Wireless World November 1973 20p

Tuner-amplifier survey Model railway control system

Australia 78 cents Belgium Fi, 41.00 Canada So zents Denmark Kr, 8.00 Rhodasia 70 cents Finland Br, 8.300 South Africe 65 cents Germany Em. 3.50 South Africe 65 cents Sweden Kr, 4.25 Inkl morts Switzerland Fr, 4.20 U.S.A. \$ 1.06

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LOW COST VOLTMETERS

These highly accurate instruments incorporate many useful features, including long battery life. All A type models have $3\frac{1}{4}$ " scale meters, and case sizes 5" x 7" x 5". B types have 5" mirror scale meters and case sizes 7" x 10" x 6".



PORTABLE INSTRUMENTS





A.C. MICROVOLTMETERS

 $\label{eq:Voltage} \begin{array}{l} \mbox{Voltage δ db RANGES: $15\mu V, 50\mu V, $150\mu V, \dots 500V f.s.d.} \\ \mbox{Acc. $\pm 1\% \pm 1\% f.s.d. $\pm 1\mu V at 1 kHz. $= 100, $-90...$ + 50dB,} \\ \mbox{scale} = 20dB/+ 6dB rel. to 1m W/600 \Omega. \\ \mbox{RESPONSE: $\pm 3dB from 1 Hz to 3MHz. $\pm 0.3dB } \\ \mbox{from 4Hz to 1MHz above 500 } \mu V. Type TM3B can be \\ \mbox{set to a restricted B. W. of 10Hz to 10 kHz or 100 kHz,} \\ \mbox{INPUT IMPEDANCE: Above 50mV : $> 4.3M\Omega < 20pf. \\ \mbox{On 50}\mu V to 50mV : $> 5M\Omega < 50pf. \\ \mbox{AmpLiFIER OUTPUT: 150mV at f.s.d.} \end{array}$



D.C. MICROVOLTMETERS

VOLTAGE RANGES: 30μ V, 100μ V, 300μ V... 300V. Acc. $\pm 1\%$, $\pm 2\%$ f.s.d., $\pm 1 \mu$ V. CZ scale. CURRENT RANGES: 30μ A, 100μ A, 300μ A, 300 mA. Acc. $\pm 2\%$, $\pm 2\%$ f.s.d., $\pm 2 \mu$ A. CZ scale. LOGARITHMIC RANGE: $\pm 5\mu$ V at $\pm 10\%$ f.s.d., $\pm 5 m$ V at $\pm 50\%$ f.s.d., $\pm 500 m$ V at f.s.d. RECORDER OUTPUT: ± 1 V at f.s.d. into > $1k\Omega$

£55 type TM10 (appearance similar to type TM9B)

D.C. MULTIMETERS

VOLTAGE RANGES: $3\mu V$, $10\mu V$, $30\mu V$... 1kV. Acc. $\pm 1\% \pm 1\%$ f.s.d. $\pm 0.1\mu V$. LZ & CZ scales. CURRENT RANGES: 3pA, 10pA, 30pA... 1mA (1A for TM9BP) Acc. $\pm 2\% \pm 1\%$ f.s.d. $\pm 0.3pA$. LZ & CZ scales. RESISTANCE RANGES: 3Ω , 10Ω , 30Ω ... $1kM\Omega$ linear. Acc. $\pm 1\% \pm 1\%$ f.s.d. up to $100M\Omega$. RECORDER OUTPUT: 1V at f.s.d. into > 1k Ω on LZ ranges.



BROADBAND VOLTMETERS

H.F. VOLTAGE & dB RANGES: 1 mV, 3mV, 10mV... 3V f.s.d. Acc. $\pm 4\% \pm 1\%$ of f.s.d. at 30MHz. - 50dB, - 40dB, - 30dB to + 20dB. Scale - 10dB/+ 3dB rel. to 1mW/50 Ω . ± 0.7 dB from 1MHz to 50MHz. \pm 3dB from 300kHz to 400MHz. L.F. RANGES: As TM3 except for the omission of 15 μ V and 150 μ V. AMPLIFIER OUTPUT: Square wave at 20Hz on H.F. with amplitude proportional to square of input. As TM3 on L.F.



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WW-004 FOR FURTHER DETAILS



Line Matching Transformers from Standard to Super Fidelity

It's easy to choose the right Line Matching Transformer from the five Gardners ranges.

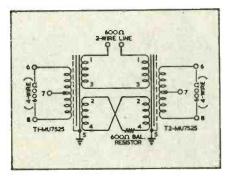
The Super Fidelity Series, with a frequency response of 10Hz to 80kHz – 0.5dB, gives the widest possible bandwidth for high accuracy instrumentation and recording applications.

Then there's the Wide and Extra Wide-band ranges. Outstanding performers with a frequency range 30Hz – 20kHz or more – for the 0.5dB points. Used a lot by broadcasting and recording companies throughout the world.



The Miniature and Standard ranges provide excellent bandwidth for most purposes, 30Hz – 22kHz for the 1.0dB points.

Except for the very smallest in the range, all Gardners Line Matching Transformers are fully magneti-



cally shielded, giving very high hum rejection ratios. Prices start from £3.19 (recommended retail price) and all types are usually available from stock.

Complete technical information is given in brochure GT.5 'Audio Frequency Transformers' which we'll be glad to send on request.

So accurate is the balancing of the windings on some of these transformers that, when used as pairs in a hybrid circuit (as illustrated) we can guarantee a rejection of better than -55dB over the frequency range 50Hz to 10kHz and normal rejection of up to -75dB may be expected.



Specialists in Electronic Transformers and Power Supplies



Gardners Transformers Limited, Christchurch, Hampshire, BH23 3PN Tel: Christchurch 2284 (STD 0201 5 2284) Telex: 41276 GARDNERS XCH.

is this the price you pay?

Probably if you're still using an ordinary soldering iron Ordinary soldering irons can cause damage to transistors and integrated circuits - damage which wastes time and costs money. Now, with the unique ANTEX X25 and CCN low leakage soldering irons no harm can come to the most delicate equipment. even when soldered 'Live'. (You could be making quite a saving). All prices include V.A.T. at 10%

MODEL X25

220-240 Volts or 100-120 Volts. The leakage current of the NEW X25 is only a few microamps and cannot harm the most delicate equipment even when soldered "live", Tested at 1500v, A.C. This 25 watt iron with it's truly remarkable heat-capacity will easily "out-solder" any conventionally-made 40 and 60 watt soldering irons, due to its unique construction.advantages. Fitted long-life ironcoated bit 1/8" other bits avail-able 3/32" and 3/16". Totally enclosed element ceramic and steel shaft. Bits do not "freeze" and can easily be removed PRICE: £1.93 (rec. retail) P & P 8p. Suitable for P & P 5p. production work and as a general purpose iron.

MODEL CCN 220 volts or 240 volts. The 15 watt miniature model CCN also has neglibible leakage. Test voltage 4000v. A.C. Totally enclosed element in ceramic shaft.

Fitted longlife ironcoated bit 3/32". 4 other bits available 1/8", 3/16", 1/4" and 3/64" PRICE: £2-15 (rec. retail).

MODEL G - 18 watt miniature iron, fitted with long life iron-coated bit 3/32". Voltages 240, 220 or 110. PRICE: £2.15 (rec. retail). P & P 5p.

MODEL C - Miniature 15 watt soldering iron fitted 3/32" ironcoated bit. Many other bits available from 3/64" to 3/16". Voltages 240, 220, 110, 50 or 24. PRICE: £1.93 (rec. retail). P & P 5p.

ST3 Stand - This stand is made from high grade insulation material with a chromium plated strong steel spring. It is suitable for all models and replaces all previous stands. The two sponges at the side which are easily replaceable, serve to keep the soldering bits clean. Spare bits can be accommodated as shown on the illustration.

PRICE: £1.00 (P & P 8p). SAVE 10 PENCE X25 & ST3 or C240 & ST3 for £2.83 (P & P 13p).

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3/32", heat sink, solder, stand

and "How to Solder" booklet,

MODEL MLX KIT Battery-operated 12v. 25 watt iron fitted with 15' lead and 2 heavy clips for connection to car battery. Packed in strong plastic wallet with booklet "How to Solder' PRICE: £2.27 (rec. retail). P & P 12p

	Contains 15 watt	
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bit, 2 spare bits 5/32" and 3/32 heat si solder, s and "Ho Sol bookle PRICE: £2 PRICE: £3-25 (rec. retail), P&P12p (rec. retail) P&P8p.

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MODEL SK.2 KIT

WW-006 FOR FURTHER DETAILS

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Another advanced Hi-Fi stereo tape recorder/amplifier from Philips.

3 heads. Solenoid-operated. Tip-touch controls. 2 x 12 watt RMS amplifier usable with the DC motors switched off. Two built-in loudspeaker enclosures.

This is the N4418, number two in the Philips range of advanced Hi-Fi stereo tape recorders. In producing this range, Philips have drawn on decades of experience in professional tape recording installations for studios, computers and airports the world over.

Each machine easily meets the DIN 45 500 standard for Hi-Fi tape recorders. Sophisticated design gives precise control, simple operation, and great reliability. Here are the main features:

4 tracks. 3 speeds $-7\frac{1}{2}, 3\frac{3}{4}, 1\frac{7}{8}$ ips.

Suitable for stereo and mono recording and playback, multiplay, echo during recording, A-B monitoring.

2 x 12 watt RMS Hi-Fi amplifier usable with recorder's motors and tape transport switched off.

