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FCC May Charge License Fees

The FCC proposes a charge for licenses and other regulatory functions. Suggested rate schedule calls for $150 for new commercial broadcast stations or major changes in existing AM and FM stations, and $250 for similar TV applications. For TV translators and other broadcast applications, the fee would be $30. Safety and special radio services would be charged $5 for amateur and disaster services, and $20 for all other special radio services. Charges for common-carrier applications would range from $10 to $150. A $20 fee is proposed for experimental-service applications.

The commission also suggests $2 to $5 fees for commercial radio operator exams and licenses.

Atomic-Powered Weather Station Installed in Arctic

The world’s first atomic-powered automatic weather station is now operating at Sherwood Head on Axel Heiberg Island in the Arctic. The original site was to have been Graham Island, but ice and snows prevented landing the apparatus there. The new location is some 60 miles farther north.

The station transmits temperature, barometric pressure and wind speed every 3 hours.

Power for the station comes from pellets of a strontium-90 compound that generates heat spontaneously by radioactive decay. A series of thermocouples turns the heat into electrical energy, which is stored in rechargeable batteries to operate the intermittently transmitting equipment. The data are transmitted on 3.4 and 5 mc simultaneously. The total transmission takes only 9 seconds every 3 hours. Output is 250 watts on each frequency. The picture shows the artist’s concept of the station as installed, probably a much more detailed and satisfactory picture than could have been obtained by actual photography.

"Discrete" Is Discreet

For secret communications, the University of Michigan announces the “discrete frequency synthesizer” developed by its Cooley Electronics Laboratory under the leadership of Thomas W. Butler, Jr. Ph.D.

Through a process known as “pseudo-random generation,” both receiver and transmitter jump from frequency to frequency, apparently at random, but actually following a computer-designed pattern. Eavesdropping is rendered impossible.

The tuning mechanism consists of a diode that varies capacitance, allowing frequency changes up to 500,000 times per second with a high degree of accuracy—1 part in 100,000,000. Only a single crystal is required, as the diode generates a large number of harmonics. The device is built of solid-state components and contains no moving parts.

The “discrete frequency synthesizer,” says Dr. Butler, should be particularly useful in air navigation systems.

Translator Concern Proposes Cutting TV Audio

A change in the aural-visual power ratio in low-power transmitters has been recommended to the FCC as a means of fostering expanded use of uhf television channels. According to Adler Electronics Inc., who made the proposal, this would make a considerable saving in lower-powered transmitters, which can use a common amplifier for both visual and aural, and would also eliminate the costly diplexer. Experiments with a visual-to-aural power ratio of 4 to 1 and even higher have not brought forth a single reported instance of reduced coverage area, whereas, with the present 2-to-1 ratio, the aural signal coverage is greater than the visual at both vhf and uhf. Other suggestions for cutting costs in low-power stations such as those used for television translators were elimination or reduction of the requirements of vestigial sideband suppression, elimination of restrictions on antenna directivity, provision for remote control, and elimination of the current uhf channel assignments.

Radio Waves Measure Ice

The Army Signal Corps has measured the depth of a massive glacier with a new radio-sounding technique. Amory H. Waite, Jr., veteran engineer of the Research and Development Lab, reports that the soundings were made on Brue Glacier, 20 miles south of Ellsmere Island in the far-north region of Canada.

The method works this way: radio signals penetrate the depth of the glacier and return to a receiver, after reflecting off underlying soil, rock or water. Traveling time of the signal (about 93,000 miles per second—approximately half the free-
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space velocity) tells operators how deep the glacier is.

The Army Signal Corps technique has been used in measuring ice gaps, but it was thought that the greater movement of glaciers might deflect signals from their course and upset readings. No serious disruptions were observed, however.

Radio sounding is faster and less expensive than the older method of seismic sounding, which involves explosives and highly trained personnel. The work is also being carried on in the Antarctic, and will provide a clearer picture of geographical features hidden by ice in these areas.

**FM Sets New Record**

Purchases of FM radio receivers exceeded 2,500,000 in 1961, surpassing 1960's former record by 450,000 sets. FM stations have also increased, numbering 1,162 as of mid-February, 1962. A part of this increase represents a steady gain in FM which was beginning in late 1958 and has continued to increase up to the present. Accelerating factors are the entry into the field of FM stereo and the development of FM automobile and portable radios, first imported from abroad and now being made in the United States as well.

**Writer Wins Edison Award**

Amateur radio operator William G. Welsh, 34, of Cambridge, Mass., and Burbank, Calif., has received General Electric's 1961 Edison Radio Amateur Award for public service. In addition to the award trophy, he received a $500 cash prize.

Employed as an electronics engineering writer by Raytheon Corp., Waltham, Mass., and more recently by Librascope, Inc., Glendale, Calif., Welsh operates amateur radio station W1SAD/6 and uses his spare time to teach electronics. He is said to have devoted 20 to 30 hours a week to this endeavor over the past 10 years, giving free instruction to about 2,800 persons.

His courses include eight 1,800-foot code practice tapes, which he has run off free of charge and distributed to voluntary study groups throughout the nation and in at least 12 foreign countries.

Nominated by various persons in the Boston area, Welsh was chosen from 23 candidates as the tenth winner of this award.

Special citations also went to runners-up Robert T. Herrdon, Port Lavaca, Texas; Eugene M. Link, Boulder, Colo.; and George L. Thurston, Tallahassee, Fla.

**Lucien Christien Passes**

Lucien Chrétien, electronics editor of the magazine *Radio et TV* (formerly *La TSF pour Tous*) for more than 30 years, has died in Paris. In addition to his work as editor, he was the author of a number of texts on radio, television and electronics, an instructor (Ingénieur de l'École Supérieure d'Électricité), an inventor, and a technical journalist since 1917.

**Doppler Navigators To Take Over in Air?**

Aerial navigators on TWA's overseas jetliners may soon be replaced by Doppler radar sets and analog computers.

The human navigator accomplished his task with radio aids, dead reckoning and a periscopic sextant for celestial observation. Limitations of this method demanded a longer and wider block of air space for each flight. The new system, far more accurate, permits sharp reduction in ocean air-space assignments.

The TWA cockpit now contains a side-by-side pair of ground speed and drift indicators (A and B), each preset to give guidance for the first two segments of the trip—about 500 miles each. The pilot then sets A for the third segment, and the units overtake each other in leapfrog fashion for the rest of the journey.

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Although TWA officials say the system is “fantastically accurate,” the FAA requires the use of ground-based radio aids to confirm positions, at least for the present.

Calendar of Events
IRE-AIEE Symposium on Mathematical Theory of Automata, April 24-25, United Engineering Center, New York, N. Y.
NATESA Directors Spring Conference, Apr. 28-29, Americana Hotel, Miami, Fla.
SMPE 51st Convention, April 25-May 4, Ambassador Hotel, Los Angeles, Calif.
IRE, AIEE Spring Joint Computer Conference, May 1-3, Fairmont Hotel, San Francisco, Calif.
IRE International Congress on Human Factors in Electronics, May 3-4, Lafayette Hotel, Long Beach, Calif.
IRE, AIEE, EIA Electronic Components Conference, May 8-10, Marriott Twin Bridges Hotel, Washington, D. C.
IRE National Aerospace Electronics Conference, May 14-16, Biltmore Hotel, Dayton, Ohio.
Institute for Advancement of Medical Communication Council on Medical TV, May 15-16, National Institutes of Health, Bethesda, Md.
Navy Medical Dental TV Workshop, May 16-17, National Naval Medical Center, Bethesda, Md.
1962 Electronic Parts Distributors Show, May 21-24, Conrad Hilton Hotel, Chicago. Attendees limited to manufacturers, distributors, representatives and their advertising agencies. RADIO-ELECTRONICS will exhibit in Room 610.
15A National Aerospace Instrumentation Symposium, May 21-23, Marriott Twin Bridges, Motor Hotel, Washington, D. C.
IRE, AIEE, ASME, 15A National Telemetering Conference, May 21-25, Sheraton Park Hotel, Washington, D. C.
EIA Annual Convention, May 23-25, Pick-Congress Hotel, Chicago, Ill.
IRE Seventh Region Space Communications Conference, May 24-26, Seattle, Wash.
IRE Spring Conference on Broadcast and TV Receivers, June 18-19, D’Allesio Inn, Chicago.

Not All Recruiters Welcome Women Engineers

Despite the statement of Mildred Webber, placement official at the University of Michigan (RADIO-ELECTRONICS, April, 1962, page 12), who said that “women have just as good a chance as men in any science field, and can earn comparable salaries,” a survey of personnel recruiters from 30 of the nation’s large.

(Continued on page 16)
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ENROLL ME NOW SEND MORE FACTS

MAY, 1962
Now is the time to come to the aid of your party!

The more you enjoy outdoor living, the more you'll enjoy the Electro-Voice Musicaster—world's finest weather-proof loudspeaker system. A Musicaster will add to your fun wherever you are. Whether you're dancing under the stars, swimming in the pool, or relaxing around the barbecue in the backyard, music from a Musicaster adds the pleasure of outdoor high-fidelity music from your present Hi-Fi system, radio, phonograph or TV set.

It's easy to connect for permanent use outside, or you can simply move your Musicaster into the recreation room for year-round pleasure.

Designed for indoor-outdoor use, the E-V Musicaster obtains high-fidelity response from a heavy-duty weatherproofed speaker mounted in a rugged aluminum die-cast enclosure. This combination insures long-lasting satisfaction under all conditions.

Now is the time to come to the aid of your outdoor party... with an Electro-Voice Musicaster. It's easy to install... send for full information and the name of your nearest E-V sound specialist.

ELECTRO-VOICE High-Fidelity Speaker System... it's Weather-proofed!

SPECIFICATIONS:
- Frequency Response: 60-13,000 cps
- Dispersion: 120°
- Power Handling Capacity: 30 watts program
- Impedance: 8 ohms
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- Weight: 31 lbs. net
- Price: $54.00
- Musicaster II available with additional tweeter to extend response to 18,000 cps. Price: $75.00

Electro-Voice, Inc. Dept. 524E
Buchanan, Michigan

Please send me your booklet, "How to Enjoy High-Fidelity Outdoors."

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F. C. C. LICENSE — KEY TO BETTER JOBS

An F. C. C. commercial (not amateur) license is your ticket to higher pay and more interesting employment. This license is Federal Government evidence of your qualifications in electronics. Employers are eager to hire licensed technicians.

WHICH LICENSE FOR WHICH JOB?

The THIRD CLASS radiotelephone license is of value primarily in that it qualifies you to take the second class examination. The scope of authority covered by this license is extremely limited.

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The FIRST CLASS radiotelephone license qualifies you to install, maintain and operate every type of commercial radiotelephone equipment including all radio and television stations in the United States, its territories and possessions. This is the highest class of radiotelephone license available. Many companies which employ industrial electronics technicians require this license.

GRANTHAM TRAINING PREPARES YOU

The Grantham Communications Electronics Course prepares you for a FIRST CLASS F. C. C. license, and it does this by TEACHING you electronics. Each point is covered simply and in detail, with emphasis on making the subject easy to understand. The organization of the subject matter is such that you progress, step-by-step, to your specific objective—a first class F. C. C. license.

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Grantham training is available by correspondence or in resident classes. Either way, you are trained quickly and well. Write, or mail the coupon below, to any division of Grantham School of Electronics. Our free booklet will be sent to you immediately.

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To better serve our many students throughout the entire country, Grantham School of Electronics maintains four Divisions—located in Hollywood, California; Kansas City, Mo.; Seattle, Wash.; and Washington, D.C.

This free booklet gives details of our training and explains what an F. C. C. license can do for your future.

Upgrade Your Income with a First Class
F. C. C. LICENSE

HERE'S PROOF... that Grantham students prepare for F. C. C. examinations in a minimum of time. Here is a list of a few of our recent graduates, the class of license they got, and how long it took them:

<table>
<thead>
<tr>
<th>License Weeks</th>
<th>Class</th>
<th>Name</th>
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<tr>
<td>1st 12</td>
<td>1st</td>
<td>James C. Bailey, 217 Behrends Ave., Juneau, Alaska</td>
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<td>1st 20</td>
<td>1st</td>
<td>Edward R. Barber, 507 S. Winnifred, Tacoma, Wash.</td>
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<td>1st 12</td>
<td>1st</td>
<td>M. A. Dill, Jr., 20 Cherry St., Gardiner, Maine</td>
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<tr>
<td>1st 12</td>
<td>1st</td>
<td>Bernhard G. Fokken, Route 2, Canby, Minn.</td>
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<td>1st 12</td>
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<td>Kenneth F. Foltz, Broad St., Middletown, Md.</td>
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<td>1st 12</td>
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<td>James C. Greer, Mound City, Kansas</td>
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<td>1st 22</td>
<td>1st</td>
<td>Thomas J. Hoof, 216 S. Franklin St., Allentown, Pa.</td>
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<td>1st 12</td>
<td>1st</td>
<td>Clyde C. Morse, 7505 Shannonee Dr., Mentor, Ohio</td>
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<td>Louis W. Pavek, 838 Page St., Berkeley 10, Calif.</td>
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<td>1st 12</td>
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<td>Wayne Winsauer, 209 B St., Bellingham, Wash.</td>
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I am interested in: ☐ Home Study, ☐ Resident Classes

Date ______
"Loud and clear" reception begins with quality-engineered Sonotone Ceramikes. That's because Ceramikes are designed to give maximum speech intelligibility — designed for greater sensitivity to the frequencies covering the human voice. This frequency selectivity, coupled with physical design, screens out background noises. Ceramikes are inherently immune to extremes of temperature or humidity — will operate even if immersed in water. The ceramic transducer of every Ceramike is neoprene-encased, rendering it shock and impact-proof to withstand rough treatment.

There's no secret to Sonotone's ability to combine performance with durability. Sonotone has pioneered research in hearing aids — where transducers must meet the unbelievably critical demands of frequency response and day-in, day-out use and still function dependably. This know-how is responsible for this smartly engineered line-up of microphones tailored to communications requirements.

A quality trio of microphones for "loud & clear" communications

SONOTONE CERAMIKES

perfect cb team


SONOTONE CERAMIKE CM-17A — 13" Flex-mike. Ideal base station microphone for CB or other communications applications. Goose-neck mounting makes it easy to talk while keeping hands free. Sharp, clear communication with frequency response sensitivity of -56 db from 50 to 11,000 cps, ±2 db. Equipped with 6' shielded cable. List $24.50.

rugged mobile communications mike

SONOTONE CERAMIKE CM-31 — Budget-priced communications model in shatterproof plastic case features excellent intelligibility (90 to 6000 cps frequency range at -49 db sensitivity). 2-conductor coil cable — no switch. List $13.50. Fixed communications or mobile, Sonotone Ceramikes provide top-flight, long-term, maintenance-free performance.

(Continued from page 10)

est defense contractors reveals that 20% are still reluctant to hire women engineers and scientists.

The survey was made by the Research Dept. of Careers Inc., national job information clearinghouse for scientists and engineers. Since it consisted of interviews with the actual recruiters of some of the nation's largest defense contractors, it may perhaps reflect the facts more accurately than the "official" statements of corporation spokesmen.

The question "Are you reluctant to hire women scientists or engineers?" was asked recruiters representing 30 corporations. The answers were "No, not reluctant"—23, "Yes, reluctant"—6.

Electric Power Station Will Use Atomic Energy

The Atomic Energy Commission has issued a permit for a 40,000-kw high-temperature, gas-cooled nuclear power station at Peach Bottom in southeastern Pennsylvania.

The Peach Bottom plant will be built by Philadelphia Electric and 52 other electric utility companies, organized as High Temperature Reactor Development Associates Inc. The 53 companies generate 42% of all the electricity produced by the privately owned power companies of the United States.

The plant is expected to be in operation by mid-1964, and will be operated by Philadelphia Electric as a unit of its 5,500,000-kw power generating system. It will represent the first commercial application of an advanced technique of nuclear power generation known as the high-temperature, gas-cooled power reactor.

(Continued on page 20)
ANOTHER PRECISION SERVICE TIP FOR YOU.

PRECISION PETE

"A CASE OF DOUBLE TROUBLE!"

'EV'NING, MISS DORA. HELLO, MISS FLORA. WHAT SEEMS TO BE THE TROUBLE?

THE PICTURE ON MY PORTABLE IS SO DARK, I CAN'T TELL THE COWBOYS FROM THE INDIANS!

AND ON MY COLOR SET, THE PICTURE IS DIM, TOO.

MMM... THE METER ON THE CR-60 READS BAD. A BOOSTER MAY HELP WITH THE CR-60, I CAN INCREASE AC HEATER VOLTAGE TO SIMULATE A BOOSTER.

I'M SORRY, THE METER STILL READS "BAD" AND EVEN TRYING TO REJUVENATE DOESN'T HELP. YOU'LL NEED A NEW PICTURE TUBE.

OH, PEAR! ARE YOU SURE?

YES, YOU SEE, THE PRECISION CR-60 IS THE ONLY TESTER OF ITS KIND TODAY THAT NOT ONLY TELLS ME IF A "BOOSTER" WILL SOLVE THE PROBLEM, BUT ALSO LETS ME CHECK FOR TUBE BRIGHTNESS UNDER HIGH OR LOW LINE-VOLTAGE CONDITIONS.

PETE, WHAT ABOUT THE DIM PICTURE ON MY COLOR SET?

WELL, THE PICTURE TUBE IS FINE, SO THIS DIMNESS MUST BE DUE TO SOME OTHER CONDITION. PROBABLY IN THE CHASSIS. WHEN I COME BACK TO- MORROW WITH YOUR NEW TUBE, DORA, I'LL BRING MY PRECISION COLOR TEST EQUIPMENT TO FIND THE TROUBLE.

SERVICEMEN: QUICKER SERVICE WITH THE CR-60 ELIMINATES MANY CALL-BACKS, SAVES TIME AND EARN'S YOU MORE PROFIT. FOR MORE SERVICE TIPS WITH THE CR-60 (DEALER NET $64.95), WRITE FOR BULLETIN #100. IT'S FREE!

WELL, JUST ONE MORE CALL TO MAKE TONIGHT. HOPE MY PORTABLE PRECISION CR-60 CRT PICTURE TUBE TESTER AND REJUVENATOR CUTS THIS ONE SHORT.

Oh, Pete! You're wonderful! We'll see you tomorrow.

That's one call-back I'm going to enjoy, thanks to Precision's CR-60 CRT TESTER AND REJUVENATOR.

Oh, Pete! You're wonderful! We'll see you tomorrow.

WELL, THE PICTURE TUBE IS FINE, SO THIS DIMNESS MUST BE DUE TO SOME OTHER CONDITION. PROBABLY IN THE CHASSIS. WHEN I COME BACK TO- MORROW WITH YOUR NEW TUBE, DORA, I'LL BRING MY PRECISION COLOR TEST EQUIPMENT TO FIND THE TROUBLE.
The Sprague Type SK-1 SUPPRESSIKIT—
Easily installed on any truck, car, or boat engine using a 2-pole d-c generator.

RADIO HAMS, fleet owners, and CB operators can now enjoy clearer, more readable, less tiring mobile communications at longer effective ranges.

Sprague's new Type SK-1 SUPPRESSIKIT provides effective RF Interference suppression—at moderate cost—up through 400 megacycles. Designed for installation on automobiles, trucks or boats with either 6-volt or 12-volt generators, the Suppressikit makes possible high frequency interference control by means of Sprague's new, extended range, Thru-pass® capacitors.

The components in the SK-1 Suppressikit are neatly marked and packaged, complete with easy-to-follow installation instructions. All capacitors are especially designed for quiet, simple installation. Unlike general-purpose capacitors, these heavy-duty units are rated at 60 amperes, and will operate at temperatures to 125°C (257°F). This means you'll have no trouble with an SK-1 installation in the terrific temperatures found "under the hood" on a hot summer's day. There's no chance of generator failures from capacitor "short outs", as with 85°C general purpose capacitors.

The Deluxe Suppressikit is furnished complete with an 8-foot shielded lead on the generator capacitor which can be trimmed to necessary length for any car or small truck, preventing RF radiation from armature and field leads.

Containing only 5 easy-to-install capacitors, the Deluxe Suppressikit is truly a "do-it-yourself" kit. The net price of $17.85 is a little higher than that of makeshift, throw-together kits, but it saves you so much time and aggravation it's well worth the slight extra cost.

If the SK-1 Suppressikit is not available at your Sprague Electronic Parts Distributor, send your order to Sprague Products Company, 81 Marshall St., North Adams, Mass.

Compare internal construction of Twist-Lok to ordinary 'lytic!' Complete listings are shown in handy Wall Catalog C-457. Get your copy from any Sprague Distributor, or write to Sprague Products Company, 81 Marshall St., North Adams, Mass.

NEW LIGHTING CAPACITORS FOR DUTY USES.

There's temperature means; the heavy-duty units are general-purpose capacitors, packaged complete, to suit your needs. New Pressikit units are made for mobiles, Designed for shorter cost.

Sprague Type SK-1 SUPPRESSIKIT—
Easily installed on any truck, car, or boat engine using a 2-pole d-c generator.

RADIO HAMS, fleet owners, and CB operators can now enjoy clearer, more readable, less tiring mobile communications at longer effective ranges.

Sprague's new Type SK-1 SUPPRESSIKIT provides effective RF Interference suppression—at moderate cost—up through 400 megacycles. Designed for installation on automobiles, trucks or boats with either 6-volt or 12-volt generators, the Suppressikit makes possible high frequency interference control by means of Sprague's new, extended range, Thru-pass® capacitors.

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The New Sony 9 Transistor Citizens Band Class D transceiver uses a SEPARATE MICROPHONE AND SPEAKER. A quality product of the world's foremost research and development team in transistor electronics, weighs only one pound and is powered by 8 penlite cells for up to 50 hours of operation. The crystal controlled CB-901 employs a sensitive variable reluctance microphone and 2 1/4" PM speaker. Note how the microphone and speaker are each placed in the most natural position for transmitting and receiving. With 5 foot telescoping whip, push-to-talk button and volume control, the SONY CB-901 lists at $149.95 per pair, including batteries, earphones and leather case. Stop in at your dealer's and test it today.

Also see the amazing SONY 8-301W TV, the only truly portable, fully transistorized set that works on its own battery pack, 12v auto/boat battery and AC. Weighs a mere 13 1/4 lbs. List $249.95. BCP-2 alkaline battery power pack, $39.95.

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Central: 4959 W. Belmont Ave., Chicago 41, Ill.

Please send me the Sony "FACTS" booklet covering the SONY 8-301W TV and information on the SONY CB-901 Transceiver.
NAME ________________________________
ADDRESS ________________________________
CITY __________________ STATE _______

SONY CORP. OF AMERICA, 514 B'WAY, N.Y. 12, N.Y.
(Continued from page 16)

Parametric Amplifier
Features New Noise Figure

A microwave amplifier with a noise figure of about 0.9 db, the lowest noise ever achieved by this type of amplifier, is reported by Bell Telephone Laboratories. A new, hermetically sealed gallium arsenide diode is one of the factors contributing to the improvement in this amplifier. Another contributor is a new cooling arrangement, in which the amplifier is contained in a metal cavity, sealed by indium wire and immersed in liquid nitrogen. This leads to more even cooling, and improves operating stability. The nitrogen cannot leak into the device.

