystron of the V-42 type. The stream of electrons arising in the cathode is directed down the center of the drift tubes shown, being focused by the external electromagnets. R-F interaction with this beam is accomplished in the cavity-resonators, the first of which is excited by the drive which is brought in through the input connection at the top of the tube.

In cascade or triple-resonator klystrons, the first stage can be compared with a voltage amplifier, while the stage between the second and third resonators performs as a power amplifier. When the input r-f

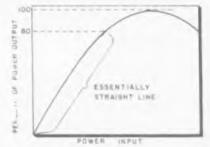


Fig. 3: Bessel function curve of klystron output vs. excitation voltage. Video signals are held within linear left section of the curve

signal excites the first resonator, electrons in the beam are bunched or velocity modulated, thereafter traveling in groups or concentrations. As these bunches pass the succeeding resonators, some of their energy is transferred to these circuits in such a way that useful power can be extracted through the output connection, also brought out the top of the tube. Because energy supplied by the beam current and the collector voltage appears in this output, it is greater than the input and amplification takes place.

Complete isolation between output and input circuits is achieved because pure electron coupling exists. Thus, very high gain is obtained without the need for neutralization. The response curve is shown in Fig. 5. Power gain corresponding with this curve is about 24 db. Bandwidth of a cascade klystron is about the same as that for a single-stage tube, and can be exchanged for gain by either loading the resonators to reduce their Q or by stagger tuning, the latter generally being preferable. The staggertuning scheme used requires no loading of the center resonator.

For power-measuring operations, Varian engineers have developed a new coaxial water load which can be supplied for installation with these tubes so required FCC output readings can be secured quickly and accurately. The unit consists of a 6ft. length of 318 in. diameter line with water connections and two thermometers-one to read incoming water temperature and the other outgoing. Electrically, the new load has an extremely low vswr of 1.1 or better from 470 to 1200 MC.



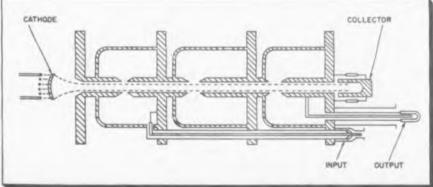
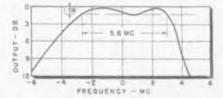
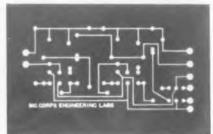


Fig. 5: Response curve for Varian V-42 klystron shows the 6 MC bandwidth between 1 db points





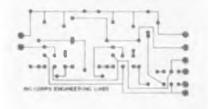


Fig. 1: Printed circuit transparencies. (1) Drawing on frosted acetate using photo opaque. (c) Negative transparency using photo resist. (b) Positive transparency for screen stencil

By WILLIAM BORNEMANN Signal Corps Engineering Labs. Fort Monmouth, N. J.

S ILK screen printing is a process whereby a print is deposited on a surface by forcing paint through the open areas of a stencil affixed to a fine mesh silk cloth. Such silk screen printing covers a broad field of applications ranging from the simple printing of decorative patterns on textiles, to printing conductive paints and etchant resists for printed electronic circuits.

The stencil for the screen may be prepared in several ways, but for the printed circuit applications being considered this stencil can be prepared most conveniently by a simple photographic procedure. The hand manipulation of the screens in printing could well be replaced by screening machines for large production: but, regardless of the degree of mechanization, the same basic principles apply. Accordingly, this article deals with the photographic preparation of the silk screen stencil and with the practical details of the art of screen printing.

As a first step in the preparation of the film type stencil, a positive transparency (black line pattern on

Techniques for Photo-

Particularly suited for experimental and cil is prepared and attached to screen.

transparent plastic base as shown in Fig. 1) is required. These transparencies may be photographic positives or may be hand drawings made with photo opaque on frosted methate.

The hand drawn type of transparency is especially suited for laboratory work since it may be quickly prepared using only common drafting equipment and techniques. This type of transparency may also be very easily altered or replaced if circuit changes are desired. The black line circuit pattern should be opaque or dense enough to block out the light under exposure.

Taping of the transparency is recommended to provide a "safe edge" on the stencil film. This safe edge will prevent the edge separation of emulsion from the backing during subsequent washing.

During exposure, the areas of the gelatin emulsion on the silk screen film which are exposed to the direct light through the positive transparency are hardened slightly and rendered insoluble in water, while those areas which are protected by the opaque lines of the positive transparency remain water-soluble. The film is allowed to soak in water, in the course of which the unexposed portions of the stencil soften and eventually wash out. The film is then mounted on the screen completing the stencil.

All steps in the preparation of a photographic silk screen stencil may be performed in daylight but working in a strong direct light is not recommended.

Silk Screen Film Sensitizing

The use of photographic silk screen film for the stencil permits the printing of the finest detail possible by the silk screen process. One type of commercial film for this purpose consists of a heavy coating of dyed gelatin on a translucent plastic backing. The film as received is not light sensitive and so must be treated with a sensitizer, made by dissolving 20 grams of potassium bichromate in one pint of water. Since this sensitizer will deteriorate with age and exposure to light, it

should be kept in an opaque container (or a brown glass bottle) and renewed monthly.

The initial step in the preparation of the film is the cutting of a piece of film that is at least 1.5 in. larger in both dimensions than the desired stencil. This film is taped smoothly along its outer edge, emulsion side up, to a piece of stiff cardboard (Fig. 2). The sensitizer is applied with a 2 or 3 in. soft camels-hair brush and must be cross-brushed carefully to prevent air bubbles, wrinkles, and streaking (Fig. 3). The next drying step may be done in the open air using a fan, or in a circulating air oven with the heat turned very low. For best results, a constant temperature of 80° to 85 F is desirable together with a relatively low humidity (about 50%).

When the film surface is dry to the touch, it is ready for use and should be used within a few hours. Film not used within 8 to 12 hours should be discarded because the film hardens and will not wash out. The film is removed from the cardboard by cutting the film free just inside the taped edges.

Exposure

A vacuum frame (commercial printer which presses transparency and stencil together) with an arc light is the ideal combination for exposing the film. A contact printer (as shown in Fig. 4) with a strong light source is adequate. During exposure the light must pass first through the back of the transparency and then through the back of the film. Not exposing through the back of the film is the most frequent mistake in stencil making. The order of set-up (using a vacuum frame) would be as follows: First. place the film on the rubber base. emulsion side down; then place the positive transparency over the film, face down; and then close the frame. Using a 20 ampere double arc light at a distance of 30 in., the exposure would be 45 to 60 seconds; or using a #2 photo-flood bulb at a distance of 16 in., the exposure would be 50 to 70 seconds. The film will tolerate up to 50% variation in

graphic Silk Screen Printed Circuits

small-scale production, detailed methods show how sten-Set-up and operation of printing process is described

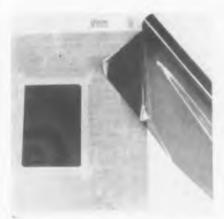


Fig. 2. Before sensitizing, silk screen photo stencil film is taped to a stiff backing



Fig. 3: Sensitizer is applied to film with a very soft camel hair brush, and then dried



Fig. 4: Contact printer used to expose sensitized stencil film to pattern on transparency



Fig. 5: Stencil is affixed to screen by bringing mesh down on stencil, pressing with paper



Fig. 6: Register guides are fastened to the printing base to locate successive base pieces



Fig. 7: Printing medium is poured at end of masked stencil and spread with rubber sque: gee

exposure but it is recommended that test strips be made to determine the best exposure time.

Washing

After the film has been exposed to light, it should be washed immediately. This may be done by placing the film face down in a large flat developing tray filled with water at approximately 110° F. After being allowed to remain face down on the surface of the water for approximately 30 to 45 seconds, the stencil film is turned face up and agitated gently beneath the surface of the water until the stenciled circuit pattern becomes clear. The film may be removed from the water and held to the light for inspection. Washing must continue until there is no trace of dye coloring in any of the lines of the patterned circuitry. The film then is given a second washing in cold water.

Transfer of the film stencil to the silk screen is done immediately after the second washing while the stencil is still wet. The finest definition may be obtained by placing the stencil on a screen of silk of about 150 mesh in such a manner that most of the lines of the patterned circuitry run at 45° angle to the mesh of the silk stretched taut on the screen frame hinged to a masonite-type base.

The stencil is affixed to the screen by placing the stencil face up on the printing base and bringing the screen down with the silk mesh covering the stencil. A clean smooth absorbent paper (newspaper will do) is then laid over the surface of the silk and rubbed gently (Fig. 5). The blotting action of the paper draws the stencil into the mesh of the silk. The screen must not be moved until the stencil is partly dry which usually takes about 30 minutes. The screen may then be raised and allowed to dry thoroughly and the stencil film backing peeled off. Blocking-out lacquer may be used to retouch any holes or unwanted lines in the stencil.

Printing

The silk screen stencil described herein may be used for either printing an etchant resist paint pattern or for depositing a conductive pattern using silver conductive paints. The screening operation itself consists of wiping a liberal (Continued on page 94)

Preview of New Equipment at

Latest developments featured by more than 75 companies at 8th annual

Tubular Twin-Lead

(61

Type 14-271 Amphenol tubular twin-lead maintains constant impedance, almost totally unaffected by weather conditions, and is par-



ticularly suitable for UHF-TV. Nominal impedance is 300 ohms and velocity of propagation is 84%. Attenuation in db/100 ft. is as follows: 30 MC. 0.63; 60 MC, 0.93; 100 MC, 125; 200 MC, 312; 400 MC, 27; 500 MC, 30, 700 MC, 3.6; and 900 MC, 4.2 List price is \$.08./t., and in lengths of 100, 500 and 1000 ft The price is \$7.93, \$35.38, and \$68. respectively.—American Phenolic Corp., 1830 S. 54th Ave., Chicago 50, III.—TELE-TECH

TV Chain Amplifier (102-103)

Model 212TV chain amplifier has twostage wideband circuit which amplifies all TV channels from 40 to 225 MC simultane-



ously without tuning or switching. Ideally suited for TV distribution systems, it has voltage gain of 21 db, maximum output voltage of 6 v., and a response characteristic of ± 2 db, with less than a 0.7 db variation over any TV channel. Intermodulation distortion with 0.5 v. rms output signals is 11 mv rms or —39 db, Harmonic distortion is 2.2% for the second, 0.05% for higher harmonics. The 12-1b amplifier uses twelve 6AK5's, is available with input impedances of 180, 72 and 52 ohms, and output impedances of 235, 72 and 52 ohms. Power consumption is 55 watts, 117 v., 50-60 cycles.—Spencer-Kennedy Labs., Inc., 186 Massachusetts Ave., Cambridge 39, Mass.—TELE-TECH.

Diffraction Loudspeaker

Model 848 Compound Diffraction Projector Speaker System for public address provides 20% increase of articulation index for speech reproduction and 2½ octaves increased range for music. Weatherproof construction provides greater sound dispersion



and efficiency. It utilizes two coaxially mounted horns working from opposite sides of a single diaphragm. Each horn is designed for optimum reproduction within its own range, providing response of ±5 db to 11.000 CPS. Low end response is augmented by 100 CPS horn taper. System delivers 2-2½ octaves more range than usual PA units. Polar distribution pattern exceeds 120° at all frequencies up to 5000 CPS. It is molded of glass fibers and edgewisewound voice coil assembly uses durable phenolic impregnated glass cloth diaphragm. Rated at 25 watts, 16 ohms, 12-lb. projector is 10.5 x 20.5 x 20.5 x 20. in. List price is \$59.—Electro-Voice, Inc., Buchanan, Mich.—TELE-TECH

Vacuum Coupling

(60-B)

No. 94235 vacuum coupling, Cenco Type "CHV", for joining tubular elements in a vacuum-tight system assures maximum con-



ductance of system by the elimination of any constriction in the bore of the coupling. Union is made by hand-tightening a knurled nut which compresses the "O" ring until metal-to-metal contact is reached. Compression is limited to provided maximum life of "O" rings. Coupling fits standard tubings of steel, stainless steel, copper, etc. Permanent connection to the tubular elements may be made by soldering, brazing, or welding. Made in seven sizes from ½ to \$14.35. Similar ½ in. coupling with release valve is available for metal-to-glass connection—Central Scientific Co., 1700 Irving Park Rd., Chicago 13, III.—TELE-TECH

Differential Analyzer

(5-6

L3 GEDA electronic differential analyzer is capable of solving problems of motion and control either by direct simulation or by



mathematical equations. It is built for use in the design of automatic industrial controls, servo-mechanism analysis, pilotless aircraft and trajectory studies. The linear computer solves differential equations to the 12th order. The L3 has 24 high-gain de amplifiers, each with four stages of amplification to give a gain of 200.000. Continuously self-balancing circuit maintains amplifier balance to within 250 av of zero equivalent input. Calibrated plug-in turrets set equation constants. Turrets are supplemented by 18 to 36 potentiometers, permitting the independent setting of 72 to 165 parameters. Complement of 131 tubes contains eight types for easy servicing. Amplifiers used are characterized by wide bandwidth, low grid current and zero drift.—Goodyear Aircraft Corp., Akron 16, Ohio.—TELE-TECH

Wheatstone Megohm Bridge (83)

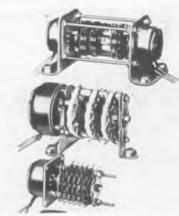
Utilizing a Wheatstone bridge in conjunction with a highly stabilized de amplifie Model 635-A direct-reading instrument pro-



vides accurate measurements through range of 10 ohms to 1.000,000 megohms. Accuracy is ± 1% from 10 ohms to 10 megohms. 2% from 10 megohms to 10.000 megohms to 5% from 10.000 megohms to 1.000,000 megohms. A built-in electronically-regulated power supply provides different voltages for both high and low ranges. Oversize solid-silver contacts in Steatite-insulated switch decks maintain long-life accuracy over a wide temperature range—Shallcross Mfg. Co., Collingdale, Pa.—TELE-TECH

Circuit Selectors

Ledex circuit selectors and stepping relays are used for remote control of multiple circuits. They are operated by rotary



solenoids. have positive detent action and are self-stepping or external pulsing. Choice of wire sizes permits wide range of operating voltages. Solenoids are available in diameters from 1½ to 3¾ in. with predetermined rotation up to 95°. Starting torque for 45° stroke range from 0.25 to 50 lb.-in DC solenoids weigh from ½ to 4.25 lbs.-G. H. Leland, Inc., 123 Webster St., Dayton 2, Ohio.—TELE-TECH

Ponogometer

(91)

Type 394-A ponogometer monitors contact resistance between potentiometer resistance element and contact. Indication is of the Go-No-go type. Threshold resistance is adjustable from 10 to 5000 ohms. Since con-



National Electronics Conference

meeting in Chicago's Hotel Sherman, Sept. 29 through Oct., 1

stant specified value of current is passed through slider contact resistance, knowledge of noise voltage is obtained. Instrument indication is independent of total resistance or angular position of slider from 0 to 100,000 ohms. Power requirements are 40 watts. 105-125 v., 60 cycles. Sensitivity is independent of slider speed from 1 to 60 rpm. Recovery time is less than 1.5 seconds. Nine-tube unit weighs 7.5 lbs., and measures 13¹⁴ × 6¹⁸ × 9³⁴ in.—Technology Instrument Corp., 531 Main St., Acton, Mass.—TELE-TECH

VHF Klystrons

(58-59)

Type 4W20000A (1) 20-kw radial-beam power tetrode for VHF-TV is water-cooled and features a unipotential cathode of thori-



ated tungsten heated by electron bombardment. The water-cooled anode is rated at 20 kw dissipation, and has coaxially arranged terminals. Eimac Type 4X2000A 20-kw radial-beam power tetrode for VHF-TV is air-cooled and all the special characteristics of the water-cooled tube, including a ceramic envelope for greater mechanical strength and higher resistance to thermal shock. Integral contact and simplify circuit construction.—Eitel-McCullough, Inc., San Bruno, Calif.—TELE-TECH

X-Y Recorder

(92-93)

Speedomax X-Y recorder has two separate electronically-balanced measuring circuits in one case, enabling it to plot the relationship between two interdependent variables. The X function is shown in the pen movement across the chart. The Y function is the vertical movement of the chart paper. Other recorders are a high precision instrument for temperature measurements



BOOTH NUMBERS at which the equipment described will be on display in the Hotel Sherman are indicated by the numbers in parentheses

and a versatile unit having a continuously adjustable zero and range suppression which can be used for a wide variety of applications.—Leeds & Northrup Co., 4901 Stenton Ave., Philadelphia 44, Penna.—TELE-TECH

Welding Analyzer . (106-107)

Model BL-213 new direct writing welding analyzer records single-phase and three-phase resistance welding machine variables Welding current and electrode force are measured and recorded simultaneously, and show the Important squeeze, weld, hold, and



off-time intervals. It also records the small 180 CPS component present in machine current when ignitron rectifiers are used. This analyzer consists of the modified Model BL-932 dc amplifier, and BL-320 universal amplifier. The modifications enable the analyzer to record 180 CPS for three-phase timing purposes. The operating variables of resistance spot, projection, and seam welding machines can also be accurately recorded.—Brush Development Co., Instrument Div., 3405 Perkins Ave., Cleveland 14, Ohio.—TELE-TECH

Waveguide Standards (46)

Waveguide vswr standards for precision tests are available in all military sizes from 1 x 0.5 to 3 x 1.5 in Reference sections have a vswr of 1.00 Standards having a miswatch at the input flange when mated with



the nominal guide or system under test of 1.05. 1.10. and 1.20 are obtainable. Inherent vswr is produced by milling narrow guide dimension less than that of maling guide to yield required mismatch. Broadband standards require no tuning. Units feature rugged, very flat sliding load, included with each set in a carrying case.—Airtron, Inc., 20 E. Elizabeth Ave., Linden, N. J.—TELE-TECH

For More Previews

to be

of New Equipment to be exhibited at the National Electronics Conference, turn to pages 78, 80 and 82. Audio Oscillator

(112-113)

Model 200AB audio oscillator covers 21 CPS to 40 KC in four ranges Power output is 1 watt or 24.5 v Load impedance is 600 ohms, distortion is 1%, and power consump-



tion is 60 watts. Large vernier dial gives long calibrated scale. Frequency stability is 2%, including warm-up, and num voltage is less than 0.1% of rated output Price is \$150. Also shown are the Model 618B signal generator, covering 3800 to 7600 MC with a variable output from 0.223 v. to 0.1 av. selling for \$2250; and Model 522B electronic counter, covering 10 CPS to 100 KC, with a time interval range of 10 assec to 100 000 seconds, sellings for \$900 —Hewlett-Packard Co., 395 Page Mill Rd., Palo Alto, Calif.—TELE-TECH

Time Mark Generator

Type 190 time mark generator has the following features: time markers of 1, 5, 10, 50, 100, 500 µsec; 1, 5, 10, 50, 100, 500 milliseconds; and 1 second, all available separately and simultaneously. Since wave out-



puts are 5, 10 and 50 MC; trigger impulses of 1, 10, 100 CPS; and 1, 10, 100 kc through UHF connector. All outputs controlled by a 1 MC crystal accurate within 0.02%. Type 180 is for oscilloscope time base calibration and also for calibrating counters, computers, etc. Weight 35 lbs. Dimensions are 10 m 16.5 m 14 in. Price \$575.—Tektronix, Inc., P. O. Box 831, Portland 7, Ore.—TELE-TECH

"Trans-Atlantic Television"

The White House and TELE-TECH's readers express varying views on proposals advanced in our editorial on page 33 of our August issue

From The White House

Consideration has been given to your letter to the President concerning the desirability of having an inter-continental television service and creating a Government sponsored committee to consider the possibilities.

Insofar as the Government's requirements are concerned, it is felt that no need exists for the appointment of a technical committee for this purpose. Existing committee structures within Government are believed to be adequate. The President is of the opinion that the electronic and communication industries are best equipped to carry on such studies and that the television industry could well sponsor such studies upon its determination that such a project is timely.

A substantial amount of work has been done over the past few years toward the reconciliation of differences in the technical standards in various countries. The United States with the help of the nation's television industry has participated in this work actively and constructively through the International Radio Consultative Committee of the International Telecommunication Union, which has a special Study Group that maintains a continuing effort on this subject.

JOSEPH SHORT

Secretary to the President

The White House

Washington, D. C.

The White House Washington, D. C.

Many Benefits from International TV

Your letter addressed to President Truman on "Trans-Atlantic TV" is most interesting and, in my opinion, most worthy in purpose. When, as and if such a TV link is accomplished, it would most certainly be the most practical means of bringing about better understanding between the peoples of foreign lands and ourselves.

Perhaps it is only a matter of viewpoint, but I believe that the people in our country have a much better and much more objective point of view with regard to world affairs and world relationships than do our brothers across the such we have many things to show that will be amazing to them and, of course, extremely educational. We, too, can learn much from telecasting in foreign lands. The objectives which would be accomplished by this means of communication would be of so great a value that the cost of such a line undoubtedly would be justified.

justified.

It occurs to me also that, inasmuch as the European countries are looking for items to manufacture which not only could be consumed by their own population but which, also, could be used as a medium of exchange through export, television manufacturing would absorb much labor and be an important aid in the building up of their economies.

mies.
Please advise if there is anything that
RTMA can do to cooperate with you in this
worthy cause.
A. D. PLAMONDON. JR.
Chairman, RTMA Board of Directors

President Indiana Steel Products Co. Valparaiso, Ind.

He Sent Pictures Across Atlantic in 1926!

I agree wholeheartedly that Trans-Atlantic TV is a must; and where that is so, the answers are bound to come.

When we first sent facsimile pictures across the ocean in 1926, it was a case of sizing up all the available factors and combining them in the way that produced the results, which have become quite routine now in the transmission of news pictures and weather maps. Somewhat the same approach must be given this TV spanning of the ocean.

Down at Orlando, Fla., during the last War, we were given the job of contacting lowrlying planes from the ground. We tried every available wave length and antenna but could not reach forward to them beyond 25 miles. Then we sent up a VHF relay plane to a height of 8,000 ft. and had no difficulty in reaching these ground hoppers some 250

miles out front. The Westinghouse Company has of course since applied this technique to TV relaying.
For immediate events such as the coming Coronation, it would seem that this extended relay-plane method is the practical answer. Ten of them should certainly succeed in spanning the Atlantic.
But for the steady operation, a series of ground stations up around the Greenland route seems right, although the number suggested of 68 is rather appalling. Perhaps multiplexing and thus reducing the individual channel band width may make is possible to extend each link and thus reduce their number.

It is certainly an intriguing challenge, which I am sure will be met.

R. H. RANGER

President

Rangertone, Inc. 73 Winthrop St Newark 4, N. J

Trans-Atlantic TV Far too Costly

While it is no doubt technically possible to establish some form of relay which would permit trans-Atlantic TV, the cost of such an operation would appear to be far out of proportion to the use which would be obtained therefrom. The great news events of Europe can be brought into American homes by way of film with very little delay and the few happenings sufficiently newsworthy to warrant immediate viewing hardly seem worth the effort.

Likewise, the underprivileged of Europe will no doubt have readier access to motion picture theaters than they will to television sets. Further, it is possible to edit the motion picture whereas some of the current TV live programming might not be suitable for the underprivileged, or for that matter, for he privileged.

In fact, I am not persuaded that Europeans are especially interested in our "Voice of America." They are subject to so much propaganda from all sides that they undoubtedly mistrust our own.

In my opinion the funds needed to get fast action on trans-Atlantic TV would be far better employed in reducing the national debt.

FRANK G. KEAR

FRANK G. KEAR

Kear & Kennedy Consulting Engineers 1302 18th St., NW Washington, D. C.

Advantages of VHF-Microwave-Relay Plan

Microwave-Relay Plan

I was pleased to note that you have given your support to Trans-Atlantic TV. From the observations I have made, a great deal of support is required to put it across. Apparently, at the present time, there are very few who accept its possibility.

Of the various systems which have been proposed in the past few years, I believe the system proposed by William S. Halstead, Research Associate of Crosby Laboratories, Inc., has the greatest practicability. Mr. Halstead proposes a microwave and VHF relay chain up the east coast of United States and Canada across to Greenland, then to Iceland, the Faeroe Islands, Shetland Islands and England. The maximum distance between relay points which this route would call for, is 290 miles. It is proposed to cover these longer distances by superpower on VHF. Superpower transmitters would be used in conjunction with a super directive antenna to span the distances by brute force. If this method fails, the inclusion of coaxial cable and relays on anchored ships is proposed for the several long over-water distances.

This microwave relay plan of Mr. Halstead's appears to me to be much more feasible than the other systems proposed. The "scatter transmission" proposal Involves signals reflected from layers of the ionosphere with the great possibility of multipath effects which would not allow good transmission of television. The express-plane ship-relay, and coaxial cable all have the limitation of an

exceedingly high cost and limited service

exceedingly high cost and limited service capabilities.

Mr. Halstead conceived this plan in 1946, and only recently was successful in gaining acceptance in engineering and management circles. The plan apparently so staggers the imagination that it is difficult to accept. However, if one considers the results which might be accomplished by the system, justification seems to be easy. I look upon such a relay system not only from the standpoint of providing inter-continental television transmission, but from the standpoint of the other communication facilities which it could provide in addition. The congestion of the short wave communication channels is now so great that it is time for some revolutionary steps such as this microwave VHF relay to provide a relief. After such a system is provided, the short wave channels may be reallocated to types of service such as marine where long distance transmission is a necessity. One microwave communication channel having a bandwidth sufficient to accommodate a television picture, would undoubtedly handle sufficient telephone and telegraph channels to carry on all of the communications now handled in the complete frequency range from 3 to 30 MC Furthermore, such a microwave channel would be far more dependable and accurate due to its freedom from fading effects, static, magnetic storms and other effects which plague short wave transmission. It would also be more free from intentional jamming MURRAY G. CROSBY President

Crosby Laboratorles Robbins Lane Hicksville, N. V.