Three motors – two DC motors for reel drive, one DC capstan motor electronically governed to keep tape speed constant.

Tape tension comparators for constant winding torque.

Three magnetic heads – one each for recording, playback and erase.

Detachable lower head cover for easy editing and cleaning.

For control of transport functions and recording mode, illuminated tip-touch controls are linked to solenoids – giving easier, quieter and more reliable operation.

Remote control unit (extra) with

same tip-touch buttons as recorder. Sliding switches for function selection-selected function illuminated. Precise sliding faders for two microphones and another signal source. Recording stand-by (level

adjustable with tape stationary). Two illuminated calibrated VU

type meters for recording/playback.

4-digit counter, zero reset, and on/off Autostop to halt tape at predetermined position.

Sockets for headphones and microphones easily accessible at front, concealed under sliding lid.

Built-in acoustical boxes giving 2×6 watts via $6'' \times 4''$ loudspeakers.

Reels lockable by means of metal hub locks.

Removable transparent lid. Amplifier detachable in one unit leaving recorder functioning.

Frequency response:

40-20,000 Hz at $7\frac{1}{2}$ ips 40-16,000 Hz at $7\frac{1}{2}$ ips with built-in stereo interference filter. 40-15,000 Hz at $3\frac{3}{4}$ ips 60- 8,000 Hz at $1\frac{7}{8}$ ips



a5

Wow and Flutter < 0.15% at 7½ ips. See your Philips dealer for a demonstration. And for a free book on all Philips Hi-Fi stereo tape recorders, write to Philips Electrical Limited, Dept SP, Century House, Shaftesbury Avenue, London WC2H 8AS.

PHILIPS Simply years ahead.



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ANDERS MEANS METERS...

■ New 100° arc high quality meters at

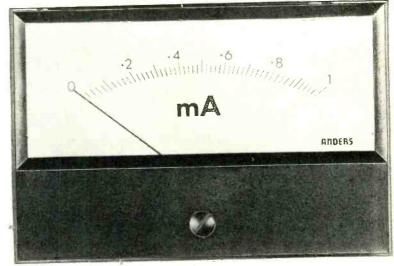
- low prices.
- Rugged taut band construction — pivot and jewel available to order
- Sensitivities to 10 μA

a6

- Very competitively priced for OEM quantities
- Modern styled meters in matt black plastic cases with flattened arc giving long scale.

TWO MODELS R55 2.5in (63.5mm) Scale length R65 3.2in (81.3mm) Scale length

Anders provide what is probably the largest range of meters available from a single source in Europe: MC/MI, dynamometer, vibrating reed, electrostatic, etc. in over 100 case styles and sizes, a few of which are shown below.



Popular models and ranges are stocked in depth while a specially equipped instrument department enables swift production of non-standard ranges and scales, to suit individual customer requirements, in large or small quantities.



Vulcan Moving Iron. 4 models, 1.5", 1.8", 2.7", 3.7" scales. Voltmeters, ammeters and motor starting meters.



Kestrel Clear Front. 7 models, 1:3"—5·25" scales. DC moving coil, AC moving coil rectified, AC moving iron.

Send for fully illustrated catalogue.



Profile 350 edgewise 4·3" scale. DC moving coil and AC moving coil rectified. Horizontal or vertical mounting.



Oxford Long Scale 240°. 2 models, 5.5″, 8″ scales. DC moving coil and AC moving coil rectified.



Models KE1 and KE2 Miniature Edgewise Meters. Nominal scale Jengths 1.2" and 2". Available in sensitivities from 50 microamps Moving Coil.



Stafford Long Scale 240 6 models, 3.5"—11.5" scales. DC moving coil, AC moving coil rectified, AC moving iron. Also 98' scale.



Lancaster Long Scale 240 . 2 models, 4", 5.5" scales. DC moving coil and AC moving coil rectified.

ANDERS ELECTRONICS LIMITED 48/56 Bayham Place, Bayham Street, London, N.W.1. Telephone 01-387 9092.

Manufacturers and distributors of Electrical Measuring Instruments. Sole U.K. distributors of FRAHM Resonant Reed Frequency Meters and Tachometers. Manufacturers of purpose built electrical and electronic equipment to customers requirements.

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it's a good deal more meaningful than most

B & W are not playing hard to get. Far from it. We've appointed – very selectively – a national network of Authorised B & W Dealers to demonstrate, install and service our famous loudspeakers.

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B & W loudspeakers are in great demand abroad. So much so, we have been honoured with the Queens Award to Industry for export achievement.



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WW-009 FOR FURTHER DETAILS

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Contact us at Mullard for all your 'communications' components... components for telecoms, broadcasting, radar and navaids. We have unique resources for their development and production, and have devoted literally millions of pounds to meeting the component needs of manufacturers of

communications equipment. Some of our products are well-established favourites, others are at the forefront of current technology.

Some are made on an extremely large scale, some are customer specials. Please let us know of your own particular requirement.

New tuning and multiplier types announced

Tuning Varactors

Three new silicon varactor diodes, all with a wide electronically tuned capacitance range, have been introduced by Mullard. Designated types BXY53, BXY54 and BXY55, they have total capacitance ratios of 4.0, 6.5 and 7.0 respectively. Typical capacitances at -4V are 1.0, 4.7 and 15pF. Reverse ratings are 60V at 10µA. Low insertion loss, another important feature, is 0.8, 0.5 and 0.25dB for the three types respectively (this is under small signal conditions with the diode at the end of a 50Ω transmission line, and measured at 2GHz for the BXY53 and BXY54,

and at 1GHz for the BXY55).

The new tuner and multiplier varactors come in the same type of standard microwave package.

Multiplier Varactors

Two silicon multiplier varactors have also been announced. These

are high efficiency types BXY56 and BXY57, and are intended for use in both low and high order multiplier circuits with output frequencies in the range 3 to 8GHz. Cut-off frequencies at -6V are 160 and 140 GH₃

respectively. Power ratings are 5.2 and 6.6W, and the reverse rating is 60V for both types. For further information on all five of these new varactors please use reader enquiry

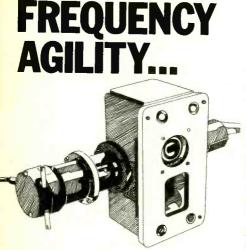
service no. WW 100.

Unique transistors-unique performance

for TV transposer service

The very strict requirements that have to be met by power amplifiers in TV transposers are reflected in the performance that is expected of individual transistors.

Mullard transposer transistors are available which are unique in being designed, specified and guaranteed for this special application. The d.c. safe operating area is exceptionally large compared with earlier types, making for completely safe operation at high powers in class A and ensuring extremely low intermodulation distortion. Furthermore, they are 100% individually tested for intermodulation in the manner prescribed by transposer manufacturers.



...key to improved radar operation An advanced diffusion process is employed in which arsenic is used as an emitter dopant. This allows the

Inpir

U)hall

Radar jamming, both unintentional and deliberate, can be overcome by the use of frequency agile systems. This well-known fact has tended to obscure the many other important advantages which frequency agile radars offer.

They greatly facilitate the detection of fluctuating echoes and so give increased range. They reduce the effects of 'glint', or interference between echoes from different parts of the target, and so enhance tracking accuracy. They provide for decorrelation of the target from clutter. And they completely eliminate early or 'second-time-round' echoes.

The key components for such systems-frequency agile magnetrons and voltage-controlled local oscillators-have been developed by Mullard against the background of a thorough study of fast AFC and related system requirements.

The Mullard magnetrons are spin-tuned, the internal tuning element being rotated via a magnetic depth of diffusion to be yery accurately controlled and a very thin base is obtained giving a minimum f_T of 2GHz. The maintenance of high performance over a long operating life is

assisted by the employment of a sophisticated gold metallisation system.

At 860MHz, the most powerful member of the Mullard transposer transistor family, the BLX98, has a power gain of typically 5.0dB, giving a minimum output of 3.5W with intermodulation distortion better than 60dB. For data on this device please use reader enquiry service no. WW 101.

coupling through the vacuum envelope. A rapid and truly random variation of frequency over the operating band is obtained. A typical 100kW X-band magnetron being made at Mitcham sweeps through 450MHz in 500μ s. Other types can be supplied, including those for J-band, and preset frequency locks can also be provided.

Mullard local oscillators for this type of application are realised in the form of microstrip integrated circuits, and a typical LO comprises a linearised varactor-tuned transistor oscillator multiplier. A salient feature of the device and its control system is, of course, its ability to follow the magnetron's large and rapid frequency variations.

A good introduction to this whole subject is provided by Frequency Agile Radar-a review of techniques and advantages. Write to Dept. CMS/C14 at Mullard House for a free copy.



WHY DO IT THE HARD WAY?

A visitor to our Application Laboratory recently couldn't believe his eyes when we showed him one of our u.h.f. wideband amplifier modules. He held the inch-long pack in the palm of his hand, and it took a demonstration to convince him that it could be taken straight from its wrapping and cover the band 380 to 512MHz without any tuning or 'tweaking up' whatsoever. In fact Mullard u.h.f. modules are completely encapsulated and the question of tuning or trimming simply does not arise.

They have outputs of 2.5, 7.0 and 17W. And if you want to couple them together there are no problems: they all have 50Ω input and output impedances. There are many other features attractive to the equipment designer. They will withstand load mismatch, they will accept input overdrive and they will remain stable even when the supply voltage sinks to 10.5V or rises to 16.5V.

