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There is a better way.
Personal communicator explosion seen
Evidence from a number of sources points to the heating up of the handheld "personal communicator" market. As presently visualized, a personal communicator will be a box that includes the functions of a scratch pad, personal computer, electronic organizer, and, perhaps, a cellular telephone.

It is expected that the user will be able to write messages for storage on a screen with a pen, send those notes elsewhere, call up files of data and phone numbers, and even make phone calls—if the box has an integral cellular phone.

AT&T has been working hard to stake out a position in the communicator market. It has two axes to grind. It would like to sell its cellular communication services in that field, and it is seeking business for its own equipment manufacturing facilities. One way to assure that foothold is for AT&T to develop the standards that will be accepted by all other manufacturers and communications services providers.

So far, AT&T has forged alliances with several major electronics manufacturers, developed the "Hobbit" microprocessor chip for the units, and has stated its willingness to provide financial backing for suppliers and support software publishers.

Matsushita (Panasonic), NEC, and Toshiba have announced plans to build communicators based on AT&T's Hobbit microprocessor. AT&T is also negotiating a licensing agreement that would allow NEC to manufacture the Hobbit microprocessor. In addition, AT&T expects to sell its own brand of personal communicator, manufactured by Eo Computer, Inc. Mountain View, CA, a joint venture between AT&T, Matsushita, and Marubeni of Japan. It expects to sell the units through its national chain of AT&T Phone Centers.

AT&T is also working with Go Corp., whose PenPoint operating system is incorporated into the Eomade products, to encourage the adoption of the operating system as an industry standard. Its plans include lining up more than a dozen software suppliers to write applications software that is compatible with the PenPoint software.

In another move, AT&T has designed the circuitry for a mininature disk drive, and it is backing Sundisk, a company that makes a data-storage device for the communicators.

Apple has developed prototypes of a similar unit called the Newton, which it calls a "personal digital assistant" or PDA. Intel is reported to be working with VLSI Technology Inc. to develop a processor for the new units, and Motorola has signed investment and cross-technology agreements with both Apple and Sony.

Doubling digital video rate
The possibility of doubling the amount of digital information that can be transmitted on cable TV channels, without additional video compression, is now a reality. Zenith Electronics of Glenview, IL, has developed vestigial sideband (VSB) digital modulation and transmission technology, which makes it possible.

Zenith's 16-level digital transmission system can send two digital HDTV signals on a single 6-MHz cable channel. That doubles the number of digitally compressed standard TV signals on a cable channel, and permits the delivery of as many as 23 movie channels or nine live-video channels. An alternative mix of only eight TV signals is also possible.

According to Zenith, radio transmission of digital TV signals results in lower quality TV received signals than cable. Programs transmitted to customers over cable are less likely to be distorted and suffer from interference. Signals in cables have better peak carrier-to-noise ratios and lower levels of interference.

Zenith took advantage of the greater noise-margin of cable transmissions to increase the information-carrying capacity, or data rate, of cable. To increase the amount of digital data delivered through a 6-MHz channel, a cable system must maintain a high signal-to-noise ratio, and must acquire and lock in the carrier, clock, and synchronization information. This is difficult to accomplish with the advanced digital modulation techniques such as 16- and 64-QAM (quadrature amplitude modulation).

By contrast, Zenith's VSB digital modulation and transmission technology, uses auxiliary signals for acquisition and synchronization. The pilot carrier, not feasible in QAM systems, and a data-segment sync signal are both independent of the data.

Zenith's 4-VSB technology obtains a data rate of 21.5 megabytes per second for its "Digital Spectrum Compatible" HDTV (DSC-HDTV) system. The company's newly developed, 16-VSB approach, an extension of the 4-VSB system, yields twice the channel data rate, or 43 megabits per second, with no increase in data compression requirements.

The 16-VSB system obtains signal acquisition even when ghosts and impedance mismatches are present. The system has simple analog-to-digital conversion needs, and it does not require the more complex adaptive equalizer of the QAM systems. Therefore, 16-VBS is said to offer cost-effective, noise-free TV pictures and digital audio. Moreover, it is said to be compatible with existing computer, telephone, and other digital communications systems.
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- BP349—AN INTRODUCTION TO SCANNERS AND SCANNING ... $7.95. Radio scanners have opened a realm of exciting radio listening. Understand radio wave propagation, types of transmissions, antennas, band assignments—the straight dope on what to hear and where to hear it! Comes complete with index, glossary of important terminology.

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• **HDTV costs.** No matter which of the five proposed HDTV systems is chosen, receiver costs are expected to be about the same. That's the conclusion of a report made to the FCC Advisory Committee on Advanced TV Service, detailing the most complete study of receiver costs made to date. The Specialist Group on Advanced TV Receiver Cost, consisting of representatives of all HDTV system proponents and engineers from receiver-manufacturing companies, found that by 1998 (which was assumed to be the first year of true mass production) the average HDTV receiver with a 34-inch widescreen (16:9) tube could retail for about $2550 and a 56-inch projection set could sell at around $3850.

These findings are interesting in view of the fact that the first two widescreen (non-HDTV) sets to be announced for the American market—a 34-inch tube set under the RCA brand and a 50-inch projector by Panasonic—both will carry suggested list prices of $4999.

The HDTV cost study group found that no proposed HDTV system had a significant cost advantage as far as receivers are concerned. Electronics in 34-inch sets varied from $216 to $258 in cost, and for projectors from $305 to $374. Cabinet cost of all 34-inch sets was estimated at $90, and for projectors at $140. The tube price was put at $700; projection optics, tubes, screen, and assembly at $1050. Retail prices were estimated by adding the normal 2.5 multiplier for various markups.

The specialist group threw cold water on those counting on new giant picture-on-the-wall displays to replace CRT-based systems. The cost of future displays with various flat panel technologies and light-valve projectors could not be estimated with any degree of accuracy, because no such displays appear ready for consumer HDTV at this time," the report stated. "Therefore direct-view CRT and projector technology were assumed to be the most cost-effective displays for the time frame of this analysis."

• **8mm/VHS VCR.** Something that home videographers have been wishing for is on the way. In Japan, Sony has introduced a dual-deck VCR that can edit from 8mm to VHS and vice versa. Both decks have high-end features such as stereo audio and capability of accommodating high-band recordings (Hi8 and S-VHS), but in standard resolution only. Included are several editing features, including jog/shuttle controls. Presumably frightened by the bustling talk of movie-industry association figures, who claim that dual decks are designed to infringe copyrights, Sony says that it has no plans to export the deck to America, but demand could convince it to change its mind.

Competition could do that as well. Go-Video, which introduced the first VHS-to-VHS dual deck to America, says that it will introduce an 8mm/VHS deck here at midyear. So does Samsung, which makes the dual decks for Go-Video.

• **CD-ROM MOVIES.** How do you sell a multimedia system when the public doesn’t know what multimedia is? Call it a movie machine. That’s the formula that will be followed by Denon America, according to its president, Robert Heiblim. People aren’t interested in buying something for which they have demonstrated no need and don’t understand, Heiblim reasons. Denon is developing a CD-based multimedia system using Intel’s Digital Video Interactive (DVI) system. The most important need is to put regular noninteractive movies on the ROM discs first, according to Heiblim. Consumers know what movies are and will buy videodisc machines that use little five-inch discs, as long as they are superior to existing laserdiscs, he predicts. When many of these CD movie machines are in place, then interactive programming can be inaugurated.

Denon says that its DVI system soon will have laserdisc quality, which is considered a prerequisite for consumer acceptance. Heiblim says that early multimedia consumer products must be marketed as “VTRs,” which stands for “videotape replacements,” because consumers won’t put their money into unknown devices. He prefers to call Denon’s system “something that plays movies and is also interactive.”

• **Video goggles.** Two companies have demonstrated ski-mask-like contraptions that provide personal video pictures using LCD’s. Sony displayed its “Visortron” system in Japan, using two small LCD’s that are viewed through built-in lens systems. Since each eye views a separate picture, it’s possible to display images in true 3-D. Sony says that it’s exploring commercial uses for the product.

But another system, “Virtual Vision sport,” was about to go into production at our press time. That system is based on the “heads-up” displays used in aircraft, and uses a single LCD and lens-mirror to display a picture that appears to be as large as 60 inches, 8 to 15 feet in front of the viewer. The picture is off to one side, so the user can perform other tasks while watching it.

The five-ounce wrap-around glasses, with a belt-packed TV tuner, battery, and jacks to connect a VCR, camcorder, or TV cable, will go on sale this spring at about $900, says its producer. Virtual Vision. An accessory will permit it to pick up wireless signals from the television.
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MONITOR BUG
I have an IBM clone and use it with a monochrome monitor. The system has always been very reliable but recently I’ve been having trouble with the monitor. I’m not sure what’s going on, but the symptoms are that the image flickers randomly. Sometimes it will be perfect for a while and then it will get brighter or darker in random spurts. If I turn the monitor off and then on again, the problem sometimes fixes itself for a while, but it’s only a matter of time before the flickering returns. Any ideas?—B. Frish, Los Angeles, CA

You may think of this as a computer problem but any experienced TV person will tell you that this is a simple problem with the clamping circuit on the video input. Most TV’s use a combination of diodes and resistors to set the white and black levels to somewhere around a volt or so. Computer monitors do the same.

If you have access to the schematic for the monitor, it should be a fairly simple matter to fix it. All you have to do is locate the relevant part of the circuitry and then take a look at the DC levels with a white and black screen. You’ll probably find that one of the diodes is intermittently failing. Changing the bad component is a quick job although it may take a bit of work—with a screwdriver—to get your hands on the component.

If you can’t get the schematic for the monitor you can still snoop around with a scope or meter until you locate the clamping circuit. If this is the first time you’ve ever thought about doing something like this, my advice is to forget about it since there are some real knock-you-down voltages floating around the inside any TV or monitor.

Since the purpose of your letter seems to be getting your computer working again, the best advice is to buy another monitor. You can get a monochrome monitor for under 80 bucks these days and they even come with warranties. If you don’t want to scrap your old monitor, take the guts out of it and turn the case into a fish tank. That’s what I did with mine!

LIMITING LED CURRENT
I’m building a circuit that has several LED’s as indicators to let me know how the circuit is performing. Quite often more than one LED is on at a time, and since the circuit is battery powered, it causes a real power drain. All the LED’s have one leg in common so I have no way to control individual brightness. Isn’t there some simple circuit that will regulate and limit the current used by the LED’s, no matter how many are lit?—W. Meredith, Elkins, WV

I’m not really clear about why you can’t use separate resistors on the LED’s to individually limit the currents, but there is another way to solve the problem. The 78XX-series of voltage regulators have been around for a long time and are even available in special low-power configurations. If I had your problem I’d use whichever regulator was suitable and wire it as shown in Fig. 1.

You should tailor the value of the capacitor to the number of spikes on the line but, in general, the 0.33 μ F capacitor shown in the schematic should work well.

When you set up the regulator as shown, it works as a current regulator rather than a voltage regulator. The output current draw will be the regulated voltage divided by R. The only thing to watch out for is that you don’t try to draw more current through the regulator than what it’s rated for. But since you only want to drive a handful of LED’s, I don’t think you’ll have any problems.

ONLY HALF-WAY THERE
I have a laser printer that I’m trying to use for printing graphics. The problem is that I can’t seem to print more than half a page—the picture is incomplete and the bottom half of the paper is always blank. What’s going on?—A. McChord, Ames, IO

Laser printers produce terrific output, but it’s amazing that, while so many people use them, so few really understand how they work. The major constraint in printing graphics with a laser printer is the amount of memory it has, and that seems to be your problem as well.

Copy machines and laser printers are very similar. The former uses an optical image as the source of its output and the latter uses an electronic image in memory for the source. If you want to print with 300-dpi (dot per inch) resolution, your printer will need enough memory to “take note” of the image. If there’s not enough memory, the printer will print the page when it runs out of memory—which, in your case, is about halfway through the image.

You have two choices to solve the problem. The first is to add memory to the printer, and you’ll need at least one and a half megabytes of RAM to do a 300-dpi full-page print. Continued on page 86
Meet the new TEST BENCH® DMMs, with more of what made the original a best seller. B-K PRECISION's original TEST BENCH testers became overnight best sellers because they fused the power of many instruments in one compact meter. These new models also out-feature ordinary DMMs, and outperform them as well. All are ruggedized, offer long battery life and carry a three-year warranty.

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INRUSH CURRENT LIMITER CORRECTIONS

There are two problems with the "Inrush Current Limiter" (Electronics Now, December 1992).

First, in Fig. 6 on page 49, the emitter of Q2 and the high end of R5 should be connected to the plus end of C2 (about 24 volts DC). As shown, the Darlington transistor, Q2, and possibly the relay, RY1 (24-volt DC coil) would burn out.

Second, the circuit is too complicated and overdesigned. I designed a much simpler circuit, shown here in Fig. 1 (a) and (b). The relay RY1 will not activate until the resistance of the NTC thermistor Rₚ drops low enough for the voltage across RY1 to reach about 80 volts (or whatever the activating voltage for the relay used might be). Resistor R₁ might be added to slow down the action by effectively boosting the needed voltage.

Find the maximum resistance (of R₁) with which the relay will activate when connected directly to 120 volts AC, and then use a resistor of about half that value. That resistor should be shorted out by another set of contacts of RY1. The effectiveness of the circuit can be seen by finding values of fuses at the just-blow threshold (or just not-blow) when the circuit is used and not used (Rₚ shorted out).

I cannot think of an instance when a delay of one second (or more), as stated in the article, would be needed. (If the capacitors in the power supplies need one second to recharge after a spike in the loading current, I would say that the circuit is in peril, and a major redesign of the power supply is needed.) Therefore, the circuit shown here should do the same job nicely.

PETER PESKA
Taylor, MI

In addition to responding to Mr. Peska's comments, I would like to point out several errors that appeared in the article. There is, indeed, an error in Fig. 6 on page 49. The emitter of Q2 and the high end of R5 should be connected to the positive end of C2 (i.e., the positive 24-volt supply). The parts placement diagram, Fig. 7, is correct.

In response to Mr. Peska's comment that the circuit is "too complicated," I'd like to point out that the circuit was designed with a line-derived regulated power supply for several reasons. The main reason to combine such a power supply and timer circuitry was to illustrate the concept of a transformerless line-derived, regulated power supply.

This circuit is popular in such commercial products as remote-controlled lamp/appliance controllers. Other advantages of the circuit are that it is independent of the load connected to it, and it features a predictable and easily adjustable time delay. Finally, the circuit is not that "complicated" in the first place: It does not consist of many components, and it is easy to construct. I agree that Mr. Peska's circuit is much simpler and will work, but my project was designed for the reasons stated in the article.

My response to Mr. Peska's comment that a delay of more than one second is unnecessary is that the circuit allows for a wide range of delays by appropriate selection of a fixed resistor or by the use of a variable resistor. Delays of one second or less are easily obtained by choosing a suitable resistance (simply reduce the value of R₄). Again, the wide range of time delays possible was given in Table 1 to illustrate the versatility of the circuit.

In the parts placement diagram (Fig. 7), resistor R₈ should be labeled MOV1, R₉ should be labeled R₈, and R₁₀ should be labeled R₉ (there is no R₁₀ in the circuit). In the first sentence of the last paragraph on page 48, the sentence containing the phrase "shorts out thermistor R₉" should read "shorts out thermistor R₈."—Douglas Wirth

AUDIO UPDATE COMPLAINT

Larry Klein's November Audio Update contains gross errors and unwarranted assumptions, and it is insulting to audiophiles and readers. For example: The "Hafler test" shown in Fig. 1 has a fatal error in that the amplifier is not even loaded. Changes in an amplifier's load usually alter the response of the system significantly, and this change would be included in the null speaker signal.

Klein assumes that a better amplifier will make a better system; this is not necessarily so. The equipment surrounding an amplifier will interact with the amplifier for better or worse, and this makes it difficult to judge an amplifier accurately without considering the related equipment. For this reason, respon-
possible reviewers list the equipment used with the unit under test.

Klein also ignores the fact that audiophiles have a wide range of music preferences that influence equipment purchasing decisions. I argue that one can objectively evaluate equipment, but must include other factors such as performance expectation and personal musical preference.

Klein fails to recognize that sophisticated listening skills take time and effort to develop into a useful tool for evaluating high-end audio equipment. I find his attitude typical of those whose hearing is underdeveloped and whose experience seems to be the result of confiding in salesmen, listening to rumors, and “wannabe” experts. Klein’s in-competence is so complete that he probably would even claim that CD’s sound better than records, contrary to what is obvious.

S.D.

Address withheld by request

Mr. Duncan’s long letter (heavily condensed for space reasons) contains several technical and philosophical confusions—aside from being stupid and insulting. To start:

The Hafler circuit shown in Fig. 1 of my article connects the “null” speaker so it can compare only the input and output of the right channel, which is loaded with a conventional speaker. The resistance loading on the left channel output simply provides the input signal for the right channel.

If I understand Mr. Duncan correctly, he believes that it’s more important to match the complementary defects of amplifiers and other equipment than to seek the best performance from each. Since well-designed power amplifiers—which were the subject of my article—are essentially audibly perfect within their power ratings, Mr. Duncan’s mix-and-match approach is chasing a wild goose up a blind alley. Incidentally, the only “responsible” high-end reviewers that I know about write for The Audio Critic, mentioned last month.

As to my inexperience in critical listening, I became an avid audiophile in the early 1950’s when hi-fi equipment first became available in the U.S. For five years I worked as a technician for an electronics kit manufacturer, where I made tests, did repairs, and handled the technical correspondence on my employer’s kits that included hi-fi kits. In the evenings and on weekends I “moonlighted” as a freelance hi-fi serviceman.

After being a technical editor at Popular Electronics for two years and a similar magazine for another two years, I became the technical editor of Stereo Review, where I was in charge of its equipment-testing program for about 20 years. During that time I auditioned countless products in my home and office listening room.

Moreover, I was invited to visit the test laboratories and factories of audio equipment manufacturers in England, Germany, Japan, Denmark, Hungary, Austria, Canada, and the U.S. during that 20-year period. At all those locations I was asked to evaluate the sound of their products (mostly loudspeakers), and I frequently was able to validate my responses against objective test data.

I do not “confide” in salesmen, rumor mongers, and “wannabes.” However, I know many product engineers and audio researchers—and guess what—most of them agree with me that, in general, CD’s do sound better than LP’s—if only for their superior signal-to-noise ratio.

It’s always good to hear from a fan.—Larry Klein

AN AUDIO/VIDEO-PHILE

I recently discovered Electronics Now, checked out every back issue from my public library branch, and spent many rewarding hours reading each one from cover to cover. I can’t follow everything yet, but I expect that will come with time.

On a general note, I enjoyed Larry Klein’s debunking of some of those outrageous claims from audiophiles. I now have an authority to quote when I say that I cannot discern any significant difference between my $5000 equipment and the $20,000 worth of equipment that is supposedly being installed in average 18 ×15-foot American living rooms.

I haven’t seen one subjective au-

continued on page 70

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March, 1983 Electronics Now
Whether powering a prototype circuit or providing power for equipment being serviced, the bench-top DC power supply is an essential tool for anyone in the electronics industry. It's also essential for anyone who plays an active role as an electronics hobbyist. B + K Precision (6470 W. Cortland St., Chicago, IL 60635) has recently introduced the Model 1626, a supply that is ideal for powering equipment rated at 12 volts.

The 1686 can deliver an output from 3 volts to 14 volts DC with a maximum current of 12 amperes. That high current rating is sufficient to power most car stereo systems, even those with high-power amplifiers. Most mobile amateur radio equipment, as well as CB transceivers, marine radios, and other high-current automotive accessories can be powered safely from the 1686.

The maximum output current available from the power supply is proportional to the output voltage. When the supply is set to deliver 13.8 volts—which is the operating voltage for most equipment nominally rated at 12 volts—the 1686 can deliver 12 amperes continuously to the load. That drops to 10 amperes at 12 volts, 4.5 amperes at 5 volts, and 2.5 amperes at 3 volts.

At all voltage settings, the specified load regulation is less than 0.8%. That is, regardless of the load at the output terminals, the supply's output voltage will deviate less than 0.8% from its initial setting. The line regulation of the supply is also rated at 0.8% from 108–132 volts AC. That means that regardless of the change in the line voltage to which the supply is connected, the output voltage will deviate less than 0.8%.

The ripple and noise is specified at less than 10 millivolts rms. Overload current limiting provides protection against excessive overload or short-circuit output. The 1686 is housed in a black metal cabinet that measures about 5½ x 6 x 12 inches; it weighs just over 12 pounds. The front panel features a pair of easy-to-read analog meters along the top edge, one for voltage and the other for current—that provide an indication of what the supply is doing at a glance. To the right of the meters is a rotary knob that controls the output voltage. The bottom half of the panel contains two sets of output connectors, a power switch, and two LED indicators.

The main voltage-output is provided on a set of binding posts. Two sets of spring-loaded terminals—much like the kind commonly found on audio speakers—are provided for connecting low-current loads. The tie points can supply a maximum of 2 amperes. Above the power toggle switch is an LED that serves as a power-on indicator. Above that is an LED that indicates that the supply is in an overload condition and has reduced its output voltage.

The rear panel contains a fuse holder and a small fan. The fan, which helps to keep the supply compact by reducing the size of the heatsinks needed, does not run constantly. Rather, it is controlled by a thermostat, and comes on only when the internal temperature of the supply is too high for safe operation.

The outputs of the supply are isolated from the chassis and earth grounds, which is essential for flexibility in connections. If required, for example, the positive output can be connected to ground for powering positive-ground automotive equipment.

The isolated outputs also allow multiple supplies to be connected together in series or parallel for powering equipment that has higher voltage and current requirements. For example, connecting two supplies in parallel will provide a continuous source of 24 amperes, while connecting two supplies in series will provide an adjustable 6 to 28-volt power supply.

The model 1686 can operate from either 120-volt or 230-volt AC power lines with frequencies of 50 or 60 hertz. A slide switch on the bottom of the chassis permits easy selection.

We found the operation of the model 1686 to be quite straightforward. The manual supplied with the supply was more than adequate, and we were happy to find that calibration instructions were included there.

B + K Precision has priced its model 1686 at $199. We think that the supply is ideal for service shops that regularly repair mobile equipment, as well as for retailers who need to power equipment on display. Of course, radio amateurs will also appreciate the 12-ampere continuous duty rating.
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Understanding Digital Troubleshooting: Third Edition; by Don L. Cannon, Sams, Division of Macmillan Computer Publishing, 11711 North College, Carmel, IN 46032; Phone: 800-428-5331 or 317-573-2500, Fax: 800-448-3804 or 317-573-2655; $24.95.

Digital systems must be effectively maintained if they are to operate reliably at peak performance levels. That is the central theme of Don Cannon’s book on troubleshooting digital electronics. Mixing general tutorial information with “how to” instruction, the book is intended to help readers keep their digital circuits operating properly “in the pink.”

Intended for readers with a wide range of experience and formal technical background from the novice hobbyist to the experienced professionals, Cannon’s book includes comprehensive text on basic electronic engineering concepts and the fundamentals of digital circuitry. After readers have learned (or refreshed their knowledge) of the fundamentals, they will be ready to start troubleshooting.

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The book also covers the solution of problems in sequential logic circuits, how to test complex digital devices, and how to select logic analyzers and computer test equipment appropriate to the maintenance task at hand. Each chapter includes a self-quiz to permit readers to evaluate their progress and understanding of the subjects to which they have been introduced.

Professional Equipment, Catalog No. 33, Professional Equipment, 153 Plainview Road, Woodbury, NY 11797; Phone: 800-334-9291; Fax: 516-367-7405; free.

This 10-page application note is the first in a planned series from Conversion Devices, a designer and manufacturer of DC/DC converters. It contains more than 180 definitions of terms commonly associated with DC/DC converters and power supplies. Arranged in alphabetical order, the technical terms are simply and completely explained.

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HANDHELD NTSC COLOR GENERATOR. A television/video signal generator small enough to fit into a field-service kit is now available from B + K Precision. The Model 1221, said to offer the same capabilities usually found only in bench models, generates 14 patterns of stable video signals for testing, servicing, and adjustment of TV’s and other video equipment.

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The upgrade also includes circuitry that returns the instrument to previous settings when changing between the meter mode and the scope mode. Additional record functions are included, and there is continuous meter-mode display of voltage, frequency, and duty cycle. A smart trigger algorithm allows hands-off duty-cycle measurements of pulse-width modulated motor-control waveforms.

The three ScopeMeters (Models 93, 95, and 97) offer oscilloscope and digital multimeter functions. They all include such features as autoset, waveform and setup memory, combined display of meter results and waveforms, and convenient menus. The Model 97 also features a built-in signal generator, a component tester, and remote control through an optically isolated RS-232 interface, printer interface, and display backlighting.

The price of the ScopeMeter Model 93 is $1350, the Model 95 is $1650, and Model 97 is $1950. Upgrades of earlier ScopeMeters are $155.

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CELLULAR NOTEBOOK LINK. A prominent Finnish electronics manufacturer has introduced its Cellular Notebook Link. Nokia designed the link for use with Compaq notebook computers equipped with the SpeedPAQ 144 modem and Nokia 121 cellular phones. The link permits data and fax transmissions to be sent and received over a cellular network. The interface is a coiled cable with a quick-release data cradle that holds the phone while it is in the fax/data mode. That design eliminates the separate interface box required in most mobile data installations. The link needs no external battery because the interface is powered by the phone’s battery and the computer’s internal power source.

When used with the Compaq SpeedPAQ 144 modem, the Cellular Notebook Link transmits data at 4800 bits per second. However, if the data is compressed, Nokia says the data throughput will exceed 11,000 bps. Fax transmissions are sent and received at 9600 bps.

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STANDBY POWER SUPPLIES. Perma Power Electronics is offering a series of standby power systems for backing up computers and peripherals if power fails. WatchDOS supplies can be used with any DOS-based computer or network, but cannot be used with Windows or memory-management software. Each system includes a “Hibernate” software utility program.
data to the hard drive, and
then safely shuts down the computer. When AC power is restored, the software system restarts the computer, restores all memory, and resumes program execution at the point of power interruption.

The 400-VA Model DPS-400L is priced at $299 and the 600-VA Model DPS-600L, for single-personal-use 386 computers, has a price of $375. The 800-VA Model DPS-800L, for office 386 and 486 computer systems, has a price of $489.

Perma Power Electronics, Inc.
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The price of the MFJ-9020 CW transceiver is $179.95.

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Electronics. Now. March 1993

CIRCLE 78 ON FREE INFORMATION CARD
BUILD THIS

ULTRASONIC CLEANER

Build a professional-quality ultrasonic cleaner and keep hard-to-clean connectors, parts, and tools spic and span.

REINHARD METZ

ULTRASONIC CLEANING HAS BEEN commonplace in commerce and industry for years, particularly for cleaning small, convoluted parts that would be a difficult or impossible to clean otherwise. Items that are routinely cleaned ultrasonically include machine parts, standard and micro-miniature tools and connectors.

Factory-made ultrasonic cleaners are still too expensive for the average consumer and hobbyist. But with the drawings, photos, and text in this article, you can build your own ultrasonic cleaner. You have options in building this ultrasonic cleaner. You can build the complete system with microprocessor-based time and temperature controls, or you can build only the basic model with on-off controls. You’ll be surprised at the low-cost of the parts, regardless of the option you choose. The basic specifications for the ultrasonic cleaner are given in Table 1.

Only non-toxic, non-flammable solutions will be needed to do effective cleaning with this ultrasonic cleaner. You’ll be able to clean many different kinds of household or shop objects that are hard to clean—or, in the past, have just been too much trouble to clean well with conventional methods. Those objects include jewelry, kitchen utensils, circuit boards, bicycle and auto parts, and tools. What is more, you can do all your ultrasonic cleaning indoors—you don’t have to go into your garage or backyard to keep noxious fumes out of your house.

Ultrasonic cleaning

The basis for ultrasonic cleaning is a bubbling action in a fluid called cavitation—millions of tiny bubbles forming and collapsing within the cleaning solution do the scouring. You have probably seen the cartoons of thousands of cleaning bubbles at work on the TV commercials for bathroom cleaners. The big difference here is that with our cleaner, the bubbles are created ultrasonically by piezoelectric transducers, not by the solution itself.

The disk-shaped piezoelectric transducers are bonded to the underside of the cleaning pan. The dimensions of these barium-titanate ceramic disks change continuously in response to high-frequency signals applied across their sensitive surfaces. These transducers are similar to those used

<table>
<thead>
<tr>
<th>TABLE 1</th>
<th>LEADING SPECIFICATIONS FOR THE ULTRASONIC CLEANER</th>
</tr>
</thead>
<tbody>
<tr>
<td>Transducers</td>
<td>piezoelectric</td>
</tr>
<tr>
<td>Operating frequency</td>
<td>40 to 60 kHz</td>
</tr>
<tr>
<td>Cleaning pan capacity</td>
<td>¾ gallon</td>
</tr>
<tr>
<td>Microcontroller</td>
<td>Intel 8751</td>
</tr>
<tr>
<td>Timing range*</td>
<td>1 to 99 min.</td>
</tr>
<tr>
<td>Solution temperature</td>
<td>w/heater*</td>
</tr>
<tr>
<td>w/ heater*</td>
<td>25 to 99°C</td>
</tr>
<tr>
<td>Power requirement</td>
<td>117-V AC, 60 Hz</td>
</tr>
</tbody>
</table>

*Optional feature
in marine depth finders.