Crosby Laboratories Robbins Lane Hicksville, N. Y.

Many Uses for **NARCOM Relay System**

Many Uses for NARCOM Relay System

Your editorial "Let's Get Action on Trans-Atlantic TV!" in the August Issue of Tele-Tech is, in my opinion, an Interesting and forceful presentation of the idea that television is emerging in the international field as a powerful new communication tool. It is clear that this medium has limitless potentialities in unifying and strengthening the peoples of the free world.

As an open letter to the President, it is to be hoped that the editorial will aid in directing the thought of our political and military leaders to full appreciation of the Immense significance of television and related wide-band telecommunication developments in furthering the two-way exchange of ideas and information of all types between the continental areas of North America and Europe.

With respect to the various proposals for attaining transmission of TV signals across the Atlantic, it is of importance to emphasize several factors that were not mentioned in the editorial but which have a direct bearing on the subject:

(1) It is intended that the proposed North Atlantic Relay Communication System, known as the NARCOM plan, will utilize mechain of microwave and VHF relay stations in carrying several hundred telephone, teletype, and facsimile channels, in addition to international TV and radio broadcast services. These general telecommunication facilities, which should be of very substantial value to international business, the news agencies, and governmental organizations, including the military forces of NATO countries, will provide a sound economic basis on which the relay system will be constructed and operated. Later, when international TV and radio broadcast networks have developed fully it may be expected that revenue from these services will form a large part of the total income of the relay system.

(2) By concentrating radio wave energy in narrow beams along the chain of relay stations at strategic mountain-top locations on the natural bridge of islands between the two continents it will be possi

adequate defensive measures to be taken at each relay point, thereby protecting the entire system. With coaxial-cable systems, on the other hand, the communication facility is vulnerable to enemy action at an infinite number of points.

(3) When future demands for expansion of facilities are encountered, or when it is desired to add multiple channels to accommodate the super-speed record transmission media such and Ultra-Fax, it will be a relatively simple matter to install the necessary relay equipments at each station to provide additional wideband channels. In this respect, it should be noted that radio-relay methods possess inherent advantages over coaxial-cable systems, in which duplication of cables throughout their lengths, including all their associated amplifiers, is required in adding wideband channels to meet increased service demands.

(4) The NARCOM route, as proposed, will cut across one of the most important areas of the world as seen from a military defense viewpoint. Observation of a polar-projection map of the North Atlantic area and the region within the Arctic Circle will show that the shortest air route between Soviet air bases in the western sector of the USSR and the east coast of the United States passes over a large part of the NARCOM relay route between southern Greenland and the Middle Atlantic states of our country. Because the unobstructed elevations at the mountain relay stations in this important area offer advantages with respect to operation of long-range radar and associated VHF air-defense communication systems. It is anticipated that many benefits will be obtained in the event that supplementary equipment of this type is installed at the relay stations itses. Moreover, the presence of wideband communication facilities at these locations, with connections to master control centers, should be of material aid in coordinating radar network and air-defense operations.

(5) Preliminary estimates of the cost of the NARCOM plan have made informal estimates that range between \$50,000,

Crosby Laboratories 25 Vanderbilt Ave. New York, N. Y.

Problem Should Be Explored, Now!

Congratulations on the quality of creative imagination and foresight displayed in your August proposal for the investigation of Trans-Atlantic TV. I believe that the history of human social development will support the contention that an improvement in effective communications in a community influences the pattern of community life away from Isolation and conflict, toward mutual understanding and mature social integration. International television, with its potential for the nearly instantaneous sharing of experiences across the horizons of the world, unfolds the most promising force for ultimate peace the world has ever known. Television can supply the needed basic elements for the development of the socially integrated world community.

While no engineer would subscribe to the conclusion that any of your proposed plans are feasible at this time, all thoughtful engineers will support you in your contention that a practical solution can be found only after there is full recognition of the nature and the boundaries of the problem. A serious exploration of the trans-Atlantic TV problem now should cut the eventual time of solution in half.

D. E. NOBLE

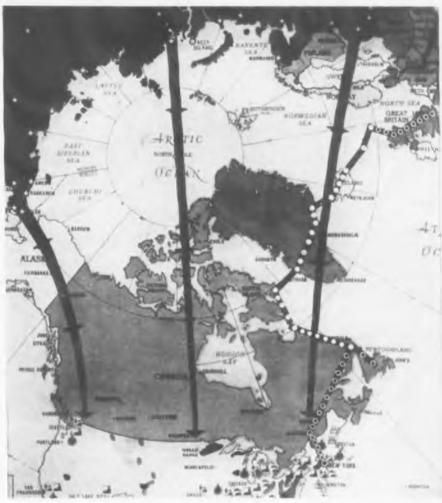
Motorola, Inc.

Motorola, Inc. 1545 Augusta Blvd., Chicago

D. E. NOBLE Vice Pres. in Charge Communications and Electronics Division

Latin-American and Asian Links Important, Too

I have read with interest your letter to The President of the United States relative to Trans-Atlantic TV. You are to be congrat-ulated for your foresightedness in this mat-ter, and you should receive the support of



Circumpolar map showing shortest bombing paths from Russia to our northern boundary. Also how proposed Trans-Atlantic TV relay would provide radar protection against eastern path

every progressive thinking person in the country.

The several methods suggested in your letter for trans-oceanic television are practical, but naturally they involve tremendous capital investment. Nevertheless, the achievement of Trans-Atlantic TV is of such importance to the public that active steps should be taken now to provide the facilities for an interchange of sight and sound between this country and other nations of the world. Perhaps, high in the order of priority is a television link between the United States and Europe, but, in my opinion, a link between the United States and Latin America and the United States and Latin America and the United States and Latin America Consulting Radio Engineers

Munsey Building Washington 4. D. C.

Will Stimulate Thought

I think your editorial "Let's Get Action on Trans-Atlantic TV" is a good one and should stimulate m lot of interesting thought that should result in a great deal of information. LEWIS M. CLEMENT Technical Advisor to General Manager Crosley Division Avco Manufacturing Corporation Cincinnati, Ohio

Technical Problems Not insurmountable

Your letter to the President urging action on Trans-Atlantic TV is very timely. The responsibility for leadership in the struggle for world peace has fallen upon our nation. How better can we portray to Europe the advantages enjoyed by a free people than through the medium of television. Conversely, and of no less importance would be the advantage to our people, to view by television, the great news events of foreign powers

powers
The technical problems are great but not

insurmountable. You and your associates are to be congratulated for the initiative you have taken. I firmly believe your efforts will be rewarded by Government action.

F. A. D. ANDREA

President

Andrea Radio Corp.
Long Island City, N. Y.

A Factor in World Peace

Your editorial on Trans-Atlantic TV certainly meems timely. The now numerous prospective methods for constructing m Trans-Atlantic circuit establish m presumption of early feasibility.

It is not clear to me whether such a circuit, if feasible, should be built and operated by public or private agencies. At the moment, my preference would be toward the latter, with some form of assistance to the private agency out of public funds to the extent needed to make the operation solvent. It meems to me probable that a gradual increase in understanding among the peoples of the world is at least m major help and perhaps even m necessary condition to the bringing about of an honorable and durable world peace. Is there a better cause to work for?

A. V. LOUGHREN Director of Research

Hazeltine Corporation Little Neck, L. I., N. Y.

Enlist Private Enterprise In Project

Your editorial (Tele-Tech, August) on transatlantic TV deserves to needle technology into action, though one might hope it would ultimately be through private enterprise which is the best touchstone of intrinsic worth. In the present instance private underwriting would constitute a warranty that a proper balance had been struck between the value of spot news or live programming, where an electrical TV feeder is

(Continued on page 92)



WASHINGTON

News Letter

Latest Radio and Communications News Developments Summarized by TELE-TECH's Washington Bureau

TELECOMMUNICATIONS PLANNING COM-MITTEE—The creation of a Telecommunications Planning Committee to formulate detailed plans for the most efficient use of the nation's communications systems in the event of war and also to study the need for and feasibility of new technological advances in the field of international communications has been announced by Haraden Pratt, Telecommunications Advisor to the President. Mr. Pratt stated that five government agencies had accepted his invitation to form the new committee. The committee's work, he noted, will be similar in many respects to that of the Defense Communications Board, later the Board of War Communications, during World War II

PARTICIPATING AGENCIES—Department of State, represented by Director Paul Barringer of the Office of Transport and Communications Policy; Department of Defense, represented by Rear Adm. John R. Redman, the Communications-Electronics Director of the Joint Chiefs of Staff: Department of Commerce, represented by Rear Adm. Charles F. Horne (USN, ret.), Administrator of the Civil Aeronautics Administration; the FCC, represented by Commissioner E. M. Webster; and the Central Intelligence Agency. Only planning and coordinating functions have been assigned to the committee. Any operating or procurement activities resulting from recommendations by the committee will be performed by the agencies affected. An immediate major task of the Telecommunications Planning Committee, in its drafting of an overall program for the communciations requirements for the nation in the event of war, will be the coordination of the existing plans of the different government agencies. Other government agencies will be expected to participate in the committee's functioning. Non-government organizations in the communications field will be consulted as necessary.

FCC TELEVISION HEARINGS—With the commencement of hearings by its corps of examiners on Oct. 1, the FCC starts on its long course of building up the nation's television coverage to an eventual total of 2,-000 or more video outlets, a goal so greatly desired by the American public. The Commission has been granting an average of more than five new station applications a week since mid-July or a total of more than 60 to date. In order to expedite the processing, the FCC has increased the staff under its Broadcast Bureau Chief Curtis B. Plummer and its License Division by approximately 25 accountants, engineers, attorneys and clerks.

That the task of the Commission will be huge is a foregone conclusion and it will undoubtedly last for two years before the 2,000 stations are authorized and are on the air telecasting.

EDUCATIONAL TV - During September and October many state legislatures will be acting upon appropriations, it is anticipated, to launch state university and state and municipal non-commercial educational television station projects. This will mean a step-up in the filing for educational video stations. Nevertheless, the FCC had received relatively few of these applications up to Tele-Tech's press deadline. However, the FCC has been advised properly by television broadcasting organizations that it should grant the same "rules of the game" for non-commercial educational television station applicants as are required of the commercial television applications. This view was epitomized by the NARTB recently in stressing in the case of the educational TV application of Kansas State College of Agriculture and Applied Science that no license should be issued until the financial ability of the applicant is proved.

MOBILE RADIO IRE MEETING-More than two hundred radio engineers who are leaders in the mobile radio field are slated to attend the third annual meeting of the Institute of Radio Engineers' Professional Group on Vehicular Communciations to be held in Washington Dec. 3 to 5. Major subject of discussion and of technical reports will be on the most economical and efficient use of the frequency space assigned to the mobile communications services. In addition, the meeting will be featured in its deliberations on the subject of adjacent and split-channel operation of mobile radio equipment. It is anticipated that there may be demonstrations of the latest types of equipment in adjacent and split channel operation by leading manufacturers such as RCA, General Electric, Motorola, Federal Telephone and Radio and Raytheon. Frederick T. Bundelman, President of the Budelman Radio Corp., is chairman of the I.R.E. Group. and FCC Safety and Special Radio Services Bureau. Edwin L. White and Joseph E. Keller of the American Petroleum Institute are co-chairmen of the meeting's arrangement committee. Key representatives from the utility, petroleum, police and bus-taxicab mobile radio fields are expected to present surveys of the progress in their respective services.

National Press Building Washington, D. C.

ROLAND C. DAVIES Washington Editor



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(Above) CINCH Octal molded socket, 1-5/16" Mtg. Center, 1-1/2" M.C. available, (Left) Loktal Molded Socket, 1-5/16" mtg. Center.

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(Above left) Cinch Noval socket — saddle type Mica filled molded with .093 mtg. hole 1-1/8" mounting center, (Left) Melded Miniature, 7/8" mounting center.

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TELE-TECH'S NEWSCAST

High-Purity Silicon Powder for Microwave Crystals

High purity silicon powders especially processed to meet the rigid chemical requirements for the manufacture of crystals for radar, video relay, and other microwave applications are now available from the Tungsten and Chemical Division of Sylvania Electric Products, Inc. of Towanda, Pa.

The new silicon powders have purities of 99.85% and 99.95% as compared to previous powers supplied with purities of 95.75%. A New process assures uniform chemical composition and physical properties from batch to batch, and should permit the production of crystals for use as microwave detectors and mixers in radar and video applications with a predictable range of electrical characteristics.

AT&T Expands **Television Services**

The long Lines Dept. of the American Telephone and Telegraph Co. has announced that a new northbound television channel from Miami. Fla. to Atlanta, Ga. will become available on Jan. 1, 1953. Designated as being for occasional service, this new channel will permit the origination of nationwide TV broadcasts from Miami.

Also scheduled for completion on Jan. 1 are two new northbound channels connecting with Dallas, Tex. and New Orleans, La. These facilities, available for occasional service, would permit interconnection of Dallas with the transcontinental microwave relay system at Omaha, Neb. and connect New Orleans with the national network at Jackson.

By early fall a new 11 station radio relay system between New York and Washington is scheduled to be put into operation. Relay towers for this system are located in Atlantic Township, New Egypt, New Albany and Swedesboro, N.J., at North East, Carney, Gambrills, Baltimore, Md., New York City, N.Y., Philadelphia, Pa., and Washington, D.C.

NARTB History to be Recorded

Harold E. Fellows, president of the National Association of Radio and Television Broadcasters has announced that a history of the NARTB will be written by David R. Mackey, assistant professor of speech, Pennsylvania State College. Professor Mackey estimates that his comprehensive examination of the 30-year history of the broadcasting industry's trade association will require a minimum of two years for completion. The finished history will be submitted to Northwestern Univ., Evanston, Ill., as Professor Mackey has chosen this subject for his Ph. D. thesis.

Sarnoff Gold Medal to SMPTE's A. Jensen

Peter Mole, president of the Society of Motion Picture and Television Engineers, has announced that the David Sarnoff Gold Medal Award will be presented this year to A. G. Jensen, director of television research, of Bell Telephone Laboratories, Murray Hill, N. J.

The official presentation to Mr. Jensen will be made during SMPTE's 72nd semi-annual convention at the Statler Hotel, Washington, D. C.

Coming Events

October 6-10-SMPTE, 72nd Convention, Hotel Statler, Washington, D. C. October 13-17-AIEE, Fall General Meeting, New Orleans, La.

October 13-15-RTCM, Fall Assembly Meeting, Hotel Roosevelt, Washington, D. C.

October 20-22-1952 RTMA-IRE Fall Meeting, Syracuse, N. Y.

October 29-November 1-Audio Fair, Sponsored by AES, Hotel New Yorker, New York, N. Y.

November 5-7-IMS, 16th Annual Time and Motion Study Clinic, Sheraton Hotel, Chicago, Ill.

November 7-IRE, Microwave Professional Group Symposium on Microwave Circuits, Auditorium, Western Union Telegraph Co., 60 Hudson St., New York, N. Y.

November 21-22—IRE, Kansas City Section, 4th Annual Regional Papers Technical Conference, President Hotel,

Kansas City, Mo.

December 3-5—Third annual IRE Professional group on Vehicular Com-munications, Washington, D. C.

December 10-12—IRE-AIEE Computers Conference, Park Sheraton Hotel. New York, N. Y.

January 14-16—IRE-AIEE Meeting on High Frequency Measurements. Washington, D. C.
March 23-26—IRE National Conven-

tion, Grand Central Palace & Waldorf-Astoria Hotel, New York, N. Y. May 18-21—Electronic Parts Show. Conrad Hilton Hotel, Chicago, Ill.

AES: Audio Engineering Society
AIEE: American Institute of Electrical

AIEE: American Historiae
Engineers
IRE: Institute of Radio Engineers
IMS: Industrial Management Society
RTCM: Radio Technical Commission for
Marine Services
Marine Mrs. Assn. KTCM: Radio Technical Commission for Marine Services RTMA: Radio-Television Mfrs. Assn. SMPTE: Soc. of Motion Picture and TV Engineers

Telecommunications Network for Europe and Near East



Map showing how principal cities of Europe can be linked in a microwave relay system that could provide an international television service along with both civilian and military communications facilities. Stations would be placed on mountain peaks and designed to operate unattended. Helicopters to be used to provide any necessary services. This system can also be integrated with a Trans-Atlantic TV System (see Aug. issue editorial and page 66, this issue). Full details in Tele-Tech next month.

STILL ANOTHER

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NEW EQUIPMENT

for Designers and Engineers

Power Transformer

A new toroidal power transformer eliminates hum-pickup in audio amplifiers. Known as type MT-1001, it replaces ordi-



nary power transformers in high gain amplifiers where an absolute minimum of humpickup through magnetic field radiation is desired. The transformer is precision wound on a ring core without air-gaps and radiates less than 01 Gauss at 5 in from its surface. By parallel or series connection and doubler or tripler circuits the following de voltages for plate supply may be obtained: 350, 700, 1200 and 1.800. It has 2 separate heater windings which are rated 6.3 v. and 1.5 amps. Millivac Instrument Corp.. Engineering Dept., P.O. Box 997, Schenectady, N.Y.—TELE-TECH

Vibrator

A new panel vibrator will introduce a vibration of known frequency and amplitude into instrument panels to increase meter ac-



curacy and prevent sticking. It is an electrically driven device operating continuously. Motor power for the vibrator is furnished by a fractional horse power motor operating at any standard dc voltage. The motor is a two-pole, two-brush design. An unbalanced weight is mounted on the end of the armature shaft. Weight provides the vibration action of the assembly. Shaking forces, at 2500 rpm, can be provided from 0.85 lb. to 3.4 lbs. by varying the weight. The frequency 2000-3000 cpm.—Globe Industries, Inc., 125 Sunrise Pl., Dayton 7, Ohio.—TELE-TECH

Capacitor Network

Type BTN capacitive network is a multisection, metal encased, hermetically-sealed paper dielectric unit. Its multiple sections can be internally connected to provide a selection of either capacitive Pi, Y, or Delta



networks and can be provided with mineral oil, pentachlordiphenyl, or electrical grade waxes as impregnants. Type BTN is said to be useful in airborne equipment power frequency circuitry where the compact single unit construction offers space and weight saving advantages over three individual types. These networks are supplied in heavily tin coated ferrous or non-ferrous cases of the "bathtub" type with metallized Pvrex glass solder-seal terminals —Sangamo Electric Co., Capacitor Div., Marion, III.—TELE-TECH

Decade-Inductor Units

The new 700 series decade-inductor units are useful in design and experimental work on audio filters, equalizers and tuned circuits



at frequencies between 150 to 20,000 cps. Four units are available in ranges from 10 m 0.001 henry to 10 x 1.0 henry. When all four units are connecting in series, 11,110 steps from .001 henry to 11.11 henries are obtained. Four type EM-1 toroid coils are used as clements in each unit. The 10 steps are obtained by series switching. "Q" factor remains essentially constant over all ranges. The decade-units are said to have excellent stability in respect to current and temperature changes and reasonable amounts of demay be run through the units with small effect on inductance—Hyoor Co., Inc., 11423 Vanowen St., North Hollywood, Calif.—TELE-TECH

Miniaturized DC Relay

A new, miniaturized hermetically-sealed relay designated the RCA-203W1, is of the 6-pole, double-throw type operating on 26.5



v. The miniaturized-type design features sturdy and compact construction, palladium contacts, moisture-free-gas filling, and long operating life. It will neet the requirements of the Air Force (Specification MIL-R-5757) and is engineered to provide longevity of service under extremes of temperature, humidity, shock, vibration, and voltage variations as stipulated in this military specification. The 203W1 weighs only 3 oz. and can be operated in any position. Its 6-pole, double-throw construction features palladium contacts rated to handle 2 amps. with a resistive load at 26.5 v. dc and one ampere with an inductive load at the same voltage. Contacts are arranged in a break-beforemake sequence.—Tube Dept., Radio Corporation of America, Harrison, New Jersey—TELE-TECH

Composite Picture Generator

Model 305-BR monochronie composite picture generator produces high-definition television picture signals from still tran paren-



cies, film positives, glass slides, or block opaques such as lettering mounted on a transparent background. This unit is useful in studio work for carrying test patterns or slides, and can also present art work, cartoons, animated displays, announcements, etc. It will provide special effects such as the pointer for a map, vertical, diagonal and horizontal wipes, lap dissolves and vignettes of any shape. In making the special effects, the unit may be used to blank or pedestal any portion of a standard television pleture, allowing normal full contrast range for the inserted picture. Standard RTMA Composite Video Signals are available: black level positive and black level negative. Resolution is greater than 600 lines at center and 500 lines at corners of standard RTMA test pattern. Gamma Correction may be removed and is variable over a wide range.—Telechrome, Inc., 88 Merrick Rd., Amityville, N.Y.—TELE-TECH

Video-Audio Switching System

Type CRS-2 video and audio preset switching system accommodates six Inputs, and one monitor and two line outputs. Auto-



matic switching of desired combination of feeds arranged on preset bank is accomplished by push buttons, Indicating lights keep tally of preset and in-use circuits. Full remote control of all switching operations is easily initiated and registered by tally lights. Rotary selector permits complete previewing of any of six inputs. Muting relays for intercom and talkback in feeding studio are actuated by outgoing signal. Design allows custom installation in console. rack and desk turret mountings to suit individual station requirements.—General Communications, Fort Atkinson, Wis.—TELE-TECH

This new Vacuum Gauge covers a range of 5,000,000:1

on a single meter from a single pickup

It's the DPi Philips Gauge, Type PHG-09, a remarkable new instrument developed by DPi high vacuum research. Here are the basic facts about it:

- A single meter covers the entire range from 0.50 mm to 10⁷mm Hg.
- A single all-metal pickup tube handles this range. It works on the glow discharge principle. Permanent magnets provide a field which lengthens the electron paths into tight spirals that give high ionization per electron, with a cascade effect.
- Having no filament to burn out, the tube can be operated at full atmosphere without damage, and the circuit is insensitive to fluctuations in the line voltage.
- With the magnets external to the ionization chamber, there is no problem of outgassing them or removing stray iron particles.
- Self cleaning, the tube at the higher pressures in the low sensitivity range automatically rids itself of deposited film because polarity is reversed.

This new Philips gauge is now being used in DPi exhaust machinery where close control of pressure is required. For information on this or any equipment for the creation and measurement of high vacuum in the electronics industry, write to *Distillation Products Industries*, Vacuum Equipment Department, 629 Ridge Road West, Rochester 3, N. Y. (Division of Eastman Kodak Company).



Also...vitamins A and E...distilled monoglycerides...
more than 3500 Eastman Organic Chemicals
for science and industry

Plug-In Amplifiers

A new line of miniature plug-in preampli-flers, line or monitor amplifiers, and power supplies designed primarily for use with the



Altec 250A speech input console are equally adaptable for custom built consoles or for any other speech input application where performance, size and quick replacement area factor. The preamplifier dimensions are: 13% x 4½ x 9 in., while dimensions of the line amplifiers and power supplies are 23% x 4½ x 9 in. Frequency response of all amplifiers is

±1 db from 20-20,000 CPS and noise level is kept very low through the use of especially designed miniature transformers with 90 db of shielding. Both the amplifiers and power supplies are equipped with a handle and plug-in connectors, and are designed to fit into a cover tray which can be permanently mounted in a rack or cabinet. On one end of this tray is the receptacle to which all wiring connections are made. The plug-in unit slides easily into the tray and automatically centers its plug with the receptacle. When necessary the unit may be quickly removed for bench servicing or for immediate replacement with a spare unit.—Distributed by Graybar Electric Co., Inc., Altec Lansing Corp., 9356 Santa Monica Blvd., Beverly Hills, Calif.—TELE-TECH

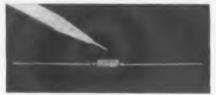
Oscillator

A new low frequency oscillator, designed as a source of signal power in the range of .01 to 100 CPS, features the use of passive elements (resistors and capacitors) for frequency determination. The circuit has been treated as a dc amplifier, and both plate and filament supplies have been carefully regulated. The output circuit is directly cou-

pled to the load and will produce 20 v. or 20 ma into any load impedance. This instrument is a true sine wave generator, and the wave shape contains only low order harmonic distortion. Two separate means for amplitude control have been provided. An oven-controlled thermistor is used as a quasi-linear element where extremely low distortion is required (in the order of 0.1 of 1%). A varistor is also provided in a unique circuit which allows it to control the amplitude by creating 1% or less distortion (primarily third harmonic). Since the non-linear amplitude controlling element does not involve the quantity "Time," there is no amplitude bounce associated with its controlling action, and the initial switching transient which occurs when changing ranges has been reduced to about 10% by keeping the range capacitor precharged to their operating potentials. The unit is housed in a welded aluminum cabinet, 18 x 18 x 12 in., and weighs approximately 65 lbs.—Southwestern Industrial Electronics Co., 2831 Post Oak Road, P. O. Box 13058, Houston 19, Texas.—TELE-TECH

R-F Chokes

A regular production line of tiny r-f chokes are believed to be the smallest chokes on the market as standard catalog



items. They range in inductance from 0.25 to 100 µh and are plainly marked and insulated for 500 v.—Condor Radio Mfg. Co., 116 N. Montezuma St., Prescott, Ariz.—TELE-TECH

Laboratory Amplifier

Model SR88 amplifier pre-amplifier com-bination can be used in conjunction with any high quality tuner not providing a



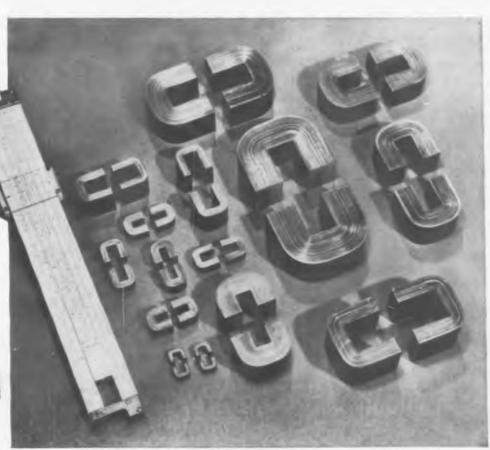
properly compensated phono pre-amplifier. Distortion at 15 watts is 400 CPS 0.32% harmonic. It does not exceed 0.5% harmonic distortion at any frequency, from 30 cycles to 15.000 CPS. Intermodulation distortion (40 & 7000 CPS. SMPE Standards) is 2.5%. Even at 25 watts, distortion is limited to 1.0% harmonic. Frequency Response is ± 2 2 db, 20 to 20K CPS. The num-free magnetic phono pre-amplifier has adequate gain for low level reluctance cartridges. Uses feedback circuit for lowest distortion and fully compensated bass response. Input and output jacks, plus cables, are provided for easy connection to switching facilities. Inverse feedback of 26 db affords an extremely high damping factor. Voltage-rise of less than 0.3 db between full-load and no-load provides maximum control over speaker and insures low distortion performance regardless of variations in speaker impedance.—The Sargent-Rayment Co., 212 9th St., Oakland 7, Calif.—TELE-TECH



27 Haynes Ave., Newark, New Jersey

SILECTRON
"C" CORES

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IN
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QUANTITIES



... wound from strip as thin as 0.00025"

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- Arnold "C" Cores are made to highly exacting standards of quality and uniformity. Physical dimensions are held to close tolerances, and each core is tested as follows:
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- ★ 4-mil cores are tested for watt loss and excitation volt-amperes at 400 cycles, at a peak flux density of 15 kg.
- ★ 2-mil cores are tested for pulse permeability at 2 microseconds, 400 pulses per second, at a peak flux density of 10 kg.
- ★ 1-mil cores are tested for pulse permeability at 0.25 microseconds, 1000 pulses per second, at a peak flux density of 2500 gauss.
- ★ ½ and ¼-mil core tests by special arrangement with the customer.