Brief Briefs

A tandem Van de Graaff 15,000,000-electron-volt accelerator is being installed by Rutgers University, New Jersey, in collaboration with the Bell Telephone Laboratories. It will be used in nuclear research by both organizations.

A semiconductor strain gage with an output powerful enough to drive panel meters direct has been introduced by International Resistance Co. The new strain-gage pressure transducer is rated for 5 volts dc output, and will not require amplifiers in most applications.

A video tape recorder weighing only 30 pounds, and able to record 3/4 hour of television pictures, was announced by the Goddard Space Flight Center. The little recorder, developed by Ampex, occupies less than 1 cubic foot of space, and will be used in satellites.

Paul B. Findley, editor of the Bell Laboratories Record for 27 years, until his retirement in 1952, died at the age of 73.
See Only the Scale You Want...in the Exact Range You Want

just set the range switch
and the correct scale appears

AUTOMATICALLY

in the new VOM and VTVM

V O M A T I C 3 6 0
AUTOMATIC VOLT-OHM MILLIAMMETER

Greatly simplifies your VOM use. Individual full-size scale for each range—and only one scale visible at any one time, automatically. Once you set the range switch, it is impossible to read the wrong scale. Reading in the range you want is amazingly easy—and direct. No reading difficulties, no multiplying, no errors.

**Sensitivity** 20,000 ohms per volt DC; 5000 ohms per volt AC. **Accuracy** ±3% DC; ±5% AC; (full scale). DC Volts in 6 ranges 0-6000. AC Volts in 6 ranges 0-6000. AF (Output) in 4 ranges 0-300 volts. **DC Current** in 5 ranges 0-10 amps. **Resistance** in 4 ranges 0-100 megohms. Supplemental ranges also provided on external overlay meter scales. Meter protected against extreme overload and burn-out. Polarity reversing switch. Automatic ohms-adjust control. Mirrored scale. Complete with 1½-volt and 9-volt batteries, test leads, and easy-viewing stand.

Net, $5995

DYNAMATIC 3 7 5
AUTOMATIC VACUUM-TUBE VOLTMETER

Once you set the range switch, you automatically see only the scale you want and read the exact answer directly. Saves time, eliminates calculation, avoids errors. Individual full-size direct-reading scale for each range. Simplifies true reading of peak-to-peak voltages of complex wave forms in video, sync and deflection circuits, pulse circuits, radar systems, etc. Includes DC current ranges, too.

**Accuracy** ±3% full scale AC and DC. **Sensitivity** 100 microampere meter movement. DC Volts in 7 ranges 0-1500. AC Volts (rms) in 7 ranges 0-1500. AC Volts (peak-to-peak) in 7 ranges 0-1500. **DC Current** in 3 ranges 0-500 ma. **Ohms** in 7 ranges 0-1000 megohms. Utilizes single DA-AC ohms probe and anti-parallax mirror. Swivel stand converts to carry-handle. Includes 1½ volt battery. Operates on 117 volts 50-60 cycle AC.

Net, $8995

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MAY, 1962
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Why take chances with the cracking and chipping problems common with conventional dipped capacitors. After all, your profits and your reputation are at stake with every set you service—protect both by replacing with only genuine Aerovox Bi-Electric Mylar® Paper Bypass Capacitors! You see, actual tests prove that the uniform, protective Polycap case from end-to-end, and the special process-controlled end seals, eliminate your cracking and chipping troubles. No wasted time... no expensive call-backs, as service technicians everywhere know from experience.

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Correspondence

LIKES TROUBLESHOOTING CHARTS

Dear Editor:

Your radio troubleshooting charts that appeared last November and December are just the thing for lazy guys like me. They sure are tops. When are you going to come out with a TV trouble chart?

R. J. CORRIGAN
Dayton, Ohio

[Whether or not he is lazy, the charts help a technician form good servicing habits—to develop a radio servicing technique that will save him time, effort and headaches. The TV trouble chart is a lot more complex. When we have one that really works you'll be sure to see it in Radio-Electronics.—Editor]

INSTANT ON

Dear Editor:

After seeing the item on "Instant On" in the January 1962 issue, I decided to add such a circuit to a small radio for testing. After studying the diagram, I could not devise a way to replace the special switch—volume control now in the set. Instead, I installed a silicon rectifier across the switch and left the B-plus on. As I see it, with the two rectifiers back to back, it is almost an open circuit anyway. Maybe my theory is wrong on this, but it seems to be working fine.

DICK ROGERS
Rogers Electronics
Brighton, Mass.

[The author thought of that, too! He tried the same thing and it popped the silicons—repeatedly. Experiments are continuing—more will appear in a future issue.—Editor]

NO SUSPICION?

Dear Editor:

Looking through your October issue I rather belatedly came across this gem of modesty by Mr. Crowhurst: "... we suspect that we now know more... than anyone else in the industry." This is no mere suspicion with Mr. Crowhurst. It's been a conviction of his for years.

In fairness to your other advertisers, don't you think it's time you started charging Mr. Crowhurst your established rates, and taking his copy out of the editorial section?

Mr. Crowhurst is less interested in advancing the art of stereo—or in anything else—than gratifying his monumental vanity, indisputably the greatest in the industry. He has a

---

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SUCCESS IS NO ACCIDENT. There is a reason why some men move ahead in electronics while others stand still, year after year, in routine, low-paid jobs. Responsible, rewarding positions in electronics require advanced technical knowledge. Without such knowledge, you cannot hope for success no matter how bright and ambitious you are.

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YOU WILL FOLLOW THE FOOTSTEPS of the thousands of CREI men who hold positions as associate engineers, engineering aides, field engineers, project engineers and technical representatives. They work in every area of electronics, from manufacturing to the space program.

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My qualifications are noted to obtain immediate service.

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- Nuclear Engineering Technology
- Automation and Industrial Electronic Engineering Technology

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Electronic Experience ___________________________

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Quam's factory is a manufacturing plant, not merely an assembly shop. By making our own speaker parts, we can guarantee the quality of the materials that go into them. Our voice coils are centered precisely; each and every speaker is thoroughly tested; the product you get meets the standards we have insisted on for almost forty years.

Quam Quality Line speakers are enameled in gold—and while the color has no effect on performance characteristics, it symbolizes the quality and reliability that's built into every Quam speaker.

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FIRST LESSON IN
PHOTOFACT
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(JUNE 1962)

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mortal fear that his genius will not be fully appreciated, a tragedy he intends to avoid if he has to hit his readers on the head.

ROBERT G. VAUGHAN
Greensboro, N. C.

QUESTION OF RELIABILITY
Dear Editor:

In your February 1962 issue there was a very interesting letter in your correspondence column from Mr. W. F. Palmer, of Palmer Electronics Labs.

In it, he suggested that the reliability of the thyratron ignition system (September 1961) was questionable, and initial and maintenance costs were high. As a manufacturer of transistorized ignition I am inclined to believe this.

Our Magnition works on a similar basis to Mr. Palmer's Transfire but is different in many ways. The Magnition has two power transistors in the switching circuit, and two transistors in a multivibrator circuit controlled by the points.

As in Mr. Palmer's circuit, a special coil is used in our unit, as well as Zener diodes for transient voltage protection.

There have been many letters of controversy in the matter of transistor vs. conventional and other types of ignition but, should I be in a position to choose, I would take transistor ignition over all.

KARL M. WEISSMANN
Design Engineer
Hofmann Electronics Co.
Wayne, N. J.

ELECTRONIC PATHFINDER
Dear Editor:

In the September 1961 issue of Radio-Electronics appeared an article on an electronic pathfinder. Don't you think this is going to a lot of trouble when something as easy as this could be built?

The pushbutton switch energizes the 12-volt relay, thermal delay relay and headlights. After 180 seconds have elapsed, the normally closed contacts of the thermal relay open, de-energizing the entire system.

WILLIAM CHAKERES
Newark, N. J.

DDT FOR GREMLINS
I note the sound and fury still running on the electronic ignition system. I finally put one together and my troubles began. But I found that, when I finally boiled it for one hour in 100% DDT, the gremlins disappeared and it was ready for the field test. I'll report when the field test is completed.

In the meantime I've been experi-
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In the NRI Communications course you get actual experience as NRI prepares you for your choice of Communications fields and an FCC License. Commercial methods and techniques of Radio and TV Broadcasting; teletype; facsimile; microwave; radar; mobile and marine radio; navigation devices; FM stereo multiplexing are some of the subjects covered. You work with special training equipment.

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For men with Radio-TV experience who want to operate or service transmitting equipment used in broadcasting, aviation, marine, microwave, facsimile or mobile communications. A Service Technician is required by law to have an FCC License to work on C-Band, other transmitting equipment. From Simple Circuits to Broadcast Operation, this new NRI course trains you quickly for your Government FCC examinations.

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menting with a simple gadget for my Jeep. It gives me a spark many-fold hotter than the standard system, yet reduces current across the breaker points to a twelfth of its former value. Also the reverse surge is well damped. For interested parties the circuit is shown here.

WILLIAM K. GUTHRIE, JR.
Central City, Colo.

ELECTRONIC IGNITION AGAIN
Dear Editor:
After building the electronic ignition system described in the September 1961 issue, I had to make a change to get the unit to work in my 1960 V8 Lark. It was simply a matter of changing C5 from the indicated .001 sf to .009 to trigger the 2D21 with the distributor points. I use the original 12-volt ignition coil on the car.

I found my lead from the ignition switch included a series-dropping resistor which gave me only 6 volts on starting. To overcome this, I installed a separate lead from the ignition switch and, by adding a dpdt switch, I retained the original wiring for use with the regular system if it should ever be needed. See the diagram for the hookup.

JOSEPH FREI
Alamagordo, N.M.

[Readers will find the value for C5 varies slightly according to the particular thyratron used and the car in which the system is installed.—Editor]

ABOUT THAT “X”
Dear Editor:
With all due respect, whoever wrote the caption “X = Trans” above Mr. Silverman’s letter (September, 1961) is misleading Mr. Pearsall (January, 1962) and possibly many more of your readers. The use of “x” as a substitute for part of a word (not necessarily “trans”) is as old as amateur radio telegraphy and perhaps as old as wire telegraphy. Typical examples include “px” (press), “wx” (weather) and “dx” (distance). See The Radio Amateur’s Handbook, first edition, page 142.

Think hard. Back in December, how many times were you wished a “Merry Transmas”?

BYRON GOODMAN, W1DX
West Hartford, Conn.

END

What is it? You might call it a philosophy... an idea... a principle.

What does it mean? Technical excellence, reliability, performance—combined with sensible pricing. On this philosophy rests the enviable Tarzian reputation for customer satisfaction. Too, it has earned for Sarkes Tarzian, Inc. recognition as the producer of “the world’s finest tuner for the world’s finest sets”. You’ll also find this same practical ingenuity in all of these electronic products from Tarzian:

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1. New professional studio recording hysteresis-synchronous capstan motor: 24 studor slots for ultra-smooth drive, ultra-quiet and vibrationless professional bearing system.
2. Two new take-up and rewind reel motors, both extra-powered for effortless operation.
3. New cored-out steel capstan flywheel with all the mass concentrated at the rim for improved flutter filtering.
4. New optimally designed capstan drive belt brings wow down to negligibility.
5. New relay provides instantaneous extra power to the take-up reel motor at start to minimize tape bounce. Provides near-perfect stop-and-go operation and eliminates any risk of tape spillage when starting with a nearly full take-up reel.
6. New automatic end-of-tape stop switch cuts off take-up reel motor power. Also permits professional editing techniques, whereby tape being edited out runs off the machine while you are listening to it.
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8. Recording level adjustment during stop-standby.
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And All These Well-known RP-100 Features:

Separate stereo 1/4 track record and playback heads permitting off-the-tape monitor and true sound-on-sound recording; separate transistor stereo record and stereo playback amplifiers meeting true high fidelity standards; monaural recording on 4 tracks; digital turns counter; electrodynamic braking (no mechanical brakes to wear out or loosen); all-electric push-button transport control (separate solenoids actuate pinch-roller and tape lifter); unequaled electronic control facilities such as mixing mic and line controls, two recording level meters, sound-on-sound recording selected on panel, playback mode selector, etc. Modular plug-in construction.

Wow and flutter: under 0.15% RMS at 7½ IPS; under 0.2% RMS at 3½ IPS. Timing Accuracy: ± 0.15% (±3 seconds in 30 minutes). Frequency Response: ± 2db 30-15,000 cps at 7½ IPS; 55db signal-to-noise ratio: ± 2db 30-10,000 cps at 3½ IPS; 50db signal-to-noise ratio. Line Inputs Sensitivity: 100mv. Mike Inputs Sensitivity: 0.5mv.

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CLOSED-CIRCUIT TV ADVANCES
... Vast New Uses for Television Are in The Making...

Mass closed-circuit TV, neglected for nearly two decades, suddenly has come of age in 1962. Closed-circuit TV is big; it means a novelty; it has been with us since the very beginning of the television art. Baby-watching via TV; police lineups to precipit stations; surveillance of inmates in prisons, or of factory workers; machine inspection; factory gate-watching by night watchmen; TV cameras in hotel and apartment house lobbies that watch the inside of self-service elevators; round-table meetings with officials in different cities; bank surveillance of tellers to verify check signatures and to alert police during holdups; TV in large railroad terminals to speed ticket service; giant TV screens installed in various theaters throughout the country, all interconnected to exhibit sporting events, etc. and other uses too numerous to mention now operate in many parts of the world.

None of these examples, however, are true mass closed-circuit TV applications, for individual use in the viewers' homes or rooms. The nearest approach today are the Community Antenna Television (CATV) Systems throughout the United States and the Virgin Islands, according to a recent report by the National Community Television Association. There are now roughly 1,000 of them. These "cable" systems average out at 800 subscribers each. Sixteen have more than 500 subscribers, and two serve more than 10,000 viewers each. It is estimated that about 2.5 million viewers use cable and are served by lines which, for the most part, carry five signals. A number carry only one, and others have as many as nine. Pennsylvania has the largest number of CATV systems, with 204 listed, while five states have only one.

Long before broadcast television, the present writer fore- saw that one day we would have actual live theater in the home via closed-circuit TV. In his former magazine, Television News, in the January-February issue of 1952, he covered the subject under the title "The Tele-Theater." Instead of paying outrageous prices for theater tickets, viewers could see all important live Broadway shows direct from the theater via TV at 50 cents. If millions of people would view such Tele-theater shows at 50¢ a family, the theater entrepreneurs would soon grow rich. While this idea has still to be realized, a parallel series of enterprises has erupted quietly without much fanfare.

In Manhattan's Hotel Statler-Hilton, the Telad Corp. has installed a system whereby one of the 2,200 hotel room guests can see a special program about sightseeing New York, shopping from the big stores, gallery openings, all sorts of special New York events, weather and transportation information, theater news, special restaurant information—in short, everything that out-of-town visitors and tourists wish to know. This information is received on regular TV receivers, tuned to channel 6 (normally blank in New York City). The program on channel 6 repeats every half hour. The company spends about 5 minutes of commercials for each half hour. Programs run 12 hours a day, seven days a week, starting at 8 AM daily.

Another company, Teleguide, will broadcast similar TV programs to 12 (or more) other hotels comprising some 12,000 rooms. This company will use channels 3, 6 and 10—all presently unused in New York City. Thus channel 3 will carry condensed programs in French, German, Italian, Japanese, Portuguese and Spanish—30 minutes for each language, for guests who do not understand English.

In Washington, D. C., similar programs will be disseminated by another company named Hotelevision in two large hotels, the Sheraton-Park and the Shoreham.

There seems little doubt that other installations will be made very soon in all the larger hotels in the U.S. It is any one's guess how many million old and new TV sets will thus be connected and interconnected in the near future.

The companies mentioned above have their plants either in the hotels or at outside quarters. In either case, they run their ½-inch-diameter coaxial cable to the hotels' master antennas for the necessary connections.

Of importance to these new broadcasters is the fact that, inasmuch as they do not utilize a radio frequency, they are not affected by FCC regulations. Presumably this may not always be the case in the future. Conceivably, if closed-circuit television becomes a nationwide big business in years to come, some Federal regulations may inevitably come about.

When the new closed-circuit TV broadcasters tapped the hotels for their new service, the major facilities were already in existence—all that was required was to connect the coaxial cable. Yet there is waiting the infinitely larger market—the public at large. How can this well paying market be tapped in the future?

While the cost of conduits and installing coaxial cable would be astronomical if a separate cable were to run to every home and every apartment individually, yet to be an economic success, such a TV system should not cost much more than the present system of electric light, gas or water lines. A number of "pay-Television" companies have tried various technical schemes to bring programs to subscribers. None has succeeded so far.

How will the housewife of the future shop via television in her supermarket or department store—a dream publicized by many forecasters for the past 50 years? From a technical viewpoint, there is nothing impossible about this. It can be done right now; it is eminently feasible—except for the fantastic cost.

The same thing is true of the writer's early Tele-theater. It, too, will become possible in the future.

How? The physical facilities are already in existence—but the technical problems have yet to be solved. Almost every home has a telephone service supplied by two wires. The same is true of the electric wire supply. The telephone companies, well aware of the television-via-wire service, have been working over that problem for several decades. Many patents are in existence, but the final breakthrough of phonovision has as yet to be realized. The chief obstacle so far has been to channel the necessary high frequencies over a pair of not too highly insulated wires. In other words, to eliminate the coax. Perhaps some semiconductor device will prove to be the key to the difficult problem.

Once the technical difficulties are solved, the economics will be solved automatically, too—even the billing of the closed-circuit TV service will be done by the telephone companies.

Will phonovision adversely affect broadcast television? Probably not in the slightest. It will simply be an adjunct—a supplementary service to broadcast TV—both decisively have their own spheres of utility.

—H.G.
A SERVO SYSTEM IS ONE IN WHICH A mechanical position or motion is controlled by a small input signal which often includes some negative feedback. Some form of amplification is an essential element in any servo system. Most servo systems today use electronic servo amplifiers which can control relatively large mechanical motions and forces with very small input signals, or by corrective (feedback) signals supplied by the controlled elements.

A great many kinds of servo amplifiers operate on different amplification principles. But all basically function on the basis of a signal at the input derived from the action at the output—the so-called closed-loop system. See Fig. 1.

Whether you wish to build a light-seeking robot or track satellites with an antenna, or perhaps wish to follow the sun with a mirror furnace (as was my plan), you will need some form of servo amplifier. The one shown is about the simplest I could devise, yet it is reliable, versatile and inexpensive.

Fig. 2 shows a block diagram of the amplifier and power supply. In my case, the input signals were derived from two small solar cells for each of two motions. One is called a polar motion (rotation about an axis approximately parallel to the earth's axis). The other is a declination motion, which here meant primarily angle above the horizon.

Whatever you call it, one amplifier is needed for each motion. With two such amplifiers you can point an object (light-sensitive cell, microphone or what have you) in any direction you wish, depending only on the mechanical limitations of your system.

**Circuitry**

Fig. 3-a shows the circuit diagram of one servo amplifier (my complete system uses two amplifiers and one power supply), and Fig. 3-b the power supply. As you can see, the amplifier could not be much simpler. Each amplifier consists of three transistors per section, one potentiometer to balance the two halves and one polarized or differential relay. If you cannot obtain either a polarized or differential relay, two sensitive relays will do in its place.
Fig. 1—Basic closed-loop servo system.

Fig. 2—Block diagram of servo system used to track the sun.

Fig. 3a (below)—Schematic of servo amplifier (two are required for author's system); b (above)—power supply schematic. Output voltage of T2 must suit the motors used.

AMPLIFIER (Fig. 3a)
R —pot. 150 ohms, 2 watts, linear taper
V1—2-p-n-p transistors (2N107, CK722 or equivalent)
V2—4-p-n-p transistors (2N35 or equivalent)
V3—4-p-n-p power transistors (2N26A or equivalent)
P1, 2—solar cells (International Rectifier 8.3 M or equivalent)
RY—2-cell polarized relay, see text
PL—phono plugs
J3—phono jacks
J4—motor jack; number of contacts depends on number of motors used

Above parts list is for one amplifier only.

POWER SUPPLY (Fig. 3b)
C1—2000 pF, 15 volts (Cornell-Dubilier A-0070 or equivalent)
C2—1-100, 36 volts
T1—primary, 117 volts; secondary, 12.6 volts at 0.5 ampere or more (Thoradin 26FL or equivalent)
T3—primary, 117 volts; secondary, 26 volts at 0.5 amperes (Stancor P6469 or equivalent)
S1—3-pole toggle switch
RECT1— silicon rectifier, 100 ma or more
RECT2, 3—300-ma silicon rectifiers in parallel
S1—3-pole toggle switch (Amphenol 1550 or equivalent)
J4—motor jack, 5 contacts (Amphenol 78-55 or equivalent)
Cable to amplifier, 5 conductor with connectors on both ends (Amphenol Ba-FMS and 79-FFS plugs or equivalents)
Chassis for amplifier(s) and power supply, line cord and miscellaneous hardware as will be shown. Each amplifier chain is a direct-coupled p-n-p n-p-n p-p-p sequence, now familiar in transistor literature.

With each side of the amplifier receiving an identical signal, the output transistors pass the same amount of current (assuming both halves of the amplifier to be equal) and cause equal pull on both sides of the armature in the relay. As soon as one side receives more signal (as shown, or less signal with reversed input polarity), the output transistors pass different amounts of current through the relay coils. The armature is attracted to the side with the greatest current, closing a contact which causes a motor to turn in one direction. Closing the opposite contact would have turned the motor in the other direction.

If the input is a set of photocells or solar cells, and if your object is to have an equal amount of light on each cell, the correction to the system is applied at the input. (Rotating the cells will even the amount of light, causing the signals to become equal again and re-storing balance.) Thus if the light moves away, as the sun does, and more light falls on one cell than the other, the system will follow the moving light.

If the input is some other system of voltage-producing elements, these must also be balanced by the motor to make the system come to rest.

The photos show the amplifiers and power supply and one of my input cells. The construction of this cell is shown in Fig. 4. Two solar cells are set side by side on one side of a dark box (painted flat black inside) with a narrow slot in the opposite side of the box. If the box is pointed directly at a light, the cells are lighted equally. As soon as the box is pointed directly at a light, one cell receives more light. This unbalances the system and causes action. If the cells had been mounted in a longer box, with greater distance from the slot, a smaller angle of rotation would have obtained the same result. Thus, by making the input enclosure larger, the system becomes much more sensitive. In my case the short boxes were good enough to make the system active in bright sunlight with only a fraction of a degree of rotation.

Adjustments
This servo amplifier contains one paradox. Its greatest advantage is also its greatest disadvantage. It is a very versatile system, with wide latitude for inequalities in transistors, components, relays and input signals. On the other hand, this makes the system a little troublesome to adjust. Setting it up will require some patience. Current through the output transistors will be greatest with no input signal.