The compression and expansion of the crystalline transducers is coupled mechanically through the bottom of the pan to create the cavitation bubbles in any cleaning solution that you use. (For a complete description of the piezoelectric effect, refer to page 46 of the January 1993 Electronics Now).

If the cleaning solution that you select is a recognized solvent for the contaminants that you expect to find on the parts to be cleaned (for example, oil or grease), the ultrasonic cleaner will enhance the cleaning action of that solution.

**Description of the cleaner.**

The ultrasonic cleaner has three main parts: a stainless steel pan with two transducers attached, a large circuit board containing the power oscillator and time- and temperature-control circuitry, and a small switch/display circuit board containing the control switches and LED displays.

The large circuit board (approximately 5 × 8 inches) is shown in Fig. 1. The left side of the board is occupied by the power transistor amplifier for the oscillator and its heat sink. The oscillator, made up of components on the board, supplies a 40- to 60-kHz, 1000-volt sine-wave to the piezoelectric transducers. The large objects in the center of the board are the two transformers—one standard and one special. The microcontroller and other IC's are located on the right side of the board.

All of the switches are located on the smaller (approximately 2 × 5-inch) PC board shown in Fig. 2. They include, from the left, the ON-OFF power switch, the TIME UP-DOWN toggle switch, the TEMP UP-DOWN switch and the START pushbutton. The green two-digit, seven-segment display on the left indicates time, and red one to its right indicates temperature.

Figure 3 shows the stainless steel cleaner pan upside down with the two piezoelectric ceramic transducers (white disks) bonded to a stainless steel plate which, in turn, is bonded to the pan bottom. The plate transmits the vibrations from the transducers more uniformly through the bottom of the pan to the cleaning solution, and it helps to protect the brittle transducers from damage that might be caused by objects accidentally dropped into the pan.

The ultrasonic cleaner will work very well without the time and temperature circuitry, but building them should be interesting, and they will add value to the cleaner. The controls will be especially useful if you plan to heat the cleaning fluid, and want to set time limits for the cleaning action on specific objects. Moreover, the controls will shut the unit off automatically.

Both time and temperature are programmable—time from 1 to 99 minutes, and temperature from 25° to 99°C. The time and temperature functions are controlled by an Intel 8-bit CMOS 8751 microcontroller, which you can program or purchase already programmed.

**Driver circuit**

Refer to the right side of the two-page schematic diagram Fig. 4. The amplifier in the transducer oscillator driver is a Hitachi 2SC1922 bipolar power transistor, Q1. The oscillator tank circuit is formed by the inductance the secondary winding of transformer T1 and the effective capacitance of transducers RES1 and RES2. Bridge rectifier B1 and capacitor C1 form a 160-volt DC power supply operated from the 120-volt, 60-Hz line. Resistor R1 provides the base bias for Q1, through the feedback winding of T1.

As Q1 turns on, current flows through the primary of T1, which generates an opposing voltage in its feedback winding, tending to turn Q1 off again. At the parallel-resonant frequency of the tank circuit, made up of the secondary of T1, RES1 and RES2, the phase shift between the base and collector of Q1 is exactly 180°, which is necessary for circuit oscillation. The winding ratios of T1 determine the
FIG. 3—VIEW OF INVERTED CLEANER PAN with two piezoelectric transducers mounted on it. The back of the control/display board is shown in the background.

The output voltage, and thus the voltage applied to the two transducers.

The input supply voltage is 160 volts DC, and the turns ratio is about 5 to 1, so the output voltage is about 1000 volts peak-to-peak. In addition, the DC startup current provided by R1 and C2 is the AC drive current for Q1. Resistor R2 and capacitor C3 suppress spurious oscillations at frequencies other than the tank's primary resonant frequency.

As the drive voltage across the transducers swings through the 1000-volt peaks, the transducers expand and contract across their thickness dimensions, and their vibrations are coupled through the pan walls to the cleaning solution.

**Time and temperature control**

The CMOS8751 microcontroller, ICI, is the key component of both time and temperature controls. It responds to input from the START button, TIME UP-DOWN switch, TEMP UP-DOWN switch, and the temperature-sensor circuit. It provides the drive signals for the two-digit time and two-digit temperature LED displays, the transducer power Triac Q2, and the heater Triac Q3.

An assembly-code listing for the Intel 8751 firmware is available from the address given in the Parts List or from the R-E BBS (516-293-3000; 1200/2400 baud 8, N, 1). The program consists of a loop, whose time corresponds to the multiplex rate of the LED displays. Each time the loop is traversed, one of the four digits is enabled; the loop rate is sufficient to eliminate display flicker. Within the loop, inputs are checked and various time, temperature, and display variables are updated. The switches provide direct input through
FIG. 4—SCHEMATIC FOR THE ULTRASONIC CLEANER is divided by dotted lines into the operating control section and the time-temperature control section.

The I/O port.

Temperature is registered in binary format, and it is converted from a digital to an analog signal by resistor string R3 through R9 and IC4-a. This analog signal is then compared with the pan temperature signal from IC5 by IC4-b. When solution temperature falls below the selected threshold, IC6 turns on to energize Q3, which provides current to pan heaters HTR1 and HTR2. When the cleaner is first turned on, the temperature is automatically reset to 25 degrees C. Whenever heat is on, the decimal point of the temperature display LED is turned on.

The timer circuit or function depends on the internal timing capabilities of the '8751, IC1.
When the start button is pressed, Q2 is energized, powering the transducers. The internally registered time is decremented and displayed, and when zero time is reached, Q2 is turned off and the original time is reset. When the cleaner is turned on, the time is set automatically to 5 minutes, but this setting can be adjusted up or down.

Finally, multiplexed segment and digit drive is provided to the displays by IC2, IC3, and current is limited by the eight 120-ohm resistors in network RN1. Power for the control section is provided by T2, D1, D2, and 5-volt regulator IC8. Further details of the firmware operation can be found by reading the code comments.

Circuit board assembly
Refer to Fig. 4, the two-page schematic for the complete ul-
The only component on that board not available as a standard catalog item is transformer T1. You can purchase transformer T1 from the same source given in the Parts List or you can wind your own if you choose to do so.

If you choose to wind your own transformer T1, it will be necessary for you to obtain a ferrite core and Litz wire. The core in the prototype is a Ferroxcube 4229-PA275 ferrite core obtainable from Philips Components Discrete Products, Saguerties, NY 12477. The primary winding has 20 turns of 21 strand/36 AWG Litz wire and the secondary has 99 turns of the same wire. Feedback is obtained with 3½ turns of No. 22 AWG wire.

Be sure to double check the values of all the components as you insert them. Power transistor Q1 is positioned on top of the heatsink as shown in Fig. 1, and both parts are fastened to the board with screws at the same time. Insulate Q1 from the...
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Age: ______ Phone: (_____ )

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California Residents add 6.5% Sales Tax: ____________________________
Total This Order: ____________________________
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Card Expiration Date: ____________________________
Signature: ____________________________

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March 1983 Electronics Now
heatsink with a mica insulator coated liberally with heatsink grease. After mounting Q1, check its isolation with a meter to be sure that it really is insulated from the other components or conductors.

Mount transformer T1 by the lugs on its frame and connect its wires individually as indicated in Fig. 4. If you plan to build the cleaner without the time and temperature controls, the positions for those components will remain open. The precision temperature sensor, LM355, (IC5) will be epoxied on the bottom of the stainless steel pan, and be connected to the board by a twisted pair of wires at P3.

Sockets are recommended for all DIP-style IC’s (IC1, IC2, IC3, IC4, IC6, IC7), particularly the microcontroller, IC1. Insert all resistors, capacitors, plugs (three-pin plug, PL1; five-pin plug, PL3; and four-pin plug, PL4), sockets (25-pin socket SO2 and two-pin socket SO5), resistor network, rectifier bridge, Triacs and diodes. Solder all leads and trim excess lead lengths. Examine the circuit board closely to be sure there are no accidental solder bridges or cold joints.

Refer to the parts positioning diagram, Fig. 6, and insert the three switches (S1-S3), the sockets for the two dual-digit, segmented LED displays, DISP1 and DISP2, and the right-angle, 25-pin header PL2. Solder all leads and trim excess. Again, check for inadvertent solder bridges or cold solder joints before inserting the displays.

Transducer plate and tank

Start the assembly of the tank and transducers by cutting out a $+3 \times 6\frac{1}{2}$-inch rectangle from 0.062-inch stainless steel plate as shown in Fig. 7. Round the corners to $\frac{1}{2}$-inch radiiuses, deburr all edges, and sand or grind both sides so the plate will lie flush against the bottom of the stainless steel tray.

Next, prepare both trans-
Producers, RES1 and RES2, for wire attachment by cleaning their surfaces with alcohol or other suitable solvent. Strip about $\frac{1}{4}$-inch of insulation from both ends of a pair of 24 to 26 AWG multistrand hookup wires approximately 12 inches long for transducer connection. Flatten the wires by fanning out their stranded ends, and tin the strands with lead-tin solder.

Carefully solder the fanned out strands of one wire to the centers of each transducer as rapidly as possible to prevent overheating and damaging the ceramic transducer. Then solder a copper wire, approximately 3 inches long to connect the reverse sides of the transducers, observing the same precautions about soldering.

Note: the transducers are polarized, and both must have the same polarity on top and on the bottom. If this is not observed, the opposing vibrations of each transducer will cancel the effect of the other one.

After the wires are soldered to the transducers, the next step is to bond the transducers to the rectangular transducer mounting plate. Refer to Figs. 3 and 8 to see how the transducers are positioned on the plate. Mix the two parts of a high quality, slow-setting epoxy and apply a film of it to the plate. Position the transducers on the plate, and while applying slight pressure, rotate them slightly so that some epoxy underneath the transducers is squeezed out to form a bead of epoxy around the edges of the transducers where they contact the plate.

When the epoxy holding the transducers has set, apply epoxy to the transducer plate assembly and cement it to the bottom of the tank, also as shown in Figs. 3 and 8. If you intend to include the optional temperature control, adhere the two heating elements, HTR1 and HTR2, to the sides of the pan (one is shown in Fig. 3.) Solder or crimp sleeves to the ends of the heater wires. Solder a...
twisted pair of hook-up wire approximately 12 inches long to the LM335 temperature transducer (IC5) and solder or crimp sleeves to the other ends of the four wires. Epoxy temperature sensor IC5 to the bottom of the pan as shown in Fig. 8. Mark the wires to identify their polarity.

**Final wiring and assembly**

There are no requirements for the ultrasonic cleaner case. You can make one by assembling a box from ¼-inch sheet plastic or you can purchase a small 6 x 6 x 9-inch plastic storage bin from your neighborhood hardware or houseware store. The bin will work very well as a protective case.

Pass the bare ends of the three-wire line cord terminated with a three-prong plug through the grommeted hole in the case. Strip the ends of the wires for soldered or crimped sleeves to connect them to three-pronged plug PL1, observing the ground wire. The on-off switch on the switch-display board will perform the switching function when the small board is plugged into the large board through plug PL5.

Install fuse F1 in its holder, and place the large circuit board in the case. Connect the transducer, heater, and temperature transducer wires by pressing their terminating sleeves over the header pins as shown in Fig. 8. Plug the switch/display board into the sockets SO2 and SO5. Carefully check all component values and placement, and all wiring against the schematic, Fig. 4, before carrying out the test and checkout procedures. Make any corrections necessary.

Before operating the ultrasonic cleaner, check to be sure that the pan is grounded to the line cord ground and the primary of transformer T1 is isolated from its secondary and tank circuit.

**Test and checkout procedure**

Temporarily support the tank next to the circuit board. Fill the pan at least half full with water. **Caution—Never operate the cleaner unless the pan is at least half full of liquid. Apply power, and turn on the cleaner. You should hear a hissing sound from the pan and you should be able to feel the vibrations with your fingertips on the edge of the pan. If you do not hear or feel these operating indications, check for the presence of the primary 160 volts at C1, and ±5 volts at C5.**

When testing, remember that the primary circuit is connected

---

**PARTS LIST**

<table>
<thead>
<tr>
<th>Resistor</th>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>R1</td>
<td>10,000 ohms, wired, 10 watt</td>
<td></td>
</tr>
<tr>
<td>R2</td>
<td>51 ohms, wired, 1 watt</td>
<td></td>
</tr>
<tr>
<td>R3</td>
<td>86,600 ohms</td>
<td></td>
</tr>
<tr>
<td>R4</td>
<td>42,200 ohms</td>
<td></td>
</tr>
<tr>
<td>R5</td>
<td>21,500 ohms</td>
<td></td>
</tr>
<tr>
<td>R6</td>
<td>10,500 ohms</td>
<td></td>
</tr>
<tr>
<td>R7</td>
<td>5300 ohms</td>
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</tr>
<tr>
<td>R8</td>
<td>2610 ohms</td>
<td></td>
</tr>
<tr>
<td>R9</td>
<td>1270 ohms</td>
<td></td>
</tr>
<tr>
<td>R10</td>
<td>8200 ohms</td>
<td></td>
</tr>
<tr>
<td>R11</td>
<td>4640 ohms</td>
<td></td>
</tr>
<tr>
<td>R12</td>
<td>316 ohms</td>
<td></td>
</tr>
<tr>
<td>R13</td>
<td>914 ohms</td>
<td></td>
</tr>
<tr>
<td>R14</td>
<td>1100 ohms</td>
<td></td>
</tr>
<tr>
<td>R15</td>
<td>1000 ohms</td>
<td></td>
</tr>
<tr>
<td>R16</td>
<td>20 - 316 ohms</td>
<td></td>
</tr>
<tr>
<td>R17</td>
<td>20 - 316 ohms</td>
<td></td>
</tr>
<tr>
<td>R18</td>
<td>21 - 360 ohms</td>
<td></td>
</tr>
<tr>
<td>R19</td>
<td>22 - 470 ohms</td>
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</table>

**Capacitors**

<table>
<thead>
<tr>
<th>Capacitor</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>C1</td>
<td>1µF, 200 volt, polyestor film</td>
</tr>
<tr>
<td>C2</td>
<td>47µF, 200 volt, polyestor film</td>
</tr>
<tr>
<td>C3</td>
<td>0.01µF, 100 volt, polyestor film</td>
</tr>
<tr>
<td>C4</td>
<td>1000µF, 15 volt, aluminum electrolytic</td>
</tr>
<tr>
<td>C5</td>
<td>1µF, 15 volts, aluminum electrolytic</td>
</tr>
<tr>
<td>C6</td>
<td>47µF, 200 volt, polyestor film</td>
</tr>
<tr>
<td>C7</td>
<td>10µF, 15 volts, aluminum electrolytic</td>
</tr>
<tr>
<td>C8</td>
<td>1µF, 39 volt, polyestor film</td>
</tr>
<tr>
<td>C9</td>
<td>1µF, 39 volt, polyestor film</td>
</tr>
<tr>
<td>C10</td>
<td>0.05µF</td>
</tr>
</tbody>
</table>

**Semiconductors**

<table>
<thead>
<tr>
<th>Component</th>
<th>Description</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>IC1</td>
<td>74C51 CMOS microcontroller with EPROM, Intel or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC2</td>
<td>74AC244PFC octal bus driver, non-inverting, National or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC3</td>
<td>74FZ44 octal bus driver, non-inverting, National or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC4</td>
<td>LM339 quad comparator, National or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC5</td>
<td>LM335 temperature transducer, National or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC6</td>
<td>74HC02 quad inverting, National or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC7</td>
<td>LM340T5 (7805) voltage regulator, 1A, Motorola or equiv.</td>
<td></td>
</tr>
<tr>
<td>IC8</td>
<td>5 - 25C192 power transistor, Hitachi or equiv.</td>
<td></td>
</tr>
<tr>
<td>Q2</td>
<td>3 - triac, Teczor C404F31 or equiv.</td>
<td></td>
</tr>
<tr>
<td>D1</td>
<td>2N4001 silicon diode</td>
<td></td>
</tr>
<tr>
<td>D2</td>
<td>LNS26GA 7-segment LED display, Panasonic or equiv.</td>
<td></td>
</tr>
<tr>
<td>D3</td>
<td>LNS26RF 7-segment LED display, Panasonic or equiv.</td>
<td></td>
</tr>
<tr>
<td>B1</td>
<td>BR840, full wave rectifier bridge, Diodes Inc. or equiv.</td>
<td></td>
</tr>
<tr>
<td>R11</td>
<td>882 ohm resistor network, CTS9043 or equiv.</td>
<td></td>
</tr>
</tbody>
</table>

**Other component**

<table>
<thead>
<tr>
<th>Component</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>F1</td>
<td>fuse, 6 ampere, standard</td>
</tr>
<tr>
<td>HTR1</td>
<td>100 watts, 120 volts</td>
</tr>
<tr>
<td>L1</td>
<td>500µF</td>
</tr>
<tr>
<td>L2</td>
<td>1000µF</td>
</tr>
</tbody>
</table>

**Miscellaneous**

- Resistors: all 1/4-watt, metalized film, 5% unless otherwise stated.
- Capacitors: all electrolytics.
- Semiconductors: all NPN, N-channel, 500 volt, silicon, if not specified.
- Other components: all as specified.
- Wires: all twisted pair, wirewound, 10,000 ohms, 1000ohms, 10,000 ohms.
- Other wires: all twisted pair, wirewound, 10,000 ohms, 1000ohms, 10,000 ohms.
- Fuses: all 1/4-inch, wirewound, 10,000 ohms, 1000ohms, 10,000 ohms.
- Other components: all as specified.

**Note:** The following parts are available from A&T Labs, P.O. Box 4884, Wheaton, IL 60187:

- Kit of parts for the ultrasonic cleaner without the transformer or control/controls/displays or case, $39.00
- Kit of all parts for the complete ultrasonic cleaner including programmed 8751 microcontroller except case, $249.00
- Double-sided, printed circuit boards—large, $25.00; small, $9.00
- Programmed Intel 8751 microcontroller, $29.00
- Custom-wound transformer T1, $69.00
- Ceramic piezoelectric transducers RES1 and RES2, $32.00
- Stainless steel cleaner pan, $19.00
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to the 120-volt power line, so exercise caution to avoid electric shock. Also, the voltage applied to the transducers is about 1000 volts. If the unit fails to function at turn-on, check for the presence of 11 MHz at pin 18 of the microcontroller ICl, and look for changes in the time and temperature display LED's. At turn-on, those digital displays should readout 5 and 25, respectively.

Although the design frequency should be close to optimal, further adjustment could improve efficiency. Perform any additional tuning by turning the slug core of transformer T1. Adjust it gradually until you are able to observe maximum turbulence in the cleaning fluid. One way to determine a maximum is by adding a drop of food coloring to the water, and adjusting for maximum dispersion rate of the color in solution.

Cleaner operation
You can purchase cleaning fluids from hardware, auto parts, and grocery stores, but you can also easily mix your own. You might want to experiment with cleaning mixtures. A general rule of thumb is that any cleaning solution that works satisfactorily in cleaning objects by hand methods will also work in the ultrasonic cleaner. Liquid detergent in water, for example, is a good general cleaner, while ammonia in water works well for jewelry. Carburetor cleaner cleans carburetors and other automotive, bicycle or machine parts that are coated with oily or greasy contaminants.

Before cleaning any object in the ultrasonic cleaner, it is a good idea to remove as much surface dirt and grime as possible manually with paper towels, brushes, or cotton rags to minimize the contamination entering the cleaning solution. The
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Precautions

The cleaner operates from 120-volt line power and there are liquids present; together these pose an added electric shock hazard if proper grounding is not maintained. Moreover, some cleaning solutions and their vapors can be toxic. Other precautions are:

- The use of flammable cleaning fluids is not recommended. If they are used, exercise all reasonable precautions by moving the cleaner out of doors and never leave it unattended while the fluid is in the pan. Be sure to return all toxic fluids to a safe storage container when cleaning is complete. Never use gasoline as a cleaning fluid!

- Never put your hands into the cleaning solution when the cleaner is on. The intense vibrations can drive particulates into your skin, and the ultrasonic energy could damage body tissues.

- Minimize any time spent close to the operating cleaner because the high-frequency 40-kHz oscillations can cause headaches and might lead to hearing impairment although they are not audible.

- Be sure that the pan is at least half filled with solution during all cleaning operations.

- Place any objects to be cleaned carefully in the pan with tongs, and take care not to drop any heavy object in the pan that could damage the fragile transducers.

- The use of chlorofluorocarbon (CFC) solvents, commonly used to remove solder paste from circuit boards, is not recommended because of their threat to the environment.
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FIELD-EFFECT TRANSISTORS (FET's) are unipolar rather than bipolar devices, and this gives them certain properties that are superior to those of bipolar transistors. Unlike the bipolar transistor, whose current depends on the movement of both electrons and holes, FET operation depends on only one of those charge carriers. Freed from the time delays that occur when those charge carrier recombine, FET's offer faster switching speed and higher cutoff frequencies.

Other advantages of the FET include:
- Voltage rather than current operation.
- Extremely high input impedance in the off state.
- Virtually constant current with respect to voltage at specific bias levels.
- Current change that is inversely rather than directly proportional to temperature.

Despite these advantages, the FET has not replaced the bipolar transistor in all applications, but it has encouraged new generations of small-signal and general purpose and RF MOSFET's as well as general purpose and RF MOSFET power transistors. Moreover, the latest digital logic families are based on FET technologies. The basic FET is a simple, three-terminal, voltage-controlled device with characteristics that are similar to those of vacuum-tube pentodes. Thus, the FET is considered to be the solid-state equivalent of a pentode.

The two major classes of FET's are the junction FET (JFET) and metal-oxide-semiconductor FET (MOSFET), formerly called an insulated-gate FET (IGFET). FET's are further divided into N-channel, P-channel, depletion-mode and enhancement-mode devices. MOSFET's with N-doped channels are called NMOS, and those with P-doped channels are referred to as PMOS.

The three electrodes in all FET's are the source, drain, and gate, analogous to the emitter, collector, and base of the bipolar transistor. Both JFET's and MOSFET's are available as discrete transistors. Some MOSFET's have dual gates and are intended for use as radio-frequency mixers.

This article explains how P-channel and N-channel MOSFET's are combined to form the popular complementary-MOS (CMOS) digital logic families. CMOS technology has made possible very large scale integrated (VLSI) memories, microprocessors and dedicated circuits that contain more than one million transistors and still have very low power requirements.

Most small-signal FET's today are fabricated with planar geometry in which all electrodes are accessible from the top of the device. The active regions are defined on the wafer or substrate by successive masking, etching, and deposition or ion-implantation steps. But power MOSFET's now being fabricated with vertical structures are actually capable of handling much higher current in smaller areas of silicon.

Junction FET's

The simplest FET, the JFET, is illustrated by the cross-section view of Fig. 1-a. It is made by selectively implanting or diffusing ions into the wafer or substrate. An N-type region is
defined on the P-type substrate by photolithographic methods, and N-type ions are implanted to form the N-channel. Later in the manufacturing process, following further masking, oxidation deposition and etching steps, P-type ions are implanted or diffused into the N-channel to form the P-type gate.

Aluminum source and drain terminals are formed directly on the N-channel and an aluminum gate terminal is formed on the P-type gate. The symmetrical construction of the JFET permits the drain and source to be interchanged, if necessary.

If a positive voltage is applied at the drain of the N-channel JFET shown in Fig. 1-a, and a negative voltage is applied at the source with the gate terminal open, a drain current flows. When the gate is biased negative with respect to the source, the PN junction is reverse biased, and a depletion region, devoid of current carriers, is formed.

Because the N-channel is more lightly doped than the P-type gate material, the depletion region penetrates into the N-channel. This region, depleted of charge carriers, behaves like an insulator. The depletion region narrows the N-channel and increases its resistance. If the gate bias is made even more negative, drain current is cut off completely.

The gate-bias voltage that cuts off the drain current is called the pinchoff or gate-cut-off voltage. However, as the bias becomes positive, the depletion region recedes, the channel resistance is reduced, and drain current increases. Thus, the JFET gate actually controls JFET current.

The schematic symbol for the N-channel JFET is shown in Fig. 1-b. As in other schematic symbols for solid-state devices, the arrowhead (representing the direction of conventional current flow) points from P-doped material to N-doped material. In the N-channel JFET symbol, the arrowhead points from the P-type gate toward the N-type channel.

A section view of a P-channel JFET is shown in Fig. 2-a. The channel of the device is P-type material, and the gate is N-type. If a positive voltage is applied to the source, conventional current flows from the source to the drain. To reverse bias the junction between the N-type gate and the P-type channel, the gate must be made positive with respect to the channel. The biasing voltages of a P-channel JFET are opposite to those of the N-channel JFET.

The schematic symbol for the P-channel JFET is shown in Fig. 2-b. The arrowhead also points from P-type material to N-type material. In this instance, it points from the P-type channel to the N-type gate region. The characteristics of the P-channel JFET are similar to those of the N-channel device, except that the voltage and current polarities are reversed.

Both N-type and P-type JFET's operate in the depletion mode; that is, they conduct with zero bias on their gates. Figure 3 shows a typical family of drain characteristics for an N-channel JFET. As the gate-to-source voltage increases, the drain current increases until a饱和 state is reached where further increases in voltage cause only small increases in current. This saturation region is marked by the pinchoff voltage, which is the minimum gate voltage required to cut off the drain current.

The gate of a JFET can be biased by a voltage source, and the drain current is controlled by changing the gate voltage. This makes the JFET a useful device for applications requiring voltage-controlled current sources or current amplifiers. The JFET is also used as a switching device, where it can be turned on and off by changing the gate voltage.
source voltage is made increasingly negative, the depletion region is increased, and drain current decreases. As a result, pinchoff voltage occurs at a lower value of $V_{DS}$. Curves for different values of gate-to-source bias, $V_{GS}$, are plotted in the figure because the FET is a voltage-operated device.

**JFET Circuits**

When an N-channel JFET is connected to a $V_{DS}$ supply as shown in Fig. 4, a drain current, $I_{D}$, flows in the device. The magnitude of $I_{D}$ can be controlled by a gate-to-source bias voltage, $V_{GS}$. Similarly, when a P-channel JFET is connected to a negative drain voltage, a drain current, $I_{D}$, flows in the device. The value of $I_{D}$ is maximum when $V_{GS}$ equals zero, and it is reduced (to bring the JFET into a linear operating region) by applying a reverse bias to the gate terminal of the device (negative bias in a N-channel device, positive bias in a P-type).

In Fig. 3, the value of $V_{GS}$ to reduce $I_{D}$ to zero, the gate-to-source pinchoff voltage $V_{P}$, is about -7 volts. The value of $I_{D}$ when $V_{GS}$ equals zero (called $I_{DSS}$ or drain saturation current for zero bias) is about 52 milliamperes for the device shown in the figure.

The gate-to-source junction of the JFET has the characteristics of a silicon diode. When reverse biased (to bring it into its linear operating region), gate leakage currents ($I_{GSS}$) are measured in thousands of a microampere at room temperature. Actual gate signal currents are only a fraction of a drain-to-source voltage ($V_{DS}$) is increased from zero to a value at which a knee occurs on each curve. Moreover, $I_{D}$ remains virtually constant as $V_{DS}$ is increased beyond where the knee occurs.

Thus, when $V_{DS}$ for any of the family of $V_{GS}$ curves is below its knee value, the drain-to-source}

![FIG. 4—N-CHANNEL JFET COMMON-source amplifier is analogous to a bipolar common-emitter amplifier.](image-url)

![FIG. 5—N-CHANNEL JFET COMMON-drain (source-follower) amplifier is analogous to a bipolar emitter-follower amplifier.](image-url)

![FIG. 6—N-CHANNEL JFET COMMON-source amplifier is analogous to a bipolar common-base amplifier.](image-url)}
as a voltage-to-voltage converter or amplifier. As shown in Fig. 4, a load resistor of suitable value, \( R_L \), should be placed in series with the JFET's drain-to-source current.

Another common JFET configuration is the common drain or source-follower configuration shown in Fig. 5. That configuration is analogous to the bipolar emitter-follower configuration. Yet another possible JFET configuration is the common-gate configuration shown in Figure 6. That configuration is analogous to a bipolar common-base configuration.

**MOSFET's explained**

The metal-oxide FET or MOSFET was developed as an improvement on the JFET, and it has become the most important form of FET. Figure 7-a illustrates an N-channel depletion-mode MOSFET with a negative gate bias. The gate of this MOSFET is fully insulated from the adjacent channel. This is the most important distinction between an N-type depletion-mode MOSFET and an N-type JFET, which is manufactured with a doped gate region directly under and in contact with the gate.

The surface of the silicon P-type wafer is first coated with a layer of silicon dioxide (SiO\(_2\)), and the source and drain windows are masked and etched to expose the P-type substrate. N-dopants are heavily diffused or implanted into those two regions. Another window is masked and etched over the channel, and it is given a lighter concentration of N dopant. In subsequent steps, the channel is recoated with an insulating oxide, and the metal source, drain, and gate terminals are deposited.

When the drain is positive with respect to the source, a drain current will flow, even with zero gate voltage. However, if the gate is made negative with respect to the substrate, positive charge carriers (holes) induced in the N-channel will combine with the electrons and cause channel resistance to increase. With increasing negative bias, the pinchoff voltage will be reached, and drain current will cease. However, if the gate is made positive with respect to the substrate, additional electrons are induced, and the channel current then increases.