Now available—"C" Cores made from Silectron (oriented silicon steel) thin-gauge strip to the highest standards of quality.

Arnold is now producing these cores in a full range of sizes wound from 1/4, 1/2, 1, 2 and 4-mil strip, also 29-gauge strip, with the entire output scheduled for end use by the U. S. Government. The oriented silicon steel strip from which they are wound is made to a tolerance of plus nothing and minus mill tolerance, to assure designers and users of the lowest core losses and the highest quality in the respective gauges. Butt joints are accurately made to a high standard of preci-

sion, and careful processing of these joints eliminates short-circuiting of the laminations.

Cores with "RIBBED CON-STRUCTION"* can be supplied where desirable.

Ultra thin-gauge oriented silicon steel strip for Arnold "C" Cores is rolled in our own plant on our new micro-gauge 20-high Sendzimir cold-rolling mill. For the cores in current production, standard tests are conducted as noted in the box at left—and special electrical tests may be made to meet specific operating conditions.

• We invite your inquiries.

*Manufactured under license arrangements with Westinghouse Electric Corp.

WAD 4218





scientifically-engineered qualities and features found in no other commercial tuner unit.

And, they are especially enthusiastic about the Tarzian approach to UHF.

PURCHASING AGENTS like it because it's competitively priced and offers more value per dollar than any other commercial tuner.

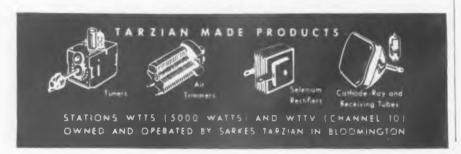
THE CONSUMER or set buyer is happy with the excellent performance of his receiver, although he doesn't have the slightest idea of the importance of the TARZIAN TUNER in the satisfactory operation of his set.

SERVICEMEN

like it because of the simplicity in servicing and aligning.

SARKES TARZIAN, INC.

Tuner Division, Bloomington, Indiana



High Voltage Tester

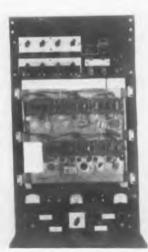
The Hi-Tronic lester is an electronic-controlled high voltage lester operating at very low current, eliminating the possibility of



dangerous shock to the operator. It will operate on circuit resistances up to 1 megohm per 100 v. (5 megohms at 500 v. or 10 megohms at 1000 v.) The need for watching an indicator light is obviated by an alarm buzzer which is incorporated in the unit. so that the operator can devote his full attention to the apparatus under test. This tester can be supplied with special circuit and relay connections to operate any device or equipment normally used in conjection with high voltage tests.—Bliss Electronic Corp., Box 123, Sussex, N.J.—TELE-TECH

Laboratory Assemblies

System for rapid assembly and testing of experimental circuits features metered power supply and test panel with decade capacitor.



decade resistor, and measuring bridge. Series of panels, mounting channels, bench supports, and layout sheets provide versatile RAK-LAB arrangement for mounting wide variety of circuits. Model 401 power supply covers 0 to 400 v. at 150 ma, 0 to 12.6 v. at 5 amps, 0 to 63.9 v. at 10 amps, and sells for \$290. Model 402 test panel, including decades and bridge for measuring inductance, resistance and capacitance sells for \$290.—Davies Labs., Inc., 4705 Queensbury Rd., Riverdalc, Md.—TELE-TECH

Reversible Motor

A reversible 2-pole, 4-coil motor for both remote control TV tuner and rotating antenna applications, has been designated the Model O. It can be furnished either as splitphase capacitor type or split-phase resistance type, depending upon application requirements. It is designed for 24, 12, or 6 v. ac, 60 cps, and may be used either horizontally or vertically without affecting performance characteristics. One motor type having 3 leads is designed for use with single-pole double-throw switch. Adaptation, with 4 leads for use with double-pole, double-throw switch is available where increased output is desired.—The General Industries Corp., Elyria, Ohio—TELE-TECH



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in 1952

The development of Mylar** polyester film by Du Pont chemists and its adaptation as a capacitor dielectric by Aerovox engineers, presents challenging potentialities in the field of electronic capacitors.

Known as Aerofilm Capacitors, these latest components permit higher operating temperatures without corresponding increase in size, as well as unusually high insulation resistance. Both gains mean much to the designers of tomorrow's fantastic weapons and again to peaceful electronic applications. Thus in 1952 Aerovax auspiciously embarks upon its fourth decade of capacitor craftsmanship.

*Aprava» Trade Mark

**Du Pont Trade Mark for polyester film



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Models ON-5A and ON-5X are designed as basic, highly flexible laboratory instruments for general pulse work. Their specifications include:

- High-gain vertical amplifiers.
- Triggered sweeps, from an external trigger or from the input to the vertical amplifier.
- Recurrent sweeps, at a repetition rate of 10 to 100,000 per second
- Vertical input delay of 0.45 microsecond (ON-

Model P4-EX is designed for applications requiring a triggered sweep, and where the signal levels met do not demand extremely high-gain amplification. Its many outstanding features include:

- Internal trigger, at a repetition rate of 50 to 5000 per second, easily synchronized with an external trigger if desired.
- Output trigger, with the same range of repetition rates, which can be continuously phased to lead or lag the sweep start by a maximum of 500 microseconds.

Detailed specifications and performance data available promptly on your request.

These new instruments represent a high level of precision design and versatility of application at remarkably low cost. Major features that are common to all three instruments include:

- Type 5UP cathode-ray tube, operating at an accelerating potential of 2600 volts. P1, P7 and P11 screens are available.
- Sweep writing rate continuously variable from 1.0 to 25,000 microseconds per inch.
- · Sweep calibration in microseconds per horizontal scale division, accurate to plus or minus 10%.
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- Vertical calibration voltages, at accuracy of plus or minus 5% for Model P4-EX, and plus or minus 10% for Models ON-5A and ON-5X
- Vertical amplifier input step attenuator.
- CRT cathode connection externally available, for application of blanking or marker pulses.

NET PRICES, F.O.B. Winchester, Massachusetts: P4-EX . . . \$465.00 ON-5A . . . \$485.00 ON-5X . . . \$535.00

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Standing Wave Detector

Featuring accuracy and simplicity, Type-1022 standing wave detector will make pre-cision low level impedance measurements in the millimeter region when used with a



suitable source and amplifier. VSWR's as low as 1.01 as to 36 kilomegacycles/sec. The unit consists of a slotted section of RC-96/U waveguide milled from a solid piece of brass and silver plated. A movable carriage is provided carrying a spring-loaded adjustable coupling probe, a silicon diode detector socket, and coaxial output fitting which will make with a UG-88/U or equivalent BNC cable connector. This carriage rests on semicylindrical polished bearing surface and is positioned by a micrometer drive. A total longitudinal probe displacement of 0.750 ln. is available. The probe position can be read accurately to 0.001 in. Total insertion length of the unit is 3.25 in.—Microwave Associates, Inc., 22 Cummington St., Boston 15, Mass.—TELE-TECH

Radar Range Calibrator

Type 2010 range calibrator

Type 2010 range calibrator, designed for production testing and calibrating of radar receivers, embodies several basic circuit features which obsolete the TS-102/AP range calibrator for applications requiring accurate pulse repetition rates and absolute freedom from marker jitter. The type 2010 offers: crystal-controlled pulse rates of 200 to 2000 pps. derived from a 327.80 KC marker crystal by the use of a binary divider system; "Master-Slave" operation permitting the use of a number of calibrators for multiposition test systems; narrow and stable 500 vard marker pulses; and a completely regulated power for operation from 105-125 v.. 100 W 50-60 cps.—Tel Instrument Co., 50 Paterson Ave., East Rutherford, N.J.—TELE-TECH

NEC Exhibits • • • •

Turn to pages 64, 65, 80 and 82 for more reviews of products being exhibited at the National Electronics Conference,

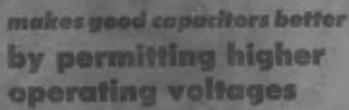
Variable Transformer (98-101)

Type 10 powerstat variable transformer for 50, 100 and 150 watt ac control applications is rated at 120 v., 60 cycles, single-



phase input. Output is 0-120/132 v., 1.25 amps. Designed for single-hole mounting. compactly constructed unit measures 3 in OD. and 2 1/16 in. under-chassis depth. Transformer weight is 1 lb., 13 oz. List price is \$8.50. Superior Electric Co., Bristol, Conn.—TELE-TECH

AMAZING - IMPREGNANT



E-therm impregnated capacitors are now available in production quantities. Extrem is a unique new impregnating material developed and compounded by Sangamo, E-therm impregnated capacitors for exceed the requirements of JAN Specifications. E-therm possesses asseptionally high thermal stability and superior electrical characteristics. E-therm impregnated capacitors mean—higher operating temperatures—lower power factor—higher resistance—longer life.



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Balun

(3)

Type 874-UB balun makes it possible to easure balanced circuits in the range 50 1000 MC using grounded measuring sys-ms. Balanced to unbalanced transformation tems Balan Is obtained Is obtained by using a semi-artificial half-wave coaxial line made of two sections of



50-ohm coax and two shunt tuning elements. Well adapted to measuring 300-ohm balanced lines, the instrument is tuned by various lengths of air line Also presented are the Type 1555-A sound-survey meter covering 40 to 136 db above 0.0002 µbar reference level, costing \$125; Type 1551-A sound-level meter covering 24 to 140 db above 0.0002 µbar, costing \$360; and Type 874-LK constant-impedance adjustable line with 50 ohms impedance, and selling for \$36. General Radio Co., 275 Massachusetts Ave., Cambridge 39, Mass.—TELE-TECH

High Frequency VTVM

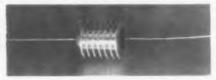
MV-22A vacuum tube voltmeter for ac is further development of the MV-12A meter ecently announced. The older instrument as a frequency range of 20 cycles to 250



KC. The new meter has been extended to 6 MC. The instrument has a six-state amplifier with a novel ac regulated power supply. It measures voltages between 70 and 1000 v — Millivac Instrument Corp., 444 Second St., Schenectady 6, N. Y.—TELE-TECH

Power Rectifier

Germanium Junction-type power rectifler has maximum rms rating of 1.2 amps, 130 v. input. Forward resistance is 3.5 ohms, while high back resistance is 50.000 ohms. Frequency range extends up to 30 KC, with



operating life of 70.000 to 100.000 hours. Small size of 5 _B x 5 _B in. makes unit desirable for TV and similar applications. Also available are photo tubes for film sound pick-up and electric eye applications. Lead sulphide cell has peak spectra response at 15 microns, cuts off at 3.4 microns. has time constant of 125 µsec. Cadmium sulphide cell has peak spectral response at 5300 Å . Is sensitive to X-rays, and has time constant in the order of milliseconds—Lectro Max. Inc., 15 S. First St., Geneva, Ill.—TELE-TECH





application)

B—I. F. Transformer

C-Horizontal width coil

D—Video peaking coil

E-Flyback transformer conventional type

F-Flyback Transformer high efficiency auto-transformer

G-Patented high voltage corona free tube socket assembly

H-Patented feed-thru interlock assembly

I—Exclusive design duo decal sector assembly

J—Duo-decal assembly for electro-static tube K-Special wiring harness (ARC-27)

RAYPAR also manufactures all sorts of I. F. and R. F. windings, such as antenna coils, oscillator coils, R. F. chokes, flyback transformers, width coils, linearity coils, video peaking coils, filter assemblies, and special purpose R. F. coils of any type or construction.

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Designers, engineers, production men everywhere are changing their thinking (and specifications) over to economical C-D-F spiral tubing. Whether it's round, square, or rectangular, C-D-F tubing is stiff, sturdy, crush resistant. It has good tensile strength, along with good dimensional stability under varying atmospheric conditions.

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The round tubing ranges from $\frac{1}{8}$ " to 6", with wall thicknesses from .0075" to $\frac{1}{8}$ ". The minimum ID of the square and rectangular tubing is $\frac{3}{8}$ ", with $\frac{21}{8}$ " the maximum ID. $\frac{1}{16}$ " is the maximum wall thickness. All tubing can be supplied in lengths from 2^{1} to 4^{1} . From our own fabricating experience, we know you will find this sturdy material easy to drill. tap, rivet, flute or thread.

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Digital-to-Analog Converter (42-43)

Model 417 digital-to-analog converter transforms information from punched cards or tape recorder to analog form so that a



representative point plot can be made on a dc plotting board. System consists of a basic timer, two temporary storage units, X and Y scale factor circuits, X and Y parallax circuits, X and Y digital-to-dc converters, two dc amplifiers, control panel, and power supply. For points spaced 4 in. or less, plotting speed is 50 points per minute. Converter accuracy is 0.02% of full scale. Accessories available are a typewriter binary converter and manual keyboard.—Electronic Assoc., Inc., Long Branch, N. J.—TELE-TECH

Frequency Analyzer (88)

Model 7T-4 Stroboconn measures all types of repetitive frequencies, constant or variable. Unit presents a continuous, visual pat-



tern for the duration of the signal. Precise analysis can be made to an accuracy of 0.05%. Minimum input is 1.5 mv. Signal is amplified to flash a neon tube which lights 12 rotating scanning discs. When one of the seven concentric patterns on a disc "stands still," the frequency is read directly in CPS. When more than one frequency is involved, other sections of the discs will appear stationary. The 67-4's range covers 22.703 to 4.186 CPS. External frequency divider extends frequency range. Stroboconn checks and measures rotational speeds and natural frequencies, calibrates precision oscillators and tachometers, and compares ratios between frequencies without regard for the actual frequencies involved.—C. G. Conn, Ltd., Elkhart, Ind.—TELE-TECH



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Cues for Broadcasters

(Continued from page 55) purposes. This is especially true when recording is done from the transmitter, with even remotes handled in the some way. To eliminate this trouble, and also to avoid bothering studio personnel who might be busy at the time when the circuit was needed, a dialing system was installed, enabling the transmitter operator to dial certain combinations of studio equipment.

The control voltage originates at the transmitter, and is fed on a simplex of the spare studio-transmitter line to the dial selector at the studio. It is a simple matter to pick up, say, the network line, bridge it into a booster amplifier, and feed it to the transmitter for recording, or monitoring. Or there might be a special audition recording-then the booster amplifier could be bridged across the audition circuit on the console. In other cases it was used to pick up a certain remote line.

Makeshift Camera Crane

URING the recent National Conventions in Chicago, NBC used an electric industrial truck designed especially for the occasion by the Automatic Transportation Co. of Chicago, to obtain high angle shots above the heads of the crowds. By allowing plenty of slack in the cables to the camera it was possible to provide limited horizontal movement as well as elevation to a height of 15 ft. above the ground. The Skylift's capacity of 6000 lbs. was not unduly strained by the weight of the cameraman, camera, and tripod!

NBC uses industrial truck as camera crane





These tubes are rugged plus! They're precision engineered and quality tested for maximum dependability under conditions of high shock, vibration, and temperature. The long life of these tubes is further assured by a special Sylvania "burn-in" process before testing.

Developed by Sylvania scientists especially for the U. S. Armed Services, these premium tubes are designed for a life expectancy (80% minimum, average life) of 5000 hours, under test conditions, in an ambient temperature of 30°C.

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THE GENERAL INDUSTRIES CO.

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Direct Frequency

(Continued from page 53)

Vibrotron, a vibrating-string device whose output is a FM acoustic signal. Consideration of suitable meters and indicators to utilize this signal has led to the following comparison of meters for AM and FM signals. It will be seen that PM can use some of the same meters useful for FM signals. Insofar as this is true, this article is pertinent to pulse systems. There are, however, very few pulse transducers in general use. Fig. 3 shows typical characteristics for a frequency and an amplitude transducer.

Standards

Since a measurement system is no better than the standards used for instrument calibration, it is worthwhile to look briefly at primary and secondary standards for amplitude and frequency measurements.

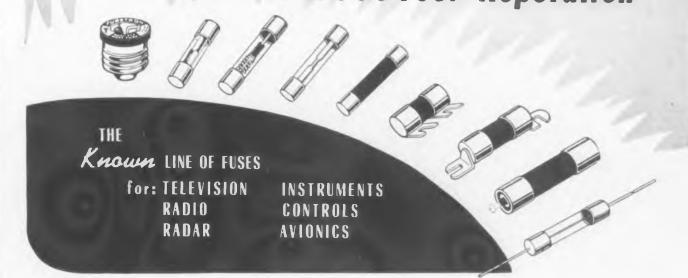
The absolute standard for voltageamplitude measurements is the saturated or normal Weston cell. Normal voltage of these cells is subject to variations so that the mean of a group of cells is used as the standard. The absolute accuracy is on the order of 1 part in 105, although secondary standards are claimed to be standardized with a precision of 1 part in 10°. The accuracy of primary standards is of less interest for voltage standards than for frequency standards since it is not possible to transmit standard voltage levels over wires or radio circuits. In commercial standardizing laboratories, economic and technical difficulties reduce accuracy to the order of 1 part in 10°, for voltage measurements.

Quartz Crystal Resonator

In contrast to standards of amplitude, there are many different methods by which accurate frequency standards can be established. The most accurate presently used are the quartz crystal resonator and atomic or molecular resonators. Although there is some discussion as to the absolute accuracy of primary standards, it is reasonable to take this figure as about 1 part in 108 or higher. Since standard frequencies can be transmitted from point to point, secondary frequency standards can be calibrated with relative ease and accuracy. Means are available for comparing two frequencies within 1 part in 1010. It is possible to buy, at relatively high cost, a secondary frequency standard accurate to 1 part in 10° over periods of several months.

(Continued on page 88)

BUSS FUSES Help Protect Your Product... Your Profit... Your Reputation



38 year's service to American homes, farms and industry is behind every fuse that bears the BUSS trademark. Your customers have confidence in BUSS... they know the BUSS name represents fuses of unquestioned high quality.

To maintain this high standard each and every BUSS fuse is tested in a highly sensitive electronic device that rejects any fuse that is not correctly calibrated — properly constructed and right in physical dimensions.

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IF YOU HAVE A PROTECTION PROBLEM

— We welcome requests for help in selecting the fuse or fuse mounting best suited to your conditions. Submit sketch or description showing type of fuse contemplated, number of circuits, type of terminals, and the like. Our staff of fuse engineers is at your service.

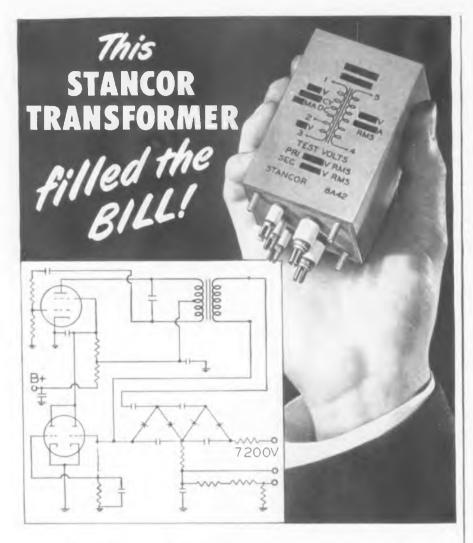
For More Information CLIP THIS HANDY COUPON NOW ...

BUSSMANN MFG, CO., Division McGraw Electric Company University at Jefferson St. Louis 7, Mo.

... *Plus*A COMPLETE LINE OF FUSE CLIPS, BLOCKS AND HOLDERS



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- Problem: \ To design and build a transformer to operate in an oscillating circuit at 1500 CPS.
 - √ Output voltage through a voltage quadrupler is to be $7200V \pm 5\%$ at 20 microamperes load.
 - √ Oscillating frequency and output voltage must remain stable from -40 °C to 65 °C and the unit must meet the requirements of MIL-T-27, grade 1, Class A, specifications for hermetically sealed transformers.

Solution: **STANCOR TRANSFORMER 8A42**

For the Answer to Your Toughest Problems of Transformer Design, Consult Stancor Engineers!

Stancor welcomes troublesome problems of transformer design, like the one illustrated, as a responsibility of leadership. We have the necessary engineering skill and resources, backed

by in-plant facilities for qualification testing of MIL-T-27 transformers. Next time you're faced with a transformer design problem, let our engineers offer you a quick, practical solution.



STANDARD TRANSFORMER CORPORATION

3572 NORTH ELSTON AVENUE, CHICAGO 18, ILLINOIS

At moderate cost, laboratory standards are available with accuracies of 1 part in 105 or better.

Cost Factor Same

On the basis of the above, it is reasonable to conclude that frequency can be measured at present to about 100 times the accuracy of voltage amplitudes. For practical measurements, the cost of the two is approximately the same. There are good reasons for the inherent superiority of frequency standards, based on the fact that frequencies can be multiplied or divided by extremely accurate methods. This property allows direct comparison of our primary frequency standards with very stable processes, such as the rotation of the earth or atomic and molecular motions. As yet, we have discovered no method of amplifying small energy changes by exact factors to give us comparable standards of voltage or current.

Part Two will appear in the November issue.

New NBS Booklet on Capacitor Paper Available

The new 10-page National Bureau of Standards Circular 532, Measurement of the Thickness of Capacitor Paper, by Wilmer Souder and S. B. Newman, is available from the Government Printing Office, Washington 25, D.C., for \$.15. The circular discusses the applications, limitations, instruments and data analysis involved in three measuring methods: 1) Direct observation across an edge ection by a micrometer microscope; 2) Measuring the separation of two geometric surfaces between which specimens are placed; and 3) Determining the mass of an area and computing thickness by means of a density parameter.

Test Equipment by Lloyd's Enterprises

Lloyd M. Jones, with KFI AM-FM-TV for 19 years and with KTTV for 11/2 years as operations engineer left KTTV the latter part of September to embark upon his own manufacturing business. The business will be known as LLOYD'S ENTERPRISES, Box 313, Altadena, Calif.

During the war he was with the Radiation Lab., Mass. Inst. of Tech., Cambridge, Mass., as a staff member. Projects included APG-1, APG-5, APG-8 and APG-15. He was with the XX Bomber Command in India and the Pacific during the latter part of the war as Liaison to General Curtis LeMay.

Test equipment for TV and electronic research will be entirely new types, not intended to compete with present types of equipment on the market.

4th Annual AES Convention

The fourth annual convention of the Audio Engineering Society will be held in conjunction with the Audio Fair at the Hotel New Yorker in New York City from October 29 to November 1. More than 100 manufacturers are participating with exhibits of professional and high fidelity audio equipment. Theme of the Fair is "Audio Today and Tomorrow."

The AES annual banquet will take place on Thursday Oct. 30 at 7:30 PM. There will be a binaural broadcast over station WQXR (AM & FM) from 9:05 to 9:30 PM. Among the technical papers scheduled for presentation are:

Binaural Disc Recording, Emory Cook, Cook Labs.

Methods of Measuring Surface Induction of Magnetic Tape, J. D. Bick, RCA Victor Div.

A New Magnetic Recording Tape, Edward Schmidt, Reeves Soundcraft Corp.

Constant Current Operation of Power Amplifiers, Howard T. Sterling, Waveforms, Inc.

A New Pocket Wire Recorder, O. Read, Radio and Television News Musical Therapy, R. L. Cardinell, Magnetic Programs Inc.

Gun Shot Reinforcers and Synthesisers, J. L. Hathaway, NBC.

The Deposited Carbon Resistor, L. B. Keim. Audio Consultant.

Electrolytic Capacitor, Why & When, Mark Vanbuskirka, P. R. Mallory & Co., Inc.

& Co., Inc.
Choice of Tubes for Audio Circuits,
W. R. Ayres, RCA Victor Div.

Review of New Printed Circuit Development and Audio, Frequency Application, A. W. Kelly, Jr. Photocircuits Corp.