To adjust, you can shunt each input with a 100,000-ohm resistor, for example. Then—assuming the relay is balanced—balance the amplifier by adjusting potentiometer R. If that fails, swap transistors in each stage progressively (turn off the power before

Fig. 4—Construction of solar-cell box.
withdrawing a transistor), and try to balance the amplifier. If that also fails, there is always the relay adjustment. If you use the relays I indicate, there will be tremendous latitude in balancing, by adjusting the contact spacing or the holding magnets (or both) on each side. You can check initial relay balance by pushing the armature one way or the other. Even though the holding magnets may make the armature seem sticky on either side, it should return to center if the current is equal in the two coils. You can make sure of this condition by testing with the coils in series but opposing across a low-voltage source (3.5 volts will do).

[Western Electric 202 FJ relays were used by the author. These may be obtained as surplus from Red Johnson Electronics, 3311 Park, Palo Alto, Calif., or relay No. 255A at $16 per unit may be ordered from Metropolitan Telecommunications, 5814 Dean St., Brooklyn 38, N. Y. These are two-coil polarized relays with a coil resistance of approximately 100 ohms.—Editor]

Each amplifier chain should give from 600 to 1,000 gain, depending on the condition of the transistors used. This means that with the relay shown, which requires a difference current of only 3 ma, a few microamps of difference at the input will activate the servo motor. Such a small current can be obtained from a set of photocells. Fig. 5 shows the diagram for a set of Clairex CL-2 photocells in place of the solar cells. The input could equally well be a pair of thermistors with a voltage source, but in that case the time required to heat or cool the thermistors might slow the system down considerably.

This brings up the point of hunting. If the system is made very sensitive, and, as a result, quick-acting, it might overshoot the balance point, backtrack to correct and overshoot in that direction, and then again go forward, and so on, oscillating back and forth. This is called hunting. Eventually the system would come to rest because of the mechanical friction represented by the motor if for no other reason. But any hunting is undesirable. It can be corrected by making the system less sensitive, or less rapid, by introducing electronic "friction." This is most easily done by shunting the relay coils with large capacitors.

![Fig. 5—Photocells and an external voltage source may be used.](image)

Boxes housing solar cells.

To operate the motor with other than a polarized or differential relay, use the circuit shown in Fig. 7. Here two sensitive relays take the place of one polarized one, and the signal directivity is controlled by the diode rectifiers. An alternate is to use less sensitive relays, and simply circuit them as in Fig. 8-a, but the armatures then must be mechanically linked so that only one at a time can be attracted (Fig. 8-b).

To avoid overlap without the mechanical linkage in Fig. 7, each relay can energize a motor only if the other one is not energized. This can result in a "dead" spot if the relays have a great deal less holding than attracting current. Although differential relays and polarized relays also suffer from a "dead" spot, they are generally designed to have as little of this as possible. A single-coil polarized relay would be connected as shown in Fig. 9.

For more sensitive relays, the output transistors need not be power transistors. These were used because the

![Fig. 8—a—Two relays may be used if armatures are linked (see text); b (low) — simplified sketch showing method of linking relay armatures.](image)

![Fig. 6—Either mechanically unbalanced (a) or electronically (b) bridge may be used to supply input signals.](image)

![Fig. 7—Sensitive relays may be used in place of differential relay. Extra set of normally closed contacts is used to protect power supply in event both relays are energized.](image)

![Fig. 9—A single-coil polarized relay may be used.](image)
Servo amplifiers (two) and power supply. Author eliminated transformer T3 by adding a second 25-volt winding to T2.

Underside of power supply and amplifiers. Selenium rectifier was used in author's unit because it was readily available. Parts and layout of second amplifier are same as amplifier No. 1.

coil resistance is around 100 ohms. With sensitive high-resistance relays, the output transistors could be the same as the input transistors (2N107's, CK722's or equivalent).

Mechanical construction is of course totally uncritical, with one exception. The two sets of transistors should be exposed equally to any temperature change, in which case the system is almost entirely balanced for this factor. With the sun falling on only one part of the amplifier, you might find the system working without any input signal.

To protect the power supply, a male chassis connector should be used on the amplifier rather than the female one (J3) used in the original model.

Whatever your plans—robots, sun follower, heliograph, bridge balance or followup system, wherever you need a servo amplifier, this one will very likely fill the bill. With all the ways of compensating for differences in transistor characteristics, it can be built with inexpensive transistors. Very economically, in other words. If in the last analysis you still have difficulties solving the balance problem, resistors in the base connections of the transistors help a great deal. Their values will depend on the inequality of your transistors. The larger the resistors, the more sensitivity you sacrifice. This does not matter too much. Unless you hope to track stars (requiring much more sensitivity than this unit can provide), there is enough to spare for most purposes.
circuits for FM stereo

By NORMAN CROWHURST

What makes that FM stereo equipment work?

In the coming months RADIO-ELECTRONICS will cover every important or unusual circuit used for FM stereo. We will tell exactly how they are arranged and exactly how they operate. Detailed descriptions will accompany each schematic.

Our primary purpose is to show the many different forms taken to make FM stereo possible. This month circuits used by Sherwood, Pilot, Knight and Lafayette are presented. Others will appear in succeeding issues.

THE SHERWOOD CIRCUIT USES A REFINED FORM of switching. Like the others, the diodes attenuate the channel momentarily "unwanted", by about 18 dB. This eliminates the diode characteristics from the performance figures. The cathode-follower triode with 19 kc tuned in its plate is a conventional input. A 19-kc oscillator uses cathode, grid and screen of the pentode section, while the plate doubles to produce 38 kc, which is transformer-coupled to the switching bridge. A 19-kc trap across the cathode resistor of the follower eliminates any residual 19 kc from the composite, which is then fed to the center of the switching bridge.

The attenuation of the channel in which the diodes are momentarily conducting (by the instantaneous phase of 38 kc) is set very precisely by the 33,000- and the two 10,000-ohm resistors. The separation and balance adjustment in the cathode circuit of the two output tubes then produces virtually a perfect null at the plates, for left in right channel and vice versa. These plates feed through twin-T filters to remove 38-kc switching components and provide correct de-emphasis.
PILOT'S MODEL 200 USES SWITCHING WITH AN important difference. The cathode follower is fed with a high-frequency compensated divider. At the same time an amplifier stage feeds the 19-kc tuned amplifier that synchronizes the 38-kc oscillator. The 19-kc also feeds the switching amplifier which rectifies it for the dc amplifier controlling the relay.

In the earlier version of this circuit, the relay in the plate circuit of V3-b was mechanical. This has been changed to the solid-state circuit shown. A bias of three-fifths of B-plus is placed on the three lines isolated by 0.1-µf blocking capacitors by 1- and 1.5-megohm resistors. In monophonic (no 19 kc) the plate of V3-b is less positive than the lines, so the top two diodes are nonconducting, isolating the stereo channels from the output, while the bottom two are conducting, making a connection (for audio purposes) directly through the 47,000-ohm resistor.

In stereo, the 19 kc makes the plate of V3-b more positive, so the top two diodes conduct and the bottom two don't. Now stereo channel connections are made, and the monophonic connection is open. This change in voltage also operates the neon indicator. The regenerated 38-kc is fed to the double-wound transformer whose secondary (and primary) has a center tap.

The composite from the input cathode follower feeds through the SCA rejection filter to the secondary center tap of the 38-kc transformer. The two 220,000-ohm resistors, each shunted by 500 µf, maintain a charge close to the instantaneous peak value of 38 kc. Thus the matched pairs of diodes each conduct for only a short period near the peak of the 38 kc in one direction. When each conducts, it lets a sample of the composite fed in at the center tap through to the channel connected to that diode junction.

Where other switching circuits deliver half the composite waveform, on a time-division basis, to left and the other half to right, this circuit delivers just a short-time peak of each, when the 38-kc modulation (coming in from the transmitter, as distinct from the regenerated subcarrier) is at the point on left or right waveform, as the case may be. This avoids the reduction in L — R as compared with L + R inherent with normal switching circuits, and so does not need a separation adjustment to compensate for it.

MAY, 1962

www.americanradiohistory.com
THE KNIGHT SELF-POWERED KN-MX ADAPTER uses an input stage that is cathode follower for all but the 19-kc oscillator, using screen, grid and cathode. This gives an input impedance of more than 5 megohms. Composite stereo from V1-a's cathode is fed through a filter to remove SCA subcarrier and a further filter that partially shapes sidebands to the grid of a beam-switching 6AR8. The plate circuit of the tube used as a 19-kc oscillator doubles frequency and feeds the beam switching electrodes with push-pull 38-kc. The plate circuits of the 6AR8 include filters to remove switching frequency and deemphasis.

THE LAFAYETTE LT-200 ADAPTER RETURNS TO the matrixing concept. It uses half a 12AX7 as cathode follower, with the 19 kc tuned at the plate. Input impedance is about 10 megohms. The follower divides to feed the 15-kc low-pass filter (for L + R) and a 23- to 53-kc bandpass filter, with 67-kc rejection. Output of the latter is rectified by diodes D1 and D2 in opposite phase, to produce L - R and R - L. These outputs are combined in a matrixing bridge with L + R (after a separation adjustment in the L + R channel) to give L and R. The subcarrier is regenerated by a 19-kc oscillator (6C4) with 38-kc tuned plate circuit to pick off the doubled frequency. This 38 kc is fed into the output from the bandpass filter. Each channel feeds through a twin-T circuit to an amplifier stage with voltage feedback. Mono-stereo switching bypasses filters and uses the left-channel output amplifier on mono, paralleling the output jacks so both are the same.
ELECTRONIC TECHNICIAN equips himself for his job as compared to the carpenter or the machinist.

Contrast the usual way the electronic technician equips himself for his job as compared with skilled craftsmen in other fields. They have to provide an extensive range of tools at considerable expense to themselves. Compared with them, "our" man arrives at his job empty-handed. Yet by the very nature of his own skill he can provide himself, at minimal cost, with aids that are just as useful to him as the chisel to the carpenter or the calipers to the machinist.

Despite the small amount of money involved, very few technicians use these devices on their jobs though many of them have similar gadgets for home experiments. There seems to be an axiom in the electronic field—what the firm does not provide, do without.

How will this tool kit be useful? Very rare is the company which has an abundance of test equipment. Having worked in different plants on the production of equipment for home entertainment, industry and government, I have yet to find anything but shortages. This condition becomes especially acute when one works in the home consumer section of the industry. The pattern goes somewhat like this:

The firm plans a new production run. The pilot models have been made, tested, modified, tested again, and pronounced satisfactory. The unit goes into mass production, and the call goes out for more technicians. Now there is a sudden increase in the number of people who want to use the scopes and meters which were already in short supply. But this is not all.

What you need

When there is multiple hiring usually some inept or inexperienced personnel are acquired. Thus, after waiting in line for the multimeter, you get it with a blown fuse. And all you wanted it for was to test for a short! Why not have a simple continuity checker of your own? It will save your time and sanity. And most important, it will be there when you need it!

There are the numerous times when you want to jump, ground out or temporarily hook up a component. I always see these jobs done with solder and iron. In a busy shop, jumper leads are never to be found. If there ever were any, they long since found their way to the lab. Carry your own jumpers; in fact, carry three! They are as useful as a third hand.

You get a dead set from the production line. All tubes are lit, B-plus is...
Fig. 1—Signal-tracing probe has low-capacitance, doubler and demodulator, and isolation probe functions.

The signal tracer

All items can be made from easily obtainable commercial components, and a small drill is the only metal-working tool needed.

The signal-tracing probe (Fig. 1) is wired on a piece of perforated circuit board cut to fit snugly into a JAN type TS 102U08 tube shield. The probe housing is made from two of these shields placed end to end. Modify one shield by cutting the bent flange at the top in several places, and straighten it almost in line with the sides. Then push the second shield down over the straightened flange portions so it fits firmly. Finally, solder in two places.

Next take a JAN type 7-pin miniature tube socket with a shield base. Reverse the shield base (this is easier to do) so the socket pins are inside. Connect each probe input on the circuit board to a separate socket pin, and note which is connected to which.

For the other end, cut from a piece of 1/16-inch plastic a disc a little smaller than the inside diameter of the probe housing. I used the top of the plastic cylinder that Ungar soldering tips are packaged in. Burn or drill a hole in the center of the disc to take a Johnson nylon tip jack. If the hole is slightly small, the jack will cut its own thread. Otherwise, use the nut to hold it in position. Now solder the common probe output to the jack terminal, and the probe is ready for assembly.

Use one of the springs that are normally inserted in these tube shields in its normal position against its retaining flange, then place the circuit board with the disc against the spring. Now push on the housing over the shield base with the usual twist fit and everything will fit very firmly. The output jack will fit a meter or scope probe tip nicely.

For the multiprobe tip, cut about 1 1/2 inches of a paper clip so that you take in the bend portion. The bend will give a ready-made hook to hook on to component leads, and also something to grip with the fingers when changing tip positions. The probe you want is selected by inserting the tip in the appropriate tube-pin socket. If the tip is a loose fit, tin it with solder until it fits firmly. Connect a ground lead to the mounting hole of the tube base, which in turn is connected to the probe circuit ground. Drill a hole opposite the variable capacitor in the low-capacitance probe so it can be adjusted.

Signal injector

The circuit of the signal injector is in Fig. 2. Any audio-frequency transistors should work in this circuit. I used the only two transistors I had on hand. The waveform is unbalanced, but that is not important here. If you have
to buy the transistors, get two of the same type. If the 2N38 is not available, use a 2N34, 2N109 or similar type.

As with the signal-tracing probe, I used easily obtainable commercial components for the probe housing and all other sections. I got a Winchester penlight and disassembled it. The bezel type nose takes a standard insulated phone-tip plug, which is the probe tip. Only ¾ inch of the bakelite screw-on insulator acts as a retaining nut.

The circuit is wired on the same type of perforated board used for the signal tracer. The width is cut to fit the penlight case, and the length so the circuit board and one penlight cell fill the space normally occupied by two. Keep the circuitry in a little from each end of the board to allow for trimming. To use, clip one of your jumper leads to the pocket clip for a ground connection to the circuit under test.

I found that when the battery weakened to about 1.2 volts, the multivibrator would not start on closing the switch. I also found that momentarily grounding the junction of C1 and R3 never failed to start oscillations. To provide for this, I drilled a small hole in the penlight case opposite the junction of C1, R3. When the occasion arises, I just poke at the lead with any piece of wire I have on hand and the multivibrator never fails to start.

Those who do not want to go to the trouble of a perfect fit in the housing can solder a thin lead to the positive terminal of the battery from a ground point of the circuit. The multivibrator is always on, but so little current is drawn that battery life is long.

An alternative is to do what I did and use the penlight on-off switch to switch on the multivibrator. This entails soldering the round portion of a ground lug to the positive terminal of the battery to give a wider contact area and make sure the housing is in firm contact with the circuit board when slipped over the circuit board.

Build the circuit breadboard style first to make sure your components work. With some transistors, 1.5 volts may not be enough to start the multivibrator oscillating. Check this by temporarily hooking in 3 volts. If it still does not work, recheck the wiring.

The earphone (Lafayette MS-260) has a .001 uf blocking capacitor (small disc type for compactness) in series with the hot lead, and alligator clips to clip on with.

The continuity checker is another penlight or a single-cell novelty light serving a dual purpose. As a flashlight it will always be valuable. For use as a continuity checker, drill a small hole in the case so you can insert two thin, insulated leads that can be fed through and soldered to the respective positive and negative points. Now when the other ends of the leads are stripped and touched together, they bypass the switch and the bulb lights. Some novelty lights are of odd shapes and provide plenty of room to run leads in.

This is my suggested service kit, and it is just a handful.

END

By DONALD L. STONER

Although it is not generally known, you can operate a radio-controlled model without a license. Anyone who has taken the time to read paragraph 15.205 of "Part 15—Incidental and Restricted Radiation Devices" of the Federal Communications Commission Rules and Regulations will discover that a low-power communications device may operate between 26.97 and 27.27 mc (27.12 mc ±150 kc) provided it complies with the following requirements:

- The carrier of the device shall be maintained within the band 26.97 to 27.27 mc.
- All emissions, including modulation byproducts below 26.97 or above 27.27 mc, shall be suppressed 20 db or more below the unmodulated carrier output.
- The power input to the final radio stage (exclusive of filament or heater power) shall not exceed 100 milliwatts.
- The antenna shall consist of a single element that does not exceed 5 feet in length.

The intended use is not specified and thus Part 15 radio-control equipment may be considered permissible. Note also that no specific channel assignments are made (subpart a) and that any frequency between the limits specified can be used. The carrier frequency could be "wedged" between two Citizens band channels where interference is at a minimum.

There is one other point which should be mentioned in connection with the rules and regulations: Part 15.208 (d) states, "The certificate may be executed by a technician skilled in making and interpreting the measurements that are required to assure compliance with the requirements of this part." Thus, if you are technically qualified to make the required measurements (second harmonic, modulation bandwidth, power input, etc.), you can build a transmitter or modify a commercial unit. No second-class radio-telephone license is required. However, if equipment is found to be operating improperly or in violation of regulations, then the certifying person may be called for a hearing before FCC examiners. If he is found to be unskilled in making and interpreting measurements required for certification, then he may be prosecuted.

Although the power input of equipment used under Part 15 is limited to 100 milliwatts (0.1 watt), this is adequate for up to 1-mile range. Radio-control transmitters are usually operated with a continuous carrier. Only the tone is pulsed to actuate a receiver escapement or relay. This system is more reliable since the carrier tends to override interfering stations. Experience has shown that battery-consuming high-power transmitters are not required since the model seldom goes.

Inside the GW-30. This unit is about to be modified for license-free R/C use.
more than 1/2 mile away. Modern transistor receivers are more selective and sensitive than their vacuum-tube predecessors. Completely transistorized receiver and transmitter systems are not only practical but are commercially available (Wen-Mac, etc.)

A Part 15 R/C transmitter

To prove that a low-power transmitter could be used for radio control, a Heathkit GW-30 Citizens-band transmitter was modified to work in conjunction with a transistor radio-control receiver, an F & M Electronics Pioneer model. The circuit of the GW-30 is shown in Fig. 1.

The modifications involve disabling the GW-30 receiver and inserting feedback in the modulator section to generate a tone. The transmitting frequency of the GW-30 need not be changed.

Here's how to modify the GW-30. Take the unit out of its leather case and remove the back panel. Lift the printed-circuit board from the case after removing the three screws that secure the chassis. Familiarize yourself with the location of the pushbutton switch contacts (Fig. 2 and the photographs). This switch is modified so the transmitter carrier comes on when the volume control–switch is turned on. Depressing the button, in the modified GW-30, then produces a tone rather than turning on the carrier.

It is easier to bend the switch contacts than to rewire the switch to do this. They may be straightened later if a return to the original operation is desired. Note the dotted lines in Fig. 2. Bend the fixed contact on section B up so it touches the moving contact. This completes the emitter circuit of transmitter transistor V4. Next bend the fixed contact on section C up. This breaks the primary circuit of T1 and disables the receiver. Do not modify section D. Finally, on section A, bend the upper fixed contact up to clear it from the moving contact. Bend the lower fixed contact of section A so that it touches the moving contact at all times. This connects the antenna to the transmitter section. Finally, the modulator is made to oscillate by introducing feedback.

This can be done by reconnecting section D of the switch to tie the modulator output to the input. Locate the wires which connect section D to the speaker and T2. Reverse these two wires by "swapping" the connections from section D of the switch on the circuit board. Thus you can see that when they are connected in this manner, depressing the pushbutton connects the speaker winding on T1 to the speaker winding on T2. When this is done, the audio stages break into oscillation and tone-modulate the transmitter. This completes the changes to the unit and it can now be reassembled.

Although the modifications sound complicated, it actually takes more time to tell how to make them than to do the job.

To test the conversion, check the transmitter by energizing a radio-control receiver in a model on the ground. It should actuate the control surface reliably over a distance of 1,000 feet and more when the model is held aloft. In operation, the transmitter is energized, before launching the model, by turning on the volume control. As soon as the model is 50 to 100 feet from the transmitter and has enough elevation, the control button can be depressed. The exact sequence of operation will depend on the escapement used. END

"CENSORED"

may be a horrible word. But when applied to mail order tube advertising in Radio-Electronics, it protects readers from receiving seconds or rejects, when they believe they are buying new tubes. All mail order tube ads must specifically state the condition of the tubes offered for sale...new or used, seconds or rejects.
Fold the top down and back, keeping the cover facing you. Then trim the right and left edges. Now staple the booklet along the vertical center fold, about 3/4 inch from the top and bottom. Now fold from left to right, keeping the cover facing you. Trim a fraction of an inch off the top and trim the bottom to size and you're finished. You now have another useful piece of service data, exclusive with RADIO-ELECTRONICS.
Power Measurements with your Scope

A scope will show you many things a wattmeter doesn’t and will work where a wattmeter can’t be used at all.

Hundreds of important scope applications in electronics work are unknown in many shops. This is not surprising, simply because the field of electronics has become so large. Let us start with a few more basic applications.

A scope can be connected to show either the voltage waveform or the current waveform in a circuit. For example, Fig. 1 shows the appearance of the voltage and the current in a simple neon-lamp circuit.

What do these waveforms show? The current waveform (Fig. 1-b) shows that the neon lamp conducts over a part of the complete cycle. The horizontal line through the pattern is the zero-current level. While the spot is moving along this level, the neon lamp is not conducting.

We see that the lamp jumps suddenly into conduction from the zero-current level. There is a sudden tail spike of current when the lamp ionizes. Thereafter, a sine wave of current flows until the lamp extinguishes. The current is zero for a time; then the sequence is repeated through the negative half-cycle.

The voltage waveform (Fig. 1-c) shows that a clipped sine-wave voltage is dropped across the neon lamp. The resistance of the lamp is practically infinite until the moment of firing. At the instant the tube ionizes, its internal resistance falls suddenly to a low value.

Although the current flow through the tube is changing, the voltage drop across the tube remains practically constant. This is an interesting property of gaseous conduction.

Note that a voltage spike precedes the clipped portion of the voltage waveform. In other words, the striking voltage is greater than the conduction voltage drop across the tube. We see from this why a current spike appears in the current waveform, preceding conduction.

Voltage vs current

Thus, we know that there are voltage waveforms, and that there are current waveforms. Another important type of waveform is the power waveform—a voltage vs current pattern. Let us see what this means.

If we have a load such as a motor connected to an ac line, it draws more or less real power from the line. An induction motor draws a lagging current. A synchronous motor draws a leading current. An ideal motor draws an in-phase current. A suitable combination of motors on a line is practically the same as an ideal motor. In-phase current is drawn from the line, and the power company is happy.

Let us look at Fig. 2. Here, the scope’s vertical input terminals are connected across the line—line voltage is applied to the vertical amplifier. A small resistor, R, is connected in series with the line. The scope’s horizontal input terminals are connected across the resistor—line current is applied to the horizontal amplifier.

The load is a capacitor. A nearly circular pattern is displayed on the scope screen. In this arrangement, the pattern means that the current is 90° out of phase with the voltage. To put it another way, the current does no work. It merely surges in and out of the capacitor, back and forth in the line. All the power in the circuit is reactive power. The rule is: If the power pattern is a circle, no real work is being done by the circuit.

Next, let us look at Fig. 3-a. Here we have a resistive load R. It might be a bank of lamps, for example, or some device that “looks like” a resistor. The scope is connected as before—vertical deflection corresponds to line voltage, and horizontal deflection to line current.