Naturally they cost somewhat more than the sum of the discrete components, but this is more than outweighed by the time you save on design, manufacture and test. All very well for the designer, but also very well for the user and maintenance engineer. For data please use reader enquiry service no WW102.

Latest broadband transistors boost performance of TV distribution systems

The excellent broadband performance of Mullard transistors such as the BFY90 and BFW16A has led to their widespread use in TV aerial amplifier and distribution systems.

These well known types are now being supplemented by a new family which, thanks to an advanced diffusion technology, has an even higher performance. It comprises types BFR90, 91, 92, 93, 94 & 96 which are ideally suited for operation from 40 to 900MHz and give an output of up to 1V across 75Ω . All are individually tested for essential parameters such as intermodulation and crossmodulation distortion.

Using BFR94s, for instance, a push-pull amplifier can be made with a bandwidth of 40 to 300MHz, and featuring 12-channel cross-modulation distortion of only -98dB at an output of 32dBmV. The 3.5GHz transition frequency of the BFR94 results in an amplifier with high power gain and a noise figure which is almost independent of frequency.

For data on transistors in the new family please use reader enquiry service no. WW 103. Don't start designing your next low-level transformer before you've asked yourself....

• Will its operating band fall within the 400Hz to 40MHz range? Am I looking for high permeability? Or low core losses? Would I like the core to be completely selfshielded so that I can pack components around it without worrying about stray coupling? · Do I expect the core to be properly and closely defined magnetically and mechanically?
Would it help to have core, bobbins and hard-

core, bobbins and hardware matched and supplied from the same source? • Does it matter whether the core is easy to wind, assemble and mount?

• Have I to keep an eye on the space available?

• Will I want to get it on a PC board?

• Should I bear the possibility of automatic assembly in mind?

If the answer's 'yes' think Ferroxcube and contact Mullard.

Full data for RM and pot transformer cores is given in the Mullard Technical Handbook (Book 3, Part 2). Use reader enquiry service no. ... for a Handbook order form and descriptive leaflet.

FOUR ADVANCED PLUMBICON[®] TUBES MARK 10TH ANNIVERSARY

Four new Plumbicon tubes, the most advanced yet, are being announced this year, the tenth anniversary of the introduction of this kind of TV camera tube. Plumbicon tubes are now regarded internationally as 'standard'-in fact 90% of the world's colour TV cameras are fitted with them.

The four new tubes are additions to the Mullard 1-inch XQ1080 family. They feature a unique anti-comettail gun and bias light pipe, and antihalation discs are fitted as standard. Output capacitance is low and ensures optimal signal-to-noise ratio.

All four new types have an ex-

*Registered trademark for TV camera tubes

Simpler gigahertz amplifiers with new transistor

A new n-p-n silicon transistor featuring a very high transition frequency and low noise has been announced by Mullard. With a noise figure of 4.0dB at 2GHz and a power gain of 8dB this new device, the 551BFY/A, considerably simplifies u.h.f. and microwave repeater station design.

Broadband amplifiers with centre frequencies of up to 2 or 3GHz can be designed relatively easily by taking advantage of the high gain of the 551BFY/A. With it microwave retended red response and are intended for monochrome and red chrominance channels. The spectral response cut-off of broadcast tube XQ1083 and its industrial counterpart XQ1084 is 900nm. Broadcast tube XQ1085 and its industrial counterpart XQ1086 are of similar construction but have infrared filters giving cut-off at 750nm.



peaters can be made to operate on a 'straight through' basis, there being no need for conversion down to an intermediate frequency.

In radar systems, too, and ultra high-speed data communications systems operating at gigahertz bit rates the 551BFY/A is an extremely attractive device. An interesting military application is in electronic warfare countermeasures where it can replace travelling wave tubes in octave band amplifiers.

The typical transition frequency of the 551BFY/A (at f=500MHz) is 5GHz. V_{CBO} max. is 20V, and I_C max. 25mA. Total permissible power dissipation up to ambient temperatures of 60°C is 300mW. A miniature ceramic encapsulation is used which is compatible with strip-line and microstrip circuits. For data please use reader enquiry service no. WW104.



A GOOD 'BUY IN'

The case for buying in sub-systems or sub-assemblies instead of working with discrete components is not always indisputable. But in many areas there are clear-cut savings to be made on development and production costs and, quite frequently, there are size and performance advantages. The modules for mobile transmitters described in this 'Contact' are a case in point. The microwave field is another.

The Mullard company is particularly well placed for this kind of microwave activity. Not only does it have the resources to design and manufacture microwave sub-systems, it designs and makes the discrete components as well. There is complete vertical integration of the whole activity, and consequent economic and technical advantages.

Much of this Mullard work has in the past involved conventional 'three dimensional' components and waveguide technology, but microwave integrated circuits using microstrip technology are now assuming greater importance.

With the tremendous advances being made in discrete microwave devices, it is not surprising that thin film circuits are more appropriate for many sub-systems. A Gunn diode of micron dimensions, for instance, is incongrous when used with 3cm waveguide plumbing. And with transistors having an f_T of 5GHz allied solid-state techniques must be used for the circuitry.

However, the customer's first need is to know whether a 'subsystem approach' is viable for his particular project. This he can find out by supplying Mullard with a 'black box' specification. A technical appraisal will be prepared and sent to him in about three weeks.





Mullard Limited Mullard House Torrington Place London WC1E 7HD

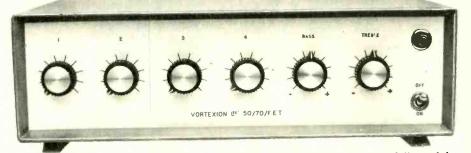
Telephone: 01-580 6633



50/70 WATT ALL SILICON AMPLIFIER WITH BUILT-IN 4-WAY MIXER USING F.E.T.s.

This is a high fidelity amplifier (0.3% intermodulation distortion) using the circuit of our 100% reliable 100 Watt Amplifier with its elaborate protection against short and overload, etc. To this is allied our latest development of F.E.T. Mixer Amplifier, again fully protected against overload and completely free from radio breakthrough.

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The mixer is arranged for 2-30/60 Ω balanced line microphones, 1-HiZ gram input and 1-auxiliary input followed by bass and treble controls. 100 volt balanced line output or 5/15 Ω and 100 volt line.

50/70 WATT ALL SILICON AMPLIFIER WITH BUILT-IN 5-WAY MIXER USING F.E.T.s This is similar to the 4-way version but with 5 inputs and bass cut controls on each of the three low impedance balanced line microphone stages, and a high impedance (10 meg) gram stage with bass and treble controls plus the usual line or tape input. All the input stages are protected against overload by back to back low noise, low intermodulation distortion and freedom from radio breakthrough. A voltage stabilised supply is used for the pre-amplifiers making it independent of mains supply fluctuations and another stabilised supply for the driver stages is arranged to cut off when the output is overloaded or over temperature. The output is 75% efficient and 100V balanced line or 8-16 Ω output are selected by means of a rear panel switch which has a locking plate indicating the output impedance selected. The Mixer section has an additional emitter follower output for driving a slave amplifier, phones or tape recorder, output .3V out on 600 ohms upwards.

100 WATT ALL SILICON AMPLIFIER. A high quality amplifier with 8 ohms-15 ohms or 100 volt line output for A.C. Mains. Protection is given for short and open circuit output over driving and over temperature. Input 0.4V on 100K ohms.

THE 100 WATT MIXER AMPLIFIER with specification as above is here combined with a 4-channel F.E.T. mixer, $2-30/60\Omega$ balanced microphone inputs.1-HiZ gram input and 1-auxiliary input with tone controls and mounted in a standard robust stove enamelled steel case. A stabilised voltage supply feeds the tone controls and pre amps, compensating for a mains voltage drop of over 25% and the output transistor biasing compensates for a wide range of voltage and temperature. Also available in rack panel form.

CP50 AMPLIFIER. An all silicon transistor 50 watt amplifier for mains and 12 volt battery operation, charging its own battery and automatically going to battery if mains fail. Protected inputs, and overload and short circuit protected outputs for 8 ohms-15 ohms and 100 volt line. Bass and treble controls fitted.

Models available with 1 gram and 2 low mic. inputs, 1 gram and 3 low mic. inputs or 4 low mic. inputs.

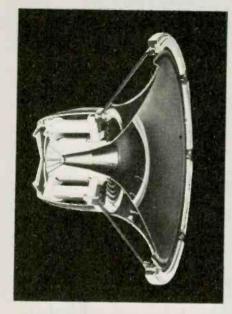
200 WATT AMPLIFIER. Can deliver its full audio power at any frequency in the range of 30 c/s-20 Kc/s \pm 1 dB. Less than 0.2% distortion at 1 Kc/s. Can be used to drive mechanical devices for which power is over 120 watt on continuous sine wave. Input 1 mW 600 ohms. Output 100-120V or 200-240V. Additional matching transformers for other impedances are available.

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VORTEXION LIMITED, 257-263 The Broadway, Wimbledon, S.W.19 1SF Telegrams: "Vortexion, London S.W.19"

Telephone: 01-542 2814 and 01-542 6242/3/4





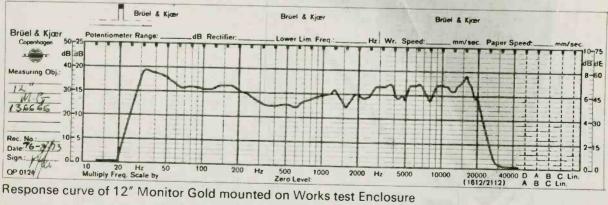
ABRIDGED MONITOR GOLD TECHNICAL SPECIFICATION

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Every Tannoy "Monitor Gold" dualconcentric loudspeaker is individually tested and given its own serial number. Every "Monitor-Gold" has a frequency curve taken on Brüel & Kjaer measuring equipment, and a copy of this curve will, in future, be provided with every unit.