The schematic symbol for the N-type depletion-mode MOSFET is shown in Fig. 7-b. The path or channel between the source and drain is shown as a solid bar. The symbol for the P-channel depletion-mode MOSFET is identical to the N-type, except that the arrow points outwards.

Figure 8 is a drain-to-source characteristic curve for an N-channel depletion-mode MOSFET. It can be seen that the current drain, \( I_D \), is inversely proportional to the magnitude of the negative gate voltages, \( V_{GS} \). Compare Fig. 8 with Fig. 3 for the N-channel JFET to see their similarities.

Planar enhancement-mode MOSFET's are made by the same methods as planar depletion-mode MOSFET's. However, the N-channel enhancement-mode MOSFET shown in Fig. 9 does not have the N-doped drain-to-source channel through the P-type substrate of the N-channel depletion-mode MOSFET. Therefore, there is no conduction between drain and source at zero gate bias.

To turn an enhancement-mode MOSFET on, positive gate bias is needed. As the gate voltage is increased, more electrons are induced into the channel. They cannot flow across the oxide layer to the gate, so they accumulate at the substrate surface below the gate oxide. When a sufficient number of

![Figure 8](www.americanradiohistory.com)

**FIG. 8—DRAIN CURVES FOR N-CHANNEL DEPLETION-MODE MOSFET showing the effects of positive and negative bias.**

![Figure 9](www.americanradiohistory.com)

**FIG. 9—N-CHANNEL ENHANCEMENT-MODE MOSFET with positive grid bias (a), and schematic symbol (b).**
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FANTASTIC FM TRANSCIEVERS
SYNTHESIZED—NO CRYSTALS

RAMSEY Electronics has remade the popular FM tuner with a new, thin, flat panel design. The RX-FM 1 operates on FM only, providing high-quality audio at an affordable price. The RX-FM 1 features a high-gain, low-noise preamplifier, wide-bandwidth, and a wide tuning range. The RX-FM 1 is perfect for home entertainment or portable use. The RX-FM 1 delivers superior audio performance and is the ideal choice for any FM enthusiast.

Features:
- High-gain, low-noise preamplifier
- Wide-bandwidth
- Wide tuning range
- High-quality audio
- Perfect for home entertainment or portable use

Order now and take advantage of our special introductory offer! RX-FM 1: $199.95

ORDER NOW

WAVE RADIO SERVICE MONITOR

COM-3 is the world's smallest service monitor. For those big or small, the COM-3 delivers advanced performance and features. COM-3 is a must-have for any serious audio enthusiast. COM-3 offers a wide range of features, including a high-quality preamp, wide-bandwidth, and a wide tuning range. The COM-3 is perfect for home entertainment or portable use. The COM-3 delivers superior audio performance and is the ideal choice for any audio enthusiast.

Features:
- High-quality preamp
- Wide-bandwidth
- Wide tuning range
- Perfect for home entertainment or portable use

Order now and take advantage of our special introductory offer! COM-3: $299.95

ORDER NOW

FREQUENCY COUNTERS

CT-70 7 DIGIT 512 MHz
CT-90 9 DIGIT 600 MHz
CT-125 9 DIGIT 1.2 GHz

New low-cost microprocessor-driven frequency counters are available. These counters display both frequencies and audio and video levels. The CT-70, CT-90, and CT-125 display both frequencies and audio and video levels. The CT-70 displays frequencies up to 512 MHz, the CT-90 displays frequencies up to 600 MHz, and the CT-125 displays frequencies up to 1.2 GHz. These counters are perfect for any application where accurate frequency measurement is required.

Features:
- Low-cost microprocessor-driven
- Frequency and audio/video level display
- CT-70 displays up to 512 MHz
- CT-90 displays up to 600 MHz
- CT-125 displays up to 1.2 GHz

ORDER NOW

MICROWAVE INTRUSION ALARM

A real microwave Dopplar detector that will detect a human or an animal from 10 feet away. The 1.4 GHz frequency is not affected by heat, light, or vibrations. Drives up to 1000 sq. ft., outdoors or indoors, on windows, doors, or flowerpots. Low voltage, 1500-2400V. Complete set with 100 ft. of wiring. Complete set: $189.95

ORDER NOW

MICROWAVE AUDIO

Now use your microwave to produce the most accurate and versatile microwave audio system available. Use your microwave oven, along with a 30-cm waveguide, to generate audio frequencies. Use this system to produce a wide range of audio frequencies for use in any application. Complete kit: $189.95

ORDER NOW

TONE DECODER

A complete tone decoder for a PC-based PC tone set. 40,000-500 MHz, high signal strength, low noise, and high immunity to interference. Can be used with your own decoder. Complete kit: $189.95

ORDER NOW

TICKLE STICK

A funny toy size Doppler LED alarm will alert you to any intruder. The light emitted by the LED is visible from several hundred feet away. Ideal for office desk, car, or home. Complete set: $189.95

ORDER NOW

VOICE ACTIVATED SWITCH

A voice-activated switch will provide low-cost, two-level control. Current capabilities include automatic-off for appliances, lights, and other devices. Complete kit: $189.95

ORDER NOW

TELEPHONE SPEAKER PHONE

Talk on the phone hands-free, great for in-home or office use. No more struggling to hold the phone line, no more struggling to answer the phone. Our speaker phone is perfect for any busy professional. Complete kit: $189.95

ORDER NOW

SPEAKERPHONE SPEAKER

A super-sensitive, low-noise microphone with a miniature power amplifier. The speakerphone speaker is perfect for any busy professional. Complete kit: $189.95

ORDER NOW
DMM 2360
$129.95
DMM + LCR Meter
Most Versatile DMM
Inductance: 1 µH - 400µH
Capacity: 1 F - 400µF
Frequency: 1 Hz - 4 MHz
Temperature: -40 to 320°F
Logic Test: 20MHz
Diode, Continuity
Volt, Amp, Ohm
3999 count display
Peak Hold
Auto power off

DMM 175A
$67.95
DMM with 20 MHz Frequency Counter
Most popular DMM
Freq. Counter 1Hz-20MHz
DCV: 1MΩ-1000V
ACV: 1MΩ-750V
Accuracy: 0.1% ±2
Cap: 1µF-20µF
TTL Logic test 20 MHz
Translator: HFE test
Diode test
LED test
3 1/2 digit display
10 MHz impedance

LCR Meter 814
$199.95
The Best Handheld LCR
Inductance: 0.1 µH - 200H
Capacitance: 0.1 µF - 200 µF
Resistance: 1 mΩ - 20MΩ
1% basic accuracy
Dissipation factor indicates leakage in capacitor and Q factor in inductor
Zero adjustment to reduce parasitics from test fixture
Very good for high frequency RF and surface mount components

LCR Meter 195
$119.95
Volume popular LCR
Inductance: 1 µH - 200H
Capacitance: 0.1 µF - 20µF
Resistance: 0.01Ω - 200Ω
Accuracy: ±1%, 0.1%, ±2%
Test frequency 1 kHz

20 MHz Oscilloscope with Delay
Sweep PS-205
$429.95
Dual Trace, Component test, 6“ CRT, X-Y Operation, TV Sync, 2 Modulation, CH2 Output, Graduated Hilum, 2 probes
1x, 10x. Best price with delay sweep
PS-200 20MHz DUAL TRACE $339.95
PS-405 40MHz DELAY $569.95
PS-605 60MHz DELAY $769.95

20 MHz Digital Storage Oscilloscope
DS-203 $769.95
Switchable between digital and analog
2 K word per channel storage
Sampling rate: 10 M sample/sec
8 bit vertical resolution
25 Larsec/div
Expanded Timebase 10msec - 500µsec
Refresh, Roll, Save at, Save Ch2, Pre-Trig
Plotter Control

Power Supply
PS-303
$169.95
0-30 VDC, 0-3A output
0.02% + 2 mV line regulation
0.02% + 3 mV load regulation
1 mVrms noise and ripple
Short circuit and overload protected

RF SIGNAL
GENERATOR
SG-4160B $124.95
100 kHz-150MHz sinewave in 6 ranges
Output: 10mVrms to 35 mV
Internal 1kHz, External 50Hz-20kHz modulation

RF SIGNAL
GEN./COUNTER
SG-4162AD $234.95
Generates RF signal same as SG-4160B
Frequency counter 1Hz-150MHz
Sensitivity: 50mV
For internal and external sources

AUDIO GENERATOR
AG-2601A $124.95
1Hz - 1MHz in 5 ranges
Output: 80mVrms sine, 10Vp-p squarewave
Synchronization: ±3% of oscillation frequency per Vrms
Output distortion: 0.05% 50Hz - 50kHz
0.5% 50kHz - 500kHz
Output impedance: 600 ohm

AUDIO GEN./COUNTER
AG-2603AD $239.95
Generates audio signal same as AG-2601A
Sensitivity: 0.5mV - 500kHz
For internal and external sources

FUNCTION GENERATOR
FG-2100A $169.95
0.2 Hz - 2 MHz in 7 ranges
Sine, square, triangle, pulse and ramp
Output: 5mV-20Vp-p
1% distortion, DC offset ± 10V
VCF: 0-10V control frequency to 1000:1

FUNCTION GEN./COUNTER
FG-2102AD $234.95
Generates signal same as FG-2100A
Frequency counter 4 digits
Feature TTL and CMOS output

Sweep Function
GEN./COUNTER 329.95
0.5 MHz to 5 MHz
Sweep: Lin, Log 10:1
20mS to 2S
AM Modulation
Gated Burst, Voltage Control Generator,
Generator Control Voltage & 6 digit Counter.
The **ATH-15** can ACCURATELY READ an input signal, DISPLAY the frequency and AUTOMATICALLY switch to HOLD status, in less than 8% of a second!!

**ATH™** refers to our exclusive new AUTOMATIC TRIGGER & HOLD circuit with AUTOMATIC CLEAN DROPOUT. With **ATH™** you can say good-bye to almost all of that annoying random counting and the false readings we have become accustomed to when using portable counters. The model **ATH-15** is a NEW ULTRA HIGH SENSITIVITY, 1 MHz to 1500 MHz frequency counter with an INTEGRATED BAR GRAPH circuit which instantly displays the signal strength of an input signal from <1 MHz to over 4 GHz. When the **ATH™** feature is used, the counter displays the last readable signal received. It automatically triggers on a readable signal and automatically switches to the "hold" status when the signal disappears. Because of AUTO TRIGGERING, the first reading is correct. If the signal stops in the middle of a sample or gate time, the last complete accurate reading will be displayed and the unit switched back to "HOLD" status, hence the AUTOMATIC CLEAN DROPOUT prevents the display of erroneous data, all this is done automatically, with hands free operation - and it works great!!

We are further responding to user requests by offering a ONE-SHOT **ATH™** option. This consists of a ONE-SHOT select switch, a push button RESET switch and two LED indicators all located on the top of the counter (not shown). When this function is used, the first readable signal that triggers the counter will be held on the display until manually reset. One push of the reset button will reset the display to zeros and enable the one-shot circuit again. The display can be blanked or turned off pending the auto triggering from an input signal, which also saves power under battery operation.

**RESPONSE TIME**, defined as the time from the beginning of the input signal to a stable, accurate, readable display, has been dramatically speeded up. The RESPONSE TIME is actually 800% faster than previous models and if you consider not having to manually throw the hold switch, at just the right time, the **ATH-15** is functionally the fastest counter you can buy!!

**MADE IN USA**

**SAY GOOD-BYE TO RANDOM COUNTING & FALSE READINGS**

**ATH-15**

**CHECK IT OUT... BEFORE YOU BUY A COUNTER**

Does Bar Graph give INSTANT readings of 3 gate times delayed?

Does Bar Graph work on every range? Over 2 GHz? With HOLD on?

Does HOLD switch CHANGE the GATE selection when turned off?

Does unit SELF-OCTILLATE - random count with no input signal?

How many switches needed to select range? Gate times range?

How long does unit operate with batteries? One hour?

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March 1993, Electronics Now
MAGNETIC WIRE
Plain enamel. Solid bare copper. For winding coils, transformers and toroids. Tapes for #71 to 8/32 spools.
$14.3.25
$16.3.30
$18.3.35
$20.3.50
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MAKING CIRCUIT BOARDS THE NEW, EASY WAY WITH TEC-200 FILM
JUST EASY STEPS - Core circuit pattern on TEC-200 film using any plain copier.
- Iron-on film to copper clad board.
- Uses off film and paper for 8 1/2 x 11 size. 

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IRON
T-25-2 .40 FT37-43 .60
T-25-6 .40 FT37-61 .80
T-37-6 .45 FT50-61 .75
T-50-2 .55 FT50-61 .75
T-60-3 .55 FT50-61 .75
T-60-6 .55 FT50-61 .75
T-60-8 .75 FT50-61 .75
T-60-10 .75 FT50-61 .75
T-114-11 .25 FT50-61 .75

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Balanced Mosfet Osc. Popular 2 stripexperimentation for building DC and superhet receivers.
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200 WATT INVERTER
Plugs into your lighter and runs
- FM Equipment
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- Portable fan
- Compact fan
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- TV with VCR
- MORE

TRIMMER CAPACITOR ASSORTMENT
Top Quality. Also contain some two and three gang units.
10 pcs. $1.50
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50 pcs. $6.95

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200mA Ammeter. Scale reads signal 0-800. Has two earfingers for clipping meters. Measures approx. 1 1/2" x 1 1/4" x 1/4". $4.00

EDGEMOUNT 5-SW-80-METER-SWR
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MULTIVOLTAGE AC ADAPTER
- Rugged 500mA Input 117VAC Output 3V, 4.8V, 6V, 7.5V, 9V, 12V DC Power supply Universal plug
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- 14002 .09
- 14003 .10
- 14004 .10
- 14005 .10
- 14006 .15
- 14007 .17
- 14008 .20
- 14501 .20
- 14502 .20
- 14503 .20
- 14504 .25
- 14505 .25
- 14506 .25
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- 14006 .15
- 14007 .17
- 14008 .20
- 14501 .20
- 14502 .20
- 14503 .20
- 14504 .25
- 14505 .25
- 14506 .25
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Gold Conditioner & Protector
- Protects Gold Surfaces & Base Metals!
- Improves Conductivity!
- Forms Protective & Anti-tarnish Coating!
- Reduces Wear & Abrasion!
- Reduces Arcing & RFI!
- Reduces Intermittent Connection Failures!

ProGold is specifically formulated to improve conductivity and protect gold, base metals and other precious metal surfaces.

A common problem with gold plated surfaces is that the base metals migrate to the surface due to gold’s soft and porous nature (dendrite corrosion). Once exposed, base metals oxidize, adding unwanted resistance that impedes electrical performance. Since gold plated surfaces are thinly coated, they are susceptible to scratching & abrasion, further exposing the base metals.

ProGold, a one step treatment, conditions gold connectors, contacts and other metal surfaces, enhancing the conductivity characteristics to efficiently transmit electrical signals. Non-abrasive/non-corrosive formula, non-flammable, non-toxic, ozone-safe.

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Improves Conductivity and Protects Electrical Connections
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- Reduces Intermittent Connection Failures
- Reduces Arcing & RFI
- Reduces Wear & Abrasion
- Extended Temperature Range, -34°C to 200°C

DeoxIT, a one step treatment, is a fast-acting deoxidizing solution that cleans, preserves, lubricates and improves conductivity on all metal surfaces. Temperature range -34°C to 200°C. Non-flammable, non-toxic, non-corrosive, non-gumming, ozone-safe.

PreservIT, seals, lubricates and preserves metal surface for protection from oxidation and contamination. For use on clean surfaces or ones pre-cleaned with DeoxIT. Temperature range -34°C to 200°C. Non-flammable, non-toxic, non-corrosive, non-gumming, ozone-safe.

These new advanced formulas contain improved deoxidizers, preservatives, conductivity enhancers, anti-tarnishing compounds, arcing & RFI inhibitors and provide extended temperature range. DeoxIT's new formulation also prevents dissolved oxides from re-attaching to metal surfaces, providing longer lasting protection.

"We were having trouble with edge connectors in our manufacturing environment until we tried ProGold Wipes...great product." J. P., General Electric

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"For many years we have been using CAIG's liquid and spray products in the lab for service and repair of connectors, switches and potentiometers. I also use their paste products on my boat to prevent corrosion from salt water and air...fine products for a variety of applications." T. S., University of California, Lawrence Livermore National Laboratory

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Orbitron antennas ("size for size") are known the world over for their superior reception and picture quality.
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10ft 349
10ft H.D. 439
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STANDARD Ku SYSTEM
Package INCLUDES all of this:
- Quality aluminum 3ft dish
- Pansat BR 1100 Receiver
- Polar tracking mount
- Polarity switching feed
- Low Temperature LNB
- 100ft All in one ribbon cable

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- Frequency: 8 x 10 display, composite video inputs
- Power Level: 75 ohms, selectible 1 volt or 4 volt full scale (100 IRE units)
- Automatic tone synthesized frequency
- Unterminated range and ±1 dB.
- Price: $495.00

**Tektronix Solid State Portable 491 Spectrum Analyzer**

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- Linearity: ±0.5 dB to 100MHz.
- Sensitivity: 50μV for 10dB.
- Distortion: <0.1%.
- Price: $959.00

**Collins 30L-1 Linear Amplifier (5-Line)**

- Frequency: 10 to 15 MHz.
- Power Output: 1000W.
- Harmonic Distortion: 30 dBc.
- Price: $595.00

**Collins KWM-2A Transceiver**

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- Power Output: 100 watts PEP.
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- Power Output: 100 watts PEP.
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**General Microwave 476 Thermoelectric Power Meter**

- Frequency Range: 0.1 to 10 MHz.
- Power Range: 1mW to 100W.
- Accuracy: ±1%.
- Price: $350.00

**Tektronix 520A Dual Channel Vector Scope**

- Measures: Luminance Amplitude, Chrominance Amplitude and Phase differential phase and gain.
- Accuracy: CR1 accuracy of 1.2° and 1.5° for vector and amplitude measurements.
- Internal calibrated phase shift with a range of 1°.
- Price: $1495.00

**Model HP 180A Oscilloscope**

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- Power Range: 1mW to 100W.
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**ANRITSU ML422B Programmable Selective Level Meter**

- Frequency Range: 3kHz to 2GHz.
- Accuracy: ±1%.
- Price: $350.00

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**Tektronix 52B Solid State N.T.S.C. Waveform Monitor**

- Frequency: 8 x 10 display, composite video inputs
- Power Level: 75 ohms, selectible 1 volt or 4 volt full scale (100 IRE units)
- Automatic tone synthesized frequency
- Unterminated range and ±1 dB.
- Price: $495.00

**Tektronix Solid State Portable 491 Spectrum Analyzer**

- Frequency: 9kHz to 2GHz with internal mixer.
- Linearity: ±0.5 dB to 100MHz.
- Sensitivity: 50μV for 10dB.
- Distortion: <0.1%.
- Price: $959.00

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- Frequency Range: 3kHz to 2GHz.
- Accuracy: ±1%.
- Price: $350.00

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**8 MM SONY VIDEO CASSETTES (USED)**

Sony
120 minute, Hi8 metal particle video cassettes. Used and bulk erased. In new condition these high quality cassettes would sell for considerably more. A great deal for 8mm camcorder users. CAT# VCU-8 $2.50 each • 5 for $11.00

**Solid State RELAY For D.C. Loads**

Opto 22 # DC60S3 Control Voltage: 3-32 Vdc Load: 3 amps @ 4-60 Vdc (5 amp surge). This Solid State relay is designed to switch D.C. loads. 22.5° X 1.75" X 0.91" high. Epoxy block with metal base. Screw terminals.

CAT# SSRLY-12U $9.50 each

**General Use A.C. Switch**


CAT# ETS-1 2 for $1.00

**12 VDC 300 ma. Wall Transformer**

New 12 Vdc. 300 ma wall transformers. Cord terminates to bare wire. Large quantity available. CAT# DCTX-1231 $2.25 each

100 for $20.00 • 1000 for $185.00

**PHOTOELECTRIC SWITCHES**

Adalet model 57010. Turn lights, signs and other electrical devices on at dark and off at dusk. Built-in delay to prevent switching caused by sudden change in ambient light. 120 Vac, 300 watts. UL listed. 0.65" diameter threaded bushing for mounting. Threaded plastic nut 9" long pigtails leads. CAT# PES-1 $3.00 each

Adalet model 57000. Operates the same as the unit left, but this one is built-into an adjustable swivel mount to facilitate aiming the device. Base of swivel is threaded 3/4" threaded bushing designed to screw into standard electrical knock-out box. CAT# PES-2 $4.00 each

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Premium quality metal tape in C-60 cassettes (30 or more per side). One of the finest "brand-name" tapes on the market, in durable, clear plastic transport mechanisms. Recorded and bulk erased, the record-protect tabs have been removed and therefore, need to be taped over to re-record. Audiophiles will appreciate the wide dynamic range of this tape. If your cassette deck has a "metal" setting you will hear the difference. A real bargain!

CAT# C-600M $1.25 each

10 for $10.00

**CASSETTE STORAGE CASE**

Black, unbreakable plastic audio cassette storage case. CAT# CBOX 5 for $1.00 • 100 for $15.00

**CABLE TIES**

<table>
<thead>
<tr>
<th>Type</th>
<th>Approx. Length</th>
<th>Min. Tensile Strength</th>
<th>Color</th>
<th>Max. Bundle Dia.</th>
<th>15'</th>
<th>100'</th>
<th>1000'</th>
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<tbody>
<tr>
<td>TR-400</td>
<td>4&quot;</td>
<td>18 lbs</td>
<td>neutral</td>
<td>15/16&quot;</td>
<td>.30</td>
<td>$2.50</td>
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<td>TR-400B</td>
<td>4&quot;</td>
<td>18 lbs</td>
<td>black</td>
<td>15/16&quot;</td>
<td>.35</td>
<td>$3.00</td>
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<tr>
<td>TR-800</td>
<td>6&quot;</td>
<td>30 lbs</td>
<td>neutral</td>
<td>1 1/2&quot;</td>
<td>.50</td>
<td>$4.00</td>
<td>$30.00</td>
</tr>
<tr>
<td>TR-800B</td>
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<td>black</td>
<td>1 1/2&quot;</td>
<td>.50</td>
<td>$4.00</td>
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<tr>
<td>TR-800C</td>
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<td>50 lbs</td>
<td>neutral</td>
<td>1 3/4&quot;</td>
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<tr>
<td>TR-1500</td>
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<td>50 lbs</td>
<td>neutral</td>
<td>4&quot;</td>
<td>1.00</td>
<td>$8.00</td>
<td>$70.00</td>
</tr>
<tr>
<td>TR-1500B</td>
<td>15&quot;</td>
<td>50 lbs</td>
<td>black</td>
<td>Heavy-duty 15&quot; cable tie.</td>
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<tr>
<td>TR-1500L</td>
<td>15&quot;</td>
<td>120 lbs</td>
<td>neutral</td>
<td>4 1/4&quot;</td>
<td></td>
<td>$1.50</td>
<td>$12.00</td>
</tr>
</tbody>
</table>

**DYNAMIC MICROPHONE 115 VAC COOLING FAN**

Good quality dynamic mike. Brushed aluminum with black trim. 0.93" dia. X 4.42" long. 5" cord with 3.5mm mini-plug.

CAT# MIKE-12 $1.50 each

Open frame cooling fan with 3.25" square plastic cage. Mounting holes on 2.75" centers.

CAT# CF-16

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**15" POWER CORD**

15" Bolden SVT 18/3 black detachable power cord. 3 prong right angle grounded AC plug one end, IEC socket other end

CAT# LCAC-15 $1.25 each • 10 for $1.00

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Electronics News March 1993
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**WARNING!!!**

DO NOT BUY these products if you do not know the dangers of laser energy! We are selling components only. If assembled into a complete laser system, they must comply with all C.E.R.L. regulations.

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**Laser Tube**

Siemens # LG7 659
1 mW helium-neon laser tube.
22.5 mm diameter X 146 mm long. 1.7 mrad beam divergence. 7 kV start voltage. 1kV operating voltage. 3.5 mA current.

**Circuitry includes**

Useful for special effects of flash lighting.

---

**Laser Power Supply**

Epoxy encapsulated power supply for up to 2 mW lasers.
4 1/2" X 1 1/2" X 1 7/16".
Input: 9 Vdc @ 1 amp
Output starting voltage: 7 to 8 kV
Operating voltage: 1.1 to 1.5 kV
Operating current: 4 to 5 mA
Recessed 0.250 quick connect terminals for output. Color coded wire leads for input.

**CAT# LT-1 $25.00 each**

---

**NEW LOW PRICE!! REDUCED ELECTRONIC FLASH UNITS**

ITT Magicflash. Originally designed for Polaroid One-Step and Pronto cameras. Nice bright flash can be triggered by external 3 Vdc pulse. Operates on 6 Vdc, 4 AA cells (not included).

Useful for special effects of flash lighting.

Circuitry includes a very desirable 600 uF 330V photoflash capacitor which is, by itself, worth the price of the unit.

**CAT# FSH-2 $3.00 each**

---

**150 Watt SWITCHING POWER SUPPLY**

TRW# 095-10001. Input: 115 Vac

Outputs:
- 5 Vdc @ 20 amp,
- 12 Vdc @ 4.2 amp,
- -12 Vdc @ 0.1 amp.

Fan cooled switching power supply with solid state relay turn-on protection. RF/RFI filter. On/off switch and reset button. Housed in vented metal cabinet.

Requires IEC type power cord

(our CAT# LCAC-C7 $3.00 each or similar).

UL and CSA listed. 9.5" X 7.25" X 3.45"

12" long wire leads terminate to 0.1" single row connector. Operation note: the solid state relay must be energized to operate supply.

This is accomplished by jumping the dark gray and red wires.

**CAT# PS-300 $27.00 each**

---

**TOUCH-TONE KEYPADS**

American Telecommunications Corp. Telephone keypad assembly with circuitry for producing touch-tones.
7 wire output.
Gray with white letters and numbers. 3" X 2.25" X 1.5".
Hook-up diagram available.

**CAT# TKP-1 $4.00 each**

---

**Electroluminescent BACKLIGHTS**

At last! A low cost electroluminescent glow strip and inverter. These brand-new units were designed to backlight small LCD TVs made by the Citizen Watch company. The inverter circuit changes 3 or 6 Vdc to approximately 100 Vac, the voltage required to light the glow strip. Luminescent surface area is 1.7" X 2.25". The strip is a salmon color in its off state, and glows white when energized. The circuit board is 2.2" X 1". Glow strip and circuitry can be removed easily from plastic housing. Ideal for special lighting effects and backlighting. Citizen # 92TA operades on 3-6 Vdc.

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<thead>
<tr>
<th>Model</th>
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<tr>
<td>DS-201</td>
<td>$25 each</td>
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<table>
<thead>
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<th>Description</th>
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<td>CC-LNK</td>
<td>DB25 females and DB9 females For serial use only</td>
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<td>DB25 females, DB9 males</td>
<td>6 ft $20 set</td>
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<table>
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<th>250W</th>
<th>800W</th>
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<tr>
<td>Price</td>
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<td>$199.</td>
<td>$499.</td>
<td>$849.</td>
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<th>Converter Type</th>
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<td>$37.50 each - 100 lot</td>
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- Variable DC Offset Control
- ± (1 Hz + 1 digit + Time Base Error)

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- ± (1 Hz + 1 digit)

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- 3-1/2 Digit LCD
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- ±5V, 2A

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- ± (0.5% + 2 digits)

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- 10 MHz Frequency Counter

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- Over Range Mark
- Protective Holster
- Tilt Stand

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$345.00
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- Logic CMOS/TTL
- Data Hold
- Diode
- Continuity Beep
- Case Included

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- Diode
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- Auto Polarity

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$24.00
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<th>5</th>
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*REFURBISHED AS NEW.

CONVERTERS

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<td>T P550 (550 MHz WPARENTAL)</td>
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<td>*Jerrold DR5-450</td>
<td>$59.00</td>
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<tr>
<td>*Sylvania TExscan 4040</td>
<td>$55.00</td>
<td>$45.00</td>
<td>$36.00</td>
<td>CALL</td>
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| Sylvania TExscan 4040-DIC  | $79.00  | $74.00 | CALL |
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<th>Used by:</th>
<th>SOVTEK®, RUSSIA</th>
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<td></td>
<td>12 at $4.75 each</td>
<td>25 at $4.25 each</td>
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</table>

## Sovtek, Russia

- **5U4G** $5.25 each
- **12AX7/WA/7025** 4.35
- **6922** (military 6DJ8) 6.75
- **EL84/6BQ5** 2.90
- **EL84M/6BQ5WA** 5.80
- **6V6GT** 4.25
- **6L6GC** 3.80
- **5881/6L6WGC** 7.25
- **811** 14.00
- **813** 19.00

### Sino, China

- **2A3** $13.50 each
  - 10 at $12.50 each
  - 25 at $11.50 each
- **6L6G** 4.50
- **12AX7** 3.85
- **12AT7** 3.90
- **12AU7** 4.10
- **6550** 10.00
- **KT88** 13.50

### El, Yugoslavia

- **EL34/6CA7** $5.50 each
  - 10 at $4.90 each
  - 25 at $4.50 each
- **6D8** 3.50
- **12AT7/ECC81** 3.50
- **12AU7/ECC82** 3.50
- **12AX7/ECC83** 3.15

### Siemens, Germany

- **EL34** $7.25 each
  - 10 at $6.75 each
  - 25 at $6.20 each
- **12AT7/ECC81** 3.90

### Tesla, Czechoslovakia

- **EL34BL (Cobalt Blue)** $8.25
  - 7.75
  - 5.90
  - 4.95
- **E83CC/12AX7a** 5.90

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- **5U4GB** $12.50 each
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- **6L6F** 19.25
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  - 10 at $18.25 each

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Built into tube socket. Direct plug-in replacement for all 5Y3, 5U4 and 5AR4 types.

