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CCD309 Color/B&W IR Waterproof Bullet Camera $169.95

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Lost In Space?

It was back in August that NASA attempted to fire the engines of its CONTOUR spacecraft, but to no avail. Controllers could neither contact the vessel, nor did the vessel attempt to automatically contact control, as it was programmed to do in case of a failure. Nearly two weeks after the incident, Chief Engineer Theron M. Bradley Jr. was appointed as the leader of an investigation unit that has been tasked to find out what exactly happened. An earth-based observatory spotted three objects within the guesstimated region of the craft, and this has led to the belief that the CONTOUR broke apart. Now, I know my readers can empathize with a team who has just lost their project to some unexplained (as of this printing) glitch. How many times have we built a prototype, with care, precision, and passion, only to see it either not work at all, or destroy itself in a fit of mechanic mayhem? Unfortunately, the apparent destruction of the CONTOUR also marks the destruction of some pretty nifty ancillary equipment. These included a high-tech dust sampler and a spectrometer to measure trace elements. The CONTOUR was designed to chase comets, observe them up close, and beam back the data. Many non-techs and adversaries of space exploration whined in unison once they found out how much money was inadvertently lost, and they even went as far as to suggest that funding should be stopped. Luckily, the powers that be understand the need for the exploration of space, and how important it is that we learn more about the relationship of our planet to the rest of the solar system. This includes chasing comets, which have a direct impact on our environment (especially our oceans and atmosphere). So, it is with a somber “via con debris” that we say goodbye to the CONTOUR spacecraft.

Enjoy,

Chris La Morte
Managing Editor
Dateline: November 1952 (50 years ago)

Magnetic tape TV recording is almost here—a milestone in the television industry—and discussed in *Radio Electronics*’ editorial. The cover feature is a transistor-operated sawtooth oscillator that functions as a signal source for testing others. A bit of trivia: 2,517,157 TV sets had been produced during the first seven months of the year, along with 5,280,079 radio sets and 1,639,097 auto radios.

Dateline: November 1972 (30 years ago)

"Looking Ahead" in this month’s *Radio Electronics* reports that more than 10% of the nation’s homes are receiving television by cable. Western Electric is producing lithium tantalite crystals, the first practical alternative to quartz for use in communications equipment. Building R-E’s Grinchwal digital test equipment makes the cover story; and Volkswagen introduces computerized self-analysis, for automotive diagnosis, to the auto industry.

Dateline: November 1992 (10 years ago)

Looking to install your own telephone system? Refer back to this issue of *Popular Electronics* Construction articles cover a voice-mail alert system, a 49-MHz FM transmitter, and a one-amp current injector. An instant replay multi-standard VCR, roadmap software for the PC, and a universal remote control are all in the “Gizmo” product review.
EXCITING NEWS!

POPTRONICS Interactive Edition

Beginners to electronics now have a new medium to help them. POPTRONICS has launched a new e-magazine on the Web, aimed at covering basic electronics with easy-to-understand theory and lots of construction projects. Now you can enjoy your hobby even more!

It's called POPTRONICS Interactive Edition and will be released each month, entirely on the Web. This fantastic new concept has been in the design-stage for two years and now the first issues are on the site for viewing! Each month the site will increase with a range of articles and projects. Everything will be linked for easy access and navigation. Get in on the ground floor and visit the site now...

Type the following into your browser: www.poptronics.com/interactive/intro.html. There are sample pages and articles so you can see how we have laid things out and what's in store. It's very easy to navigate. It's like sitting down and reading a magazine, but with the impact of full-color and interactive features such as circuits that move and self-scoring tests. The site will contain many different sections and everything will be based on a "learning approach."

The first issues of the e-magazine will cover the basics of electronics, and in this way, everyone will be brought up to the "starting-line."

POPTRONICS Interactive Edition will also present complex projects as well, so everyone will be catered to. As with any course, projects will be offered at every stage, and these can be purchased by simply clicking the "Buy Me" button at the side of the article and a couple of clicks gets the kit(s) to you very quickly.

New sections will be constantly added, and the first issues include a Basic Electronics Course, a PIC Microcontroller Programming Course and the basics of electroluminescent emission.

The Basic Electronics Course starts with a new approach. Mathematics has been kept to a minimum and components are introduced via simple circuits. An on-line calculator for resistors and capacitors (in parallel and series), as well as an easy-to-use color code calculator for 4- and 5-band resistors, helps identify these important components. The Basic Electronics Course continues with circuits that "move" so you can see how a technician "sees" a circuit operating. You must be able to see how a circuit works if you want to work on it successfully. Basic circuits are called "Building Blocks." As your knowledge of these "blocks" increases, you will be able to design your own circuits.

The PIC Microcontroller Programming Course also starts with the basics and has a complete Library of Terms. The microcontroller we have chosen is the PIC16F84, as this is re-programmable so a project can be "up-and-running" at very little cost.

A low-cost programmer is available, as well as prototyping boards and a display project with more than 28 experiments. They are designed to reinforce your understanding. After carrying out the experiments in the 5 x 7 Display project, you will be well on your way to understanding PIC language.

The Electroluminescent Emission section introduces electroluminescent material in a flat format, as well as tubular material. By combining our driver projects with the wide variety of shapes and colors of electroluminescent material, you can create displays for model-railway layouts, promotional displays, or anything that needs illumination. You can also combine fiber-optics into the display to get even more stunning effects. All the materials and kits for the projects are available via the Order Form in the article, so you are not left "up-in-the-air" when it comes to putting your ideas into practice.

Everything on the website is linked. Simply type www.poptronics.com/interactive/intro.html into your browser, and everything else is just a click away. Sample pages and projects are viewable for FREE, while the remainder of the site requires a password. To obtain a password, you will need to subscribe.

SUBSCRIPTION RATES:

A subscription to POPTRONICS Interactive Edition costs $19.95 for 12 issues. This allows unlimited viewing and downloading. Alternatively, you can take a 2-issue trial subscription for $3.99. A new issue will be available on the first day of each month. Many of the articles, tables and data sheets will be linked to keep information "at hand," so it's important to keep your subscription current as you will be constantly referring to the site. If you are already a subscriber to POPTRONICS, a special offer is available. Simply quote your POPTRONICS SUBSCRIPTION NUMBER (located on your subscription label) when subscribing, and you will only have to pay $9.99 for a 12-issue subscription. A two-issue trial subscription costs $1.99.

POPTRONICS will remain in its printed format. The material and content of POPTRONICS and POPTRONICS Interactive Edition will be kept separate, and if you are into electronics, you will want both versions. Log on to POPTRONICS Interactive Edition now. You will be amazed at the content and layout.

www.americanradiohistory.com
Feedback
Hello, folks. I guess it has been some time since we've last seen "Letters" in these parts, so now's as good a time as any to reinstate some feedback. After all, what our readers have to say is important. Your letters are like a metric that is used to gauge the performance of the magazine. If we do something good, you'll tell us; and if we do something silly, you'll tell us twice. So, once again, we give the floor to the readers. First up is a fledgling engineer who is perhaps our youngest reader. Check out his picture on this page. No doubt this technical tyke is destined for success, armed with his trusty copy of Poptronics and an enormous power tie.—Editor

A Well-Groomed Engineer
My Daddy and I love your magazine! Thanks for all the ideas and information! I learn so much every day.
TIAN SNYMAN, future electronic genius Melbourne, FL.

Glad to hear you enjoy our magazine, Tian. Many hobbyists are growing concerned that electronics is a dying pastime ever since computers took over the spotlight. Yet, as long as we have parents like T.J. and Ana Snyman, who know how to nurture their children on quality print media, all is well for the hobby. Although, Ana admits that Tian likes to look at the schematics mostly.

—Editor

I Made a Mismatch
Stanley Clarke? Does he live anywhere near the Great Pyramid?
A DISAPPOINTED SUBSCRIBER via e-mail

Mike Eck offers this formula: Stanley Kubrick + Arthur C. Clarke = Stanley Clarke

Yes, indeed! This was a classic cross-association of semantics. We have director, writer, and musician all jumbled together. Ah, to err is human. I am happy to see that readers of our magazine know their way around the Speculative Fiction (dare I say Sci-Fi) aisle.—Editor

Circuit Suggestion
I am a devoted reader of Poptronics. May I suggest the development of a "Vibration Analyzer" circuit based on a PIC? This circuit could be very interesting and useful. Thank you.
EDUARDO ESQUIVEL, Peru

We'll see what we can do, Eduardo. Until then, take a look at T.J. Byers monthly "PIC-tronics" column for interesting and useful projects that are controlled by one of the most popular lines of microcontrollers. Also, take a peek at Poptronics Interactive at www.gernsback.com. There you'll find Colin Mitchell serving up a fine sampling of PIC-based projects.—Editor

Remembering Grace
I met Grace [Hopper] at one of her lectures. She looked me up and down as though I were a lab specimen and, with a disapproving look on her face, said, "You're not much more than six nanoseconds tall." Then she grinned and reached out to shake hands. A feisty young lady (at heart), she had a smile that warmed you to her. She was noted for having repetitively requested, "Show me a nanosecond," until one of her cohorts gave her a piece of electric cord cut to the length of one nanosecond. My meeting with her led me to develop Tynon's NANOSTIK, and I'd like to send one to the author of this excellent article. The NANOSTIK is a plastic ruler, one nanosecond in length, marked off in 10 major divisions, each divided into ten minor divisions. It is marked, "In MEMORY OF CAPTAIN HOPPER, USN."

KEEP IN TOUCH
We appreciate letters from our readers. Comments, suggestions, questions, bouquets, or brickbats... we want to hear from you and find out what you like and what you dislike. If there are projects you want to see or articles you want to submit—we want to know about them. You can write via snail mail to:

Letters
Poptronics
275-G Marcus Blvd.
Hauppauge, NY 11788

Sending letters to our subscription address increases the time it takes to respond to your letters, as the mail is forwarded to our editorial offices. Our e-mail address can be found at the top of the column. Of course, e-mail is fast. All of our columnists can be reached through the e-mail addresses at the head of each column. And don’t forget to visit our Web site: www.gernsback.com.

Here is one-year old Tian Snyman relaxing with a brightly colored issue of Poptronics.
Fig. 1. This is the corrected schematic for the "Watt/Hour Meter" that originally ran in the April 2002 issue of Poptronics.

FRANK TYMON
Quartz Hill, CA

Tube Talk

As a lifelong (46 years and counting) electronics hobbyist and professional, I enjoy your publication immensely. I noted that the schematic for the "Tubeester" on page 24 of July 2002's issue shows one error and one omission. The battery polarities for the positive and negative nine-volt stacks for the ICs and the 6F5 tube are reversed in the drawing. The connection to pin four of IC1 is also supposed to go to the negative nine-volt connection, but it is unlabeled. My compliments go out to the author in his mix of old and not-so-old technology into an interesting project. Warmest tropical regards.

PAUL R. DEDRICK, CET, CSM, A+ via e-mail

If you check your tube manual, you'll find that a 6F5 heater draws 300 mA, not the 150 mA stated. As always, I enjoy the magazine and have been reading Gernsback Publications since the Shortwave Craft and Radio Craft days.

BLAKE HAWKINS, N+YCQ via e-mail

Thank you both for your insight.—Editor

Transistor Test

In the July 2001 "Q and A" column there was a question about identifying transistor base, collector, and emitter leads. I have frequently used an ohmmeter for that purpose. The base/collector diode is slightly more conductive than the base/emitter diode. On an analog ohmmeter it is usually about a needle's width lower for the base/collector diode. With a digital ohmmeter it is harder to observe the difference. I recently measured a 2N4403 and the readings were .670 and .671 using the diode-test setting. You will have to repeat the test several times in order to notice the difference.

STEVE WHITESIDE, Ph. D., EE via e-mail

Watt/Hour Meter Corrections

This is in reference to the April 2002 Poptronics issue. I became very interested in building the "Watt/Hour Meter" in that issue; however, at the time I was a student and did not have much free time. Now that I started looking at the schematic closer, I have noticed errors.

JEREMY MILLER
Fargo, ND

Thank you for your keen eye and attention to detail. We have incorporated your findings in the corrected schematic on this page.—Editor
Find Your Way

Never get lost again! The Handheld Electronic Compass ($47.95), featuring patented magnetic sensor technology originally developed for the military, is rugged and reliable—ideal for outdoor and marine use. It comes with clock, timer, stopwatch function, and reference-pointer electronic calibration. Water resistant to ten feet, the compass features a large, easy-to-read display and sounds a warning when there's magnetic interference.


CIRCLE 50 ON FREE INFORMATION CARD

Ultra-Sonic

Experience supreme sound quality and Dolby Digital technology through these 900-MHz Wireless Surround Sound Headphones ($299.99). Compatible with both digital and analog audio/video equipment, the headphones promise sonic detail virtually identical to that of a movie theater. The signal transmits up to 300 feet, through walls, floors, and ceilings; and the batteries hold the charge for more than six hours at a time.


CIRCLE 53 ON FREE INFORMATION CARD

Sound In Style

A fine blend of technology and craftsmanship, the Infinity Kappa 600 Loudspeakers ($1199 each) are three-way floorstanding speakers that deliver full-range performance in sophisticated home-theater and music systems. Measuring 38 × 8¼ × 17 inches, the Kappa 600's all-C.M.M.D. (Ceramic Metal Matrix Diaphragm) driver complement includes a 1-inch tweeter, 6½-inch midrange, and 8-inch side-firing woofer. The system reproduces music with clear, extended high frequencies to 27 kHz, and open, detailed mid-range, and low-frequency extension down to 30 Hz.


CIRCLE 51 ON FREE INFORMATION CARD

Triple Tough

Designed for the great outdoorsman, the Pathfinder Triple Sensor Tough Solar Watch ($250) is a valuable piece of gear for mountain climbing, trekking, and other extreme outdoor activities. Not only does the watch tell time, but it is equipped with a special triple-sensor system that identifies direction, altitude, and important weather data. One especially cool feature—the back-light inclination sensor automatically switches on whenever the user bends his arm to check the watch.


CIRCLE 52 ON FREE INFORMATION CARD

Dream-Loungers

Hand-built, the DreamLounger Home Theatre Seating collection—the Jazz Recliner/Rocker ($1700), the Cruiser ($2700), and the Montreal, leather ($2180)—comes standard with a 22-inch wide seat, offering both comfort and style. Each lounger boasts unique features: The contemporary-looking Jazz reclines or rocks according to preference; the low-riding Cruiser has a matching ottoman; and the Montreal is covered in plush leather with ultra lumbar and head support.

Theatre Design Associates, 2224 W. Fulton, Chicago, IL 60612; 800-786-6832 or 312-829-8703; www.theatre design.com.

CIRCLE 54 ON FREE INFORMATION CARD
Sky Surfers

Fly away! With a 30-inch wingspan and individually controlled strut-mounted propellers, the Power Air Surfer Radio Control Airplane ($50) can soar as high as 100 feet and as far as 300 feet. Easy to launch and land, the plane is perfect for beginners or advanced R/C pilots—with practice it can do dives, barrel rolls, spirals, and spins. The plane also comes in two different styles, has two on-board motors, a portable field charger, and a unique wing design that prevents most crashes.

Hasbro, Inc. 1027 Newport Ave., P.O. Box 1059, Pawtucket, RI 02862-1059; 401-725-8697; www.hasbro.com.
CIRCLE 55 ON FREE INFORMATION CARD

Super Sets

Offering a smooth, crisp picture and enhanced, high-tech audio, the 34-inch Flat-Plate Direct-View RCA Scenium D34W13SD TV ($2599) features a built-in DVD player. The monitor has an exclusive, decorative Clip-On Frame—easily snapped on to the face of the TV—that allows you to change the cabinet design according to your room decor. It also comes with Virtual Dolby Surround capability, secure digital DVI-HDTV inputs, and dual Syncrosan HD component video inputs.

Thomson Multimedia, 10330 N. Meridian St., Indianapolis, IN 46290; 317-587-4450; www.rca.com.
CIRCLE 57 ON FREE INFORMATION CARD

Short and Sweet

For use at your bedside or anywhere in your home or office, the Boston Acoustics AM/FM Radio ($150) has a maximum of 19 presets, as well as alarm capabilities. Available in white or silver/gray and designed to be competitive with the Bose Wave, this compact radio boasts great reception, precision tuning, and superb sonic performance.

CIRCLE 58 ON FREE INFORMATION CARD

Power Tower

Taking up barely a square foot of space, this DVD Power Tower ($169.95) organizes up to 80 DVD movies in their cases. Turn the switch on and your entire collection rotates 360 degrees right or left, fanning the front, back, and spine of each DVD for easy selection. Even better—when the motor is activated, a built-in, ultra-bright LED lamp illuminates the case in a darkened room, and then automatically turns off about 20 seconds after rotation stops.

CIRCLE 59 ON FREE INFORMATION CARD

Eye Spy

Planning a sting operation or want to check on your babysitter? This Remote-Control Activated Wireless Surveillance Camera ($2395) is just what you need to observe your subject without he/she having a clue. Disguised as either a plant, clock, or smoke detector, the camera can be charged and placed in the area you'll be monitoring. When the subject enters the area, just hit the button on the remote and begin transmission. The package comes with camera, recorder, receiver, and color monitor.

CIRCLE 59 ON FREE INFORMATION CARD
PC Protection

Shield yourself from dangerous viruses, malicious hackers, intrusive cookies, and annoying Internet ads with the ZoneAlarm Pro 3 ($39.99). This complete security solution provides solid protection for your computer system around the clock. Pinpoint and map the origin of would-be intrusions with new, advanced hacker-tracking and stop unwanted advertising with customizable ad blocking. The program also includes powerful cookie control and enhanced MailSafe protection.


Creative Control

You can turn your PC into a powerful multi-track recording studio with Cakewalk Home Studio ($129). Musicians can record unlimited audio and MIDI tracks, mix with real-time audio and MIDI effects, compose and print sheet music, and create video soundtracks. The software supports real-time DirectX effects, MIDI FX plug-ins, and more. Pyro MP3 and CD Maker (trial version), Virtual Sound Canvas DXi soft synth, Dreamstation DXi soft synth, and an ACID-format audio loop library are all included in the package.


At Your Fingertips

Staying organized couldn't be easier with the Palm m130 Handheld ($249). With the included bonus software, read an eBook; view Word, Excel, and PowerPoint files; create a digital photo album; beam video clips—all in the palm of your hand. The backlit, easy-to-read display supports thousands of colors to make games and photos come alive. The expansion card slot enables you to add games, applications, eBooks, and more. You can also snap on options, such as a portable keyboard.