We see a straight diagonal line on the scope screen in Fig. 3-b. This pattern tells us that there is 100% real power in the load. There is zero reactive power. All the current is doing work. It is converted completely into heat by the resistor. No reactive power is surging back into the line.

In many practical electronic configurations, both real power and reactive...
power are present. In other words, the real power is doing work. The reactive power is merely taking current and returning the same current to the line. This situation is shown in Fig. 4. The current drawn by resistor $R$, does work in heating the resistor. On the other hand, the current drawn by capacitor $C$ is merely stored for a short time and then returned to the line. This surging current corresponds to reactive power.

This time the scope pattern is an ellipse. In other words, the pattern is between a line and a circle. The amount of area in the ellipse, compared with the area in a circle, indicates the amount of real power compared with the reactive power. If we choose, we can measure the vertical and horizontal deflections, to determine the power factor, and find the exact amounts of real and reactive power.

Non-sine-wave current

In many electronic circuits, a current sine wave does not flow when a voltage sine wave is applied. A rectifier tube, for example, changes a sine wave into a half sine wave. Thus, many scope patterns are not as simple as those discussed above.

Let us consider the simple power supply shown in Fig. 5. A scope is connected to show current flow into the circuit in terms of vertical deflection, and to show output voltage in terms of horizontal deflection.

Fig. 2a—Load across line is capacitor. Scope connected to show voltage vs current (power) waveform. b—Nearly circular pattern shows practically no real power is drawn from line by capacitor.

Fig. 3—Scope connected to check power in resistive load $R$. (a) produces the straightline pattern (b) that shows 100% real power in the load.

Fig. 4—This basic circuit (a) takes both real and reactive power from the line and produces an elliptical pattern (b).

Critically, the patterns are not as simple as those that would occur when a sine wave is applied. In other words, a sine wave is applied.

Non-real factor

If we were to measure the area of the ellipse, we would find it to be larger than the area of a circle of the same diameter. This is because the ellipse encloses a larger area.

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Wattmeter is no help

Here is an extremely important fact that the electronic technician must keep in mind: A wattmeter test in this circuit is completely misleading. In other words, a wattmeter does not read correctly unless the voltage and current are both sine waves. We know that the current is not a sine wave. Hence, we should never try to check such electronic circuits with wattmeters. A false read-

Fig. 6—Pattern for normally operating circuit.

b—Pattern when output filter capacitor is low in value.

c—Pattern when input filter capacitor is low in value.
ing is unavoidable.*

On the other hand, if we check a motor circuit or a lamp bank with a wattmeter, we read the real power in the circuit. The reading is correct because the load operates from a sine wave voltage and a sine wave current. Note that the wattmeter indicates only the real power in the circuit. An induction motor might be drawing considerable reactive as well as resistive current. The wattmeter shows only the resistive power. The wattmeter does not see the reactive power.

However, we can easily find the reactive power in such a motor circuit by supplementing the wattmeter reading with voltage and current measurements. Many service wattmeters also have current and voltage scales. Here is the basic principle: We measure the voltage and current in the circuit. For example, we might measure 100 volts and 1 ampere. Then, there are 100 volt-amperes in the circuit. Now, if the wattmeter reads 75 watts, 75 watts of real power are present. The 25 watts difference is reactive power (VARS—volt-amperes reactive), which merely surges in and out of the load, doing no real work.

Wattmeters must be used with great caution in electronic circuits. Whenever the voltage or current, or both has a non sinusoidal waveform, we cannot use wattmeters.* By the same token, we cannot use rms reading voltmeters and ammeters. This is why the scope is such a valuable tool in electronics work.

More waveforms

Now let us look at some other interesting waveforms found in a simple power supply. A simple test is made by connecting the scope’s vertical input terminals across the input filter capacitor. We display the waveform in the ordinary manner using sawtooth sweep. Fig. 7-a shows the normal pattern compared with the distorted pattern (Fig. 7-b) displayed when the input filter capacitor is faulty (when it loses capacitance and develops internal resistance). When a filter capacitor develops high internal resistance, it has a poor power factor. We can measure the power factor with a capacitance bridge, which will also show any capacitance loss which may have taken place. In other words, we confirm the scope test by disconnecting the capacitor and checking it on a bridge.

Next, let us connect the vertical input terminals of the scope across the output terminals of a transistor. Whenever the difference is real, the wattmeter reading should be the same as the wattmeter reading when no resistance is in the circuit. Where does the spurious high-frequency oscillation come from? In this example, we do not have a simple resistive load connected to the filter output. Instead, the filter feeds supply voltage to an ac-dc radio. With a faulty filter capacitor, normal bypassing (decoupling) is not accomplished. Instead, the receiver circuits break into spurious oscillation.

The beginner may judge the scope a mysterious and complicated instrument. However, it is really quite simple. It is only necessary to become familiar with reading distorted waveforms, so that we know what they mean. The best way to do this is to start with simple breadboard circuits or ordinary radio receivers which are operating unsatisfactorily. A little practice with the scope will open new fields of electronic savvy.

END

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New Idea in

Tape Recorders

Since corresponding portions of the tape are played at the same speed (approximately) in recording and playback, this speed variation is not noticeable when tape is played back on the same machine. Although two machines were not available for testing, it would seem that tapes could be played back almost equally well by a similar machine; any individual variations would probably be too small to be easily detectable.

Used for voice, the little unit performs very satisfactorily. No attempt was made to check it on music—it does not look to be designed as a hi-fi device. The amplifier has four transistors (the last two in a push-pull output stage). The equipment operates off two size-C flashlight cells, one for the motor and one for the amplifier.

Several recorders of this type are being sold in the U. S. The one shown here carries the brand name Continental.
TV Camera You Can Build

Six-tube instrument at far lower cost than commercial units

By W. E. PARKER

SIMPLIFIED CIRCUITRY AND COMMERCIALLY AVAILABLE VIDICON CAMERA DEFLECTION COMPONENTS NOW MAKE IT POSSIBLE TO BUILD YOUR OWN CLOSED-CIRCUIT TV CAMERA.

The single-unit self-contained TV camera has the essentials of a miniature television station. To form a complete closed-circuit (wired) television system, only the addition of a modern TV receiver is required.

The output signal of the camera is tuned in on a TV set the same way as a standard TV broadcast station is tuned. A single cable connects the camera output to the receiver antenna terminals. No other connections to the TV set are required. The modulated rf signal may be received on channels 2 through 6, depending on how the camera is adjusted. NO ATTEMPT AT BROADCASTING OR OTHER USES OF THE RADIO-FREQUENCY WAVES FOR RADIATED TRANSMISSIONS MAY BE MADE WITHOUT EXPRESS PERMISSION BEING OBTAINED FROM THE FCC.

Applications

There are many uses for the TV camera presented in this article. They are limited mostly by the user's imagination and the available light necessary for a satisfactory picture. From observing junior in his crib to the salesman knocking at your front door, there are limitless possibilities for your own private television system.

For the licensed amateur radio operator who contemplates the thrill of amateur TV transmissions on the currently authorized 420- to 450-mc band, this TV camera is ideal.

Now build it

The camera (Fig. 1) is housed in an 8 x 10 x 4½-inch aluminum case that is built around the chassis. The two end sections are the same size and shape. The bottom is a piece of 3/16-inch aluminum plate with a ¼-20 hole tapped near the point of balance for tripod mounting. The top section requires only two right-angle folds. One of the side panels has ventilation holes. The side panel without openings covers the wiring side of the chassis. No attempt was made to miniaturize the camera. Simplicity and accessibility are the keynotes of its design.

While not critical, parts placement must be considered. Weight distribution and ventilation were also considered in the parts layout. Locate the power

www.americanradiohistory.com
Fig. 1—Complete circuit of the home-built camera.
transformer away from the deflection components. Arrange the first video amplifier as near as convenient to the signal ring of the vidicon. Keep the rf oscillator away from the first video amplifier or provide adequate shielding.

The beam, target and focus controls are adjusted frequently, and must be readily accessible. The remaining controls require less adjustment after initial setup. The horizontal sweep generator consists of V7-a and V7-b connected as a cathode-coupled multivibrator synchronized by V6, a 15, 750-cycle crystal oscillator. An alternate circuit with L-C stabilization is shown in Fig. 2. If the L-C stabilized horizontal oscillator is used, it may be wise to provide external adjustment for the HORIZONTAL FREQUENCY control.

Small insulated standoffs were used in place of terminal strips. The peaking coils are inexpensive standard replacement units.

Early adjustments

The vidicon is relatively delicate and must be handled with care. Be especially careful of the area around the exhaust tip (Fig. 3).

Many initial checks and adjustments can be made without the vidicon tube installed. This is a good idea as its photosensitive surface can be damaged by improper deflection or loss of deflection.

With all tubes except the vidicon installed, measure the three power supply voltages. Even if the camera is not adjusted properly, this will not affect the readings appreciably.

Adjusting L4 while watching a nearby TV receiver should produce some bars on the screen if the receiver is tuned on one of the lower-frequency unassigned channels. This shows that the rf oscillator is working and the modulator is modulating the rf carrier. The bars are caused by the vertical and horizontal sync information. If an attempt to lock in the picture fails, the next step requires a general-purpose oscilloscope.

Waveforms

With the vidicon tube still removed, examine the vertical waveform on your scope screen. Do not proceed until waveforms almost identical to those shown in Fig. 1 are obtained. It is not absolutely necessary that the amplitude of the waveforms be exact at this point.

Check the horizontal waveforms next. They will differ from camera to camera to some extent. Do not install the vidicon until both the horizontal and vertical waveforms are reasonably correct.

When you have reasonably correct waveforms, a locked-in raster without video modulation should be obtainable. To check the video amplifiers place the tip of a screwdriver near the grid of V1-a and look at the locked-in raster on the TV set. Wavy lines or bars will be seen, indicating that the video amplifier is capable of amplifying.

Before installing the vidicon, check each socket pin for proper voltage and whether it can be varied by the associated control. Upon completion, install the vidicon tube, making certain that the signal electrode is connected and does not touch ground. Place the lens system in position.

Do not expect to see a picture right away! Expect to see blurred light and dark areas that move as the camera is positioned.

However, by adjusting the lens and the beam, target and focus controls an image should form. Adjust the linearity, height and width controls to improve the picture further. The positioning controls will aid in picture alignment. It may be necessary to rotate the yoke.

Lens systems

A lens with a focal length of approximately 1 inch (25 mm) will do nicely for general coverage. A lens with a speed of F:2.8 or better that has an adjustable iris will prove satisfactory. Movie camera 16-mm lenses are recommended, although some 8-mm lenses will do.

Miscellaneous

The deflection components are available from Cleveland Electronics Inc., 1974 E. 61 St., Cleveland 3, Ohio. The VK-200 coil kit is of the highest quality. The alignment coil was not used and need not be ordered. The scanning beam is aligned by passing a small amount of de through each of the deflection coils (see R40 and R63). If you wish to wind your own coils, you will find all needed data next month.

Grade B and C vidicon tubes are available from Al Denson, P.O. Box 122, Rockville, Conn. (A grade-B tube has minor imperfections that are of little consequence to hobbyist, ham or home experimenter.) Vidicons other than the 6198 may be used.

Next month we'll also see just how each of the many camera circuits operate.

Kerosene Generator Powers Radio

This Aztec thermoelectric generator will power a transistor radio for 24 hours on one pint of kerosene. It delivers ½ watt at ¾ volt to a transistorized voltage converter built into the base of the lamp. This unit steps up the output to 6 volts dc at 175 mw. The lower photo is a view looking straight down on the generator when it is in place over the lamp. Made by Minnesota Mining and Manufacturing Co., the Aztec generator is designed as an emergency power source for use in fallout shelters, farms, sportsmen's camps and other remote locations away from power lines.
TUNNEL DIODE-TRANSISTOR MODULES operate at bit rates as high as 500 mc. They go together to form a computer system that can add four times as fast as conventional computers with only one-tenth of the circuit components. The G-E-built system is officially called a pumped tunnel diode-transistor logic system.

REAR WINDOWS IN RADAR CRT allow auxiliary displays to be projected onto the tube screen along with the actual radar image. For example, you might project a map or grid onto the face of the tube. Then the radar display would indicate exactly where the pip was located in relation to the area shown on the map. The tube was developed by General Atronics Corp.

ULTRASONIC TRANSLATOR turns 35,000- to 45,000-cycle sound into audible frequencies. It's used to detect early stage friction in bearings, bushings and other machine parts. Here an engineer is checking for lubrication requirements on the tail rotor drive shaft of a helicopter with The Deleon Leak and Friction Detector.

BALL TRACKER centers the pip on radar screen. The single control adjusts two potentiometers simultaneously, speeding the process considerably. Turning the ball moves the pip both horizontally and vertically at the same time and the operator has only the one control to fuss with, rather than two interdependent controls. The device is made by Hughes Aircraft.
By JOSEPH MARSHALL

The purchaser of an FM tuner kit looks for two things—the highest possible performance and the greatest immunity to trouble in assembling and adjusting it. Since these two ends conflict, the kit tuner designer is faced with no easy problem. The Dynatuner presents a most interesting and unconventional solution from a circuit standpoint.

The FM-1 Dynatuner bucks the current trend in front ends by using a cathode-coupled rf stage instead of the almost universal cascade or the new nuvisor neutrode. The noise figure of the cathode-coupled stage is inferior to a cascade arrangement with the same tube or an equivalent triode in the neutrode circuit. But it has some very significant advantages over the other two—particularly in a kit. It is much simpler and less critical than either the cascade or neutrode, requires no neutralization and fewer parts. Also it is less susceptible to cross-modulation and thus more nearly immune to spurious signals in local areas and easier to construct and align.

Despite its higher noise figure, the Dynatuner has a very respectable effective sensitivity. The manufacturer specifies 4-µv IHFM sensitivity, and individual tuners have measured sensitivities as good as 2.5 to 3 µv. Very few run higher than the specified 4 µv.

**Circuit features**

The converter is also unconventional, though not new. Oscillator voltage is injected into the screen of a pentode through a direct connection to the plate coil of the tuned-plate-tuned-grid oscillator. This gives a high degree of injection, which results in exceptionally uniform gain over the entire FM band. Moreover, it isolates the local oscillator from the tuned circuit in the converter grid, resulting in almost complete freedom from “pulling.” As a result, the tracking adjustment for the front end is uncritical, since converter-coil peaking has no effect on the oscillator frequency. Also, strong stations adjacent to weak ones do not “pull” the tuner away from the weak stations. The oscillator is carefully temperature-compensated and shows no significant frequency drift even in the very first few minutes of operation.

The four-stage if amplifier is arranged by proportioning the plate and bias voltages so that all four provide some amplification on weak signals and some degree of limiting on strong ones. The gain is so high that, with no signal input, the noise of the input tube alone is enough to produce some limiting. The tuner has an extremely steep limiting curve and suppresses noise completely on inputs as low as those needed for equivalent noise suppression with tuners of higher absolute sensitivity. Although a 3- or 4-µv signal is needed for 30-db noise suppression, only 6 µv is needed to produce a 40-db signal-to-noise ratio and about 10 µv for 50-db noise suppression. Complete limiter saturation occurs with a signal of around 25 µv and results in a 60-db noise ratio.

Tuner sensitivity is more effective because of the extremely wide bandpass of the if amplifier. It appears to be between 270 and 300 kc wide—as far as I am aware the widest bandpass in any tuner today. More remarkably, it is
WITH A TWIST

It has an add-on power amplifier, a very unusual power supply and some circuitry that is rare in FM.

done with undercoupled if transformers and thus produces a response curve with a single hump. This permits accurate alignment with very simple means. Thus even an overmodulated signal finds plenty of room to pass through the tuner without generating significant distortion. Signals above 5 or 6 µv have completely negligible distortion—0.5% or less. Even at the 30-db IHFM test point, distortion is only about 1% and constitutes only a third of the residual noise.

Since random noise is more tolerable than distortion, extremely weak stations, even those with poorer than 30-db noise ratio, are often more tolerable than with tuners of higher sensitivity but narrower bandwidth. Such tuners provide greater noise suppression but produce higher distortion. In our tests we found that although a signal may be too far down in the noise to be intelligible, even the weakest signal is not too distorted to be intolerable.

The tolerance of overmodulation—unfortunately all too common—is almost phenomenal. With a signal generator you have to exceed 200% modulation before distortion becomes audible annoying.

Despite the wide bandwidth, skirt selectivity is good. The "alternate-channel" selectivity (400 kc from resonance) is better than 50 db. Hence, there should be no trouble with interference in local areas where stations are spaced at least 400 kc apart. It is quite possible to separate two stations 200 kc apart unless one of them is many times stronger. Indeed, the 200-kc selectivity is considerably better than average because of the lack of oscillator pulling and the good capture ratio (6 db). The selectivity may be inadequate only in the case of a listener, for example, in New York who desires to hear a station in Philadelphia only 200 kc from a local station. (However, only two or three tuners, using six or seven if transformers, can give acceptable reception in such a situation.)

The detector

Although at first glance this looks like a ratio detector, it is actually a balanced-bridge discriminator using a pair of matched crystal diodes. Because of the bridge configuration, it provides a high degree of AM and noise suppression, like a ratio detector. This is true because the AM and noise divides equally between the two legs of the bridge and are cancelled in the output, whereas the FM is always unequal in the two legs and the output represents the difference. The detector bandwidth is only moderately wide—about 600 kc—but, with the very stable local oscillator and the wide passband of the IF amplifier, provides uncritical tuning.

A very simple and foolproof method has been devised by the designers for aligning the detector, using the tuner's own electron-ray indicator.

For years I have considered the counter the best of the FM detectors. On direct comparison, I find that the Dyna balanced-bridge is closely equal in terms of low distortion, and superior in AM and noise rejection. The counter permits the noise of the final limiter to come through; the Dyna suppresses this final noise component effectively. The Dyna detector is superior to the ratio detector in distortion.
and nearly equal in noise suppression. It is superior to other discriminators both in lower distortion and noise suppression. The use of solid-state diodes further maintains the maintenance of an extremely low noise level, not only because of the inherently lower noise level of crystals over electron tubes, but also because with no heaters no hum is injected at this point. The detector's performance is further aided by its coupling to the audio stage through the high impedance of a cathode follower. This prevents loading the detector by the de-emphasis network (R30–C28).

The audio amplifier has more than 20 db of feedback. In fact, the stage gain is only 10 db. The response curve is unusually wide, ranging well below 1 db from below 20 to above 50,000 cycles. Overall distortion is well below ½% from 20 to above 20,000 cycles for any signal exceeding 10 µV.

As this is being written the Dynatuner MX adapter is not yet available. However, the design of the tuner forecasts exceptionally good stereo FM performance, assuming a multiplex circuit as good as that of the tuner. The very wide passband, the outstanding ability to receive weak signals with low distortion, and the flat audio response are all highly favorable for multiplex reception.

Meanwhile the manufacturer does offer a very compact 10-watt amplifier (model FMA-2) which will fit the space left for the stereo adapter and thus provide a complete FM receiver. This amplifier is also notable for the unconventional but clever way it uses the very small power transformer of the tuner to power both the tuner and the amplifier.

Built-in power amplifier

If one of these tuners is brought into your shop with the power amplifier, you may well jump to the conclusion that the tubes are a terrible boner in wiring. Actually the wiring is correct (Fig. 1), and the amplifier operates with conventional voltage parameters. If you measure the voltages from cathode to plates and grids, you will find that the plates are about 250 volts positive and the grids around 14 volts negative, as they should be. And, while it is true that the power supply delivers around 70 ma to the output tubes and another 70 ma to the tubes in the tuner, the transformer is operating only some 5% above its dissipation rating, which is well within its tolerance. How is it possible to steal 70 ma from a power supply with a 100-ma rating without overheating the transformer?

Fig. 2 is a simplified diagram showing the power supply as it looks when the amplifier is added. A pair of diodes is connected across the transformer with the cathodes on the transformer side to rectify the negative half-cycle. The normal “full-wave” rectifier makes only partial use of the negative half cycle. By using it with another pair of rectifiers to feed a second load, we do increase the total load on the transformer. This is partly offset by the fact that operation is 30% more efficient in this mode. If we put a load on the negative supply equal to the load on the positive one, we increase the dissipation of the transformer only 50% instead of the 100% you would expect. Since the Dynatuner transformer was operating with a 60% factor, the addition of the 70-ma load of the amplifier merely brings the dissipation up to the rated dissipation of the transformer or perhaps 5% more. In any event, the transformer heats little or no more than it would if it were drawing the full 100 mils of current with a single full-wave rectifier.

Some adjustments have to be made to make this thieving power supply work well. The filaments of the EL84's must be fed by a separate transformer. Otherwise the heater-to-cathode potential would be around 250 volts, considerably above the permissible potential difference. The two halves of the power supply should be as closely balanced in load as possible. In this instance, the 12AX7 of the amplifier is fed by the tuner power supply, thus adding just enough drain to balance the two sides.

The amplifier circuit itself is only slightly modified from the standard Dyna configuration. The output transformer is smaller and not as linear as the bigger Dyna transformers. It will deliver 10 watts with less than 2% distortion from 30 to 15,000 cycles. Below 30 cycles and above 15 kc, the power output slopes and distortion is higher. The voltage amplifier is direct-coupled to the phase splitter through a voltage divider which is compensated with a capacitor to provide a step at the low-frequency end to make up for the slope of the output transformer and thus maintain stability at the low end. There is an inner feedback loop from the plate of the lower output tube to the input cathode to provide a step at the high end and to compensate for the frequency unbalance at the high end of the split. Also, there is a feedback loop around the input stage.

Although extremely compact and inexpensive, the amplifier delivers excellent performance. It was demonstrated at the Chicago and New York shows driving an AR-2 speaker to perfectly satisfactory levels even under the rather high noise levels that exist at shows. In no sense a substitute for a bigger amplifier, it does offer an economical and simple means of obtaining FM reception where space and cost are the main considerations. It is also ideal for use as a supplement to a big high-fidelity system for use in the bedroom, kitchen, porch or summer cottage.

Miscellaneous notes

The Dynatuner is available in three forms—the normal kit, a partially assembled kit and fully assembled. In the normal kit, the constructor mounts

Fig. 1.—You'll note that in this power amplifier the screens and plates of the output tubes are grounded.
replacing Japanese transistor radio batteries

JAPANESE RADIOS USUALLY COME WITH JAPANESE BATTERIES. When these wear out and have to be replaced there is often some confusion on what US replacement to use. Perhaps this little list will help.—Warren Roy

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<th>Burgess</th>
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**REPLACING JAPANESE TRANSISTOR RADIO BATTERIES** (sizes shown are approx actual)

MAY, 1962

END
Measure dc millivolts with a dc-to-ac converter

By FORREST H. FRANTZ, SR.

Simple, low-cost unit adapts ac vtm for low-level dc voltage measurements

The problem of measuring small dc voltages rapidly and accurately has challenged the electronics industry for years. Many practical measurement techniques and instruments have been developed, but most of them have been beyond the practical reach of the experimenter, hobbyist and service technician. Most dc millivolt measuring instruments cost hundreds of dollars.

Another difficulty has been zero drift—a problem encountered when vacuum tubes or transistors are employed as direct-current amplifiers in the instrument. And even the comparatively simple potentiometer type of dc measuring instrument, although it is extremely accurate, is objectionable because of the time-consuming nulling procedure.