### Odd Ball Tubes (Mostly USA Stock)

<table>
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<th>Type</th>
<th>Price</th>
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<td>3.90</td>
<td>OC3</td>
</tr>
</tbody>
</table>

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<table>
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<th>Item</th>
<th>Price 5</th>
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<td>NEW TVT-3 DIGITAL TRIBI ADD-ON</td>
<td>$51</td>
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<td>NEW SCIENTIFIC ATLANTA 8580-338</td>
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<tr>
<td>NEW SCIENTIFIC ATLANTA 8590</td>
<td>CALL</td>
<td>CALL</td>
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<tr>
<td>REFUR JERROLD STARCOM 6 (DPV5)</td>
<td>CALL</td>
<td>CALL</td>
</tr>
<tr>
<td>REFUR HAMLIN 6600 or 6000-3-M</td>
<td>$65</td>
<td>$55</td>
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<tr>
<td>REFUR HAMLIN MLD1200 Built-In Converter/Descrambler</td>
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<td>REFUR HAMLIN-MLD-1200-2</td>
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<tr>
<td>NEW JERROLD STAR 7 Add-on</td>
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<tr>
<th>Item</th>
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<tr>
<td>11-1155</td>
<td>IDS-10 $24.99</td>
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<td>11-1159</td>
<td>Programming Pad $9.95</td>
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<th>PRIMARY DIM. (X Y Z)</th>
<th>SECONDARY DIM. (X Y Z)</th>
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<td>4 x 8 x 8 x 12 x 12 x 2 x 4 x 16</td>
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<td>DS-12</td>
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<td>ET-20</td>
<td>4 x 4 x 8 x 8 x 8 x 12 x 12 x 2 x 4 x 16</td>
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<table>
<thead>
<tr>
<th>Model</th>
<th>Battery Test</th>
<th>Transistor HFE Battery Test</th>
<th>Transistor HFE Capacitance</th>
<th>AC/DC Current</th>
<th>Kelvin</th>
<th>100 Basic</th>
<th>150 Basic+</th>
<th>200 Advanced</th>
<th>PRO 400</th>
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<td>100 Basic</td>
<td>150 Basic+</td>
<td>200 Advanced</td>
<td>PRO 400</td>
</tr>
</tbody>
</table>

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<table>
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<th>Crystals</th>
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<td><strong>FUNDAMENTAL MODE CRYSTALS</strong></td>
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<td>1.001-30.0 MHZ</td>
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<td>HC6/U, HC17/U, HC33/U</td>
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<td><strong>SECOND MODE CRYSTALS</strong></td>
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<td>2.0-30.0 MHZ</td>
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<td>HC25/U, HC18/U MINIATURE</td>
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<td><strong>THIRD MODE CRYSTALS</strong></td>
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<td>18.75. MHZ</td>
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<td>110.5-150. MHZ</td>
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<td>Power Meter 10MHZ to 12.4GHZ</td>
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<td>CR 1482R Inductance Standard 5.0 H</td>
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<td>CR 1482T Inductance Standard 10.0 H</td>
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<td>CR 1650B RCL Bridge</td>
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<td>HP 323A Distortion Analyzer</td>
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<td>HP 324A Distortion Analyzer</td>
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<td>HP 3336B w/Opt. 1,5 Synthesizer Level Generator</td>
<td>$995.00</td>
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<td>HP 3586B w/Opt. 1,3,4 Selective Level Meter</td>
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<td>HP 4645856 Generator</td>
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<td>HP 8616A Signal Generator 1800 to 4500MHZ</td>
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<tr>
<td>Rockland 5100 Frequency Synthesizer Audio to 2MHZ</td>
<td>$300.00</td>
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<tr>
<td>Shalltronix 817C Decade Box 01 to 100 ohms (new)</td>
<td>$125.00</td>
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<tr>
<td>TEK 7D13 Digital Multimeter, 3-1/2 digit</td>
<td>$175.00</td>
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<tr>
<td>TEK 453 Scope 50MHZ</td>
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<td>TEK 453A Scope 50MHZ</td>
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<td>TEK 465 Scope 100MHZ</td>
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<td>TEK 475 Scope 200MHZ</td>
<td>$800.00</td>
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<tr>
<td>TEK 1480R NTSC Waveform Monitor</td>
<td>$1,500.00</td>
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<tr>
<td>TEK 2213 Dual Trace Scope 60MHZ</td>
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- Used for industrial and laboratory applications to control voltage, current, power, heat, speed, light and electromechanical forces.

**General Electric Volt-Pac Model #9T2A**

- INPUT VOLTAGE: 120 VAC
- OUTPUT VOLTAGE: 0 - 120
- CONSTANT CURRENT LOAD: 4 AMPS
- CONSTANT IMPEDANCE LOAD: 5.8 AMP
- CYCLE: 60 HZ
- SIZE: 4 3/8" DIA. X 4" HIGH
- WEIGHT 6 LB.

---

### POTTHER & BRUMFIELD RELAYS

**T90 series low cost, 30 amp. DC coil PC board relay.**

- P & B Relay-P/N T90N11D215-02
- 12 TO 15 VDC, SPST, NORMALLY OPEN
- HORIZONTAL MOUNT, OPEN FRAME, 430 OHM
- COIL RESISTANCE, CONTACT RATING 30 AMP @ 250 VAC BRAND NEW, P & B BOXED

**Each** $5.90; 10 for $50.00; 100 for $40.00.

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### Solid-State

**Opto-isolated solid state relay features synchronous zero crossover switching**

**HEINEMANN**

- HEINEMANN MODEL $241-10A-140
- BRAND NEW INDIVIDUALLY BOXED
- SIZE: 2"L X 1"W X 1/4"H
- INPUT = 3-32 VDC
- OUTPUT 140 VAC
- CONNECTIONS 1/4" MALE TAB

---

### EMI Suppression Filters

**EMI Suppression Filters**

- **muMetE ERIE suppression filters**
- **Model** $241-10A-140
- **Brand** NEW INDIVIDUALLY BOXED
- **Size** 2"L X 1"W X 1/4"H
- **Input** 3-32 VDC
- **Output** 140 VAC
- **Connections** 1/4" MALE TAB

---

### MALLORY TYPE CG5

**MALLORY TYPE CG5**

- MADE IN U.S.A.
- 2900 UF 200 VDC
- MAX SURGE 250 VDC POS & NEG 5 3/4" HIGH X 2" DIA
- 3200 PCS. IN STOCK

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### Electrolytic Capacitor

**Part # UBU1662MA**

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- SIZE: 2.5"L X 1.18" DIA.

**Radial Leads**

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300W MOSFET POWER AMPLIFIER (MONO)
AF-35
Power output: 300W into 4 ohms (0.1% THD), 150W into 8 ohms (0.2% THD)★
Frequency response: 10 Hz - 20 kHz★
Total Harmonic Distortion: Less than 0.05% ★
Input Sensitivity: 4 ohms ★
Load Impedance: 4 ohms ★
Power Requirements: 55-85V DC ★
Dimensions: 287 x 205 x 60 mm.

300W MOSFET POWER AMPLIFIER (MONO)
TA-477
Power output: 400W into 4 ohms (0.1% THD), 200W into 8 ohms (0.2% THD)★
Frequency response: 10 Hz - 20 kHz★
Total Harmonic Distortion: Less than 0.05% ★
Input Sensitivity: 4 ohms ★
Load Impedance: 4 ohms ★
Power Requirements: 55-85V DC ★
Dimensions: 287 x 205 x 60 mm.

100W = 100W NEW CLASS D STEREO PRE AND MAIN AMP
TA-1500 ★★
Power output: 100 watts per channel into 8 ohms ★
Total harmonic distortion: Less than 0.05% ★
Frequency response: 10 Hz - 20 kHz★
Input Sensitivity: 4 ohms ★
Load Impedance: 4 ohms ★
Power Requirements: 55-85V DC ★
Dimensions: 287 x 205 x 60 mm.

Mark V Model 1001 Transformer

Mark V Model 1002 Transformer

Mark V Model 2003 Transformer

Mark V Model 3003 Transformer

Mark V Model 4003 Transformer

Mark V Model 5003 Transformer

Mark V Model 6003 Transformer

Mark V Model 7003 Transformer

Mark V Model 8003 Transformer

Mark V Model 9003 Transformer

MARK V ELECTRONICS, INC. - 8019 E. Sluson Ave., Montebello, CA 90640

CIRCLE 292 ON FREE INFORMATION CARD

www.americanradiohistory.com
<table>
<thead>
<tr>
<th><strong>TEKTRONIX 7623A</strong></th>
<th><strong>TEKTRONIX 576</strong></th>
<th><strong>HEWLETT-PACKARD 141T</strong></th>
</tr>
</thead>
<tbody>
<tr>
<td>Storage Oscilloscope, 100 MHz BW. Comes with the following plug-ins 7A26, 7A26 and 7B53A.</td>
<td>Curve Tracer, tests two and three terminal discrete semiconductors. Power capability up to 220 W. Convenient scale factor readout. Accepts test fixtures.</td>
<td>Spectrum Analyzer mainframe with broadband RF Section, 01 to 18 GHz and high resolution IF section.</td>
</tr>
<tr>
<td><strong>$1075.00</strong></td>
<td><strong>$2650.00</strong></td>
<td><strong>$3200.00</strong></td>
</tr>
</tbody>
</table>

**HEWLETT-PACKARD SWEEP OSCILLATOR MAINFRAMES AND PLUG-INS.**

<table>
<thead>
<tr>
<th>Model</th>
<th>Description</th>
<th>Price</th>
</tr>
</thead>
<tbody>
<tr>
<td>8620A Mainframe</td>
<td>$600.00</td>
<td></td>
</tr>
<tr>
<td>8620C Mainframe</td>
<td>$850.00</td>
<td></td>
</tr>
<tr>
<td>8622A 10 MHz-2.4 GHz NEW</td>
<td>$2750.00</td>
<td></td>
</tr>
<tr>
<td>8622B 10 MHz-2.4 GHz</td>
<td>$2300.00</td>
<td></td>
</tr>
<tr>
<td>8623B 1.8-4.2 GHz</td>
<td>$1200.00</td>
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</tr>
<tr>
<td>86235A 1.7-4.3 GHz</td>
<td>$1150.00</td>
<td></td>
</tr>
<tr>
<td>86240A 2-8.4 GHz</td>
<td>$1350.00</td>
<td></td>
</tr>
<tr>
<td>86260A 12.4-18.0 GHz</td>
<td>$1100.00</td>
<td></td>
</tr>
<tr>
<td>86290A 2-18.0 GHz</td>
<td>$2650.00</td>
<td></td>
</tr>
<tr>
<td>86290B 2-18.6 GHz</td>
<td>$3250.00</td>
<td></td>
</tr>
</tbody>
</table>

**TEKTRONIX 485**

350 MHz Portable Oscilloscope, dual trace, 1 nS/div sweep rate, 2.0 div nS writing speed, switchable input impedance.

**$1300.00**

**TEKTRONIX 7904**

500 MHz Oscilloscope mainframe with the following plug-ins. 7A24 dual trace amplifier, 7A26 dual trace amplifier, 7B85 delaying time base, 7B80 delaying time base. Includes a manual for each plug-in.

**$2000.00**

**WANDEL & GOLTERMANN TSA-1**

Frequency Range 100 Hz to 180 MHz 5 modes of measurement. Spectrum analysis, network analysis, phase jitter, selective level, demodulation. New cost $40. K.

**$2750.00**

Same as above but includes network analyzer

**$3550.00**

**HEWLETT-PACKARD 5763**

100 MHz Oscilloscope Mainframe CRT readout, has the following plug-in, 7A18, 7A18 and 7B53A. Includes all manuals.

**$975.00**

**HEWLETT-PACKARD 7603**

10 MHz to 22 GHz range with internal mixing, internal preselection 1.7 to 22 GHz, wide choice of resolution bandwidths, simple three knob operation.

**$7750.00**

**HEWLETT-PACKARD 8553A/8555B SPECTRUM ANALYZER**

Spectrum Analyzer plug-in, 100 MHz, 1 kHz resolution, -117 dBm dynamic range. Comes in a 853A Spectrum Analyzer Display.

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**HEWLETT-PACKARD 3586B**

Selective Level Meter makes carrier measurements to 32.5 MHz, voice channel measurements from 50 Hz to 100 kHz, works with the 3336B level generator. Options available.

**SPECIAL $2000.00**

**HEWLETT-PACKARD 8565A**

10 MHz to 22 GHz range with internal mixing, internal preselection 1.7 to 22 GHz, wide choice of resolution bandwidths, simple three knob operation.

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**WE ACCEPT VISA AND MASTERCARD**
TEST EQUIPMENT AT DISCOUNT PRICES

DIGITAL METERS

<table>
<thead>
<tr>
<th>Equipment Type</th>
<th>Model</th>
<th>Price</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Digital Multimeter</td>
<td>CM-1550B</td>
<td>$58.95</td>
<td>9 Ranges, .1%-20,000 ohm, 5% basic accuracy, Zero control w/ Case, Big 1&quot; Display by Elenco</td>
</tr>
<tr>
<td>Digital Capacitance Meter</td>
<td>B+K Model 878</td>
<td>$239.95</td>
<td>Auto / Manual Range, Many Features with Q Factor, High Accuracy</td>
</tr>
</tbody>
</table>

QUALITY AMERICAN MADE POWER SUPPLIES

<table>
<thead>
<tr>
<th>Power Supply</th>
<th>Model</th>
<th>Price</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Digital Triple Power Supply</td>
<td>XP-765</td>
<td>$289</td>
<td>0-20V @ 1A, 0-20V @ 1A, 0-120V, 0-15V, 0-25V, 0-5V @ 5A</td>
</tr>
<tr>
<td>Quad Power Supply</td>
<td>XP-580</td>
<td>$169.95</td>
<td>0-20V @ 1A, 12V @ 1A, 5V @ 5A, Fully regulated and short circuit protected</td>
</tr>
<tr>
<td>Triple Power Supply</td>
<td>XP-620</td>
<td>Assembled $75, Kit $49.95</td>
<td>2 to 15V @ 1A, 2 to 12V @ 1A (or 4 to 30V @ 1A) and 5V @ 3A</td>
</tr>
</tbody>
</table>

GENERATORS & VIDEO PRODUCTS

<table>
<thead>
<tr>
<th>Generator Type</th>
<th>Model</th>
<th>Price</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Function Generator</td>
<td>Blox #660</td>
<td>$28.95</td>
<td>Provides sine, triangle, square wave from 1Hz to 1MHz, AM or FM capability</td>
</tr>
<tr>
<td>Color Convergence Generator</td>
<td>SG-250</td>
<td>$89.95</td>
<td>Kit $69.95, Finest in the industry, 10 color steady patterns RF &amp; Video output</td>
</tr>
<tr>
<td>Wide Band Signal Generators</td>
<td>SG-9000</td>
<td>$129</td>
<td>100K-450MHz AM Modulation of 1KHz Variable RF output</td>
</tr>
<tr>
<td>Digital Multimeter Kit with Training Course</td>
<td>Elenco Model M-266SK</td>
<td>$49.95</td>
<td>Fun &amp; Easy to Build, Ideal School Project</td>
</tr>
<tr>
<td>Multi-Function Counter</td>
<td>Elenco F-1200</td>
<td>$259</td>
<td>Measures Frequency, Period, Totalizer, 8 LED digits, Crystal Oven Oscillator, 5ppm Accuracy</td>
</tr>
</tbody>
</table>

EDUCATIONAL KITS - FUN & EASY TO BUILD

<table>
<thead>
<tr>
<th>Kit Type</th>
<th>Model</th>
<th>Price</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>Robotic Arm Kit</td>
<td>Model Y-01</td>
<td>$48.95</td>
<td>Teaches basics of robotics, Arm grabs &amp; releases, lifts &amp; lowers, &amp; 100mm, 1kHz, 1mA, 12V</td>
</tr>
<tr>
<td>AM/FM Transistor Radio Kit</td>
<td>Model AM-FM 108</td>
<td>$27.95</td>
<td>14 Transistors, 5 Diodes, Easy to build because schematic is printed right on the PCB, Makes a great school project, Model AM 550 AM Only $17.95</td>
</tr>
<tr>
<td>XK-500 Digital / Analog Trainer</td>
<td>$159.95 Assembled, $129.95 Kit</td>
<td>A complete mini-lab for building, testing, prototyping analog and digital circuits</td>
<td></td>
</tr>
</tbody>
</table>

POWER SUPPLIES

- Variable Power Supply: +1.25 to 20VDC @ 5 Amp, +1.25 to 15VDC @ 1 Amp, -1.25 to 20VDC @ 5 Amp, -1.25 to 15VDC @ 1 Amp, +20VDC @ 1 Amp, -20VDC @ 1 Amp, +5VDC @ 1 Amp, -5VDC @ 1 Amp, 30VAC Center tapped @ 15VAC @ 1 Amp

ANALOG - SECTION

- Function Generator Sine, Triangle, Square wave forms
- Frequency adjustable in five ranges from 1 to 100kHz
- Fine frequency adjust
- Amplitude adjust
- DC offset
- Modulation FM AM

DIGITAL - SECTION

- Eight data switches
- Two NO bounce logic switches
- 8 LED readouts, TTL buffered
- Clock frequency 1 to 100kHz
- Turns amplify 5VPP square wave

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ELENCO S-1325

25MHz 2 Channel $349
S-1340 40MHz Dual Trace Oscilloscope

$495
S-1360 60MHz Dual Trace - Delayed Sweep

$775
DS-203 20MHz, 10MS/s Digital Storage Oscilloscope

$775

20MHz $395 Model 2125 $539.95
2 Channel Delayed Sweep

40MHz DUAL-TRACE
Model 1541B

749.95
- 1mV/div sensitivity
- Video sync separators
- Z axis input
- Single sweep
- V mode-display two signals unrelated in frequency

60MHz DUAL-TRACE
Model 2160

949.95
- 1mV/div sensitivity
- Sweep to 5 ns/div
- Dual time base
- Signal delay line
- V mode-display two signals unrelated in frequency
- Component tester

100MHz THREE-TRACE
Model 2190

1,395.95
- 1mV/division sensitivity
- Sweeps to 2ns/division
- Dual time base
- Calibrated delay time multiplier
- Signal delay line
- 19kV accelerating voltage

20MHz ANALOG
WITH DIGITAL STORAGE
Model 2522

869.95
- 20MHz analog bandwidth
- 10MS/s sampling rate
- 2k memory per channel
- 20MHz equivalent time sampling
- Pre-trigger capture

1.0GHz PORTABLE
SPECTRUM ANALYZER
Model 2610

2,595.95
- 32 channels (VC-3120) or 48 channels (VC-3130)
- 25MHz synchronous operation on all channels
- 100MHz asynchronous operation (8 or 12 channels)
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V-522 - 50MHz, Delayed Sweep $949
V-222 - 20MHz, DC Offset $849
V-422 - 40MHz, DC Offset $749
V-222 - 20MHz, DC Offset $625

Hitachi Compact Series Scopes

V-660 - 60MHz, Dual Trace $1,095
V-665A - 60MHz, Dual Trace $1,325
V-1060 - 100MHz, Dual Trace $1,375
V-1065A - 100MHz, Dual Trace $1,649
V-1085 - 100MHz, Dual Trace $1,995
V-1100A - 100MHz, Quad Trace $2,195
V-1150 - 150MHz, Quad Trace $2,695

Hitachi RSO Series

RSO's feature, roll mode, averaging, save memory, smoothing, interpolation, pretriggering, cursor measurements.

VC-6023 - 20MHz, 20MS/s $1,650
VC-6024 - 50MHz, 20MS/s $1,950
VC-6025A - 50MHz, 20MS/s $2,350
VC-6045A - 100MHz, 40MS/s Call
VC-5145 - 100MHz, 100MS/s Call

Logic Analysers

385

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Connects to standard PC parallel printer port

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  27C010A, 23 seconds
  28C020, 34 seconds
  27C040, 95 seconds
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- Flash 28F020, (29C256—29C010 (EMP-20 only))
- Micros 8741A, 42A, 42AH, 48, 49, 48H, 49H, 55, 87C51, 87C51FX, 87C751, 87C751, 752
- GAL, PLD from NS, Lattice, AMD-16V8, 20V8, 22V10 (EMP-20 only)

EMP-20

PB-10 Internal Card for PC

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40 PIN ZIF

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BBS (916) 972-8042
FAX (916) 972-9960

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BP7 12v 600 mah $59.00
SA/SAT
BP62/BP3
BP63A 7.2v 750 mah $59.00
BP64 7.2v 1000 mah $59.00
BP65A 9.6v 600 mah $59.00
BP65B 12v 600 mah $59.00

KENWOOD
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KNB4 7.2v 2200 mah $59.00
PK6 7.2v 750 mah $46.00
PB7 7.2v 1500 mah $55.00
PB8 12v 750 mah $55.00

MOTOROLA
HT300 7.2v 1600 mah $45.00
HT90 12v 600 mah $34.00
HT440 12v 600 mah $39.00
MT500 15v 500 mah $59.00

RADIUS
P-10 500 mah $28.00
SABER
7.2v 1100 mah $59.00

ICOM-SA/SAT

SPECIALS
ICOM-72A CHARGER WITH
BP-84 (Equiv)—3" High
7.2v @ 1000 MAH $135.00
or
BP-85B (Equiv.) 3" High
12v 600 MAH $164.00

INSERTS KENWOOD
PB-21 $13.00, PB-25, 26—$20.00

ICOM
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$45.00

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MOTOROLA
$55.00

"FLIP"
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**speakers**

- **5" Full Range Speaker**
  Good quality 5" speaker with 6 oz magnet and 8 ohm voice coil. Rated 8 watts RMS (12 watt peak). Great for compact applications.
  - G3209 $4.95

- **4"x 6" Coaxial**
  Great for many types of auto or home applications. Features built-in tweeter, dust cover and 8 ohm 15 watt peak rating.
  - G3213 $8.00

- **6"x 8" Universal Auto Speaker**
  Great for replacement or new construction. This speaker is rated 8 watts, 6 oz magnet and 4 ohm impedance. Standard mounting for many FORD cars. Has built in dust screen.
  - G3210 $4.75

- **6"x 9" Universal Auto Speaker**
  Universal auto sound speaker features 6 oz ceramic magnet, 8 watt 4 ohm voice coil and built in dust screen.
  - G3211 $5.95

**SUPER WOOFERS**

- **5" Super Subwoofers**
  (Pincusion Mount) Heavy duty in a very compact size! Features 1 1/4 aluminum voice coil, massive 20 oz ceramic magnet, 4 ohm impedance, 50 watt RMS (75 watt peak) power. Response to 400 Hz vented backplate, air suspension edge and dust screen.
  - G3212 $21.95

**POWER WOOFERS**

**Guitar, Stereo and Auto Applications**

<table>
<thead>
<tr>
<th>SIZE</th>
<th>RATING</th>
<th>VOICE MAGNET STOCK/PRICE</th>
</tr>
</thead>
<tbody>
<tr>
<td>12&quot;</td>
<td>100W</td>
<td>2&quot; 4Ω 30 oz G3217 $35.00</td>
</tr>
<tr>
<td>15&quot;</td>
<td>150W</td>
<td>2 1/2&quot; 8Ω 54 oz G3218 $49.00</td>
</tr>
<tr>
<td>&quot;15&quot;</td>
<td>200W</td>
<td>3 1/2&quot; 8Ω 95 oz G3219 $100.00</td>
</tr>
</tbody>
</table>

**2 Way 75 Watt Peak Speaker**

**System Components**

Consists of a 10"/16 ounce magnet, cloth roll, air suspension, 8 ohm woofer, a 3"/square tweeter and a press fit quick connect terminal with 75 watt crossover. These were made by Pioneer for a custom manufacturer. You make your own enclosure and save a bundle. All 3 components for one low price!

- G3208 $29.95

**MISC. SMALL SPEAKERS**

<table>
<thead>
<tr>
<th>SIZE</th>
<th>IMP</th>
<th>WATT</th>
<th>STOCK</th>
<th>PRICE</th>
</tr>
</thead>
<tbody>
<tr>
<td>1 3/4</td>
<td>32Ω</td>
<td>.15</td>
<td>G3214</td>
<td>$1.00</td>
</tr>
<tr>
<td>2 1/4</td>
<td>32Ω</td>
<td>.25</td>
<td>G3215</td>
<td>$1.60</td>
</tr>
<tr>
<td>2 1/2</td>
<td>8Ω</td>
<td>2</td>
<td>G3289</td>
<td>$1.29</td>
</tr>
<tr>
<td>2 5/8</td>
<td>4Ω</td>
<td>3</td>
<td>G3285</td>
<td>$1.50</td>
</tr>
<tr>
<td>3&quot;</td>
<td>16Ω</td>
<td>.5</td>
<td>G3216</td>
<td>$1.75</td>
</tr>
<tr>
<td>4&quot;</td>
<td>8Ω</td>
<td>6</td>
<td>G3208</td>
<td>$3.95</td>
</tr>
</tbody>
</table>

**COMBO TV/VCR REMOTE**

Hand held remote made by zenith. We just got these in and have no other info except that they have a few scratches on the case.

- G2555 $1.00

**COPPER CLAD BLOWOUT**

Great for making high quality PC boards. These are standard glass epoxy double sided copper clad blanks. Size is an incredible 12"x12". Each panel is large enough to make many smaller PC boards. A SUPER VALUE.

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**BRIGHT ORANGE LED**

Jumbo T1 3/4 diffused lens, orange LED.

- G2554 10/$1.00
  - 100/$9.00
  - 1000/$70

**STROBE TUBE & SCHEMATIC**

Bright xenon tube for making strobe lights. Size: 1.5".

- G936 $1.39

**SPECIALS**

**20W + 20W Stereo Amp Kit**

Two separate high power amps on one PC board put out an incredible 20 watts RMS each. Features low distortion circuitry. Great stereo booster amp for your car sound system. Use with any speakers capable of handling at least 20 watts. Operates on 12VDC. Size of board: 6"x2.25".

- C6442 $19.95

**20 Watt RMS Mono Amp Kit**

High power amp for various booster applications. Kit features short and open circuit protection and very low distortion (1% or less). Has red LED "on" indicator and will boost any tuner, radio, cassette or CD player to room filling volume! Operates from 12VDC. Size of board: 3.75"x2.1". Complete with parts, PC board and instructions.

**SKILL LEVEL 2**

- C6444 $14.95

**10W + 10W Stereo Amp Kit**

Similar to the 20W+20W stereo amp only this one puts out 10 Watts RMS to each channel. Features one level control that sets level in both channels and red LED "on" indicator. Use this amp with your speakers to boost portable tape players, radios or CD players to room filling volume. Operates from 12VDC. Size of board: 3.75"x2.25". Complete with all parts, PC board and instructions.

**SKILL LEVEL 2**

- C6443 $16.95

March 1983. Electronics Now

CIRCLE 241 ON FREE INFORMATION CARD
**EQUIPMENT SPECIALS**

**TEKTRONIX MAINFRAME MADNESS STRIKES AGAIN!**

<table>
<thead>
<tr>
<th>MODEL</th>
<th>DESCRIPTION</th>
<th>REGULAR</th>
<th>SALE</th>
</tr>
</thead>
<tbody>
<tr>
<td>VC-6023</td>
<td>2 Ch, 20 MHz, 20 MS/s, 2KV/ch.</td>
<td>1895.00</td>
<td>CALL</td>
</tr>
<tr>
<td>VC-6024</td>
<td>2 Ch, 50 MHz, 20 MS/s, 2KV/ch.</td>
<td>2195.00</td>
<td>FOR</td>
</tr>
<tr>
<td>VC-6025A</td>
<td>2 Ch, 50 MHz, 20 MS/s, 50 MHz repetitive sampling, 2 KV/ch, frequency counter, RS-232 w/HPGL support</td>
<td>2695.00</td>
<td>QUOTES!</td>
</tr>
<tr>
<td>VC-6045A</td>
<td>2 Ch, 100 MHz, 40 MS/s, 100 MHz equivalent sampling, 4X Mem, frequency counter, RS-232 w/HPGL support</td>
<td>3295.00</td>
<td>FOR</td>
</tr>
<tr>
<td>VC-6145</td>
<td>4 Ch, 100 MHz, 100 MS/s (1 ch), 4X Mem, frequency counter, RS-232 w/HPGL support</td>
<td>4395.00</td>
<td>PRICE</td>
</tr>
<tr>
<td>VC-6155</td>
<td>2 Ch, 100 MHz, 100 MS/s (2 ch), 4X Mem, frequency counter, RS-232 w/HPGL support</td>
<td>3995.00</td>
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**PORTABLE PACKAGE DEALS**

<table>
<thead>
<tr>
<th>MODEL</th>
<th>DESCRIPTION</th>
<th>PRICE</th>
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</thead>
<tbody>
<tr>
<td>TEK 465</td>
<td>100MHz, Dual Trace, Delayed Sweep, Probe and Manual</td>
<td>$495</td>
</tr>
<tr>
<td>TEK 465B</td>
<td>100MHz, Dual Trace, Delayed Sweep, Probe and Manual</td>
<td>$575</td>
</tr>
<tr>
<td>TEK 475</td>
<td>200MHz, Dual Trace, Delayed Sweep, Probe and Manual</td>
<td>$725</td>
</tr>
<tr>
<td>TEK 485</td>
<td>350MHz, Dual Trace, Delayed Sweep, Probe and Manual</td>
<td>$995</td>
</tr>
<tr>
<td>TEK 466/DM44</td>
<td>100MHz Storage, D/T, D/S, Probe and Manual</td>
<td>$995</td>
</tr>
</tbody>
</table>

**LAB POWER SUPPLIES**

| TEST LEADS from E.F. JOHNSON (NEW) | $35 |
| BNC to RED & BLACK MINI HOOKS, 36' length | $3ea or 4 for $10 |
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Most homes and offices have hot spots with strong artificial electro-magnetic fields, where chronic exposure may cause mental or physical problems. Even the EPA names these fields as suspected carcinogens. You can reduce your risk by avoiding these high-field areas.