		T	1
	10″	12″	15″
Power Handling Capacity	25W	35W	50W
Frequency Response	27-20,000 HZ	25-20,000 HZ	23-20,000 HŻ
Intermodulation Products	less than 2%	less than 2%	less than 2%
Impedance via Crossover network	8 ohms (5 ohms min.)	8 ohms (5 ohms min.)	8 ohms (5 ohms min.)

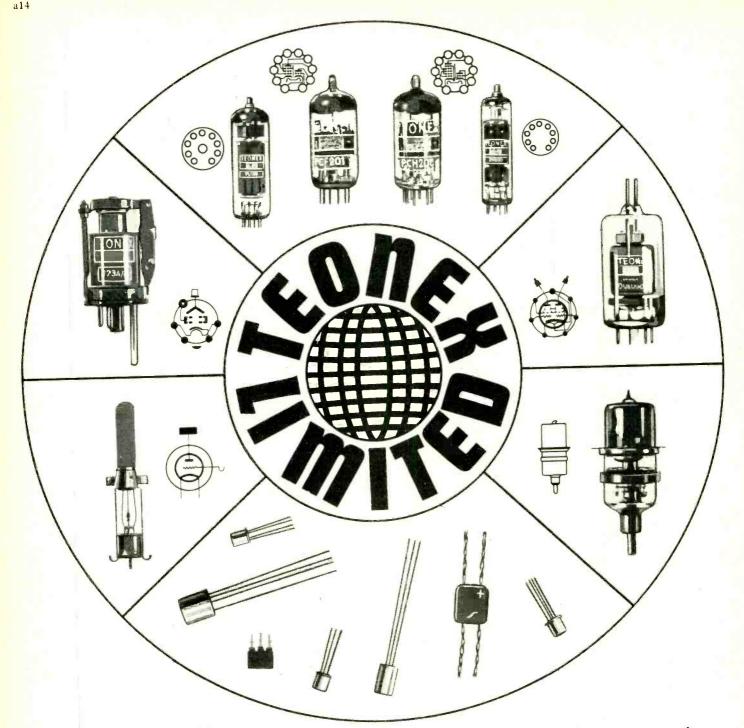
The whole range of Tannoy Dual-Concentric units sounds very similar, depending on the selected enclosure, and the different types are ideal for combinations in Quadraphonic systems.



Norwood Road, West Norwood, London SE27 9AB Tel: 01-670 1131



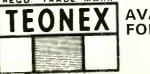
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Wireless World, November 1973

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For the attention of Mr____

Company name and address_



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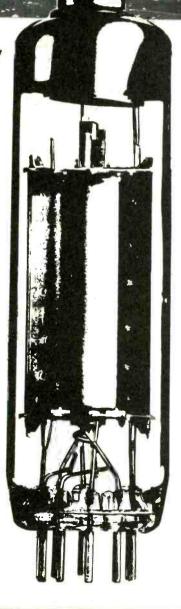
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SHIBADENS NEW TIME LAPSE RECORDE A single VTR that brings maximum FLEXIBILITY to any application

Shibadens new Time Lapse Recorder mixes and matches recording and playback times so that whatever your requirement you can get the complete answer with this versatile new VTR unit. The SV 612 E (K) will shorten one recording and lengthen another or vice versa. And however you use the Recorder – for Traffic Systems, the study of nervous diseases, sporting events or to improve security – no matter what the mode, you will not be troubled with tape compatibility, because the SK 612 E (K) uses tapes on any EIA-J type I format VTR.

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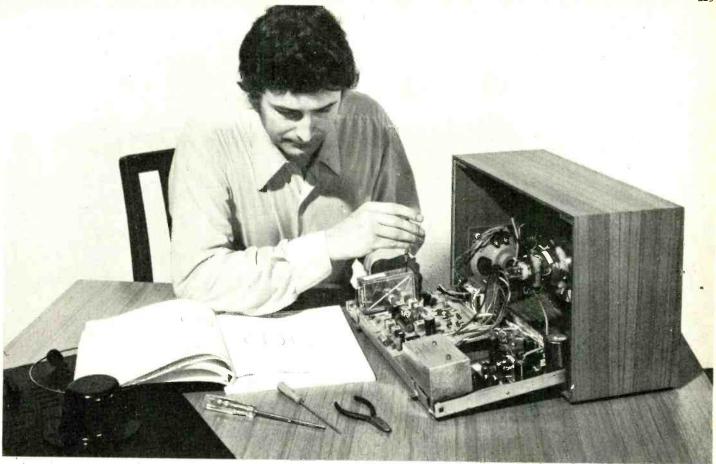
Slewing rate:200 mm/secSensitivity:50µV/cm - 500 mV/cm [with pre-amplifier]Speeds:1, 2, 5, 10, 20 sec/cm, 1, 2, 5, 10 min/cmPaper size:270 mm wide [DIN 16230]Paper drive:Digitally controlled stepper motorPen type:Ballpoint, fibre tip, capillaryPen drive:Infinite resolution d.c. potentiometric servo

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Learn about modern TV design by building this

The new Heathkit GR-9900 portable 12" UHF Monochrome Television kit. A unique chance to double the pleasure available from any other television set because you build this yourself.

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The GR-9900 is portable too-equally at home on

the mains or off your 12 volt battery for car, boat or caravan use. Add to this Heath's world renowned experience in the design of equipment for first-time kit builders, and you will be impressed on all counts of engineering, styling, and performance.

The instruction manual is surprisingly simple with big, clear illustrations to map out your way. Would-be TV engineer? Here's your chance to learn—by actually building a television yourself. The manual not only shows you how to get 100% personalised quality control on your own; in the event of anything going wrong, a Trouble-Shooting section enables you to find the fault and, in most cases, to put it right unaided.

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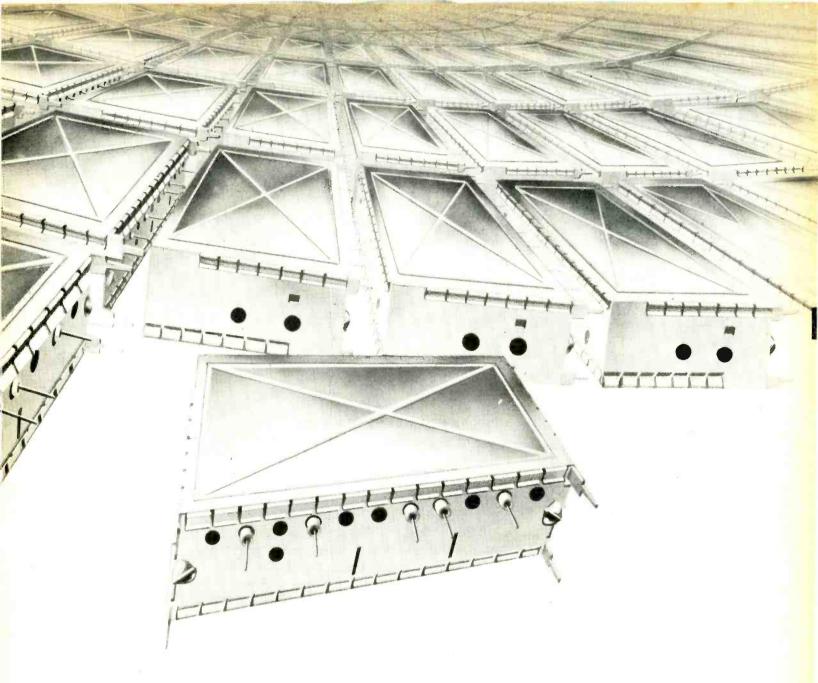


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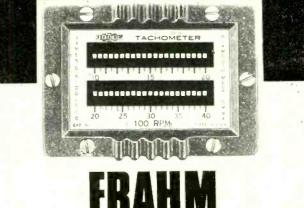


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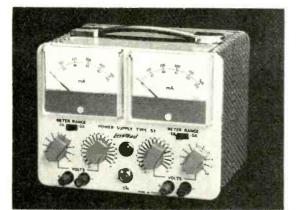
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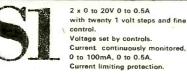
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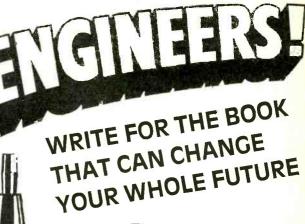






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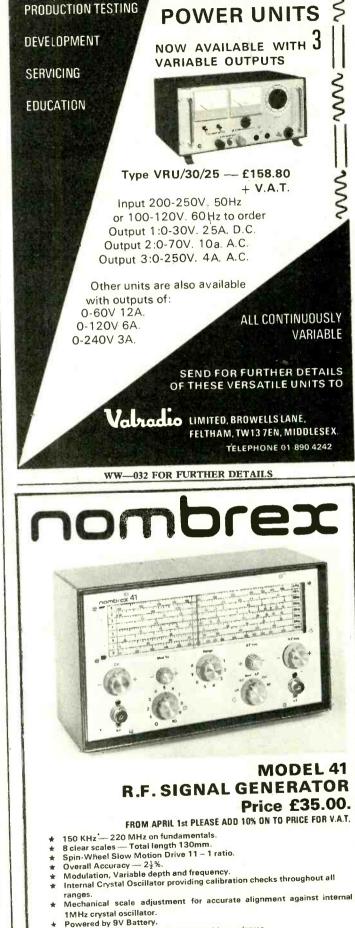
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A good cartridge should take from a record all the subtle shades of original sound that are stored there, and re-create them for your enjoyment. The Practice is a little more difficult.