The most satisfactory approaches to the problem of dc millivoltage measurements have usually involved a dc-to-ac converter. The ac output of the conversion unit is proportional to the dc input in this scheme, and can readily be measured with an inexpensive audio voltmeter such as the Heathkit AV-2 or AV-3 or with an audio amplifier and the ac range of a multimeter (Fig. 1). The multimeter is set to a low ac volts range and connected to the amplifier's output. The converter feeds the amplifier's input. With the amplifier's gain set fairly high, use the amplifier's gain control and the converter's scale-factor control adjusted so the multimeter reading corresponds to the dc input.

The dc-to-ac converter described in this article is intended to be used in this way. Its cost is less than $10. Extremely compact—only 1½ x 2½ x 1 inch—it can be assembled in about 2 hours. Power is obtained from a
The entire unit fits into a small plastic case.

single self-contained inexpensive penlight cell. Battery current drain is approximately 1 ma.

How it works

The basic circuit of the audio oscillator used in the dc-to-ac converter is shown in Fig. 2. Note that the dc voltage to be measured furnishes the dc operating voltage for the audio oscillator. The desired response is an oscillator audio output voltage directly proportional to the dc voltage supplied at the input. On a graph of ac output voltage against dc input voltage, this would be a straight line.

Curve A of Fig. 3 shows that, if the emitter bias $R_3$ is unbypassed, the audio output is not a linear function of the input, and above 0.25 volt dc input, the audio output voltage is constant. This characteristic would be highly desirable where a constant output signal is desired regardless of battery-voltage variations. But it is unsuitable for a dc-to-ac converter. Also note that oscillation does not begin till the applied dc voltage is 0.12 volt or more.

If the emitter resistor is bypassed with a 10-pf capacitor, the response is linear as shown by curve B. If $R_3$ is decreased, the slope of the curve gets steeper as shown by curves C and D. Furthermore, oscillations begin when the applied dc voltage is only 0.7 volt.

Although the desired linear response has been achieved and oscillations do begin at 0.7 volt, the range of the arrangement can be useful only if oscillation begins just above zero volts. This can be done by inserting a 0.7-volt dc bias in series with the dc input voltage. This shifts curves B, C and D in Fig. 3 to the left so they can pass through zero.

The circuit for the practical converter is shown in Fig. 4. The variable-emitter resistor $R_4$ is the scale adjustment which varies the slope of the response curve. The battery and resistors $R_1$, $R_2$ and $R_3$ provide the bias voltage for zeroing the converter. The resistance of the voltage divider is small in comparison to the converter’s input resistance. The zero bias required may vary slightly from one converter to another due to transistor and component tolerances. Potentiometer $R_3$ adjusts the bias for these and for battery aging.

$R_3$ and $R_4$ are adjusted when the instrument is calibrated initially and must not be readjusted each time it is used. $R_4$ should be checked and, if necessary, readjusted about every 6 months to compensate for battery aging.

Construction and calibration

Building the unit is comparatively simple. Make the holes for the potentiometers, transformer, on-off switch, input leads and output jacks first. A heated ice pick and a taper reamer will do the job nicely and minimize the risk of cracking the plastic case. Mount the potentiometers and output transformers next. A small piece of perforated board forms the chassis. After all connections are made and the unit is checked for operation, cement the perforated board to the potentiometers.

To calibrate the converter, adjust $R_3$ to about 2,500 ohms, and connect the output terminals of the converter to the audio vtm. Set the audio vtm to the 0.01-volt range and short the input terminals of the converter. Adjust $R_3$ till oscillation begins (evidenced by an up-scale reading on the audio vtm). Then back off $R_3$ to the point where oscillation just ceases.

Next, connect the converter terminals to a 0.3-volt dc source with the audio vtm set on its 0.3-volt range. This voltage may be obtained from the circuit shown in Fig. 5. Adjust $R_4$ for full-scale meter deflection. Disconnect the converter terminals from the voltage source and short them again. Repeat the $R_3$ adjustment, since the change in $R_4$ may alter the oscillator zero bias slightly.

Curve E in Fig. 3 shows the response of the completed instrument. The dc-to-ac ratio is 1 to 1. The calibration is as good as the accuracy of your calibrating voltage and the care you put into making the calibration. The range of the converter is 0 to 0.3 volt, which you can cover in four ranges — 0.01, 0.03, 0.1 and 0.3 volt — with the range switch of an audio vtm. Since voltages above 0.3 can readily be measured with a conventional general-purpose vtm, no provisions were made for using the converter to measure higher voltages.

---

**Fig. 4—Circuit of dc-to-ac converter.**

**Fig. 5—Calibration circuit. Adjust $R_3$ until dc voltmeter reads 1 volt.**
Parts are arranged in both halves of the case.

The converter will draw approximately 8 mA from the dc circuit if it measures for a 0.3-volt input and approximately 3 mA for a .03-volt input. Circuit loading is quite small, and accurate measurements may be anticipated for circuits of moderately high impedance. If a dc-to-ac conversion ratio of less than 1 to 1 is employed by increasing the value of R4, input current requirements can be reduced even further. Since the 1-to-1 conversion ratio allows direct reading from the ac vtvm meter scale and range switch, it was considered more advantageous than an arrangement which would introduce a conversion constant that had to be remembered and applied to meter readings. This way we get an easy-to-use direct-reading instrument.

The emitter resistor R4 stabilizes the circuit against drifts due to temperature changes. Any user of this circuit will be well pleased with its stability, linearity and overall performance.

**WHAT'S YOUR EQ?**

It's stumpin' time again. Here are three little beauties that will give you a run for the money. They may look simple, but double-check your answers before you say you've solved them. For those that get stuck, or think that it just can't be done, see the answers next month. If you've got an interesting or unusual answer send it to us. We are getting so many letters we can't answer individual ones, but we'll print the more interesting solutions (the ones the original authors never thought of). Also, we're in the market for puzzles and will pay $10 and up for each one accepted. Write to EQ Editor, Radio-Electronics, 184 West 14th St., New York, N. Y.

For answers to last month's puzzle see page 68.

---

**Variable-Current Black Box**

This particular Black Box has two terminals. When 50 volts dc is applied, 2 amperes flows. If 100 volts at 60 cycles is the supply source, the current is 12 amperes and the power 1,200 watts. With 151 volts at 400 cycles, the current is 10 amperes.

Draw the circuit and give the values of the components in the Black Box.—Frank A. Lopez

---

**An Easy One?**

Some readers have complained that many of the problems require calculus—or at least quadratics—to figure out. Here is one that can be done without calculation. Observe the circuit pattern and determine the voltage across the 1-ohm resistor.—Albert C. W. Saunders

---

**Iterative Network**

Engineers will recognize this problem as the very simplest type of iterative network, but it will be interesting and useful to beginners. Good training for transmission lines, too!

The circuit shown above consists of 1-ohm resistors. The lattice extends to infinity. What is the total resistance of R, looking into points A and B?—Mordehai Arditti.

---

Making Twisted Cable

By ELMER CARLSON

LENGTHS OF TWISTED PAIRS OF WIRES for filament and power circuits can be easily made with a hook bent from 3/16-inch OD tubing or rod. It may be necessary to heat some rod or tubing while bending it.

If both wires are the same color, simply unravel a little more than twice the required length and, with the loose ends held together, tie an overhand knot. With the knot end held in the hook, loop the doubled end over some solid, stationary object (a doorknob or tightened vise handle will do), and start winding with the drill (Fig. 1). For extremely long lengths, use an electric drill.

Fabric-covered wire needs a different technique. It is necessary to provide some means for the individual wires to twist at the far end while winding. This requires a special jig consisting of two parts and for best results, an assistant.

Each wire is tied separately to an eyebolt mounted on a plate. The ring is on one side, a flat washer and two nuts on the other (Fig. 2).

---

When three or more wires are twisted, a separator must be used to steady the wires. This keeps them from whipping, and maintains their spacing for a smooth, even twist.

A discarded ping-pong paddle can be used. It is evenly notched along the edge with keyhole-shape slots to guide the wires. As twisting progresses, the assistant moves away from the twisting end, keeping the wires separated.  

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Very seldom do troubles occur in TV transmitters or control equipment. However, no experienced engineer would deny that they do happen now and then. If the TV technician can recognize them, he may save a lot of time spent tearing down innocent TV receivers.

One of these troubles is occasional overmodulation of the transmitter. This results in an almost complete “white-out” of the screen (Fig. 1). It is caused by overmodulating the video carrier transmitter, thus reducing the amount of signal being radiated. Fig. 2 shows the difference between 100% and 120% modulation, which is about the level equivalent to the effect shown in Fig. 1. Note that actually less rf is being radiated during the overmodulated periods.

With our TV sets designed as they are, the stronger a signal is, the blacker our pictures are. In other words, our TV receivers start with a white screen. The signal extinguishes the beam of the picture tube by cutting it off. So if we receive a very weak signal, areas in the picture which should be black are gray, because the signal is too weak to make them a clean black.

This type of trouble occurs more often with smaller stations. The larger stations, and the network originating stations, have very well designed automatic devices to prevent this. Fast-acting age circuits in the video output (before the video signals are added to the sync) maintain a constant level. At times, troubles are found in the station itself. At one station, the age circuit was installed, by mistake, in the output of the console going to the transmitter. Here, it controlled, not only the video, but the total amplitude of the signal, sync and all. Thus, when a white burst came along, the net result was not only overmodulation, but a severe case of momentary sync clipping.

One other question often heard concerns the ghost images seen on the screen after the cameras have been moved to another shot. Lettering from commercials, the newscaster’s head, and other stationary objects can be seen on the screen, overlying the other subject. This is due to burning-in of the image on the mosaic of the image orthicon in the camera. It generally means that the tube has just about reached the end of its useful life. At times, even with a good tube, it is possible for an inexperienced camera operator to burn in an after-image on his screen by carrying his beam current too high. However, the chief engineer usually takes care of these gentlemen, especially after he watches a program or two.

Color shrinking
My RCA CTC4 color TV shrinks sideways on color programs only. Black-and-white reception seems OK. Width control is at its full-width position. High voltage runs about 28,000 volts.—J. I. H., Reseda, Calif.

I’ve run into this problem on several sets, including mine, and the answer seems to be something different each time (shrinkage, that is, not necessarily on color only).

The major cause seems to be a very slightly weak 6CBS horizontal output tube. Try replacing this tube, also the damper, and resetting the drive and high-voltage controls. Incidentally, RCA now OK’s the replacement of the 6BL4 damper tube in this series with a 6AU4-GT. Since they brought the voltage rating up on the 6AU4, it will work here.

One more cause here might be burned resistors in the high-voltage lead. Check the three 22,000-ohm resistors inside the doghouse, near the high-voltage connector. They have gone out in several sets when the focus control went bad. While you’re in there, have a look at R306, R276, the two 1-megohm resistors in the focus circuit.

There is one more rather unusual prospect in this circuit, the video amplifiers. Due to the weird circuitry (for black-and-white TV practice) used in the brightness and contrast control circuits, it is also possible for a defective final video amplifier tube or stage to cause a problem along these lines. In other words, if the video amplifier can affect the brightness, it can certainly affect the width, by changing the CRT beam currents. It’s worth checking out, at any rate. Look for leaky coupling capacitors and shifted resistors in the video grid circuits.

By the way, you might look at the three pots in the screen control circuits, too. These parts carry the 800-volt B-boost voltage and they can run pretty hot and burn up sometimes. This causes color-hue drifting and assorted troubles along that line. However, if your background and color temperature are OK, they’re OK too.

No vertical sweep
I have an Admiral 20Z/PS TV on the bench that is giving me lots of trouble. No vertical sweep. I read about 800 volts on the 6S4 plate, but there’s no pulse there at all. I’ve tried a new yoke, without results. The two 18,000-ohm resistors from boost to the output transformer are overheating. I ought to get 580 volts on that plate, but it isn’t there.—M. S., Monterey, Tenn.

I believe this trouble is going to be found in the vertical output transformer. It sounds as if it is leaking to ground. If the two 18,000-ohm resistors between boost and the bottom of the output transformer are overheated, something is causing excessive current drain in that circuit. If the tube has been changed and the yoke checked for grounds, then there is only one thing.
left—that vertical output transformer (Fig. 3).

There is one other possibility, but I expect you've checked that: the 10-µf electrolytic capacitor connected between the vertical output transformer (the red wire) and the 6S4 cathode.

Also check the 20-µf electrolytic between cathode and ground. Incidentally, if the 10-µf unit is shorted, it could have blown the vertical linearity control, opening the cathode of the 6S4 or shorting it to ground through the bad capacitor. Both have been known to happen. Sudden opening of the cathode could have caused a spike of voltage to be fed to the transformer, causing the windings to break down to the frame.

You should read about 425 volts on the load side of the two 18,000-ohm resistors and about 410 volts on the 6S4 plate. Check the resistors for signs of changing value due to overheating.

Double-trouble

An RCA KCS-19 keeps blowing the ½-amp fuse in the high-voltage supply. Whenever I change it, the set plays for a while (several hours to a day or two) and then it blows again. I changed the 6BG6-G and the damper tube, and it blew just as soon as the high voltage came up! The only trouble I can find is a charred resistor feeding the vertical output transformer primary from the boost. I replaced the resistor and the 6K6 vertical output tube. This time it played for about ¼ hour before the fuse went out again—K. M., Pittsburgh, Pa.

It looks as if the thing is trying to throw you a curve, with that burned resistor in the vertical circuit. From the description, I'd say that this was the result of a previous short in the vertical output tube some time ago. The only cause for this trouble (in that circuit) would be an intermittent short to ground in the vertical output transformer and this would cause a different set of symptoms. Every time this has happened to me, the immediate result has been a sudden collapse of the vertical sweep (the thin white line) followed by the fuse blowing.

I think you'll find the trouble in the horizontal output circuit. Look for excessive screen voltage on the 6BG6-G, an intermittent short in the width control or the horizontal drive trimmer.

Fig. 3—No vertical sweep in this circuit may be caused by the vertical output transformer windings being partially shorted to ground.

Check plate current of the 6BG6-G. This should be 80 to 105 mA and never over 105 mA.

Check the de drive voltage on the 6BG6-G. This should be about 22. I would recommend monitoring as many of these voltages as possible simultaneously while watching the set to see what happens when the fuse goes.

You might try replacing the 6W4 damper tube with a 6A4 (which has a much higher heater-cathode breakdown rating) and clipping off the heater-cathode jumper at the socket. There is a possibility of an intermittent ground in the damper heater winding in the power transformer.

Needs a flyback

I'm working on a Crosley 10-410MU set with a burned-out flyback. The original part number is NAC 14744. I can't get one anywhere. Can

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61
Horizontal roll

An Admiral 24UY3C has horizontal roll. I can hold the picture still with the adjustments for a minute or two, then it falls out both horizontally and vertically.

I've replaced all parts in the oscillator; ringing coil, etc.—T. O'B., Prosser, Wash.

This trouble is in the sync circuits, not in the oscillator, since you can hold

Fig. 4—Changes shown in sync circuit will improve its action.

a picture still with the horizontal hold control.

I suggest changing the horizontal afe diodes; they are the most common cause of trouble in such complaints.

To improve sync, there have been some modifications in the sync circuits of this set. Fig. 4 shows the original parts and the changes.

Drift after warmup

I repaired intermittent horizontal drive in a Bendix TM17, then it had insufficient height, the complaint it came in for! All waveforms are OK, but brightness increases after warmup, width and linearity change, and the vertical hold is critical—F. C., New York.

This is damper and boost trouble, apparently. Run a complete adjustment on the horizontal linearity. From the symptoms, it sounds as if the horizontal linearity is not set properly and is on the edge. Also, replace the 6W4 damper with a 6A4U, which has a higher current-carrying capacity.

April 15—May 15

By STANLEY LEINWOLL

This month a major change is being made in the propagation tables.

In the past we have shown for each hour the short-wave broadcast band nearest the optimum working frequency. This has restricted the use of the tables to short-wave listeners interested in international broadcasting.

To make the tables more useful to the many other users of the high-frequency spectrum (fixed, amateur, aeronautical, etc.), the tables will hereafter show the optimum frequency, in megacycles, for propagation of short-wave signals between the locations shown during the time periods indicated.

To use the tables, select the one most suitable for your needs and your location, read down the left side to the region in which you are interested, then follow the line to the right until you are under the appropriate time. (Time is given at the top of each table in 2-hour intervals from midnight to 10 pm, in your local standard time.) The figure thus obtained is the optimum working frequency, in megacycles.

The best band for the particular service in which you are interested is the one nearest the optimum working frequency.

For example, a resident of New York City would use the Eastern USA table. At midnight, signals to and from Western Europe would be optimum in the 8-mc band. A radio amateur would be most likely to establish communications in the 40-meter (7-be) band. A short-wave listener would try the 7-, 8-, and 9-mc broadcast bands, in that order.

The tables are designed to serve primarily as a general guide, since day-to-day variations in receiving conditions can be considerable. At certain hours, propagation over some of the paths given in the tables may be extremely difficult or impossible.

In general, circuits passing through the northern auroral zone will be more difficult than those over more southerly paths. In addition, circuits lying entirely in daylight or darkness will be better than those passing from daylight to darkness, or vice versa.

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MAY, 1962
PUT MORE ON YOUR TAPE

By JAMES MASKASKY

Nearly all systems for multi-channel tape recording are either too complicated or too expensive for the average audiophile. There is one method you can easily experiment with at home. By taking advantage of an angular property of tape recording, you can record and play back six or more channels with one ordinary half-track tape head.

Before we go any further, one condition behind this system must be made clear. When recording, the erase head must be disabled. If you have a recorder with permanent-magnet erase, you have no problem—simply remove the erase magnet. But if you have a tape recorder with a multiple-function head, you may not be able to disable the erase head. If you have a recorder with a separate erase head, remove the head but leave it connected. Its inductance may be a part of the bias oscillator circuit. If it is and you disconnect it, you will not be able to record properly. I added an additional record-playback head on a special mount so it could be rotated as desired. Naturally, I selected a head that matched my recorder. I left the erase function on the original head.

How it works

In ordinary tape recording, the record head is perpendicular to the tape and the signal recorded on the tape runs the full height of the gap in the record head (a trifle less than the ¼ inch for half-track heads, shown in Fig. 1). Now if we rotate the record head 60° to the right, we can rerecord the portion of the tape that is now covered by the tape-head gap height.

Fig. 2-a shows this vertical height to be cos 60° times the original height: ½ × ¼" = 1/16 inch for the height of the remaining part of the first channel. A picture of the tape after this two-channel recording is in Fig. 2-b.

Before we discuss playback, let's look into some elementary tape recording theory. If a tape is recorded at one angle and played back with the head at a different angle, signal strength drops and distortion increases. This becomes increasingly noticeable as the playback angle increases relative to the record angle.

Playback problems

Now let's go back to our prerecorded tape (Fig. 2-b). The second signal, recorded at 60°, can be played back if we turn the playback head to the same angle. Since this is the only signal that crosses the tape head, it will be the only one audible.

Fig. 1—A half-track record head has a gap that is slightly less than ¼ inch high. For convenience ½ inch is used.

Fig. 2—Composite diagram shows the signal on the tape when two channels are recorded on the same track.

Fig. 3—Here, three channels are recorded on a single track.

Fig. 4—How gap width is figured for various angles of tilt.

Rotating the tape head back to 0° we get the remaining portion of the vertical signal on the extremes of the tape head, and the second signal at an angle of 60° in the middle of the tape head. Since this angle is large enough to cause a significant reduction in volume of the middle signal, we hear only the signal originally recorded on the first channel.

By expanding this one more step, we can see that by choosing a number of angles, three or more signals can be recorded on each half track. The theoretical angles for three channels would be: (cos⁻¹ 1), (cos⁻¹ ½), and (cos⁻¹ ¼).

The author used this arrangement to tilt the head to the desired angle. Assembly has its own built-in tape guides.

The tape head has been rotated 60°.
In numbers, this would be approximately 0°, 45°, and 70°, but for practical reasons (they're explained later) 0°, 45°, and 60° were chosen for three channels. Fig. 3 shows the magnetic pattern of this three-channel system. For four channels, the angles could be 0°, 40°, 55° and 70°.

One question some reader may be asking at this point is, "Why was 90° ruled out as a limit?" For this apparatus, it is impossible to get an adequate signal at 90° because the gap height (1/8 inch) becomes the tape-head gap width seen by the tape, which means that at 7 1/8 ips, the top theoretical frequency is 30 cycles.

**Angle vs response**

This reminds us that we had best consider the effective gap width and the frequency response for the angle we intend to use. In Fig. 4 we have illustrated what happens in our three-channel system, but the same thing happens to any number of channels. As illustrated in Fig. 4-a, the vertical signal width equals W (1/cos 0°), or W, where W represents the original gap width. For the second angle, the effective width equals W (1/cos 45°), or 1.4 W. For the third channel, it is W (1/cos 60°), or 2.0 W. This is shown in Figs. 4-b and 4-c.

Since the top frequency is inversely proportional to the gap width when the tape speed is constant, the result is that the top frequency for channel 2 is 0.7 times channel 1's top. And channel 3 is 0.5 or 0.33 the maximum frequency of channel 1.

A few practical experiments showed that any recorded selection with an angle greater than 70° was too poor in quality and too difficult to tune to be of any use. This is why 60° was chosen as the largest for three channels, leaving 45° as the best possible choice for the other angle.

The measured crosstalk for two channels (0° and 60°) was better than -60 db. For three channels (0°, 45° and 60°) it was -46 db between the second and third channels, and -52 db for the second and third signals on the first.

In making the pivotal apparatus to mount the tape head:

- Use extremely flexible audio lead to the tape head or it will break under the constant stress.

This novel way to increase the amount of information recorded on a magnetic tape won the author a prize in a New Jersey science-fair competition for high-school students last year. The editor and several experts in tape recording were so impressed with the originality of the idea that we asked Mr. Maskasky to write an article describing it. The author has since graduated from high school and is now enrolled at the Massachusetts Institute of Technology, the first step, we are sure, to a successful career in electronics.

**NEW...**

This method of recording offers simplicity of operation, saving of money on prerecorded tapes, and no need for ultra-critical factory adjustments. The system does not eliminate the need for separate tracks. Instead, it enables us to put much more information on the width of tape used for each track. Minor improvements in the apparatus and technique can raise the quality of this system to comply with high-fidelity standards. From there, the possibilities are limitless.

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**MAY, 1962**
high-voltage substitution speeds TV servicing

How to avoid losing your shirt on "no raster" calls

By DELLROYE D. DARLING*

Ask the average service technician what's the toughest part of his business and he will say, "Estimating!"

Most customers are pretty insistent about learning the price of a repair job before they give an OK to go ahead. On some complaints a good technician can pretty well guess from the symptoms just about what the job will cost. But what do you do when the only symptom you have is no raster?

You can pull the anode lead and check for high voltage by arcing it to the chassis but, if high voltage is missing, (and it usually is in these cases), you still don't know very much.

Is it the yoke? Maybe. On the other hand, it could be the horizontal output transformer, or no B-plus, or an open screen grid resistor on the horizontal output tube, and so on. All these can kill the raster, but an estimate based on a burned resistor will hardly cover a shorted flyback transformer.