The TriField™ meter detects far more of these fields than any other electromagnetic pollution meter. It's the only one that independently reads AC electric fields, AC magnetic fields, and radio/microwave fields. It also reads field strengths in all directions simultaneously. Every other meter that sells for under $150 reads only magnetic and only in one direction - they can entirely miss a magnetic field unless pointed correctly and are blind to radio/microwaves and electric fields, both of which cause biological effects.

The TriField™ meter reads all three types of fields numerically and with a SAFE/BORDERLINE/HIGH SCALE, weighted proportional to effect on the body. Thresholds are based on epidemiological and laboratory studies. (While no absolute hazard thresholds have been established, reduction of relative exposure is prudent.)

The TriField™ meter comes ready-to-use with battery, instructions, and one-year limited warranty. The cost is $144. postpaid.

AlphaLab / 1272 E. Alameda Avenue / SLC, UT 84102
For literature and information, call (503) 621-9701

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AUTOMATIC TELLER MACHINES are a goldmine for thieves, numerous security precautions and countermeasures have been exposed. 100+ methods detailed, includes Physical, Holog, E, Cipher, PIN compromise, card countermeasures, money withdrawal, iflop, fraud, etc. Includes comprehensive security precautions. AMTs contain up to $250,000 in cash! Recent $550,000 ATM crime reveals many methods, challenges, and their many variations. Protect yourself $29.

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Cons & scams fleece American of $100's billion- plus! The most committed, naive and easy mark - naive and easy mark - naive and easy mark - naive and easy mark - naive and easy mark. Written in plain English, on cons & scams of all kinds - from the classic to the high-tech. Simple to read, explains many variations. Protect yourself $29.

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<table>
<thead>
<tr>
<th><strong>MAGNETIC PROBE SENSES MAGNETIC FIELDS</strong></th>
</tr>
</thead>
<tbody>
<tr>
<td>This safe non-contact probe allows you to trouble-shoot AC and DC solenoid-operated devices, relays or any device using a coil. Also detects transient pulses as fast as 10μS and identifies north and south poles. Place the probe close to the coil and if the LED is on the device is energized. Probe operating frequency is DC-400Hz.</td>
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<thead>
<tr>
<th><strong>HANDHELD 1.25GHz FREQUENCY COUNTER</strong></th>
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<tbody>
<tr>
<td>Microprocessor-based counter measures frequency from 10 Hz to 1.25GHz and period from 0.1μS to 100μS. Includes data hold, min/max/average readings and relative frequency measurements. Complete with 4 AA batteries, manual and 1-year warranty.</td>
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<tr>
<th><strong>ESD FIELD SERVICE KIT</strong></th>
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<tbody>
<tr>
<td>Kit includes a blue static-dissipative vinyl work surface (18&quot;x22&quot;x0.30&quot;) with two female snap fasteners, a common-point grounding cord (15'), one adjustable wrist strap with a 1 megohm resistor, a 6&quot; cord and a 7&quot;x13&quot; storage case.</td>
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<tr>
<th><strong>PROGRAMMABLE DIGITAL TIMER</strong></th>
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<tbody>
<tr>
<td>Provides up to 6 on and 6 off settings per week with a minimum switch time as low as 1 minute. Plugs into 3-prong 110VAC outlet and has battery backup (AAA battery incl) to prevent programs from being cleared during power failure. Rated at 15amps. UL listed.</td>
</tr>
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<tr>
<th><strong>X1, X10 SWITCHABLE OSCILLOSCOPE PROBE</strong></th>
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<tr>
<td>Monolithic probe features a 100 MHz bandwidth, a 3.5ns risetime, a 3.5μs timebase, and a wide compensation range (10μF to 60pF). Complete with spring hook, BNC adapter, IC and insulating tip and trimming tool. Cable length is 1.5 meters.</td>
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<tr>
<th><strong>AUDIBLE CONTINUITY TESTER</strong></th>
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<tr>
<td>Tester gives a clear audible sound on point-to-point continuity and is suitable for Go/No-Go test for wires, cables, LEDs, switches, diodes, transistors, etc. Complete with test probes and detachable alligator clips. Operates on 9V battery (not incl.).</td>
</tr>
</tbody>
</table>

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Offer Expires April 30, 1993
Beckman Industrial

**4 DIGIT TRUE RMS DMM**

- 41 segment analog bargraph
- 3-year warranty

Full-function, auto-ranging DMM with 4 digit, 10,000 count resolution measures DC voltage and current, resistance and true RMS AC voltage and current. It features a contiunity beeper, diode test, an Auto Min-Max mode, a relative mode and a probe hold mode. Comes complete with manual, test leads, battery(9V), and protective holster.

**Reg.$149.00**  
**Model ZRMS225**

**$299.00**  
**Reg.$365.00**  
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**THE PROFESSIONAL’S TOOL CASE**

- Case top has built-in document holder
- Case bottom is partitioned into 3 areas
- Two removable pallets hold over 60 tools

A handsome black case to organize and transport your valuable tools and instruments. This is the same quality case used by thousands of professional field engineers. Case is made of high impact polypropylene, and has snap-action key locks and a padded handle.

*Size: 17 1/2" x 12 1/2" x 5"*

**117-PC. PROFESSIONAL FIELD SERVICE KIT**

The complete kit comes with the tool case described above and a complete selection of tools, including Diamond, Xcellte and Weller. The kit includes screwdrivers, pliers, tweezers, cutters, wrenches, alignment tools, hex driver blades and a crimping tool, wire stripper, soldering iron & supplies, socket set, penlight, inspection mirror, hammer and more.

*Lifetime Guarantee: Any tool that fails under normal use will be replaced free of charge.*

**$99.00**  
**Reg.$128.95**  
**Model RWTCPS**

**SERVICE VACUUM CLEANER**

Features a powerful 2.2 peak HP motor, easy change double-layer filter bag, shoulder strap and built in handle. Toner-safe. Complete with 6" Tuflex hose, dusting brush, crevice tool and brush, tube adapter, snorkel tube and small dusting brush. 12"x11"x5". 8 lbs.

**$49.00**  
**Reg.$58.90**

**Model ZP1KB**

**DIGITAL THERMOMETER**

Measures 0° to 159°F, has a hi-lo limit setting, an accuracy of ±1° and a built-in clock function. ABS covered probe is suitable for air/immersion applica-tions. 1.5V battery incl. 4oz.

**$49.95**

**Model Z7201F**

**$59.95**

**Reg.$80.00**  
**Model RIM5 Tool Case**

**$299.00**  
**Reg.$365.00**  
**Model R22-IM5 117 Pc. Tool Kit**

**Beckman Industrial**

**$159.00**

**Model ZRMS225**

**$129.00**

**Model R38091F**

**$109.00**  
**Reg.$139.00**  
**Model R38091**

**DCA/ACA CLAMP METER**

Functions as 3 1/2 Digit DMM

Transformer jaws measure up to 400A AC/DC and a peak-held function provides recall of AC or DC current surges. As a DMM it measures AC voltage, DC voltage, AC/DC current and resistance. The meter has the following ranges: ACV: 750V; DCV: 200mV, 200V; DCA/ACA: 200A, 400A; Resistance: 2000 ohms. Resolution down to 0.1mV, 0.1A and 1ohm. Comes complete with test leads, battery, carrying case and 1-year warranty. Model R38091F also has a built-in temperature function, 0-1400°F.

**$149.00**  
**Reg.$183.26**  
**Model ZC2093**

**SERVICE VACUUM CLEANER**

Features a powerful 2.2 peak HP motor, easy change double-layer filter bag, shoulder strap and built in handle. Toner-safe. Complete with 6" Tuflex hose, dusting brush, crevice tool and brush, tube adapter, snorkel tube and small dusting brush. 12"x11"x5". 8 lbs.

**$49.00**  
**Reg.$58.90**

**Model ZP1KB**

**DIGITAL THERMOMETER**

Measures 0° to 159°F, has a hi-lo limit setting, an accuracy of ±1° and a built-in clock function. ABS covered probe is suitable for air/immersion applica-tions. 1.5V battery incl. 4oz.

**$49.95**

**Model Z7201F**

**$99.00**

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15,000 MFD 75 VDC Small size, mfg. by Cornell Dubilier. 2 In. Diam. X 4 1/4 In. Tall Part # DCM 153U075BCB Perfect for audio amps or regulated power supplies. 1990 Date Code. $4.95 ea. or 10 for $35

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#1 100 MFD / 450 VDC #2 330 MFD / 250 VDC
40 mm X 24 mm. 85° C. $1.29 $1.95
45 mm X 30 mm. 85° C. RADIAL LEADS

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SIEMENS SMART LED DISPLAY

#DLO-7135. 5x7 Red. With built in logic! Requires only a chip select and an ASCII input. Operates on 5 VDC. 1 Inch tall. w/Data. Data. New Units ! Displays entre 128 char. set! PRICE CUT! $2.95 ea.

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INSTRUCTION MANUAL

HOW TO:

* Clean Video Heads pg 3
* Check tape end sensors pg 5
* Renew drive wheels pg 4
* Adjust loading posts pg 7
* Renew pinch roller pg 6
* Clean erase & autio heads pg 7
* Check Spindle sensors pg 9
* Adjust tape guides pg 8
* Adjust Tracking head pg 9
* USE IN "G" CHASSIS
* PLUS MANY TIME SAVING TIPS

CIRCLE 299 ON FREE INFORMATION CARD

NOTICE !!

THE ORIGINAL VHS VU-THRU TOOL WILL WORK IN ALL VCR'S, NEW UNITS OR OLDER UNITS-FRONT LOAD,-TOP LOAD,-SIDE LOAD, AND CAMCORDER, INCLUDING THE DISCONTINUED "G" CHASSIS VCR'S.

(see page 9 of our up-dated ILLUSTRATED & COPYRIGHTED instruction manual)

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The Original Pocket Sized Counter, 1MHz to 2.4GHz – 8 digit LED. Maximized Sensitivity, ±1ppm TCXO. Includes Hold Switch, NiCads and Charger/Adapter! $99.

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CC12 - Padded Black Vinyl carrying case for 2300 size LED Counters .................. $12
CC30 - Padded Black Vinyl carrying case for 3000 size LCD counters. .................. $15

Antennas
TA100S Telescoping Whip Antenna ....... $12
Antenna Packs:
Ant-Pak 1 (includes RD77, RD600, TA100S – Save $11) .................. $65
Ant-Pak 2 (includes five assorted rubber ducks, 27-1000MHz – Save $32) .................. $99

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P30 - Counter/Oscilloscope probe - for direct coupling to signal sources or circuit test points. 1X/10X, switchable ............... $35
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Just in -- industrial torque wrenches by Mountz! These brand new items are calibrated from 20 to 200 kgf.cm and feature "click" action torque control. Snap-fit heads include useful 3/8" ratchet, 11/16", 30 mm and 13 mm open ends, and 17mm box. HSC 13655 Set only $19.95

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<tr>
<td>16 x 1</td>
<td>3 for $25.00</td>
<td></td>
</tr>
<tr>
<td>20 x 2</td>
<td>12.00</td>
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<tr>
<td>32 x 4</td>
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<tr>
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<tr>
<td>1.2 Mb</td>
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By Staff Writer

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Actual Output from HP LaserJet IIP at 150dpi

<table>
<thead>
<tr>
<th>MODEL #</th>
<th>CS100-40*</th>
<th>CS60-25</th>
<th>CS40-25</th>
<th>CS20-25</th>
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<tr>
<td>PRICE</td>
<td>$795</td>
<td>$695</td>
<td>$595</td>
<td>$495</td>
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<tr>
<td>BANDWIDTH</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Repetitive (-3dB)</td>
<td>100 MHz</td>
<td>60 MHz</td>
<td>40 MHz</td>
<td>20 MHz</td>
</tr>
<tr>
<td>Single-Shot (Sample Rate)</td>
<td>10 MHz</td>
<td>6.2 MHz</td>
<td>6.2 MHz</td>
<td>6.2 MHz</td>
</tr>
<tr>
<td>MAXIMUM DIGITIZING RATE (Two-Channel Simultaneous)</td>
<td>40 Ms/sec</td>
<td>25 Ms/sec</td>
<td>25Ms/sec</td>
<td>25 Ms/sec</td>
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<tr>
<td>NUMBER OF CHANNELS</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>TIME BASE RANGE **</td>
<td>20ns-2 sec/div</td>
<td>50ns-2 sec/div</td>
<td>50ns-2 sec/div</td>
<td>50ns-2 sec/div</td>
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<tr>
<td>MAXIMUM TIME RESOLUTION</td>
<td>250 ps</td>
<td>400 ps</td>
<td>400 ps</td>
<td>1 ns</td>
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<tr>
<td>VERTICAL RESOLUTION</td>
<td>+/- 0.4% (8-Bit A/D)</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>MEMORY (Standard)***</td>
<td>8K words</td>
<td>8K words</td>
<td>8K words</td>
<td>8K words</td>
</tr>
</tbody>
</table>

* = Available 4th Qtr 92
** = Screen display can zoom up to 10X
*** = 32K option available

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electrons has accumulated, the P-type substrate material is converted into an N-channel, and drain-to-source conduction occurs. The magnitude of the drain current depends on the channel resistance, but it is controlled by the gate voltage.

The schematic symbol for an N-type enhancement-mode MOSFET is shown in Fig. 9-b. In this symbol, the gate does not make direct contact with the channel. The arrowhead points from the P-type substrate toward the (induced) N-type channel, shown as a line broken into three sections to indicate an intermittent channel.

Current flow in the channels of both kinds of enhancement-mode MOSFET's is proportional to the voltage on their gates, $V_{GS}$. This can be seen for an N-type enhancement-mode MOSFET by examining the family of gate voltage ($V_{GS}$) curves in Fig. 10. Current drain, $I_D$, is directly proportional to the positive value of gate voltage.

A P-channel enhancement-mode MOSFET is made the same way as the N-channel enhancement device except that P-type drain and source regions are diffused into an N-type substrate. The symbol for a P-type enhancement-mode MOSFET is the same as the one shown in Fig. 9-b except that the direction of the arrow is reversed. In the case of a P-type enhancement-mode MOSFET, the drain current is directly proportional to the negative values of its grid voltage.

The high gate impedance of all MOSFET's makes them susceptible to damage from even
low-energy electrostatic discharge (ESD). For this reason many discrete MOSFETs and ICs based on MOSFETs are protected with on-chip Zener diode circuits.

**CMOS logic devices**

An enhancement-mode MOSFET can act as a switch when it is turned on or off by a voltage applied to the gate electrode. N-channel MOSFETs are switched with positive gate voltage, and P-channel MOSFETs are switched with negative gate voltage. These are known as complementary responses, and they form the basis for complementary MOS or CMOS digital logic families.

Figure 11-1 is a section view of a complementary pair of MOSFETs on a common substrate, the basic topography for all CMOS gates. The common substrate that is used for this pair is an N-doped silicon wafer. To make an N-channel MOSFET on an N-doped substrate, it is necessary to diffuse or implant a P-doped well in the substrate. The smaller N-type wells can then be formed in this P-doped region.

Because the substrate is N-doped, fewer steps are required to form the P-channel FET. The P- and N-doped guard bands isolate and insulate the individual transistors in this integrated circuit to prevent mutual interference. (Although not illustrated here, these guard bands are actually N- or P-doped rings formed around the complete FET below the oxide layer in this CMOS technology.

The two transistors in the section view, Fig. 11-a, can be connected to form a CMOS logic inverter, the simplest of digital logic circuits. This is accomplished by connecting the gates together to form an input (V_in) terminal, and taking the output (V_out) from the common drain. The source on the left side of the diagram, V_sss, is grounded, while the source on the right side is connected to the positive supply, V_DD.

Those connections are shown schematically in Fig. 11-b. How does the inverter work? Consider the P-channel device to be the driver and the N-channel device to be the load. Recall that an N-channel enhancement-mode MOSFET conducts with a positive gate voltage, while a P-channel enhancement-mode MOSFET conducts with a negative gate voltage.

When the voltage input to the inverter is low (logic 0), the gate voltage of the P-channel device is negative, equal to the supply voltage V_DD. As a result, the P-channel MOSFET is switched on, and there is a low impedance path from the output to V_DD. Because the N-channel is off (gate voltage is zero), there is a very high impedance path from the output to ground. Therefore, the output voltage rises to V_DD.

When the input voltage is high (logic 1), the situation is reversed. The P-channel FET is cut off, and the N-channel FET is on, so the output voltage falls to zero. Therefore, the circuit is a logic inverter: a low input results in a high output, and vice versa.

In either logic state one FET is on while the other is off. Because one FET is always turned off, the quiescent current of the CMOS unit is extremely low. These properties of N- and P-type enhancement-mode FETs combined to form CMOS gates provide many advantages:

- Extremely low power consumption.
- Wide power supply voltage range.
- High DC noise margin.
- High input impedance.
- Wide operating temperature range.

The diagram in Fig. 11-a illustrates standard CMOS metal-gate technology (74C/4000), but there are many other CMOS technologies including the high-speed silicon-gate HC, HCT, and FACT families. Another digital logic technology called BiCMOS takes advantage of the lower power consumption and higher integration density of CMOS, and the higher speed and superior drive capability of bipolar transistors.

**Power MOSFET's**

Power MOSFETs exhibit the properties of small-signal MOSFETs such as high-input impedance and voltage control, and they have drains, sources and gates, but they are designed continued on page 89.
Learn more about capacitors—how they are made, and how you can apply them more cost-effectively in your circuits

CAPACITORS

RAY MARSTON

CAPACITORS RANK NEXT TO RESISTORS AS THE MOST WIDELY PURCHASED ELECTRONIC COMPONENTS. FIXED AND VARIABLE CAPACITORS FOR ELECTRONICS AVAILABLE FROM COMMERCIAL SOURCES HAVE CAPACITANCE VALUES FROM A FEW PICOFARADS (pF) TO FARADS (F). AND THESE COMPONENTS ARE MADE FROM AN AMAZINGLY WIDE VARIETY OF MATERIALS.

THE OUTSTANDING TREND IN CAPACITOR DESIGN AND MANUFACTURE OVER THE PAST 85 YEARS—PARTICULARLY THE ARRIVAL OF THE INTEGRATED CIRCUIT—HAS BEEN MINIATURIZATION. THE OBJECTIVE OF ALL EFFORTS HAS BEEN TO CRAM AS MUCH CAPACITANCE AS POSSIBLE INTO SMALLER PACKAGES, WHILE AT THE SAME TIME INCREASING THEIR RELIABILITY.

TO GAIN A BETTER UNDERSTANDING OF THIS TREND, AND TO APPRECIATE WHAT HAS BEEN ACCOMPLISHED, IT IS WORTH REVIEWING THE FUNDAMENTAL CAPACITOR FORMULAS. THE ABILITY OF A CAPACITOR TO STORE ELECTRIC ENERGY IS A FUNCTION OF ITS GEOMETRY AND THE PHYSICAL CHARACTERISTICS OF ITS DIELECTRIC.

THE AMOUNT OF ENERGY THAT A CAPACITOR CAN STORE IS GIVEN BY THE EQUATION:

$$Q = CV$$

WHERE $$Q$$ = THE MAGNITUDE OF THE STORED CHARGE IN COULOMBS

$$C$$ = CAPACITANCE IN FARADS

$$V$$ = APPLIED VOLTAGE IN VOLTS

FIGURE 1-a SHOWS THE SIMPLEST CAPACITOR AND IDENTIFIES ITS PRINCIPAL PARTS AND PHYSICAL VARIABLES; FIG. 1-b IS THE ACCEPTED SCHEMATIC SYMBOL IN NORTH AMERICA FOR A FIXED CAPACITOR.

AND FIG. 1-c IS THE ACCEPTED SYMBOL FOR A VARIABLE CAPACITOR.

CAPACITANCE IN FARADS IS DETERMINED BY:

$$C = kA/d$$

WHERE $$k$$ IS THE DIELECTRIC CONSTANT (PERMITIVITY), THE RATIO OF THE ABILITY OF A DIELECTRIC MATERIAL TO STORE ELECTROSTATIC ENERGY TO THAT STORED BY A VACUUM BETWEEN THE SAME ELECTRODES (SEE TABLE 1).

A = DIRECTLY OPPOSING PLATE AREA

D = DISTANCE BETWEEN THE PLATES

DIFFERENT MULTIPLYING FACTORS CAN BE APPLIED TO THIS EQUATION SO THAT THE VALUE FOR $$C$$ IS IN MICROFARADS OR PICOFARADS WHEN $$A$$ AND $$D$$ ARE MEASURED EITHER IN INCHES OR MILLIMETERS. NEVERTHELESS, IMPORTANT ENGINEERING TRADEOFFS CAN BE SEEN FROM BOTH OF THESE EQUATIONS:

- TO STORE A GIVEN CHARGE, MORE VOLTAGE IS NEEDED FOR A SMALL CAPACITOR THAN A LARGE ONE.

- IF THE OPPOSING PLATE AREA, $$A$$, IS HELD CONSTANT, THE VALUE OF CAPACITANCE CAN BE INCREASED BY:
  a. DECREASING THE THICKNESS OF THE DIELECTRIC, $$h$$.
  b. USING A DIELECTRIC WITH A HIGHER CONSTANT, $$k$$.
  c. DOING BOTH (a) AND (b) SIMULTANEOUSLY.

WHILE NOT APPARENT FROM THE FORMULAS, OTHER FACTS ABOUT CAPACITORS TO BE CONSIDERED ARE:

- THE MAXIMUM VOLTAGE THAT CAN BE IMPRESSED ACROSS A CAPACITOR, WITHOUT DESTROYING IT, DEPENDS ON THE DIELECTRIC AND THE SEPARATION OF THE PLATES.

- FOR A GIVEN DIELECTRIC, THE ALLOWABLE MAXIMUM VOLTAGE CAN BE INCREASED AS THE DISTANCE BE-
The fabrication of increasing numbers of capacitors within very large scale integrated circuits such as microprocessors and digital signal processors has not reduced sales of discrete capacitors; in fact, the sales of certain kinds of capacitors have increased because of the proliferation of ICs. Moreover, capacitors are necessary in the external circuitry for the dedication of such multifunction linear ICs as compandor and modulation chips. Thin- and thick-film capacitors are being formed on ceramic substrates for networks and hybrid circuits that operate well into the microwave band.

Variable capacitors, still used primarily in radio-frequency circuits, are also being made from improved plastics and ceramics. A departure from their traditional dielectrics of air, glass, and ceramic, to reduce their size, extend their capacitance range, and cut cost.

Capacitor terms
Capacitors are widely specified with a glossary of widely accepted technical terms. A knowledge of these terms will be helpful to anyone who specifies or uses capacitors.

Capacitance. The basic unit for capacitance is the farad, but most capacitors for electronics applications need capacitance values that are only small fractions of a farad: microfarad (μF—one-millionth of a farad) and picofarad (pF—one-millionth of one-millionth of a farad).

Ambient temperature. The actual value of a capacitor depends on the temperature of its environment, known as ambient temperature. Percent capacitance change, a function of temperature, is referred to room temperature, 25°C.

Capacitive tolerance is the variation in capacitance value of the capacitor expressed as a percentage of its value at room temperature, 25°C, which is referred to as the nominal value. Temperature coefficient (TC) is the change in a capacitor’s capacitance per degree change in temperature, expressed in parts per million per degree Celsius (ppm/°C). The coefficient can be positive, negative, or zero. The letter P indicates that the coefficient is positive: N if negative. The designation NPO identifies a zero-temperature coefficient. Rated working voltage is the maximum permissible operating voltage at which a capacitor can be continuously operated at maximum rated voltage (without derating). This rating must be specified as AC or DC because they are not usually equal.

Surge voltage is the maximum instantaneous voltage to which the capacitor should be subjected: exceeding that voltage will cause the capacitor’s breakdown. Surge voltage is higher than working voltage.

DC leakage is the small amount of direct current that flows in a capacitor at a specified voltage. Caused by the presence of free charge carriers within the dielectric, it is the reason why a charge cannot be stored indefinitely in a capacitor; eventually it leaks off.

Insulation resistance (IR) is the resistance of the dielectric. High resistance results in low leakage current. This variable is inversely related to ambient temperature.

Capacitive reactance (Xc) of a capacitor is inversely related to the product of capacitance and frequency in accordance with:

\[ X_c = \frac{1}{\omega C} \]

where 0.159 is a conversion constant

\[ X_c = \text{capacitive reactance (ohms)} \]

\[ f = \text{frequency (hertz)} \]

\[ C = \text{capacitance (farads)} \]
Power factor (PF) expresses the ratio of energy dissipated to the energy stored in a capacitor, as a percent. It typically exhibits a negative slope below room temperature and positive slope above it.

Equivalent series resistance (ESR), expressed in ohms, is the sum of all internal resistance values of a capacitor. These include lead resistance, terminal losses, and dissipation in the dielectric. ESR increases with frequency.

Impedance (Z) of a capacitor is the total opposition it offers to the flow of alternating current at a given frequency:

\[ Z = \sqrt{X_c^2 + (\text{ESR})^2} \]

where \( Z \) = impedance (ohms)
\( X_c^2 \) = capacitive reactance (ohms)
\( \text{ESR} \) = equivalent series resistance (ohms)

Capacitive impedance is inversely proportional to frequency and temperature; ideally, it equals capacitive reactance.

Dissipation factor (DF) of a capacitor is the ratio of energy dissipated to energy stored in the dielectric. DF is a figure of merit for the quality of a capacitor.

\[ \text{DF} = \frac{\text{ESR}}{X_c} \times 100\% \]

Ideally capacitors have low values of DF over wide temperature ranges.

\( Q \) or Quality factor is the ratio of energy dissipated to energy stored, so it is the reciprocal of dissipation factor at low frequencies.

\[ Q = \frac{1}{\text{DF}} = \frac{X_c}{\text{ESR}} \]

The highest quality capacitors have high Q's.

Ripple current is the result of a periodic AC voltage wave superimposed on the DC voltage applied to the capacitor. Ripple current flowing through the ESR of a capacitor can generate heat, raising the temperature of the capacitor.

Volumetric efficiency is a measure of relative capacitance per unit volume. One capacitor has a higher volumetric efficiency than another capacitor of the same size (volumetric dimensions) if it is able to store more charge, or has a higher capacitance rating.

Capacitor applications

Capacitors have many different applications in electronic circuits:

- **Blocking**—limiting the flow of direct current or low frequency alternating current without significantly affecting the flow of high-frequency AC.
- **Bypassing**—providing a low-impedance path around a circuit component to permit the flow of alternating current.
- **Coupling/decoupling**—coupling or decoupling alternating signals between circuits and systems.
- **Energy storage**—storing electric energy for later release to power a device or circuit.
- **Filtering**—removing the DC component from a signal.
- **Smoothing**—reducing the ripple on an input signal.
- **Timing**—providing capacitance value in timing circuits.
- **Tuning**—providing capacitance value for tuning in a tank circuit.

Fixed capacitors

Figure 2 is a diagram showing how fixed capacitors are classified as electrostatic and electrolytic. Electrostatic capacitors are so named because an electrostatic charge is stored between opposing plates. They are named for the dielectrics between their plates. This can be air or a vacuum or such solid materials as plastic film, ceramic, mica, and glass.

Electrostatic capacitors are further classified by packaging method: leaded or non-leaded (chip); radial or axial leaded; molded, conformally coated, or dipped in an encapsulant, typically epoxy. A film capacitor can be further classified by the specification of its plastic film such as polyester or polycarbonate.

Electrolytic capacitors are made of metals, normally either aluminum or tantalum, that form extremely thin anodic oxide layers of high-dielectric constant and good electrical characteristics during electrolytic processing. These capacitors are classified by the metals from which their anodes are made—aluminum or tantalum—and capacitor configuration: wet foil, wet slug, or dry slug (solid electrolyte).