Smart Storage

Now you can digitally store all your music in one place with the i Pac Music Center ($399). This 17-inch home-audio component uses PC intelligence to record and store your entire digital and analog music collection in MP3 format. It has enough capacity for nearly 400 audio CDs or 5000 individual songs, creates an unlimited number of custom play lists, and lets you listen to Internet radio stations from around the world.


Classy Camera

Portable and sophisticated, the Digital Revio KD-400Z Camera ($499) has a stainless steel alloy exterior, an ultra-slim body that enhances mobility, and a sliding protective lens cover. The SD Memory Card and Memory Stick Dual Memory slot allows users to easily transmit images to PCs and peripherals, including mobile phones, PDAs, and photo printers. The camera also features a high-performance 3X optical Hexanon zoom lens and ultra-high 4.13-megapixel resolution.


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Cyber Security

Let's face it. Almost all of us surf the Net, send and receive e-mails, and engage in online activity without a second thought about our privacy. Who could possibly be spying on us? Who would even care? The truth is that there are a lot of "peeping Toms" who are interested, for one reason or another, in what we are doing online.

From marketing companies to hackers, from scammers to nosy bodies, there are people who want to know about us. You can actually be tracked from your mouse clicks; and the pages you read tell those vigilant individuals just what to sell to you, what to scam from you, and countless other private things.

This article isn’t meant to scare you into never going online again. Using the Internet is inevitable and necessary for most of us. The point is to make you aware and to present precautions. There are ways around the Internet “spies” and many ways to protect yourself. A little knowledge can go a long way.

E-MAIL—A DANGEROUS JOURNEY

You innocently type your personal e-mail message to a recipient miles and miles away. You think it magically appears—unscathed, unopened—on the receiving end. Not true. Once you press that SEND button, your e-mail travels from one computer to another down an undetermined path through network traffic and routers—it basically takes the scenic route, dotted with overlooks and pit-stops—until it reaches its final destination. Before the message reaches the recipient, however, it must check in at the Post Office Protocol (POP); where it is either delivered immediately or temporarily saved for postponed delivery.

The e-mail’s journey can prove hazardous to both parties, as there are ways that a third party can scan that e-mail along its way. There’s actually software that can search for keywords, names, and e-mail addresses. Any e-mails that contain something of interest can be saved and looked at later.

Hackers do this all the time—either for a specific reason or just for kicks. Marketers can do this, also, to target their customers and plan their sales strategies. Later, we will get into how it’s done and how to protect yourself.

E-MAIL SCAMS, SPAMS, AND MORE

I’m sure you’ve been spammed before and don’t even know it. Sounds like you’ve been violated, right? Well, in a sense, you have. Spamming (which is illegal, by the way) occurs when a company pumps out thousands of e-mails (similar to junk mail) to an intended audience, selling or pitching something. Did you ever wonder how or why you are suddenly receiving e-mails advertising sporting equipment?

Then you remember that just recently you purchased a set of golf clubs from a Web site.

Your name and information can spread like wildfire through the Internet. Just like they sell mailing lists and demographic lists to retailers, companies on the Web also scrutinize every move you make, examine every purchase, and pass that information on to willing buyers.

Although most spamming is completely harmless, it can be intrusive and annoying. You may have to delete dozens of e-mails every day just to organize and clear out your in-box. It’s the scamming that you must beware of. Just recently I was the target of an international e-mail scam (I was actually somewhat honored that I was chosen!). Apparently some extortion group in Nigeria was trying to siphon small amounts of money from thousands of people. They would send an e-mail stating something like "If you send a check to our bank for $$$$ and invest in our company, we promise so much on your return in just a few months." Now, I don’t know how many folks actually fell for this, but it isn’t uncommon for these con-artists to try and swindle money through the Internet. Just use common sense as you would for anything else, and you should be fine.

NOT YOUR ORDINARY COOKIE

I’m not talking about good old chocolate chip cookies. These are menacing cookies that aren’t meant to be eaten. Many organizations use these "cookies" to track your every move on the Web. A cookie is a unique identifier that a Web server places on your computer (sort of like a tag that’s attached to an animal in the wild to track activity and behavior). Once your identity becomes known, that one...
company is free to share it with mail-order companies and anyone else willing to pay for the information. This practice could have some scary implications—just use your imagination.

There are ways to disable cookies. There is cookie-management software, or you can simply tell your browser that you don’t want cookies. Before taking these steps, I would look into it a little further, as it can become somewhat complicated depending on the browser.

**TAKING PRECAUTIONS**

There are several things you can do to protect yourself—ranging from the very extreme action, such as encrypting your messages, to just using your head and following a few simple guidelines. We’ll cover both ends.

Please take this advice and pass it on to your children and/or grandchildren. There are a few “Never”s in the Internet world. Never give out your last name, home address, or phone number in chat rooms or on bulletin boards. Never give out your screen name, user ID, or password except to close family or friends. Never give information about yourself to anyone or any Web site if you don’t feel comfortable. Companies should never ask for anything that isn’t relevant to the situation or purchase at hand.

These are just a few common sense tips to follow for minimal protection. A couple of more intense security methods follow.

**SOFTWARE SECURITY**

There are software security packages that can protect your IP address, neutralize cookies, and generally prevent tracking of your online activity. ZoneAlarm (see the review in “Gizmo”) and Freedom WebSecure are two of these programs. This privacy software acts like a shield to safeguard your personal information so you can surf the Web anonymously. It encrypts and reroutes your connection requests through proxy servers so hackers can’t track you, and the programs also block potential security and privacy threats. Although the concepts the software uses—like encryption, which we will get into later—are complicated, the packages are easy enough to install and use.

**FIREWALLS**

In the physical world a firewall keeps a fire from spreading from one area to the next. In the computer world, a firewall is a program or hardware device that filters information coming through the Internet into your computer or network. It creates a barrier to keep hackers and offensive forces away.

These filters use several traffic-control techniques.

Packet Filtering—Packets, or small clumps of data, are analyzed through a set of filters and then sorted; and they are either sent through or discarded.

Proxy Service—Information is retrieved from the Internet by the firewall, sent to the requesting system, and vice versa.

Stateful inspection—This method compares key parts of data to a database of trusted information. It is monitored for certain characteristics and then either allowed through or discarded.

**ENCRYPTION**

This term sounds like something out of a spy movie, but encryption is now seen as a pretty secure way of transmitting e-mail. It works something like this. When you want to send an e-mail, you type it just the way you want it. You would then hit an “encrypt” option on the mailer software, and it then mixes and re-mixes each binary bit of the message. The message can only be unscrambled by the same exact software, using the sender’s private code. The receiver would then hit the “decrypt” button, type in the code, and Voila—a readable message that only that recipient could decipher.

It seems like a big digital mess— and it is while it’s in the encryption mode—but it is one of the safest, most foolproof methods of keeping your e-mail private. Of course, as with anything, there are hackers out there who will try and break the codes. Some will succeed, but it will take a lot of effort.

Encryption software has actually been around for quite some time, maybe twenty years or so. However, it wasn’t as secure and tamper-proof as it is now, and it is becoming more popular because of technical improvements, efficiency, and availability.

**WRAP UP**

There are many books on the subject of Internet security. If you are really interested in protecting your privacy online, I would suggest doing some research first. There is a lot of information online, also. Just remember—use your head and be aware that “Big Brother” may be watching at any time.
A TV in Your PC?

If you've ever given it any thought, you'll realize that most PCs have better video capabilities than most television sets. A good quality television has about 500 lines of vertical resolution, while even a VGA-resolution computer display has 640 lines. The two aren't really comparable, because the TV display is mapped for the lower resolution; so it won't actually improve all that much from the increased number of displayable lines.

In fact, some interpolation needs to take place so that an image designed to be displayed at 500-525 line resolution is correctly displayed at 640 lines. S-Video, such as that from a Super VHS VCR, has over 700 lines of vertical resolution and actually looks terrific on a computer display set for VGA (640 x 480) or SVGA (800 x 600) resolution.

None of the current crop of video cards has the slightest bit of trouble displaying a television transmission. If you have a large display of decent quality attached to your PC, the only thing that you really need to watch TV on your computer is a tuner that's capable of picking up broadcast or cable transmissions.

These tuners have been available for years, either completely integrated into the PC video card or as add-in cards. ATI and Matrox have both offered video cards with built-in TRV tuners, and Matrox and Hauppauge Technologies have also offered add-in TV tuners. None of these, however, have sold all that well over the years. That is, until recently.

SEE IT YOUR WAY

The spark that ignited the interest in computer TV hasn't been the availability of inexpensive large displays, though that hasn't hurt. Rather, a device from Philips called TiVO, sold under it's own and several other vendors' brands, has made PC owners aware of some of the advanced possibilities that add-in TV capabilities to your PC can offer.

TiVO, and a similar device from S3, are PVRs, or personal video recorders. They contain a cable-ready TV tuner, a hard disk of varying capacity, and electronics. These electronics allow you to scan a program guide, and decide what TV shows you want to watch. The PVR stores your request and, at the appropriate time, records the show in a compressed format on its internal hard disk. When you want, you can simply turn on your TV set and watch the recorded show from the PVR.

So far, the PVR doesn't sound much different from the VCR it is probably replacing, other than the ability to automatically record choices from an Internet-based guide such as GemStar's or Titan's. Where the PVR starts to strut its stuff is in the versatility it displays. TiVO can note what type of shows you like to watch, and automatically record that type of show without further user intervention. Another great feature is that you can set the device to skip commercials. Needless to say, the TV advertising industry is less than enthralled by this feature.

EASY PVR

You can get the equivalent of a TiVO box simply by adding TV Tuner capability and some software to your PC. There are several ways to do this. The simplest is to just add a video card that contains its own TV tuner. We tested two of these, a Personal Cinema card from Compro (www.comprousa.com), and an All-In-Wonder RADEON 8500 from ATI Technologies (www.ati.com). Both cards are similar in concept, with the Compro card we tested based around NVIDIA's GeForce4 Ti4200 chipset and the ATI card using ATI's own RADEON 8500 video chipset.

The Compro card, which retails for about $299, has a small green external box to which you can connect the external TV antenna or, in our case, the cable connection. This breakout box also has connectors for S-Video and composite video in and out, so you can attach a VCR or camcorder to the Personal Cinema and either output video from the tuner to a VCR or other recorder or perform video capture from an external device. The card has both analog and DVI digital output for connection to your display and comes with Intervideo's WinDVR for PVR functions, WinDVD for playing back DVDs, and MGI VideoWave SE for video capture and editing. We found the WinDVR easy to use, and the card provided excellent video performance as both a gaming video card and PVR.

The ATI All-In-Wonder RADEON 8500 ($199) also gives excellent performance in both of these areas. ATI
has announced its next generation of video chips, the RADEON 9000 series, so there may be an All-in-Wonder board based on this new chipset by the time that you read this. The All-In-Wonder also has a break-out box with connectors for video and audio inputs and outputs, but one is a dongle-like cable that we found just a touch less convenient than Compro's approach. On the other hand, Compro's Personal Cinema uses an infrared remote control, while ATI uses an RF-based remote. This feature means that you'll have to position the green breakout box on the Personal Cinema where it can "see" the remote's signal. The All-In-Wonder's connector can remain out of sight under a desk if that is more convenient. ATI provides its own software, but it operates very much like the WinDVR that's supplied with the Compro card.

IF IT AIN'T BROKE...

If you are quite happy with your present video and don't like the idea of being forced to upgrade it to gain PVR capabilities, there is an alternative. SnapStream Media (www.snapstream.com) has a terrific PVR package, SnapStream 2.0 that works with most of the TV-tuner-enabled cards currently available. A list of compatible cards can be found on the vendor's Web site.

We tested SnapStream Personal Video Station (PVS) 2.0 with a card that was supplied with the software, a Hauppauge WinTV PCI card. This is an inexpensive tuner and video-capture card that works in conjunction with the video card already installed in your PC. Hauppauge has a variety of different TV cards, starting at about $99.

SnapStream 2.0 is very easy to install, but the TV card needs to be working before you start. We installed the Hauppauge WinTV card in a Pentium 4 system that was running an NVIDIA GeForce 4 Ti4600. We installed the WinTV drivers and software and attached the cable from one of the cable TV outlets. The WinTV software needs to be configured as to the video source, and you also need to let the software run the tuner up the channels to see where there is actually a signal. Then go back and remove the channels that are scrambled, as the WinTV card does not function as a cable TV descrambler. You can also run a cable from a cable box and use that input to record premium channels that you subscribe to. In this setup, you'll be recording from the output channel that the cable box uses (usually 2 or 3), not the actual channel itself.

Once you have the WinTV card working and configured, install SnapStream 2.0. You can set SnapStream 2.0 to record at different picture quality settings, depending upon how much hard-disk space you have available. SnapStream works with the Titan on-line program guide. This guide is free; just register where you live and what cable system you subscribe to, and you can see what's on simply by logging onto the site. Click on the little red button icon, and Titan will automatically tell SnapStream to record the program that you want to watch.

SnapStream works well, though with the WinTV card we occasionally experienced some out-of-sync audio. Since it also works with other TV-capable video cards, we tested it with the Compro Personal Cinema card. We actually got a bit better performance with the GeForce4-based Compro card over the WinTV card SnapStream provided us with.

On-line program guides such as those offered by Gemstar (www.gemstartvguide.com) and Titan (www.titantv.com) have made searching through local programming a breeze. Most of these services are provided free of charge.

SOURCE INFORMATION

ATI Technologies
www.ati.com

Compro
www.comprousa.com

Gemstar On-Line TV Program Guide
www.gemstartv.com

SnapStream Media
www.snapstream.com

Titan On-Line TV Program Guide
www.titantv.com

JUST LOOKING

Regardless of whether you simply add a tuner to your existing card or replace the card with a video card that includes a tuner, it's easy to set up and use your PVR. The newest generation of NVIDIA-based products has dropped the price of the GeForce2 Personal Cinema cards dramatically. The original GeForce2 MX Personal Cinema card is, as this is being written, available from Compro's on-line store for a clearance price of $79. There are comparable prices for other Personal Cinema cards, depending on which GeForce card the PVR is based on. ATI also has blow-out prices on the earlier versions of its All-in-Wonder cards. So now is a great time to add a TV and PVR to your PC, ASAP!
Tips on Useful Tips

Some people love to tinker—to take what they have and try to improve it. Others regard tinkering as the equivalent of sticking a screwdriver inside an electrical outlet.

A personal computer and the software that runs on it, as customizable as they are, give you great opportunities for tinkering. Many people personalize their PC with add-on hardware, software utilities, keyboard shortcuts, and other tricks to such an extent that the PC becomes an extension of their very personality. Other people keep their PCs at, well, arm’s distance, running only those programs that came with them and even here sticking only to the basics.

KEEPING TIP-TOP

There are good reasons for tinkering, and there are equally good reasons for leaving well enough alone. The most compelling reason for hunting down computer tips and techniques is that it can make you more productive. You can perform tasks with your PC that you couldn’t otherwise or you can perform tasks that you currently do, but faster or with less hassle.

The single best software utility program, for instance, that I’ve come across—I’ve been using various versions of it for years and have found none better at what it does—is PowerDesk Pro (www.ontrack.com/powerdesk). This Windows file manager lets you copy, move, and compress files on your hard disk with greater dexterity than the tools provided by Windows itself. If you need to stay organized in this way, this $30 add-on will more than pay for itself.

Some tips are simply fun. Microsoft PowerToys lets you make adjustments that Windows alone doesn’t, including viewing the icon of the application window you are switching to when pressing Alt-Tab, magnifying part of your screen from the taskbar, and managing up to four virtual desktops. Different versions of PowerToys exist for different versions of Windows, with the Windows XP version at www.microsoft.com/windowsxp/pro/downloads/powertoys.asp.

Other tips can help keep in check the inevitable wear and tear your body experiences from sitting in front of a PC for long periods of time. My favorite is using Microsoft XP’s accessibility options—although primarily designed for people with limited use of their hands or eyes, they can be used by anyone. What I do is direct Windows to use a high-contrast combination of text and background colors—white text on a black background instead of the traditional black text on a white background. This dramatically reduces both the amount of light shining into my eyes from my computer monitor and the eyestrain I experience from using my PC.

To make this change, you can access Accessibility Options through the Control Panel, or you can use the shortcut keyboard combination Alt-Shift-PrintScreen. Most programs and Web sites work fine this way, but, with some, you’ll need to temporarily switch back.

RISKY BUSINESS

There is, of course, the risk of mucking things up whenever you tinker: deleting important data, corrupting programs, or temporarily disabling your computer. Tinkering can create support headaches for larger organizations, which is why some restrict it.
Writing Well for the Web

Quick and Easy Tips for Non-writers

by [Author Name]

You can learn more about writing for the Web by reading the numerous references for writers available on the Internet.

The risk of using tips is fairly small, and it shouldn't deter the adventurous. Even if things do go wrong, data can be retrieved from backups, programs can be reinstalled, and the offending add-ons can be removed.

Whether you use a Windows PC, Mac, Linux box, notebook PC, or handheld PC, there are hundreds of tips and techniques worth investigating (though not necessarily all at once!).

The best sources for these tips that I've found are computer magazines such as PC World (www.pcworld.com) and MacHome (www.machome.com), which employ a high degree of professionalism in testing the tips and techniques they recommend and in offering advice, in general. Subscribing is most convenient, but you can also access much of the same information through their Web sites.

Other Web sites can also be good sources, with recommended sites including CNET (www.cnet.com), ZDNet (www.zdnet.com), SuperSite for Windows (www.winsupersite.com), and Macintosh Watering Hole (mac.map.com).

Another good source of tips can be fellow computer users, though you have to be careful about whom you listen to. Some people are more knowledgeable and accurate than others. You can often get very good advice from online discussion groups or you can join a computer user group—they typically meet once a month. Members (or sometimes guests) give presentations on new products or on how to best use existing products. You can search for a user group near you at the Web site of the Association of Personal Computer User Groups (cdb.apcug.org/loclist.asp).

TIPS ON NET COMMUNICATION

As an information-delivery medium, the Internet in many ways is similar to other media; and you can use magazines and newspapers as examples when researching, writing, and presenting information online. However, the Internet comes with its own set of tips and techniques.

Doing Research—Much here depends on whether you're writing for a Web site or a discussion group. Despite the noise of online arguments, much valuable inside information is offered in Usenet, e-mail, and Web discussion groups. Online discussion groups are just that—discussion groups—where people talk by typing. Mistakes can be quickly corrected with follow-up messages. You don't want to be careless, as many people may read what you write; but you don't have to give the same amount of time to research and fact-checking, as with a less fluid medium.