The main difficulty is that even though these troubles cause symptoms of their own which could be used to identify them, they all cut off the high voltage, so the identifying symptoms can't be seen.

Now, signal substitution from a working set to a defective one is nothing new, nor is high-voltage substitution. However, even many technicians who use this technique don't realize how much it can simplify estimating, and so don't use it often enough. Even if estimating isn't the real problem, substitution can save time, and time is money!

Case history

Let's take a typical case. You have a 21-inch Motorola on the bench. It has no raster, and the customer wants an estimate. Ordinarily, we would almost have to repair the set before we could tell all that was wrong with it, but let's do it the easy way.

Take another set — any set that has normal high voltage — and set it up alongside our dog. Plug both sets in and turn them on. Naturally, the outside man has tried tubes, so we shouldn't need to go into that. Pull the anode lead out of the pix tube connector on both sets. Connect a jumper between both chassis. Connect a well insulated jumper between the anode lead on the good set and the anode button on the defective one. (It's a wise idea to turn the "good" set off while making this connection.) Make sure the brightness control is turned well up on the dog. Aha! Now we have a raster. But look at its shape. (Fig 1) It's trapezoidal, or keystoned. Any good technician knows the one thing that can cause keystoning. This set has shorted turns in the deflection yoke. Now we have something on which to base a reasonable estimate.

Take another step

But wait, why not kill two birds with one stone? Every once in a while we make an estimate based on no raster, the customer OK's the job, then when we fix the raster problem we find the set also has video troubles that we couldn't see before. This means persuading the customer to accept an increased estimate so the job can be completed. This seldom improves his opinion of TV service technicians.

As long as we have the high voltage from the good set giving us a raster, why not connect an antenna to the defective set and have a look at the picture? Naturally, if the raster is distorted, the picture will not be completely normal, but we can at least tell if the contrast is correct, all channels present, sync OK, etc.

Other troubles

Let's see what symptoms some other no-raster troubles can cause. Suppose our high-voltage substitution reveals a narrow raster with a very bright drive line down the center (Fig. 2). This is a sign of an overdriven horizontal output tube. If the tube is good, there is one other common fault that can cause these symptoms — an increased value of the screen-grid resistor in the horizontal output tube circuit.

Ordinarily, we know that defective vertical circuits can cause a single horizontal line on the screen. However, if something has shorted in the vertical section (usually supplied from boosted B-plus), it can also cause loss of raster. High-voltage substitution will produce the horizontal line that tells us definitely that the trouble is in the vertical section.

A narrower-than-usual raster with extremely poor horizontal linearity (Fig. 3) can be caused by a shortened linearity coil. This set does not have a linearity control, but a little thought suggested that the trouble might be in a linearity capacitor (B-boost filter). Sure enough, one of them had decreased from 0.1 µf to a negligible value.

Although any technician is familiar with a horizontal white line on the screen caused by loss of vertical sweep, not many have seen a vertical line (Fig. 4), because most faults that can produce this condition also kill the high-voltage supply.

Several things can cause this line, but much can be learned from it. For

*Director, Industrial Electronics Radio Electronic Television Schools, Detroit, Mich.

RADIO-ELECTRONICS
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What's Your EQ? April Solutions

Too-Automatic Tuner

This chassis uses an ultrasonic automatic tuner circuit, operating around 45 kc or so. When horizontal hold was thrown off frequency, either the fundamental or a harmonic, radiated as sonic waves by the flyback or yoke, got into the input of the automatic tuner, which is a microphone at the front of the chassis! Turning the horizontal hold control would cause the auto-tuner to react on one of its functions, depending upon the frequency being generated by the horizontal output at the time!

Black Box No. 4

The black box contains a resistor equal to the internal resistance of one cell, as shown in the figure. When the cells are in series, the current is equal to the total voltage divided by the sum of the resistances of each of the cells plus the resistor in the box. With the cells in parallel, the voltage of one cell is applied to the resistance in the box plus the resistance of one cell divided by the number of cells. Try it with a couple of examples!

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May, 1962

340 PAGES
A VARIABLE-VOLTAGE TRANSFORMER

You can save money by adding a case, fuse, receptacle and meter posts to the basic autotransformer

By L. A. JAMES

Many pieces of equipment found in industrial and commercial electronic laboratories would be valuable in the home electronic workshop. Many of these are too expensive for once-in-a-while use, but this one isn't. One of the most often used pieces of equipment in the professional lab is a variable-voltage transformer. This type of transformer is available under such trade names as Variac, Adjust-A-Volt and Powerstat. Prices run from $8.50 to over $100.

For the average home workshop, the smallest size, 165 volt-amperes, should be adequate. It can be connected so that it will provide an output from 0 to 135 volts. For those of you who aren't familiar with the variable-voltage transformer, perhaps a word of explanation is in order.

Round laminations are used. Along one side, the enamel is removed from the wire and a contact brush rides on this scraped wire. You may remember that a toy-train transformer is made somewhat like this. Since the variable-voltage unit is round, it is hard to handle and set up for use. Several dollars can be saved (and some enjoyable hours had) by making the housing and mounting and wiring the components yourself.

A fuse holder, pilot light, on-off switch, ac receptacle and a pair of binding posts are added to make the transformer more useful. The binding posts are very handy for connecting a meter to monitor the output voltage. The photographs show how the parts are mounted. Be sure to use as least No. 18 hookup wire, on all connections (except the pilot light and voltmeter terminals. You will note that the fuse holder is wired between the transformer and receptacle. A 1-ampere fuse gives the maximum amount of protection to the transformer (rated at slightly over 1 ampere) which is the most valuable component in the circuit.

After wiring, the unit should be tested. If you have an ac voltmeter, use it; if not, a light bulb can be connected to the receptacle. With the transformer set at zero, turn on the power. The pilot light should glow. Slowly advance the control knob and the output voltage will increase and the bulb will glow more brightly. Remember that you can get up to 135 volts from the unit, which may burn out the bulb. As you find more and more uses for this piece of equipment, you will wonder how you ever got along without it.

Output voltage is variable from 0 to 135 volts and may be metered from posts on panel.

Schematic of transformer.

Note comfortable layout. Plenty of space means a cool-running unit.
To paraphrase William Shakespeare, "To build a kit or not to build a kit, that is the question." The old-timers are amazed to see so many thousand kits being built, while hardly anyone builds a piece of electronic equipment from scratch. Time was when most hobbyists designed their own units, fabricated the sheet metal, mounted parts, wired, tested and finally used the item. Now the electronic enthusiast sits down with a catalog of kits and in a few minutes has made his choice and sent in the order. As one of the few survivors who like to build from scratch, I decided to examine the pros and cons of each side—see if I could find out why kits are so popular.

There is no shortage of good construction articles on almost any facet of electronics, in this and the other magazines devoted to electronics. You can find circuits for audio amplifiers (mono or stereo), test equipment, receivers, transmitters, or for just plain experimenting. There are also handbooks for radio amateurs and other interested people. Other circuits can be found in textbooks, catalogs and literature from kit and component manufacturers.

Attractive metal cabinets to house the home-built equipment are far easier to get than when everyone built from scratch. More than a half-dozen companies specialize in metal cabinets and chassis of all sizes, shapes and descriptions. They also come in several materials and colors.

More parts and components are available than ever before. You can obtain them by mail, wherever you live, at attractive prices. All the magazines carry advertisements of new and different components as soon as they become available. Meters are available to measure any value of voltage, current or resistance.

On the other hand, did you ever try to figure up the cost of all the parts in a kit? We did. The price of the parts contained in a kit would cost twice as much as the kit if they were purchased separately. There are also special parts in many kits that would be hard or impossible to purchase.

One outstanding feature of any kit using a meter is its special calibrated scale. Meter calibration is one bugaboo of home construction that is nearly impossible to overcome. Expensive standards are used to calibrate the first engineering models of every kit. Very few home experimenters have access to precision standards such as those needed for meter calibration. The printed or silk-screened meter scale is also out of reach.

One thing that sets a kit apart from home-made equipment is the front panel. Most kits use a silk-screened or etched design on the front of the cabinet. The cost of the artwork and making the screen often exceeds the cost of a complete kit.

Another desirable feature of a kit is the calibrated frequency dial. Just as in the case of the meter scales, expensive signal frequency standards are needed to calibrate the prototype dial scales. The home experimenter does not have these frequency standards.

Many experimenters have boxes of radio parts on hand in the so-called "junkbox". I know one who has been accumulating components for over 14 years. He has salvaged many war surplus parts, he has junked several TV sets and has had many items given to him. This man seldom buys a kit be-

By JAMES A. FRED
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cause he has almost all the parts needed for any project he may decide to work on. He also enjoys the mechanical work that goes into laying out sheet metal and drilling and punching the holes.

Building a kit gives this man very little challenge. He owns only two kit instruments even though he has wired and assembled more than 50 kits for other people. He built his kit oscilloscope according to the instruction manual and it is still in its original form. His other kit, a vtm, has been rebuilt into a panel-mounted instrument. He replaced the slide switch with a toggle switch, added a fuse holder, a pilot light, five-way binding posts and an improved type dc connector. This instrument is now the equal of any industrial type meter made.

There is another angle to remember in the kit business. Many times medium-quality parts are used because the kit must be designed to sell for a certain price. In lower-priced kits there are often no fuses or pilot lights, and the power switches may not be of the best design. If you build your own equipment using war surplus parts you would have a superior piece of equipment, since the government used the finest, most expensive parts available.

You can see there is a lot to be said on both sides of the question. If you are simply interested in having a piece of test equipment or an amplifier and don't get any special kick out of construction, a kit is for you every time. You will have less trouble and better results.

If, on the other hand, you are a designer at heart, get more kick out of building the instrument than in using it, and have had to modify the kits you have built to satisfy your requirements, kits are not for you. You would simply be bored with the work of assembling them, and not fully satisfied with them after they were built.

But if you find yourself somewhere between these two groups, these general rules may help you:

1. If you have no accumulation of parts, by all means buy a kit.
2. If the most important part of the instruments is a calibrated meter or frequency dial, buy a kit.
3. If the new parts you need, in addition to what you already have, cost more than the kit, then buy the kit.
4. If the instrument you want has no dial or meter, then you should build it from scratch.
5. If you have all the necessary parts on hand, then you should build the device from scratch.
6. If you need a piece of equipment that isn't available in kit form then you have no choice, you must plan and build it.

Many experimenters who are new at our hobby will find new joy and satisfaction from building some electronic project up from scratch. They will develop new skills as well as a deep down feeling of fulfillment in a project that they carried through from design to finished product. END

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There are so many things you can do with a 'scope! This absorbing feature uses 30 photos of waveforms to dramatize the large number of tests and techniques. The TV/radio service technician will get as much out of this as the industrial man.

GOLD MAKES BETTER RESISTORS—
"That's gold in them resistors"—literally! The ends of resistors made in the new Western Electric automatic resistor plant are coated with the precious metal before the end caps are put on. Why, how, and the advantages of doing things that way make a fascinating article.

You'll find a mine of other precious reading in the scores of other articles and departments in the JUNE issue of Radio-Electronics.

ON SALE MAY 22

EQUIPMENT REPORT

THIS LITTLE UNIT IS A COMPACT, RUGGED, battery-operated, all-transistor variable signal generator covering 50 cycles to 3.3 mc. Its output voltage is continuously variable from zero to 9 volts, peak-to-peak. This is enough to drive a speaker's voice coil directly, making the unit useful when troubleshooting transistor radios, amplifiers, tape recorders, TV, etc.

The Genie's frequency range is in two overlapping bands (fundamental square-wave pulses). The low band runs from about 47 to 3,300 cycles; the high band from 1,000 cycles to 3.33 mc. Its output consists of very short duration pulses having an excellent flat top and extremely short rise and fall times. Harmonics go well above TV channel 13, thus permitting direct injection into vhf TV tuners.

How it works

When the power switch is turned on (see Fig. 1), the current flows momentarily through R4 from V2's collector. The drop across R4 causes a positive pulse through C2 (or C1 and C2) to be applied to the base of V1. The positive pulse on V1's base creates a greatly amplified collector current, which flows through R1 into the base circuit of V2, causing the collector current of V2 to continue to rise. This ac-
tion is so rapid (millimicroseconds) that V2 is brought into saturation abruptly, causing a flat-top pulse.

Now there is no increase in the voltage drop across R4, V1’s current drops, and an abrupt negative fall in V2 collector current causes V1 to go sharply into nonconduction and thereby cut V2 off. R1 (4,700 ohms) limits the maximum base current of V2 for a maximum collector current of 9 ma, the saturation point of V2.

C1 and C2 are chosen to permit R2 (a special-taper 1-megohm potentiometer) and R3 (about 270 ohms) to tune over the band of frequencies or pulse repetition rate.

A pulse of this type can readily shock-excite an inductance on the output circuit at its own natural resonance frequency, causing a series of damped sinusoidal waves, modulated by the repetition rate of these pulses. (Fundamentals are 50 cycles to 3,333 mc.)

A 600-volt blocking capacitor protects the instrument and the equipment being worked on. Battery life of the portable tester is equal to shelf life or about 1 year.

Four controls are available to the technician using the Genie. An ON-OFF switch (its function is obvious); an OUTPUT ATTENUATOR which varies signal strength from zero to full output; a VARIABLE FREQUENCY control which varies the frequency over the range selected with the HI-LO band switch.

As the unit uses only transistors, there is no warmup period, and no hum is introduced into the circuits being tested as a pure dc (battery) supply powers the unit. Fig. 2 shows the output waveform of the tester as seen on a scope with excellent high-frequency and square-wave response.

Now let’s try some actual servicing procedures which will demonstrate how the Genie is used and what the technician can do with one.

Amplifiers, PA, hi-fi and intercoms

Complaint: Low gain or dead amplifier, B-plus is OK.

Test procedure: 1. Warm up the amplifier and turn on your Genie. Flip the bandswitch to HI and turn the VARIABLE FREQUENCY control completely counterclockwise (approximately 1,000 cycles). Turn the OUTPUT ATTENUATOR fully clockwise and clip an output cable across the woofer speaker’s voice-coil lead points A, B in Fig. 3. If the speaker is good you’ll hear a tone. No tone means an open voice coil.

Now turn the output control all the way down and clip leads to points B. Increase the output. If the output transformer is good, you will hear the tone again. Without changing the output control setting, apply the generator to point C. The tone should be louder. Go back to D. If the tone weakens, suspect the coupling capacitor.

In this way, checking back through H, it is possible to check almost every component in the amplifier as fast as you can clip and unclip the leads. An especially interesting test is at I. Any strong response here indicates a low-capacitance cathode capacitor.

If you can check back to the source (microphone cable, phonograph or tape input, shorts or opens in the cable can be picked up quickly.

Transistor radios

After checking all voltages with a voltmeter, inject a 1,000-cycle signal into the voice-coil terminals, as if checking an amplifier. Then go back through the audio section, remembering to keep the signal down so as not to overload the transistors. Your strongest signal level is needed for voice-coil testing only.

Check the volume control at points A and A1 (Fig. 4). Vary the volume control, noting its action.

Shift the band switch to HI and inject a signal between B and ground. Adjust the VARIABLE FREQUENCY control for loudest signal. Go back through C, D and F, watching for a signal increase as you move from the collector to the base of the transistor. Point E checks the emitter bypass capacitor. If you get a strong signal, the capacitor is open. Inject a signal into G to see if the oscillator transformer is open or shorted or if the tuning capacitors are shorted.

Continue back toward the antenna, clipping the Genie from point H to ground to see if the signal is being passed on to the IF circuits. It may be useful to vary the frequency again for best output. Point I checks overall if gain and also the input of the converter transistor. The rod antenna may be found useful when checking rf stages.

Aligning the rf stages

First adjust the oscillator trimmer to bring in a broadcast station near 1600 kc at the correct point on the dial. Now turn the dial to a clear spot on the high end of the dial (between 1400 and 1600 kc). Loosely couple the Genie output to the antenna coil or lead, selecting a signal of approximately 1000 kc on the high band. Adjust the rf and antenna trimmers, keeping the Genie output low so as not to activate the ave circuits of the receiver.

To adjust the oscillator padder (usually the core of the rf coil), turn the receiver to the low end (600 to 620 kc) and inject a weak signal by radiation from the rod antenna. Adjust the padder for maximum output, again being careful to keep the signal low. Re-check at the high end after the padder adjustment.

Fig. 2—The Genie output waveform.

To check video circuits

Inject a strong signal into the kinescope input circuit (grid or cathode). Select a frequency from 1,000 cycles down. If the input to the picture tube is OK, bars will be seen sharply on the screen. Adjust the Genie frequency till a convenient number appears. Then work back as in an audio amplifier, watching for any sudden falling off of signal or failure to increase in gain when moving from one stage to another.

(B) By varying the frequency of the Genie, you can lock in the vertical or horizontal circuits for a rough sync circuit check.)

Troubleshooting tape recorders

The amplifier of a tape recorder is checked as described for audio amplifiers.
It's an emergency!

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Inside view of Metrox Genie.

fiers. To check the head, make a small induction coil by winding about 50 turns of fine wire (No. 30 or smaller) on a dowel or old alignment tool with a diameter of ¼ inch or less. Leave leads about 12 or 18 inches long, solder them to an RCA type plug and plug into the Genie. Now you can couple a signal into the head by induction, as indicated in Fig. 5. Bring the coil as close to the front of the playback head as possible. If a loud tone is heard, the head is good. No sound or weak sound might indicate a defective coil in the head, broken leads or improper connections.

Other tests

The Genie has a large number of uses. Hooked up to the input of an amplifier, it can, for example, check the speakers for rattle. Simply rotate the frequency control slowly. If the speaker tends to rattle at any point, the rattle will be heard as the Genie is tuned past that frequency.

A rough square-wave test may be made by setting the Genie to produce a square wave on the scope, with scope vertical amplification at its greatest. Now turn the scope amplification down, attach the amplifier output to the vertical terminals, and apply the square wave to the amplifier input. Compare the amplifier output with the original square wave as seen on the scope.

---

Fig. 5—Checking a playback head.

Faulty shielding or internal breaks in cables may be discovered by using them as input cables to an amplifier, then sliding the Genie rod antenna along the outside of the cable with the Genie output at maximum. As the rod is slid toward the amplifier, a sudden increase in signal indicates the point of poor shielding or the break.

Various other uses will occur to the technician. The Genie has been used for a large number of checks and tests, even including (with the help of a scope) if transformer testing. Whenever a signal ranging from low audio to high rf is needed, the Genie will do the job.

END
The Marvelous Automatic Tube Bopper

I go out on this call and the lady starts talking. "This is a real good set. It's got written circuits."

"Written circuits?" I asked.

"Of course," she said, "the ones before printed circuits."

"Oh," I said.

"You don't seem to know much about TV sets," she said. "Do you think you can fix this one?"

"I'll try," I replied.

I checked the set and told the lady, "You have an open cathode."

She seemed highly insulted until I made it clear that I was not referring to her clothing or anatomy.

"Look," I pointed out. "When the picture gets dark, I can hit the neck of the picture tube and it gets bright again. You have an open cathode... in your picture tube," I hastened to add. "I can try to weld it closed but you might need a new picture tube."

This turned out to be stubborn one that wouldn't weld. "You need a new picture tube," I told her.

"I don't want a new picture tube. Just leave the back off and I'll hit the tube every time it gets dark."

"I can't do that," I said. "You go sticking your hand back in there and you'll light up like a pinball machine."

"Well, I can't afford a new picture tube. Can't you fix it without one?"

"No new picture tube?" I asked.

"No new picture tube!"

"Well, I'll see what I can do."

Reaching into my handy tube caddy, I pulled out a photocell, a relay and a solenoid which I just happened to have with me. I mounted the photocell in front of the picture tube and the solenoid on its neck and hooked up the circuit (see diagram). I set the photocell so that when the picture got dark, the photocell activated the relay and the relay closed the circuit that caused the plunger of the solenoid to shoot out and bop the neck of the picture tube, making the picture bright again.

"There you are, lady," I said. "It works without a new picture tube."

"Well, I must say you really know your TV repairing," she purred.

I think I'll apply for a patent.—David W. Cramp

MAY, 1962

IT'S EFFORTLESS STEREO WITH THE
dynatuner

integrator

It takes a little longer to make a good thing better, and the long-awaited Dynatuner FMX-3 is proof that multiplex stereo reception is as simple as mono. Hidden within the Dynatuner chassis, it performs every stereo function automatically without need for switching or adjusting.

The integrator does not detract from the inherently superior performance characteristics of the Dynatuner. The effective sensitivity, noise level, and low distortion are virtually unchanged. The Dynatuner's exclusive reference-grid tuning eye is coupled with Dyna's unique STEREOBEAM (you know when it's stereo because it says so). Exact adjustment, for stereo and mono, can be done at anytime without need for test equipment — thus insuring minimum distortion at all times.

And Dynakit has thought of everything: there are no problems with tape recording off the air; mono broadcasts come through both low impedance outputs at the same level as stereo; front panel volume control adjusts both channels; silent, all-electronic switching; no increase in interstation noise; and best of all, its modest cost.

Slightly higher in the West. Write for detailed information on this and other Dynakits.

DYNACO, INC., 3912 Powelton Avenue, Philadelphia 4, Penna.
CABLE ADDRESS: DYNACO, PHILA.

FMX-3 integrator kit $27.95 FM-1 tuner kit $39.95 Factory Wired multiplex tuner $167.90

www.americanradiohistory.com
The Trans-Key is a transistorized electronic key which will do much to provide perfect code transmission for hams. A light, compact and low-power unit, it is suitable for portable and mobile as well as fixed-station use. The speed and duration of the dots and dashes are selected with a single control. Power requirements are a modest 12 volts at 10 to 20 ma (higher current drain on the higher-speed ranges). Power can be supplied in a variety of ways—dry cells, car battery or low-voltage power supply.

Circuitry
Each transistor is connected as an on-off switch to furnish current to a sensitive relay in the collector circuit. When the key lever is pushed to the left for a dash and released, capacitor C1 is temporarily connected to the collector of R9—2,200 ohms, linear taper.

Trans-Key schematic. Use R9 when dashes can't be made long enough with R1.
Interior of Trans-Key.

when the key lever is pushed to the right, V2 conducts approximately a third as long as V1 due to the lower values of R6 through 8. With the timing resistors shown, the speed ranges are approximately 8, 12 and 15 words per minute.

Construction

The layout and construction of the Trans-Key are not at all critical. My unit is built into a 4 x 4 x 2-inch utility box with attached shelf, and all components fit comfortably. The speed switch (S1) is mounted on the front panel. Two cables run from the back of the cabinet to connect to a modified speed key and the transmitter's keyed circuit. The speed key was modified to provide separate contacts on each side of the key lever, and a separate binding post was added to the key's base for the third connection. If you desire, a home-made key made from a strip of spring steel and a few pieces of hardware will do the job as well.

Most parts are readily available from the surplus-parts box. The relay was obtained from military surplus gear. Almost any sensitive type (1 to 5 ma at 5,000 to 8,000 ohms) can be used, if it has the required contacts—double-pole single-throw with one pair of contacts normally open and the other pair normally closed. I used a dpdt type with one set of contacts for the normally open pair and the other connected normally closed.