Now Goldring bring the ideal closer with the new 820 series.

A brand new family of cartridges that builds on the advances already achieved by the Goldring 800 series. Providing cartridges that are not only capable of making the most of all that good recording can offer now, but have the capacity to keep pace with new developments in the art of quality recordings. The 820 series retains the true transparency of

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The 820 - one of the models in the new range. Performance characteristics: Sensitivity @ 5 cm/sec-1Khz:5mV. Separation @ 1 Khz:20dB Recommended playing wi 2 grammes Stylus point radius: .0006" 154 Frequency range: 20hz-20Khz.

It brings advances in every aspect of design.

The small low-mass diamond point which is mounted on a new type of specially polished lightweight aluminium tube, combined with the new visco-elastic material used for the pivot pad, makes for greater

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The total effect is a cartridge that, other equipment being equal, can narrow almost to vanishing point the difference between the original recording and the sound that comes out of your speakers.

There are three models in the range. The 820 with spherical stylus. The 820E and 820 Super E, both with bi-radial styli. Write for details and full specifications. And satisfy yourself that 'what goes in comes out'.

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The new 820 series

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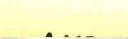
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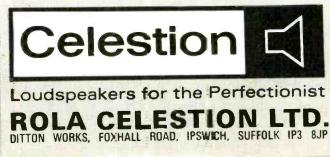
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Ditton 66 Studio Monitor



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A new Loudspeaker of advanced design suitable for studio use and for home installations of the highest qua ity. UNITS: HF 2000 (dome 'pressure' type) MF 500 (Mid-range Dome 'pressure' type) Ultra linear 12" bass driver and 12" ABR. The crossover has resulted from considerable research and crossover points are at 500 Hz and 5000 Hz 80 Watts Maximum, 4-8 ohm. This monitor loudspeaker system has an exceptionally wide and flat frequency response. Very low order harmonic and inter-modulation distortion. Precise response to transients. Beaut fully maintained polar response ensures absence of unwanted directional effects and provides a highly satisfactory stereo image throughout the listening area. Matchec pairs. SIZE 40 × 15 × 11 Natural Teak or Walnut Cabinet



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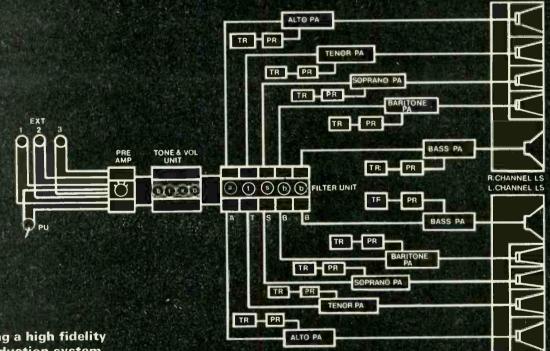
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Power Controlled Soldering

System Type PC/1

When not in use the iron can be safely left in the easy-location spring holder. In the event of a fault in the iron, the unit is protected from damage by the output fuse.

The signal lamp on top of the power unit shows when power is on, and varies in intensity with power setting.

Specially designed low-voltage power supply unit built into the bench stand base. The output power to the iron is controlled by a transistor circuit and is completely free of sharp transients, R.F.1 etc. which could causedamage to semi-conductors. bit. The wiping sponge is mounted on the top of the power unit just where it is needed.

Reliable joints need a clean

The iron is connected to the power unit by a 3-core lead fitted with a 3-way nonreversible plug, which mates with a matching socket on the power unit.

The power being fed to the iron is regulated from 6 watts (approx. 200° C) to 25 watts (approx. 450° C) by simply rotating one control on the front of the power unit.

The long-life, thermally efficient element is fully protected from physical damage by being enclosed in the stainless steel shaft. The low voltage, transient free D.C. element supply ensures absolute safety for both operators and sensitive components: no induced or leakage voltages can be present at the bit. As an additional safety measure the element shaft is earthed (the earth can easily disconnect if the bit and element shaft are required to 'float'). The element unit can be replaced simply at low cost when necessary.

A wide range of non-seize, fully slotted bits are available in both plain copper and iron-coated 'long life' types. The handle of the iron is specially designed to provide ease of handling and maximum operator comfort and efficiency. The virtually unbreakable one piece nylon moulding remains cool even after prolonged production line use at maximum power. The light weight and perfect balance of the PC/1 iron make rapid and accurate soldering almost automatic.

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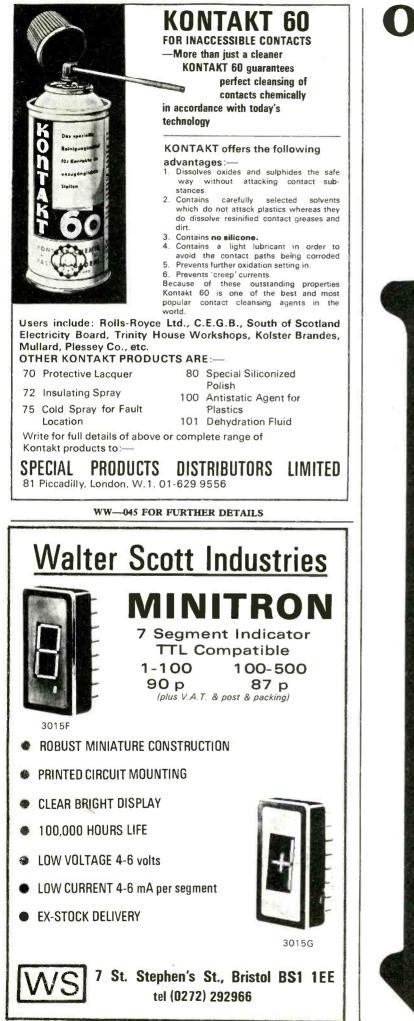
YATES ELECTRONICS (FLITWICK) LTD. DEPT. WW ELSTOW STORAGE DEPO KEMPSTON HARDWICK BEDFORD	Catalogue which contains data sheets for most of the
RESISTORS W Iskra high stability carbon film—very low noise—capless construction. $\frac{1}{2}$ W Mullard CR25 carbon film—very small body size 7.5 x 2.5 mm. $\frac{1}{2}$ W 2% ELECTROSIL TRS. Power Values watts Tolerance Range available I-99 100+ $\frac{1}{2}$ 10% 4.7Ω-2.2MΩ E24 1p 0.8p $\frac{1}{2}$ 10% 1Ω-3.9Ω E12 1p 0.8p $\frac{1}{2}$ 2% 10Ω-1MΩ E24 3.5p 3p $\frac{1}{2}$ 10% 1Ω-3.9Ω E12 1p 0.8p $\frac{1}{2}$ 10% 1Ω-3.9Ω E12 1p 0.8p $\frac{1}{2}$ 2% 1Ω-0HΩ E12 1p 0.8p $\frac{1}{2}$ 2% 5% 4.7Ω-1MΩ E12 1p 0.8p $\frac{1}{2}$ 2% 5% 5% 5% 5% 5% 5% 5% 5% 5% 5% 5% 5% 5%	MULLARD POLYESTER CAPACITORS C296 SERIES 400V: 0:001μF, 0:0015μF, 0:0022μF, 0:0033μF, 0:0047μF, 2½p. 0:0068μF, 0:01μF, 0:015μF, 0:022μF, 0:033μF, 3p. 0:047μF, 0:068μF, 0:1μF, 4p. 0:15μF, 6p. 0:22μF, 7½p. 0:33μF, 11p. 0:47μF, 13p. 160V: 0:01μF, 0:015μF, 0:022μF, 0:033μF, 0:047μF, 0:068μF, 3p.1μF, 33p. 160V: 0:01μF, 0:015μF, 0:022μF, 0:033μF, 0:047μF, 0:068μF, 3p.1μF, 33p. 160V: 0:01μF, 0:015μF, 0:022μF, 73p. 0:68μF, 11p. 1:0μF, 13p. MULLARD POLYESTER CAPACITORS C280 SERIES 250V P.C. mounting: 0:01μF, 0:015μF, 0:022μF, 3p. 0:033μF, 0:047μF, 0:068μF, 11p. 1:0μF, 13p. 0:1μF, 4p. 0:15μF, 0:22μF, 5p. 0:33μF, 6½p. 0:47μF, 83p. 0:68μF, 11p. 1:0μF, 13p. 1:5μF, 20p. 2:2μF, 24p. MYLAR FILM CAPACITORS 100V 0:01μF, 0:005μF, 0:01μF, 0:02μF, 3p. 0:01μF, 0:05μF, 0:068μF, 0:1μF, 3½p. 1:00pF to 10,000pF, 2p each.
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$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	LARGE (CAN) ELECTROLYTICS 1600µF 64V 74p 2500µF 64V 80p 4500µF 16V 50p 2500µF 40V 74p 2800µF 16V 50p 5000µF 50V £1.68 2500µF 50V 58p 3200µF 16V 50p 5000µF 50V £1.10 HIGH VOLTAGE TUBULAR CAPACITORS—1,000 VOLT 0.01µF 10p 0.047µF 13p 0.22µF 20p 0.022µF 12p 0.1µF 13p 0.47µF 22p POLYSTYRENE CAPACITORS 160V 22% 10pF to 1,000pF E12 Series Values, 4p each. SMOKE AND COMBUSTIBLE GAS DETECTOR—GDI The GDI is the world's first semiconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical resistance when it absorbs deoxidizing or combustible gases such as hydrogen, carbon monoxide methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke This decrease is usually large enough to be utilized without amplification. Full details and circuits are supplied with each detector. Detector GDI, £1. Kit of parts for detectors including GDI and P.C. board but excluding case. Mains operated detector £5:20. 12 or 24V battery operated audible alarm £7:30 As above for PP9 battery, £6:40. PRINTED BOARD MARKER 97p Draw the planned circuit on to a copper laminate board with the P.C. Pen, allow to dry and immerse the board in the etchant. On removal the circuit remains in high relief