Measurement of Non Linear Distortion, A. Bolch, Audio Instrument Co. Inc.

Distortion in Phonograph Reproduction, H. E. Roys, RCA Victor Div.

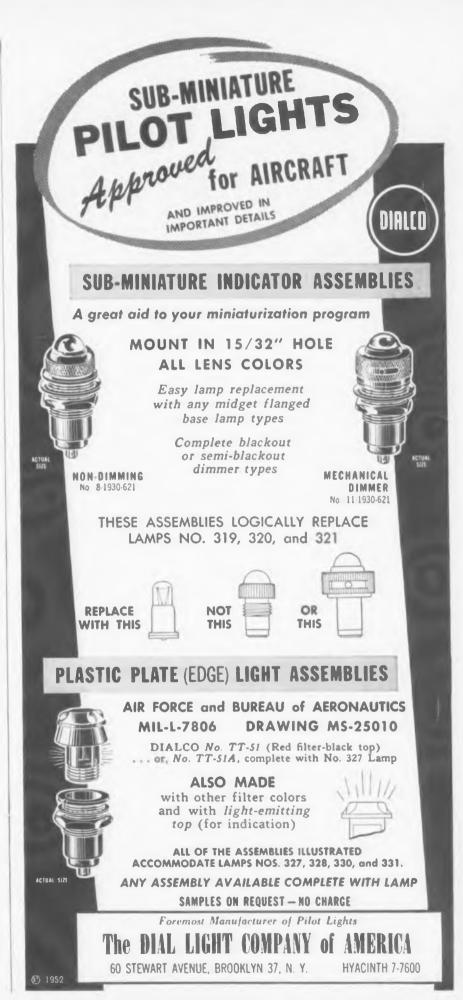
Basic Problems in Audio Systems
Practice, W. E. Stewart, RCA Victor Div.

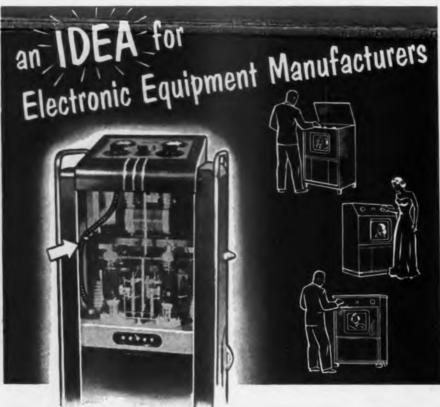
Audio Frequency Input Circuits, W. B. Snow, Vitro Corp. of Amer-

Design of Speech Input Colsoles for TV, Robert H. Tanner, Northern Electric Co., Ltd.

Consideration of Some Factors Concerning The Use of Audio Transformers, W. E. Lehnery, Audio Development Co.

Bypass and Decoupling Circuits in Audio Design, L. S. Goodfriend, Audio Instrument Co., Inc. (Continued on page 106)





Coupling with S.S.White Flexible Shafts Adds Flexibility to Your Designs!

The diathermy unit above shows how easy it is to control a hard-to-get-at circuit element from a conveniently placed control knob by means of an S.S.White flexible shaft. The shaft, which is especially designed for remote control duty, would, in fact, provide smooth, responsive tuning regardless of the relative location of the coupled parts.

By planning to use S.S.White flexible shafts as couplings between variable elements and their control knobs, you can get far greater flexibility in designing electronic equipment. Control knobs can be located wherever desired for better appearance, more convenient grouping and easier manipulation. Variable elements can be mounted to satisfy circuit, wiring and assembly requirements. Yes, when it's a question of control think of S.S.White flexible shafts.

SEND FOR THIS 256-PAGE FLEXIBLE-SHAFT HANDBOOK

Complete, authoritative information on flexible shaft construction, selection and application. Copy sent free if you write us direct on your business letterhead, giving your title. There's no obligation.



NEW YORK 16, N. Y.

THE Sublite INDUSTRIAL DIVISION
DENTAL MFG. CO. Dept. Q, 10 East 40th St.

Western District Office • Times Building, Long Beach, California

Core Materials

(Continued from page 42) tra-thin material have been made by a technique using ceramic spools on which the material is wound. The magnetic material and spool as a unit is annealed at the required high temperature to obtain the desired magnetic quality. Only a few turns of steel are used on each spool, but it is important that these few turns be well insulated from each other, and techniques of using magnesia powder for this purpose have been developed. The coil windings are put on this core by a toroidal winding machine.

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TELE-TEC

As electronic circuit development proceeds, these ultra-thin magnetic cores present a wide variety of possibilities. They have the big advantage in magnetic amplifier and



Fig. 8: Cores of Hiperthin 1/2-mil steel are wound on ceramic spools and then spot-welded

magnetic flip-flops in that they are far more rugged than vacuum tubes, require no replacement, and do not deteriorate in quality, thus insuring maintenance of accuracy.

After World War II and before the present emergency, some steps were taken to introduce these new developments in standard apparatus for commercial purposes, and great improvements were made, notably toward greater economy. A typical example of the start of this type of development was the application of five-mil Hipersil cores in the deflection yoke of a commercial TV receiver and the incorporation of standard Hipersil cores into the design of the power transformer for the receiver. This work had barely been started before the present emergency was upon us, but it did show that there are distinct performance and economy possibilities

1. C. C. Horstman, "Electrical Steel for Transformers—Thinner and Better." Westinghouse Engineer. July, 1944, p. 120.
2. J. K. Hodnette and C. C. Horstman. "Hipersil, A New Magnetic Steel and Its Use in Transformers." Westinghouse Engineer August, 1941, p. 52.



Arthur C. Omberg has assumed the directorship of engineering and research of the Bendix Radio Div. of Bendix Aviation Corp. He succeeds W. L. Webb who has been promoted to the company's central engineering staff.

Vice Admiral Carl F. Holden, USN (ret.) has been elected president of Federal Telecommunication Laboratories, Inc., Nutley, N. J., research unit of IT. & T. He has had extensive operational experience in communications. having served in 1942 and 1943 as Director of Naval Communications.





Karl E. Bretz has been named executwe vice president of Skottie Electronics. hc., Peckville, Pa., manufacturers of eramic, disc, plate and tubular capacitors. He was formerly affiliated with the Hi-Q div. of Aerovox Corp., Olean, N. Y. B. J. Garnett has been appointed asstant chief engineer of the airborne quipment div. of G. M. Giannini & Co., Pasadena, Calif.

Clyde R. Dupree has been named a development engineer for J. A. Maurer, Inc., Long Island City 1, N. Y., manufacturers of professional motion picture ameras and accessories.

Thomas Murphy has become chief ingineer of the Condenser Products Co. Company headquarters are at 7517 N. Clark St., Chicago 26, Ill.

James B. Lindsay, formerly vice president of Thomas Electronics. Inc., as been appointed special engineering epresentative of the Kahle Engineering Co., North Bergen, N. J.

C. P. Boggs has been appointed vice resident in charge of manufacturing of the Brush Development Co., Clevend, Ohio, He will direct all manufactwing activities of Brush products influding industrial and research instruents, acoustic devices, magnetic reiding equipment and piezo-electric ystals and ceramics.

Kenneth B. Boothe has been elected vice president of Audio & Video Deices Corp., 730 Fifth ave., New York N. Y. He was formerly manager of the company's instrumentation div.

Dr. Yuen T. Lo has been appointed engineer of Channel Master orp, Ellenville, N. Y.



Send today for free catalog and engineering bulletin.

> Toroidal Industrial Solenoid **Bobbin** Radio **Television**

> > COILS

Another "beat" by Bond! Here at last, is a true axial lead resistor with completely non-corrosive joints without the use of solders or fluxes. All the quality features and durability of Bond's widely acclaimed resistors. with new and ingenious innovations assuring better, longer performance! Protection plus . . . the new Bond resistors are absolutely protected from chassis or mounting surface, due to the true axial termination—affording greater dielectric path. Guaranteed to exceed the requirements for JAN R-93 type RB-51.

Bond resistors are made to all standard tolerances and are wound in a wide range of alloys to meet requirements of varying resistance values. They are built to customer specifications and Bond facilities are available for making the following custom-built coils:

Size Range Of The New Bond Axial Lead Resistors:

BOND	IN HE	B. BE	RESISTANCE RANGE		POWER RATING		· ·	- 11
	OVER- LENG INCH	OVER- DIA INCH	MIN. OHMS	MAX. MEG OHMS	COMM.	JAN.	FOUNT	٢
1515	11/10	3/8	1.0	0.42	1/3	1/4	RB51	
1516	11/16	3%	1.0	0.85	1/2	1/4	RB51	
1517	15/16	%	1.0	1.25	1.0			4
201	11/16	7/16	1.0	1.15	3/4	1/4	RB51	П

ELECTRONICS CORPORATION

60 SPRINGFIELD AVENUE, SPRINGFIELD, N. J.



For more than 18 years, Eclipse-Pioneer has been a leader in the development and production of high precision synchros for use in automatic control circuits of aircraft, marine and other industrial applications. Today, thanks to this long experience and specialization, Eclipse-Pioneer has available a complete line of standard (1.431" dia. X 1.631" lg.) and Pygmy (0.937" dia. X 1.278" lg.) Autosyn synchros of unmatched precision. Furthermore, current production quantities and techniques have reduced cost to a new low. For either present or future requirements, it will pay you to investigate Eclipse-Pioneer high precision at the new low cost.

*REG. TRADE MARK BENDIX AVIATION CORPORATION

AVERAGE ELECTRICAL CHARACTERISTICS-AY-200 SERIES**

	Type Humber	Input Voltage Nominal Excitation	Input Current Milliamperes	Impai Power Watts	Imput Impedance Ohms	Stater Output Veltages Line to Line	Reter Resistance (DC) Ohms	Stator Resistance (DC) Ohms	Maximum Error Sproed Minutes
	AY201-1	26V, 400~, 1 ph.	225	1.25	25+}115	11.8	9.5	3.5	15
Transmitters	AY201-4	26V, 400~, 1 ph.	100	0.45	45+j225	11.8	16.0	6.7	20
Receivers	AY201-2	26V, 400~, 1 ph.	100	0.45	45+j225	11.8	16.0	6.7	45
Centrol	AY201-3	From Trans. Autosyn	De	pendent	Upon Circuit (42.0	10.8	15	
	AY201-5	From Trans. Autosyn	De	pendent	Upon Circuit 1	250.0	63.0	15	
Resolvers	AY221-3	26V, 400~, 1 ph.	60	0.35	108+j425	11.8	53.0	12.5	20
	AY241-5	1V, 30~, 1 ph.	3.7	-	240+j130	0.34	239.0	180.0	40
Differentials	AY231-3	From Trans. Autosyn	De	pendent	Upon Circuit I	Design	14.0	10.8	20

*Also includes High Frequency Resolvers designed for use up to 100KC (AY251-24)

AY-500 (PYGMY) SERIES

Differentials	AY533-3	From Trans. Autosyn	Dependent Upon Circuit Design			45.0	93.0	30	
Resolvers	AY543-5	26V, 400~, 1 ph.	9	0.1	900+j2200	11.8	560.0	165.0	30
	AY523-3	26V, 400~, 1 ph.	45	0.5	290+j490	11.8	210.0	42.0	30
Control	AY503-5	From Trans. Autosyn	De	pendent (Upon Circuit Des	\$50.0	188.0	30	
	AY503-3	From Trans. Autosyn	De	pendent (Jpon Circuit Des	ign	170.0	45.0	24
Receivers	AY503-2	26V, 400~, 1 ph.	235	2.2	45+j100	11.8	23.0	10.5	90
Transmitters	AY503-4	26V, 400~, 1 ph.	235	2.2	45+ 100	11.8	25.0	10.5	24

For detailed information, write to Dept. B.

ECLIPSE-PIONEER DIVISION of

TETERBORO, NEW JERSEY



rt Sales: Bendes International Division, 72 Fifth Avenue New York 11, N. Y

Transatlantic TV

(Continued from page 67)

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(Continued from page 67)

a must, and other features or specialtie quite as well handled in the form of fin transported to be scanned. Private backing would further guarantee that the parallel experiences of overseas sound transmission and recording had been fully drawn upon especially in relation to their time- and frequency-sharing of facilities with overseat telephony and telegraphy.

Everyone connected with international cable and radio communication is bullish about economically increasing the sum total of facilities between the United States and Europe. When something comes long in the form of a radio relay or submarine cablink with a transmission band broad enough for television, it carries potentialities of revolutionizing all overseas communication, whether its realization is brought about by ner transistor techniques in direct underwate coaxials or by application of broad-band over-water radio jumps across the Arctic horizons.

You render a public service by keeping attention focussed on the possibilities.

You render a public service by keeping attention focussed on the possibilities.

You render a public service by keeping attention focussed on the possibilities.

You render a public service by keeping attention focussed on the possibilities.

You render a public service by keeping attention focussed on the possibilities.

Technical Solution Can Be Found

I can see that this could have tremendous possibilities and that if the funds were available a technical solution would be found.

G. E. GUSTAFSON Vice President in Charge of Engineering

Zenith Radio Corp. Chicago, Ill.

Military and Other Civil Uses **Would Justify Project**

Would Justify Project

While at a first glance Trans-Atlantic TV may appear to be impractical, serious consideration would support the theory that if the economics of a relay system via Canada Labrador, Greenland, Iceland, etc. can be satisfied, particularly by the inclusion of communication circuits which would provide consistently reliable telegraph and telephone communication, then the overall rout may well be justified.

The international exchange of television programs should be a powerful aid in the promotion of better understanding between continents. International communications require augmentation due to the increase of telephone and telegraph traffic. Militarily the system should have great strategic and tactical value.

I fully concur in your editorial of August 1952 that a competent technical committee should be appointed to investigate the feasibility and cost of a TV Trans-Atlantic system.

A careful study of the technical feasibility

A careful study of the technical feasibility and cost of the various systems being considered is necessary in order to establish the most satisfactory route to be utilized.

Considerable work has to be done in the study of propagation factors, in the design and production of equipment capable of handling the wide band widths required with satisfactory commercial signal noise ratios, and reliability of service.

The northern relay route proposed don not present insurmountable obstacles as radio stations have been in existence, staffed and maintained in these regions for many years.

J. J. KINGAN General Manager

Canadian Marconi Co., 2442 Trenton Ave., Montreal 16, Canada

Despite Difficulties Sees Trans-Atlantic TV a Future Certainty

Atlantic TV a future Certainty

Your letter addressed to the President and published in your August issue of Tele-Ted is very timely, and the action which you recommend very appropriate.

It is not clear to me what type of riograms would profitably be transmitted from Europe to the United States and from the United States to Europe. It is obviously possible to take moving pictures and to televist these. Hence, programs which do not require a contemporary broadcast would not result the every large expense of a transaction of the program requiring trans-Atlantic link. This might reduce the type program requiring trans-Atlantic links is political affairs and sports. In the field sports there is little in common between in United States and Europe. It is possible course, that the existence of a television in would alter this situation. In the political able interest. Here again some study would have to be made of the language barrier also of the time difference. For example, be-

France and the West Coast of the lied States there is a time difference in neighborhood of ten hours. Does this m that the broadcasting of programs a France to the West Coast is unsuit-

in that an arrance to the West Coast is a France to the West Coast is left for the form of the form of

aytheon Mfg. Co. Waltham 54, Mass.

Cost Not Formidable

Cost Not Formidable
Narom seems to be a necessity for UN use
of for NATO. An investment of the order
mamitude of the cost of the SS "United
lies" (which is only a fraction of the cost
an aircraft carrier") would seem to be
the in the national interest and to the
east of international relations. The cost of
a system is not so great that it would
set pivate enterprise from taking on the
moter if the treaty aspects could be armoded by the countries involved.

Oday we need the same quality of teleservice from New York to London, or
Buenos Aires, as we have to San Franm. If the means existed they would be
d. Here is a new challenge to creative
that can have a highly beneficial efthe on government and business.

MEADE BRUNET

V.P. & Managing Director
Division 30 Rockefeller

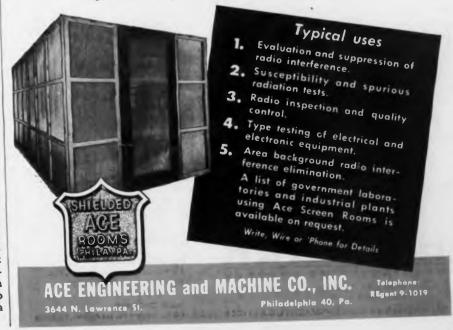
International
Division, 30 Rockefeller
Plaza, New York 20

Air Force Receives Global etwork Transmitters

Westinghouse Electric Corp., Balti-Md., reports the delivery of 375,000 worth of radio transmitters the USAF global network project. se transmitters will be part of a rld-wide communications network ground-to-ground and ground-tocontact with any Air Force base in world. Built to radiate signals up to miles, the transmitters have quency range of 2 to 30 MC.



10,000 mc. (or higher on special order)



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With mountings to your specifications or without mountings. Inductances held to $\pm \frac{1}{2}$ of 1%.

COMPLETE LINE INCLUDES:

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5/6" diameter x 7" long

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2417 Kenwood Ave., Ft. Wayne 3, Indiana

Irv. M. Cochrane Co. 408 So. Alvarado St., Los Angeles, California

Silk Screen

(Continued from page 63) quantity of the paint across the silk screen stencil with a single stroke of a rubber squeegee. The squeegee serves to force a thin film of paint through the stencil, depositing the pattern on the material being printed. Enamel is a satisfactory etchant resist for etching copper patterns with ferric chloride. It suggested that the first prints of any stencil be made on paper until the proper sharpness of definition has been achieved. A second resist pattern may be screened over the etched conductors for solder-din assembly.

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The finished screen and stencil are prepared for printing by first carefully locating the register guides. These are small pieces of material of the same thickness a the material to be printed, and are carefully taped or fastened to the printing base to guide the placement of the material to receive printing (Fig. 6). To locate the register guides, a piece of the base material is selected as a sample and is carefully located on the printing base in such a position that when the screen is brought down the stencil is in exactly the desired location. Two or more register guide are then carefully taped into position along any two adjacent sides of the samples. With these register guides each successive piece wil then be printed with the pattern of circuitry in exactly the same location. After the registers have been placed the screen may be masked

Masking

Masking is done by cutting piece of heavy Kraft paper to fit inside the screen; then, by holding the screen to the light, an area may be traced 2 in. larger than the stend pattern in each dimension. This area is removed. The remaining sheet of paper is securely taped into place. Masking tape should be applied completely around the outer edges of the paper, sealing to the frame. Tape is also used hold down the edges of the paper around the stencil. Tape 0.75 or 1 in. wide should be used and kept a least 0.5 in. back from any of the patterned circuitry of the stencil Masking is done to prevent a los of paint through the open areas the screen outside the stencil.

Regardless of printing medium used (enamels, asphaltum, conductive paints, resistor inks, etc.), i must be used freely as a lack of sufficient medium will cause drying and clogging of the screen and yield

imperfect prints.

The printing medium should be poured into the screen across one end of the stencil but not over any part of the pattern. The squeegee is brought down behind the paint and then brought across the stencil with a smooth steady motion (Fig. 7). If the paint is of the proper consistency a single stroke of the squeegee will usually produce a print of the finest definition. It may be found necessary to hold down the finished print when the screen is raised. This may be done by fastening a piece of tape under the printed material, adhesive side up. Commercially, vacuum arrangements are used to hold the pattern down during this release step.

Assuming the stencil to be adequate, there are two factors which greatly influence the quality of the prints. These are: (1) the sharpness, pressure and slant of the squeegee, and (2) the consistency of the paint. Also the bottom portion of the rubber squeegee should be cut sharply at a right angle and have sharp straight edges.

The squeegee pressure and slant must be determined by experience since they vary with each type of printing medium. A fairly light pressure with a 15° forward slant will usually produce satisfactory

resuits.

Paint Consistency

The viscosity of the paint is one of the most sensitive variables in good silk screen printing. A less viscous medium will produce a quicker drying print and will result in less screen clogging, but may produce more blots and smears. A paint that is thick will usually produce sharp clear prints but may display more mesh marks and unprinted areas with an increased tendency of the printed material to stick to the bottom of the screen.

In printing conductive paints, the thickness of the deposited paint may be controlled by adjusting the consistency and squeegee slant. A thin paint with little squeegee slant will usually result in a thin deposit of paint while a thicker paint with increased slant of the squeegee and light pressure will result in a heavler deposit of conductive paint.

Once printing is started, there should be as little delay as possible between prints. This will help avoid clogging of the screen by drying paint. If the screen should become clogged it may be cleaned either (Continued on page 96)

LIFESIZE PICTURE OF A GREAT BIG VALUE There's more to this Carbonneau Gold Cup 10-inch speaker than meets the eye, for the power-packed gold cup features a new magnetic structure, which is unmatched for compactness and efficiency. Write for details. CARBONNEAU INDUSTRIES, INC. GRAND RAPIDS 2, MICHIGAN

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by SUPREME





Every year more and more manufacturers are using Supreme meters as initial equipment in hundreds of electrical and electronic devices. Quality built in every respect with many outstanding features such as EFFICIENT ALNICO BAR MAGNET—SELECTED PIVOTS AND JEWELS—DOUBLE BRIDGE CONSTRUCTION—HIGH TORQUE MOVEMENT—STRONG TOUGH POINTER—RUGGED MOVING ELEMENT. Available in a variety of sizes and types with or without special dials. Write Supreme today about your meter needs. Requests for prices and delivery either street and delivery either street. delivery given prompt attention.

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of wiring and component parts for

DIELECTRIC BREAKDOWN with the BLISS HI-TRONIC TESTER

An electronic Hipot—an entirely new

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ABSOLUTE SAFETY TO OPERATOR

Practically currentless; no possibility of shock to operator.

PROTECTS EQUIPMENT UNDER TEST

Will not create arc on surface of faulty phenolic

HIGH SENSITIVITY

Unerringly detects faulty insulation or leakage between conductors or circuits,

ORAL ALARM SIGNAL

Unnecessary to keep eye on indicating lamp. Emits clear, loud signal

EASE AND SPEED OF OPERATION

Quick and easy viewing. Voltage is varied without shutting off tester. Also available in 5,000 & 10,000 volt units, continuous variable output.



- Guaranteed shockproof to operator.
- Sensitivity 1 megohm/per 100 volts. A switch is provided to reduce sensitivity when testing ca-pacitive circuits such as long multiple shielded multi-conductor
- Oral (buzzer alarm) indicator.
- No surface arcs (no damaging carbonizing).
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entirely or in part with the appropriate paint thinner. After printing the prints may be either air or oven dried.

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Silk screen printing of a resist pattern by the hand methods described herein is most practical for the printing of small or medium quantities where the cost of setting up the more elaborate processes would be prohibitive. Silk screening is especially suitable for the production of laboratory development models of prefabricated conductor patterns where small quantities and frequent changes requiring pattern revisions are involved.

Field Strength Meters

(Continued from page 46)

reflect radio signals. Such a rite was selected at Hybla Valley, Va. The setup is for the employment of both induction and radiation components of the standard field using horizontal polarization. Two posts are located 100 ft. apart and antenna masts provide for mounting the two antennas at ten-foot heights above the ground. The standard receiving antenna is a half-wave dipole which has been shortened slightly for self-resonant operation. It is constructed of small dural tubing, giving a large ratio of length to diameter. The transmitting antenna is similar to the receiving antenna and the associated equipment is housed in a small frame building about 200 ft. away. The building was specially constructed to contain a minimum of metal.

A standard signal generator, vacuum-tube voltmeter monitor, and balun similar to those used in the other tests on VHF field-strength meters are used at the field site. A portable heterodyne frequency meter is used in maintaining the frequency within about $\pm 0.1\%$. The balun is located immediately under the transmitting antenna and its output is connected through a balanced transmission line to the antenna input.

Voltage Measurements

The voltage induced in the standard receiving antenna by the standard field is measured with a balanced crystal voltmeter. The voltmeter consists of a type 1N28 crystal rectifier mounted in the center of the dipole antenna. The dc output is filtered by an RC network and measured by means of a portable precision potentiometer. For each day's test the crystal must be calibrated to determine the relationship between its dc output and r-f input. The ini-

(Continued on page 99)

tial r-f calibrating voltage to the crystal is determined by use of a calibrated 5-ma r-f vacuum thermoelement. The signal generator is tuned to about 50 or 100 Mc. Its output is attenuated in 3-db intervals by the standard piston attenuator used in the other tests. A balun converts to balanced output. This output is applied to the thermo-element. The crystal is connected across the thermo-element input through disctype dc isolation capacitors. Portable precision potentiometers are used to measure the dc ouptputs of the thermo-element and the crystal. Fig. 4 shows the arrangement of the equipment for this test.

Antenna Roda

Prior to beginning tests for determining the antenna coefficient of VHF field-strength meters, antenna rods of the proper length must be prepared for each frequency at which coefficient measurements are to be made. Although the transmitting antenna rods are not critical, they are made the same length as the receiving rods for convenience. Proper rods for the frequency to be used are put into place on the antenna mounts. Clamps on the antenna posts automatically align the antennas properly when the masts are put into place. A third mast is provided for mounting the antenna of the field-strength meter. VHF field-strength meters employ halfwave dipole antennas having adjustable rods

The signal generator is tuned to the desired frequency and connected to the transformer or balun. The transmitting antenna and the fieldstrength are meter's antenna mounted on their respective posts. The field-strength meter is located about 20 ft. away in line with the antenna, so that the observer will have minimum distorting effect upon the field. The portable potentiometer used to measure the crystal output is located nearby and is connected to the crystal through an ordinary twin-lead insulated line. The equipment arrangement is shown in Fig. 5.