R6 and R7 are actually two resistors in series because they were readily available, but they can be replaced by single resistors of 820 and 2,000 (5%) ohms, respectively. R9 is needed only if dashes cannot be made long enough with R1.

If other speeds are desired, increase the number of switch contacts and resistance combinations. The ratio of V1's to V2's timing resistors should be approximately 2½ to 1.

Adjustments

After construction, connect the keying leads to a tone generator or a code-practice oscillator. Rotate S1 to the highest speed range and tap the key to produce dots and dashes. Listen to the duration of each and adjust R1 and R5 to get the proper time ratio. The dash should be approximately three times longer than the dot. Check these settings on the other two ranges and readjust if necessary. This is all that is necessary.

The relay's keying contacts can be used to key an oscillator or buffer stage in the transmitter as long as the contact ratings are not exceeded. The Trans-Key can also be used to key an audio generator in an alarm calling system as interrupted tones demand quicker attention. A compact code oscillator can be built in with the keying circuit in one enclosure.

END

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Industrial Electronics Dictionary

from ultrasonics to X-ray tube
(concluding installment)

By ED BUKSTEIN

Ultrasonics: High-frequency vibrations above the range of human hearing. Ultrasonic generators usually employ a crystal transducer—the crystal transfers its vibrations into the surrounding medium—air, liquid, metal, etc. The magnetostrictive oscillator is sometimes used to generate ultrasonic vibrations. In this type, a metal bar inside an oscillator coil becomes alternately longer and shorter as the magnetic field alternates, transmitting vibrations into the surrounding medium.

Ultrasonic vibrations are used industrially for cleaning and "drilling" metals, for mixing liquids and for detecting internal flaws in metal structures by the echo detection (radar) method.

X-rays: A form of electromagnetic radiation of extremely short wavelength. The X-ray spectrum extends from approximately .06 to 120 Angstroms (an Angstrom is ten-billionth of a meter). X-rays are useful industrially because of their penetrating power, their ability to excite a fluorescent screen and their ability to expose a photographic film. (See Fluoroscopy and Radiography.)

X-ray tube: A tube specifically designed for producing X-rays. Electrons emitted from the tungsten filament of the tube are attracted to the target, a tungsten insert in the copper anode. The target is operated at a high potential with respect to the filament, typically about 100,000 volts. When the high-speed electrons from the filament strike the target, some of their energy is converted to X-radiation. Most of the energy, however, is converted to heat, and some means of cooling the anode must be provided. Water and oil cooling are commonly used in addition to cooling fins mounted on a copper rod extending from the anode. Some tubes use a motor-driven anode so that electrons do not continually strike the same point on the target surface.
The X-ray circuit consists basically of high-voltage supply for anode of X-ray tube, filament supply and associated controls.

As shown in Fig. 29, the associated circuitry consists basically of a high-voltage supply, a filament supply and controls for varying anode voltage and filament current. At higher values of anode voltage, X-rays of shorter wavelength are produced. These are more penetrating and are known as hard-X-rays. Anode voltage is controlled indirectly by varying the input to the primary of the high voltage transformer. A rheostat in the filament circuit permits control of filament temperature and consequently of the quantity of X-rays produced.

Coil-Spring Connectors

These coil-spring connectors replace binding posts in telephone blocks. When a wire is forced between two turns of the coil, the sharp square edges of the wire cut through the insulation and make a good electrical connection. Developed by Bell Telephone Labs, the connectors are expected to cut connecting time in half as compared with connections made to binding posts.

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ALL-TRANSISTOR MOTOR-CONTROL RELAY

By HOWARD T. BAILEY

Using transistor amplifiers to control reversible shaded-pole motors reduces the size and weight of the control unit, and cuts operating costs. Also, a properly designed transistor unit should improve the reliability of the control system. One such unit is described here.

The control-system principle is the same as that of a vacuum-tube amplifier. The direction of rotation is set by the relative phase of the control signal and field current. Speed is controlled by the magnitude of the control signal.

A transistor amplifier for motor control must provide high gain without phase shift and supply enough power to feed the shading coils of the motor being controlled.

The first requirement can be met by suitable circuit design, while the problem of enough power may be overcome by using high-wattage power transistors.

A typical motor-control circuit is shown in the diagram. It uses four p-p transistors and provides a maximum stall torque of .05 lb in for a 0.62-mv input with a Barber-Colman DYAE continuous-duty motor. The input is an ac signal from a bridge circuit that detects physical conditions in terms of voltage differences.

Circuit action

The input signal from the bridge is applied via C1 to V1's base. V1 is a common-emitter amplifier. R1 provides constant emitter-current bias to help stabilize the stage against current changes caused by temperature variations. This resistor is bypassed by C3 for maximum gain. V1's output is fed to V2, another common-emitter amplifier.

R2 provides constant emitter-current bias for temperature stabilization, C4 being a bypass capacitor. A small amount of negative feedback is applied to V1's base from the voltage drop across R3 to improve the operating stability, the gain of the first two stages being high. C2 and C5 also supply some negative feedback to reduce harmonic distortion in the first and second stages, respectively.

The driver stage, V3, is a power transistor operated as an emitter follower. This stage gives no voltage amplification but provides a large current to drive output stage V4. It also provides correct impedance matching to the output stage. The full negative supply is connected to the collector and the base is biased in a reverse direction by returning it to ground. C6 is a blocking capacitor in the feed from V2's collector. The output current from V3's emitter is applied directly to the base of output transistor V4.

The current from V4's collector flows through the shading windings of the reversible motor. A control signal applied to the unit causes an amplified signal voltage to be set up across the shading coils, and the motor then turns in a direction determined by the relative phasing of the signal voltage and the reference voltage in the field winding. The amplitude of the signal voltage decides the speed of the motor in either direction.

Temperature stabilization of V4 is provided by diode D1. This is preferred instead of a resistor in the emitter feed as its stabilizing effect is more constant at various values of emitter current. The larger capacitor, C7, absorbs high-voltage peaks set up across the shading coils at the moment of switching off. Without C7 such peaks could damage the output transistor.

The negative supply for the transistors is obtained by full-wave rectification of a 26.5 center-tapped supply across the secondary of transformer T1. Many devices can be used as the detecting element of the bridge—temperature-sensitive resistances, light-sensitive cells, humidity-sensitive chemicals, etc. In general, any means of varying a resistance can be used as a detection device if it can be incorporated in a bridge circuit.

END
NEW PRODUCTS


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MULTIPLEx ADAPTER model MX-109. 28-db separation, 1.5-volt output, less than 1% third harmonic distortion. Response +1 db, 15 cycles to 15 ke. Tube complement: 1—EC86, 2—12AX7, 1—6X4, 2—1N541 diodes. Dual inputs, left and right stereo outputs. Power consumption 117 volts, 30 watts. Built-in noise filter, front-panel separation control or maximum separation adjusted at factory.—PACO, Div. Precision Apparatus Co., Inc., 70-31 84th St., Glendale 27, N. Y.

FM STEREO TUNER, model TP50. Flat frequency response to 75,000 cycles; sensitivity 0.3 µv, 20-db quieting. Age maintains ± 0.5-db audio-output level; signal-to-noise ratio 10 to 10,000 µv. Built-in tape recording filter. Hum and noise level: —60 db, 100% modulation.—Regont-Prento Div., Siegert Corp., 100 Box 100, Paramus, N. J.

STEREO PREAMP, model C-11. 3-dimensional illuminated front panel. Response ±0.5 db, 20-20,000 cycles, distortion less than 0.1% full rated output. 5 high-level stereo inputs for tuners, tape units, auxiliary signal sources and tape monitors 250,000 ohms sensitivity 0.25 volt. 2 phone inputs 2 mv, 47,000 ohms; tape head 2 mv, 1 meg; mike 2.5 mv. 1 additional mono line for remote amplifier and speaker. Main output 2.5 volts at rated input, tape output 0.25 volt at rated input. 8-position input switch, input mode selectors, separate channel controls, stereo balance control, master volume control.—Mintoh Laboratory, Inc., 5 Chambers St., Binghamton, N. Y.

TRANSISTOR STEREO SYSTEM, Astro AM and FM tuners, FM multiplex, dual preamps, dual amplifiers. 55 watts, response 1 db, 20-20,000 cycles. Harmonic distortion less than 1% at 20 watts. Channel separation 30 db. Headphone receptacle, index-locked balance and tone controls, source selector, instantaneous signal playback. Loudness contour, channel reverse, phase reverse, rumble filter, afe, AM bandwidth adjustment—Altec Lansing Corp., 115 S. Manchester Ave., Los Angeles, Calif.

FM STEREO TUNER, Citation III-X. Built-in multiplexer. Front panel single control for mono, stereo and stereo SCA filter to eliminate stray noise in multiplex broadcasting of background music. SCA filter defeat for stereo. Sensitivity 0.65 µv, 20-db quieting. Selectivity: 240-kc bandwidth; 6 db down. Discriminator.

HI-FI ENCLOSURE, Petrie. Cone-constructed woofer, incorporating voice coil. Woofer matched to tweeter through crossover network with volume control. Input 8 ohms, power rating 6 watts.—Arora Products Co., 301 Main St., Geneva, Ill.


BOOKSHELF SPEAKER SYSTEM, 24 x 10 x 9 inches British speaker. For amplifiers 8 to 50 watts, response 45-15,000 cycles, 8-inch harden twistdifusion cone, 8-inch high comion woofer with almost 1/4-inch cone displacement.—Anglo American Acoustics Ltd., 129 Maryland Ave., Freeport, N. Y.

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4-TRACK TAPE RECORDER, Statesman Stereo 4, model 839. Records and plays back stereo. 2 speeds, 8-10 hours recording time on 7-inch reels. Pushbutton controls, automatic tape lifter, constant-speed hysteresis motor, digital tape counter. 2 full-range dynamic microphiones, 2 four 4 oval dynamic speakers, 2 YU meters. Power requirements 85 watts, 110-117 volts ac only, 60 cycles. Tube complement: 3—12AX7, 2—6SNB, 6AR5, SM15OC (selenium rectifier). Response 50—14,000 cycles, 1.5 ips. Flutter and wow 3% at 7.5 ips. Synchronous-to-noise ratio better than 45 db per channel. Output power 5 watts per channel. Input impedance 500,000 ohms for auxiliary inputs using AM/FM multiplex tuner, stereo record and tape, 59,000 ohms for dynamic microphones. High output impedance for external main amplifier connections. External speaker or headphone connections for hooking up to 4- or 8-ohm speakers. Tape, reels, pitch cords.—International Products Co., 1230 S. La Brea Ave., Los Angeles 19, Calif.

12-INCH TURNTABLE MAT, model PC-22, to protect record grooves, reduce wow and flutter. Replaces worn mats, fits over existing one. 8 ridges provide support for 7-, 10- and 12-in. records.—Redial Industries Corp., 36-27 Prince St., Flushing 56, N. Y.

Automatic Record Changer, model UA16. Dynamically balanced motor, self-lubricating, lifetime bearings, mounted with full rubber suspension. One-piece aluminum die-cast heavy-gauge steel construction. Pressure roller drops away from capstan when not in operation to protect roller. Speed accuracy with 4-pole induction motor, ± 3%, ± 2% or better. Multi-speed drive system for 3 speeds, 4-pole shaded-pole induction motor dynamically and statically balanced, shock-mounted, less than 40°C heat rise in continuous operation. Wow and flutter 25% or better, maximum average 2% cycles.—Cook Electronics Corp., 1006 Lyons St., Evans- ton, Ill.

Automatic Tape Recorder, Phono Trix Executive 88-B. Battery-operated. Immediate playback through mike while connected to power line. Wow 0.2%, flutter 0.06%, rumble ± 50 db, 4 speeds, plays all record sizes of same speed interchange. Concentrically weighted turntable—BBR (USA) Ltd., 115-10 14th Rd., College Point 56, N. Y.

MINIATURE TAPE RECORDER, Phono Trix Executive 88-B. Battery-operated. Immediate playback through mike while connected to power line. Wow 0.2%, flutter 0.06%, rumble ± 50 db, 4 speeds, plays all record sizes of same speed interchange. Concentrically weighted turntable—BBR (USA) Ltd., 115-10 14th Rd., College Point 56, N. Y.
input jack. Used with manufacturer's desk amplifier, SB-8, becomes PA system, records and amplifies simultaneously. Pushbutton-operated, top controls.—Matthew Stuart & Co., Inc., 156 5th Ave., New York 10, N. Y.

PORTABLE TAPE RECORDER, model TK-40. 4-track monaural pushbutton unit records and plays back 3 speeds. Equipped for dual sound effects. Built-in permanent dynamic speaker. Input jacks for microphone, radio, phonograph, telephone adapters. Output jacks available for external loudspeaker, remote control, earphones, playback through radio, 8-mm film projectors or connection to second tape recorder. Built-in splicing rule, tape counter, magic-hand recording level indicator, flywheel drive and tone and monitor controls.—Majestic International Sales, Inc., 743 N. La Salle St., Chicago, III.

MONOURAL TAPE RECORDER, model SPC-4N. Automatic 3-speed control, tone control operates on record and playback. Neon recording level indicator; pause and edit control; separate jacks for mike, external speaker and radio-phones. Safety interlock. Precision braking; wow and flutter less than 0.25%. Push card, professional desk stand mike, two 4-in reels, 600 feet of tape. Accommodates up to 7-in reels.—The Sampson Co., Electronics Div., 2244 S. Western Ave., Chicago 8, Ill.

ALL-PURPOSE MICROPHONE, model DDS. Response 70-15,000 cycles. Two sound entrances at back of diaphragm provide unidirectional polar characteristics for this dynamic mike. Correct positioning of unit controls program feedback, etc., in PA systems. Moving a wire alters impedance from 50 to 400 ohms, 11-con. unit equipped with 18-foot, two-conductor shielded cable. Available in phased, matched pairs.—American Egypt Ltd., N. Y. Co. (Div. G. C. Electronics, 400 S. Wyman St., Rockford, 111.

TRANSISTORIZED POWER CONVERTER, Continental 30-122: Changes 12-volt battery current to 110-volt 60-cycle ac. Capacity 275 watts continuous, 300 watts intermittent. For operating tape recorders, TV sets, sound cameras, amplifiers, test equipment, hand-power tools and

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6 oz. Spray can. Also available 2 oz., 8 oz., 32 oz. containers
FREE 6" Plastic Extender With Every Can

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VOLUME CONTROL AND CONTACT RESTORER

EVER-QUIET is a free-flowing liquid that leaves no powder residue. Scientifically designed to strip around the shaft and penetrate the control or potentiometer, cleaning the contacts and leaving a safe protecting film. Harmless to metals, wire or carbon.

2 oz. Bottle & dispenser. Also available—6 oz. Spray can

CHEMICAL ELECTRONIC ENGINEERING, INC., Matawan, New Jersey

INDEXED STORAGE CHEST, for film and recording tape. Holds 124 styrene containers, accommodates 5- and 7-in recording tape plus 8-mm home movie film. Swivel-twist lock—Saxton Products, Inc., 4320 Park Ave., Bronx 57, N. Y.

SWITCH KNOBS, contoured top and bottom, tapered sides, for Lever and Televe

REPLACEMENT KNOB HEADS, 6 types to fit stems currently in stock. Also 21 new stems, assorted lengths, to fit various shafts—Colman Electronic Products, 3101 N. E. 3rd Ave., Amarillo, Tex.

OUTLET BOX, Safcord, model W-5. For quick installation of multiple electric outlets, 6 heavy-duty standard receptacles, on-off switch, pilot light. 10 feet heavy-duty appliance cord. Both sides of line fused. 125-volt unit rated at 10 amps, 1,250 watts.—R. Marzinski, Dept. RE-1, 61 Trudy Lane, Buffalo 25, N.Y.

CHEMICAL SPRAYS. 6 oz. aerosol spray cans contain Super Freeze Mist for pinpointing bad components through quick cooling. Sprays lubricates and eliminates noise caused by dust and corrosion on switches, relays, and sliding contact devices. Super Contact Cleaner, heavy-duty spray with silicone compound, protects all controls.—GC Electronics, Div. Textron, 400 S. Wyman St., Beckford, III.

Changes in communications are born at . . .

5th and Kostner Aves., Chicago 24, Illinois

www.americanradiohistory.com


MIDGET-SIZE SCREWDRIVER, cat. no. 18S. Beryllium-copper, nonmagnetic, nonsparking. For electrical and electronic assembly and service. 1/2 x 2-1/2-inch beryllium-copper round blade in plastic handle fitted with pocket clip.

18-inch leads, insulated alligator clip, thin test probe, 16-volt, 6-volt battery, 2 transistors, on/off switch on control potentiometer.—GC Electronics, Inc., Div. Tektronix Electronics, Inc., 400 S. Wyman St., Rockford, III.

PORTABLE GRID-DIP METER. Fully transistorized, 14-oz. 1-hand operation. Measures transistors, diodes, and waveforms of any real or imaginary circuit, in the field or in the laboratory. Measures any frequency or waveform—sinusoidal, square, square-wave, or any frequency ratio.—Multiplex Instruments, Inc., 10514-8, Minneapolis 6, Minn.

Overall length 4 1/2 inches.—Xedite, Inc., Orchard Park, N. Y.

MUTUAL-CONDUCTANCE TUBE TASTER KIT, model FT-1A. Built-in adapter for testing compartment, nuvisor, Novar, and 16-pin miniatures. Checks Gm and grid current in multi-element tubes; diodes, rectifiers, voltage regulators, low-power theratrons, electron eye resonant frequencies, checks antenna resonance; locates parasitic frequencies as rf detector, absorption wavemeter and sig gen. Fiberglass-coated plug-in coil, banana plugs. 3 coils (0.1-1000), phone jack, battery. Kit or assembled.—PEL Electronics, PO Box 555, Ridgewood, N. J.

3 BETA TRANSISTOR TESTER, model $2000. Tests silicon or germanium transistors, diodes, Zener diodes, accuracy ±0.05%. Measures ac and dc beta, leakage, other transistor characteristics.

Built-in roll chart lists data for beta and leakage tests on more than 1,800 transistors. Leakage ranges cover 0-0.05 µm full scale to 0-25 ma full scale. Chopper and high-sens amplifier for leakage current measurement on low-current scales. Instruction manual gives manufacturer’s data for ltc0, ltc1, input resistance, output conductance, mutual conductance and collector saturation voltage. Continuously variable VCM and L, provide tests based on user’s special requirements.—ID Instruments, Div. Hickok Electrical Instrument Co., 10514 Dupont Ave., Cleveland 8, Ohio.

If you can’t afford a Fisher tuner... build one!

Introducing the newest Fisher StrataKit: the KM-60 FM-Stereo-Multiplex Wide-Band Tuner. Fisher FM tuners have always been reasonably priced considering their unsurpassed sensitivity and matchless overall design—but, even so, not everyone can afford them. If economics have thus far deterred you from buying the very finest, the new Fisher KM-60 StrataKit solves all your problems in exchange for a few evenings of entertaining and instructive work. It incorporates Fisher FM engineering at its most advanced, including built-in Multiplex and sophisticated wide-band circuitry—yet it costs almost one-third less than the nearest equivalent Fisher-built tuner.

This spectacular saving involves absolutely no risk, even if you are ‘all thumbs.’ The StrataKit method of kit construction has eliminated the difference between the expert technician and a totally unskilled person as far as the end result is concerned. You assemble your StrataKit by easy, error-proof stages (strata), each stage corresponding to a particular page in the Instruction Manual and to a separate transparent packet of parts. Major components come already mounted on the chassis, and wires are pre-cut for every stage—which means every page!

In the KM-60 StrataKit, the front-end and Multiplex circuits come pre-aligned. The other circuits are aligned by you after assembly. That is accomplished by means of the tuner’s laboratory-type d’Arsonval signal-strength meter, which can be switched into each circuit without soldering.

This is the world’s most sensitive FM tuner kit, requiring only 0.6 microvolts for 20 db quieting! (IHFM-standard sensitivity is 1.8 microvolts.) Capture ratio is an unprecedented 2.5 db; signal-to-noise ratio 70 db. The famous Fisher “Goldie” Cascade 8F stage, plus four IF stages and two limiters, must take most of the credit for this spectacular performance and for the superb rejection of all spurious signals. Distortion in the audio circuits is virtually non-measurable.

An outstanding feature of the Multiplex section is the exclusive Stereo Beam, the Fisher invention that shows at a glance whether or not an FM station is broadcasting in stereo. It is in operation at all times and is completely independent of the tuning meter. Stereo reception can be improved under unfavorable conditions by means of the special, switchable sub-carrier noise filter, which does not affect the audible frequency range.

Everything considered, the KM-60 is very close to the finest FM tuner that money can buy and by far the finest you can build. Price $169.50.*

The Fisher KX-200 80-watt stereo control amplifier StrataKit, $169.50.*

*Walnut or Mahogany cabinet, $24.95. Metal cabinet $15.95. Prices slightly higher in the Far West.

USE THIS COUPON FOR FURTHER INFORMATION
Fisher Radio Corporation 21-51 44th Drive, Long Island City 1, N. Y.
Please send me without charge the complete Fisher StrataKit catalogue.

Name

City Zone State

RES13

MAY, 1962

87
The Harmon P-315A Regulated Power Supply

Gives you... all these features at this low price*

... and it is lightweight and compact enough to make it ideal for field work, despite the fact that it is in the category of the finest laboratory equipment by performance standards.

Whether you are working with transistorized circuits, hybrid tubes, or are involved in any test, maintenance or design work requiring 0 to 15 volts of d.c. at up to 3 amps, you will be delighted with this new Harmon Power Supply. The full wave filtered output will supply "lab-type" power at continuous current loads and the .1% regulation at inputs varying from 105 to 125 volts A.C. (55 to 65 cycles) insures 100 microsecond recovery time during voltage surges. This compact package weighs but 5¼ pounds and measures 8½" x 6½" x 5½".

Specifications

- Input 115 volts a.c., 55-65 cps.
- Voltage Regulation ±1% at 115 volts. Input voltage may vary from 105 to 125 volts.
- Output 0-15 volts d.c., fully regulated, at up to 3 amperes.
- Circuity Solid state. 4 power transistors, heat-sink mounted.
- Ripple 10 mv. RMS at 50% load current; 30 mv. RMS at full load.
- Fusing All components short-circuit protected.
- Recovery Time Less than 100 microseconds after full load surge.
- Voltage Control Precision Potentiometer

*Introductory Price 99.50

Available through your electronic distributor. Write for technical brochure and name of nearest distributor.

George Harmon Company Inc.

IGNITION ANALYZER, model TD-10. Locator trouble in coils, spark plugs, points, capacitors. Direct-reading meter. Vtvm section measures to 30,000 volts without circuit drain.

Capacitance clip for shock-proof high-voltage measurements, including surges. Power derived from 12-volt car battery: may be used on all 4-, 6- and 8-cylinder engines. Variable resistance-loading circuit simulates heavy engine load.

TRANSMITTER DUMMY LOAD. Contained. Handles power to 1 kw, less than 1.5 vswr to 300 me. Impedance 60 ohms. Coax input connector for transmitter, phone jack for de output to vvm or vtvn. Oil-cooled temperature-stable resistive element. Oil capacity = gal. = Heath Co., Benton Harbor, Mich.