Web sites are typically more formal than discussion groups, but you can also quickly correct mistakes or add to incomplete information. Because people are usually more casual online, you have to be more careful about the research you do there. It's often good policy to check with multiple sources when searching for information, and it's often good policy to present your credentials when offering it.

With a Web site, make sure you identify yourself or your organization and indicate your experience. With online discussion groups, most software lets you automatically append a "sig" to each message, where you can include a few lines of biographical information or a link to your Web site.

Don't think that because you can't find something online, the information doesn't exist. Much valuable information is only available in print. On the

(Continued on page 56)
Modulation Methods, Part 1: CW and AM

Transmitting information on some form of carrier (usually electromagnetic radiation) depends on a process called modulation. The ability to generate the required amounts of energy at any frequency is, of course, necessary for transmission of intelligence via electromagnetic radiation. If this energy cannot have information applied to it in some way, it is useless for most communications purposes. Parameters that can be controlled are the amplitude or power level, frequency of the radiation, and the phase of the waveform of the energy with respect to a known reference.

In addition, some means of extracting this information from the transmitted radiation is needed. This process is usually called demodulation or detection. For this discussion, we will assume that a carrier consisting of electromagnetic radiation in the radio-frequency spectrum will be used. Any frequency can be used, but we will assume it is one between 10 kHz and 300,000 MHz.

These limits are those presently allocated for communications purposes. Ten kHz is low enough in frequency to be audible as a high-pitched tone, if a headphone or speaker is used. Above 300,000 MHz, which is about as high as can be readily handled by microwave techniques, the radio spectrum is called the submillimeter region.

Above about 30,000,000 MHz (10 microns wavelength), it is the far infrared region of the spectrum. This radiation can be felt as heat rays. Visible light starts at about 430,000,000 MHz (0.7 microns wavelength), perceived by the eye as red light. Lasers operate in the far infrared to visible spectrum, and these can also be modulated.

These frequencies allow almost unlimited modulation bandwidth and are used for fiber-optic communications. Even though we will confine this discussion to radio frequencies, be aware that other forms of radiation can also be modulated. The same theoretical concepts will apply, although the physical methods and techniques will generally be very different from those used in the radio spectrum.

Digital-Type Modulation

The simplest and oldest form of modulation is a digital type, that of turning on and off a source of energy (light, RF carrier, etc.). (See Fig 1.) Originally, lanterns with shutters were used. Then, the Morse telegraph used a DC current that was turned on and off to form the dashes and dots of Morse Code. Later, radio waves were used to do the same thing. A key turns a transmitter on and off, generating a continuous wave (CW) signal. Although this technique is not used as widely today, it remains one of the simplest and most efficient means of communication. Only a very simple transmitter, even a very simple oscillator circuit with a single transistor, is needed. The inherently narrow bandwidth occupied by the signal permits the use of a very narrow-band receiver (20 to 100 Hz). This setup enables low-power transmitters to send signals thousands of miles. Reception with a relatively simple receiver is possible.

Radio amateurs do such transmission quite often. This activity is called “QRP operation,” where QRP is CW shorthand for reduced or lowered transmitter power. Worldwide contacts have been made with only a milliwatt of power in the HF region of the spectrum (2-30 MHz), often enough as to be almost commonplace.

Before we discuss modulation methods, let’s look at one factor that limits the potential performance of any given system. This factor is the noise inherent in any physical system.

Let’s Do The Math

The limiting factor on how weak a signal can be and still be received depends on the receiver bandwidth, temperature, and type of modulation. In the following discussion, some high school math is used (algebra and trigonometry). Sorry for the math, but there is really no better way to present this information properly. Mathematics is a fascinating field and the language of science. If you really want to get into electronics or other aspects of engineering or the physical sciences, you need mathematical proficiency to fully understand many theoretical and practical design concepts. If you would rather not follow the math, you will have to take our word for the figures and numbers we use.

The noise power measured in watts in any bandwidth is given by the formula

\[ P_{\text{noise}} = K \frac{T \times B}{2} \]

where \( P_{\text{noise}} \) is the noise power, \( K \) is Boltzmann’s constant, which is equal to \( 1.38 \times 10^{-23} \) joules/degree K; \( T \) is the absolute temperature in degrees Kelvin; and \( B \) is the bandwidth in cycles per second (Hz). One joule is equal to one watt for one second and is a measure of energy. At normal room temperature (taken as 20° C or 68° F), \( T \) is 293° K. Multiplying this out, at room temperature in a 1-Hz

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bandwidth we have a noise power of $4.04 \times 10^{-18}$ watts of power. The watt is inconveniently large for this work, so the milliwatt (.001 watt) is used instead. This noise level is then $4.04 \times 10^{-18}$ milliwatts. Since in RF systems we are usually dealing with very large variations in power levels, the decibel system is used to avoid inconveniently large or small numbers and ratios. Converting this power level to the more useful measurement of decibels referred to as a milliwatt and remembering that a decibel is a logarithmic ratio of two power levels results in:

$$dB = 10 \log \left( \frac{P2}{P1} \right)$$

for a ratio of $4.04 \times 10^{-18}$ where $P2/P1$ is the power ratio

$$dB = 10 \log (4.04 \times 10^{-18}) = 10 \log 4.04 + (-18) \times 10 \log 10$$

dB = 10 (0.606 - 18) = -173.94 dBm (very closely equals -174 dBm)

Note:

dB = 10 log (P2/P1) where P2 and P1 are power levels

dB = 20 log (V2/V1) where V2 and V1 are voltage levels

$dBm =$ decibels with respect to 1 milliwatt reference power level

0 dBm = 1 milliwatt = 0.223 volts RMS in a 50-ohm system

As an example, the following figures are typically those signal levels one would encounter in operating HF (2–30 MHz) SSB or CW amateur radio equipment. Figures have been rounded off, are for a 50-ohm impedance (the usual situation), and are approximate within a percent or so. These readings are those that would be seen on a typical short-wave receiver signal-strength (“S”) meter:

-20 dBm = 22.3 millivolts, “pegs” S meter, very strong signal

-47 dBm = 1 millivolt (approx.), S9 + 26 dB, strong signal level

-60 dBm = 223 microvolts, S9 + 13 dB, a good signal

-73 dBm = 50 microvolts, an S9 (average) signal

-87 dBm = 10 microvolts, (S7+), a weaker but still decent signal

-107 dBm = 1 microvolt, (S3), weak, SSB marginal, CW is OK

-127 dBm = 0.1 microvolt, very weak, only CW readable

The dBm is independent of the resistance or impedance of the system, but the impedance must be specified for it to have any relation to actual voltages or currents. Since noise voltage is related to power and resistance, and power is $P2/P1$, then the noise voltage across a resistance is

$$V_{noise}^2 = \frac{KTB}{R}$$

and

$$V_{noise} = \sqrt{\frac{KTB}{R}}$$

In any generator with a voltage $V$ and internal resistance $R$, the maximum power available to the load occurs when $R_{load} = R$ generator. This is the maximum power transfer theorem. The load power will be $(V/2)^2/R$ or $(V^2/4R$. Then the noise voltage will be:

$$V_{noise} = \sqrt{\frac{KTB}{R}}$$

$$T = \text{Temp deg K}; \text{ note: deg K = deg C + 273}$$

$$B = \text{Bandwidth Hz}$$

$$R = \text{Resistance in ohms}$$

Normally, we use power levels in noise work as it is more convenient. In a system, for example, the noise power
level is inherently -174 dBm in a 1-Hz bandwidth. Considering a 10-kHz bandwidth typically used in an AM broadcast receiver, we could take the ratio of 10 kHz to 1 Hz as 10,000 to 1. This is a 40-dB power ratio (10 log 10,000, or 10 \times 4 since the log of 10,000 is 4; therefore a 10,000 to 1 ratio, which is 40 dB). Adding 40 dB to -174 dB gives -134 dBm, or 134 dB below a milliwatt. In a 50-ohm system, 1 milliwatt equals 0.223 volts RMS across 50 ohms. Since:

\[ \text{dB} = 10 \log \left( \frac{P_2}{P_1} \right) \]

then

\[ \log \frac{P_2}{P_1} = \text{dB}/10 \]

and

\[ \frac{P_2}{P_1} = \text{antilog} (\text{dB}/10) \]

Here we divide the dB ratio by 10 and find the inverse log of the result, in this case 13.4. Since we want the voltage ratio—the square root of the power ratio for a given resistance, we can divide the logarithm by two, which gives 6.7. Finding the antilog of this will give the voltage ratio that 134 dB represents.

\[ \text{antilog} (6.7) = 5.01 \times 10^{\exp(6)} \]

or a 5.01 million to one ratio. Thus, \(-134 \text{ dBm} = 0.223/5.01 \times 10^{\exp(-6)}\). It comes out to be 0.045 microvolts across 50 ohms—the noise-power level in a perfect receiver with a 10-kHz bandwidth. Theoretically, this is the minimum detectable signal (MDS), assuming that the received signal power equals the noise power. (This is only an assumption, as techniques exist for detecting signals below the noise, and the MDS also depends on the signal processing used in the receiver.)

**Dealing With Noise**

A good Morse code operator can usually copy a weak signal that is at the receiver noise level. However, receivers are not perfect. Good receivers used for VHF-UHF work may have noise figures of 1 dB, which means that the receiver noise level is 1 dB above ideal. A typical HF receiver has a 10- to 20-dB noise figure; thus, the signal detectable in a 10-kHz bandwidth, in this case, would be 10- to 20-dB higher (a three to ten times voltage ratio).

External and atmospheric noise limits reception anyway, so noise figures lower than 15 dB or so are of dubious advantage in an HF receiver, especially below 20 MHz. (Strong signal performance is generally more important in the HF region.) It would then be ten times 0.045 microvolts, or 0.45 microvolts.

However, for voice work, at least a 6-dB signal-to-noise ratio is needed for barest intelligibility, with 10 dB being more like it. This requirement raises the minimum input signal to the 1- to 1.5-microvolt level for copying a voice signal, such as that from an AM medium-wave or short-wave station. You would probably not listen to this program for a long time, as it would be quite noisy. Another 10- to 20-dB signal level would be needed for comfortable copying, depending on how badly you wanted to listen to it, bringing the signal level up to 5 to 15 microvolts for reasonable reception. The important thing is the signal-to-noise ratio and not just the signal level. In noisy reception areas, stronger signals are needed. For any system, the bandwidth is important in optimizing the quality of the received signal: too wide, we get more noise and poorer signal-to-noise ratio; too narrow, we may lose some of the information in the signal or introduce distortion.

**The Morse CW Signal**

In the case of the Morse CW signal, the necessary bandwidth can be estimated by examining the signal. (See Fig. 1.) At a speed of 25 words per minute (a fairly rapid, but comfortable speed typical of experienced CW operators), this would be about 125 Morse characters per minute, assuming an average five-letter word. This is roughly one letter and space per 500 milliseconds.

Taking the worst case, the Morse code symbol for the number 5 has five consecutive dots and can be considered as a square wave with five complete cycles in half a second. This is equivalent to a 10-Hz square wave. A square wave consists of frequencies that are mainly fundamental, and the third and fifth harmonics (odd) of the fundamental.

If the square wave is asymmetrical (typical for Morse Code as there are dots, dashes, and spaces), there are second and fourth (even) harmonics, also. Although it is an approximation, a square wave decent enough to be copied as a Morse Code signal consists of harmonics up to at least the fifth. Therefore, a minimum bandwidth of 50 to 100 Hz would be needed in this example, for 25 words-per-minute speed of transmission. This minimum allows for some tuning error and short-term receiver drift. More than this, the signal-to-noise ratio will start to decrease. Less bandwidth will cause loss of the higher harmonics and rounding of the waveforms to where the signal would be difficult to copy, unless the sending speed were reduced.

If speeds of five words per minute were used, bandwidth could be reduced accordingly at the expense of speed of transmission. For this reason, very weak signal CW work is done at slow transmission speeds—to allow narrow bandwidth and an increase in effective receiving sensitivity.

In practice, many receivers for amateur radio CW use 200- to 400-Hz bandwidth, as it allows for more comfortable tuning by the operator, for some receiver drift, and less costly filtering. Even with 400-Hz bandwidth and a 20-dB noise figure, the minimum discernable signal level is around 0.1 microvolts, depending on the operator's skill and hearing acuity.

In most cases, external noise will be the limit anyway. A 0.5-microvolt signal is typically comfortable to copy. Contrast this with the 5- to 15-microvolt figure needed for AM or 2 to 5 microvolts for SSB for marginal copy, and you can readily see the advantages of CW techniques using Morse code or other forms of slow-speed digital modulation in weak signal work. In this era of cheap and powerful computers, the Internet, cell phones, and sophisticated equipment, simplicity still is important.

It is a sobering fact and somewhat amusing to note that the use of plain old (obsole...?) Morse Code, 1940-era radio technology, with a skilled operator can give reliable and dependable emergency communications when all else is knocked out. Only a simple transmitter, a shortwave receiver, and a length of wire strung up between two trees or other supports are needed to get a station on the air. A 12-volt auto battery will do for power. In emergency situations, communications might be impossible using much more sophisticated equipment, whose operation depends on a vulnerable infrastructure destroyed or rendered inoperable in a natural disaster; or made useless and/or inaccessible during a lockdown, terrorist, or national emergency. Do not count on using the
Internet, the telephone system, or your cell phones at these times.

**Amplitude Modulation**

The next form of modulation that evolved was probably amplitude modulation, called AM. In this case, the amplitude of the signal is modulated in some way by the waveform of the intelligence to be transmitted. Here, the envelope of the transmitted AM signal is a replica of the modulating waveform. (See Fig 2.) Usually, the carrier is a sinusoidal waveform, and the modulation is audio or data. The modulating waveform can be represented as a superposition of harmonically related sine-wave components (Fourier's Theorem). The amplitude of the carrier waveform is modulated by the modulation (audio/data), and a mixing action takes place.

The carrier waveform can be represented as:

\[ V_c(t) = A \sin \omega_c T \]

where

\[ \omega_c = \text{freq. radians/second} = 2\pi \times \text{Frequency in Hz} \]

\[ A = \text{peak amplitude of sinewave in volts} \]

\[ V_c(t) = \text{Instantaneous voltage of carrier} \]

\[ T = \text{time} \]

If a waveform is available, having an amplitude that swings between zero and \( V_m \) volts, described as:

\[ V_m(t) = 1 + M \sin \omega_m T \]

where

\[ V_m(t) = \text{total modulating signal} \]

\[ V_s(t) = \text{modulating signal} \]

\[ \omega_m = \text{modulating frequency rad/sec} \]

\[ T = \text{time} \]

\[ M = \text{relative amplitude of modulation} \]

\[ (M \text{ is 0 minimum to 1 maximum}) \]

then this signal can be used to modulate a carrier signal.

If these two signals are mixed (multiplied together) in a modulator circuit that produces an output proportional to the mathematical product of the input signals, the resultant output is an amplitude-modulated signal. We will assume this circuit has a gain of unity for simplicity. Then, multiplying the two signals we get an output signal as follows:

\[ V_c(t) \times V_m(t) = A \sin \omega_c T + AM (\sin \omega_c T)(\sin \omega_m T) = \text{resultant signal} \]

A trigonometric identity from your high school trigonometry book says that the product of two sines of two angles is as follows:

\[ \sin X \sin Y = \frac{1}{2} \cos (X-Y) + \frac{1}{2} \cos (X+Y) \]

For simplicity, assume \( A = M = 1. \) (This will result in a 1-volt carrier with a 1-volt peak modulating signal.) Substituting, in the trigonometric identity, \( X = \omega_c \text{ and } Y = \omega_m, A = B = 1 \)

\[ V_c(t) \times V_m(t) = \sin \omega_c T + \frac{1}{2} \cos (\omega_c - \omega_m) T + \frac{1}{2} \cos (\omega_c + \omega_m) T \]

Now, we have three components in the resulting signal:

1) \( \sin \omega_c T, \) which is a unit level sinewave signal at the carrier frequency.

2) \( \frac{1}{2} \cos (\omega_c - \omega_m) T, \) which is a half-unit level cosinusoidal signal at a frequency equal to the difference between the carrier frequency and the modulating signal frequency. This is called the lower sideband.

3) \( \frac{1}{2} \cos (\omega_c + \omega_m) T, \) which is a half-unit level cosinusoidal signal at a frequency equal to the sum of the carrier frequency and the modulating signal frequency. This is called the upper sideband.

The three signals produced are the carrier, the lower sideband, and the upper sideband. A cosinusoidal waveform is just a sine waveform shifted in phase by 90 degrees, so at \( T = 0 \) it is maximum, falling to zero at \( \omega T = 90 \) degrees.

(Continued on page 36)
As you probably know, recent events have made us all more security conscious. It is now common to require those entering public and governmental buildings, boarding airplanes or cruise ships, and even attending high-profile sporting and entertainment events, to submit to some kind of security check. People have to pass through a metal detector on entry; and briefcases, baggage, and packages are generally inspected, and often X-rayed.

Frequently, frisking occurs if any metal is detected, and any one may be subject to random frisking. To eliminate actual hand contact, a device that looks like a wand or small baton is commonly used. This device is a small metal-detector system for locating hidden forbidden items, such as knives, guns, or anything that could be used as a weapon.

Sniff out metallic contraband with this hand-held device.
PARTS LIST FOR THE FRISKER

SEMICONDUCTORS
IC1—CD4060BE, 14-stage ripple-carry binary counter/divider and oscillator
IC2—LM386N
Q1—MPF102, JFET, N-Channel
Q2—2N3904, NPN-Si, AF/RF amp, driver
D1—1N914, silicon switching diode
D2—MV209, rectifier

RESISTORS
(All resistors are 1/4-watt, 5% units.)
R1—220,000-ohm
R2, R12, R15—10,000-ohm
R3, R6, R7—33,000-ohm
R4—470-ohm
R5, R14—100-ohm
R8—100,000-ohm
R9, R10—4700-ohm
R11—2200-megohm
R13—2200-ohm
R16—1000-ohm
R17—10-ohm
R18, R19—100,000-ohm potentiometer

CAPACITORS
C1—22-pF, NPO, ±5%
C2, C13, C15, C16—.01-µF, ceramic-disc, GMV
C3—100-pF, NPO, ±5%
C4—47-, 82- or 120-pF, NPO, ±5%
C5—3-40-pF, trimmer

C6, C17—.22-µF, 35-volt, tantalum
C7, C11—.47-µF, 35-volt, tantalum
C8—470-pF, ceramic-disc, ±20%
C9—47-pF, NPO, ±5%
C10—33-pF, NPO, ±5%
C12—.001-µF, Mylar
C14, C18—100-pF, 16-volt, electrolytic

COILS AND CHOKEs
L1—Sensing coil, 375 T, center-tapped
X1—Crystal, 4-MHz, ±.01%, 20-pF, parallel-cut

ADDITIONAL PARTS AND MATERIALS
SPDT toggle switch, two shafts for pots, piezo speaker (Z > 16-ohm), 9-volt battery, battery connector, PVC or ABS box, 3/4-inch x 9-inch tubing (PVC, Sch 40), 3/4-inch PVC pipe cap, PVC cement, PC board, hardware as required

A kit of parts is available from North Country Radio, PO Box 53, Wykagyl Station, New Rochelle, NY, 10804-0053, and can be ordered on their Web site: www.northcountryradio.com. E-mail sales and order information: rgraf30832@aol.com. E-mail tech support: support@northcountryradio.com. Kit price is $49.75 plus $5.50 for p/h. NY residents please add $4.10 NY sales tax. The kit includes a drilled, etched, and screened PC board; all the parts that mount on it; switch; a suitable plastic case; speaker; plastic pipe; pipe cap; and complete, detailed documentation. Cement, tape, miscellaneous hardware, and 9-volt battery are not included and are easily obtained at your local hardware supplier or home center.
This article describes the theory, operation, and construction of the Frisker, a small metal detector similar to those described above—used by security personnel to find concealed metallic objects while avoiding physical contact with the subject. The Frisker will find such concealed weapons or any improvised weapons made of metal without requiring the subject to remove them from his or her pocket.