With its antenna adjusted to the proper length, the field-strength meter is tuned to the signal frequency and adjusted for normal gain. The generator output is adjusted to give a convenient reading on the output meter of the field-strength meter. This reading is observed. The antenna is replaced by the standard receiving antenna and crystal output is observed. This is repeated at each frequency where an antenna coefficient is desired.

(Continued on page 100)

Medical Color TV

CBS has announced the appointment of Wilmot Castle Co., Rochester, N.Y., as exclusive sales agents of their industrial color TV system for medical applications. The equipment has already been installed at the U. of Chicago, U. of Kansas, U. of Penna., and at a European location.

The camera is mounted in the center of a cluster of four special lights, suspended over the operating table and focused on the operating field. The TV camera is remotely controlled from a booth overlooking the operating room. Closed circuits carry the scene to various locations in the hospital for instructional and supervisory purposes. A small microphone and headphone inside the surgeon's mask permits oral descrip-

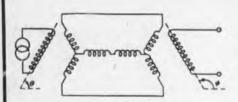
tion by him, and queries from the distant audience. A senior surgeon can monitor the operation from his office and speak privately to the operating surgeon over a separate audio system. The complete color TV camera and control equipment is approximately one-quarter of the size of present-day monochrome studio equipment.

Philco Appoints Radio VP

William H. Chaffee has been appointed vice-president of Philco's newly-formed Radio Div., headed by Larry F. Hardy, president of the division. Mr. Chaffee was named vice-president and director of purchases of Philco Corp. in 1949, and elected to the Board of Directors in 1950.



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The foregoing procedure applies to field-strength meters whose attenuators are in the i-f section of the instrument. In the case of field. strength meters having attenuators in the r-f circuit, antenna coefficients must be determined at each frequency for each position of the r-f attenuator. This presents the difficulty of requiring very small values of field strength at the lower attenuator steps, fields which are below the useful range of the standard receiving antenna and crystal voltmeter setup. For this test the equipment is connected as before (Fig. 5) with one exception: the vacuumtube voltmeter is replaced by a monitoring circuit consisting of a VHF radio receiver and a high-frequency. decade-type standard attenuator. The VHF receiver is connected through the standard attenuator to the output of the generator.

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With the field-strength meter set to its highest r-f attenuator position. a field-strength measurement is made in the same manner as before. The standard attenuator is set for maximum attenuation and the VHF receiver tuned to a reference indication. The field is then reduced to one-tenth of its original value by removing 20 db of attenuation from the standard attenuator and readjusting the generator output until the VHF receiver returns to the reference point. Further reductions in the field can be made in the same way over

a range of 1000 to 1.

Antenna Coefficient

The antenna coefficient is computed from the measurements by the formula K = E/MA, where

K = Antenna coefficient

 $E = Field strength, \mu v/m$

M = Output meter reading

A = Attenuator setting.

Corrected values of output meter readings and attenuator ratios as determined in the two previous tests are used in the computations. From the calibration curve of the crystal, the voltage induced in the standard antenna for each value of crystal output is obtained. The field strength E, is determined by the induced voltage and the effective length of the antenna. Thus, $\mathbf{E} = \mathbf{V}/\mathbf{L}_{\mathrm{H}},$ where

E = Field strength, µv/m

= Open-circuit voltage induced in the standard receiving antenna measured at the center, µv.

LH = Effective length of receiving antenna, meters.

Effective length of a transmitting antenna is defined as the length of an antenna which, if carrying a uniform current equal to the current flowing at the reference point of the actual antenna, will produce the same field strength as the actual antenna. The effective length is unchanged if the antenna is used as a receiving antenna. The effective length of the standard antenna used is approximately the same as for an infinitelythin halfwave dipole, i.e., λ/π meters. This results from the nearly equal and opposite effects of the finite antenna diameter on the current distribution and on the physical shortening for self-resonant opera-

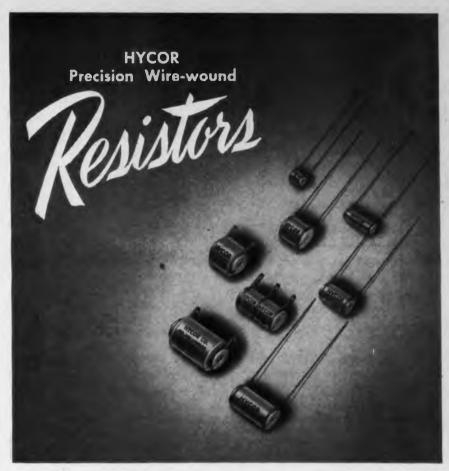
A brief history and description of the calibration services for commercial field-strength meters offered by NBS have been given. The usual calibration consists of determining the overall linearity, attenuator ratios, and antenna coefficients of the instrument. Overall linearity and attenuator ratio measurements are certified to $\pm 2\%$ from 10 KC to 300 Mc. Antenna coefficients are certified as follows: loop antennas, ±3% from 10 KC to 5 MC and ± 5% from 5 MC to 30 CM; dipole antennas, $\pm 10\%$ from 30 to 150 MC and $\pm 15\%$ from 150 to 300 MC.

F. M. Greene and M. Solow, "Development of Very-High-Frequency Intensity Standards," J. Research NBS RP 2100, 44, pp. 527-547, May 1950.
 IRE Standards on Radio Wave Propagation (Measuring Methods), pp. 1-8, 1942.
 F. M. Greene, "The Influence of the Ground on the Calibration and Use of VHF Field Intensity Meters," J. Research NBS RP 2062, 44, pp. 123-130. Feb. 1950.

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(Continued from page 56)

Noise Improvement Ratio (NIR) is

$$NIR = \frac{\sqrt{g_{P}}}{\begin{cases} 1 + \frac{2}{N_{O} \left[\frac{1}{N_{O}} \frac{N_{O}^{2}}{N_{O}} \frac{1}{2} \right]} \end{cases}}$$
(3)

where No is the ratio of average peak output noise to rms output noise. N is the signal-to-noise ratio defined above, $(\overline{V'_{ac}}^2)^{\frac{1}{2}}$ is the rms component of the noise on top of the pulse, and (Vac2) 1/2 is the rms component of the noise on the base line.

It is emphasized that the second detector does not itself produce an improvement in signal-to-noise ratio. Its function is to set up the conditions for signal-to-noise improvement by converting part of the noise energy into a dc voltage which can be readily eliminated from the output of the receiver.

Detector & Video Amplifier

At the input to the detector the noise is assumed to be "white," i.e., having a uniform spectrum within the i-f pass band, but after passage through the detector, beating of the harmonic components of the noise takes place, producing a triangular power spectrum at the output with the apex of the triangle at zero frequency, declining to zero power density at a frequency equal to the bandwidth of the i-f amplifier. The video amplifier affects this noise in two ways. It amplifies, and, unless video bandwidth is as wide as the i-f bandwidth, it filters out the higher harmonic components of the noise. In practical receivers the maximum bandwidth of the video amplifier does not exceed half the i-f amplifier bandwidth; hence filtering of the noise will occur. Although the video amplifier also filters out some of the very low frequency components of the noise signal, the output is not appreciably affected thereby except for filtering out the dc component of noise voltage.

Filter and Detector

It is convenient to consider the filter action of the video amplifier and the detector action of the second detector jointly. Let Vnii (t) represent the noise output from the i-f amplifier, which output is presumed to be uniform in frequency over a relatively narrow bandwidth (f_b-f_a) . (By relatively narrow is meant a center frequency between fa and fh which is of the order of ten times (f_b-f_a). The power density of the noise is equal to Wo in this band and

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The outputs are through a system of double jacks allowing a selection between balanced and unbalanced output depending on how the jack-plug is connected. All outputs are 5 volts across 600 ohms. Total distortion less than 1 %. The jacks are covered with snap covers to prevent dust and moisture from entering the units.

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Some amplifiers may be eliminated if a smaller number of outputs aré required. We have 25 other standard models. Our smallest model weighs less than one

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Laboratories

Precision Freq. Standards WILLIAMS BAY . WISCONSIN to zero outside it. The approximate expression for the power density of the continuous noise spectrum in the low frequency band is

We (f) =
$$\frac{\text{Wo}}{4\sigma} \left[1 - \frac{\text{f}}{(f_b - f_a)} \right]$$

for

The mean squared component of the low frequency noise is

where f_c is the cutoff frequency of the video amplifier. Since

$$\overline{v_{ac}^2} = \frac{f_c}{g_{ac}(f_b - f_a)} \left[2 - \frac{f_c}{(f_b - f_a)} \right] \cdot \left[\overline{v_{n|f}(t)} \right]^2 \qquad \text{(4)}$$

It is seen that Eq. (4) is the same as Eq. (2) to good approximation when $f_c = (f_b - r_a)$, i.e., when the video amplifier passes all of the harmonic components of the noise. At first sight it may be puzzling that apparently two different approaches should give essentially the same answer. Actually, these two approaches are one and the same. The theory from which Eqs. (1) and (2) are derived also accounts for the triangular noise spectrum. The only point of interest is that when determining the filtering action of the video amplifier, it is convenient to work with the equivalent power density spectrum from which the mean-squared noise voltage is obtained.

With reference to the video amplifier, there is one more consideration. In Eq. (4), $\overline{V_{ac}}^2$ is the mean-square low frequency noise appearing at the output of a network consisting of a linear detector followed by a low pass filter with a cutoff frequency equal to that of the video amplifier. To obtain the rms noise appearing at the output of the video amplifier, $(\overline{V_{ac}}^2)^{\frac{1}{2}}$ is multiplied by the voltage gain of the video amplifier. Thus the ms noise voltage at the output of the receiver (output of the video amplifier) is

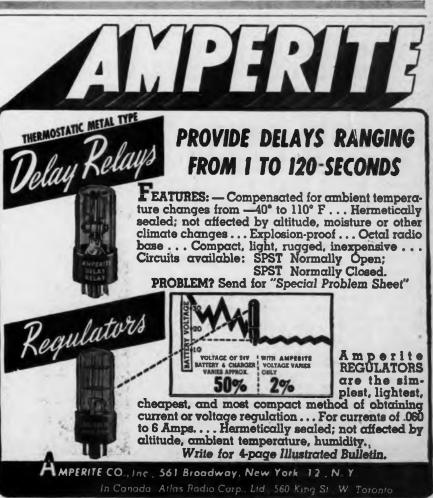
$$\left(\overline{v_{ac}}\right)_{3} : G_{\nu}\left(\overline{v_{ac}}\right)_{3}$$
 (5)

The specification of receiver sensitivity is designed to insure a given operation, but a knowledge of receiver noise figure will tell whether such operation is practicable. For example, one sensitivity specification for a radar receiver states in effect: "For an output pulse signal plus peak noise to peak noise ratio of 5 volts to 1 volt the input signal level to the receiver shall be 89 db below 1 volt." For this specification to be met, the noise figure of the receiver

(Continued on page 104)



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cannot exceed a certain value. If this maximum noise figure is too low to be achieved by the techniques available to the "state of the art," then the receiver with the required sensitivity cannot be built. Unless a detailed analysis of noise at the various functional levels of the receiver can be made from design considerations, the only recourse is to construct the receiver and try it out. A frequently used method for estimating receiver noise figures gives erroneous results because it fails to take account of the improvement possibilities provided by the second detector.

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This method consists in noting the specified signal-to-noise ratio at the output of the receiver and the specified input signal required to produce this signal-to-noise ratio. Then the ratio of the input signal to minimum theoretical noise is calculated, and the ratio of this quantity to the output signal-to-noise ratio is taken as the noise figure of the receiver. The method overlooks the division of noise in the output of the second detector into dc and ac components. a division which results in a favorable signal-to-noise indication in the output. Consequently, the noise figure of the receiver obtained by this method is better than the actual noise figure. To what extent this is true in an actual case is discussed in an example given later.

Receiver Noise Figure

Fig. 1 represents an installation for measuring receiver noise figure. The usual procedure is to read on the noise meter the noise output of the receiver for zero output from the diode noise generator. Then the output of the noise generator is increased until the reading on the noise meter is doubled. When this happens, the noise introduced to the input terminals of the receiver by the noise generator must equal the equivalent input noise of the receiver itself. As the noise generator is calibrated, the equivalent input noise voltage of the receiver is thus determined. The db ratio of the output noise voltage as read on the noise meter to this equivalent input noise voltage is the noise figure of the receiver in db.

Fig. 2 shows a pulse signal in the presence of receiver thermal noise as displayed on an oscilloscope. The relation between average peak noise and rms noise is indicated.

Once the properties of the noise in the second detector and video amplifier have been described, a summation of noise levels throughout the receiver is then straightforward. By

recording noise levels at various stages in the receiver, beginning with the specified output noise, it is possible to obtain a value for the input noise which is equivalent to the noise locally generated in the receiver. This input noise can then be compared with minimum theoretical noise to obtain the receiver noise figure. At the input terminals of the receiver the equivalent rms noise voltage is

$$\overline{[V_{nrf}](t)]^2}^{\frac{1}{2}} = \frac{K L_p \overline{V}_{acv}}{N_o G_v G_{if}}$$

where

$$K = \begin{cases} \frac{9 \cdot (t_{12} - t_a)}{t_c \left[2 - \frac{t_c}{(t_b - t_a)}\right]} \end{cases}$$

L is the loss factor in the preselector, Vacy is the average peak noise at the output of the video amplifier as read on an oscilloscope, No is the ratio of average peak ac output noise to rms output noise, G, is the voltage gain in the video amplifier, and Gif is the voltage gain in the i-f amplifier. The ratio of the noise voltage in Eq. (6) to the minimum theoretical noise voltage in rms volts (calculated for the noise bandwidth which is approximately the i-f amplifier landwidth) is the noise figure of the receiver. The difference of the noise voltage in Eq. (6) and the theoretical noise voltage, both expressed in db, is the noise figure of the receiver in db.

Sample Calculations

The relation for the "noise improvement ratio" is given in Eq. (3). Assume that the ratio of signal plus average peak noise to average peak noise is 5 and that the average peak noise is 1. A frequently used value for N_{..} is 2.5, so that $(\overline{V_{ac}}^2)^{\frac{1}{2}}$ is 0.4. Suppose also that \hat{V}_s is estimated to be 4. The ratio $(\overline{V'_{ac}}^2)^{\frac{1}{2}}/(\overline{V_{ac}}^2)^{\frac{1}{2}}$ is found to be about $\sqrt{2}$. Hence,

$$\frac{\sqrt{8^n}}{\left[1 + \frac{2}{2.5 \cdot (5 - 1.34)}\right]} = 4.1, \text{ or about 12 db noise improvement}$$

The noise level at the input to the eceiver is obtained from Eq. (6):

the case of an actual receiver the Parameters are: $L_p = 1.2$ (1.5 db); = 1 volt (average peak level); = 25 (8 db); $G_v = 3.2$ (10 db); $G_{\rm b} = 3.8 \times 10^{\rm s} \ (110 \ {\rm db}) \ (f_{\rm b} - f_{\rm a}) =$ Mc (i-f bandpass); and $f_c = 2.5$ Mc video cutoff).

These parameters, with two excepons, can be written down from a mere perusal of the specification. For mample Vacy is directly specified. The required overall gain can be duced readily from the specificaon of sensitivity. Gif and Gv can NI-TECH . Octaber 1952

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then be assigned more or less arbitrarily, provided their total contribution to gain is consistent with the required overall gain, any special receiver requirements, and sound technical practice. The quantity (f_b-f_a) is specified directly, and f_c is inferred from the pulse output rise time requirement. The two exceptions are No which is a constant, independent of the receiver, and L (the loss factor in the preselector) whose value can be assigned, to good approximation, from past experience.

In the construction of this receiver it proved advantageous to have a voltage stepdown between the output of the second detector and the video amplifier of 4 to 1. This does not, however, alter the assignment of the above parameters except that in effect we assign 12 db less gain to the i-f amplifier. If we compute the equivalent noise voltage at the input to the receiver, taking the values of the parameters as listed and including the 4 to 1 stepdown, we have the following:

$$K = \left[\frac{\theta - 4}{2.5 \left(2 - \frac{2.5}{8} \right)} \right]^{\frac{1}{2}} = 6.9$$

$$20 \log_{10} \frac{10}{\left[V_{\text{orf}} (t) \right]^{2}} = 20 \log_{10} \left[\frac{6.9 \times 1.2 \times 4 \times 1}{2.5 \times 3.2 \times 3.2 \times 10^{5}} \right]$$

$$= 9846 \text{ below 1 v. rms}$$

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This noise level must be compared with minimum theoretical noise to obtain the noise figure of the receiver. The minimum theoretical noise is obtained from the relation:

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Minimum Theoretical Noise Pow. $er = K T (\Delta f)_{NBW}$ where $(\Delta f)_{NBW}$ the noise bandwidth of the receiver, is approximately given by the i-f bandwidth. Since $K = 1.37 \times 10^{10}$ watts sec/cycle deg.; T = 290° Abs.; and $(\Delta f)_{NBW} = 8 \text{ Mc}$: Minimum Theoretical Noise Power = 1.38 × 10-11 imes 290 imes 8 imes 10 $^{\scriptscriptstyle 6}$ = 3.1 imes 10 $^{\scriptscriptstyle -14}$ watts = 135 db below 1 watt = 118 db below 1 v rms (assuming 50 ohm resistor).

Thus, the equivalent noise at the input to the receiver is 20 db above minimum theoretical noise, and this is the noise figure of the receiver. It is possible to check this with the aid of available receiver noise data (for a receiver which employs a 1N72 crystal as converter, the characteristics of which are similar to those for a 1N25) and the formula for receiver noise figure:

20 log 10 NF (Receiver) = 20 log 10 Lc (t + (N;1 - 1))

where $N_{tf} = 2$ (6 db); t = 2.5 (8 db), the crystal noise temperature; and $L_c = 2.5$ (8 db), conversion loss.

Thus, 20 log₁₀ NF (Receiver) = 18.9 db. This agrees rather well with

AES Program

(Continued from page 89)

RC Networks, Edward S. Sisson, Bell Sound Labs.

Attenuation Equalizers, F. R. Bies, Bell Telephone Labs., Inc.

Anaylzing the LP Pickup Problem, T. Lindenberg, Pickering & Co.

A New System of Variable Frequency Compensation, H. Leak, H. J. Leak & Co., Inc.

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RMS In Larger Quarters

RMS has moved to a new location at 2016 Bronxdale Ave., New York 60 N. Y., the site of a former sports club. The modern structure provides 45,000 sq. ft. of space for the firm's electronics production. The company's Antenna Div. will remain at West Farms Rd. in the Bronx.

a) ostalliz.

the noise figure of 20 db as obtained above.

It is interesting to compare this result with the noise figure of the receiver obtained by the method mentioned previously, which neglects division of noise into ac and de components in the detector output. The signal-to-noise ratio at the output of the receiver is approximately 12 db for a signal plus average peak noise to average peak noise ratio of 5 to 1. The noise level is 1 v. Thus, the signal is 20 db above rms noise. At the input to the receiver the corresponding signal is specified as 89 db below one volt (matched load). This is 29 db above minimum theoretical noise level. But since the signal at the output is 20 db above rms noise, the net increase in relative noise is 9 db, so, according to this method, the noise figure of the receiver is 9 db which does not agree with the experimentally determined value.

Conclusion

Quantitative relations have been derived from which the noise figure of a receiver can be calculated, knowing only the specified receiver sensitivity and the gain and loss parameters of the receiver. The theory is checked against measured data on a pulse receiver, and there is found to be good agreement with the receiver noise figure computed from measurement of the noise figure of the i-f amplifier, and data on the conversion loss and noise temperature of the crystal converter. The ability to estimate receiver noise figures correctly from design considerations alone is important because we can then state whether or not the specification of receiver sensitivity is realistic in advance of construction. Moreover, the noise figure can be readily computed, thus dispensing with the need for a noise generator and noise meter.

This paper was presented at the National Electronics Conference in Chicago, Oct. 1951.

Heyer Forms New Division

Heyer Products Co. of 471 Cordtland St., Belleville, N.J. announces the establishment of an electronic division to be headed by J. A. Van Auken, formerly with General Electric and Utility Electronics Corp. Previously Heyer Products manufactured for its own use only, but now engineering and manufacturing facilities for the production of transformers, meters, relays, switches and complete harnesses will be made available to the electronic industries.





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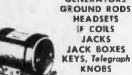
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"RESERVISOR"

(Continued from page 57)

two main parts, an address storage section and an inventory storage section, Fig. 3. Each plate has reserved for it 64 spots on the drum where the addresses for the inventories on that plate are stored. It should be noted that this enables one inventory or flight to appear on several plates as the same address may be stored in several spots. The inventory section is referenced only by the address stored in the address section of the drum and, therefore, one address will imply only one inyentory. Since the plates are used on any date of the ten day storage period, this one address may imply one of ten inventories, depending on the date used. From this, it is seen that the address for an inventory must be read before an inventory may be read. Each drum will hold approximately 200,000 digits and rotates at 1200 rpm.

Programming Standard

The programming is standard and slight variations are set up for one of three types of calls when that call comes in. See Fig. 4. The three most common call types are an availability check, a sale, and a cancellation. The following is a brief description of the operations performed by the machine for each call.

Availability: This first implies that eight flight legs or inventories will

be inspected. Read address for leg 1: open gate 1a into register 2 at proper time. Read inventory for leg 1; open gate 1b per address. From this subtract the number of seats (C) requested. If the remainder is greater than or equal to zero, remember leg 1, that is, line a into register 4. Read address leg 2. Read inventory leg 2. etc., until leg 8 is finished, Stop and send out legs whose remainder was greater than or equal to zero, output X, as an answer.

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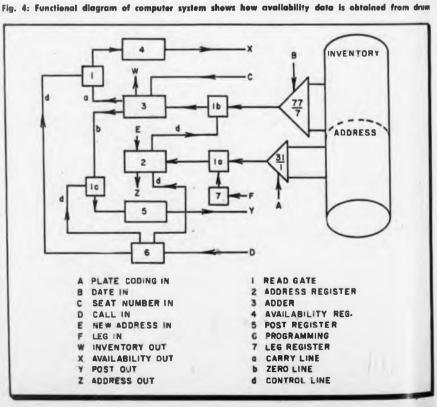
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Sell call: This implies that one or more, up to eight, legs or inventories will be looked at, e.g., two legs. The machine operations (see Fig. 4) are: Read address for first leg. From this subtract seats requested. If the remainder is greater than or equal to zero, go to second leg. If the remainder is greater than or equal to zero, go back to first leg and read address. Read inventory and from it subtract the number of seats requested. If the remainder is zero, line b, remember which leg it is by opening gate 1c to register 5. Write the remainder into the drum at the address of the first leg. Read out the remainder just written and check. Read address for second leg and so on as in the first leg. Stop. If zero was the remainder on any leg, send Post signal (flights sold out) and leg number to posting printer, output Y, On a cancellation, the same operation is done but the number of seats



are added to the inventory instead of being subtracted. Information coming from the drum is at a 20 KC rate.

Design Considerations

Maintenance and reliability were the main considerations in design. All working components, such as tubes, resistors, capacitors, and diodes are mounted in functional sub-assemblies and are easily interchanged. There are about 35 different types in the total 500 sub-assemblies such as, gates, counters, matrix, and binary arithmetic units. Some interesting statistics of the Reservisor central office equipment are: 5,000,000 soldered connections, 150 yards of coaxial cable, 1500 vacum tubes, 44 mi. of wire, and 1400 relays. Normal total power consumption is 6.45 kw.

Due to the 24 hour operation only two hours are allowed for the reservisor to be taken out of service for full testing. Each night during this time bias and plate voltages are lowered to produce marginal conditions. In this way, it is possible to replace units before they may cause trouble in service.

Special Features

Special features to the system include an instantaneous printed record of the flights that have been sold out. This is called a posting. One agent set near the loading gate is able to read the exact number of seats that are left on a plane at any particular time. At midnight one of the ten days of storage has gone out of date and, therefore, it is necessary to use the drum storage for the new tenth day. Under normal conditions this would mean that 1000 new inventories would have to be written into the drum. To avoid this time consuming task, a standard inventory for each of the 1000 inventories is stored in what is referred to as the Advanced Day Storage. Once every night the Advance Day inventories are copied into the new tenth day. On an average day, the reservisor handles about 22,000 calls into the machine, most of them occurring in a ten hour period.

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MAGNETRON TEST

(Continued from page 37)

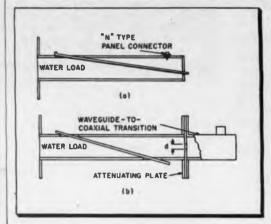




Fig. 5: (1) Two methods of sampling r-f in water load systems. Fig. 6: (r) R-F power moniter

pressing devices. The TE₀₁₁ mode is particularly useful in these cylindrical cavity resonators, since it does not require an electrical short between the tuning plunger and the cylinder walls. The details of design will not be described here, since they are a straightforward application of conventional procedures employing a so-called mode chart. Based on Technique of Microwave Measurements, by C. G. Montgomery, an S-band wavemeter with an average dispersion of 0.25 ${\rm MC}/0.001$ in. has been constructed with a ratio of $({\rm D}/{\rm L})^2 \sim 3$. The same design point has been used for an X_B-band wavemeter with a dispersion of 1.0 Mc/0.001 in.; while an Xband wavemeter with an average dispersion of 0.25 MC/0.001 in. was based on a (D/L)2 ratio of 0.5.

control grid so that thyratron plate current is permitted to flow. Whenever the r-f power level in the waveguide transmission line diminishes to the point at which the neon bulb is extinguished, a dc bias voltage appears on the thyratron grid, plate current ceases to flow, and the relay switch placed in series with the thyratron plate opens the circuits controlled by the monitor unit.