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7400	18	16	14	3 745	18	16	14	13	74141	100	95	90	85
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7402	18	16	14	13 7454	18	16	14	13	74150	330	280	250	220
7403	18	16	14	3 7460	18	16	14	13	74151	110	100	95	89
7404	20	18	16	14 7470	30	28	25	24	74153	120	110	105	95
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7406	50	45	40	35 7473	40	38	36	30	74155	150	120	100	86
7407	56	50	44	38 7474	40	36	32	28	74156	130	120	100	96
7408	36	30	27	23 7475	55	52	50	49	74180	155	136	112	105
7409	36	30	27	33 7476	40	36	32	30 85	74190	195	190	185	180
7410	18	16	14	13 7480	100	95	90	85	74191	195	190	185	180
7411	23	21	20	8 7481	125	115	110	105	74192	200	190	180	164
7412	36	30	27	23 7482	100	96	90	85	74193	200	180	170	150
7413	34	28	26	22 7483	100	97	95	92	74196	200	190	180	170
7416	45	43	39	34 7484	120	115	110	105	74197	200	195	100	170
7420	18	10	14	13 7485	250	245	240	230		_		-	
7421	36	30 29	27	23 7486	45	42 67	37	33 52		1	LINEAR IC	's	
7426	32	29	23	20 7490			60 85	79	709		14 pin DIL	-	40p
7430	20	18	16 32	14 7491A 28 7492	100	92 70	05	60	741		8 pin DIL		40p
7432	40	30			75	68	60	52	74		14 pin DIL		38p
7440	20 80	18 75	16 70	14 7493 65 7494	95	90	00	80	723		14 pin DIL 14 pin DIL		95p
7441 7442	80	75	70	65 7494 65 7495	105	100	95	90	747		14 pin DIL		85p
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7447	175	165	150	120 74100	250	240	235	230	DIL sockets		14 pin and	l6 pin	16p
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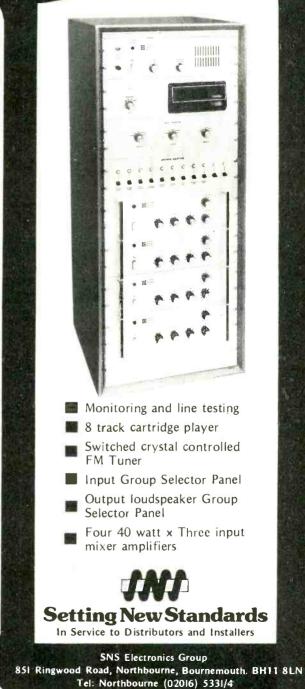
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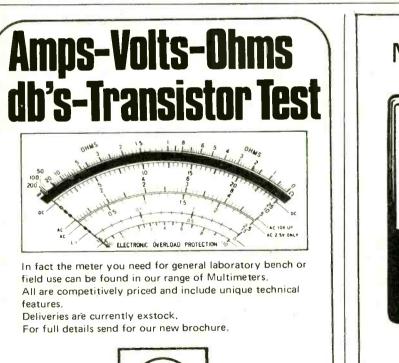
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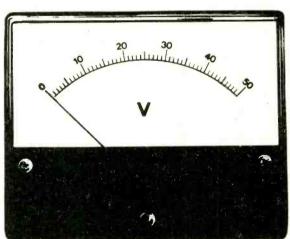
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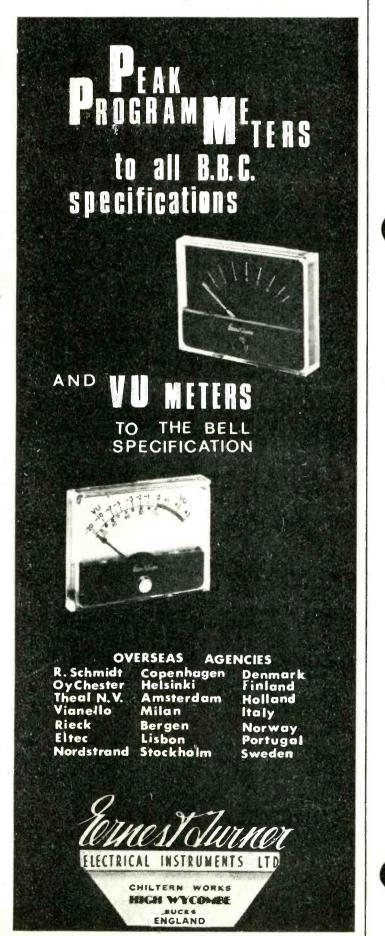
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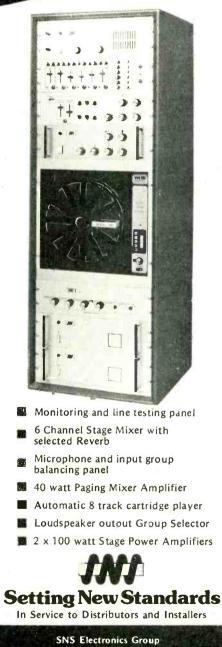
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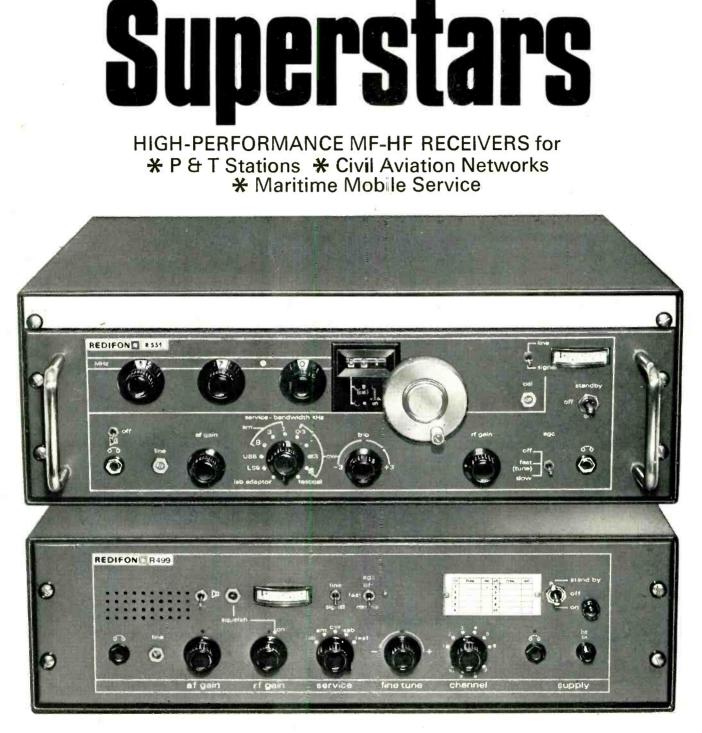
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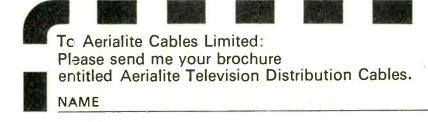
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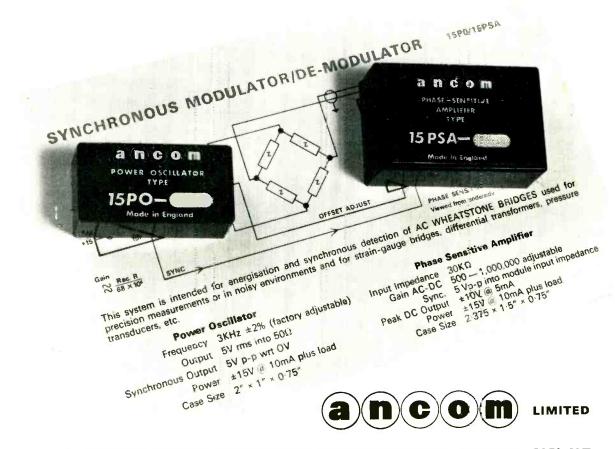
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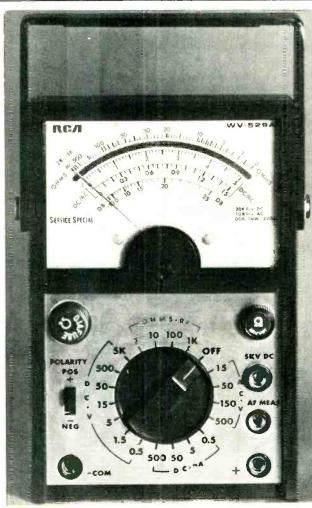