How It Works. Unlike X-ray systems, there is no hazardous radiation that could cause personal injury or could damage incidental items, such as photographic materials and some medicines. The device consists of a probe about nine inches long and one inch in diameter, with a small enclosure at one end for battery and speaker. This enclosure also serves as the handle. The metal detector’s electronics and sensing coil are contained within the probe.

In actual use, the unit is turned on and a tone emanates from the built-in speaker. (See Fig. 1.) The end of the probe is run across suspected areas that may contain metal. A change in speaker volume or tone frequency indicates the presence of metal in that area. A common 9-volt transistor-radio battery powers the Frisker.

Theory Of Operation. When a metallic object is brought near a coil of wire, the inductance of that coil will change. A non-ferrous metallic object will act as a shorted turn and cause the coil inductance to decrease. Ferrous metals will also cause an inductance change, which may be an increase in inductance due to permeability effects, combined with the same shorted turn effect.

Ordinary steel or iron objects larger than the sensing coil will produce more of a shorted turn effect, while ferrites or smaller iron objects may cause an inductance increase. If this coil is part of a frequency-determining circuit such as the inductance in an L-C oscillator, this increase will cause a small frequency shift. Translating this shift into an audio tone makes it audible to a human ear, if the tone is used to drive a small speaker.

The detector-oscillator frequency is mixed with a fixed-reference frequency derived from a crystal oscillator. A mixer circuit produces an audio signal equal in frequency to the difference in frequency of the detector oscillator and the reference. Since small differences in audio frequency tones are noticeable, a frequency shift of 50 Hz or less in the detector oscillator can be readily heard.

Construction. Refer to the block diagram (Fig. 2) and the schematic of the Frisker (Fig. 3) for the following discussion. A foil pattern for the Frisker is provided in Fig. 7. An oscillator circuit—consisting of the JFET, Q1, and associated components—contains a sensing coil, L1, which is mounted at the end of the probe assembly shown in Fig. 1. Capacitors C3, C4, and C5—along with Varactor diode D2, bypass capacitor C2, and L1—make up a resonant circuit tuned to approximately 125 kHz. The frequency can be adjusted to this value via trimmer C5 and the bias voltage on D2, and set with pot R19 and isolation resistor R2. The coil, L1, is tapped, and the tap is connected to the source of Q1.

The junction of L1 and tuning capacitors C3, C4, and C5 is connected to the gate of the JFET via C1 and bias network R1 and D1. Capacitor C6 bypasses the drain of Q1 to ground, and DC is fed through R4 from the Vcc supply, which may be +5 to +9 volts. Any metallic object near L1 will affect the frequency of oscillation. The reference frequency is generated by IC1 and associated components.

Much of the circuitry needed is contained within this
chip. Crystal X1 is a 4-MHz crystal and operates in fundamental mode. Components R13, C9, C10, and bias resistor R11 make up the crystal circuit. The oscillator active components are inside the chip. The signal at 4 MHz is divided by 32 internally in the chip, and a 125-kHz square wave appears at pin 5 of this chip. Resistors R10 and R5 feed some of this reference signal to the emitter of mixer transistor Q2. The decoupling components, R14 and C13, provide DC power to IC1.

Mixer transistor Q2 is biased by R5, R6, R7, R8, and R9. Capacitor C7 prevents degenerative feedback and keeps the gain of Q2 high. The detector oscillator signal is coupled via isolation resistor R3 and capacitor C8 to the base of Q2. Mixing of the detector and reference oscillator signals takes place in the emitter-base junction of Q2. The mixing products (mainly the detector and reference oscillators, and their sum and difference frequencies) are amplified by Q2 and appear at the collector. Components R12, C11, and C12 form a DC-blocking and low-pass filter network and suppress the higher frequency components. All we want is the frequency difference product, which lies in the audio range. Resistor R18 is the volume control, and R15 and C15 further attenuate unwanted high-frequency components. Semiconductor IC2 together with peripheral components C17, R17, and C18 make up an audio amplifier stage that delivers up to a few hundred milliwatts of audio to a small speaker mounted off the PC board.

The Frisker is designed to only sense objects within an inch or so of the probe tip. Sensitivity is proportional to coil size; and a larger coil would detect objects at greater distance, but with somewhat decreased resolution. Also, proximity effects would be somewhat more evident (capacitive detuning of the oscillator). With a larger coil (4-8 inches diameter or 10-20 cm), the Frisker could be used as a conventional metal detector. The 2-cm coil used here is a reasonable
FIG. 5. CONSTRUCTION

FIG. 6. BATTERY BOX & WIRING
compromise between sensitivity and size.

The electronics are mounted in the probe assembly on a single-sided PC board, 0.7 × 5.5 inches. (See Fig. 4 for the PC board parts layout and component and lead locations.) This board is designed to fit inside a standard ⅜-inch (19-mm ID) schedule 40 PVC plastic pipe. A length of 9 inches (23 cm) was used, but this is not critical. This material is very inexpensive and readily available at home improvement centers and in the plumbing sections of hardware stores. Often, small lengths are available at these stores, as an alternative to the standard ten-foot lengths that are sold by plumbing suppliers.

A PVC-pipe cap secures the probe to a small plastic box (2 × 4 × 1.5 inches, or 5 × 10 × 4 cm) that houses the 9-volt battery, on-off switch, and a small piezo speaker. The PVC cap is cemented to the plastic box (made of ABS or PVC plastic) using standard plastic pipe cement, and a hole is drilled for passing the four leads from the PC board into the box. CAUTION: PVC cement is toxic, volatile, and very flammable. Do the cementing outdoors far away from any flame or lit cigarettes. Be very quick and use only enough cement to coat the surfaces—no more, as it sets very rapidly. Although this cement will appear dry in a few minutes, set the parts aside for at least two hours to ensure that the bond is strong enough to withstand handling.

The sensing (detector) coil is mounted to the other end of the plastic pipe using PVC electrician’s tape. It consists of 375 turns of #36 wire, center-tapped, on a ⅜-inch plastic bobbin. It is scambled wound. A ready-made coil is included in the Parts Kit available from the source listed in the Parts List. The coil fits on the end of ¼-inch pipe, and the tape may be coated with PVC cement to form a permanent bond. This is unnecessary as it prevents easy access to the PC board inside the pipe. The board is held in place by the two shafts for the frequency adjust and volume pots and cannot move once the shafts are installed. Three holes of .187 inches (about 7 mm) are drilled into the probe housing for the two pot shafts to protrude and for access to trimmer capacitor C5. See Figs. 5 and 6 for details of construction. Packaging is not critical and you may wish to make some modifications to fit the parts you have available.

**A Simple Tune-Up.** After checking the assembly of the PC board for errors, connect a speaker of 16-ohm impedance, or higher, to the speaker leads. Connect the sensor coil to the PC board leaving the coil leads loosely twisted together and about 3 inches long. Connect a 5- to 9-volt supply to the power leads. Be careful to observe polarity, as reversed battery polarity could damage C14 and IC2, and possibly IC1.

You should hear an audio tone of some sort from the speaker. Set C5 with the plates half meshed (mid-way between full and minimum capacity.) Adjust the volume control, R18, for comfortable volume and R19 for a tone frequency around 1–2 kHz (a whistle, not critical). Now adjust C5 so the pitch gets lower, ideally to zero. At this point, the tone will disappear as a low growl. Continuing to rotate C5 in the same direction will cause the pitch to rise again. The point at which the pitch is lowest and disappears is called “zero beat.” You may have to select different values for C4 if you cannot get this whistle.

If rotating R19 fully clockwise decreases the pitch, the oscillator is too low in frequency. In this case, use an 82-pF capacitor in place of the 120-pF capacitor, C4. If the pitch is now better but not quite enough, try the 47-pF capacitor. Similarly, if turning R19 to the left decreases the pitch but not enough to get very low-pitched tones, add a 47-pF capacitor across the existing C4, or even 82-pF in some cases. The tuning range of C5 is small (about 2–3 kHz); therefore, it is normal to have to change C4 if C5 cannot compensate for tolerances. The optimum value of C4 is that which results in zero beat with both R19 and C5 set near the center of their adjustment range.

Alternatively, if you have a frequency counter you can connect it to the source of Q1 through a 15- to 33-K resistor and then adjust C5 for 125 kHz with R19 centered. The sensing coil should be away from any metal when this adjustment is made. Bringing metal (coin, keys, a knife, etc.) near the sensing coil should cause a noticeable change in pitch. If no audible whistle is obtained at all with any value of C5, there is something wrong.

Check your assembly and the circuit board for shorts and open joints. Look for misplaced/oriented components. There is little to go wrong if the assembly is correctly done. After you are sure all is operating correctly, disconnect the power supply. Solder four 6- to 8-inch leads to the PC board for power and speaker connections. Slide the board into the PVC pipe (see Fig. 5) and position it inside the plastic pipe so that the centers of the pots R18 and R19 are visible through the two closely spaced holes at one end.

The third hole should be directly over C5 to allow future access to the trimmer capacitor for any final adjustments. Insert the two pot shafts into R18 and R19; this will lock the board in place. Fasten the sensing coil, L1, to the end of the tube. The wires can be twisted together. Be sure they do not block the hole for C5 access. The leads connected to the control end of the PC board are brought out the other end. A small notch cut or filed into the coil end of the tube provides

(Continued on page 29)
Build This Theremin, Part II

Last month, we described the circuitry behind Theremax. This month, we will show you how to build it.

Although all of the signals in Theremax have frequencies below 1 MHz, it’s important to build the unit carefully. Keep the point-to-point wiring as short as possible, and leave plenty of space between the four oscillators to minimize oscillator lock.

Construction. The easiest way to build the electronics of Theremax is either to make or buy the printed-circuit board presented last month. The component-placement diagram for the board is shown in Fig. 3. If you construct the circuit or just parts of it on perforated prototyping board, try to follow this layout as closely as possible since care has been taken to isolate parts of the circuit that might interact. Note in particular the use of a star ground point with traces emanating from circuit board point “G,” and the grounded lands that encircle each oscillator. Make sure the metal cans of the inductors are grounded as well.

For the most part, Theremax is very forgiving of the specifics of components. For example, almost any NPN silicon transistor will work in place of the 2N4124 specified—2N3904s or 2N2222s will be fine. Even the inductor values are not very critical; and you will find that most suppliers carry IF transformers and local-oscillator coils that can be made to work in the circuit, probably without even changing the operating points of the transistors. Make sure the “cans” you use have a tapped primary (you may have to reverse the ends of the primary to get the tap closer to the collector end) and a secondary (polarity doesn’t matter here).

Do not substitute silicon diodes for the germanium types used in the ring modulators. The forward voltage drop of silicon diodes makes them inappropriate here.

The other critical components are the ceramic-disc capacitors used in the tank circuits. These must be NPO types to minimize oscillator drift with changes in ambient temperature.

Connect the front-panel controls and jacks to the lettered pads on the circuit board with No. 22 AWG stranded wire, as shown in Fig. 4. Note that you must mount some of the fixed resistors between solder lugs on the panel controls, as shown. Mount the LEDs by twisting their cathode leads to their current-limiting resistors and soldering. Mount the front panel to the lectern case from the inside; the controls are exposed though a hole that’s routed-out in the front of the case. The shapes of the case pieces have been kept as simple as possible. (See Fig. 5.) Assemble the case with simple butt joints, countersunk screws, and glue. (See Fig. 6.) The case for the prototype was cut from clear white pine and finished with walnut-tinted tung oil. If you start from scratch, you may choose other materials and configurations. If you decide on a metal case, make sure that the antennas are insulated from it.

Form the antennas from No. 6 AWG copper buss bar—the kind that power companies use for ground connections. This material was chosen for its malleability and ease of fabrication. Reformable antennas can be easily shaped for experimental purposes. For example, zigzag pitch antennas might give a different
means of obtaining vibrato—you could hold the pitch hand vertical while running it up and down, rather than waving it closer to the antenna. You can form the volume antenna from a length of the buss rod and bend it in any appealing, roughly loopish pattern. While the specific shapes that you choose for the antennas are pretty much up to you, be sure to keep them at right angles to one another to minimize interactions between them.

Mount the antennas to the case by passing them through 3/8-inch holes drilled in the end panels. Secure them to the back of the case with large washers, wing nuts, and No. 8 flat-head screws that pass through loops bent at the end of the buss rod, as shown in Fig. 7. Make the connection to the antennas with RG-174/U coaxial cable. Ground the shield only on the circuit-board end.

Make the bottom of the case from metal to form a ground plane that cuts down on any interactions between the pitch and volume sections. Mount the circuit board to the bottom plate with standoffs and 4-40 hardware. (See Fig. 8.)

Testing and Tuning. After examining your work carefully—looking for solder bridges, incorrectly placed or oriented parts and so on—it’s time to power up. Plug the power adapter into a wall outlet and turn on the power switch, S1. You should immediately see the power LED light. If you don’t, stop. Re-examine your work, and find out why.

Begin testing and initial tuning by setting the front-panel controls so that the pitch trim and vol trim controls are at about the midpoint of their range. Set the pitch cv, timbre, and velocity controls fully counterclockwise; and rotate the volume control clockwise to its maximum setting. Connect the audio output of Theremax to the input of a hi-fi, instrument, or general-purpose amplifier.

Verify the operation of the oscillators and set the heterodyning pairs to the same frequency. With an oscilloscope, look at the voltage of the emitters of the oscillator transistors (Q1 to Q4) and observe the 500-kHz to 900-kHz sine waves with amplitudes of about 250 millivolts peak-to-peak and DC offsets from ground at about a volt. As the slugs of heterodyning pairs of oscillators are adjusted, the beat frequencies—0 to 10 kHz, 0.5 volts peak-to-peak sine waves—can be seen at the collectors of the amplifier transistors, Q8 or Q9. They’ll have a typical DC offset of 5 to 6 volts above ground. First, turn the slugs of L2 and L3 clockwise until you feel resistance (don’t try “tighten” them), and then back them out about a half turn. Now, adjust L1 while watching Q8’s collector. At some point in the rotation of the slug, you will see a sine wave that builds in amplitude while decreasing in frequency; and then goes to zero before once again increasing in pitch.
THE FRISKER
(continued from page 26)

clearance for the leads of L1, as well as for flush mounting of L1 to the tube end.

The small plastic box has a battery and speaker mounted inside it, with an on-off switch (see Fig. 6). A PVC ½-inch pipe cap was cemented to the top of the box as described earlier. The tube assembly is then inserted into the pipe cap. DO NOT CEMENT THIS TOGETHER. You will permanently seal the assembly, making access to the PC board difficult or impossible without cutting the plastic. Friction fit is sufficient, or you can drill a small hole and use a small (#4 x ½-inch) self-tapping or sheet metal screw if you prefer.

Using The Frisiker. The Frisiker works by placing the sensing coil against the subject and moving it around, while listening for a change in audio pitch. A slight steady change in tone caused by body capacitance may occur, but metal will cause a much larger change. Coins, keys, and other metallic objects can be readily detected.

Surgical implants will not usually cause an indication if deep inside the subject. The Frisiker can also be used around the house to locate nails and screws in trim, moldings, and walls. This feature will also prove handy when doing certain household chores, such as mounting pictures, shelves, and other objects on the walls.

Fig. 4. Off-board wiring for Theremax. Some fixed resistors and LEDs mount directly to the front-panel controls and jacks.

The zero (null) point is your target. Do the same thing with L4 while watching for zero beat at the collector of Q9.

If you don't have an oscilloscope, a pocket AM radio can be pressed into service to verify that the oscillators are working and set to appropriate frequencies. Start by setting the radio to some quiet point between 650 and 750 kHz, and placing it as close as possible to the modulator diodes, D2 to D5. Set the radio to a fairly high volume and adjust the tuning slug of L2 up and down. At some point, you should hear a click or chirp as the frequency of the oscillator passes through the frequency set on the radio dial. Tune the slug very slowly back toward where you heard the chirp, and you will hear "whines"—faint whistles, feedthrough from adjacent stations and so on—as you get closer to the setting of the radio. As you turn further, you should reach a null where the previous "whines" are replaced by the hiss of white noise (there's no modulation so the only audible signal for the radio to detect is the noise of the transistors in the oscillators, which is fairly faint). When you have turned too far, you will begin to hear the same "whines" that you heard approaching the null. Leave

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the slug set as close to the null as possible; it doesn't have to be exact.

Now adjust the slug of L1. At some point you will hear a loud chirp as the oscillator you are adjusting passes through the common frequencies of the local oscillator and the radio. Slowly adjust back to the chirp and you should hear a very loud, pure tone descending in pitch as you approach the null. Leave the slug set as close to null as possible and verify that the front-panel pitch trim control can be used to set an exact null. Leave the control set so that a low-pitch tone can be heard.

To adjust the volume oscillator pair, set the radio dial to a quiet spot between 900 and 1000 kHz and adjust L3 in the same way that you previously adjusted L2. When

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**TIPS FOR MAIL ORDER PURCHASE**

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Be sure to include copies of all correspondence.
L3 has been set close to the frequency of the radio, adjust L4 for zero beat of the heterodyne signal as you did with L1. Verify that the VOL TRIM potentiometer provides a vernier control of the frequency.