Film capacitors

Film capacitors are made with thin dielectric plastic films such as polyester (Mylar), polycarbonate, polystyrene and polypropylene that is 0.06 mil (1.5 micrometers) to over 0.8 mil (20 micrometers) thick. The electrodes of film capacitors can be metal foil (film/foil) or metal directly deposited on the film (metalized). Film/foil capacitors are made of dielectric film sandwiched between tin or alumi-
Both film/foil and metalized-film capacitors are made with axial or radial leads in a variety of case sizes. They can be hermetically sealed in tubular or rectangular metal cases, or encapsulated by molding or conformally coating with epoxy.

Film capacitors are most widely specified for capacitance values from 500 picofarads to 10 microfarads. (Refer to Table 2.) Their working voltages typically range from 50 volts DC to 630 volts DC—although they can have higher ratings. Capacitance tolerance is typically from ±1% to ±10%

Film dielectrics

The four most widely used film dielectrics are:
- Polyester (tradename Mylar) capacitors are the most popular general-purpose film capacitors. This film permits high volumetric efficiency, low leakage, and a moderate temperature coefficient. Some film/foil and metalized units can operate to 125°C at 50% of rated voltage. Metalized-polyester units can perform blocking, coupling, decoupling, bypass, and filtering.
- Polycarbonate capacitors have operating temperatures from -55°C to as high as +125°C with proper voltage derating.

Capacitive tolerances can be as low as ±5%. This dielectric film offers high insulation resistance and stability.
- Polystyrene capacitors have characteristics that are similar to those of polypropylene, but they have lower volumetric efficiency. They have capacitive tolerances as low as 1%. Film/foil units are widely used in inductive-capacitive filters.
- Polypropylene capacitors have higher volumetric efficiency than polyester capacitors. Except for AC rating, their characteristics are similar to those made from polystyrene. They have tolerances as low as ±2%. These capacitors are specified where precision, reliability, and low losses are important: e.g., tuning, filtering, and timing.

Ceramic capacitors

There are three ceramic capacitor styles: single-layer disc, single-layer tubular, and monolithic multilayer. There are three principal classes of ceramic dielectric based on their k rating: Class I, II, and III. Low-k materials have linear characteristics, and their properties are independent of frequency over their normal range. They are suitable for resonant-circuit or filter
characteristics. High-K ceramics have very high effective dielectric constants. They are suitable for coupling and decoupling applications.

- **Disc ceramic** capacitors are made by metalizing both surfaces of a thin low-k (Class III) ceramic disc with silver-based ink to form the electrodes, firing the disk, and soldering on radial leads. They are jacketed by dipping in phenolic resin or epoxy. These capacitors are being replaced by tubular ceramic units made of the same materials that save circuit board space and permit automatic parts placement.

- **Tubular ceramic** capacitors are made by coating the inner and outer surfaces of Class III ceramic tubes with silver-based thin-film ink, firing, and attaching leads to the tube before jacketing it by epoxy dipping.

- **Monolithic multilayer ceramic** (MLC) capacitors are made by screening thin-film, precious metal-based conductive ink on thin layers of "green" or unfired layers of higher k (Class II and III) ceramics. The screened layers are then stacked (up to 40 layers), compressed, and fired to form monolithic capacitors, as shown in Fig. 4.

If the MLC capacitor is to be a chip capacitor for a hybrid circuit or surface-mounting, conductive-metal terminations are plated on its ends, as shown in Fig. 4. The terminals of surface-mount chips are further plated with lead-tin alloy to improve the terminal-to-pad solder joints.

Demand for MLC chips has risen with the worldwide growth of surface mounting. Chip MLC's will withstand the molten-solder temperatures encountered in reflow and wave soldering. They are available in standard sizes to fit the grasping tools in automated pick and place machines. The most common sizes are 0.08 x 0.05 inch (0805), 0.125 x 0.063 inch (1206), and 0.05 x 0.225 inch (2225).

Cylindrical leadless capacitors are also made for surface mounting. These capacitors

### Table 2
**Characteristics of Popular Fixed Capacitors**

<table>
<thead>
<tr>
<th>Type</th>
<th>Capacitance Range</th>
<th>Working Voltage</th>
<th>Maximum Operating Temp. (°C)</th>
<th>Tolerance (Percent)</th>
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<tbody>
<tr>
<td>Electrostatic</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Film</td>
<td>0.001 - 1.0</td>
<td>80 - 200 VDC</td>
<td>+125*</td>
<td>±5 - ±10</td>
</tr>
<tr>
<td>Polyester (Mylar)</td>
<td>0.001 - 10.0</td>
<td>60 - 630 VDC</td>
<td>+125*</td>
<td>±5 - ±10</td>
</tr>
<tr>
<td>Polycarbonate</td>
<td>0.01 - 10</td>
<td>100 - 630 VDC</td>
<td>+125*</td>
<td>±5 - ±10</td>
</tr>
<tr>
<td>Polystyrene</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Film/foil</td>
<td>47 pF - 0.039</td>
<td>63 - 630 VDC</td>
<td>+85</td>
<td>±1 - ±5</td>
</tr>
<tr>
<td>Polypropylene</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Film/foil</td>
<td>47 pF - 0.022</td>
<td>63 - 630 VDC</td>
<td>+85</td>
<td>±2 - ±5</td>
</tr>
<tr>
<td>Metalized</td>
<td>0.001 - 3.3</td>
<td>250 - 100 VDC</td>
<td>+85</td>
<td>±5 - ±10</td>
</tr>
<tr>
<td>Ceramic</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Multilayer</td>
<td>10 pF - 0.56</td>
<td>200 VDC</td>
<td>+125</td>
<td>±5 - ±10</td>
</tr>
<tr>
<td>Disc</td>
<td>0.75 pF - 2.2</td>
<td>50 - 6 KVDC</td>
<td>+125</td>
<td>±5 - ±10</td>
</tr>
<tr>
<td>Mica</td>
<td>1 pF - 0.1</td>
<td>50,000</td>
<td>+150</td>
<td>±25 - ±5</td>
</tr>
<tr>
<td>Glass</td>
<td>10 pF - 0.15</td>
<td>6000</td>
<td>+125</td>
<td>±1 - ±20</td>
</tr>
<tr>
<td>Electrolytic</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Aluminum</td>
<td>1.0 - 1 MEG</td>
<td>5 - 450</td>
<td>+105</td>
<td>-10 - +100</td>
</tr>
<tr>
<td>Tantalum</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Wet slug</td>
<td>1.7 - 2400</td>
<td>6 - 630</td>
<td>+125</td>
<td>±5 - ±20</td>
</tr>
<tr>
<td>Wet foil</td>
<td>0.12 - 3500</td>
<td>3 - 300</td>
<td>+125</td>
<td>±5 - ±20</td>
</tr>
<tr>
<td>Solid slug</td>
<td>0.0023 - 1000</td>
<td>6 - 100</td>
<td>+125</td>
<td>±5 - ±20</td>
</tr>
</tbody>
</table>

* With derating

![FIG. 5—VIEW OF AN ALUMINUM ELECTROLYTIC CAPACITOR](image)

**FIG. 5**—VIEW OF AN ALUMINUM ELECTROLYTIC CAPACITOR shows how the cathode (porous paper spacer filled with liquid electrolyte) is sandwiched between the oxidized aluminum anode foil and cathode connection foil, rolled into cylinder, and then sealed in an aluminum can.
have metalized-band contacts on the ends of their epoxy-coated bodies for soldering to lands of surface-mount circuit boards.

For conventional through-hole mounting, axial or radial leads are attached, and the chip is jacketed by dipping or molding in epoxy. MLC capacitors are specified for bypassing noise to ground, timing, and frequency selection.

**Ceramic dielectrics**

Ceramic dielectric materials are classified by dielectric constant $k$ as Class I, Class II and Class III:

- **Class I** dielectrics are made by mixing magnesium titanate (for a positive temperature coefficient) with calcium titanate (for a negative coefficient) to form a dielectric material with low $k$ values, and properties essentially independent of frequency. They exhibit ultrastable temperature coefficients of $\pm 30$ ppm/$^\circ$C over the temperature range of $-55^\circ$C to $+125^\circ$C. Class I includes NPO (negative, positive, zero), also known as COG and BY.

- **Class II** dielectrics are high-$k$ materials (called ferroelectrics) based on barium titanate. With the addition of barium stanate, barium zirconate, or magnesium titanate, their dielectric constants can be lowered from values as high as 8000 for increased temperature stability. These dielectrics include general purpose X7R (BX) and Z5U (BZ).

- **Class III** dielectrics were developed primarily for ceramic disc capacitors because they permit high volumetric efficiency. But this introduces a trade-off between high leakage resistance and low dissipation factor. Class III capacitors have low working voltages.

**Other electrostatic capacitors**

The dielectric in a mica capacitor is mica, a natural mineral that is chemically inert and very stable. The capacitor is generally made as a "sandwich" of alternating layers of tin-lead foil plates and mica. These capacitors can operate at temperatures up to $+150^\circ$C. Silvered mica capacitors offer greater mechanical stability and more uniform characteristics. They are made by screening and firing a thin layer of silver on the surface of the mica to form the plates.

**Glass** capacitors are made by stacking alternate layers of thin glass dielectric in a sandwich structure similar to that of the mica capacitor. They are specified where temperature stability is a requirement.

**Electrolytic capacitors**

The dielectrics of aluminum and tantalum electrolytic capacitors are oxides formed by electrochemical reaction with those metals. There are three styles of electrolytic capacitor: wet foil, wet slug, and dry or solid slug. Aluminum electrolytic capacitors are wet foil units, but tantalum capacitors are also available as wet-slug and solid slug units. They can be polarized or nonpolarized.

All electrolytic capacitors exhibit high capacitance per unit volume (high volumetric efficiency). An aluminum electrolytic capacitor can store four, five or more times the charge of an equivalent-size film capacitor, and a tantalum capacitor can store three times as much charge as an equivalent aluminum capacitor.

However, aluminum electrolytic capacitors have higher DC leakage and lower insulation resistance than electrostatic capacitors. Moreover, they have higher power losses because of their higher equivalent series resistance (ESR).

The anodes of aluminum electrolytic capacitors are made from high-purity aluminum foil that has been electrochemically etched to increase its effective surface area. A thin aluminum-oxide-dielectric layer, about 0.01 micron, is then grown on the etched foil in another electrochemical process. The enlarged surface area of the etched foil provides a far larger dielectric surface than would be possible with unetched foil.

A porous paper spacer filled with a liquid electrolyte is sandwiched between the etched and oxidized anode foil and another aluminum cathode foil. The liquid electrolyte is the actual cathode, but the cathode foil is in contact with the liquid electrolyte and is needed to complete the electrical circuit.

After attaching a series of connecting tabs to the foils, the "sandwich" is rolled, as shown in Fig. 5, and inserted in an alu-

---

**FIG. 6—CUTAWAY VIEW OF WET-SLUG TANTALUM CAPACITOR SHOWS TANTALUM SLAG FILLED WITH WET-ELECTROLYTE SEALED IN A SILVER CASE.**

**FIG. 7—CUTAWAY VIEW OF A SOLID TANTALUM CAPACITOR JACKETED BY DIPPING IN EPOXY.**
minum can, which is then sealed. However, the sealed can has an overpressure vent.

Direct current must flow in only one direction in a polarized electrolytic capacitor. Even short-term current reversal could destroy the oxide dielectric and short-circuit the capacitor. A "+" mark on the case identifies its positive terminal.

Aluminum electrolytic capacitors are made with radial or axial leads, and some styles for switchmode power supplies have spring-metal terminals that snap into circuit board holes. An external plastic sleeve permits off-ground applications for the capacitor.

Nonpolarized aluminum electrolytic caps are essentially two polarized capacitors back-to-back with their cathode terminals connected. The anode terminals make the external circuit connection, while the cathode terminals are isolated by an insulator. Both foils are anodized to form oxide barriers, and they share a common electrolyte-filled porous spacer.

A nonpolarized capacitor has half the capacitance of a comparably sized polarized capacitor with the same voltage rating. Although not as efficient as polarized capacitors, the nonpolarized units are used for AC motor starting and other AC control applications.

**Tantalum capacitors**

Tantalum electrolytic capacitors are available in three forms: wet-foil, wet slug, and dry slug. Wet-foil tantalum capacitors are made in the same way as aluminum electrolytics. As a group, tantalum capacitors exhibit higher volumetric efficiency, more stable characteristics, higher operating temperature ranges, and longer shelf lives than aluminum capacitors. However, they cost more and have lower voltage ratings.

Both wet and dry slug tantalums are made from porous pellets of tantalum. The anode slug is formed by pressing tantalum powder and a binder in a mold, and firing it in a vacuum furnace (sintering) to bond the powder and drive off the binder.

The tantalum oxide dielectric is electrochemically formed in the porous pellet.

Figure 6 is a cutaway view of a wet-slug tantalum capacitor with an acid electrolyte. Its volumetric efficiency about three times that of a comparably sized foil unit. Moreover, wet-foil tantalums are the most reliable of all capacitors.

The high cost of wet-foil and wet-slug tantalums makes them too expensive for most consumer and industrial applications. However, those high-reliability capacitors are widely specified for military electronics and avionics. Military specifications MIL-C-3965 and MIL-C-39006 govern the procurement of military-style wet-foil and solid-slug units.

The solid-anode or dry-slug unit, shown in Fig. 7, is the most popular and economical tantalum capacitor. It has a thin film of manganese dioxide chemically deposited on its tantalum dioxide dielectric to act as a second electrode. Solid-slug capacitors can be sealed in metal cases, or protected by dipping in epoxy as shown in Fig. 7. The solid-slug units have the longest life and lowest leakage of any tantalum caps. Chip capacitors for surface mounting, as shown in Fig. 8, are made by the same process.

**Capacitor identification.**

Today the capacitor's nominal value (and sometimes its tolerance) are printed on its body where space permits. Values such as 47 and 68 are typically in microfarads, while values such as 120 or 4700 are usually in picofarads. A capacitor might also be marked with its working voltage: for example, 63 V or 100 V.

Some capacitors are still marked with colored bands based on the EIA system used for identifying resistors. The colors of the bands are read from left to right. A black band represents zero, brown represents one, and red, orange, yellow, green, blue, and violet represent the digits two to seven, in that order. Grey represents eight, and white represents nine. As in resistor coding, a gold band denotes a capacitive tolerance of 5%, while a silver band denotes 10%.

You might encounter capacitors with obsolete coding schemes in old radios or TVs or at surplus sales. Some of those codes are based on colored dots, spots or "hashmarks." It is wise to consult a radio engineering handbook or data reference book published before 1970.
you want to find out how to interpret those codes if you plan to use them in your circuits and are in doubt about their ratings.

Connecting capacitors

Figure 9 illustrates capacitors connected in series and parallel. The formula for calculating the effective value of two capacitors in series is:

$$C_{TS} = C_1 \times C_2 / (C_1 + C_2)$$

For two or more capacitors in series it is:

$$C_{TS} = 1 / (1/C_1 + 1/C_2 + 1/C_3 + ... + 1/C_n)$$

For capacitors in parallel the formula is:

$$X_{TP} = C_1 + C_2 + C_3 + ... + C_n$$

Variable capacitors

For many years the most prominent variable capacitors were those used to tune radio receivers, transmitters, and oscillators. However, in the latest transistorized equipment they have been largely superseded by varactors or voltage variable capacitors. These are silicon or gallium arsenide PN junction diodes that make use of the variation of junction capacitance with reverse bias. Nevertheless, the design concept embodied in the tuning capacitor lives on in a wide range of miniature, PC board-mounted variable capacitors for many different tuning applications.

Figure 10 is a simplified sketch of an air-dielectric tuning capacitor. Its capacitance value can be changed by rotating its control shaft so that the movable set of metal plates (rotor) meshes in different positions with respect to the fixed set (stator). Its capacitance value is greatest when the rotor is fully meshed with the stator.

The rotor plates of tuning capacitors can be shaped so that, with shaft rotation, capacitance variation is linear or nonlinear. For example, it might follow a nonlinear logarithmic or square law function. Two or more tuning capacitors can be ganged together so that they vary in unison, simultaneously tuning separate circuits to different frequencies.

Trimmer capacitors are "set and forget" variable capacitors made for infrequent adjustment. Many different types are available for commercial and industrial applications. Vane types are miniaturized versions of the tuning capacitor shown in Fig. 10, except that layers of solid dielectric, typically plastic, are inserted between the rotor and stator plates.

Vane-type trimmers with body diameters of less than a half inch are made for PC-board mounting. They have plastic cases and dielectrics of polypropylene, polyethylene, polycarbonate, or PTFE films. These trimmers are made for screwdriver and/or key adjustment.

There are also simpler trimmer capacitors that permit more limited capacitance variation for high-frequency tuning applications.

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ONE OF THE MANY modern sensor technologies is really keeping engineers and hobbyists quite busy designing circuits. Billed as the ultimate switch technology, the Force Sensing Resistor (FSR) is a tactile sensor that discerns variations in applied force. The harder you press this thick-film device, the more its resistance decreases. The FSR was first developed for musicians who wanted their electronic pianos to play louder when the keys were pressed harder. FSRs are temperature, chemical, and moisture resistant, and they are insensitive to vibration and electromagnetic interference. FSRs contain no moving parts to wear out, and can withstand over ten million operations. Figure 1 shows some of the different types of FSRs.

FSRs are as thin as business cards, and can be designed to sense forces as light as a fingertip or as heavy as a truck. They can also sense variations in applied pressure and alter their response accordingly. In addition, the sensor's actuation threshold can be adjusted using simple electronics. Applications for FSRs are virtually unlimited, as you can see from Table 1. The FSR is ideally suited to keypads, computer input devices, touch switches, alarm sensors, limit switches, electronic keyboards, digitizers, and pressure sensors.

An FSR device typically exhibits three decades of dynamic resistance change with respect to force and it can operate at much lower currents than most other sensors. The FSR can also be used to construct a linear potentiometer which can monitor the position of a force as well as the amount of applied force. A three-layer XYZ-type FSR device can be constructed that will give an X-Y coordinate position indication with a 0.005-inch resolution, as well as provide the force (Z) measurement. The XYZ pad is ideal for such applications as a graphic pad, pen stylus tablet, or mouse-type device for computer input. The FSR sensors can also be configured into many different types of switch arrays, with sizes up to $22 \times 32$ inches, at much lower cost than many other force sensors.

In the past, there were two principle types of force sensors: piezopolymers and ceramic strain gauges. The fast rise times and high sensitivities of the piezopolymers cause a lot of unwanted acoustic and vibration pickup. Piezopolymer sensors often require more complex interfacing than the FSR devices. FSR sensors are not as accurate for precise absolute measurement, but they are much more rugged and cost considerably less than strain-gauge sensors.

The construction of an FSR is a sandwich of two polymer films or sheets. A conductive pattern is deposited on one of the polymer sheets as a pattern of inter-
digitizing electrodes as shown in Fig. 2. The electrode pattern often looks like a comb, with the teeth and spacing typically being less than one millimeter. Next, a proprietary polymer is deposited on the other sheet. The sheets are then faced together so that the conducting fingers are shunted by the polymer.

The output resistance of the FSR is typically around one megohm with no external force applied. A force-versus-resistance graph is shown in Fig. 3. The graph displays the log/log characteristics of an FSR where the resistance varies from one megohm to around 50 kilohms, depending on the applied force in grams (g). (We know that a gram isn't really a force, but let's just think of it that way for the moment.) Figure 4 shows a force-versus-conductance graph in which a simple linear response is shown from a force of zero grams. A key element in the design of an FSR is the fineness of the pitch of the conducting fingers. The force-versus-resistance relationship is strongly affected by sensor and actuator size, shape, and materials.

Linear potentiometer FSR's
When force-sensing resistors are used to make a linear potentiometer (an FSR-LP), the device can be used to sense both position and applied force. Figure 5 depicts the layered construction of an FSR-LP. When wiring an FSR-LP, a voltage is applied between the hot lead and ground. When a force is applied to the force-sensing layer, the wiper contacts are shunted through that layer to one of the conducting fingers of the resistance strip. The voltage from the wiper is then proportional to the distance along the strip. To sense a force, a resistance measurement is made between the wiper terminal and either the hot or ground lead. Two alternative FSR-LP connection diagrams are shown in Fig. 6.

Force and position measurements are not entirely independent; however, the position measurement can be made unambiguously if the measuring device draws a negligible amount of current (less than 1 microampere) so that there is no voltage drop across the wiper resistance. Therefore, an LF411 or similar op-amp—with a low $V_{OS}$ and $I_{IHAS}$—is recommended when interfacing to an FSR-LP. Because the contact between the wiper and the resistor is momentary, some kind of sample-and-hold device must be used to interface an FSR: quite often a capacitor between the wiper contact and ground is sufficient to accomplish this.

Force measurements are less ambiguous, and very good approximate measurements can be obtained by shorting the two fixed resistor ends (hot and ground) together, and measuring the resistance between the

<table>
<thead>
<tr>
<th>TABLE 1—FSR APPLICATIONS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Graphic pads</td>
</tr>
<tr>
<td>Cursor keys</td>
</tr>
<tr>
<td>Mouse devices</td>
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<tr>
<td>Pen stylus tablets</td>
</tr>
<tr>
<td>Pressure sensors</td>
</tr>
<tr>
<td>Piano keyboards</td>
</tr>
<tr>
<td>Toner-level sensors</td>
</tr>
<tr>
<td>Foot pedals</td>
</tr>
<tr>
<td>Gait-analysis sensors</td>
</tr>
<tr>
<td>Artificial-limb force sensors</td>
</tr>
<tr>
<td>Dental-byte sensors</td>
</tr>
<tr>
<td>IV drip pressure sensor</td>
</tr>
<tr>
<td>Bed weight distribution sensor</td>
</tr>
<tr>
<td>Security tiles/alarm sensors</td>
</tr>
<tr>
<td>Load cells</td>
</tr>
<tr>
<td>Suspension sensors</td>
</tr>
<tr>
<td>Accelerometers</td>
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<tr>
<td>Water-level sensors</td>
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<tr>
<td>Panel switches</td>
</tr>
<tr>
<td>Digital tuning controls</td>
</tr>
<tr>
<td>Joysticks</td>
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<tr>
<td>Game controllers</td>
</tr>
<tr>
<td>Steering wheels</td>
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<tr>
<td>Gas pedals</td>
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<tr>
<td>Robotic touch sensors</td>
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<tr>
<td>Industrial keyboards</td>
</tr>
<tr>
<td>Deadman safety switches</td>
</tr>
<tr>
<td>Smart brake pedals</td>
</tr>
<tr>
<td>Oil-pressure sensors</td>
</tr>
<tr>
<td>Limit switches</td>
</tr>
</tbody>
</table>

For the force measurement, $V_{OS}$ and $I_{IHAS}$ are: 

$V_{OS} = \pm 10\text{mV}$

$I_{IHAS} = \pm 0.1\mu\text{A}$
combined leads and the wiper. If the force is applied at the middle of the potentiometer, the device will have an additional resistance of one half of the total fixed resistance, because the resulting middle contact parallels the two halves of the fixed resistor. If, on the other hand, force is applied to either end of the FSR-LP's active area, the fixed resistance is essentially shorted out. That problem can be overcome by making the FSR resistance high compared to the potentiometer resistance, therefore making a low-current position measurement a must. The slight force-measurement error can also be subtracted out with a simple analog circuit or, given a position measurement, compensated for in software if a microprocessor is used with the system.

The positional resolution of a force and position sensing resistor (FPSR) depends on the width of the applied force, distribution, and the fineness of the conductive fingers, which is typically in the 10–100 micro-meter range.

**FSR-LP XYZ**

An XYZ pad or tablet is constructed by placing two FSR-LP's back-to-back and perpendicular to each other. An XYZ pad can measure the position of a force on an X-Y coordinate plane, as well as the applied force (Z). Figure 7 shows the layered construction of an XYZ pad. Note that an unambiguous position can be measured only for a single applied force: multiple force contacts will cause false readings. That is not a problem for graphics pads, mouse devices, or pen stylus tablets, but the XYZ pad cannot be used for complex pattern recognition. Position accuracy of an XYZ pad based on FSR-LPs is typically about 1 percent.

A true force sensor will give a constant reading at a constant force, independent of the area over which the force is applied, or its distribution. If a constant force is applied to a true pressure sensor, the reading will be inversely proportional to the area of the applied force. An FSR has a function that is between a force and pressure sensor. A typical FSR will display the resistance of the square root of the area of the applied force. That holds true when the force footprint is smaller than the FSR's active area, and large compared to the spacing between the conductive electrodes or fingers. Because of the sensitivity of the FSR's resistance to the area and distribution of force, the force footprint must be held constant in position and distribution. An elastomeric or rubber overlay placed over the sensor can solve that problem. The FSR can be used as a pressure sensor when the applied force is large compared to the FSR's active area.

FSR devices are designed to be easily interfaced with a wide variety of circuitry. A simple analog interface is shown in Fig. 8. A basic requirement for interfacing an FSR is to ensure that the current through the device does not exceed 1 mA/cm² of the activation footprint. The voltage measurement across the FSR is then related to the applied force, and increased pressure results in increased...
LF351/353 or the TL071/72 series of low bias-current devices. The low bias currents of those op-amps reduces the possible input offsets, due to the high source impedances of the FSR.

Figure 10 shows a force-to-frequency converter. In that circuit, an oscillator is constructed with the FSR as a feedback element around a Schmitt trigger integrated circuit. At zero pressure, the FSR is an open circuit. Depending on the last stage of trigger, the output remains constant—either high or low. When pressure is applied to the FSR, the oscillator starts, and its frequency increases with increasing force applied to the FSR. Resistor R1 limits the current through the sensor. Bypassing R1 with a capacitor will cause the curve to be steeper at higher forces. Connecting a large-value resistor in parallel with the capacitor (C), quenches any tendency for the circuit to oscillate at low applied forces. When using the circuit with CMOS or TTL, a digital process can be controlled by counting leading or trailing edges of the oscillator output.

Industry-standard connectors, such as pin- or compression-types, can interface the FSR devices. Conductive adhesives are also commonly used to attach leads to FSR devices. Do not attempt to solder wire leads directly to the polymer sensor, because direct heat will destroy the device.

The force-sensing resistors require a backing for activation accuracy, as mentioned previously. The most unpredictable aspect of the FSRs force/resistance characteristic is the pressure range under 100 grams/cm². If you are going to measure small forces with your FSR, you can preload the FSR with a 100–200 gram/cm² load and measure the resistance changes. Elastomer or plastic overlays can be used to enhance the FSR’s response characteristics by evenly spreading the actuator’s force.

FSR sensors are available in many sizes, configurations, and shapes, and custom devices can be designed by the manufacturer. For more information on FSR technology, write on your company letterhead to Interlink Electronics, 1110 Mark Ave., Carpinteria, CA 93013. An evaluation/prototype kit is also available for $79.95.
OUR TIME-DELAY RELAY WILL DRIVE up to a 3-ampere AC load for a specified period of time, and then shut the load off automatically. It can turn electrical appliances and lights off after a time interval ranging from just a few seconds all the way up to about an hour.

One of the many possible jobs for the relay is the control of indoor Christmas lights—just push a button and the lights will stay on for a few hours, and then automatically turn off. Outdoor Christmas lights, although a considerably larger load, can also be controlled by one of these relays.

The author has several different antennas that are connected to amateur radio equipment in his garage. As a precaution, the feedlines to the radios are routed through mechanical relays that keep them grounded when not powered, and they are connected to the radios only when the reset switch on the time-delay relay is pushed. Several hours later, if he has been called away from the radios (and forgotten that they were on), the relay drops out, and the antennas will have been automatically grounded.

One of these units can even be used with a coffee maker. Quite often coffee makers are left on overnight or over the weekend; the owner returns to find a ruined coffee pot—and a very hot one at that. A time-delay relay in the burner circuit will solve that problem. Simply set the timer to stay on for 2 hours, and if it's not reset, it will allow the coffee pot to cool off.

**Operation**

The circuit, shown in Fig. 1, is based on a 4060 CMOS 14-stage binary counter with an on-board oscillator driver. The basic frequency is set by the values of R1, R2, and C1, and it's roughly 1/R1 × C1. Resistor R2 should be about 10 times the value of R1. The values shown generate an approximate 4.5-hertz frequency, which is then divided down by IC1. Divided outputs are available ranging from divide-by-4 to divide-by-16384 (see Fig. 1).

The chosen output is tied to the base of Q1 through current-limiting resistor R4, and to the base of Q2 through R3. Transistor Q1 is the hold transistor for the timing circuit, and transistor Q2 turns on the solid-state relay.

![Time Delay Relay Circuit](https://www.americanradiohistory.com/archives/march1983/69.jpg)

**FIG. 1**—THE CIRCUIT is based on a 4060 CMOS 14-stage binary counter that controls a solid-state relay.
When you push reset button S1, all of IC1's outputs go low (including the one you have tied to the transistor input). Transistor Q1, an NPN unit, shuts off and its collector, which is tied to timing resistor R2, presents no load to the timing circuit. Transistor Q2, a PNP unit, turns on when a low is applied to its base, thus turning on the solid-state relay.

When the chosen output of IC1 goes high, Q1 turns on, grounding the clock input to IC1, stopping any further counting until S1 is pushed again. At the same time, Q2 shuts off, which turns off the solid-state relay, thus cutting off power to the load.