It is usually desirable to incorporate in the design of the unit a time delay of the order of, say, one second between the instant the neon bulb is de-ionized and the time when the switching action of the relay occurs, to guard against the test station being shut off owing to momentary arcing of the magnetron. This delay time can be controlled by the RC

R-F Power Monitor

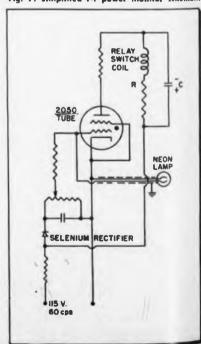
It may be desirable, particularly during unattended life-test runs of magnetrons, to monitor the microwave power output of the magnetron oscillator and to disconnect the high-voltage circuits (power supply, modulator) whenever the magnetron output power falls below a specified level. This can be accomplished by means of the compact monitor unit shown in Fig. 6, the essential components of which are illustrated in Fig. 7. In this device, a neon bulb is used as the r-f power-sensitive element.

The circuit consists of a thyratron tube with a 60 cps signal applied to its plate. The neon bulb, placed near the magnetron transmission line and connected to the monitor unit by means of a shielded two-wire cable, is ionized by the leakage r-f power radiated from the water load. When ionized, the neon bulb removes the dc bias voltage from the thyratron

Fig. 7: Simplified r-f power monitor schema

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combination in the thyratron plate circuit shown in the diagram.

The examples of specific microwave devices employed in the testing of magnetrons have served, it is hoped, to illustrate the method of approach, which is to make use of the relatively high power levels and the limited range of operating frequencies peculiar to magnetron os-cillators. The proper use of these, and similar, instruments may greatly reduce testing time on a magnetron test facility called upon to handle appreciable quantities of magnetron tubes and serviced by semi-skilled operators.

ODR ANTENNA

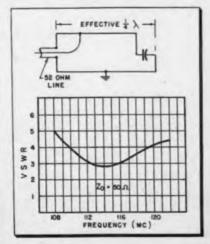
(Continued from page 59)

Antenna AT-(XA-109)/ARN-14 is a special Omni-Directional Range Receiving antenna for use with Radio Set AN/ARN-14 in F-90 aircraft. It



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RG-8/U or similar 52 ohm coaxial cable is used in connecting the antenna to the radio set. One antenna is installed on each side of the nose of the F-90 aircraft and the two are fed in p opposition through a balun, thus obtaining 360°



aircraft pattern coverage. This zero-drag antenna is described in USAF Specification No. X-7197. Weight of the unit is 8 lbs. Its size is: everall length, 26 in.; everall width, 18 in.; everall depth, 7 in.; length of element, 23 in.; and width of element, 7 in.







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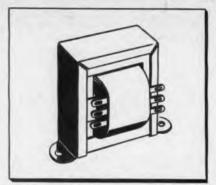
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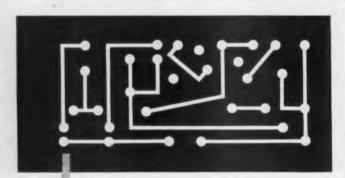
featured are two continuously variable blas supplies of 0 to -150 voits dc stabilized. Ripple of all the outputs is less than 10 my. Separate meters monitor output voltage and current of each supply.—Oregon Electronic Mfg. Co., 2232 East Burnside St., Portland 15, Ore.—TELE-TECH

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cable	9.0	ZA	microwave		HA	impedance		BBH	control, studio	15	PAF
color, miscl.	10	KH	police, etc.		DA	resistance		BBI	control, video		MK
lighting		NA	remote pickup	. 2	BA	Cabinets	. 33	HHA	dubbing, audia		PM
RICTOWGYE	7	GD	remote pickup, video	16	QB	Cable		DDA	fixture		HHC
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liniting	12	MB	Bases, antenna	. 4	DB	ceramic		DDC	video		MT
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mixing		PE	Batteries, dry	31	FFA	mica		DDE	Cranes, camera		CF
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remote, aud o	15	PJ	manuals, tube		בונ	Clarks 0 Charman Area	33	ННВ	Devices, anti-static	. 23	XA
remote PU, cudio	17	RA	manuals, TV maintenan		סונ	Connectors, cable		ZB	indicating, miscl.		CCH
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And -	12	MC	reports & digests, FCC	34	JJF	power		Zi.	servo	9.4	Y A
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The basic TC-4A (left-hand and center sections) with a master monitor (right-hand section) as normally used at the transmitter (i.e., no video origination at this location).



The same setup with a film comera control unit added (at the left) for programming of slider and films from the transmitter—or far small stations without "live" stations.

A Control Canaole (3rd and 4th units from left) and with three monitor sections to provide with striles operating control from a position to benamitter room, in this arrangement the first of the consolie (starting from the low) is the "live" of the consolie (starting from the low) is the "live" or centrol and monitor, the second is a film a centrol, the third unit contains south federa with and video switching, the fourth unit contains and video switching and remetely located equipal sentrals, the fifth unit is the line massier member, and video amplifiers, power supplies, other with the contains of the contains and video amplifiers, power supplies, other laws of the contains and with any RCA TV transmitter. It was a supplier of the contains and walls video fortilities can, and the used with any RCA TV transmitter.



FC-4A with mixing mental and, provine module and, and her lamen control with land two and are the as two time. If desired, restaurs can be consequed to shape of Library to the control of the



Similar sature with two common relified until two live and non-film at two films, such at upod to the RCA "Bess Buy" for FV.

then be assigned more at less arbitrarily provided their total contribution to gain is consistent with the required overall gain, any special receiver requirements, and sound technical practice. The quantity (f = f_i) is specified directly, and f_c is inferred from the pulse output rise time requirement. The two exceptions are N which is a constant, independent of the receiver, and L_{ij} (the loss factor in the preselector) whose value can be assigned, to good approximation, from past experience.

In the construction of this receiver it proved advantageous to have a voltage stepdown between the output of the second detector and the video amplifier of 4 to 1. This does not, however, alter the assignment of the above parameters except that in effect we assign 12 db less gain to the 1-f amplifier. If we compute the equivalent noise voltage at the input to the receiver, taking the values of the parameters as listed and including the 4 to 1 stepdown, we have the following:

$$80 = 3 \cdot \left(\frac{v_{-1}}{4.5 \left(2 - \frac{2.5}{3.5}\right)}\right)^{2} = 6.9$$

$$80 = 3 \cdot \left(\frac{v_{-1}}{4.5 \cdot \left(2 - \frac{2.5}{3.5}\right)}\right)^{2} = 6.9$$

$$80 = 3 \cdot \left(\frac{v_{-1}}{4.5 \cdot \left(2 - \frac{2.5}{3.5}\right)}\right)^{2} = 6.9$$

$$= 990 \text{ permaitive } 1 \cdot v_{-1} = 3.5$$

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This noise level must be compared with minimum theoretical noise to obtain the noise figure of the receiver. The minimum theoretical noise is obtained from the relation:

were for the contract

Minimum Theoretical Noise Power = K T (Δf)_{NBW} where (Δf)_{NBW}, the noise bandwidth of the receiver, is approximately given by the i-f bandwidth. Since K = 1.37 × 10⁻²³ watts see cycle deg.; T = 290 Abs.; and (Δf)_{NBW} = 8 Mc: Minimum Theoretical Noise Power = 1.38 × 10⁻²³ 290 8 × 10⁻¹ = 3.1 × 10⁻¹⁴ watts = 135 db below 1 watt = 118 db below 1 v rms (assuming 50 ohm resistor).

Thus, the equivalent noise at the input to the receiver is 20 db above minimum theoretical noise, and this is the noise figure of the receiver. It is possible to check this with the aid of available receiver noise data (for a receiver which employs a 1N72 crystal as converter, the characteristics of which are similar to those for a 1N25) and the formula for receiver noise figure:

20 100 10 WF (Receiver) = 20 log 10 Lc (t = (H/f + 1))

where $N_{1f} = 2$ (6 db); t = 2.5 (8 db), the crystal noise temperature; and $L_c = 2.5$ (8 db), conversion loss.

Thus, 20 \log_{10} NF (Receiver) = 18.9 db. This agrees rather well with

AES Program

(Continued from page 89)

RC Networks, Edward S. Sisson, Bell Sound Labs.

Attenuation Equalizers, F. R. Bies, Bell Telephone Labs., Inc.

Anaylzing the LP Pickup Problem, T. Lindenberg, Pickering & Co.

A New System of Variable Frequency Compensation, H. Leak, H. J. Leak & Co., Inc.

Concert Hall Realism Through the Use of Dynamic Level Control, J. Nigro and J. Minter, Measurements Corp.

Testing & Adjusting Speaker Installations with the Sound-Survey Meter, W. R. Thurston, General Radio Co.

RMS In Larger Quarters

RMS has moved to a new location at 2016 Bronxdale Ave., New York 60, N. Y., the site of a former sports club. The modern structure provides 45,000 sq. ft. of space for the firm's electronics production. The company's Antenna Div. will remain at West Farms Rd. in the Bronx.

the noise figure of 20 db as obtained above.

It is interesting to compare this result with the noise figure of the receiver obtained by the method mentioned previously, which neglects division of noise into ac and de components in the detector output. The signal-to-noise ratio at the output of the receiver is approximately 12 db for a signal plus average peak noise to average peak noise ratio of 5 to 1. The noise level is 1 v. Thus, the signal is 20 db above rms noise. At the input to the receiver the corresponding signal is specified as 89 db below one volt (matched load). This is 29 db above minimum theoretical noise level. But since the signal at the output is 20 db above rms noise, the net increase in relative noise is 9 db. so, according to this method, the noise figure of the receiver is 9 db which does not agree with the experimentally determined value

Conclusion

Quantitative relations have been derived from which the noise figure of a receiver can be calculated, knowing only the specified receiver sensitivity and the gain and loss parameters of the receiver. The theory is checked against measured data on a pulse receiver, and there is found to be good agreement with the receiver noise figure computed from measurement of the noise figure of the i-f amplifier, and data on the conversion loss and noise temperature of the crystal converter. The ability to estimate receiver noise figures correctly from design considerations alone is important because we can then state whether or not the specification of receiver sensitivity is realistic in advance of construction. Moreover, the noise figure can be readily computed, thus dispensing with the need for a noise generator and noise

This paper was presented at the National Electronics Conference in Chicago, Oct. 1951.

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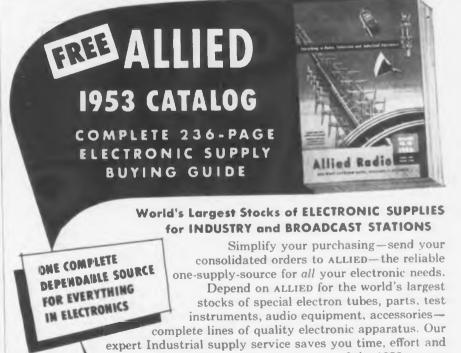
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"RESERVISOR"

(Continued from page 57)

two main parts, an address storage section and an inventory storage section, Fig. 3. Each plate has reserved for it 64 spots on the drum where the addresses for the inventories on that plate are stored. It should be noted that this enables one inventory or flight to appear on several plates as the same address may be stored in several spots. The inventory section is referenced only by the address stored in the address section of the drum and, therefore, one address will imply only one inventory. Since the plates are used on any date of the ten day storage period, this one address may imply one of ten inventories, depending on the date used. From this, it is seen that the address for an inventory must be read before an inventory may be read. Each drum will hold approximately 200,000 digits and rotates at 1200 rpm.

Programming Standard

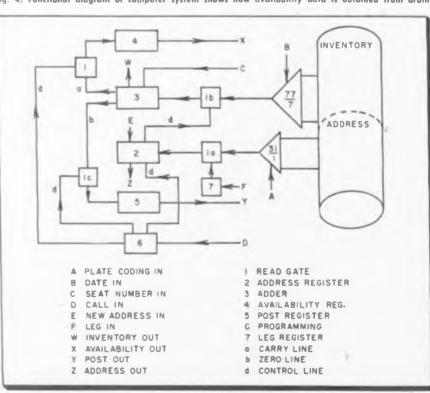
The programming is standard and slight variations are set up for one of three types of calls when that call comes in. See Fig. 4. The three most common call types are an availability check, a sale, and a cancellation. The following is a brief description of the operations performed by the machine for each call.

Availability: This first implies that eight flight legs or inventories will

be inspected. Read address for leg 1; open gate 1a into register 2 at proper time. Read inventory for leg 1; open gate 1b per address. From this subtract the number of seats (C) requested. If the remainder is greater than or equal to zero, remember leg 1, that is, line a into register 4. Read address leg 2. Read inventory leg 2, etc., until leg 8 is finished. Stop and send out legs whose remainder was greater than or equal to zero, output X, as an answer.

Sell call: This implies that one or more, up to eight, legs or inventories will be looked at, e.g., two legs. The machine operations (see Fig. 4) are: Read address for first leg. From this subtract seats requested. If the remainder is greater than or equal to zero, go to second leg. If the remainder is greater than or equal to zero, go back to first leg and read address. Read inventory and from it subtract the number of seats requested. If the remainder is zero, line b, remember which leg it is by opening gate 1c to register 5. Write the remainder into the drum at the address of the first leg. Read out the remainder just written and check. Read address for second leg and so on as in the first leg. Stop. If zero was the remainder on any leg, send Post signal (flights sold out) and leg number to posting printer, output Y. On a cancellation, the same operation is done but the number of seats

Fig. 4: Functional diagram of computer system shows how availability data is obtained from drum



are added to the inventory instead of being subtracted. Information coming from the drum is at a $20~{\rm KC}$ rate.

Design Considerations

Maintenance and reliability were the main considerations in design. All working components, such as tubes, resistors, capacitors, and diodes are mounted in functional sub-assemblies and are easily interchanged. There are about 35 different types in the total 500 sub-assemblies such as, gates, counters, matrix. and binary arithmetic units. Some interesting statistics of the Reservisor central office equipment are: 5,000,-000 soldered connections, 150 yards of coaxial cable, 1500 vacum tubes. 44 mi. of wire, and 1400 relays. Normal total power consumption is 6.45

Due to the 24 hour operation only two hours are allowed for the reservisor to be taken out of service for full testing. Each night during this time bias and plate voltages are lowered to produce marginal conditions. In this way, it is possible to replace units before they may cause trouble in service.

Special Features

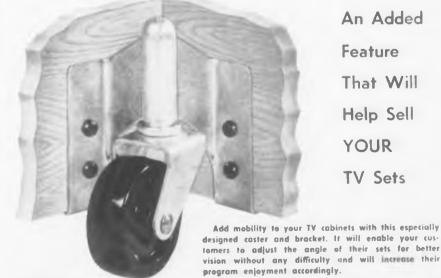
Special features to the system include an instantaneous printed record of the flights that have been sold out. This is called a posting. One agent set near the loading gate is able to read the exact number of seats that are left on a plane at any particular time. At midnight one of the ten days of storage has gone out of date and, therefore, it is necessary to use the drum storage for the new tenth day. Under normal conditions this would mean that 1000 new inventories would have to be written into the drum. To avoid this time consuming task, a standard inventory for each of the 1000 inventories is stored in what is referred to as the Advanced Day Storage. Once every night the Advance Day inventories are copied into the new tenth day. On an average day, the reservisor handles about 22,000 calls into the machine, most of them occurring in a ten hour period.

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MAGNETRON TEST

(Continued from page 37)

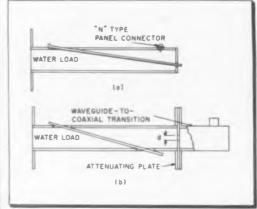




Fig. 5: (1) Two methods of sampling r-f in water load systems. Fig. 6: (r) R-F power monitor

pressing devices. The TEon mode is particularly useful in these cylindrical cavity resonators, since it does not require an electrical short between the tuning plunger and the cylinder walls. The details of design will not be described here, since they are a straightforward application of conventional procedures employing a so-called mode chart. Based on Technique of Microwave Measurements, by C. G. Montgomery, an S-band wavemeter with an average dispersion of 0.25 MC/0.001 in. has been constructed with a ratio of $(D/L)^2 \sim 3$. The same design point has been used for an X_B-band wavemeter with a dispersion of 1.0 Mc/0.001 in.; while an Xband wavemeter with an average dispersion of 0.25 MC/0.001 in. was based on a (D L)2 ratio of 0.5.

control grid so that thyratron plate current is permitted to flow. Whenever the r-f power level in the waveguide transmission line diminishes to the point at which the neon bulb is extinguished, a dc bias voltage appears on the thyratron grid, plate current ceases to flow, and the relay switch placed in series with the thyratron plate opens the circuits controlled by the monitor unit.

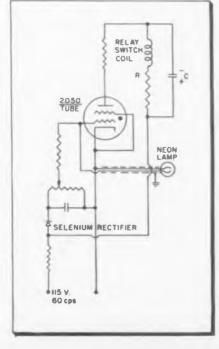
It is usually desirable to incorporate in the design of the unit a time delay of the order of, say, one second between the instant the neon bulb is de-ionized and the time when the switching action of the relay occurs, to guard against the test station being shut off owing to momentary arcing of the magnetron. This delay time can be controlled by the RC

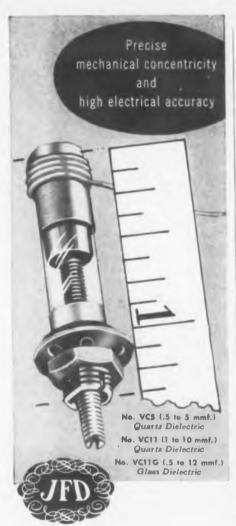
R-F Power Monitor

It may be desirable, particularly during unattended life-test runs of magnetrons, to monitor the microwave power output of the magnetron oscillator and to disconnect the high-voltage circuits (power supply, modulator) whenever the magnetron output power falls below a specified level. This can be accomplished by means of the compact monitor unit shown in Fig. 6, the essential components of which are illustrated in Fig. 7. In this device, a neon bulb is used as the r-f power-sensitive element.

The circuit consists of a thyratron tube with a 60 crs signal applied to its plate. The neon bulb, placed near the magnetron transmission line and connected to the monitor unit by means of a shielded two-wire cable, is ionized by the leakage r-f power radiated from the water load. When ionized, the neon bulb removes the dc bias voltage from the thyratron

Fig. 7: Simplified r-f power monitor schematic





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world's largest manufacturer of TV antennas & accessories combination in the thyratron plate circuit shown in the diagram.

The examples of specific microwave devices employed in the testing of magnetrons have served, it is hoped, to illustrate the method of approach, which is to make use of the relatively high power levels and the limited range of operating frequencies peculiar to magnetron os-cillators. The proper use of these, and similar, instruments may greatly reduce testing time on a magnetron test facility called upon to handle appreciable quantities of magnetron tubes and serviced by semi-skilled operators.

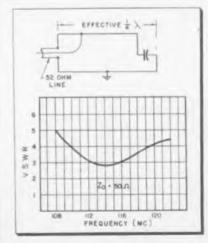
ODR ANTENNA

(Continued from page 59)

Antenna AT-(XA-109) ARN-14 is a special Omni-Directional Range Receiving antenna for use with Radio Set AN/ARN-14 in F-90 aircraft. It



is in the experimental development category. it operates over the frequency range of 108 through 122 MC, and is horizontally polarized. RG-8/U or similar 52 ohm coaxial cable is used in connecting the antenna to the radio set. One antenna is installed on each side of the nose of the F-90 aircraft and the two are fed in phase opposition through a balun, thus obtaining 360°



aircraft pattern coverage. This zero-drag an-tenna is described in USAF Specification No. X-7197, Weight of the unit is 8 lbs. Its size is: overall length, 26 in.; overall width, 18 in.; overall depth, 7 in.; length of element, 23 in.; and width of element, 7 in.







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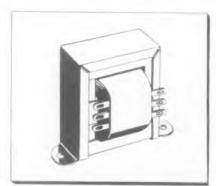
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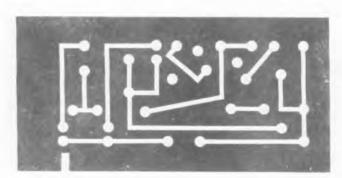
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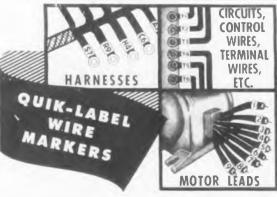
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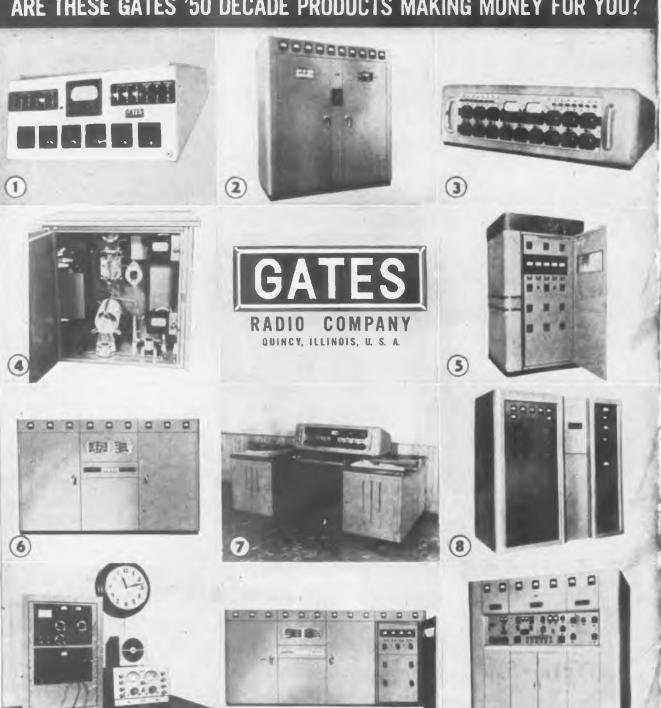
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Batteries

Power Supplies

ARE THESE GATES '50 DECADE PRODUCTS MAKING MONEY FOR YOU?



- 52-CS Studioette Speech Console.
- BC-1F Air-conditioned 1KW Broadcast Transmitter.
- 3. SA-50 Dual Channel Speech Console.
- 4. Gates Antenna Coupling Equipment.
- 5. Typical 4-Tower Centralized Phasing Cabinet.
- 6. HF5-10 High Frequency Phone and Telegraph Transmitter.
- SA-40 Single Channel Speech Console on CB4 Control Desk.
- 8. GY-48 Complete 250 watt. Radio Broadcasting Station.
- 50-watt Telephone and Tele-graph Communications Trans-mitter.
- IO. BC-5B 5KW Transmitter with Phasor.

(10)

HF-15 15,000-watt Telegraph Transmitter. 11.

(11)

MUST

TELE-TECH's

STATION & STUDIO EQUIPMENT

1953 DIRECTORY 1953

TV-FM-AM MICROWAVE--C:VILIAN MILITARY

Making available to all users and potential users of station and broadcast equipment, a complete listing of every manufacturer of communications equipment in whose product they are likely to be interested.

Designed also as a compilation of "end products," this Equipment Directory includes listings of all major replacement parts for communication equipment. Manufacturers who build and design government and military equipment are also presented.

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lighting	13	NA	remote pickup	2	BA	Cabinets		HHA	dubbing, audio		PM
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Centralized Control... with



tailored switching and monitoring

TC-4A Control Console combines Audio-Video
Switching with Transmitter Control—makes it
possible to centralize all operations at one position

Now you can do all (or any desired part) of your audiovideo switching right in your transmitter room . . .

And you do not have to take a fixed group of units to do it. You can have whatever group of audio and video facilities you need to fit your particular requirements. Moreover, you can add further audio and video facilities as needed.

You get this economy and flexibility by building your equipment layout around the new TC-4A Control Console. The TC-4A is a two-section unit containing basic switching facilities for handling up to 8 audio and 8 video signals (remote or local). It can fade to black and "program-switch" network, remote, film, and local studio signals. Up to twelve signals can be monitored including transmitter operation.

To this two-section unit you can add as many console sections (for "on-air" monitor, preview monitor, individual camera monitors) as you need to take care of your individual requirements. In this way you can build up a "centralized" control position from which one man can (if necessary) perform all operations.

Moreover, you do all of this with standard RCA units exactly like those used by the largest stations and the networks. Thus, if you decide later to expand to a multiple studio layout you can very easily rearrange these same units for that type of setup.

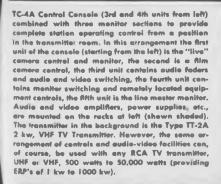
Remember . . . in TV it's good business to buy the best to begin with.



The basic TC-4A (loft-hand and conter sections) with a master mentior (right-hand section) as normally used at the transmitter (i.e., no video originals on at this location).



The same sotup with a film camera control unit added (at the left) for programming of slides and films from the transmitter—or for small stations without "live" studies.





TC-4A with master monitor unit, preview mention unit, and two comerc control units some live and one film or two film). If desired, pections can be arranged United to the Control of the weighted provided to the control of the contr



Similar satup with two comerc control units (and five and one film, or two film), such as uned in the RCA "Racis flow" for TV.



RADIO CORPORATION OF AMERICA
ENGINEERING PRODUCTS DEPARTMENT CAMDEN, N.J.

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TYPE 313 5000 WATT TRANSMITTER

The CONTINENTAL Type 315
Transmitter, at left, offers a deluxe design for 5 KW AM operation. It has many features not ordinarily incorporated in transmitters of this class, including special equipment for matching transmitter output into sharply tuned loads often encountered in directional arrays.