At this point, you should be able to start listening to Theremax through an amplifier connected to the audio output. With the volume control of the amplifier advanced slightly, bring your right hand up to the volume antenna—you should hear a tone swell in the amplifier's speaker. If you don't hear a tone, check to make sure that there is still some audible signal being produced by the pitch oscillators. If that's not the problem, check the rest of the audio signal and control path. Read the volume-control-
voltage at the emitter of Q6 to make sure that it goes from about 0 to 6 volts as your hand approaches the volume antenna. If that’s OK, check the differential pair, Q10 and Q11, and its control current source Q12. Finally, check the output stage, IC2. If there’s no volume CV, check the amp. Q9, as described earlier; and check the output of the Schmitt trigger, IC1-b, at pin 1, where there should be a rail-to-rail square wave at the heterodyne frequency of the volume pair. If this signal is present, make sure the components of the differentiator/integrator (R25, C25, C31, D12, and D13) are in proper order.

With a tone audible, rotate the TIMBRE CONTROL clockwise and observe that the tone gets considerably more “sharp-edged” as you fade from sine-wave to square-wave output. Turn the TIMBRE CONTROL fully counterclockwise. Advance the VELOCITY CONTROL fully clockwise and observe that as your hand rapidly approaches the volume antenna, the gate/trig LED comes on. Also notice that the character of the sound now changes as your hand approaches the volume antenna—getting “fuller” when your hand approaches rapidly; and settling to a purer tone when you slow down, stop, or withdraw.

Playing Theremax. Playing the theremin is an art that can’t be taught in a few paragraphs. Still, much can be learned by observing the playing style of Clara Rockmore. Clara’s background was as a concert violinist, but a palsy in her hands that developed at a young age appeared to have put an end to her career as a performing musician until she started playing the theremin. (See the Sidebar in Part I.)

In many pictures of Clara taken over more than a thirty-year span she is seen in front of a huge free-standing loudspeaker. This pose was not just for the theatrical effect of the apparent glory behind her head, though in some of the photos this aspect is quite striking. She positioned the speaker directly behind her so that she could hear the note she was getting ready to play before it was loud enough for the audience to hear, performing pitch corrections in that last split second.

Reviews and other accounts of performances remark on her motionless, trance-like stance while playing; only her hands dancing back and forth over the antennas. That theatrical presence was rooted in necessity: A theremin doesn’t respond to the motion of your hands only; it responds to body motion as well. If you’re moving around while playing, you will find it more difficult to hit an exact pitch.

Clara had developed “aerial finger” techniques that allowed her to play rapid passages with legato and even staccato articulation. Some years back when Bob Moog—the father of Moog synthesizers and manufacturer of theremins—was preparing an...
PARTS LIST FOR THE THEREMAX

SEMICONDUCTORS
IC1—LM339 quad comparator
IC2—748 op-amp
Q1—Q12—2N4124 NPN transistor
D1—8.2-volts, 400-milliwatts, Zener diode
D2—D9—1N34A germanium diode
D10—D14—I N914 silicon diode
D15, D16—Light-emitting diode, red

RESISTORS
(All resistors are 1/4-watt, 5%, unless otherwise noted.)
R1—100-ohms
R2, R19—3300-ohms
R3, R8, R13, R17, R69—680-ohms
R4, R9, R14, R18, R48, R49, R61, R65, R66—56,000-ohms
R5, R6, R20, R21—47-ohms
R7, R12, R53—3900-ohms
R10, R15, R22, R23, R56—1000-ohms
R11, R16, R41, R50, R70—10,000-ohms
R24, R25, R54, R57—1-megohm
R26, R45, R59—4700-ohms
R27, R29, R60—470,000-ohms
R28, R67, R68—470-ohms
R30, R33, R34, R36, R37, R38—47,000-ohms
R31, R62—39,000-ohms
R32, R63—330-ohms
R35, R46—10-megohms
R39, R40, R55, R58, R64—22,000-ohms
R42—220,000-ohms
R43, R77, R78—2200-ohms
R44—4.7-megohms
R47—68,000-ohms
R51, R52—15,000-ohms
R71, R72, R73, R74—100,000-ohms
R75, R76—1500-ohms
R79, R80—1000-ohms, panel-mount potentiometer
R81, R82, R83, R84—10,000-ohms, panel-mount potentiometer
R85, R86—270-ohms

CAPACITORS
C1, C20—100-µF, 10-volts, electrolytic
C2, C4, C8, C12, C16, C33, C34—0.01-µF, ceramic disc
C3—1000-µF, 10-volts, electrolytic
C5, C9, C13, C17, C39—100-pF, ceramic-disc
C6, C10—100-pF, NPO, ceramic-disc
C7, C11, C15, C19, C28, C31—470-pF, ceramic-disc
C14, C18—68-pF, NPO, ceramic-disc
C21, C26, C32—10-µF, 10-volts, electrolytic
C22, C27, C34, C37—220-pF, ceramic-disc
C23, C35, C36, C38—1-µF 10-volts, electrolytic
C24, C25, C30—0.1-pF, Mylar
C29—4.7-µF, 10-volts, electrolytic
C40—0.001-µF, ceramic-disc

ADDITIONAL PARTS AND MATERIALS
J1, J3, J4, J5, J6—1/4-inch phone jack
J2—1/4-inch stereo phone jack
S1—SPST switch
P1—DC wall-mount adapter, 9-volts, 100-mA
L1, L2, L3, L4—796-kHz (nom.) oscillator coil
Knobs, circuit board, wire, solder, hardware, case, etc.

Note: The following items are available from PAIA Electronics, Inc., 3200 Teakwood Ln., Edmond, OK 73013; 405-340-6300; www.paia.com/paia.
Complete kit of all electronic parts including power supply, circuit board and knobs less antenna and case (#9505K): $88.75 plus $7 shipping.
Case kit with pieces cut from white pine and drilled for assembly, includes hardware, formed antenna: bottom plate and punched, anodized, and legended control panel (#9505C): $77.25 plus S12 shipping. Partial Case Kit*: Front panel, antenna and antenna mounting hardware only (#9505PA): $28.50 plus S7 shipping.
Please NOTE: The mounting hardware is not appropriate for metal cases.

Instrument for use in what was to be her last concert, he was quoted as remarking that he had to "hang it on the edge" to please Mrs. Rockmore. In the interest of ease of playing, Theremax is designed to be somewhat less sensitive. However, substituting smaller capacitors in the tank of the oscillators will take its sensitivity up to this concert-level performance. If you make these changes, be warned that you'll also need concert-level skills to handle them.

For maximum sensitivity to hand gestures, the PITCH TRIM control should be clockwise from null so that the heterodyne frequency is two octaves below middle C (64 Hz or so). When tuned this way, the maximum range of about six octaves will correspond to an 18-24-inch range of hand motion. Only the rare performer will be able to use more than three or four octaves, because the last couple requires that the hand be very close to the antenna.

Volume on the original theremins was increased by moving the hand away from the antenna. If you want to play Theremax this way, you should null the VOLUME TRIM control for minimum volume with your hand an inch or so from the antenna. Playing may seem more intuitive if you reverse this, so that volume increases as you move closer. To accomplish that, just null the VOLUME TRIM with your hand removed. Either way, volume must be nulled completely for the velocity feature to work properly.

Closing the contacts of a SPST switch plugged into the MUTE jack turns the audio output off completely. You may find that a foot switch—either momentary or push-on, push-off—makes playing easier. This switch closure could also be an open collector transistor output from other equipment, such as the "S" triggers used in some synthesizers. Muting the audio has no effect on the control-voltage outputs.

Many contemporary electronic musical instruments have provisions for external control of key parameters by means of control voltages, foot pedals, and so on. In many cases, Theremax's control voltages can be connected directly to these inputs. The availability of both gate and open-collector switching outputs on the GATE/TRIG output, J2, makes switch-style interfacing easy. In some cases, instruments expect a variable resistance at their external control jacks. In these cases, Theremax's control voltages can be converted to a resistance using an optocoupler, as shown in Fig. 9.

In some circles, voltage-controlled analog music synthesizers, antiques that they are, have great cachet. Theremax makes a useful supplemental controller to the keyboards typically used in these instruments. Figure 10 shows only...
one of an unlimited number of possible "patches." The PITCH CV output sets the frequency of the synthesizer's voltage-controlled oscillators (VCOs), so that the right hand still controls pitch. VCOs will typically provide a greater selection of waveforms than just sine or square, and multiple oscillators will produce a fuller sound.

The VOLUME CV isn't used to control volume; instead it's routed to the control-voltage input of the filter, so that the left hand now con-

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Fig. 8. The case bottom and the front panel should be made of metal.

Fig. 9. An optoisolator can convert Theremax's control voltage to a resistance.
Voltage-controlled synthesizers can be controlled by Theremax. Trots timbre instead.

So if volume is really timbre, how do you control volume? This is the cool part. As with most synthesizer patches, the dynamics of the sound—how fast it builds up and dies away—is controlled by an envelope generator, which here is triggered by Theremax's gate output. The volume hand does still control volume, sort of, but now moving the hand quickly toward the antenna will trigger a sound with dynamics set by the envelope generator. Remember that the place where the hand ends the triggering move sets the timbre (VCF). You've got air drums! Theremax's gate output and control voltages don't just respond to the gestures of a performer; they're actually general-purpose people sensors and could be used to turn on or brighten lighting instruments arranged to accentuate different parts of a sculpture on the approach of an observer. They could also produce kinetic art that responds to how quickly it's approached and how close a person stands. Music is just the beginning—there are a lot of possibilities. Have fun playing with Theremax.

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degrees. A sinewave starts at zero at \( T=0 \) and has a maximum at 90 degrees. Note that the two sidebands are one half that of the carrier in amplitude and are different in frequency from the carrier by the modulating frequency.

There is also a 90-degree phase shift. The ratio of the modulating signal to its peak value at full modulation is called the modulation index and is denoted by the letter \( M \). \( M \) has a value between zero (no modulation) and 1 (maximum modulation). If \( M \) exceeds 1, this is called overmodulation and results in distortion.

The important thing to see is that the total signal bandwidth needed to pass these three components is twice the modulation frequency. It does not depend on the value of \( M \). Therefore, for a standard AM broadcast signal with a maximum modulating frequency of 5 kHz, a 10-kHz bandwidth is required in the receiver. Also note, since the carrier term is simply a constant amplitude sine wave, it carries no intelligence and its amplitude is constant. Now, comes the big kicker!

Sidebands

Note that the amplitude of each sideband is only half of that of the carrier, even when \( M = 1 \). Therefore, the power in each sideband when \( M = 1 \) is only one quarter that of the carrier. Since there are two sidebands, there is a total sideband energy of only half that of the carrier. Since these sidebands are identical, differing only in frequency by twice the modulating frequency, they both carry the same information and are redundant from an information viewpoint. The sidebands contain only one third the total signal power generated by the transmitter, but they carry all the information. Really, only one is needed, the other being redundant.

The modulating system must supply this sideband energy, half the power of the carrier signal if \( M = 1 \). The modulating power needed is equal to one half \( M \) squared. A 1000-watt AM carrier, for example, needs 500 watts of audio to fully modulate it. Well, then why not generate the AM signal at low level and amplify it? Not very efficient. Since the total peak amplitude of the signal is twice that of the carrier, a peak power of 4000 watts is present in a 1000-watt AM signal. Therefore, a power amplifier used for AM must be capable of delivering four times the carrier power on modulation peaks. The 4000-watt amplifier is delivering only a 1000-watt carrier and seldom operates at full power except on modulation peaks.

The overall efficiency is then low. Just as in real life, you do not get something for nothing. The alternative to a 500-watt modulator and a 1000-watt RF amplifier in this case is a low-level audio amplifier and a 4000-watt RF amplifier running inefficiently. Not that this is so bad, because at high-power levels it has the advantage of eliminating the expensive and heavy 500-watt modulation transformer needed to couple the audio energy to the transmitter-power amplifier. No matter how you look at it or do it, AM is a rip-off from an efficiency standpoint. However, it is simple to do, has fairly good audio fidelity, and still has better weak-signal performance over certain other modulation methods. It is easily received with a simple low-cost receiver and is not critical as to receiver mistuning. AM is still used worldwide for short-, medium-, and long-wave broadcasting, and for air-to-ground VHF voice communications.

It was realized in the early days of radio that since only one of the sidebands is needed, why bother to transmit the carrier and the other sideband? The carrier doesn’t “carry” anything, as both the sidebands are RF and can be radiated by an antenna. Getting rid of the carrier and one sideband gets rid of five sixths of the radiated power with no loss of information. So the transmitter power can be effectively increased by a factor of six, since all the energy can be placed in the transmitted sideband.

Furthermore, the receiver bandwidth can be reduced by a factor of two. This gives a total of 8-dB transmitter gain and 3-dB receiver sensitivity, or 11-dB improvement in signal-to-noise ratio. The likelihood of interference to or from other signals is also reduced by using half the bandwidth; and channel capacity of a frequency band can be doubled, since each signal needs only half the bandwidth of an AM signal. This modified form of AM modulation is called single-sideband, or SSB. We will discuss this subject in the next part of this article. Tune in next month.

NORTH COUNTRY RADIO: A HAVEN FOR WIRELESS BUFFS

Graf and Sheets are no strangers to the pages of Gemsback. Their educational projects, such as the RF-Field Strength Meter and the MPX2000 FM Transmitter, can be found at North Country Radio. Established in 1986, this company offers projects related to amateur TV transmitters/receivers, AM and FM transmitters/ receivers, video cameras, and numerous other subjects. Visit the Web site at www.northcountryradio.com for more information.

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Q & A

mailto: q&a@gernsback.com

Smart Outlet Box

Reader Wil Higdon let me know that Sears (www.sears.com) sells the Craftsman Auto Switch, Sears number 00924031000, which duplicates the function of the Heathkit Smart Outlet Box as described in my August 2002 column. Wil writes, "It has one master (sense) outlet and two slave outlets and does exactly what C.W. asked. For example, switching on the table saw (master outlet) could turn on a work light and a shop vacuum (slave outlets). Mine is used for a different application, though. My TV is on the master outlet and a stereo amp is on one of the slave outlets. Turning on the TV automatically switches on the amp for better sound than the TV alone can provide. All this for $19.99. It would be hard to purchase the project parts for less than that."

Thanks, Wil. As their slogan and jingle went in the 70s, "Sears has everything." I agree that $19.99 is a better deal than trying to cobble something together from new parts. On the other hand, for those of us who already have a well-stocked junkbox, that may not be true. Then there are those of us who like to reinvent the wheel and will build something for three times what a pre-assembled model will cost, just so we can say, "I made that."

Regarding your application for your stereo, it indicates that there is obviously a low-end current drop-out below which the device will not trigger. Nearly every TV made consumes a small amount of power even when "off" to keep the IR remote electronics alive.

DBs Are Not Always DBs

I had a very interesting note from reader Gary Jarman concerning the "DB-25" connectors (see my August column) used for serial and parallel computer interface. He made several points, fleshing out what I had written in the column and added some other information that I'd like to share.

Remember that the RS-232 interface standard doesn't do much more than define a few lines and insure that if you plug two devices together, you won't get smoke. Gary reiterated the fact that RS-232 does not set a communication standard, which is often why two "RS-232" devices won't talk to each other. A device can be RS-232-compatible but use any coding scheme it wants, whether it's the teletype Baudot, Morse code, or ASCII. ASCII is the normal assumption.

He notes that, in general, DTE (data terminal equipment), such as computers, uses male pins on their serial connectors; while DCE (data communications equipment), such as external modems, uses female connectors. He went on to specify numbers, stating that the minimum number of lines required for serial communications is three. These are for transmitted data, received data, and ground; although most serial devices that use hardware handshaking use at least seven wires.

In his note, Gary was leading up to a section that really caught my interest. He writes, "The real reason for all this wordiness is a lead-in to one of my pet peeves. The D subminiature connector series was first used in 1952 in Korean-conflict-era military equipment. There are hundreds of variations and design functions still available. The series is used for almost anything that needs an economical, small connector with many pins. It is available with high-frequency coaxial inserts and for high current or high voltage, as well as for the common low-energy data signaling."

"My real point is that there is no such thing as a DB9 or DB15 connector in the OEM (original equipment manufacturer) catalogs. This is a product of misuse over many years of computer sales just as 'kodak' and 'frigidaire' have been in the past. The D comes from the D-shaped outer shell, which is a quick and easy polarization scheme. Although they are [physically] large by current standards, the design series is called a D-subminiature connector. The second letter, such as the 'B' in 'DB' is an identifier for the shell size. The number after the shell size is the number of pins within the connector. The last symbol of the part number is a P for 'pin' and S for 'socket'. The 9-pin size used commonly for serial ports should be called a DE-9P. The 15-pin size used for joysticks and midi connectors is a DA-15S. Obviously the 25-pin serial-chassis port is a DB-25P and the parallel port is a DB-25S. The mating parallel cable end is a DB-25P. There are also DC-37 and DD-50 connectors used in instrumentation."

"Please keep up the good work. The Q&A section is always informative and useful and is often the first thing I read in Poptronics."

Gary, the confusion of the "DB" as applied to all connectors was something new to me, and I've been messing with this stuff for nearly 40 years. I guess we all sometimes get stuck using terms like that erroneously, whether it's "DB-15," "Crescent" wrench, "Channellock" pliers, "Scotch" tape, "Xerox" copies or "Kleenex." Sometimes the holders of the tradenames don't like the generic use of their names, but it sure shows who's getting credit for the original idea whether they had it or not.

Bugs, Taps, and Other Nasties

Q An illegal extension has been placed on my telephone lines. I have plenty of evidence. Not only is the phone tapped, but my alarm system and computer are on the phone lines, allowing access to these items to be disrupted.

How do I find where the extension has been placed or what type of telephone device is being used? Is there a typical place to attach a device? Also, all of this is being controlled by a remote-control device or devices, which I found out can be done through one of your magazine articles. The phone company is useless. What do you suggest? Any help is appreciated at this point. I live in a single-family home, and I know who is behind this and why. I just can't get the evidence the police need. —M.V., via e-mail

A We can assume here that all paranoia is aside and that there are no black helicopters on regular flights over your home. First of all, call the alarm company and make sure that you aren't interpreting as unauthorized traffic any calls in or out that are being initiated by their

www.americanradiohistory.com
I checked with ADT and they rarely make calls in to a residential alarm and then only when the home is unoccupied. Usually, the resident initiates any downloads from his keypad as instructed by an ADT technician. Most alarm companies operate in a similar manner.

Second, you didn’t mention whether or not you had a satellite receiver system similar to DirecTV. Such a system might make occasional calls to the mother ship to upload pay-per-view billing and other such things with automatic use of the phone line that might be messing with your mind.