**Construction**

The author built his prototype relay on a small piece of perforated construction board using point-to-point wiring, and arranged the parts so that the board would mount on the end of the solid-state relay (the input terminals are big enough to support the circuit board). Figure 2 shows the inside of the prototype. Note that the author has built in a 9-volt power supply that is not shown in the schematic.

**PARTS LIST**

All resistors are 1/4-watt, 5%.
- R1—470,000 ohms
- R2—4.7 megohms
- R3—R5—4700 ohms

**Capacitors**
- C1—0.47 µF, 25 volts, tantalum

**Semiconductors**
- IC1—4040 CMOS timer/divider
- Q1—2N2222 NPN transistor
- Q2—2N2907 PNP transistor
- S1—Normally-open pushbutton switch

**Miscellaneous:** Solid-state relay (sized for the application you have in mind), perforated construction board, wire, solder, AC linecord, project case.

**The relay in action**

To use the solid state relay, simply plug the relay into a 120-volt outlet, plug an appliance (that draws no more than 3 amperes) into the time-delay relay, and push the reset button. The circuit will begin timing and will shut off at the end of the period you have selected. When you use the time-delay relay to shut off your appliances, you'll not only be adding a safety feature and saving money—you'll also be doing something good for the environment!

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**LETTERS**

continued from page 17

diovisual phenomenon discussed anywhere. During a TV broadcast of a choir singing, my attention would inevitably focus on an individual singer (usually the cute one), and I would swear that I could hear her individual voice against a background of the entire choir.

Sure enough, when the camera zoomed in on her, she sounded exactly as I had earlier perceived she would. If there were several attractive choir members, I would be able to pick out their individual voices too. The cameraman apparently often agrees with my choices, and pans his camera on the photogenic singers during the performance. I can even keep track of their individual voices with closed eyes.

The same phenomenon seems to occur during orchestral performances, where I seem to be able to isolate individual instruments from the whole orchestra.

I cannot think of a way to test this phenomenon scientifically because what comes out of the speaker is a blended waveform. Thus, the perception must be the result of my visual clues together with the audio. I will chicken out with an escape clause: The human brain must be a wondrous organ if it is able to interpret such fine subtleties from a blended signal. But, all the same, I wonder if anyone else shares my illusions, or is there something more to this?

KELVIN MOK
Edmonton, Alberta, Canada

**SILICON CHIP**

I was recently looking at Silicon Chip, an Australian electronics magazine that had lots of interesting projects in it. It would be good if **Electronics Now** could reprint some of these articles for readers in this country.

WILLIE JONES
Valley Stream, NY

Good news for you! The magazine you mentioned, Silicon Chip, will soon be in print in this country. See the ad for it on page 25 of this magazine.
It seems that everybody is an audio enthusiast these days. With compact discs, stereo TV, hi-fi video tapes, and laserdiscs cheaply available to the general public, nobody wants to settle for ordinary sound. If you build our audio processor, you won’t have to settle for ordinary sound either! Our audio processor, which can be built in one evening, can be installed easily between any audio output source and any audio input source, and it can “supercharge” any mono or stereo audio signal.

Some of the many uses for the audio processor include enhancing the audio output from a stereo system or any scanner, shortwave, CB, or ham radio receiver. Stereo and mono TV sound can also be greatly enhanced; a pseudo-stereo effect can be added to a mono sound track, and if stereo audio is already in use, you can add enhanced stereo effects. The processor also has amazing effects on old mono or pre-Dolby cassette and 8-track tapes—it’s great for doing restoration of old recordings.

Features
The audio processor provides a complete array of controls that give the user maximum flexibility in adjusting the processor. The unit has switch-selectable stereo sound from a stereo source, spatial (widened) sound from a stereo source, and pseudo-stereo sound from a mono source; LED’s indicate which mode is selected.

The unit exhibits very low noise (−64 dB minimum) and low total harmonic distortion (maximum THD is 0.5% at 1000 Hz). The input and output resistance is 100 kilohms, which is the standard line-level resistance. The left and right channels provide a minimum of 60 dB separation, and there’s an adjustable input attenuator for each channel, which provides a minimum of 70.0 dB attenuation. There’s independent gain adjustment of the left and right channels in the spatial stereo mode, and independent gain adjustment of the left and right channels in the mono pseudo-stereo mode.

Theory of operation
The audio processor, whose schematic is shown in Fig. 1, is based on the Signetics/Philips TDA3810N stereo, spatial, pseudo-stereo processor IC. A block diagram of the chip is shown in Fig. 2. The device is essentially a system of internal op-amps used as active filters. The chip contains three op-amp stages, switching circuitry, power-supply regulation circuitry, and LED drivers.

The easiest way to understand how the chip works is to follow the audio signal through the chip for each individual mode.

Stereo mode
When the stereo mode is selected, the left input signal passes through input attenuator R14, and is coupled via C4 to pin 2 of IC1 (the TDA3810N). The right input signal passes through R15 and C3 to pin 17 of IC1. The various active filters within IC1 serve as a unity-gain bandpass filter with a −3 dB low-frequency cutoff occurring at 20 hertz, and the −3 dB high-frequency cutoff occurring well beyond 20,000 hertz.

Spatial mode
As shown in Fig. 3, when the spatial, or widened, stereo mode is selected, active op-amp circuits selectively remove certain parts of the audio spectrum. The effect is achieved by feeding the audio input to the non-inverting input of an op-amp. The inverting input is fed by the output of the internal buffer/amplifier coupled with a cross-channel signal through R2. Both channels operate in the same way. The gain of each channel can be adjusted independently: R3 adjusts the left channel and R1 adjusts the right channel.
FIG. 1—THE AUDIO PROCESSOR is based on the Signetics/Philips TDA3810N stereo, spatial, pseudo-stereo processor IC.

PARTS LIST

All resistors are 1/4-watt, 5%, unless otherwise noted.
R1, R3—50,000 ohms, panel-mount potentiometer
R2, R4—R6, R10—12,000 ohms
R7—25,000 ohms, panel-mount potentiometer
R8, R9—22,000 ohms
R11, R12—100,000 ohms
R13—R15—100,000 ohms, panel-mount potentiometer
R16—4700 ohms

Capacitors
C1—C5—0.1 µF, 50 volts, metal film
C6—0.033 µF, 50 volts, metal film
C7, C8—0.015 µF, 50 volts, metal film
C9—C11—100 µF, 16 volts, electrolytic
C12, C13—4.7 µF, 35 volts, electrolytic

Semiconductors
IC1—TDA3810N audio processor chip (Philips)
IC2—78L09 9-volt regulator
D1—1N4001 diode
LED1—LED3—light-emitting diodes (use three different colors)

Other components
S1—DP3T panel-mount switch
J1—2.1 mm panel-mount power jack (optional)

Miscellaneous: 18-pin IC socket, metal project case, 12-volt DC wall transformer (100-mA), 6 knobs, PC board, shielded cable, wire, solder, etc.

Note: The following items are available from HESC, PO Box 12649, Fort Wayne, IN 46864-2649:
- A kit of parts including a PC board and all parts that mount on it (does not include potentiometers, project case, or wall transformer)—$19.95 + $3.05 S&H
- PC board and TDA3810N—$14.95 + $3.05 S&H
- TDA3810N—$7.00 postage paid
Please allow 6 to 8 weeks for delivery.

Pseudo stereo mode

As shown in Fig. 4, when the mono pseudo-stereo mode is selected, the processor creates a “stereo” image using the various active filters differently on each channel. The left channel is fed through a flat-response amplifier (200 Hz to 20 kHz) to achieve a constant gain across the audio spectrum. The gain is adjustable via potentiometer R7, which controls feedback. The optimum setting recommended by Philips, the chip manufacturer, is +2.00 dB at 15 kHz; R7 gives an adjustment range of −69.0 dB to +6.0 dB at 15 kHz.

The right channel uses a twin-T notch filter to give the illusion of signal separation, or the pseudo-stereo effect. Between 100 and 1600 hertz, the notch filter attenuates the audio range by −33.0 dB at its lowest point, which occurs at about 450 hertz. The gain is adjustable by R13, which controls feedback. Philips recommends 0 dB at 15,000 Hz, although R13 gives a range of −68.0 dB to +6.0 dB. Figure 5 shows the frequency response of each channel.

Remaining circuitry

The TDA3810 contains a muting circuit with built-in hysteresis (controlled by C11) that prevents the status LEDs from flickering when switching from mode to mode. Also included is the mode selection switch (S1-a and -b) and the corresponding status indicators LED1, LED2, and LED3.

The project requires an external power supply of +10.5–24.0 volts DC, which passes through polarity-protection diode D1 to the input of IC2, a 78L09 +9.0 volt DC, 0.1-amp voltage regulator. Capacitors C1 and C2 provide decoupling and anti-oscillation protection for IC2.

Construction

Most of the parts for the audio processor are available from many electronics distributors. A foil pattern is provided if you want to make your own PC board, or you can use the board available from the source men-
FIG. 2—BLOCK DIAGRAM OF THE TDA3810N. The device contains three op-amp stages, switching circuitry, power-supply regulation circuitry, and LED drivers.

FIG. 3—IN THE SPATIAL STEREO MODE, active op-amp circuits selectively remove certain parts of the audio spectrum.

tioned in the Parts List.

Because this is an audio project, component tolerances and the matching of component values between the left and right channels is important. All resistors should be within 5 percent of the listed value, and it's a good idea to check them. Be sure to use high-quality capacitors, as poor-quality capacitors can adversely affect the overall frequency response of the circuit's processor.

Following the parts-placement diagram in Fig. 6 as a guide, install all resistors and capacitors, paying attention to the polarity of the electrolytics. Also mount diode D1, observing its polarity. Mount the 78L09 voltage regulator (IC2) with the flat side pointing toward the outside edge of the PC board. It's a good idea to use a socket for IC1, and you can install it now and then insert the IC. Observe the proper pin-1 orientation when putting the chip in its socket.

A metal enclosure will provide the best shielding from interference. However, a plastic box will probably be acceptable as well. Prepare the enclosure by laying out the front and rear panels for drilling. After drilling, deburr and clean the enclosure. The author mounted solder posts at each point on the board that must be hard-wired to another component. That made it easy to mount the board, jacks, and controls in the case, and then do the point-to-point wiring. Otherwise, all wires will have to be soldered to the board before mounting it in the enclosure. In either case, mount the completed PC board to the enclosure using appropriate hardware.

If you haven't done so yet, mount all of the potentiometers, jacks J1–J5, the LED's, and switch S1 to the enclosure. Then solder all cables and wires from the board to the jacks and controls. Following Fig. 6, pay careful attention to the places where shielded cable must be used. Hook-up wire can be used for all other connections. When connecting the feedback gain-control potentiometers (R1, R3, R7, and R13), wire them so their resistance increases as they are turned clockwise. Figure 7 shows the inside of the completed prototype.

Testing

When the project is complete, check all components for proper location and polarity, and also check your soldering. Using a DC voltmeter, check for the fol-
FIG. 4—IN THE MONO PSEUDO-STEREO MODE, the processor creates a “stereo” image using the various active filters in different ways on each channel.

FIG. 5—FREQUENCY RESPONSE of each channel in the mono pseudo-stereo mode.

FIG. 6—PARTS-PLACEMENT DIAGRAM. Pay attention to those controls that require shielded cable for connection to the PC board.

loowing voltages after applying power to the circuit:
Power-supply output—10.5–24 VDC
IC2 output—8.55–9.45 VDC
IC1 pin 1—4.2–4.8 VDC
IC1 pin 2—4.2–4.8 VDC
IC1 pin 3—4.2–4.8 VDC
IC1 pin 4—4.2–4.8 VDC
IC1 pin 5—4.2–4.8 VDC
IC1 pin 6—4.2–4.8 VDC
IC1 pin 13—4.2–4.8 VDC
IC1 pin 14—4.2–4.8 VDC
IC1 pin 15—4.2–4.8 VDC
IC1 pin 16—4.2–4.8 VDC
IC1 pin 17—4.2–4.8 VDC
IC1 pin 18—8.55–9.45 VDC

If all of those voltages are correct, the audio processor is ready to use.

Installation and use
If the audio processor is placed near a TV set and tends to pick up stray interference, move the processor around on the TV until the interference disappears. Also, be sure to use a well-filtered DC power pack or power supply to eliminate hum from the AC line.

Be sure all input and output cables are shielded. and well grounded to the PC board ground foil. Improper grounding can cause ground loops and other noise problems that are hard to track down. When the processor is to be installed between the TAPE IN/TAPE OUT jacks on a stereo system, hook it up the same way as if a tape deck were being installed.

Some stereo TV sets have line-level output jacks on them. In that case, all you have to do is install the audio processor unit between the TV’s output jacks and the stereo’s auxiliary or tuner input jacks.

If the audio processor unit will be installed between a speaker output and an amplifier input, the speaker output level must be reduced to a level that the audio processor can safely handle, which is a maximum of 2 volts rms. Always set the input-attenuator potentiometers to maximum attenuation before applying an input signal to the processor. Connect all mono audio sources to both of the inputs.

continued on page 82
HARDWARE HACKER

Nichrome and resistance wire, epoxy encapsulation myths, semiconductor suppliers III, FCC part-68 phone interface, and copy protection absurdities.

DIN LANCASTER

History often repeats itself, first as a tragedy and then as a farce. It sure amazes me how many hardware hackers and software types refuse to learn from the past.

For instance, over a decade ago, the Apple II community conclusively proved beyond a shadow of a doubt that copy protection does not work. Never did and never will.

Neither do hardware locks or similar add-ons. Yet many IBM-PC-compatible folks are hell-bent on wasting new time, dollars, and energy reproving this fundamental truth to themselves. You will find only three known effects of copy protection: (a) it annoys and inconveniences legitimate users, sending them all to unlocked competitive products; (b) it diverts time and energy that is best spent improving and updating your code; and, of course, (c) any copy protection dramatically increases the number of the bootleg copies of your product that get circulated.

The reason for (c) is simple. Copy protection always attracts attention to itself, causing scads of ultra-creative people to devote countless hours of time and amounts of energy toward cracking the secrets of your product.

The bottom line is this: Undoing copy protection is fun! Not only is the challenge fun, it is by far the fastest and most cost-effective way to learn machine-language programming. It’s also one of the best and the cheapest high-quality learning experiences you will find anywhere—and it’s a positively superb entertainment value.

For most hardware offerings, even grinding a part number off the key integrated circuit will have the exact opposite of the intended effect. All that does is cause lots of high-energy people to puzzle out what the chip is and where to get one. The universal hacker popularity for that BA1404 stereo FM broadcaster can be directly traced to one firm stupidly grinding off one too many part numbers.

By far the most absurd notion on hardware copy protection that has been resurrected is to...

Pot it in epoxy!

I simply can’t believe the number of calls and letters I’ve gotten on this lately. Back in the late 1950’s, it was conclusively seen that potting your circuits in epoxy offers no design security whatsoever. In fact, epoxy potting will always have the exact opposite effect.

First, any reasonably good design engineer could select a “black box” approach and carefully look at the inputs and outputs of the circuit. From the circuit’s size and cost, and from information in trade journals, data books, distributor’s catalogs, and ap notes, an engineer can easily come up with three or four methods to perform the same function—at least one of which will end up far cheaper, better, and more creative than yours.

Second, it’s a simple matter to x-ray any potted project—free even, if it’s a small module and you visit a reasonably curious dentist.

Third, most of the epoxy sources also supply epoxy strippers. These dissolve out the potting compound, cheaply, rapidly, and conveniently so it can be quickly washed away.

Fourth, epoxy could have several disruptive effects on your circuits. It changes the heat distribution and the operating temperatures of components. It can subtly detune polystyrene capacitors and its weight shifts mechanical resonances to more destructive frequencies.

Fifth, a very little-known fact: The ferrite RF beads used on typical high-frequency analog circuits must be able to change in size slightly or they will not work properly. The high-frequency energy gets absorbed by magnetostriction that, in turn, converts to heat. Locking ferrite beads in epoxy can alter their response.

Used with care, there are times and places where epoxy potting is an appropriate technique. Especially for water resistance or use in hazardous environments. But epoxy potting for copy protection just does not work.

Getting Nichrome wire

I’ve gotten several calls and letters recently asking for hacker sources for Nichrome wire. I’ll show you some sources and alternatives in just a bit. But please note that Nichrome is a trade name for a resistive alloy from Driver Harris Co. that can be drawn into wire or sputtered on a substrate.

Most often, you’ll want all of your electrical or electronic wiring to be very efficient, wasting as little energy and producing as little heat as possible. But there are other times and places when you want to cause a wire to intentionally generate heat or create a specific voltage drop.

Obvious examples include toasters, electric blankets, hot-wire plastic or foam cutters, laminating machines, space heaters, soldering irons, motor starters, thermal re-
lays, refrigerator defrosters, or for dummy transmitter loads. Some non-obvious places for carefully controlled resistance wire include current-meter shunts, and sensors that turn your printer on whenever you power your computer.

Most elements, alloys, and other materials are grouped into four types. Conductors can pass electricity fairly easily and have low resistances. Conductors can include both ordinary wire and resistance wire.

Semiconductors offer a moderately high resistance to electrical currents, with silicon and gallium arsenide being the most obvious examples. Insulators offer very high resistance to electrical current. Rubber, glass, plastics, and ceramics are typical insulators.

Superconductors can offer zero resistance to electrical currents. But most superconductors are complex formulations that work under special conditions at extremely low temperatures. You'll find more on superconductors in the Hardware Hacker II reprints.

<table>
<thead>
<tr>
<th>MATERIAL</th>
<th>RESISTIVITY measured in µΩ-cm</th>
<th>RESISTIVITY as compared to copper</th>
</tr>
</thead>
<tbody>
<tr>
<td>Aluminum</td>
<td>2.8</td>
<td>1.64</td>
</tr>
<tr>
<td>Brass</td>
<td>7.0</td>
<td>4.07</td>
</tr>
<tr>
<td>Constantan</td>
<td>44.1</td>
<td>25.60</td>
</tr>
<tr>
<td>Copper</td>
<td>1.7</td>
<td>1.00</td>
</tr>
<tr>
<td>German Silver</td>
<td>33.0</td>
<td>19.18</td>
</tr>
<tr>
<td>Gold</td>
<td>2.4</td>
<td>1.42</td>
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<tr>
<td>Invar</td>
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<td>47.00</td>
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<tr>
<td>Iron</td>
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<td>5.81</td>
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<tr>
<td>Magnesium</td>
<td>4.6</td>
<td>2.67</td>
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<tr>
<td>Molybdenum</td>
<td>5.7</td>
<td>3.31</td>
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<tr>
<td>Music wire</td>
<td>11.8</td>
<td>6.96</td>
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<tr>
<td>Monel</td>
<td>42.0</td>
<td>24.40</td>
</tr>
<tr>
<td>Nichrome</td>
<td>150.0</td>
<td>57.20</td>
</tr>
<tr>
<td>Nickel</td>
<td>7.8</td>
<td>4.53</td>
</tr>
<tr>
<td>Platinum</td>
<td>10.0</td>
<td>5.81</td>
</tr>
<tr>
<td>Silver</td>
<td>1.6</td>
<td>0.95</td>
</tr>
<tr>
<td>Tantalum</td>
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<td>9.01</td>
</tr>
<tr>
<td>Tin</td>
<td>11.5</td>
<td>6.69</td>
</tr>
<tr>
<td>Tungsten</td>
<td>5.5</td>
<td>3.20</td>
</tr>
<tr>
<td>Zinc</td>
<td>5.7</td>
<td>3.34</td>
</tr>
</tbody>
</table>

Fig. 1—The resistivity of any material is defined as the face-to-face electrical resistance of a unit cube. Here are several resistivity values for some of the more widely used metals and alloys.

Take a one-centimeter cube of any element, alloy, or material. Next, apply a voltage from full face to the opposite full face. Then measure the current. By Ohm’s Law, the ratio of the voltage to current determines the resistance of the cube. But we have a special name for the resistance of a unit cube. This is the resistivity, and is identified ρ, the Greek letter rho.

The resistance of a wire increases with its length and decreases in proportion to area. The metric resistivity units are ohm-centimeters (ohm-cm). I’ll use a wonderfully oddball unit of microOhm-centimeters (µΩ-cm) here so our numbers look nicer.

Resistivity values let us compare materials independent of their actual sizes. Some popular resistivity values are shown in Fig. 1, while Fig. 2 shows you how much resistance you can expect for various wire sizes of selected materials.

The lowest resistivity of common elements or alloys is silver, checking in at 1.6 µΩ-cm. But silver is fairly rare and readily tarnishes, and the commodity price of silver changes all over the lot. So, silver isn’t used too much except for RFI suppression microwave equipment, and exotic military stuff.

Copper, of course, is the universal choice for a conductor. It has a resistivity of a mere 1.7 µΩ-cm—only five percent worse than silver.

At first glance, aluminum appears almost as good as copper, having a conductivity only 64 percent worse. In theory, the thicker but cheaper and lighter aluminum conductors could be substituted.

But aluminum has a pair of nasty habits which include electrochemical decomposition and the building up of sapphire-hard (literally!) oxide coatings. Making a solid connection to an aluminum wire is not a trivial task. Several decades ago, a bunch of house trailers burned up after some abortive attempts at trying to perfect aluminum wiring.

Most of the other popular elements and alloys have resistivities that are moderately higher than copper. But a magic alloy of 61 per-
cent nickel, 24 percent iron, and 15 percent chrome provides a resistivity over fifty times higher than copper. When combined with its other useful properties, this Nichrome alloy makes an outstanding resistance wire.

Figure 2 shows you how much resistance to expect for various wire sizes for each of these materials. A foot of 20-gauge Nichrome wire has a resistance of 0.659 ohms. The same alloy in 30-gauge provides around 6.75 ohms total.

Resistance wire gets measured in ohms per thousand feet. Or you may prefer its equivalent of milli-ohms per foot. Naturally, resistance wire works just like any other resistor, obeying Ohm’s law and the usual P = E²/R power relations. A watt of electricity is, of course, a watt of heat. And a BTU of heat equals 17.58 watts. So you can easily calculate the amount of heat. BTU or British Thermal Unit is the amount of heat needed to raise the temperature of one pound of water by one degree Fahrenheit.

<table>
<thead>
<tr>
<th>MATERIAL</th>
<th>10 gauge</th>
<th>20 gauge</th>
<th>30 gauge</th>
<th>40 gauge</th>
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</thead>
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<tr>
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<td>169</td>
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<tr>
<td>Brass</td>
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<td>41</td>
<td>419</td>
<td>4260</td>
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<td>Constantan</td>
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<td>260</td>
<td>2640</td>
<td>26800</td>
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<tr>
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<td>1</td>
<td>10</td>
<td>103</td>
<td>1050</td>
</tr>
<tr>
<td>German Silver</td>
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<td>194</td>
<td>1970</td>
<td>20100</td>
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<tr>
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<td>141</td>
<td>1480</td>
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<td>Invar</td>
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<td>477</td>
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<td>49300</td>
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<tr>
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<td>3</td>
<td>27</td>
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<td>2800</td>
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<td>Molybdenum</td>
<td>3</td>
<td>34</td>
<td>341</td>
<td>3470</td>
</tr>
<tr>
<td>Music wire</td>
<td>7</td>
<td>70</td>
<td>706</td>
<td>7180</td>
</tr>
<tr>
<td>Monel</td>
<td>24</td>
<td>247</td>
<td>2451</td>
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<tr>
<td>Nichrome</td>
<td>65</td>
<td>659</td>
<td>6750</td>
<td>70240</td>
</tr>
<tr>
<td>Nickel</td>
<td>5</td>
<td>46</td>
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<td>4750</td>
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<tr>
<td>Platinum</td>
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<td>59</td>
<td>598</td>
<td>6080</td>
</tr>
<tr>
<td>Silver</td>
<td>1</td>
<td>10</td>
<td>98</td>
<td>991</td>
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<td>91</td>
<td>928</td>
<td>9430</td>
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<td>Tn</td>
<td>7</td>
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</tr>
<tr>
<td>Zinc</td>
<td>3</td>
<td>33</td>
<td>344</td>
<td>3450</td>
</tr>
</tbody>
</table>

Values in milli-ohms per foot—or—Ohms per 1000 feet.

Fig. 2—Some typical resistance values for different materials and wire gauges.

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Other resistance-wire variables include the tensile strength, the temperature coefficient of resistance, and the temperature coefficient of expansion. The resistance-temperature coefficient gets important fast in such things as meter shunts. The expansion temperature coefficient becomes crucial if the wire passes through some ceramic seal. Should the wire and the ceramic expand at different rates, one or both can self destruct at high temperatures.

The fastest and simplest way to get some Nichrome wire to play with is to gently crush up a surplus power resistor in a vise and unwind the wire. Different sizes offer different lengths and gauges of wire. Resistance wire often ends up at surplus stores at bargain prices, especially at Fair Radio Sales. American Science and Surplus also offers cheap resistance wire originally intended as refrigerator defroster elements.

One big supplier of new resistance wire is MWS Wire Industries. Its equivalent to Nichrome is known as MWS-675. It also offers two dozen other variations. Its MWS-875 provides even higher resistivity with better temperature coefficients for both resistance and expansion. This alloy includes chrome, aluminum, and iron, with traces of carbon and silicon. It is also slightly lighter in weight.

By the way, other trade names for alloys similar to Nichrome are Trophet C, Alloy C, HAI-NiCr60, Chromel C, Nikrothal 6, and Electrolyt.

For this month’s contest, just tell me about a new or unusual hacker use for resistance wire. There’ll be all of the normal Incredible Secret Money Machine II book prizes, along with an all-expense-paid (FOB Thatcher, AZ) tinaja quest for two going to the best submission of all.

As usual, send your written entries to me here at Synergetics and not to the Electronics Now editorial offices.

A hacker interface

In several past columns, we have looked at the FCC Part 68 Interfaces. These are required any time you want to put voice, music, caller-ID data, or modem tones on or off of the phone line. The key component needed is just a fancy transformer with a high isolation voltage rating, a very good balance, and the ability to accept DC primary current.

There are lots of dollars, time, and effort needed to get an interface FCC type approved. And it is now illegal to make any connection to the phone line without going through an FCC approved, Part 68 interface. At least in the U.S.

Several firms now offer “pass through” interfaces that you can include within your own circuits to get an instant and automatic type approval. The two major suppliers are now Cermetek and Dallas Semiconductor. Sadly, their pricing has been too high for most hacker uses.

A startup outfit by the name of CircuitWerkes is now offering a new and hacker-friendly Part 68 interface at an acceptable price of $29.95. And yes, it offers a full type-approval pass through. It’s subject to only a few easy rules that involve component spacing, labels, documents, and modifications. Figure 3 shows you the circuit.

A small relay makes the on-hook and the off-hook state connections. To “seize” or “answer” the line, apply 12 volts DC to the relay, providing 60 milliampere.

The ring-detector circuit is active only when on-hook. It consists of a optoisolator that responds to the high AC ringing voltage (typically 140 volts at a frequency of 28 to 40 Hertz). The output of the ring detector is an open collector. You’ll have to provide both an external pull-up
resistor and a filter capacitor to ground. Suitable values are 12,000 ohms and 5 microfarads.

The main data path is active both on- and off-hook. This dual feature is needed for a caller-ID compatibility. When you are on-hook, the data path is capacitor-coupled.

When off-hook, the data path is DC-coupled through the transformer primary. A second optoisolator in parallel with the primary acts as a line-current detector. The line current is detected by monitoring the DC voltage drop across the primary.

The line-current detection lets you know when your calling party hangs up. The optoisolator also offers open-collector output. A pull-up resistor is also required here.

The main data path is a special transformer with two clipping diodes that limit the maximum applied audio. A jumper option allows you to select a balanced or single-ended 600-ohm source/sink for your audio output.

Typically, your computer will first monitor the ring detector. After a ring, it seizes the line and optionally grabs the caller-ID tones. Then it will send or receive your voice or data. Finally, you can hang up by causing the relay to drop out—either by detecting the absence of line current or by hanging up on purpose.

As a second contest for this month, just tell me about a new or unusual application for a hacker-legal Part 68 interface project.

Much more information on those caller-ID applications appears in a dozen files on my GEnie PSRT.

More semiconductor resources

We will wrap up our continuing listing of the major semiconductor houses in a third and final sidebar. This month, we will cover OKI up through Zilog. I've tried to zero in on those suppliers with the greatest hacker interest.

A complete list will appear in the Hardware Hacker IV reprints. I've also gathered them together into the ICMFGRS PS download you'll find on GEnie PSRT.

As we have seen before, your best bet here is to request a short-form catalog, the price list, and a literature directory. Be absolutely sure to use professionally sound phone calls or your own custom PostScript laser letterhead. A ball-point pen on tablet paper flat out won't hack it. Much more on finding and using technical information is in my newly revised Incredible Secret Money Machine II.

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new publications for this month. The first is Dick Oliver's new Nonlinear Nonsense, a free quarterly newsletter on fractal modeling, chaos science, artificial life, and creative graphics. His 3-D fractal design software is also being offered commercially.

Also free on professional request is the new Spread Spectrum Handbook from Stanford Telecom. This is a dozen pages of ap-notes and useful references, along with bunches of data sheets for the company's high-end digital spread-spectrum chips.