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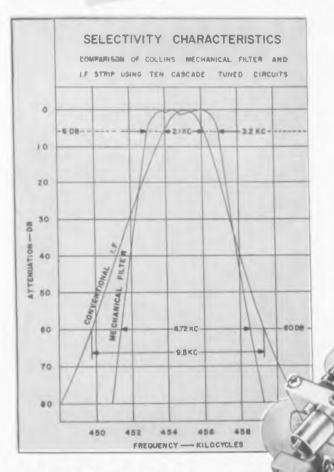
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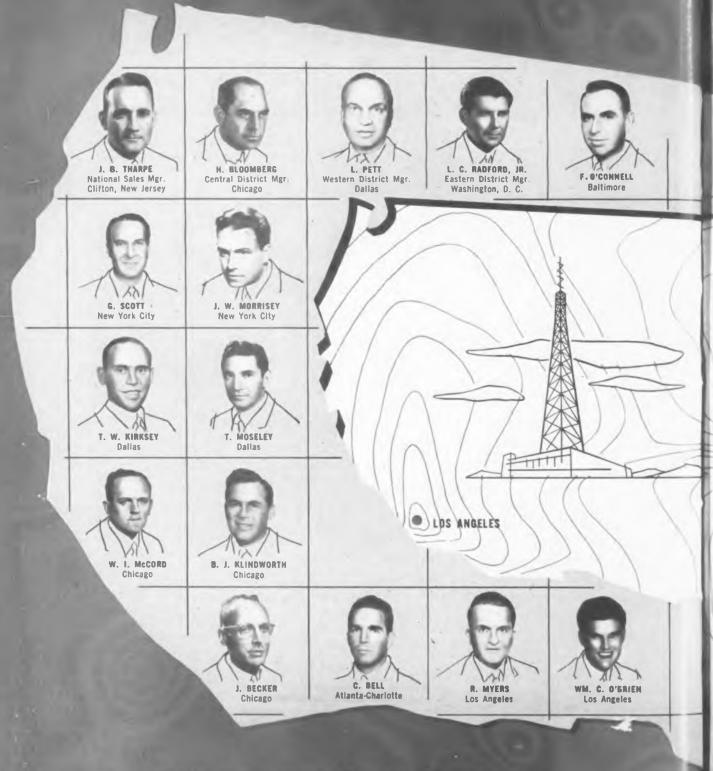
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4 Margolin, Sheridan Ave Bethpage, L. I., N. Y. -BA Du Mont Labs., Allen B., 1500 Main Ave., Clifton, N. J. BA BB BC, BD, BF, BG, BJ BK

Eidson Electronic, 1802 N. Third St., Temple, Tex.—BE
Electronic Development Lab., 43-07, 23rd Ave., Long
Island City 5, N. Y.—BB, BC, BD, BG, BK
Electronic Research 4, Mfo., 1420 E, 25th St., Cleveland 14, Ohio—BB, BI
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Insuline Corp., of America, 36-02 35th Asc., Long Island
City 1 V.—BA, RL,
International Research Associates, Div. of Iresco., Inc.,
2221 Warwick Ave., Santa Monica, Calif.—BC, BF,
RG, RJ

Kalbfell Labs., Box 1578, San Diego 10, Calif.—BI Kepco Labs., 131-38 Sanford, Flushing 55, N. Y.—BU, BG Kings Electronics, Inc., 50 Marbledale Ave., Tuckaboe. Kings Microwave Co., 50 Marbledale Ave. Tuckahoe, V - RA, BF Knights Co., James, Sandwich, III.— BE

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Nebel Labs., R. E., 1104. Lincoln Place, Brooklyn 13,
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Opad-Green Co., 71 Warren St., New York 7, N. Y .-BC. BG. Oregon Corvek, 1005 N.W. 16th Ave., Portland 9, Ore.

Pacific Mercury Television Mfg., 5955 Van Nuys Blvd., Van Nuys, Calif.—BG, BH, BI, BJ Pederson, Electronics, P.O. Box 572, Lafayette, Calif. Permofiux Corp., 4900 W, Grand Avc., Chicago S9, III. BR
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-RR BC RF RG, R1
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Todd-Tran Corp., 752-8 Tidrd Ave., Mt. Vernon, N. Y.
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Steel & iron	118,915 tons
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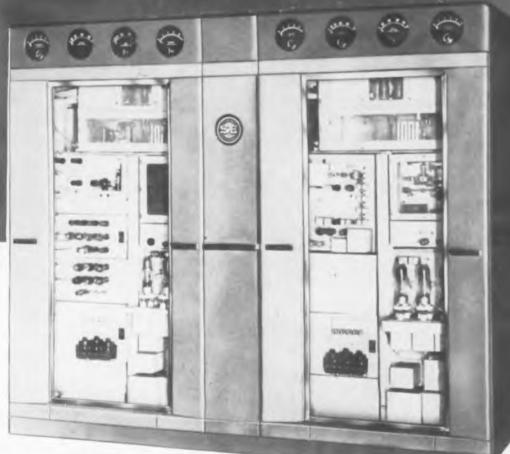
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Similarity of tube line up, oural and visual	YES	NO	NO	YES	NO
Physical length	178 in.*	160 in.	199 in.	215 in.	206 in.
Self-contained, both bands	YES	NO	NO	NO	NO
Arr cooled, both bands	YES	YES	YES	YES	NO
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Ability to use driver as stand by transmitter	YES	NO	NO	NO	NO

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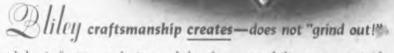
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MACHLETT ELECTRON TUBES

TR	A N S	MITT	ING	AND) IN	DUST	RIAL	TUB	ES	
	CATH	ODE		l l	IAX. AN	DDE RATIF	IG	FULL		
TYPE	VOLTS	AMPS	MU	VOLTS	AMPS	WATTS	DISS. WATTS	FREQ.	COOLING	
AL-2C39A	6.3	1.0	100	1000	0.125	125	100	2500	Forced-Air	
AL-207	22.0	51.0	20	15000	2 0	30000	10000	1.6	Water	
AL-212E	14.0	6.0	16	3000	350		275	1.5	Convection	
AL-220C	21.5	41.0	40	15000	1.5	_	10000	4	Water	
AL-220CA	21.5	41.0	40	15000	1.5	-	5000	4	Forced-Ai	
AL-228A	21.5	41.0	16	6000	1.5	-	5000	3	Water	
1L-232B	20.0	60.0	40	20000	3.0	_	25000	3	Water	
AL-240B	21.5	41.0	40	12000	1.7	_	10000	20	Water	
AL-241B	14.0	6.0	16	3000	350	_	275	7.5	Convectio	
1L-242C	10.0	3.25	12.5	1250	. 150	188	100	6	(onvectio	
AL-279A	10 0	21.0	10	3000	.800	_	1200	20	Convectio	
IL-298A	27	225	32	20000	11.0	_	100000	4	Water	
1L-298B	27	225	57.5	20000	11.0	-	100000	4	Water	
AL-342A	20 0	67	40	20000	2.5	_	25000	4	Water	
AL-343A	21.5	57.5	40	18000	2.0	_	10000	4	Water	
AL-343AA	21.5	57.5	40	18000	1.5	_	5000	4	Forced-A	
AL-356	7.5	170	20	12500	6.0	60000	22500	25	Water	
AL-357B	10.0	10	30	4000	0.5	1600	400	110	Convection	
AL-379A	10.0	21.0	10	3000	.800	-	1200	20	Convection	
AL-381	63	1.0	100	3500	0.01°	35°	35*	3000	Forced-A	
AL-450TH	7.5	12.0	38	6000	0.6	_	450	40	Convection	
AL-805	10.0	3.25	Vor.	1500	0.210	315	125	30	Convection	
ML-813	10 0	5.0	8.5	2000	0.180	360	100	30	Convection	
AL-814	10.0	3.25	_	1250	.150	180	50	30	Convection	
AL-833A	10.0	10.0	35	4000	0.50	1800	400	20	Forced-A	
ML-846	11.0	51	40	7500	1.0	7500	2500	50	Water	
ML-880	12.6	315	20	10500	6.0	60000	20000	25	Water	
ML-889A	11.0	120	21	8500	2.0	16000	5000	50	Water	
ML-889RA		120	21	8500	2.0	16000	5000	40	Forced-A	
ML-891	22 0	60	8.5	12000	2.0	18000	6000	1.6	Water	
ML-891R	22.0	60	8.5	10000	2.0	15000	4000	1.6	Forced-A	
			50		2.0	30000	10000	1.6	Water	
ML-892	22.0	60		15000		18000	4000	1.6		
ML-892R	22.0	60	50	12500	2.0				Forced-A	
ML-893A	20.0	183	35	20000	4.0	70000	20000	5	Water	
ML-893AF		183	35		4.0	70000	20000	3	Forced-A	
ML-5530	5.0	55	26		1.75	8750				
ML-5541		57	26	8500		23000		110		
ML-5604		176	19.5			32500		22.5		
ML-5606		60	50	15000		30000		1.6		
ML-5619		176	19.5			32500		22.5		
ML-5658		310	20	12500		60000				
ML-5666		120	21	10000		20000				
ML-5667	11.0	120	21	10000	2.0	20000	7500	22.5	Forced-A	
ML-5668	22.0	60	50	14000	2.0	28000		5	Water	
ML-5669	22 0	60	50	14000	2.0	28000	10000	5	Forced-A	
ML-5681	12.0	220	23	15000	12.0	150000	75000	30	Water	
ML-5682	16.5	325	32	16000	20.0	300000	100000	30	Water	

for Broadcasting and Industry

	CAT	HODE	ANODE	RATINGS			
TYPE	VOLTS	AMPS	INV.	PEAK AMPS	INSULATION	COOLING	
ML-102	20	19.0	75	750	Air	Convection	
ML-103	10	11.5	125	78	Oil	Convection	
ML-106	11	19.0	140	157	Oil	Convection	
ML-108	13	12.5	140	200	0i1	Convection	
M1-110	10	11.5	140	78	Air	Convection	
ML-115	10	11.5	125	100	Air	Convection	
ML-120	13	12.5	140	200	Air	Convection	
ML-121	10	11.5	140	100	Oil	Convection	
ML-126	13	12.5	150	200	Air	Convection	
ML-170	13	12.5	200	200	Air	Convection	
ML-180	13	12.5	200	200	Oil	Convection	
ML-222A	21.5	41	25	5000	Air	Water	
ML-5575/100	20	24	150	1000	Air	Convection	
ML-5576/200	20	32	150	2500	Air	Convection	

						ANODE RATINGS		
	CAT	HODE	TUBE	FIL.		INV	PEAK	AV.
TYPE	10000	CODLING	PKV	AMPS	AMPS			
ML-255B	5 0	19	15	Quad	Forced-Air	20	20 0	5 0
ML-2668	5.0	42	15	Quad	Forced-Air	22	40.0	10.0
ML-2678	5 0	6.75	10	Quad.	Convection	7.5	8.0	2.0
ML-315A	5.0	10	15	Quad_	Convection	12.5	8.0	2 0
ML-319A	5.0	6.75	10	Quad.	Convection	7.5	8.0	2.0
ML-321A	5.0	10	15	Quad.	Convection	12.5	8 0	2.0
ML-575A	50	10	10	In-Ph.	Convection	15	6.0	1.5
ML-673A	5.0	10	10	In-Ph.	Convection	15	6.0	1.5
ML-8578	5.0	30	15	Quad.	Forced-Air	22	40 0	10.0
ML-866A	2.5	5.0	15	In-Ph.	Convection	10	1.0	0.2
ML-8698	5 0	19	15	Quad	Forced-Air	15	20 0	5 0
ML-872A	5.0	7.5	10	In-Ph	Convection	10	5.0	1.2
ML-8008	5.0	7.5	10	In-Ph.	Convection	10	5.0	1.2

Machlett Electron Tubes are distributed in the United States by Graybar Electric Company, 420 Lexington Avenue, New York 17, N. Y. and in South America, Europe, Asia and Africa by Westrex Corporation, 111 Eighth Avenue, New York 11, N. Y.

Note: For additional technical data or prices, write to Machlett Laboratories, Inc., Springdale, Conn., or contact your nearest Graybar or Westrex office.

*Duty cycle: 0.0033



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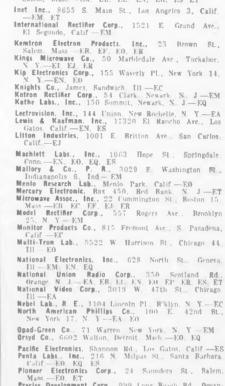
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Calif.—EA
Nytron Radio & Electronics Co., 70 Lafayette St.,
Salem, Mass.—EA. EB. EL. EN. EO. ES ET

Orsyd Co., 6602 Walton, Detroit, Mich.—EO. EQ
Pacific Electronics, Shannon Rd., Los Gatos, Calif.—ES
Penta Laha, Inc., 216 N. Milpas St., Santa Rarbara,
Calif.—EO. EQ. ES
Ploneer Electronics Corp., 24 Saunders St. Salem.
Mass.—EO. ET
Precise Development Corp., 949 Long Beach Rd., Oceanside, L. L. N. Y.—ED
Precision Crystal Lah., 2223 Warwick Ave., Santa
Monica, Calif.—EC
Process & Instruments, 60 Greenpoint Ave., Brooklyn
22. N. Y.—EO.

"Q" Glass Co., 470 Broad St. Bloomfield N. J.—EA. EI. EJ. EO EQ. ES

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N Y — ER. EF EM. ER. Rauland Corp., The, 4245 N. Knox Ave., Chicago 41.
III. EA EQ.
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Ross Mfg, Co., N60 Washington St., Burlington, Iowa
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13. N. 1.— EA. EB. EL. ES.
Taffet Radio & TV Co., 2530 Belmont Ave., New York 58, N. Y.— ET.
Taylor Tubes, Inc., 2312 Wahansia Ave., Chicago 47, III.— EN. FO. EQ. ES.
TelAutograph Corp., 16 W. 61, New York, N. Y.— ET.
Tel-O-Tube Corp., of America, 180 Van Riper Ave., E. Paterson, N. J.— EA.
Thomas Electronics, Inc., 118 9th St., Passgic, N. J.— EA.

EA. Tang-Sol Electric Inc., 95 Eighth Ave. Newark 4, N. J.—EA. EK, EL. EN. EO. EP. ER. T. V. Development Corp., 2024 McDonald Ave., Brooklyn 23, N. Y.—EM.

United Electronics Co., 42 Spring St., Newark 2, N J.—EN EO, EQ. ES United Technical Labs., Morristown N J.—ED Universal Electronics Co., 2012 S. Septilveda Blvd., Lox Angeles 25, Calif.—ET

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Varian Associates, 990 Varian St., San Carlos, Calif.
—EI ES

Varo Mig. Co., 1801 Walnut St. Garland Tex.—ET

Vickers Elec. Div., 1815 Locust St., St. Louis, Mo.—
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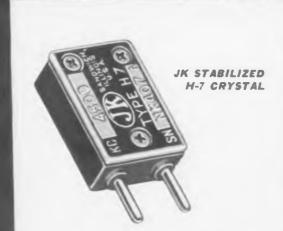
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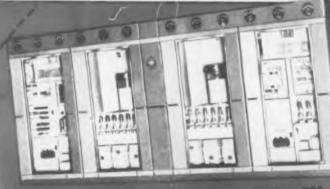
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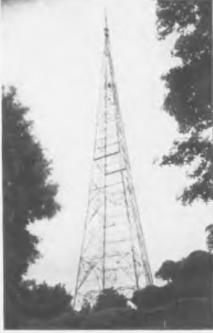
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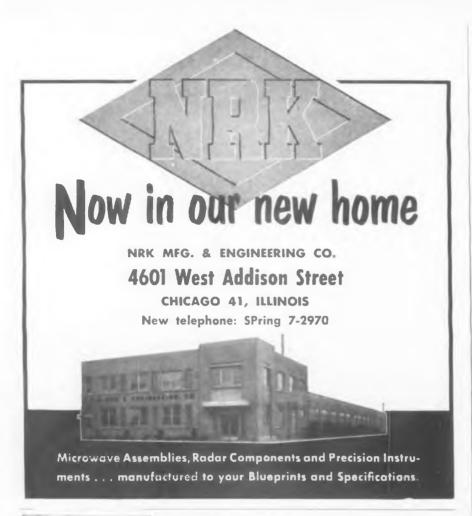
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JuMont Labs., Allen B., 1500 Main Ave., Clifton
N. J.—GA. GB. GC. GD. GE. GH. GI.

Federal Telecommunication Labs., Inc., 500 Washing ton Ave Nurley 10 N J GN GB GE, GH GI Federal Telecommunication Labs., Inc., 500 Washing Federal Telephone & Radio, 100 Kingsland Road, Clifton N. J —GE

General Electric Co., Electronics Div., Electronics Park Syracus: N. Y.—GA. GR. GC. Glv. GE. GM, GI. G. neral Precision Lab., 63 Bedford Rd., Pleasantville G. W. Associates, Box 2263, El Segundo, Calif. GA. GD.

Hammarlund Mfg., 460 W. 34th St., New York 1, N. Y. Haydon Prods., 1801 8th Ave. Brillyn 15 N.Y. GB. H. wlett-Pickard Co., 395 Page Mill Rd. Palo Alto. Calif GD Hughey & Phillips, 4075 Bevirly Blvd. Los Augeles 4 Calif GD Hydon Mfg., 2961 E Colorado St. Pasadena S. Calif —GA. GB. GC. GD. Gl.

My-Lite Antennae, 242 E 137th. New York, N. Y. —GB Imperial Radar & Wire, 4342 Bronx Blod Bronx 66 Natural Research Associates, Div. of Iresec. 2221 Warwick Are., Santa Monica, Calif.—GD, GE, GH, GI

Kelioga Switchboard & Supply, 6650 S Cicero Ave., Chicago 38, 111.—GD Kings Microwave Ca., 50 Marbledale Ave. Tuckahoe, N.Y.,—GA, GB, GD

Lings & Son, 2814 Buren Are., Camden 5, N. J. GB Link Radio, 125 W. 17th St., New York 11, N. Y. GA, GB, GE, GH, G1 Lynch Carrier Systems, Inc., 96 Jessie St., San Fran-risco 5, Callf. - GC

Magna Electronics, Rox 338 Inglewood, Calif = GR
Mark Products, 3547 49 Montrose Are, Chicago 18, 10,

—GA, GB, GD, GF
Micro Eng's Corp., 6233 Hollywood Blvd Hollywood 28
Calif = GA, GE
Microlab, 301 S. Ridgewood Rd, So Orange, N. J.

Microwave Assoc., 22 Cummingtor St. Boston 15, Mar-

Network Mfg. 213 W. 5th. Bayonne N. J. GA. GB. N.R.K. Mfg. & Eng'g. 4601 W. Addison St., Chicago 41, III —GA. GD.

Phileo Corp., Gov't & Indus. Div., 4700 Wissalickon
Philoro Mrg., 60-66 Sackett St., R'khrn. N. V. GR
Pickard & Burns. 240 Highland M.
Miss. G. GR
Polarad Electronics Corp., 100 Metropolitan Av. Brook Polytechnic Research & Develop Johnson Brooklyn, N. Y. (1)
Premier Instrument, 52 W. H. (1)
N. Y. (2)
Product Development, 307 Borgen W. Kearny, N. J. (1)

Schutter Mfg., Carl W., 80 E. Montank Highway. Ltd denhurst. L. T., N. Y=-GA. GD Shevers, Inc., Harold, 123 W. 64th St., New York 23, N. Y=-GA.

Slerra Electronic Corp., 1030 Britten Ave. San Carlin.

Calif Cl
Sperry Gyrosope Co., Div. of Sperry Corp., Great Neck,
L. I. N. Y.—GD
Square Root Mfg., 191 Sam Mill River Rd. Yorkers 2,
V. Y.—GA GR. GC
Sylvania Electric Prods., 1740 Broadway, New York 19,
N. Y.—GC, GD

Technicraft Labs., Thomaston Waterbory Rd., Thomaston,

Tennelerate Laus., Fromasion Valering, Rd., Fromasion, Forn., 16). GE.

TelAstograph Corp., 16 W. 61st St., New York 23, N.Y.—GC. GH. GT.

Telechrome, Inc., 88 Merrick Rd., Anityville, L. 1., N.Y.—GC. GH. GE. GH. GT.

Telemarine Communications Co., 5 0.542 W. 27th St., New York 1. N.Y.—GT.

Telex., Inc., Asbury Park, N. J.—GA.

Torngren Co., C. W., 236 Pearl St., Somerville, U.; Mass.—GA, GD.

T-V. Products, 152 Sandford, Rklyn 5, N.Y.—GR.

Vectron, Inc., 2 5 High St., William Mine CD

Waveline, Inc., P. O. Rox 470 toldwell, N. J. 4(A. GD) Weymouth Instrument, 1440 Commercial St., E. Weymouth 88, Mass.—4(A. GD) Wheeler Labs., 122 Cutter Mill Great Neek, N. Y.—GD White & Son. 374 Verona Are., Newark, N. J.—GR Wind Turbine Co., E. Market, St. & P.R.R., West Chester, Pa.—GD Workshop, Associates, Div. of Gabriel Co., Endicott St., Norwood, Mass.—GA. GB

ESTIMATED PRODUCTION for YEAR 1952 RADIO and TV RECEIVERS

Table radio receivers	5,220,000
Auto radios	4,650,000
Portable radio receivers	1,260,000
Radio-phono combinations	711,000
TOTAL RADIO RECEIVERS	11,841,000
Table & console TV receivers .	5,800,000
Combination TV-radio-phono	155,000
TOTAL TV RECEIVERS	5,955,000
TOTAL RADIO and	
TV RECEIVERS	17,796,000

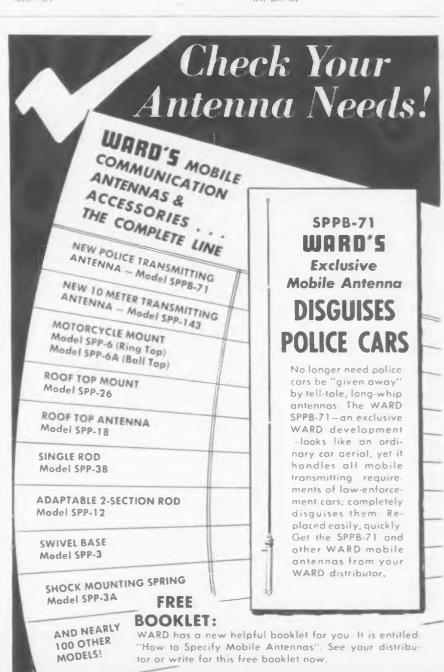
8-Point-to-Point Microwave **Communication Equipment**

Antennas				 	. H/
Auxiliary				 	. H
Complete	packag	je		 	. H
Receiver				 	. HI
Slotted lin	es			 	. H
Test equi	pment			 	. H
Towers				 	. H
Transmissi	on line			 	. HI
Transmitte	r			 	1
Wave gui	de, co	uplin	gs .	 	. H
Wave gui	des, fle	xible		 	. Hi
Wave gui					

Aero Electronics, 1512 N. Wells St., Chicago 10, 111.-Ainslie Electronic Prods., 312 Quincy Ave. Quincy 69.

Airtron. Inc., 20 E. Elizabeth Ave., Landen, N. J.—
HH, HJ, HK, HL
All Channel Antenna, 70-07 Queens Blvd., Woodside 77,
N. Y.—HA HG
Allied Research & Engle., 1041 N. Las Palross Ave.,
Hollywood 38, Cahif.—HL
—143 HG
Alpan Mire, 450 St. Francis St., Redwood City, Calif.
—143 HG
Alpan Wire, 450 Broadway, New York, N. Y.—HH
Alpradec, Inc., Rtc. 2, Rox 94, Mineral Wells, Tex.—Bi;
Amarican Electroneering, 3025 W. Jefferson Blvd., Los
Angeles 16, Cahif.—HF
American Phenolic Corp., 1830 S. 54th Ave., Chicago
50, III.—HA, HH
Andrew Corp., 363 E. 75th St., Chicago 20, 111.
—114, HE, HH, HJ, III.
Antenna Research Lab., 797 Thumas Lanc. Columbus 14,
Olito—HA, HF
Automatic Electric Ce., 1033 W. Van Buren St.,
Chicago 7, Jil.—HC
Beam Instruments, Corp., 250, 75th Med.

Beam Instruments Corp., 350 5th Are, New York 1, N Y — HJ HK HL.
Blaw-Knox Div., Blaw-Knox Co., P. O. Box 1198, Pittsburgh 30, Pa.— HG
Bone Eng's Corp., 701 W. Broadway, Glendale 4, Calif.— HE, HY, Hl. HL.
Budelman Radio. 375 Fairfield Ave., Stamford, Cong.— HA, HD, HI



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Calnevar Co., 1732 W. Wishington Risd., Los Angelea 7, Callf.—HF HJ. HJ. Century Mealstraft., 11806 Oxnard SL. Van Niusa, Calif. HF Mealstraft., 11806 Oxnard SL. Van Niusa, Calif. G. Labs., 391 Lindlow Stinford. Conn.—HF Columbia Technical Corp., 5 E 57th St., New York 22,

N. Y.—HH.
Co-Operative Industries, 100 Oakdale Rd., Chester, N. 2
—HH. HJ. HK. HI.
Cuble Corp., 2-441 Cunon St. San Diego C. Calif.
HA. HB. HC. HD. HE. HF. HH. HL.

Danbury-Knudsen, Inc., Danbury, Louin IIJ

De Mornay-Bonardl, Inc., 1223 Burton Ave., Burbank,
Calif. IIE, IF III III.

Diamond Mfg., 7 North Av., Wakefield Mass.—IIF

Dittmore 4 Freimuth. 251 1 Norwich 5 Cudahy

Wise.—IIA

Wise - HA
Derne & Margolin, Sheridan Ave., Bethpage L. I., N. Y
--- HA

Edin Co., 207 Main St., Worester R., Moss — HF Electron-Radar Prods., 1041 N. Pular i Rd., Chicago 51, III.— HA, HF Electro Precision Prods., 119-01 22nd Ave., College Point N. Y.—HA, HJ, III. Electro-Tech Equip., 308 Canal St., New York 13, N. Y.—HF

NY—HF

Electrotechnic Corp., 15601 Arrow Highway, Azusa, Calif—HC. HD. HT.