Also, if the bill is your indicator of fraudulent line use, check to see if there has been any calling card use. When we moved into our first home in 1978, our initial phone bills were in the $1500 to $2500 range. As it turned out, either whoever originally had that phone number still had a live phone card or a stolen phone card was being used—all kinds of international calls were being made and billed to us. Ma Bell took care of that in short order. It’s easy for a thief to gather your phone card information while watching or listening to you at a public phone.

All that was more or less for any readers with similar problems. Your follow-up letter does indeed indicate that it is likely that there is a tap on your line that is being used for malicious purposes, so let’s look at the possibility of a physical line tap. Since you’re located in a single-family residence, you should be able to physically trace out the lines. Outside the home, there are a couple of spots that are easy to tap to check. First is the telephone company’s pedestal where your line connects into the underground trunk lines. There are always two lines running into your home, even though only one may be in use. The second line is for, well, a second line or can be used as a back-up line in case the original line develops a defect. That way, the phone company doesn’t have to lay a new cable right away. So, your neighbor could tie your line over to their second line at the pedestal, and it wouldn’t be obvious unless you were deliberately looking for something like that.

Problem is, I think it’s just as illegal for you to open that pedestal as it is for someone to tap your line, so you might have to have some phone company help here, like it or not. I guess you could always call them up with a lie, “Hey, there’s this scrawny little guy in a purple jacket that has that gray (green, whatever) telephone box in the yard open and is messing with the stuff inside. It looks like he’s rewiring it or something.” Then get ready to meet the phone guy where he shows up … but make sure you’re not a scrappy little guy in a purple jacket, or you’ll have to change your original call a bit. At this time, you can indicate to the phone guy that maybe someone was trying to tie into someone else’s phone line to steal service so that he’ll think to look for line crossovers.

Another spot is where the line enters your house. These days, it usually goes underground from the pedestal and then goes into a little box where there’s a ground wire heading over to a ground stake or to the ground on the electric meter base. Otherwise, the box and ground could be inside the house where it connects to a cold water pipe. Most phone installations made since 1980 include a Subscriber Interface Box, where a short cable with an “RJ” connector plugs in so that you can isolate your home from the incoming line for troubleshooting purposes. Wherever the phone line enters your house, you should be able to physically trace every inch of it to insure that there are no taps or other unauthorized devices on the
line, checking each extension and break-out point where an extension attaches to the main line coming in. Every line should be clean or any wires and devices identified as being yours, all the way from the entrance into your home up to your end device—be it phone, modem, answering machine, or alarm system.

I have heard of instances where taps were illegally initiated by phone company personnel for purposes of stalking. If the person you suspect works for the phone company, your line can just as easily be in his house with all the connections being made electronically at a switcher. If such activity can be proven, that employee will be out of a job instantly and probably be up on criminal charges to which you could likely add civil charges.

I've always been irritated at the number of phone installations (mine is one) where the interface box is on the outside of the home. Any thief can walk up and plug a telephone into that jack and make all sorts of long-distance calls at your expense. If your "evidence" consists of a lot of unauthorized long-distance calls on your bill, this may be a hot spot. Most outside boxes have a little hasp affair that you can loop a small padlock through to make that access a little more difficult. Just make sure that if you call in a phone problem to take that lock off, if you're not going to be home "sometime between the hours of 8 a.m. and 8 p.m."

You indicated that you have been referred to the California Public Utilities Commission. That sounds like the prudent direction to take. I know that it seems like the "buck" is being passed with every agency you contact. It's likely that these agencies really don't know how to deal with such things and you just have to land on the right one accidentally. Maybe we have some readers with professional expertise on such things who can tell us whom to contact so that you can get some positive action.

Don't know make, model or year.—D.W., via e-mail

A D.W. also posted his question on the Gernsback Forum (www.gernsback.com) and friend Ron H. suggested that he try a search on the Google search engine. Google does seem to do well for us electronic types and that search does turn up the information that a substitute for the coil is a Borg-Warner E40. Another suggestion was to use a "cheap transistor ignition coil, i.e., mid to late 70s Dodge." The Google search engine is found at www.google.com.

Voltage-Divider Errors

Reader Bill Stiles is a frequent contributor to this column (in other words, he catches a lot of my errors) and agrees that those series resistors that have been discussed lately, if all identical, will have an overall tolerance that is no larger than the tolerance of an individual resistor.

However, he points out that you don't want to be swayed into thinking that the tolerance of the voltage output of a voltage divider using such resistors will be within that of the resistor tolerances. He cited a common example of a simple two-resistor divider typically used to increase the range of a digital panel meter (DPM) from 200mV to 200V, where you would use a 1000-to-1 divider.

More accurately, the resistor values would be exactly 99.9K ohms for R1, if R2 were established at 100 ohms as shown in Fig. 1. These values will produce an output of exactly 100mV when you have an input of 100V. I might add that the addition of a 10-megohm DPM across R2 has virtually no effect on this circuit, so I'll consider it to be negligible for purposes of error calculation. Bill notes that if the value of the large resistor increases by 1% and the value of the small resistor decreases by 1%, the final output voltage will be almost 2% lower in value, exactly 98.0217 millivolts when it should be 100 millivolts. He points out that this problem occurs when the divider ratio is high. Had both of the resistors been of the same value, the output voltage would have only been off by 1%. Circuits like this need to have resistors with tighter tolerances to complement the accuracy of the DPM. He also notes that Mouser Electronics (www.mouser.com) sells resistors with 0.1% tolerances for critical applications such as this.

Again, if you're going for a higher ratio yet so that the DPM can measure over 200 volts, you'll have to start watching the voltage ratings of the resistors, possibly using series-connected resistors as we discussed in previous columns. I might also note that if you're working with ultra-precision resistors, treat them like you used to treat the old point-contact germanium transistors and heat-sink the leads with pliers during the soldering operation so that you don't threaten the resistor's nominal value with high temperatures. Bill, thanks for that important item of information.

The Whiners Are Back

I love for readers to write to offer their slant on some of the items that we've been discussing. A few months ago, a reader was having trouble with "whine" getting into his automotive VCR/TV system and we discussed several sources for that problem. Reader Chuck Budack said that he had a similar problem between his stereo control "head" and his external amplifiers. He solved his by using an "Audio System Ground Loop Isolator" from RadioShack (catalog number 270-054). He describes the device as a pair of isolation transformers designed for audio frequencies that allows the audio to pass through but blocks any ground plane differential between the equipment. It works in place of the standard RCA phono patch cable. He says that this device may be a fast and inexpensive fix for the original problem. Chuck, thanks for the tip. I normally think of ground-loop problems as producing "hum" in

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**Ignition Coil For A Tesla Coil**

I am building the Tesla coil from the November 1999 Popular Electronics, but I'm unable to find the two ignition coils.

The type listed is a Wells LU800. I have looked online and have not been able to find any place that carries them. Is there a part number equal to it or a place where can I get one? Supposedly it is used in a Toyota, but I
Oscilloscope Construction

Q I appreciate your extensive answers to write-ins. I have a project about which I would like some information. A long time ago, your predecessors had a project on a small oscilloscope that used a 1-inch tube. 115 volts, and some old-time electronics, but it still fit in a small box. Is it possible that this can be updated to modern solid-state technology and run on 12 volts?—G.K., Navato, CA

A An oscilloscope construction project is a mighty intensive undertaking; and the only one that I can remember was in an early 70's issue of Electronics Illustrated, which was a Fawcett bi-monthly publication rather than one of our predecessors. That project was a really neat triggered sweep oscilloscope with a calibrated vertical attenuator and a calibrated timebase, and it had the 1-inch cathode ray tube (CRT) that was usually used for things like frequency-shift-keying converter displays. Except for the CRT, it was all solid-state but had no integrated circuits and was built on perfboard. That particular article was in two parts; and I'm missing one of those magazines, so I have the pictorial layout but not the actual schematic diagram. As you said, it was fairly small, about the size of a hardcover Tom Clancy novel, but not quite as thick.

Although the little CRT would deliver a crisp, well-defined display, most folks today don't want to deal with the high-voltage circuitry and extra power needed to support it in a low-voltage world. They would rather see a scope modeled around a liquid-crystal display. You have to hit the surplus markets pretty intensively to find that little CRT. At the price that high-quality, high-performance, used scopes can be found, the only reason to build one from scratch is simply for your own construction experience. You're sure not going to save much money doing it that way; and you'll never get decent performance from the little guy without investing a lot of time, engineering, and greenbacks.

In your letter, you had other projects in mind for the magazine to consider, and I've forwarded that note to our editors for their consideration. Most of our articles stem from an author's suggestion rather than from an editor's request, so it's pretty difficult to satisfy a reader's request for a specific type of construction project. However, if enough readers have an interest in the same type of project, the editors may contact an author within that discipline to see if they would be interested in developing something along those lines.

New Topics on the Forum

Q I had a question that I would have posted on the Poptronics forum, but I'm still trying to find out how to post a new question. My browser doesn't seem to give me the option.—S.E., via e-mail

A There are several forums associated with Poptronics. All forums are accessible at the www.poptronics.com site by clicking on “Forums” on the left-hand side. Navigation through the “new” forums is tremendously more difficult. However, they do have the capability of easily posting drawings, a feature that the old forums did not have unless you were heavy into HTML. The new forums make posting any .bmp or .jpg file as easy as a few mouse clicks.

One of the problems of the old electronics bench forum, which by the way is still the most popular, is that you have to wait for it to load the entire page before you come to the “post new topic” button at the very bottom. That isn't very convenient for most of us. That's why the first time most of us did this, we'd wait for that button, click on it, and save the resulting Web page in our Favorites. Then new postings were very fast. To avoid going through all of that, here's the URL of the “Post New Topic” page on the “old” Electronics Bench forum: www.gernsback.com/HyperNews/edit-response.pl/forums/ElectronicBench.html.

There have been some attempts to coerce the forum folks to place that “new post” button at the top of the page, but it may be that it's not being moved so that folks will want to use the “new” forum instead. I don't think it's working if that's the case.

Over-The-Horizon Model Planes

Q I have an R/C remote control B-2 bomber that has a range of half a mile. Is it possible to modify the controller with a tunable wireless FM transmitter to gain a farther range? Or is there another way to modify it? It's a three-channel, 72-MHz, fully proportional Pro-style transmitter.—W.R., via e-mail

A We've come a long way from the days when you used to get dizzy flying a model airplane, haven't we? With words like “half a mile,” I'm trying to imagine finding a dot in the sky that I'm trying to control from the ground. If you had full-bore telemetry and video feeds back to you, it would be more like using Flight Simulator rather than flying a model airplane. And you want that dot in the sky to disappear by sending it even farther away! I'm not convinced that's a good idea. Those R/C transmitters are limited in their power for good reasons. Disappearing dots are one reason. FCC regulations are another. A third reason is that the more power the transmitter has, the more chance there would be of interfering with other models on the same or adjacent channels.

I hate to rain on your parade, but folks on the ground would probably prefer that you keep your airplane in sight and under control. The FAA also may have some input if you have the capability and propensity to fly a drone high enough to violate legal airspace. I can imagine all sorts of awful things happening with a high-power transmitter if you managed to get the plane two miles out, have it run out of fuel, and drop like a rock through someone's windshield on the Interstate.

Writing to Q&A

As always, we welcome your questions. Please be sure to include:

1. plenty of background material,
2. your full name and address on the letter (not just the envelope),
3. and a complete diagram, if asking about a circuit; and
4. type your letter or write neatly.

Send questions to Q&A, Poptronics, 275-G Marcus Blvd., Hauppauge, NY 11788 or to q&a@gernsback.com, but do not expect an immediate reply in these pages (because of our backlog). We regret that we cannot give personal replies. Please no graphics files larger than 100K.

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DC Motor Management

Often my columns are inspired by real-life experiences. This time it was a young friend (you might notice I like working with budding hobbyists, both young and old), who was having a problem with his bot. The problem was controlling the speed of the drive motors that give the bot motion. His bot would either stagger like a drunk or go in circles.

Such is the dilemma of the permanent-magnet DC motor often used for propulsion in robotics. While the advent of the PWM (pulse-width modulated) controller has tamed the DC motor considerably, it lacks one thing—speed control. The bot will go slower over carpet, faster over smooth flooring, slower uphill, and faster downhill.

In order to maintain a constant speed, some kind of feedback is needed—something that tells the controller when to increase power when the going gets tough and to back off power when all the motor has to do is coast. The traditional way to monitor rotational speed is to attach an encoder wheel to the shaft and count the number of times the shaft goes round. Unfortunately, it’s not a practical solution for most robotics projects.

However, there is a trick that can be used to measure the speed of a DC brush motor that doesn’t require an external encoder or sensing resistor. It relies on the “noise” generated by the brushes.

Small motors usually have two brushes and three or five commutator segments. Consequently, there are six or ten places per rotation where a brush hits the space between commutator segments and produces a small electrical spike. While slightly less accurate than an encoder, this spike can be used to measure the RPM of the motor.

**PIC’n Up The Pace**

This column isn’t a project (although you can buy a kit of parts to play with the concept), so feel free to experiment with different drives and offset voltages. You’ll understand as we go along. Follow the bouncing code (and I do mean bouncing, because I took the liberty of tightening it up considerably to fit in the pages I have) in Listing 1.

The program determines the speed of the motor by counting the time between the pulses. The slower the motor spins, the more time it takes between commutator pulses, and the higher the number. To handle the counting, I used the inter-
rupt routine (the Interrupt Service Routine (ISR)= header in the code). Each time the motor generates a pulse, the PIC generates an interrupt that starts the TMRO counter.

Hang on, because we're only part way there. Generally, commutator motors are filthy—they generate more than one pulse per crossing (which is why they are heavily filtered for EMI). So what I did was to accumulate the period for ten pulses instead of one. In effect, I'm spreading out the error over a longer period of time, which makes it more accurate. This binary value is then output on Port B. The slower the speed, the larger the binary number.

Now comes the nifty part. Rather than use a DAC (digital-to-analog converter) chip, I decided to use weighted resistors for the digital conversion. The resistors are in increments of base-2, so that the highest current flows when the most significant bit is turned on. Let's say the output code is 00000010—this tells us that the RPM is high and the time between pulses is very low. In this state, only the 8.2-k resistor is conducting. As the motor speed slows down, this time will increase to something like 10000000, which kicks in the 1-k resistor that has eight times the current flow through Q1 (See Fig. 1). At full power, the binary output will read 11111110.

I know this code is a little more advanced than we've talked about in past columns, but I didn't find a reason for a module. However, it gives me a good excuse to introduce the interrupts and register coding, which are extremely annotated in the Listing. Therefore, I don't need to discuss it here; you can read it yourself in Listing 1. Let's get to the hardware.

**Time To Try**

As the permanent-magnet DC motor loses speed, it requires more current to keep it going. The code given here does just that. However, you need a place to start—an established RPM for a reference. I thought about this at length and came up with several solutions—but none that would work for all situations. So, I'm leaving that for you to figure out. However, I can make some recommendations (See Fig. 2).

Circuit (a) uses a high-power op-amp with an operating voltage of 16 to 60 volts and an output of 3 amps. You can replace the LM675 with a smaller op-amp and use it to drive a transistor that

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**LISTING 1**

PIC assembly code for a small DC motor controller

```assembly
#include <P16F628.inc>
#ifdef _INTRC_OSC_CLKOUT & _WDT_OFF & _PWRT_OFF

;==Date: 08/00/02

;==Description:
;This code monitors RA1 for an incoming pulse. When it's found, we start TMRO counting.
;When the signal rises, we move the value of TMRO to PORTB which represents the time elapsed.
;There is a resultant voltage on PORTB by way of a resistor ladder network.
;TMRO overflow time = 256 * (TMRO * Prescaler) / (Freq / 4)
;@ 60mS, RPM is 1000 (our cutoff value). Divide 60mS by 256 and we get 234μS per TMRO increment. With the internal osc. running @ 4MHz,
;that's 1MHz internal clock divided by 256:1 prescaler=256μS

;=========================================================================

;==RAM variables====
p_count equ 0x20

;==Constants used===
#DEFINE NumPulses .10 ;# of pulses from commutator

;==Vectors (Reset/ISR)===
org 0
goto main
org 4
goto ints

;==Interrupt Service Routine (ISR)===

;Triggered on every pulse from motor.

ints bcf INTCON, INTF ;Clear the interrupt
btfsc INTCON, TOIF ;Test if TMRO overflowed
goto stalled ;If it did, motor is stalled
movf p_count, w ;No, proceed with caution...
sublw NumPulses ;W=NumPulses-W
btfss STATUS, Z ;If Z=1 then we're starting fresh.
goto $+2 ;Z=0, we're still counting pulses
clrf TMRO ;Begin counting pulses
decfsz p_count, f ;Decrement pulse counter
retf ;TMRO is still counting, return back to "main"
movf TMRO, w ;Done counting pulses
movwf PORTB ;Move TMRO value to PORTB
movlw NumPulses ;Reload pulse counter
movwf p_count
retf ;Break out of ISR

stalled bcf INTCON, TOIF
movlw 0
movwf PORTB
```

Poptronics, November 2002

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matches your voltage and current requirements. I’m really proud of circuit (b) because of its simplicity. The LM317 voltage regulator biases the bottom end of the motor above ground using the 2.5-k pot. This sets the RPM range of the motor. Q1 in Fig. 2B acts as a variable resistor; and because it’s configured as an emitter follower, it has its own self-regulation built in. Don’t forget to use a large heatsink for Q1, and remember that the maximum current is limited to 1.5 amps (0.5 amp for TO-39).

Notice that I only used every other

FOR EXPERIMENTERS

A kit of parts suitable for experimentation is available for $22 from Futurlec, 1133 Broadway, Suite 706, New York, NY 10010 (www.futurlec.com).

The kit includes a programmed PIC, perfboard, IC sockets, and a heatsink. A programmed PIC is also available separately for $12.

most-significant bit of the Port B output. I did that on purpose. Remember, I said that this method was fairly accurate, but not as accurate as an encoder. Well, 4 bits are good enough for most applications. Referring to Fig. 1, you can insert additional resistors on the empty outputs (they are part of the code) to increase the resolution to 7 bits if you wish. For example, a resistor on RB6 is 1.5k and RB4 is 3.0k. That’s the pattern, except for RB0 on Port B.

If you discover that the range of $V_{out}$ doesn’t match up to your requirements, change the value of Q1 for higher or lower gain as needed and/or the 220-ohm emitter resistor.

I added one more feature. If the motor stalls (that is the TMRO counter overflow), RB0 goes high. Do what you wish with that signal. What I’d do is check a sensor for a blocked path—like a brick wall the hot is trying to push down. Maybe include a routine that puts the motor into reverse and makes a 180-degree turn?