The Scrambling News has detailed insider information on the current TV video scrambling and descrambling methods. It also offers books full of schematics, modifications, and related technical information. A competing newsletter is the Satellite Watch News.

The SRS Encoder is a new monthly newsletter from the Seattle Robotics Society. Lots of regional information on great surplus buys are included here.

Joe Singer's Printer's Devil is a superb alternative publication on home printing and presswork. "A press in every home: a home in every press." It is published quarterly at a bargain $10 per year subscription price.

Finally, the New Age Alternatives Discount Catalog is another resource for pseudoscience devices and information. Fascinating reading for sure. This one is offered by Lor'd Industries.

A reminder here: I have reprints available for most of my columns. Both in Book-on-demand published hard copy and on-line at GENIE PSRT. The titles now include my Ask the Guru, Hardware Hacker, the Blatant Opportunist, LaserWriter Secrets, and the new Resource Bin. Check my nearby Synergetics ad for more details.

As usual, I have gathered most of the mentioned resources together into our Names and Numbers and Semiconductor Manufacturer's III sidebars. Also, as usual, you can get technical help, consultant referrals, and lots of off-the-wall networking by calling my helpline. ☜

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In the stereo mode, the only adjustments are the input-attenuator controls (R14 for the left and R15 for the right). For a line-level input, set them for 0 attenuation. Other higher-level sources should be adjusted as desired by the user (without exceeding the 2-volt rms maximum input limit).

In the spatial stereo mode, the input attenuator controls should be adjusted the same way as in the stereo mode. The spatial controls (R3 for the left and R1 for the right) can then produce very interesting spatial effects. Also, adjusting the input-attenuator controls produces interesting effects due to the cross-channel coupling provided by resistor R2. Experiment with those four controls to determine their optimum settings.

In the mono pseudo-stereo mode, the input-attenuator controls should be adjusted the same way as in the stereo mode. The pseudo stereo controls (R7 for the left and R13 for the right) should be set as follows: R7 should be set to give a +2.0 dB higher output level versus the right output channel control (R13). For example, set R7 for an output of +2.0 dB, and set R13 for an output of 0 dB. The specific levels are not critical; just keep a 2.0 dB differential between the left and right output channels.

When using a mono input source, the spatial stereo mode will produce some very interesting and useful effects. The input attenuator controls will also have interesting effects.

**FIG. 7—A METAL ENCLOSURE provides the best shielding from interference. Here's the inside of the completed prototype.**

**FOIL PATTERN for the audio processor.**
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remote control and sends it to one gate of a CMOS 4014 non-inverting hex buffer. The output from the buffer drives an LED that flashes the received signal to let you know that the remote control (or at least the one button you pressed) is working and emitting an IR signal.

We’ve provided a foil pattern to make a PC board for this project, but the circuit can easily be made using point-to-point wiring. Figure 2 shows the parts-placement for the PC board, should you decide to use it. The completed circuit can be installed in any suitable case. Mount the IR phototransistor where it can easily receive the IR signal, and mount the LED where it’s easy to see. A 9-volt battery powers the circuit, but you can certainly build an AC-powered supply if you wish.

Once constructed, the tester will determine if your remote control is causing the problem. Simply point the remote control at the IR phototransistor, and press each button. The LED will flash for proper operation.

COMING NEXT MONTH
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AND LOTS MORE!
Here is another collection of helpful (or at least interesting) audio questions and answers from reader mail and my files.

**Audio education**

I’ve been intensely interested in music recording and audio technology ever since my early teens. At this point, I’m seriously considering entry into the audio field in a professional capacity. Where can I get information about my options and the educational requirements?

T.M.

Norwalk, CT

You’re in luck. A definitive *Directory of Educational Programs* has been published by the Education Committee of the Audio Engineering Society (AES) that covers courses ranging from seminars to four-year graduate programs that grant degrees. Institutions, facilities, courses, degrees, and tuition are listed in a convenient format.

As a bonus, there are helpful articles that discuss the variety of job opportunities within the field and ways to approach the education process. The postpaid cost of the directory is $5 for AES members, $6 for nonmembers. Delivery is 4 to 6 weeks. Send your check to Audio Engineering Society, 60 E. 42nd St., Room 2520-RE, New York, NY 10165. While you are writing, you might also ask for an AES membership application.

**Flat sound**

Recently I told a friend that I built my own speakers from scratch. To my annoyance, he immediately asked, “How flat are they?” Are we getting so wrapped up in specifications that we forget the basic goal—good sound the way we like to hear it? I spent over 50 hours reworking my ported speakers so I could have a lot of bass—the way I like it. Don’t get me wrong; specs and test reports are definitely helpful, but keep in mind that I’m spending money to have sound the way I want to hear it—not as some expert says it should be heard.

P.W.

Rochester, NY

If P.W. had written about choosing the paint color for his new kitchen walls or selecting a blend of coffee—or a wife—I would not argue with the subjectivity of his approach, although my own tastes would probably differ. Everyone has a right to his own tastes—however absurd they might be. I assume you are using “good” in the sense that it satisfies you. However, when the goal is to reproduce a recorded sound, then the system that’s doing it must not add any special sound characteristics of its own. If P.W. prefers speakers that readjust the original tonal balance of the program material in a given direction, that’s his privilege. But I must point out that his speakers, by definition, are then not providing high-fidelity reproduction. Theoretically, fidelity to some original is what hi-fi is all about.

**Planned obsolescence**

I use my audio equipment at least four hours a day, and next year my receiver will be 10 years old. How does wear affect audio equipment, and how long will it be before planned obsolescence sets in?

H.S.

Elliston, VA

Congratulations to your receiver on its 10th birthday! Before I answer your question on wear, I’d like to discuss “planned obsolescence,” a term that seems to be fading from popular use. Actually, the alleged practice that the term describes never did make much sense; what most people really meant by it was planned deterioration. In other words, certain parts or components in a device supposedly were designed to have both a short life and a high replacement cost, thereby encouraging the purchase of a new replacement. But it seems to me that the ill will engendered by premature breakdown would cause consumers to avoid the faulty brand when considering a replacement—thus defeating the purpose of the alleged planned obsolescence.

The loudest complaints of planned obsolescence usually occur when a new audio format threatens to render obsolete someone’s treasured collection of program material. For example, the industry switched from 78 rpm’s to LP’s, LP’s to cassettes, and then cassettes to CD’s. The obsolescence in those cases was, truthfully, planned to obtain higher fidelity—or in the case of cassettes, greater convenience—for the music collector and listener.

The general public (unlike some of the audio magazines and syndicated columnists) does not automatically extend a warm welcome to every new trend in audio. Witness, for example, the marketplace fiascoes of such components as the “elcassette” and, lately, DAT. I suspect that there are other fiascoes of the digital variety now waiting in the wings.

In regard to your question about wear, solid-state devices, unlike high-power vacuum tubes, do not have an inherently short life. This is not to say that transistors never fail, but rather that their predicted life span extends far beyond that of tubes. Because of minute manufacturing flaws, small-signal transistors (and integrated circuits) can develop leakage over time, and power devices ultimately can flex themselves to death from repeated heat-
ing and cooling cycles during normal use. Other components, such as electrolytic capacitors, fail over time for a variety of mechanical and electrochemical reasons.

**Whizzers**

I’m curious about the speakers installed in the lower front-door panels of my car. I removed the grille from one of the speakers and found it to have a single gray 6-inch cone with a separate small white cone cemented to its center. Does the smaller cone serve as a tweeter?

**D.C.**

Lancaster, PA

Sort of, but not really. What you’ve described is known as a “whizzer,” and its purpose is to enhance the high-frequency sound from your speakers. A whizzer is a small, light, and stiff subsidiary cone with an unsupported outer edge that is cemented to the center of the main cone. The area of attachment is directly over the driver’s voice coil. The whizzer picks up the high-frequency vibrations from the voice coil, and helps to send them out into the world as sound.

**X-ray problems**

Despite the printed reassurances posted at the passenger inspection areas of airports, I’ve always tried to keep my films and tapes from being X-ray inspected. I recently heard that color TV sets can also produce X-ray radiation. How far away from my TV should I keep my audio and video tapes to be safe, or will it not make a difference?

**M.O.**

Burlington, VT

As far as I can determine, X-rays at the levels used in baggage examination have no effect on tapes or the signals recorded on them. It’s true that the stray magnetic fields produced by X-ray equipment and color TV cathode ray tubes might affect a recorded signal, but one expert told me that the tapes would have to be stored inside the operating equipment in close proximity to a transformer or deflection coil before an erasure is likely to occur. However, metal detectors, also used in airports, can be hazardous to the health of your recorded tapes.

**Parameters**

“Parameter” seems to have become a new catchword among those involved with politics and/or the Pentagon. Is “parametric” derived from the same word, and exactly what does it have to do with equalizer design?

**J.H.**

Chevy Chase, MD

My copy of Webster’s dictionary defines parameter as “A (mathematical) quantity or constant whose value varies with the circumstances of its application, as the radius line of a group of concentric circles, which varies with the circle under consideration.” The adjectival form is “parametric.” In other words, a parametric equalizer does not limit you to the specific built-in fixed operating frequencies and bandwidths of a conventional graphic equalizer. Instead, you can assign “arbitrary values” as the equalization needs arise. This can be very handy, for example, when the frequency of the peak that you want to reduce doesn’t line up very well with one of the sliders on a standard 1/2-octave graphic equalizer.

**Q&A**

continued from page 12

graphics image. The second, less expensive alternative is to print at 150-dpi resolution—half the number of dots means half the memory requirements. If you can live with the lower resolution, the latter is a cheap, quick fix for the problem.

There’s one more possible answer to your problem but I doubt that it’s applicable. It may be that you have enough memory in the printer to do 300-dpi, but you’re using the memory to hold downloaded fonts and other things. Remember that memory used for fonts isn’t available for graphics. Check your software (and not just the graphics stuff) to see whether this is true or not. If it is, unloading the fonts may free up enough printer memory to permit you to print graphics at the maximum 300-dpi resolution.

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Believe it or not, there’s not a lot more to the design of the basic descrambling circuit than the subject matter we’ve covered over the past few months. But if you’re really interested in video, there’s much more for you to learn—the video-scrambling stuff we’ve been going through is just one small part of the subject. Video is a complex business, and once you get the hang of how signals can be manipulated, you’ll find that there’s no end to the kind of circuitry you can design. There’s also a huge market for it as well. But back to the subject at hand.

When we first started work on the SSAVI descrambler, the block diagram probably looked quite complex. But if you look at Fig. 1, you’ll see that most of the work has been done. The most difficult job left for us is to come up with the counter that’s needed by the phase-locked loop. It’s a job we have to do carefully because the success of the descrambler depends on how well we can maintain the stability of the horizontal-sync signal.

The phase-locked loop in our design is driven by a 504-kHz clock based on an R-C network. That frequency was chosen for two basic reasons: The first is that it’s exactly 32 times the NTSC line frequency of 15,750 Hz, and that makes it easy for us to do the division necessary to produce horizontal sync pulses. The second, and somewhat more subtle reason, has to do with the period rather than the frequency.

A 504-kHz clock has a period of 1.98 microseconds. That’s interesting because, by using five of the counts, we can get a pulse that has a width of 9.92 microseconds, which is close enough to the NTSC’s established standard of 10.7 microseconds for a horizontal blanking pulse.

Before we go any further, I have to comment on my apparent disregard for precision. I’ve been using language and design techniques that are loaded with phrases like “close to,” “pretty much the same as,” “in the ballpark,” and so on. Now, I’m amazed at how sloppy the signal really is. The average horizontal frequency might be 15,750 hertz, but there’s considerable jitter from line to line in the signal. The same is true for burst, blanking, and all the other components in the line.

Despite these variations in the signal, the picture that shows up on your TV screen is apparently unaffected by them. The difference be

![Diagram](https://www.americanradiohistory.com/magazine/1983/87.png)

**FIG. 1—MOST OF OUR BLOCK DIAGRAM has already been turned into actual circuitry.**

Now we need a counter for the phase-locked loop.
The 4040’s clock input is fed with the 504-kHz signal generated by the 4046, and we’re using a series of gates to decode the count and provide horizontal blanking and some other timing signals needed for the descrambler. The actual circuit is shown in Fig. 3. You should understand why each of these signals is needed before you start hooking everything up to the back of your TV set. To see what we need from the counter, let’s use it to restore horizontal sync and then figure out what else we need to completely unscramble the incoming video.

Getting a horizontal sync clock for the phase-locked loop circuit is simple. All we have to do is pick off the Q4 output. That is a divided-by-32 version of the input clock from the phase-locked loop’s 504-kHz oscillator and, as shown, it’s fed back to pin 3 of the 4046. Now that the phase-locked loop is provided with a constant reference signal, it will accurately generate sync pulses—even when they’re not sent along with the transmitted video.

The remaining problem to deal with is turning off the generated sync pulses during the vertical interval when real transmitted sync is present. (Remember that the video isn’t scrambled during the vertical interval.) To do that, we have to count the lines of video as they’re received and make sure that transmitted sync is processed for the first 26 lines of each frame. The starting point for the count is the vertical sync signal and, as you recall, we’ve already isolated the signal. The sync separator we built earlier produces a positive-going version of vertical sync. If we use the rising edge of that signal as the zero point for the counter, we have to count a number of lines to reach the point where the lines of video are carrying picture information and are therefore scrambled.

The two lines in the frame that mark the beginning and end of the transmitted horizontal sync are 260 and 27, respectively. We need a circuit that can count the received lines and let the rest of the descrambler know when to use received horizontal sync and when to use the artificial sync generated by the phase-locked loop. The zero point for the counter will be the rising edge of our vertical sync signal. Since that occurs at line 3, we have to decode a count of 24 and 257.

We can use a 4040 to do that job as well. This is the same sort of counter decoding we’ve done before in this project and others. When the counter reaches 24 we have to enable a gate that will send thephony horizontal sync pulses to the video amplifier at the circuit’s input. When we get to a count of 257, the gate has to be disabled to let the real horizontal pulses through to resync the phase-locked loop circuit.

Decoding those two numbers is a pain in the neck since it involves watching nine counter lines. You can do that with a bunch of gates, but a better way is to use an EPROM. The choice is yours although, if you haven’t had much experience in this sort of decoding, it’s probably a good idea to work out the logic and build the decoder with gates. Otherwise an EPROM is the way to go. Assuming, of course, that you have programming capabilities.

When we get together next time, I’ll give you the truth table for the EPROM and we’ll finish off the descrambler. All that’s left is a couple of flip-flops, a bit of work on the video section, and a way to detect the presence of normal or inverted video. Simple stuff!
FET's

continued from page 56

to handle higher currents. As majority-carrier devices that store no charges, they can switch faster than bipolar power transistors.

Figure 12 is a section view of an N-Channel, enhancement-mode power MOSFET. Unlike its small-signal counterpart, the latest power MOSFET's are fabricated with vertical rather than planar structures. They are made with the double-diffused (DMOS) process, and they have conductive silicon (polysilicon) gates. The gate of this device is isolated from the source by a layer of insulting silicon oxide.

When a voltage is applied between the gate and source terminals, an electric field is set up within the MOSFET. This field alters the resistance between the drain and source terminals, and it permits conventional current to flow in the drain in response to the applied drain circuit voltage. There are also P-channel, enhancement-mode power MOSFET's in which conventional current flows in the opposite direction of the N-channel device. Figure 13 is the schematic symbol for a DMOS enhancement-mode, N-channel power MOSFET.

Figure 14 is a cutaway view of a typical DMOS power MOSFET. It is made up of many cells or transistor elements connected in parallel. Each source cell consists of a closed rectangular or hexagonal channel which separates a source region from the substrate drain body. The cells are formed in an integrated circuit process, and there might be more than a half million cells per square inch of substrate. All of the source cells are connected in parallel by a continuous deposition of aluminum metalization, which forms the grid-like common-source terminal.

The DMOS power MOSFET contains an inherent PN junction diode, and its equivalent circuit can be considered as a diode in parallel with the source-to-drain channel, as shown in the schematic symbol of Fig. 13.

International Rectifier (IR) makes DMOS power MOSFET's that have hexagonally shaped cells, so it calls its products HETFET's. Motorola Semiconductor also offers DMOS power MOSFET's, but its devices have rectangular rather than hexagonal cells. Motorola named its power MOSFET's TMOS to call attention to the T-shaped current flow that occurs in the cells between the common drain and the channels to the multiple sources.

Power MOSFET's are widely specified for high-frequency switching power supplies (generally those that switch at frequencies above 100 kHz), AC and DC motor speed controls, high-frequency generators for induction heating, ultrasonic generators, audio amplifiers, and amplitude modulation transmitters.

The advantages to using power MOSFET's over power bipolar transistors include:

- Faster switching speeds and lower switching losses.
- Absence of the bipolar's second breakdown
- Wider safe operating area
- Higher input impedance
- High, if not higher, gain
- Faster rise and fall times
- Simple drive circuitry

The principal disadvantages of power MOSFET's are their higher cost and a higher static drain-to-source on-state resistance, which can cause unacceptable power losses in certain switching applications. However, the manufacturers have made progress in reducing those resistance values. DMOS geometry has largely replaced the V-groove or VMOS process that was widely used to fabricate power MOSFET's back in the 1970's.

Radio-frequency power MOSFET's are now available that will operate over the 2 to 200 MHz frequency range. The high power and high gain of these devices makes them suitable as power amplifiers in solid-state transmitters for FM and TV broadcasting.
1992 drew to a close with some of the most exciting developments in the PC industry in years. There is no single overarching product or technology, but lots of little bits and pieces that together point to the emergence of a new class of personal computers with unprecedented power, versatility, and connectivity. Core technologies include powerful and upgradeable CPUs, general-purpose digital signal processors (DSP's), rapid acceptance of local buses and corresponding decrease in the ISA/EISA/MCA bus wars. Other trends involve accelerated true-color graphics, motion video compression and decompression, drastically reduced power consumption, increased semiconductor and magnetic storage, full-featured operating systems, built-in local-area network connectivity, 100-MHz + LAN speeds, and wireless cellular networking.

PC architecture

During the past year, the 486 has quickly surged ahead of the 386 as the platform of choice. Spurred on by competition from Cyrix, AMD, and others, Intel has released a wide variety of 486-based devices, with many more to come. Prime features of all include low power and performance enhancement through clock-doubling—and tripling, as demonstrated by IBM recently—technology. The clock doublers have been well received, even though pricing continues to hover near that of full motherboard upgrades that provide better performance.

And speaking of Intel, you may think of the company primarily in terms of CPUs, but during the past few years, Intel has stuck its corporate thumbs in numerous pies—and has come out holding several juicy plums. Of course, there are the CPU's. There is also video-compression technology, exhibited first as the Digital Video Interactive (DVI) boards for digitizing and displaying full-motion video on desktop computers. Part of DVI is Real Time Video (RTV), which Intel has ported from the i750 video processor to the 386D/486/Pentium architecture, and now calls Indeo. Indeo is one of the compression algorithms included as part of Microsoft's Video for Windows; Indeo is also being supported by Apple's QuickTime, and by IBM's recently announced Ultimotion. As discussed here in the preceding few months, software-only video is gimmicky, but an important first step in computer video.

Then there are network cards; Intel's cards are highly regarded, and are available for extremely competitive prices. Next come faxes and modems. Intel's SatisFAXion 400 is the highest-performing general-purpose modem and fax card combination on the market, although its bundled software leaves something to be desired. And let's not forget about PC integration chip sets, especially the upcoming Peripheral Component Interconnect (PCI) devices that will provide a standard local-bus architecture for 32- and 64-bit microprocessors. PCI-based systems should start appearing about the time you read this.

Of course, PCI is not the only kid on the block; a competing standard is the VL bus, named after the Video Electronics Standards Association's local bus. Both VL bus and PCI provide high-performance links between a CPU and its peripherals (such as network, video, and disk controller cards). In the words of one industry analyst, VL-bus seems to be better supported by expansion-card manufacturers, and PCI by systems developers. Despite the lack of accepted standards, local-bus video is catching on. At last fall's Comdex, the computer industry's leading trade show, numerous video-card manufacturers announced VL-Bus products, including ATI, Cardinal, Genoa, Matrox, VideoLogic, and VidTech. Nonetheless, Intel's influence should not be underestimated. It will probably take 18–24 months for VL bus or PCI to emerge as a clear victor; in the meantime, both will be well supported by many manufacturers. One irony of all this is that the ISA vs. EISA vs. MCA bus war initiated with IBM's April 1987 introduction of the PS/2 line has become moot. The traditional expansion bus will be relegated to mouse, modem, and other low-speed devices.

The emergence of Windows (and to a lesser extent OS/2) has driven video card manufacturers to unprecedented levels of price/performance in just a few short years. Little more than two years ago, high-speed, high-resolution, high-color (24-bit) cards were available only on coprocessor-based boards, with prices beginning around $1000. Today, you can get "accelerated" video adapters that provide 80% of the performance for 20% of the price of the coprocessed boards.

High-resolution monitors have also fallen in price, but not nearly as much as required. In addition, screen sizes greater than 16 inches invariably mean bulky, heavy, power-hungry devices. The monitor remains the weakest overall component of today's computer system.

One area of potential concern is semiconductor memory. The U.S. Department of Commerce recently instituted import duties on memory chips from several Korean manufac-
urers; street prices have already risen 25–30%. The DoC is expected to make a final ruling in early spring about whether those manufacturers are "dumping" chips below market value. If so, growth of Windows, OS/2, and corresponding applications software will likely slow. On the other hand, IBM and other manufacturers have started shipping 16-Mbit DRAM's on various systems. Clearly, the day of 16-, 64-, and 128-megabyte systems is not far off.

Digital-signal processing is poised to change dramatically the way PC's deal with analog data. Texas Instruments recently introduced a DSP chip and several corresponding boards that provide fax, modem, sound synthesis, speech-recognition, and data-compression capabilities. If this chip were made a standard part of every motherboard, it would eliminate the need for dedicated fax, modem, sound, and compression boards.

**Pervasive networking**

It won't be long before every desktop and portable PC, Macintosh, and workstation comes with built-in network capability. Chips & Technologies and Standard Microsystems have joined AMD, Artisoft, and National Semiconductor in the market for low-cost, single-IC Ethernet interfaces. These devices provide a complete network interface in a $20 package (in lots of 1000+ pieces). Zenith Data Systems was the first to include a built-in Ethernet port, but other manufacturers are following suit.

In the local-area networking arena, Microsoft released Windows for Workgroups (WfW), a version of Windows with built-in peer-to-peer networking. Although not as robust as market leader Lantastic, WfW has built-in scaled-down versions of Microsoft's widely regarded E-mail and group-scheduling applications. The main thing lacking is a DOS client (i.e., it is not possible to attach to a WfW server from a DOS-only machine). However, Microsoft will sell one separately, and may well bundle it with the forthcoming DOS 6.0, which will also include antivirus, disk-compression, and robust backup utilities. That should further squeeze Symantec/Norton and Central Point Software, providers of popular utility programs. WfW will not likely displace large NetWare (or other brand) LAN's. Microsoft appears to be targeting first-time network users and corporate workgroups with traditional client-server systems (e.g., NetWare) that also need peer-to-peer services.

Wireless networking is on the verge of exploding. There was a burst of interest on this subject at Fall Comdex. For example, two leading computer companies (IBM and Apple) have teamed up with several cellular telecommunications providers (McCaw, Ram Mobile Data, Ardis—itsself a joint venture between Motorola and IBM—and others) to support Cellular Digital Packet Data, a way of delivering digital data (e.g. E-mail) to one or more recipients anywhere, on demand, and in real time. IBM, Apple, Motorola, and a startup called Eo demonstrated various notebook computers, stylus-input devices, and personal digital assistants (PDA's) performing CDPD activities with attached cellular modems and cellular telephones.

**Portables and printers**

More manufacturers are supporting the PCMCIA (Personal Computer Memory Card Industry Association) standard. One vendor has gone so far as to call PCMCIA the ISA bus of the 90's. PCMCIA is not, however, without problems. The technology has gone through several fairly rapid evolutionary stages, PCMCIA 1 and PCMCIA 2, the latter being the current version. PCMCIA 1 was originally designed for memory expansion; but the idea of credit-card-size expansion devices quickly caught on and was expanded. IBM, for example, recently introduced several products called Credit Card Adapters that provide Token Ring and Ethernet connectivity, and 3270 terminal emulation. Other vendors also provide fax and modem adapters.

The technology has evolved more rapidly than the standards, so there is a potential for incompatibilities. To help avoid those problems, Intel developed an enhancement to PCMCIA 2, the Exchangeable Card Architecture (ExCA), which appears to be catching on. In addition to basic PCMCIA 2 compatibility, ExCA addresses several other issues, including the use of multiple cards in a system, and hot swapping (the ability to insert and remove cards with power on). Caveat emptor if you plan to buy new systems with PCMCIA expansion capabilities.

On the other hand, pen-based computing (as discussed here in the February 1992 issue), has taken off much slower than expected. Originally, the industry expected to see significant activity by the end of 1992, but now it looks as if little will happen before late 1993. However, as one manufacturer puts it, "The timing for our projections was off—not the projections themselves."

Hewlett-Packard has once again created a ground-breaking product: The LaserJet IV. It is a true 600-dots per inch laser printer, with street prices starting around $1300; for PostScript, add about $500. You don't have to look twice to see the difference between 300 and 600 DPI, especially when reproducing fine curves and gray-scaled photographs. Another innovation is bidirectional communications, which allows the printer to inform a host computer of such printer faults as paper out and paper jamming.

Compaq also broke into the high-resolution market last summer with an extremely competitive, large-format laser printer that accepts useful add-ins including a send/receive fax modem. That idea quickly spread to the retrofit market for older LaserJet II's and III's, which now have several choices for faxes that interface through font-cartridge slots. Microsoft will shortly introduce a II/III upgrade cartridge of its own. The company claims that this cartridge will print Windows graphics much quicker than with the use of either PostScript or PCL. It will also provide a voice interface that will, for example, inform the user aurally that paper is out.

On the workstation front, DEC recently released seven computers ranging from $10,000 workstations to $300,000 mainframes, all based on the long-awaited 64-bit Alpha microprocessor. DEC has also publicly

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The article above is from *March 1992, Electronics Now*, page 91.
demonstrated Windows NT running on an EISA-based Alpha PC—that, incidentally, includes a PCI-based local bus. Sun and HP simultaneously announced competitive upgrades to their lines. Sun appears to be going after the high-end PC market, claiming much better AutoCAD performance than with a 50-MHz 486. Industry feeling is that HP provides the performance edge—but Sun still holds the largest market share, about 34%. IBM has been strangely silent about its well-received RS/6000 line throughout these recent scuffles.

Conclusions

Together, all these developments add up to a new era of power and convenience for personal-computer users. The day is not far off when you will be able to connect to a worldwide network from anywhere, at any time, and obtain any available information. The rate of approach to this goal has increased rapidly during the past year, and the trend is likely to continue. More next time.

Product watch

Figure 1 shows a screen shot of a ground-breaking new Windows database: Microsoft’s Access. This is a product made to order for people whose needs exceed the capabilities of typical flat-file databases, but who don’t enjoy writing code in dBASE (or whatever), and who, in any case, want a wholly Windows-based solution. To understand Access, imagine uniting a powerful, multilingual, multiuser database engine with a visual development environment like that in Visual Basic, giving it a good dose of object-oriented behavior, and topping it all off with extensive help and tutorial information suitable for occasional database developers.

In addition to its own format, Access can read and write ASCII, Btrieve, dBASE, Excel, and Paradox files in their native formats. Access can also attach to SQL databases (at present, only Microsoft’s SQL server, but Oracle support is scheduled soon). Access has extremely intuitive form-, report-, and query-building tools. For example, the form builder lets you draw fields, attach attributes (e.g. color and input validation criteria), and go.

Like Microsoft’s other major Windows applications (Word and Excel), Access has just the right balance of power and ease of use. As with the other products, Access makes it easy to get started, and macros and a full development language called Access Basic provide lots of room for growth as your needs evolve. Access supports typical data types (character, date, numeric, logical), as well as binary objects including images, sound, and video.

Access is a fully relational product that allows one to create "virtual" tables, called Dynasets, that consist of records concatenated from other tables joined by common fields. Any updates to a Dynaset propagate back into the source tables from which the data came. Access also provides multiuser network access (including WfW support) and record-level locking. Initial pricing was set at about $100. If you can get a copy at that price, grab it. It’s one of the best software deals around.

Home hardware hackers will want to check out Home Automation Laboratories, which publishes a catalog chock-full of information and product listings for devices that control lights and other electrical appliances remotely through special control panels or your PC. Simply reading the catalog can be an education in itself.

If you’re looking for special laser printer paper or labels, check out the Paper Direct catalog. It lists numerous specialty items including foils that you can run through your laser printer to add color to presentations, prefolded brochure blanks that go through your laser printer and have business-card cutouts, and lots of other goodies. In both cases, tell 'em we sent you.
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<th>Description</th>
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<th>Output Voltage (VDC)</th>
<th>Current (mA)</th>
<th>Dimensions (L x W x H inches)</th>
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<tr>
<th>Model</th>
<th>Frequency</th>
<th>ConV. Loss</th>
<th>Isolation</th>
<th>LO Level</th>
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<td>1-500</td>
<td>5.5</td>
<td>45 40</td>
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<tr>
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<td>+7</td>
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<td>68 45</td>
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