Elizabeth Iron Works, Rox 360 Elizabeth 8, N. J.—HG.

Emerson & Coming, 126 Massachusetts Ave., Boston 15, Mass.—HA. HC.

Empireering Associates, 434 Patterson Rd., Dayton 9, Ohio—HE. HF.

Equipment & Service Co., 6815 Oriole Dr., Dallas 9, Tex.—HF.

Federal Telecommunication Labs., 500 W shington Ase, Nutley 10, N. J.—118 HC HD HE Figure Mfg., 132 S Main St., Orange Calif MJ Frequency Standards Corp., No. 66, Entontown N. J. HP

General Electric Co., Electronics Div., Electronics Park, Syracture N. V.—HC.
General RF Fittings Co., 702 Beacon St., Boston 15, Moss—HI.
G. & M. Equip. Co., 7315 Varna Ave., North Hollywood, Calif—HF.
G. W. Associates, P. O. Box 2263, El Segundo, Calif—HA, HE, HF, HJ.

Hewlett-Packard Co., 395 Page Mill Rd., Palo Alto. Calif — HE HF 113 Holub Industries, 412 DeKalb Are., Sycamore, 111—HF

Ideco Div. Dresser-Stacey Co., 875 Michigan Avr., Columbia R Oblo- HG Imperial Radar & Wire Corp., 4342 Bronx Blvd Bronx G6 N Y—IIK International Research Assoc., Div. of Iresco, 2221 War-wick, Santa Monica, Calif.—IIC, IID, IIF

Korb Engineering & Mfg., 30 Ottawa Ave., Grandville. Mich — III.

Kay Electric Co., Maple Ave., Pine Brook, N. J.

III: HF HE HF
King Microwave Co., 50 Marbledale Are., Tuckahoe, N. Y.
—HA, HR, HJ, HL

Laboratory for Electronics, 75 Pitts St., Boston 14 Lehigh Structural Steel, 17 Battery Place New York 4 N Y - HG Lenkurt Electric Co., 1105 County Rd., San Carlos Calif - IRC Leonard Electric Prods. 67 34th St., Brooklyn 32, N. Y. IID III Link Radio, 125 W. 17th St., New York 11, N. Y. IIA, IIC. IID. III. III.

Mark Products Co., 3547-49 Montrose Ave., Chleago 18, 111—HA, HE, HH, HL, HL, Melpar, Inc., 452 Swann Ave., Alexandros, Va., HA, HC, HD, HH, HL, HL, HL, HB, HC, HD, HE, HB, HG, HH, HL, HL, HL, HB, HG, HH, HL, HL, HB, HG, HH, HB, HG, HB, HG, HB, HB, HB, HB, HB, HC, HB, HB, HB, HB, HB, HB, HS, Augusta Rhd, Chleago 51, 111—HB, HC, HD, HI

Nichols Prods., 325 W. Main, Monrestown, N. J.—HE. N.R.K., Mfg. & Engly Co., 4601 W. Addison St. Chleago 41, 111—11A, 1111, 113, 114

Panoramic Radio Prods., 10 S. Second Ave . Mount

Panoramic Radio Prods., 10 S. Serond Ave. Mount Vermon. N. Y.—HF.
Penn Boller & Burner Mfg., Lancaster Pa. HG.
Philoc Corp., Gov't & Indus. Div., 4700 Wissahirkon Ave.
Uniladelphia 44, Pa.—HA. HB. HC. HD. HF. HG. HI.
Plekard & Burns. 240 Highland, Needham. Mass.—HA.
Polytechnic Research & Develog., 55 Johnson St., Brooklyn N. Y.—HE. HF. HJ.
Product Develog., 207 Bergen, Kearny, N. J.—HA. HII.
Premax Prods. Div., Chisholm-Ryder Co., Highland &
College Aves., Ningara Falls. N. Y.—HA.

College Aves., Niagara Falls. N. Y.—HA

Radio Corp. of America. RCA-Victor Div., Camden, N. J.—HA

HB HC. HD, HE HF, HG, HH, HI

Radio Eng's Labs., Inc., 36 40 37th St., Long Island
City 1. N. Y.—HA HB HC. HD HI

Radio Labs. Inc., 1846 Westlake North, Scattle 9, Wash.—HD, HI

Brd. Arrow Electronics. Inc., 420 Alden St., Orangr.
N. J.—HJ, HL

Resdel Eng's Corp., 2351 Riverside Dr., Los Angeles 39
Cally.—HC, HF

Rosen Eng's Prods., Raymond, 32 & Walnut Sis. Philadelphia 4, Pa.—HC

Schutter Mfg., Carl W., 80 E. Montauk Highway, Lindon hurst, L. L., N. Y.—HE, HF, HH, HJ, HL, Seaboard Electric, 417 Canal, New York, N. Y.—HF

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PHILADELPHIA 34, PENNSYLVANIA

Sierra Electronic, 1050 writtan Ave., San Carlos, Calif.—
HF. HI
Simpson Electric, 3200 W. Kinzle, Chicago, III.—
HI
Seathern Elec. A Transmission, 3127 Holmes St., Dallas
15, Tex.—HB
Sperry Gyroscope Co., Div. Sperry Corp., Great Neck,
L. I., N. Y.—HE. HF
Sware Root Migs., 391 Sam Mill River Rd., Youkers 2,
N. Y.—HJ, HN, BL
Sunrise Prods. Co., Box 173, Hawthorne, N. J.—HA
Toffett Radio & Tv. 2530 Belmont Ave.
N. Y.—HF
Technicraft Labs., Inc., Thomaston Waterbury Rd.,
Thomaston, Conn.—HF. HH, HJ, HK, HL
Tetronix, Inc., Box 831, Portland 7, Ore.—HF
Telantograph Corp., 16 W. 61st St., New York
N. Y.—HR, HG, HF
Telectro Industries Corp., 35-16, 37th St., Long Island
City 1, N. T.—HE, HF, HI
Telectro Industries Corp., 35-16, 37th St., Long Island
City 1, N. T.—HE, HF, HI
Telectro, Inc., Asbury Park, N. J.—HA
Torngren Co., E. W., 236, Foarl St., Somerville 45,
Mass.—HA, HJ, HK, HL
Tower Construction Co., 107, 4th St., Stoux City.

Orders Received From U. S. Gov. **Communication - Electronic** Equipment Jan. 1 - Aug. 27, 1952

COMMUNICATIONS (a) Transmitters

(b) Receivers	66,609,874.25				
(c) Transceivers	72,225,954.00				
Total Communications	160,693,327.06				
Radio Navigational Aids	45,423,158.00				
Radar	263,131,886.94				
Sonar	10,783,479.80				
Lab and Test Equipment	13,459,401.71				
Piezoelectric Quartz Crysto	als **				
Miscellaneous	45,296,101.98				
Grand Total	\$538,794,477.69				

\$ 21,857,498.81

* Information supplied by RTMA

ea Less than required number of companies re-ported in this category. Total, however, includes all figures reported.

Transmitter Equip. Mfg., 345 Hudson St., New York 14 N. Y.—HD. 111
Transport Prods., Gillespie Airport, Santee, Calif.,—HR
Triplett Electrical Instra., Bluffton, Ohio—HF
Troscon Steel Co., Youngstown I. Ohio—HG
Vectron. Inc., 235 High St., Waltham, Mass.—HF
Ward Products Corp., Div. of Gabriel Co., 1523 E.
45th St., Cleveland 3, Ohio—HA
Waveline, Inc., P. O. Rox 470, Caldwell, N. J.—HE,
HH, HH, HJ, HK, ML
Westinghouse Electric Corp., 2519 Wilkens Ave., Balti
more 3, Md.—HC
White 4, Son, James L., 374 Verona Ave., Newark 4,
N. J.—HJ, HL
Wincharger Corp., E. 7th at Division. Sloux City 2,
Ilowa—HG Transmitter Equip. Mfg., 345 Hudson St., New York 11, N. Y - HD, 111 N. J.—HJ. HL Wincharger Corp., E. 7th at Division, Sioux City 2, Iowa—HG Wind Turbine Co., E. Market St. & P.R.R., West Chester, Pa.—HQ Workshop Associates, Div. of Gabriel Co., Endicott St., Norwood, Mass.—HA. HJ Yonkers Industries, Subs. Electronic Designs, 28 School St., Yonkers, N. Y.—HF

9—Receivers

Antennas, TV receiver JA
Aviation, fixedJB
Aviation, mobile JC
Broadcast, AMJD
Broadcast, FM JE
Broadcast, TVJF
Communication, AMJG
Communication, FM JH
Remote PU, civilian defense
Remote PU, fixed
Remote PU, mobile JK
Remote PU, special purpose
Tuners, TVJM

Admiral Corp., 3800 Cortlandt St., Chicago 47, Ill -JD, JE, JF Aeronastical Radio Mfg., 155 First St., Mineola, N. Y.— Air Assoc., 511 Joyce St., Orange, N. J.—JB, JC, JG, JH All Channel Antenna, 1000 Queens Blyd., Woodside Aloha Radio Television, 330 W Broadway Long Beach 2. Calif JJ.

Aftee Lansing, 9356 Santa Monica Blvd. Reverly Hills, Calif JD. JE.

American Electroneering, 5025 W. Jefferson Blvd. Los Angeles 16, Calif.—JB. Jt. JG, JJ. JJ., JK, JL.

American Phenolic, 1830 S. 54th Ave. Chicago 50, 111. American Television, 5050 Broadway, Chicago III. JF Amy, Aceves & King, 11 W New York, N.Y. Andrea Radio. 27 01 Bridge Plaza N., Long Island City 1. N. Y.—JD. JE. JF.
Ansley Electronics, S5 Tremonf St., Meriden, Conn.— Frods., 7627 W. Lab. St., River Forest, III. JH, JI.
Arvin Industries, Columbus, Ind.—JD. JF
Atlantic Video, 18 Clinton & B'klyn 2 N. Y. JA.
JD. JE. JF. JM
Addar, Inc., Box 438 M. Pusadena, Calif.—JD.
Automatic Radio Mfg., 122 Brookline Ave., Roston 15,
Mass—JD. JE. JF
Onca Television, Green & Lenning Sts., 8 Hackensack,
N. J.—JF. Mass—JD, JE, JF

Bassett, Inc., Green & Laming Sts., S. Hackensack, N. J.—JF

Bassett, Inc., Rex., 1314 N.E., 17 Court, Ft. Landerdale, Fla.—JB, JG

Bell Television, 552 W. Sard New York N. Y.—JA

Bendix Radio Div., Bendix Aviation Corp., Baltimore 4, Md. JB, JC, JD, JE, JF, JG, JH, JB

Berger Communications, 109 21 72nd St., Forest Hills, L. L., N. Y.—JD, JE, JF, BG, JH, JE, BG, LL

Bogen Co., David, 29 9th Ave. New York 12 N. JD, JE, JG, JL

Branswick Div., Radio & Television Inc., 114 W. 57th St., New York 16, N. Y.—JD, JE, JE, JE, JE, JG, JH, JE, JF, JE, JG, JH, JJ, JK, JI, Lad tlae Electronics, 19 W. 26 St., New York, N. Y.—JF

Canoest Eng. & Elec. Co., 828 N. Highland Ave. Los Angeles 38, Calif.—JD, JF, JF, Cambarn, Inc., 32-49 57th, Woodside, N. Y.—JF

Cardwell MG, Allen D., Plaintille, Conn.—JM, CBS-Columbia, Inc., 170 53rd St., Brooklyn 32, N. JD, JE, JF

Certified Radio Labs., 5507 13th Ave., Brooklyn 19, N. Y.—JF

Cef.S. Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, G. S., Labs.

N Y JF C.G.S. Labs., 391 Ludlow St., Stamford, Conn.—JB, JC, JC, JH ll Master, Napanoch Rd., Ellenville N. Y. - JA Instruments, 919 Jesup Blair Dr., Silver Spring,

Md —JL.

Clear Boam TV Antennas, 100 Prospect Ave. Burbank, (alif — JA Collins Audio Prods., P.U Box 368, Westfield, N. J.-JD. JE. JL.
Collins Radio Co., 855 35th St., N.E., Cedar Rapids,
Iows - JB, JC. JG
Colortronics, Inc., 1311 Riverside Dr., Los Angeles, 31,
Calif. - JC.

Communications Co., 300 Greco Ave., Coral Gables 34. Fla — JB. JC, JG, JH Communications Devices, 2331 12th Ave., New York 27. N. Y.—JJ. JK
Conrae, Inc., Glendale, Calif.—JF
Cornell-Dubilier Elec., 333 Hamilton Blvd S Plainfield, N. J.—JA.
Crosby Lahs., Box 233, Hicksville, N. Y.—JG, JH.
Crosby Div., Aveo Mfg., Corp., 1329 Arlington St., Cincinnati 25, Ohio—JD, JE. JF.
Cubic Corp., 2841 Canon. San Diego, Calif.—JH.
Custom Craft Mfg., 236 E. 98th. Biklyn 12 N. Y.—JI.
Dayton Aviation Radio & Equip., Box 167, Vandatia Dayton Aviation Radio & Equip., Dota 101, Valuation Ohio JC
Deleo Radio Div., General Motors Corp., Kokomo, Ind.
JB. JC. JD. JE. JF. JR. JR.
DeWald Radio Mfg. Corp., 35-11 JF Ave. Long.
Island City. N. Y.—JD. JE. JF
Dittmore & Freimath Co., 2517 E. Norwich St. Cudahy Island City N. Y.—JB. JE JF
Dittmore & Freimath Co., 2517 E. Norwich St., CudalnyWise: JA. JB. JC.
Du Mont Labs., Inc., Allen B., 1500 Main Ave., Clifton
N. J.—H. JM.

J. Radio Products Co., 2300 W. Armitage Asc.
Chicago 47, Hi.—JM.
Eckstein Radio & Television Co., 3400 E. 42nd St.
Minneapolis 6 Minn.—JD. JE.
Edin Co., 207 Main St., Worcester S., Ma.)—JL., JI
Electrotechnic Corp., 15601 Arrow Highway, Azusa, Calif.
—JB. JC., JG., JH., JJ., JJ., JK. JJ.

Elex Co., The, 69–19–215 St., Bayside, L. I., N. Y.

JD. JF.
Elm Labs., 18 S. Ridway, Dobbts Ferry, N. Y.
Emerson Radio & Phonograph Corp., 111 Eighth Abe.
New York 11, N. Y.—JD., JE. JF
Empire Devices, Inc., 38-25 Bell RIAd., Bayside 61

Empire Radio, 125 E. 46th St., New York 17, N. Y.—
JD. JE. JF.
Engineering Associates, 4234 Pasterson, Rd., Double. JD. JE. JF Engineering Associates, 434 Patterson Rd., Dayton II Objection Olio-JC

Equipment & Service Co., 6815 Oriole Dr., Dallas

Trx., DJ., JE

Ereo Radio Labs., Inc., Stewart Ave., Garden City, N.,

—JB., JG., JH

Espey Mfg. Co., Inc., 528 E. T., Bl., New York 21

N. Y.—JD., JE., JF

Fada Radio & Electric Co., 525 Main St., Belleville, N. J.—JD., JE., JF

Federal Mfg. & Engineering Corp., 311-213, Steuben St., Brooklyn 5, N., Y.—JG. Brooklyn 5, N. Y.—JG Ferrar Radio & Television Corp. W 26 84, New York 10, N. Y.—JD Finney Co., The, 4612 St Clair Ave Develord I. Olio—JA, JC Fisher Radio Corp., 41 E. S. New York N. Fisher Madio Corp., 41 F.
JII. JE
Franklin Mfg. Corp., 43 20 34 St. Long Island City 1.
N Y.—JM
Freed Radio Corp., 200 Hudson St., New York El.
N. Y.—JD. JE. JF.
Functional Music, Inc., 179 N. Michigan Ave., Chicago 1, Gadgets, Inc., 3629 N. Dixle Dr. Dayton, Ohio—JA, JR. Garod Radio Corp., 70 Washington St., Brooklyn 1, N. Y.—JD, JE. JF. Gates Radio Co., 123 Hampshire St., Quincy 1, III.—JG. General Cement Mfg. Co., 919 Taylor Ave., Rockford General Electric Co., Electronics Div., Electronics Park, Syracuse, N. Y.—JD. JE. JF. JI.

Gonset Co., S01 8. Math. Burbank, Calif.—JII.

Grem Engineering, 200 8th Ave., Brooklyn 15, N. Y.—

The True True. JD, JE, JF Hallitrafters Co., 4401 W. 5th Ave., Chicago, III.—JF Hammarlund Mfg. Co., 460 W. 34 St., New York 1. Hammaruno wig. Co., 1878

Y. Y. J.R. R.
Harvey-Wells Electronics. Inc., North St., Southbridge-Mass. B. JC. Jl. Jl., JK. Jl.
Haydon Products Corp., 1801 × Ave., Brooklyn 15, N. Y. Hoffman Radio Corp., 6200 S. Avalon Blvd., Los Angeles 3. Calif JF

Howard Industries. Inc., 1740 State St., Racine, Wise, JI, JJ. JK, Jl.

Hy-Lite Antennae, Inc., 242 E. 137 St., New York 51. Industrial Television, Inc., 369 Lexington Ave., Clifton. N. J. JF. Insuline Corp. of America, 36-02 35 We Long Island International Research Associates, A Div. of Iresco Inc., 2221 Warwick Ave., Santa Monica, Calif. JF. JG. International TV Corp., 238 William St., New York 7. N. Y. JF. Intervox Corp., 1846 Westlake N. Seattle 9, Wash.—JG. Jackson Industries, 58 E. Cullerton St., Chicago 16, Ill. Jarvis Electronic Corp., 6058 W. Fullerton Ave., Chicago 39 111 — JB JC Jewel Radio Corp., 10 40 45th Ave., Long Island City 1 N Y — JD, JE FD Mfg. Co., 6127 Little Ave. Willyn 4 N Y — IA Kaye-Halbert Corp., 3555 Hayden Ave., Culver City.

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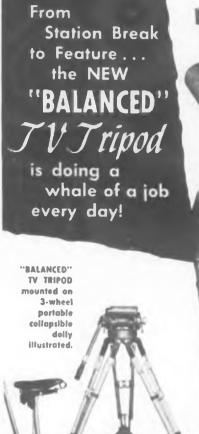
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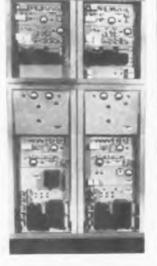
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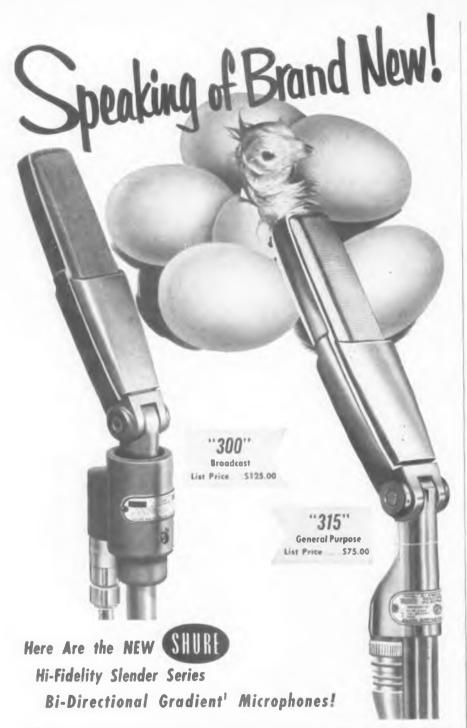
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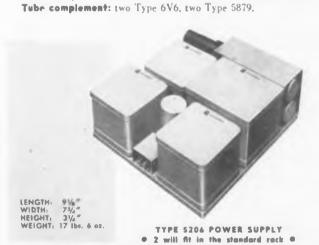
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Frequency characteristic: 0.5 db from 30 to 15,000 cps.

Power requirements: 70 ma DC at 300 v, 1.2 amps AC at 6.3 v.



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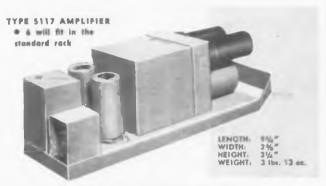
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Output load impedance: 150/600 ohms, with center tap on 600 ohm position.

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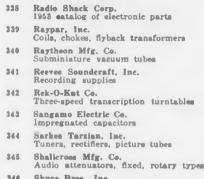
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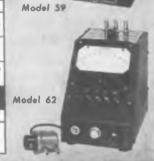
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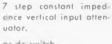
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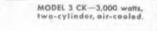
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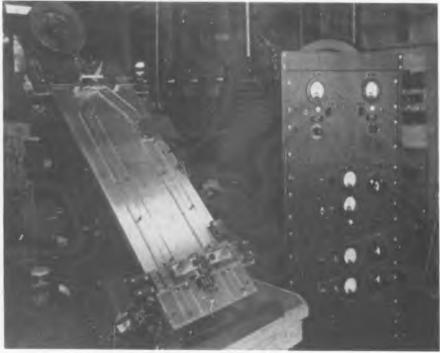
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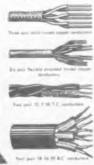
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"Circuit Digests" in "Television Retailing"

The "TV-Electronic Technician" section of Caldwell-Clements' "Television Retailing" has been enlarged with the September issue and appears as a Second Section containing a number of "Circuit Digests" of leading makes of TV receivers.

These Circuit Digests for latest TV models, each complete on a single large sheet, present four-page reproductions of schematics, tube layouts, parts lists, and electrical and mechanical instructions from the manufacturers, besides general suggestions and tips on solving servicing problems common to all sets.

Up to eight "Circuit Digests" will be included in each month's Technician supplement in future issues, in addition to the usual servicing information in the main section of the magazine. In this way, the subscriber will shortly accumulate a collection of Circuit Digests and schematics covering all lines of new TV sets on the market.

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Marshank Sales Co., 672 S. Lafayette Park Place, Los Angeles has completed a large-scale expansion program. The additions to the staff include: W. J. Monteforte, Peter Pohl, L. B. Winters, and I. R. Stern.

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Magnetic Amplifiers

The first line of Magamp magnetic amplifiers produced by the Westinghouse Electric Corp., Pittsburgh 30, Pa., is described in a new 18-page booklet (TD-52-600). Curves, tables and wiring diagrams are included in sections which deal with component parts, applications and operating characteristics. Copies may be obtained from Westinghouse, Box 2099, Pittsburgh 30, Pa.

Introduction to Microwave

A 20-page booklet, entitled "An Introduction to Microwave," provides a semi-technical description of RCA microwave equipment. Chapter headings include: microwave radio; how it works; propagation characteristics, operational advantages, economic factors influencing choice of frequencies, and desirable design characteristics. Copies may be obtained from the Microwave Communications Section, Radio Corporation of America, Camden 2, N. J.

Digital Printing Counter

An electronic digital printing counter for counting, totaling and printing results from electronic computers, oscillogram readers, test instruments and transducers and digital read-out machine are the subjects of new bulletins released by Clary Multiplier Corp., San Gabriel, Calif. Typical applications of both pieces of equipment are illustrated and described.

The Red Point Dual Impregnating Unit. designed for impregnation under vacuum of porous articles, such as electric windings, etc., is described in a brochure published by Red Point Products, 1907 Riverside Drive, Glendale 1. Calif. Use of the Red Point dual system is said to accomplish a perfect impregnation within the shortest period of time.

Motor Speed Controls

"Variaci) Motor Speed Controls" is the title of an 8-page prochure being made available by the General Radio Co., 275 Massachusetts Ave., Cambridge 39, Mass. Technical data presented includes speed-torques curves and typical applications for all models.

TV Camera Chain

Allen B. Du Mont Laboratories, Inc., has published a new bulletin describing the company's universals image orthicon camera chain model TA-124-E. Copies may be obtained from the Television Transmitter Div., Allen B. Du Mont Laboratories, Inc., 1500 Main Ave., Clifton, N. J.

Toroidal Inductor

Precision wound high Q toroidal inductors are listed in Lenkurt's new four-page bulletin TL-P4. Five different types of coils are available with or without hermetically sealed cases. Included in the bulletin are Q curves and other design data for representative standard values of the varied coil types. Information is also included about the effect of dc current on the inductance values of each type of coil. Copies of bulletin TL-P4 are available nn request from Lenkurt Electric Sales Co., 1116 County Road, San Carlos, Calif.

Telephone Handsets

Telephone Handsets

A combination file folder and catalog sheet, describing the Company's line of telephone handsets and accessories, has been released by the Connecticut Telephone and Electric Corp., 70 Brittania St., Meriden, Conn. The file folder is not only a compact, easy-to-use catalog but contains identifying photographs, descriptive data, wiring diagrams, cordage codes and connection assemblies for various handsets, headsets and wall or desk telephone sets, as well as components, both for military and commercial application. ponents, be application.

Miniature Connectors

Miniature Connectors

The Advance D-1 bulletin contains photos, data and dimensional drawings of the "D" series of Cannon connectors. Contact complement ranges from 15 contacts to 50. Suitable for rack and panel mounting, connectors in this series may be used as plugs on either side of the assembly by the addition of m junction shell, having an integral clamp. Copies may be obtained from the Cannon Electric Adv. Dept., 420 W. Ave. 33, Los Angeles 31. Calif.

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RCA-217D1 Focusing Coil
RCA-218D1 Alignment Coil
RCA-233T1 Horizontal Deflection Transformer
RCA-234T1 Vertical Deflection Transformer

For complete data on the RCA-6198 Vidicon and associated components, write RCA, Commercial Engineering, Section JR57, Harrison. N. J., or contact your nearest RCA Field Office

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