That’s all for this month. This should give you plenty to play with. Next month, I’ll do something in keeping with the Holidays. ‘Til then, have fun.

If you have any questions or comments for me, then send an e-mail to tjbyers@aol.com.
Bi-Pedal Walker, Part 5

Welcome to the final installment of our bi-pedal walker project. For those who have been following this series of articles, the bi-pedal robot does walk. I have placed a short movie file at the following address for those who wish to see the bi-pedal robot walk. (www.imagesco.com/catalog/biped/walker.html) The starting frame for the movie is shown in the accompanying photograph.

This has turned out to be a very challenging project, more challenging than I had imagined in the planning stage. It taught me a lot about designing and building artificial legs, bi-pedal robots in general, and walking algorithms. Everything I have learned I have tried to describe to you in these series of articles. Looking back at this project (hindsight really is 20-20, as they say), I realized some things that could have been done differently to simplify it.

Primarily, I could have stayed with the IBM PC servomotor controller. At the time I got too tied up in getting full power (torque) from the servomotors for the robot to stand up and walk on its own. The two PIC controller circuits I built after that only improved the servomotor performance slightly and not to the point where it contributed much to the algorithm development.

I realized that to use the PIC servomotor program effectively I only needed to change the bi-pedal robot stand setup. Instead of a setup where the legs can lift and walk with the stand, it would have been better to attach the legs to a much taller stand where the legs would hang freely without touching the ground. Doing it this way means that full power from the servomotors is not required to lift and carry the stand. The adjustment and positioning of the servomotor legs to develop a walking gait could take place in midair. I feel the pulse-width numbers generated from this arrangement would be just as accurate. By "just as accurate," I mean the pulse-width numbers would need to be adjusted and fine-tuned in the final program.

Fine-Tuning the Program

When I compiled the walking program based upon the pulse-width numbers I obtained in my previous experiments, the robot didn't walk. The numbers were in the ballpark, but not hitting a home run. The reason is that without the display routine to slow down the program the microcontroller updated the walker servomotors at 50 Hz and developed the proper torque in each servomotor. Having the proper torque shifted the positions of the servomotors. To fine-tune the program, I had to start from the very beginning, with the bi-ped's starting pulse-width numbers, when standing still.

For instance, the old starting numbers provided last month were:

Left Leg Servomotors
- Start: 207- 201- 152- 152-

Right Leg Servomotors
- Start: 4- 5- 6- 7-
- 208- 199- 176- 169-

Note: In last month's column, there was an error in the table listing the leg movements. Numbers 0-3 and 4-7 were moved one column to the left. They are correct above.

—Editor

I entered the pulse-width numbers for the starting standing position and put the robot in a holding routine. I needed to change the pulse-width number for servomotor number 4 to get the bi-pedal robot to stand properly. The new starting numbers are almost the identical to the old numbers—servomotor number 4's pulse-width number changes from 208 to 214.

With the standing-still numbers corrected, I could add the next movement. Before I did so, I created a two-second standing-still loop before the program continued on to the following movements.

The next movement added to the program was the tilt-ankle movement. I placed this movement after the two-second standing-still routine and before the holding routine. So, when the program runs, it stands still for two seconds and then goes to the tilt routine where the movement is held.

Holding the "tilt" movement allows you to examine the tilt and decide if any correction is needed. If an adjustment is needed, the pulse-width number is changed; and the program is run again to check the results. This adjustment-check cycle continues until the tilt pulse-width number is the best you can make it.
LISTING 1
PICBasic Pro Walker Program

Declare Variables
B0 VAR BYTE
B1 VAR BYTE
B2 VAR BYTE
B3 VAR BYTE
B4 VAR BYTE
B5 VAR BYTE
B6 VAR BYTE
B7 VAR BYTE
B8 VAR BYTE
B9 VAR BYTE

'Initialize Variables
B0 = 207  'Servomotor 0
B1 = 201  'Servomotor 1
B2 = 152  'Servomotor 2
B3 = 152  'Servomotor 3
B4 = 214  'Servomotor 4
B5 = 199  'Servomotor 5
B6 = 176  'Servomotor 6
B7 = 169  'Servomotor 7
B8 = 0
B9 = 0

start:

'loop to hold position 2 seconds before moving
B8 = B8 + 1
GoSub servoout
IF B8 < 100 Then GoTo start
B8 = 0  'reset loop counter

'Leg Movements

'Need Slow Speed Routine
M1:
B8 = B8 + 1
  IF B9 = 3 Then M12
  B9 = B9 + 1
  GoTo M13
M12:
B7 = B7 - 1
B3 = B3 - 1
B9 = 0
M13:
IF B7 < 156 Then
  B7 = 156
  EndIF
IF B3 < 139 Then
  B3 = 139
  EndIF
GoSub servout
IF B8 < 50 Then GoTo M1

B8 = 0 'reset loop counter

B1 = 225
B2 = 167
B0 = 193
M2:
   B8 = B8 + 1
   GoSub servout
   IF B8 < 30 Then GoTo M2

B8 = 0 'reset loop counter

B7 = 169
B3 = 152
M3:
   B8 = B8 + 1
   GoSub servout
   IF B8 < 30 Then GoTo M3

B8 = 0 'reset loop counter

B5 = 215
M4:
   B8 = B8 + 1
   GoSub servout
   IF B8 < 30 Then GoTo M4

'Need Slow Speed Routine
M5:
   B8 = B8 + 1
   IF B9 = 3 Then M52
   B9 = B9 + 1
   GoTo M53
M52:
   B3 = B3 + 1
   B7 = B7 + 1
   B9 = 0
M53:
   IF B3 > 168 Then
      B3 = 168
      EndIF
   IF B7 > 185 Then
      B7 = 185
      EndIF
   GoSub servout
   IF B8 < 90 Then GoTo M5

B8 = 0 'reset loop counter

B1 = 201
B4 = 192
M6:
   B8 = B8 + 1
   GoSub servout

'2nd Movement Lift Leg

'3rd Movement Straighten Out

'4th Movement Right Knee

'5th Movement Tilt opp. side

'6th Movement
IF B8 < 30 Then GoTo M6

B8 = 0

'B8 = 0

'B2 = 152
B6 = 185
M7:
B8 = B8 + 1
GoSub servoout
IF B8 < 30 Then GoTo M7

B8 = 0

'B8 = 0

'B5 = 199
M8:
B8 = B8 + 1
GoSub servoout
IF B8 < 30 Then GoTo M8

B8 = 0

'B8 = 0

'B7 = 169
B3 = 152
M9:
B8 = B8 + 1
GoSub servoout
IF B8 < 30 Then GoTo M9

B8 = 0

'B8 = 0

'B6 = 176
M10:
B8 = B8 + 1
GoSub servoout
IF B8 < 30 Then GoTo M10

B8 = 0

'B8 = 0

'B0 = 207
B4 = 214
M11:
B8 = B8 + 1
GoSub servoout
IF B8 < 30 Then GoTo M11

B8 = 0

'B8 = 0

hold:
GoSub servoout
GoTo hold

'servoout:

'Output servomotor position(s)
When satisfied with the tilt movement, insert the next movement after the tilt routine and before the hold routine. Each movement is checked, adjusted, and checked again until optimized. I continued in this manner, working my way through the entire sequence of movements that make up one whole step. Once each movement is optimized in the program, I set up a small counter for the bi-pedal robot to take three forward steps in a row.

A Little More On the Tilt

Tilting the robot is critical to shifting its weight from one leg to the other. One next thing I found to do was to tilt both ankles to the left or right, instead of just one. This shifted the robot's weight more easily.

When tilting the robot, I also added pulse-width number delay inside the routine. This delay was necessary because the robot would start and stop so quickly that the tilt movement could topple the robot.

**Schematic**

The PIC microcontroller schematic is shown in Fig. 1. Not all of the bi-pedal servomotors are shown in the schematic; only servomotor 0 is shown as a reference. All other servomotors (1–7) are connected in a similar manner. You can see from the schematic that there are five open I/O lines on the 16F84 microcontroller that may be used for control functions. A simple walking PICBasic program is provided elsewhere. This program produces a little jerky walk, but it does the job. It is also suited for modifying to fine-tune the program movements, as described earlier.

I subsequently wrote a more sophisticated program that uses a smoothing (slow speed) algorithm throughout all the step movements. This was the program used to generate the bipedal.avi movie on the Web site. In contrast to the program above, it also combines a few step movements when possible. The program source code for this program will also be available from the same Web page listed above for the .AVI movie.

**Future Walking Algorithms**

The walking programs presented are basic. There is much room for improvement in the walking algorithm. As an example, once when I was re-writing the original program, I inadvertently reversed a few movements and the bi-ped almost walked backwards. Other improvements will incorporate improved strides, higher steps (maybe even stair climbing), and turning. Turning, I think, will be a little tricky and may require a design change.

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Fig. 1. The PIC microcontroller schematic is shown above. Not all of the bi-pedal servomotors are in the schematic; only servomotor 0 is shown as a reference. All other servomotors (1–7) are connected in a similar manner.
Understanding And Testing Low-Power Laser Diodes

Laser diodes are now used in a wide variety of electronic equipment including CD and DVD players and drives, other optical storage devices, laser printers, barcode scanners, and perimeter alarm systems—and, of course, laser pointers. When repairing such equipment, it is desirable to be able to test the laser diode (LD). When any of these devices are retired (except possibly for laser pointers), the failure is often not the laser diode, and salvaging them for other uses is possible. This “Service Clinic” deals with some of these issues for the typical low-power laser diodes in consumer electronics equipment.

Safety, First

Despite their small size and low input power, laser diodes may still present a significant hazard to vision. This is especially true where the output is collimated and/or invisible (near IR) and/or higher power than the typical 3 to 5 mW. At least, you don’t have to worry about getting zapped by any high voltage (as in a HeNe or argon laser).

Never look into the beam of any laser—especially if it is collimated. Use an indirect means of determining proper operation such as projecting the beam onto a white card, using an IR detector card or tester (where needed) or laser power meter.

Laser diodes in CD players operate at 780 nm (near IR, virtually invisible). While they are safely tucked away inside the optical pick-up, risks are quite minimal because the output is usually less than 1 mW and the emerging beam is highly divergent. However, if modifications are made to the pickup (such as removing the objective lens), a 5-mW collimated beam can be produced that can burn holes in the retina without your even being aware there is a problem.

Common visible red laser diodes, diode laser modules, and laser pointers produce 1 to 5 mW at various wavelengths between 670 and 635 nm. When collimated (as in the case of a module with internal optics or a laser pointer), the entire beam can enter the eye and burn holes in the retina. Note that light at 635 nm appears more than five times as intense as light at 670 nm. Therefore, the apparent brightness of a source is not a reliable indication of its actual optical power output.

Currently, green laser pointers are not simple diode lasers but are Diode-Pumped Solid-State Frequency-Doubled (DPSSFD) lasers (this may change in the future, however). For a given power, green appears substantially brighter than red wavelengths, but they are also limited to a maximum power of 5 mW. However, since there is a high-power IR laser diode inside a green pointer and not all such pointers include an adequate IR-blocking filter, there could be other dangers lurking even if the green output is weak or dead. With both these lasers, the beam from the bare laser diode is highly divergent. Therefore, it’s less of a hazard since the lens of the eye cannot focus it to a small spot. However, there is still no reason to look into the beam.

Writeable optical drives (WORM, CD-R) may use IR laser diodes producing tens of mWs. A typical CD-R drive sets the laser power at 3 to 5 mW for read and 25 to 30 mW for write. Various types of laser cameras and laser typesetters may use laser diodes of hundreds of mWs. These lasers are extremely dangerous, even if not that well collimated. Furthermore, they also use near-IR wavelengths so that there is essentially no warning that a beam is present. In fact, since the response of the human eye to near-IR radiation results in a weak indication of red light, one may come to the false conclusion that the output is a weak visible beam. The actual optical power is 10,000 times higher, and the damage would already been done.

Much higher power visible and IR diode lasers are available and becoming more common and affordable with
the popularity of diode-pumped solid-state lasers (including green laser pointers that contain a high-power IR laser diode). These devices represent an even greater danger to vision and potentially even a risk of heat damage or fire from a focused beam.

**Follow These Guidelines**

While laser diodes and LEDs share some similarities, laser diodes are much more sensitive to EVERYTHING and will die with the least provocation. To minimize the chance of damage to your precious laser diodes during assembly, rework, or removal from equipment, read and follow the guidelines below. Some of these apply only to those using optical feedback, while others apply to all types.

- Keep the LD (remember LD is laser diode) in its original antistatic packaging until ready to install or poke it in antistatic foam (for salvaged diodes).

- Keep the laser-diode leads shorted together with some fine wire or other means before installation, while soldering, until the driver is fully connected.

- Where the LD needs to be attached with a connector (it isn't permanently installed in a circuit), add a parallel combination of a small capacitor, resistor, and reverse-protection diode. Some typical values: 1 nF, 1K, 1N4148 for a low-power diode; or 0.01 μF, 100K, 1N4148 for a 1-watt pump diode.

- Take reasonable ESD precautions including the use of a grounded wrist strap. Don't work in a wool sweater with your feet rubbing on an Oriental wool carpet!

- When soldering, minimize heating of the LD itself by soldering as quickly as possible. Pre-tin the wires or pads to which the LD will be attached.

- Use a properly grounded temperature-controlled soldering iron with a fine-point tip. A 100-watt Weller soldering gun isn't the right tool for reworking or assembling a fine-line printed circuit board!

- Provide adequate heatsinking or a ThermoElectric (TE) cooler along with the proper mounting of the diode to assure that temperature of the diode itself never exceeds 35 to 40°C.

- Use only a driver that is guaranteed to have no overshoot or reverse-polarity spikes. Even if the diode came with complete test data, assume that your environmental conditions may differ by enough to affect key parameters like monitor photodiode sensitivity—start low and work up to rated power using a proper measuring technique. Make sure the current limit is set to a safe value for the diode—optical feedback can get confused.

- Double-check your pin/terminal connections. For bare LDs (especially high-power ones), the heatsink is almost always the Anode (positive) and the top terminal is the Cathode (negative). This is the reverse of what most engineers expect! For packaged LDs, there is no standard! Close is only valid in horseshoes and hand grenades—with LDs, it often means total destruction!:-)

- For bare LDs, avoid getting anything on the output facet. Even a single speck of dust can cause instant permanent damage to the diode. Once a system is completely built, it should be sealed, preferably with dry nitrogen, to prevent contamination. For packaged high-power LDs, anything on the output window will likely be burnt to a crisp, which may damage the window.

- Avoid inadvertent reflection of the diode's output back toward the diode. Such reflections can interfere with lasing, resulting in excessive current for optical-power feedback-regulated diodes.

**Finding Specifications For Salvaged Laser Diodes**

The optical assemblies from CD players, laser printers, and other deceased or obsolete equipment are a fabulous source of low-cost LDs. It would be nice if something were known about their specifications!

- Measure the voltages, currents, signal waveforms, etc., before you rip it apart! However, it may not be possible to do so if the equipment was received in a non-working state. In addition, performing such tests on the laser-diode assembly itself can be risky. Hopefully, there will be labeled test points for laser-diode current, at least.

- Obtain schematics and/or service manual for the equipment. They might provide enough information to use the existing circuitry or to design circuitry to replace it. However, schematics are rarely available, at least not economically. Even if they are, the needed details may not be present. In addition, the actual circuitry is inside an integrated circuit, which is part of some overall control system, and may not be useful for stand-alone applications, anyhow.

- Reverse-engineer the circuits. Trace the component layout from the actual circuit board to determine what is going on and then duplicate or use them as desired. This strategy should permit laser-diode operating current and/or photodiode sensitivity to be determined. With some equipment, it isn't that difficult as the driver circuitry is relatively simple. With others, it is next to impossible.

- Identify the laser diode. Remove the LD from its mounting (taking appropriate ESD precautions) and hope it has a legible part number. Then, go to www.qsl.net/k3pgp/Notebook/Ldspecs/ldspeks.htm (K3PGP's Laser Diode Specifications) maintained by K3PGP (e-mail: k3pgp@qsl.net) or to an optical devices databook to locate its specifications. Many major laser diode manufacturers have Web sites with extensive information and search facilities.

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Pinning Down Pinouts

Note that if you have a device from a CD player, CD-ROM, or other optical drive with eight or ten pins, it is a combined laser diode and photodiode (PD) array in a single package. You will first have to identify the three connections to the LD itself. You should be able to determine this by tracing the wiring—there may even be markings on the circuit board. In many cases, the LD is driven by discrete components, whereas everything else goes to a preamp IC. Once the pinout of the LD is known, it can be treated in exactly the same way as the more common three-pin type.

The following assumes you know nothing about your device other than that it is a 3- to 5-mW laser diode with three pins. (There are a few with four pins and totally separate LD and PD connections, but these are not common.)

The first step is to identify which pair of terminals is the laser diode and photodiode. Your LD package will be configured like those in Fig. 1.

The most common polarities for low-power LDs seem to be the ones shown in Fig. 1B. The common (C or COM) terminal will then be connected to a positive supply (+V) relative to LDC and PDA. The PD will be reverse-biased. Its anode (PDA) will feed a load resistor and sense amplifier for the optical-feedback current-regulator. The LD will be forward-biased. Its cathode (LDC) will connect to a driver transistor and/or network to regulate LD current, based on the photodiode current and possibly a modulation circuit.

Where you can see both the pins and the inside of the LD package, it is easy to identify which pins go where. The COM will be connected to the case and the platform on which the laser diode and photodiode are mounted. There will likely be no actual pin visible inside the case.

The connection to the LD will attach via a fine wire to the laser-diode chip, which is near the front (optical window) of the package. The connection to the PD will attach via a fine wire to the PD chip mounted (probably at a slight angle) deep inside the package.

If you can confirm these three connections by inspection, only the LD and PD polarities will need to be determined experimentally.

The following assumes you did not have this luxury. The PD's forward-voltage drop will be in the approximately 0.7-volt range compared to 1.7-2.5-volt for the LD. So, for the test below if you get a forward-voltage drop of under a volt, you are on the PD leads. If your voltage goes above 3 volts, you have the polarity backwards.

CAUTION: Some laser diodes have very low reverse-voltage ratings (e.g., 2 V) and will be destroyed by modest reverse voltage. Check your spec sheet. However, the LDs found in CD players seem to be happy with 4 or 5 volts applied in reverse. Of course, a shorted or open reading could indicate a defective LD or PD.

If the LD is still connected to its circuitry (probably a printed flex cable), it is likely that the laser diode will have a small capacitor directly across its terminals and that the optical-sensing PD will be connected to a resistor or potentiometer. In particular, this is true of Sony pickups and may help to identify the correct hookup.