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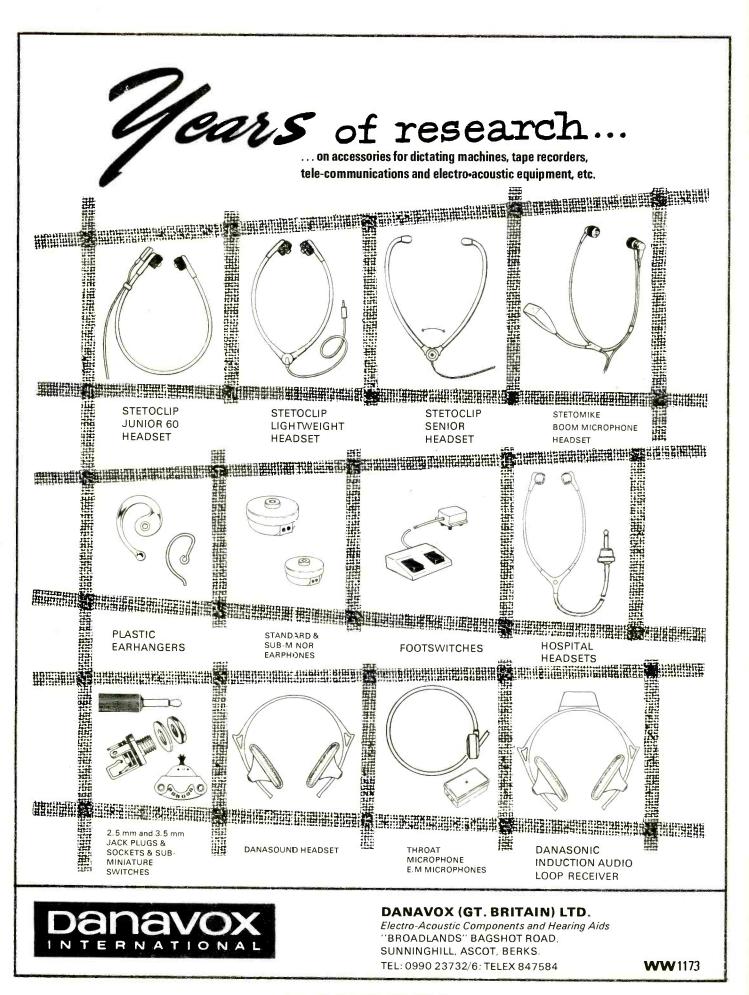
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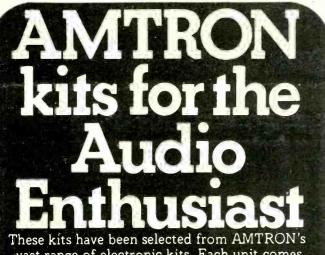
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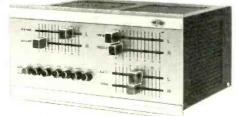


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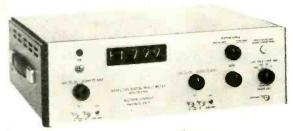
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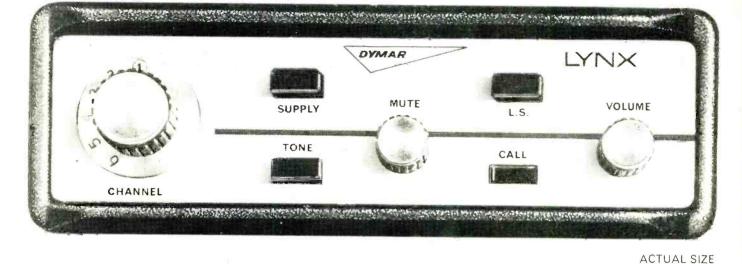


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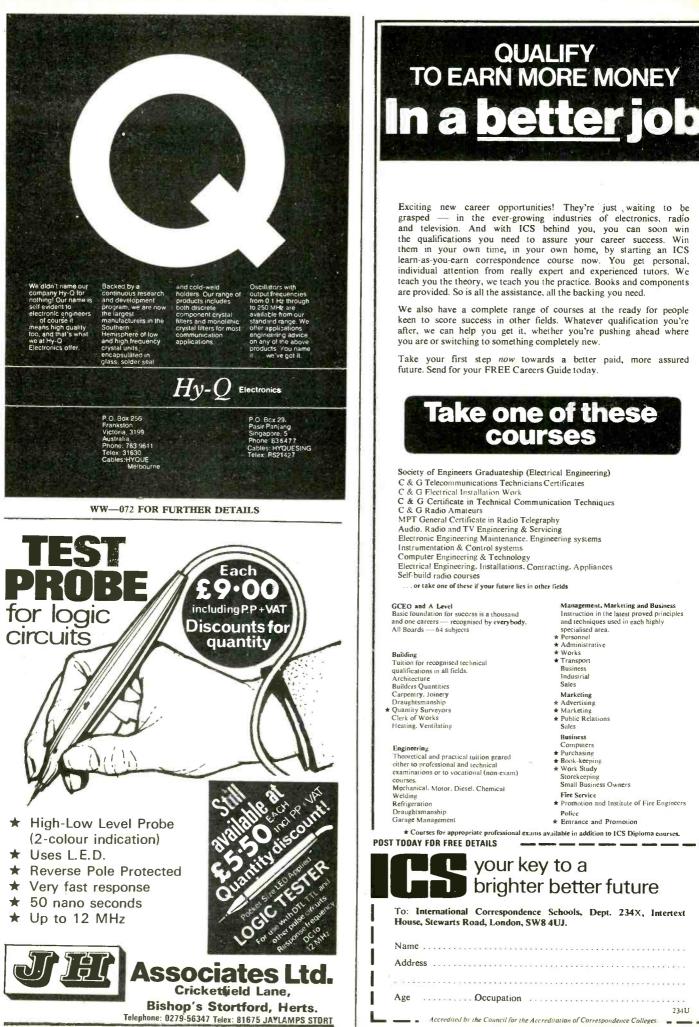
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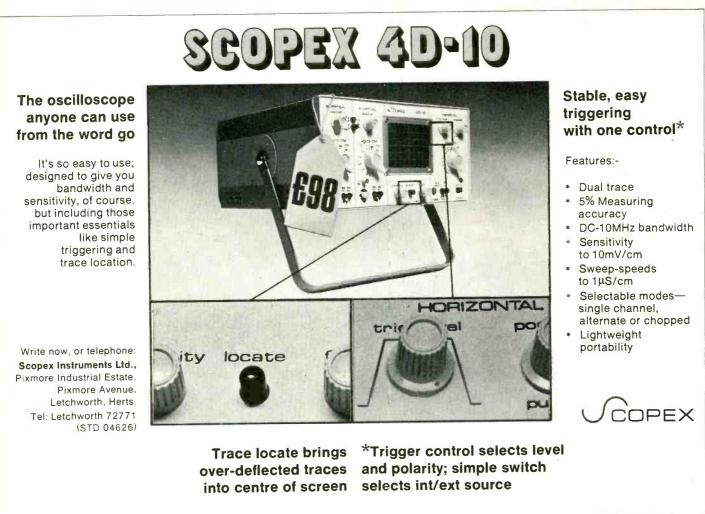
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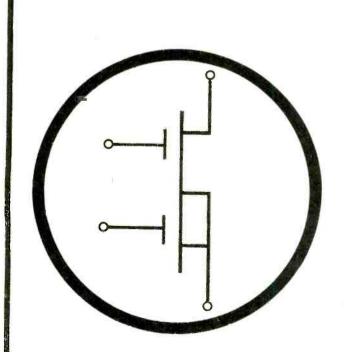
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Wireless World, November 1973





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KWP/BL139

WW-077 FOR FURTHER DETAILS

REALISM IN SOUND FOR The home constructor

During the past 10 years, loudspeaker technology has advanced to a degree that it is no longer possible for the amateur to design and build a loudspeaker which matches the performance of a high quality commercial product. At one time, building a loudspeaker was simply putting a full range drive unit in a box of suitable size and shape. By present-day standards, a full range loudspeaker drive unit can no longer be considered in the high fidelity class.

The high fidelity loudspeaker started with the introduction of two-way systems, comprising bass and high-frequency drivers, and a simple frequency-dividing network. The dividing network was generally a coil in series with the bass driver, and a capacitor in series with the high-frequency driver. Although little attempt was made to ensure crossover at the best point in the frequency range, or the integration in respect of sensitivity, this was a considerable improvement over most single drive unit loudspeakers. It became apparent later, however, that the weaknesses of the single drive unit loudspeaker were still inherent to a degree in the two-unit system in respect of adequate frequency coverage. The relatively large and heavy diaphragm required for satisfactory bass response produces a poor performance above 1 kHz, and a high-frequency unit designed to have a satisfactory response to 15/20kHz is unsatisfactory below 3kHz. Most large bass drivers have a high-frequency resonance between 1kHz and 2kHz. The low-frequency resonance of high-frequency drivers is between 1kHz and 3kHz. These resonances produce transient colouration and an irregular response characteristic in the most important part of the total frequency spectrum. Optimum performance requirements thus necessitate the use of three or more drive units together with a sophisticated frequency dividing and integrating networks.

At the time of the introduction of multi-unit systems (between 1960 and 1965) drive unit design had not developed sufficiently to make it possible to produce a loudspeaker system covering the whole frequency range from 40Hz to 20kHz with a satisfactory angle of radiation using three drive units, and four-unit systems were common. Frequency crossover points were approximately 500Hz, 4kHz and 10kHz. With the introduction of the dome high-frequency driver and improvements in the mid-range driver, it is now possible to produce a three-unit system having a better performance than the four-unit system, using crossover frequencies of approximately 500Hz and 5kHz.