TRANSISTORIZED FISH ATTRACTION. Sonar-eye, model 1000. Sonic-impulse device attracts predatory game fish from as far as 2 miles away to vicinity of user. Use in fresh or salt water. - H. McCune Co., 16255 Ventura Blvd., Encino, Calif.

All specifications are from manufacturer's data

NEW BUSINESS GETTERS

REPLACEMENT NEEDLE WALL CHART

Listing replacement needles by cartridge number, illustration of needle replacement, record speed, and needle number in either diamond, jewel or conical. - Duotone Co., Newport, N.J.


CARTRIDGE/NEEDLE SALES AIDS include wall charts, cartridge dispensers, storage bins, counter displays, mobile, banners and picture attachments for hardware merchandisers. - Electro-Voice, Inc., Buchanan, Mich.

SERVICE SELECTOR. 40-page catalog describes capacitors, vibrators, rotors, decades, test instruments, other components. Includes illustrations, design features, temperature ranges, material construction, application and price. - Cornell-Dubilier Electronic Div., Advertising Dept., Federal Pacific Electric Co., 50 Paris St., Newark, N. J.

TEST ACCESSORIES—patch-cords, cable assemblies, socket savers, test-socket adapters, molded test plugs—shown in 12-page Catalog 7-62 is illustrated with many photos, offers complete technical data. - Pomona Electronics Co., Inc., 1500 E. 9th St., Pomona, Calif.


AMATEUR BAND RECEIVER NC-155 described in data sheet, with technical information and photos. - National Radio Co., Dept. RP, Melrose 76, Mass.

TRANSISTORIZED VOLTAGE REGULATORS, 1GE-581. Application Guide. Describes design procedures and solution to sample design problems for series, shunt and combination series-shunt regulators. - Semiconductors & Materials Division, RCA, Somerville, N. J. 25¢


METAL FASTENERS outlined in Catalog FL-NL. Lists complete line of staples, Lock Nails and wire for use with any type of manufacturer's industrial tachometers, statics, etc. Detailed selection data and specifications are included in the catalog- - Holler Roberts Instrument Corp., 5115 Carnegie Ave., Cleveland 3, Ohio.

LEVER TYPE SWITCHES described in 4-page Catalog No. S-57. Engineering drawings, specs and operating features, plus colored illustrations. - Switchcraft, Inc., 5555 N. Elston Ave., Chicago 30, Ill.

CLIPS AND INSULATORS offered in 8-page Catalog No. S-56, with description and illustration of approximately 70 items. Also included are display material and other sales aids. - Mueller Electric Co., 1583 E. 21st St., Cleveland 14, Ohio.

Any or all of these catalogs, bulletins, or periodicals are available to you on request direct to the manufacturer, whose addresses are listed at the end of each item. Use your letterhead—do not use postcards. To facilitate identification, mention the issue and page of RADIO-ELECTRONICS on which the item appears.

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By G. Warren Heath • One of the most valuable servicing books ever written! Lists hundreds of tough TV problems, alphabetically for easy reference. Tells you how to find 'em and fix 'em in minutes. No theory—just practical hints, plus many time-saving troubleshooting charts.

**THE VTVM** — Reg. Price $4.60

By Rhys Samuel • How to get the most out of this electronic workhorse! Suggests many new time-saving uses. Tells how and why the VTVM works, describes meter scales, probes and cables and explains the use of the VTVM in TV troubleshooting, AM-FM alignment and repair, servicing audio amplifiers, etc.

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MAY, 1962
Here's the solution for replacing speakers in transistor radios. With this complete line of midget speakers (American made with American parts) Utah provides a dependable source for replacements. Wafer-thin baskets, 12 ohm V.C. impedance—for performance equal or better than original speakers.

### SPEAKER ENCLOSURE

**Patent No. 2,969,848**

Claude C. Fairrell, 6 School St., Groton, Mass.

Close coupling between speakers is known to increase fidelity and efficiency. Here is an enclosure designed to couple two 12-inch speakers fed in the same phase.

The space between speakers opens into a "throat" and into a "horn space" which transmits the sound into the room. The chambers are lined with sound-absorbing material, and their joints are reinforced with blocks. The cabinet is made of 1/16-inch plywood.

### NO-WIND CLOCK

**Patent No. 2,957,116**


This clock is regulated by a spring and balance wheel. A transistor circuit feeds a pulse of energy to the wheel at regular intervals to compensate for friction loss.

The transistor circuit (Fig. 1) is energized by de. Its base is reverse-biased by about 0.3 volt to keep it nonoscillatory. Resistor R damps out any oscillations that may tend to arise.

Magnet M is mounted at the rim of a balance wheel. L1, L2 are wound over a magnetic core and poled for regenerative action. With the core not energized, M is attracted to it. As M passes the core, it generates a negative pulse which is fed to the base of V. The pulse is regenerated until full collector current flows through L2. It energizes the core with polarity that repels M. The collector pulse quickly decays.

After the wheel has completed its swing, the spring reverses its motion and again the core attracts M. An instant after M passes the core, it is again repelled by it. Thus the balance wheel oscillates as long as de is applied to the transistor.

Fig. 2 shows mechanical details of the clock as suggested by the inventor. Also, he describes an unbalanced bridge using temperature-sensitive resistors (not shown) for maintaining a constant de input to the transistor.
**TRI-CITY ELECTION**

*Camden, N. J.*—Members of the Tri-State Council of TV Service Associations elected the following officers:
- Tony deFranco, president; Wm. Jordan, vice president; Arnold Zenker, secretary, and Joseph Eberhardt, re-elected treasurer. Carl Welk was appointed publicity director. The Tri-State Council is made up of members of the Allied Electronic Technicians Association of New Jersey, Television Service Dealers Association of Delaware; Television Service Dealers Association of Delaware County, (Pennsylvania) and the Radio Service men’s Association of Trenton, N. J.

**ACTE S ELECTS**

*Ashtabula, Ohio.*—Election and installation of officers was the business at hand at a recent meeting of the Ashtabula County Television Service men’s Association. The new officers are:
- Edward Campagne, president; Nick Notter, vice president; Jack Stranahan, secretary; Frank Abbott, Treasurer; Joe Horvath, director of NATESA and TESA; Ed Laatu, Carl DeMarco, and Joe Turk, junior vice presidents, and John Campagne, historian and sergeant at arms.

The group’s goal for 1963 is to make the ACTSA technician the best technician available.

**NEW TECHNICIANS GROUP**

*Columbia City, Ind.*—Technicians from Churubusco, South Whitley and here met at City Hall to organize a new service association. One of the first steps taken by the group was to elect officers. They are: David F. Martin, president; Joe Weaver, vice president; I. C. Ohlwein, secretary, and Marshall Sevits, treasurer.

**MULTIPLEX MEETING**

*Detroit, Mich.*—Radio Distributing was packed with 65 TSA members and their technicians for a service meeting on FM multiplex stereo. A smorgasbord dinner was served at 7 pm and the service meeting got underway at 8 and lasted till 10:30.

Zenith field engineer Ed Kob was speaker and proved to be a capable talker and instructor. As a part of his presentation he pointed out that the circuit and tubes had been used before, but in other applications. He also stressed that, while ghosts on TV might be lived with, they were intolerable in FM stereo because they show up as distortion. It was a very profitable evening for those attending.

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Van Ness at Post, RE
San Francisco, Calif.

CSEA BANQUET
Los Angeles, Calif.—The 1962 Annual Banquet of the California State Electronics Association was the setting for a talk on "The Importance of the Independent Service Technician—Today and Tomorrow." The speaker was R. H. Bowden, president of Sencore Inc. His talk revealed his conviction that the future can be bright if the technician will keep abreast of the newest developments in testing methods and concentrate on sound business principles and improved public and customer relations.

INDIANA CIRCUIT
Kokomo—First business was to distribute copies of the association's constitution and bylaws. Next came elections. Ernest H. Golieb is the new president; Joe Martin, vice president; Robert F. Cripe, secretary, and Harold Crume, treasurer.

Ernie Golieb and Joe Martin tied on two successive ballots for president. It was moved and carried that the winner be decided by the toss of a coin, with the runner-up being vice president. Golieb won by a head.

Evansville—RTSA held its 17th Annual Combination Ladies Night and Installation Banquet. Official installation ceremonies were preceded by a family-style banquet dinner. Games and other entertainment followed.

J. Paul Wurtz turned over the president's chair to Charles F. Wilhelm. Gerald Joe Julian is the new vice president; Jerold R. Sweeny, secretary, and Don Wurtz, treasurer.

Logansport—And more election returns—president, Bill Boller; vice president, Frank Pickens; secretary, John E. Hill, and treasurer, Glenn Ogle.

Elkhart—Here too election news is the important item for the month: President, Wayne L. Clem; vice president, Arden Gaerte; secretary, Dean R. Moeh, and treasurer, Hubert McAllister.

NO TV SERVICE ON SUNDAY
Kansas City, Mo.—It's against the law to do any TV servicing on Sundays, and TESA is backing it unanimously. Under the state's Sunday Sales Law (TV service is included), TV service shops are required to close, along with most other retail businesses.

PRICE LIST
Wisconsin—The following price list appeared in the February 1962 issue of TESA-Wisconsin News. The prices shown apply to that particular service area and may differ from state to state and even from city to city.

These suggested fees cover diagnosis of trouble, location, installation or repair of component or circuit including mechanical defects. Parts are additional. They are based upon a survey of operational expense of leading service companies, tax studies and cost analysis of time required to accomplish the listed service operation on a wide variety of television receivers with operations performed by competent technicians.

Basic Service Fee—Tube Check—Cleaning chassis—Remove and replace—Setup $4.00
1. Ac input circuit ... 7.25
2. Audio circuit... 15.45
3. Afc system... 18.90
4. Agc system... 19.10
5. Control: Single unit... 6.75
       Dual unit... 9.75
6. Damper circuit... 11.60
7. Deflection yokes and circuit... 9.35
8. Filament circuit... 11.85
9. Focus circuit... 11.80
10. Horizontal oscillator circuit... 17.85
11. Horizontal output circuit... 14.55

90-DAy PARTS GUARANTEE
12. 1st amplifier circuit... 13.75
13. Picture tube; replacement... 19.50
14. Power supply circuit (Hi voltages)... 14.20
15. Power supply circuit (Low voltages)... 12.45
16. Power transformer... 10.45
17. Speaker... 4.75
18. Selenium rectifiers... 12.25
19. Sync circuit (vert or hori):... 17.40
20. Tuner (turtle type)... 12.50
21. Tuner (wafer type)... 15.90
22. Tuner cleaning and lubrication (turtle type)... 4.25
23. Tuner cleaning and lubrication (wafer type)... 6.25
24. Tuner replacement or removal:... 12.50
25. Vertical oscillator circuit... 14.20
26. Vertical output circuit... 12.20
27. Video circuit... 12.55
28. Retrace blanking circuit... 8.10
29. Printed circuits (concealed type)... 2.00
      Add $8.50 to above price
30. Clean picture tube (removal)... 3.85

Alignment of Tuned Circuits
31. Video (complete)... 12.50
32. Sound (complete)... 9.75
33. Afc Circuit... 7.75
34. Sound discriminator circuits... 4.25
35. Tuner: local oscillators only... 2.00
36. Uhf tuners... Hourly Rate
                                 "Local-zone" average service fee: 7.00
Additional TV shop fee—per hour or portion thereof... 8.50
Analysis and location of trouble when estimate is given and set is not repaired... 10.00
IWP (In warranty parts exchange fee)... 50c per part—Minimum fee... 1.20
Storage after 30 days: per month or portion thereof... 2.00

AUTOMATIC TRANSLATION FOR THE SERVICE INDUSTRY
"It's probably just a condenser."—Freely translated means—'I've just
spent $14.00 on tubes and now the thing won't work at all.
"How much do you charge to replace a fuse?"—I was looking for
a loose connection when something started smoking.
"I just had the set overhauled."—A friend put in some tubes last month.
"He didn't get it adjusted just right."—The antenna blew down last night.
"Can you just drop it off? I only
live around the corner."—We live in
a fourth-floor walkup. —TSA Service News

CORRECTIONS
On page 51 of the March issue, the Amperex tube using Cavitrap construction
was erroneously designated as the 6J6G in the caption. The tube, as the photo indicates, is a 6G6. We
thank Mr. George C. Loud, of Eastport, Me., for calling this to our attention.
There is an error in the heater circuit of the multiplex adapter on
page 31 of the December 1961 issue. The heater pins of the 12AU7's are
numbered 3, 4 and 9. The correct pin connections for the heaters are 4, 5
and 9.
We thank Mr. Robert Volino of Brooklyn, N. Y., for this correction.

509-DAy PARTS GUARANTEE
12. 1st amplifier circuit... 13.75
13. Picture tube; replacement... 19.50
14. Power supply circuit (Hi voltages)... 14.20
15. Power supply circuit (Low voltages)... 12.45
16. Power transformer... 10.45
17. Speaker... 4.75
18. Selenium rectifiers... 12.25
19. Sync circuit (vert or hori):... 17.40
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New Tubes and Semiconductors

New items are not as numerous this month, but interesting just the same. There are a couple of sharp-cutoff pentodes for FM limiter and i.f. amplifiers; a solid-state negative resistance element; a Novar type TV damper; a subminiature voltage regulator; a group of "universal" picture tube replacements, and a triode nunnistor.

6H56, 19H56

Two 7-pin miniature sharp-cutoff pentodes for use in i.f. amplifier and limiter stages of FM receivers. They have extremely high transconductance (0.500 mhos) and extremely low capacitance between grid 1 and the plate (.006 μf). Both also feature a "dark heater" which functions efficiently at operating temperatures 350°K below those of conventional heaters. Except for their heater ratings the two tubes are identical.

<table>
<thead>
<tr>
<th>Characteristic</th>
<th>6H56</th>
<th>19H56</th>
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</thead>
<tbody>
<tr>
<td>$V_{ce}$</td>
<td>6.3</td>
<td>18.9</td>
</tr>
<tr>
<td>$L_{sub}$</td>
<td>450</td>
<td>150</td>
</tr>
<tr>
<td>$V_{s}$ (supply)</td>
<td>300</td>
<td></td>
</tr>
<tr>
<td>$V_{in}$ (supply)</td>
<td>300</td>
<td></td>
</tr>
<tr>
<td>$V_{p}$ (pos bias value)</td>
<td>0</td>
<td></td>
</tr>
<tr>
<td>$P_{m}$ (neg bias value)</td>
<td>50</td>
<td></td>
</tr>
<tr>
<td>$P_{o}$ (watts)</td>
<td>3</td>
<td></td>
</tr>
<tr>
<td>$P_{o}$ (input watts)</td>
<td>(for $V_{po}$ to 150)</td>
<td>1</td>
</tr>
</tbody>
</table>

Solid-state negistor

This semiconductor device is capable of operating as a negative-resistance element. It can be used as a switch, bilateral amplifier, or loss corrector in wave filters. It can also be used in mul-
tivibrators, switching circuits and linear amplifiers to reduce cost and complexity and improve overall operation.

A 2-terminal device, the Circuit-Dyne built Negistor is available in resistance values from 10,000 to 100,000 ohms in 5% increments. Resistance tolerances—2%, 5% or 10%—may be specified. The units are epoxy encapsulated and have either coaxial or single-ended leads.

6DW4

This Novar tube is a half-wave vacuum rectifier designed for damper service in horizontal-deflection circuits of color and black-and-white TV sets.

Maximum ratings of the RCA 6DW4 in TV damper service are:

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>PIV</td>
<td>4,500</td>
</tr>
<tr>
<td>IR (peak ma)</td>
<td>1,300</td>
</tr>
<tr>
<td>IL (dc ma)</td>
<td>210</td>
</tr>
<tr>
<td>P (watts)</td>
<td>6.5</td>
</tr>
<tr>
<td>V(ohm neg with respect to cath)</td>
<td>4,500</td>
</tr>
<tr>
<td>V(ohm pos with respect to cath)</td>
<td>300</td>
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</tbody>
</table>

8228/ZZ 1000

Subminiature voltage reference tube designed to be the most stable device now available. It has a temperature coefficient of 3 mv/C (.004%/C) over a temperature range of -55 to 70°C. Its nominal reference voltage is 82 at an average current of 2 ma. The tube's variation in regulating voltage is less than 100 mv, due to its semi-hollow cathode and it is guaranteed for 30,000 hours of use. The Amperex 8228/ZZ 1000 is 1.2 inches long and ½ inch in diameter. It has leads which can be soldered into the circuit.

"Universal" Picture Tubes

RCA has announced 4 "universal" type picture tubes that will replace 33 existing types. The 4 tubes are said to take care of one out of two picture tube replacements handled by the service technician today.

The 21ALP4-A replaces:
21ALP4 21ALP4-A 21ALP4-B
21ANP4 21ANP4-A 21ATP4
21ATP4-A 21ATP4-B 21BAP4
21BNP4 21BTP4 21CBP4
21CBP4-A 21CBP4-B 21CMP4
21CVP4 21CWP4 21DNP4
21FLP4

The 21AMP4-A replaces:
21ACP4 21ACP4-A 21AMP4
21AMP4-A 21AQP4 21AQP4-A
21BSP4 21CUP4

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SHIFTING CONVERGENCE

When a color TV receiver is first turned on, the alignment of the gun structure of the picture tube may change slightly because of heating. The normal effect of this heating will vary the static convergence of the receiver, unless some allowance is made for the warmup period. Therefore, it is wise to let the set warm up for about 15 minutes before you converge it. In this way, when the customer turns his set on, instead of it drifting out of convergence, it will drift into convergence.—RCA Television Service Tips.

REGENCY TR-1

The set came in with severe audio distortion. We connected a high-impedance headset across the volume control. Sound was satisfactory here. Then we clipped the headset across the base of the audio output transistor to battery positive. Some slight distortion was noted here.

Components in the audio output stage were resistance-checked next. No off-value units were spotted. Voltage tests followed and revealed nearly zero voltage on the emitter.

When capacitor C21 (40 \(\mu\)F at 3 volts) was clipped, voltage on the emitter increased. We replaced the unit with a 6-volt capacitor and had no further trouble.—Chester S. Lawrence

HEATH CB TRANSCEIVER

Noting a decided drop in receiver gain when switching from crystal to variable tuning in a Heath GW-10 on the bench, I mistakenly thought the 6C4 oscillator tube was weak. Further troubleshooting turned up an interesting kink. There are two positions of the slug in the oscillator coil which allow tracking of the 22 channels. However, with the adjustment in the lowest position (closest to the chassis),

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the injection signal from the variable oscillator is much stronger than when it is set closer to the top. This results in a 50% or better gain in reception, raising the level of the variable receiver to that of the lock-in. Subsequently I have run across a relatively large number of GW-10's with this same complaint. Screwing this slug into the lower position cured every one.

Another suggestion while on the subject of alignment. An ordinary signal generator will not give a precise enough alignment of the 455-ke if strip. It is best to use the signal from an accurately calibrated source, such as the Lampkin frequency meter. Using an attenuated signal from another CB transmitter is an alternate but less reliable method.—Charles B. Roundall

RCA 21ID305

The complaint was intermittent black horizontal bars. The sync would lose control or the picture would pull whenever the bars appeared. The trouble was located by a long process of shunting suspected capacitors with known good units. This showed that age capacitor C155 (.022 mf) was intermittent. A quick replacement was the cure.—Chester S. Lawrence

POWER SUPPLIES FOR TRANSISTOR DEVICES

Commercial power supplies often use a resistance to drop the voltage for the lower output ranges. The low-voltage taps may not be bypassed enough to allow the ac signal to return to chassis. When this kind of supply is used to power a transistor set, audio distortion may arise which is not caused by a circuit fault.

When operating from a low-voltage tap on such a test supply, shunt the output to the radio with a capacitor. Use a 25-pF unit rated at a greater voltage than delivered by the power unit.—Joe Shane

AUTOMATIC SEARCH TUNER STALLING

Automatic signal-searching tuners in car radios sometimes stop for no apparent reason when they reach the low end of the band. The actuator bar has to be pushed again to restart it.

When this happens, try the search with the antenna pushed down. If it does not stop now, the search mechanism is OK. Do not alter the sensitivity of the search unit. The problem is caused by the if acting as a station signal at high settings of the sensitivity control in strong station areas. A touch up of the i.f. will usually fix things up; the i.f. may be tuned a trifle too broad.—Mark Sturgeon

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"Despite the popularity of bookshelf-size speaker systems, the big speaker system is far from extinct. There is still a great deal to be said for the sound quality of a really good large speaker system, one of which is University's new Classic Mark II.

In operation, the Classic Mark II handles low frequencies up to 150 cps through a 15-inch high-compliance woofer that is installed in a ducted-port cabinet. The bulk of musical program content, however, is handled by an 8-inch mid-range speaker, which covers from 150 to 3,000 cps. Above 3,000 cps, a Sphericord super tweeter takes over.

The measured indoor frequency response of the Classic Mark II was remarkably uniform. As a rule, such response curves are so far from flat that I do not attempt to correct them for the slant irregularities of the microphone's response. However, the measurements for the Classic Mark II allowed me to plot the microphone response also. This further emphasizes the uniformity of the system's frequency response. A 3-db increase in the setting of the control would probably have brought the range above 3,000 cps into nearly exact conformity with the microphone-calibration curve.

The low-frequency distortion of the woofer, even at a 10-watt input level, was very low, and it actually decreased at 20 cps, where the output was beginning to rise. Any good amplifier of 10 watts rating or better should be able to drive it satisfactorily.

In listening tests, the Classic Mark II sounded very clean...there was an undercurrent of bass, more often felt than heard, that was completely lacking in some other quite good speaker systems that I compared to the Classic Mark II. The speaker sounded at its best (to my ears) at moderate levels. At high levels the bass tended to overpower. A different listening room, of course, could easily alter this situation completely. Overall, the sound was beautifully balanced, with wide dispersion and a feeling of exceptional ease. There was never a hint that three separate speakers were operating; the sound seemed to emanate from a large, unified source.

In my opinion the University Classic Mark II justifies the substantial claims that its manufacturer has made for it. It is one of a limited group of speakers to which I would give an unqualified topnotch rating. Anyone who is in a position to consider a system of its size and price would be well advised to hear it. The price of the system is $295.00."

WRITE TODAY FOR THE COMPLETE JULIAN HIRSCH HI-FI STEREO REVIEW REPORT on the new CLASSIC, as well as the documented CLASSIC brochure and "Informal Guide to Component Stereo High Fidelity." Simply write: Desk P-4, University Loudspeakers, 80 S. Kensico Ave., White Plains, New York.
This One Picture Tube...

Replaces 19 Types


RCA-21CBP4A UNIVERSAL SILVERAMA® PICTURE TUBE may be installed in place of any of the above types, regardless of manufacturer.

Think of the simplicity, economy and efficiency of having just one picture tube type to take care of OVER 25% of your replacement needs. That's exactly what you get with the RCA-21CBP4A, one of a growing family of universal Silverama picture tubes designed to help you cover the maximum number of sockets with the minimum number of types. Other universal types are listed on the chart, below left.

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Like all Silverama picture tubes, these universal types are made with all-new electron gun, finest parts and materials, and a high-quality glass envelope that has been thoroughly inspected, cleaned and rescreened prior to reuse.

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