Powering Up

Either of the circuits in Fig. 2 can be used to identify the proper connections and polarity and then to drive the LD for testing purposes.

One approach that works for testing is to use a 0- to 10-VDC supply with a current-limiting resistor in series with the diode (Fig. 2A).

If your power supply has a current limiter, set it at 20 or 25 mA to start. You can always increase it later. Alternatively, a fixed supply with a potentiometer can be used. (See Fig. 2B.)

Resistor R2 limits the maximum current. If you know the specs for your diode, this resistor is a good idea (and it protects your power supply, as well). You can always reduce its value if your LD requires more than about 85 mA (with R2 = 100 ohms).

The two capacitors provide some filtering to reduce the risk of a transient blowing the LD. Capacitor C2 should be mounted close to the laser diode. The part about 'no overshoot' is very important. If the supply isn't well behaved, it will fry LDs.

Before attempting to obtain lasing action with either of these circuits, monitor the voltage across what you think is the LD as you slowly increase the power supply or potentiometer. If you guessed correctly (or have the pinout diagram from the spec sheet or determined from its former life), the voltage will increase until around 1.5 to 2 V and then climb more slowly. Don't push your luck, unless you are also monitoring the laser-diode current and optical output.

If you are checking voltage across the laser diode or photodiode in the reversebiased direction, it will continue to climb above 2 volts without slowing. Don't push your luck here either—the breakdown voltage of the LD may be only a little more than this and—you guessed it—exceeding this voltage is not healthy for the LD either.

If you are monitoring the PD in the forward direction, the voltage will get stuck around .7 volts. Once you have identified the correct connections, very carefully monitor the current through the LD as you slowly increase the current and...
check for a laser beam.

For IR laser diodes, you must use an IR-detector circuit, card, video camera or camcorder (with the requisite three hands) to monitor an actual IR laser beam. For visible laser diodes, you can use your eyes or any more sophisticated detector, as desired. Look from an oblique angle or better yet, place a white card a couple of inches in front of the LD. Even a 1-mW LD is an intense source of light—there will be no doubt when lasing begins.

However, some LDs may have an operating current as low as 20 mA and VCSELs (Vertical Cavity Surface-Emitting Laser diodes) tend to be much lower (but you probably don’t have any of those to play with yet). Of course, if you inherited a bag of identical LDs and can afford to blow one: (1) Send me a few before you do this, and (2) you probably could fairly accurately characterize them by testing one to destruction.

For a current below the lasing threshold for your LD, there will be some emission due to simple LED action. As you slowly increase the current, at some point (if the LD is good) as you exceed the threshold current, the character of the emission will change dramatically, and a very slight increase in laser-diode current will result in a significant increase in intensity. Congratulations! The LD is lasing.

CAUTION: Unless you have a laser power meter, be careful. The maximum safe current may be as little as 5% above the lasing threshold.

Go over by 6%, and your diode may be history. The exponential power curve seems to be steeper with visible LDs, but there is no way to be sure without specifications. It is all too easy to convert laser diodes into extremely useless DELDs (Dark-Emitting Laser Diodes) or very expensive LEDs.

I have used this approach with LDs from dead CD players without difficulty. In the case of many of these LDs, the operating current is printed on a sticker on the optical block, often as a three-digit number representing the current in tens of mAs. Typical values are 35 to 60 mA (350 to 600). Sony pickups typically average around 50 mA. Without this information, the best you can do is to estimate when it is lasing at the proper intensity by comparing the brightness of the red dot one sees by looking into the lens from a safe distance at an oblique angle. However, this is not very reliable as the optical power at the objective lens depends on the particular CD player.

Even if you have complete test data for your diode, it’s still a good idea to start low and monitor output power. The diode was originally tested under very precise conditions, which probably aren’t quite the same as you have (e.g., temperature); so laser-diode or photodiode current that you monitor could be different by enough to cause problems.

Wrapup

Now that you have the basics, go rummaging around in that junk box and dig out all those old CD players and laser printer carcasses. Although not mentioned above, in addition to the actual laser diodes, there will be useful optics and even, possibly, some of the associated driver circuits.

Just make sure to always follow the safety guidelines in working with any laser or laser-based device. Much more information on LDs and all other laser-related topics can be found on my Web site www.americanradiohistory.com in “Sam’s Laser FAQ.” I welcome feedback (via e-mail please) to sam@repairfaq.org.
Diversity

If electronics offers anything to the hobbyist, it's diversity. Almost everything we do today involves electronic circuitry in one form or another. Unlike the devices of the past, most electronic devices used today are more complex and downright unfriendly to change or modification. So we're going to start off our circuit marathon with just such a problem.

Burglar Alarm Woes

A friend has this new modern computer-chip-controlled burglar-alarm system that was designed to sound a low-volume alarm and automatically dial several numbers to alert interested parties in the event of a possible burglary in progress. In theory this might be a good idea; however, for my friend it would only work if the interested party was near his phone, and who could guarantee that?

"Could I add a much louder alarm to the system?" he asked.

"Oh sure, that should be no problem," I quickly responded. Upon looking over this electronic marvel, I knew I had spoken way too fast.

There was no external output to use for any purpose whatever available on the alarm. After reading the alarm's handbook, I immediately realized that I did not want to open the unit or make any direct connections to it. The only output available was the beep, pause, beep output of the alarm when set off. A blinking or glowing LED would have been perfect to couple to with a photo-transistor; however, although acoustic coupling was not the best choice, it was the only choice available.

A Workable Solution

The single-stage amplifier circuit shown in Fig. 1 turned out to be a simple solution for the alarm system as installed. With the added alarm sounder located outside and away from the control unit, feedback to our pickup microphone did not occur.

![Diagram of the single-stage amplifier circuit.](image)

**Fig. 1.** The single-stage amplifier circuit shown above turned out to be a simple solution for the alarm system as installed. With the added alarm sounder located outside and away from the control unit, feedback to our pickup microphone did not occur.

**PARTS LIST FOR THE AMPLIFIER CIRCUIT (FIG. 1)**

<table>
<thead>
<tr>
<th>SEMICONDUCTORS</th>
<th>CAPACITORS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Q1—2N3904 NPN transistor</td>
<td>C1, C2—.22-µF, ceramic-disc</td>
</tr>
<tr>
<td>Q2—IRF511 HEXFET</td>
<td>C3—47-µF, 25-WVDC, electrolytic</td>
</tr>
<tr>
<td>D1, D2—1N914 silicon diode</td>
<td>C4—10-µF, 25-WVDC, electrolytic</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>RESISTORS</th>
<th>ADDITIONAL PARTS AND MATERIALS</th>
</tr>
</thead>
<tbody>
<tr>
<td>(All resistors are 1/4-watt, 5% units.)</td>
<td>.39-inch diameter, electret-microphone element</td>
</tr>
<tr>
<td>R1, R4—100-ohm (see text)</td>
<td></td>
</tr>
<tr>
<td>R2, R3—2200-ohm</td>
<td></td>
</tr>
<tr>
<td>R5, R6—220,000-ohm</td>
<td></td>
</tr>
</tbody>
</table>

Fig. 2. A separate power source for the circuit in Fig. 1 and the add-on alarm sounder is shown here. A battery tender, also known as a trickle charger, supplies charging current to the 12-volt lead-acid battery.

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*By Charles D. Rakes

Charles Rakes is a hobbyist who writes for American Radio History. He can be reached at Charles.Rakes@americanradiohistory.com.
location for the mike can only be determined by testing and experimenting with the system in operation.

This particular alarm system uses the internal piezo-alarm-sounder elements for other audible function indicators. Arming the alarm sends out a beep from the piezo sounder, which must be ignored by the add-on circuit. Also when the alarm does go off, it produces a beep-pause-beep output, which must be detected by the add-on circuit. The circuit must ignore a single beep, but supply an output when the beeps are repeated. This discrimination between single and recurring beeps is primarily accomplished with the location of the mike and the RC timing of R6 and C4.

Changing the value of R1 is another variable, which sets the amplifier’s gain. However, this change should not be required for most applications and, therefore, should only be performed when all other attempts fail. Increasing the value of R1 lowers the amp’s gain, and decreasing the value raises the gain. Increasing the amplifier’s gain can really increase the difficulty in obtaining a balance between the single and recurring beeps.

OK, now let’s see how the circuit discriminates between the two signals. The beeps (and, for that matter, all other sounds) are picked up by the microphone and amplified by Q1. The amplifier’s gain is very low, making it insensitive to sounds that are not close to, and directly in front of, the microphone. The amplified signal feeds a voltage doubler, made up of C2, D1, D2, and C4, with R6 setting the discharge time. The doubler’s positive output turns on the power HEXFET, which delivers power to the load.

A short burst of sound from the alarm only charges C4 a small amount and not enough to turn Q2 on. Following the single beep, R6 begins to discharge the voltage across C4 back to ground level. A number of beeps in sequence causes the voltage across C4 to increase in steps until Q2 turns on, activating the added alarm sounder. Loud sounds from outside the room, including car horns and even thunder, have no effect on the circuit because of the amplifier’s low gain, C4’s charging time constant, and the location of the microphone. Also, the circuit is immune to inside room noises, including conversations, radios, and other ambient sounds in a typical household.

**Power For The Add-On Circuit**

A separate power source for the circuit in Fig. 1 and the add-on alarm sounder is shown in Fig. 2. A battery tender, also known as a trickle charger, supplies charging current to the 12-volt lead-acid battery.

The battery selected should have the capacity to supply the alarm sounder for at least an hour of operation. I would double the current requirement of the added alarm sounder and use a battery of that current rating. If the alarm sounder pulled 1 amp, then a good choice would be a 2-amp-hour battery.

Fuse F1 protects the battery from a faulty charger, and F2 protects the battery from an overload. The actual fuse values are determined by the battery used and the charger’s maximum charging current.

**Another Solution**

There are many avenues to follow in selecting or designing an electronic circuit to solve a particular problem, and the circuit shown in Fig. 4 is just another solution with a slight twist. An op-amp is the amplifying device, replacing the transistor in Fig. 1. The slight twist to this circuit is the addition of a gain-control potentiometer, R6. The circuit’s voltage gain can be precisely set from unity gain up to a gain of one hundred.

**PARTS LIST FOR THE OP-AMP AMPLIFIER**

(Fig. 4)

**SEMICONDUCTORS**

IC1—LM324 Quad, op-amp
Q1—IRF511 HEXFET
D1, D2—1N914 silicon diode
LED1—Light-emitting diode, any type or color

**CAPACITORS**

C1, C2—.22 µF, ceramic-disk
C3—10 µF, 25-VWDC, electrolytic

**RESISTORS**

(R5—220,000-ohm
R6—100,000-ohm potentiometer

(All resistors are ½-watt, 5% units.)
R1, R2—10,000-ohm
R3—2200-ohm
R4, R7—1000-ohm

**ADDITIONAL PARTS AND MATERIALS**

.39-inch diameter, electret microphone element; IC socket; etc.
This circuit's function is to discriminate between the beep-beep alarm on the alarm system and the loud sound coming from the add-on sounder. Under ideal conditions this is not a good thing, and, at best, it only has a 50-50 chance of operating successfully.

**PARTS LIST FOR THE SOUNDER TWO (FIG. 5)**

**SEMICONDUCTORS**
- IC1—LM324 Quad, op-amp
- Q1—IRF511 HEXFET
- D1, D2—1N914 silicon diode

**RESISTORS**
(All resistors are 1/4-watt, 5% units.)
- R1—R3—2200-ohm
- R4—R12—10,000-ohm
- R13—220,000-ohm
- R14—5000-ohm potentiometer
- R15—100,000-ohm potentiometer

**CAPACITORS**
- C1—C5—22-µF ceramic-disc
- C6—47-µF, 25-WVDC, electrolytic
- C7—10-µF, 25-WVDC, electrolytic

**ADDITIONAL PARTS AND MATERIALS**
- Two .39-inch diameter, electret microphone elements; IC socket; etc.

The remaining circuit operation is the same as in our first circuit.

### Setting The Gain

Place the microphone on the alarm unit about one inch from the piezo alarm sounder. Don’t aim the mic directly at the sounder, but in a position perpendicular to it. Temporarily tape the mic in place. If the microphone is placed directly facing the sounder, it becomes more difficult to distinguish between a single beep and sequential beeps.

Start with the gain control at its maximum resistance setting. Set the alarm off allowing the beep-beep sounds to continue. Very slowly rotate R6, lowering the resistance, until the LED turns on. Stop and observe that the LED does not flicker on and off. Reset the alarm and test again to see that the LED turns on and remains steady.

Reset the alarm and let a few seconds pass. Arm or press any button that produces a single beep and observe the LED. The LED should not flicker or light with a single beep. Also playing a radio or any other normal room sounds should not cause the LED to light.

### Setting The Parameters

One thing we don’t want to happen is that the alarm goes off and is not detected by our circuit. Two important gain settings must be determined—the gain setting where the circuit just starts to operate and the gain setting where a single beep causes the LED to flicker. Since the circuit’s gain has just been adjusted for the LED to only operate with a sequential beeping sound, we can now determine the maximum gain setting. Each time an adjustment is made, the circuit should be allowed to settle for at least ten seconds before testing. This delay will allow time for the timing capacitor, C3, to discharge.

Increase the gain slightly and test with a single beep. Continue increasing the gain with ten-second pauses between test beeps, and stop when the LED flickers or turns on.

This is the maximum gain setting. The ideal operating gain setting will be between these two potentiometer positions. Start testing with the pot set in the middle of the two settings. Testing and experimenting will yield the best gain setting for trouble-free operation.

### The Red Herring

Just as I was wrapping up the add-on alarm sounder, my friend casually stated that he also thought it would be a good idea to add a similar alarm sounder inside the very room where the alarm unit was located. His thoughts were that it would appeal to a hearing-impaired burglar and hopefully help him make the decision to leave at once. I convinced him that we should let the first one burn...
Catch Of The Day

Never duck a challenge, I thought, as I traveled home that day. The circuit in Fig. 5 just might be a possible solution to the indoor alarm quandary, and then maybe not. This one I've not had the opportunity to fully check out in my friend's settings; however, preliminary tests are promising. I'm hoping that my friend forgets all about it, and I can move on.

The circuit's function, in Fig. 5, is to discriminate between the beep-beep alarm on the alarm system and the loud sound coming from the add-on sounder. Under ideal conditions this is not a good thing, and, at best, it only has a 50-50 chance of operating successfully. With this one, you are on your own. I'll outline the circuit's operation, and then you have my permission to enjoy the frustrations of balancing the circuit between the two sound sources. Good luck, and no name-calling will be allowed.

Two microphones are used, one to pick up the sound from the alarm's piezo sounder—as in our first two circuits—and the second to detect the sound from the indoor alarm sounder.

The alarm signal from the piezo sounder is picked up by microphone 1 and is fed to op-amp "A" with a gain of one. The alarm signal from the big indoor sounder is picked up with microphone 2 and fed to op-amp "B" with a gain of one and then to op-amp "C" with a gain of one, also. The reason for passing the signal through two op-amps is to invert the signal 180 degrees out of phase with the signal coming out of op-amp "A." In theory, if the signals from the big loud sounder picked up by microphone 1 and by microphone 2 are fed to the input of another op-amp with a 180-degree phase shift, most of the signal of the loud sounder can be cancelled and not amplified. Op-amp "D" and the circuitry following it operate in the same way as our two previous circuits.

The two out-of-phase signals meet at the wiper of potentiometer R14, and the combination of signals is fed to op amp "D." Resistor R14 is adjusted to a point where the output from the loud sounder is at a minimum level, feeding op-amp "D."

Op-amp D's gain is set to a level to activate the add-on alarm when the sequential beep is detected. Getting the correct balance between the two signals and the best gain setting will be a behemoth of a chore. The challenge is yours—the circuit disappears in exactly five seconds.

Good luck!

DIGITAL DOMAIN

(continued from page 15)

On the other hand, there's much that isn't online or in print. Sometimes, you just have to talk with people or observe things firsthand to really know what's going on.

Speed Writing—The Internet is about speed. People want to get in and out quickly. Neither the Web nor the online discussion group is the best place for long uninterrupted blocks of text.

On the Web, you need to grab readers' attention and make your main points in the first screen. In online discussion groups, however, you need to do the same in the first sentence or two. Otherwise, with a quick click, readers will be off to the next site or message. Don't hesitate to present all the necessary information. Just break it up and let readers know what they're in for. Include the word "long" in parentheses at the end of the subject line of your message or indicate at the top of the body of the message that yours will be a long response.

Sometimes, people writing in online discussion groups forgo traditional print conventions, such as capitalization and paragraphing. This may look hip, but ultimately it just makes reading what you're writing more tedious. It will take readers more time to decipher where one thought ends and another begins.

Often, online writing use conversational acronyms such as IMHO (In my humble opinion) and "emoticons" such as :). The latter is a sideways symbol representing a smiling face, and it signals that you're telling a joke or trying to be friendly. Such conventions work so long as the bulk of your readers understand them. The risk is that new-comers can feel left out.

Presentation—This is primarily an issue for Web sites because typically they're more elaborately designed than text messages. Simpler is almost always better, though, even with Web sites.

The best Web sites don't merely dazzle with flashy animations or the hippest new technology. As with magazines, newspapers, and books, they try to maximize the reader's experience. Don't overdo it by including colored or textured backgrounds that interfere with readability. Similarly, overlarge graphics, dancing buttons, blinking text, and other bells and whistles can draw too much attention to themselves and detract from the reader's overall experience.

Make sure you provide the appropriate navigational aides. Include buttons to the site's major sections at the edge of all or most pages, whether on top, to the left, at the bottom, or to the right. Some sites also include a site map or index that displays all the interior links for those who feel a need to get their bearings. Be sure to include links to interior pages. Finally, with large sites, include an internal search engine so readers can quickly home in on what they're after.

Whether you want to tinker with and improve your PC and its programs or hone your Web communication skills, there are always places to go for further tips. See the sidebar for further information.

Reid Goldsborough is a syndicated columnist and author of the book Straight Talk About the Information Superhighway. He can be reached at reidgold@netaxs.com or www.netaxs.com/~reidgold/column.

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Build Your Own Wireless LAN
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Integrated Circuit Mask Design
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Debugging: The Nine Indispensable Rules For Finding Even The Most Elusive Software And Hardware Problems
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802.11 Demystified
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<th>Cost</th>
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<td>$99.95</td>
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<th>Price</th>
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<td>LABX-2</td>
<td>For 28 or 40-pin MCUs</td>
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<td>LAB-3X</td>
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