Drive unit design has now reached a very advanced state. The response characteristic obtainable is virtually flat over the desired range, in that the small variations, as measured, cannot be detected by any form of listening test. The greatest advance in recent years, however, has been the elimination of transient colouration due to standing waves on the diaphragm. Recent drivers have been designed on the concept of a transmission line to ensure perfect matching from the driving force at the coil to the terminating surround, thereby eliminating the source of termination reflections.

Recent further research by Arthur Radford has shown that the colouration which still exists in the finest forward facing (90° angle radiation) loudspeakers is due to standing wave generation between the radiation boundaries. It can be demonstrated that transient colouration is a function of the radiation angle at mid- and high-frequencies, and the wider the radiation angle the greater is the realism.

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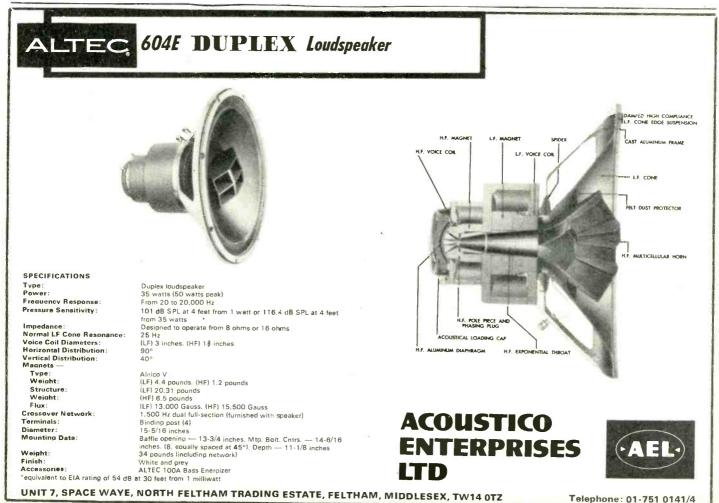
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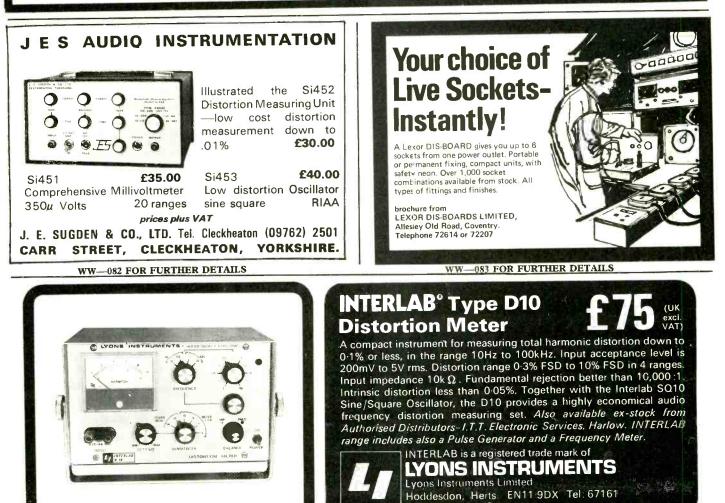
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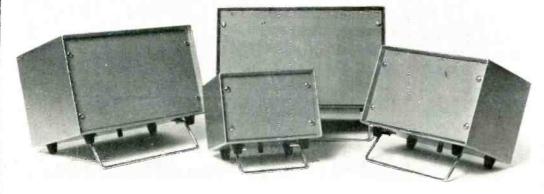
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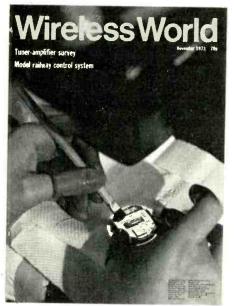
Wireless World

Electronics, Television, Radio, Audio

Sixty-third year of publication

November 1973

Volume 79 Number 1457



This month's cover picture shows the sealing in of the "works" of a digital wristwatch, including a Monsanto l.e.d. display seen as the dark rectangle in the middle.

In our next issue

(publication date November 19)

Active filters used with loudspeakers can provide greater flexibility and overcome inherent disadvantages of the passive crossover network.

Using opto-couplers. An investigation into the noise behaviour of these devices used in conjunction with transistors.



I.P.C. Electrical-Electronic Press Ltd Managing Director: George Fowkes Administration Director: George H. Mansell Publisher: Gordon Henderson

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Brief extracts or comments are allowed provided acknowledgement to the journal is given.

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Integrated Circuits in the U.K.

About six years ago we took a look at the British integrated circuits industry (Leader, Dec. 1967) and declared that 1968 may well be remembered as the year in which "the British electronics industry finally kept its national identity or became predominantly American controlled". This of course referred to control of equipment design through control of the design and marketing of integrated circuits. In fact there was not a particular critical year in which everything happened, but since 1968 we have seen the American and other foreign companies progressively increasing their hold over the U.K. integrated circuits market, until now the British i.c. manufacturers jointly have only 10-15 per cent of the market. In 1968 there were six wholly British-owned i.c. firms in operation; now there are only three, Ferranti, G.E.C. and Plessey. The greater part of the i.cs used by British equipment manufacturers is imported from about 18 American companies (led by Texas, Motorola, Fairchild, National Semiconductor and Signetics) and four European owned companies (the Philips group — which has Mullard in the U.K. Valvo in Germany and R.T.C. in France — and Siemens, SGS-ATES and SESCOSEM).

What happened after 1968 was a period of over-production of i.cs and a worldwide price war, resulting from the 1970-71 depression in trade, which caused the prices of i.cs to fall from pounds to pence. The British firms were unable to compete and only the large American companies were able to sustain the low prices. The duplication of effort on such things as the 7400 series of devices did not help matters.

There was one development after 1968, however, which we hinted would help the British i.e. industry and which did in fact take place. This was the increase in demand from equipment manufacturers for special i.es, tailor-made for particular applications — as distinct from "off-the-shelf" devices. This type of product requires close cooperation between the i.e. and equipment makers, and in Britain this obviously works best when both parties are British, since discussions on whether to manufacture the i.es do not have to be referred back to headquarters in some other country. It is for this kind of operation that the Government, through the D.T.I., is helping financially to support a research and development programme — up to £10m spread over 6-7 years. There may be additional, but probably smaller, support from the Ministry of Defence.

The trouble is that this kind of money will not go very far in present conditions. Such is the rate at which integrated circuit technology is changing — complete new classes of device appearing every few months — that any manufacturer needs a continuous injection of money into research and development just in order to stay in the race, let alone moving ahead of his competitors.

Now that we are in the Common Market it may seem inappropriate to show concern for the fate of a particular industry in a particular country: after all, we are all Europeans now. But the fact remains that our national standard of living still depends on the performance of our national manufacturing industries. Maybe we can still live by exporting woollen goods and Scotch whisky, but to neglect the huge potentialities of the world electronics market — which is expected to reach an annual £40,000m by about 1980 — is one way of helping the British to become what has already been suggested, "the peasants of Europe".

Model Railway Control System

A two-rail layout fitted with working whistle, speed control and coach interior illumination.

by P. Cowan

The system of model train control to be described is such that any chosen function does not interact with nor is dependent on any other function. No interconnections of rolling stock are necessary. Highfrequency a.c. is not used, removing problems in connection with interference. All commands are operable from a trackside controller and no sequential actions are necessary.

The system uses d.c. levels for each function and in the case of the locomotive the level is switched with deliberately slow (0.2-0.5ms) rising and falling edges at 100Hz, each piece of rolling-stock and the locomotive being fitted with a simple "level sensor". The "inertia" of the system is such that the slow rising and falling edges are not evident in practice except in that they remove interference with other apparatus — a problem which is evident when high frequency a.c. is applied to a model railway layout. The use of d.c. levels enables quite high powers to be transmitted down the rails without having to resort to tuned filters and/or large capacitors. The circuits are also easy to make and set up.

Fig. 1 shows a typical train movement. Here, the whistle is allocated 3V, the lights 6V and the locomotive 12V. Initially, with a complete train at rest and all functions off at T = 0, the whistle is sounded (a). At (b) the train moves off slowly with whistle still on and at (c) the whistle is turned off and the train continues moving forward slowly. At (d) the driver turns on the coach lights (the train still moving forward slowly), at (e) the whistle is sounded, coach lights are on and the train is picking up speed. At (f) the whistle is off, the locomotive and train are coasting, leaving only the lights turned on.

In practice it is better to arrange for the "voltage separation per function" to increase with increasing current demand from the train to make an allowance for volts dropped down the rails as the train moves away from the power connection point. The system described has worked without trouble on a Club layout 35 feet by 10 feet, including several points and crossovers with attendant contacts.

The power diagram in Fig.2 shows how the voltage separation per function is arranged in the practical controller cir-

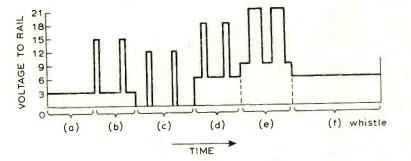


Fig. 1. A complete train movement, showing all functions operating.

cuit and details of each function's operating voltage. It can be seen that each function operates over a particular range of voltage about a correct voltage level, allowing for volts dropped down the rails and, within limits, keeping the system in sync. For example, the whistle operates at 19.5V when blown with the loco running but will still work correctly down to 16V, giving 3.5V safety margin. Fig. 2 also shows the voltage levels that each sensor must accept; and those that are to be rejected, together with details of the output current that the controller must supply.

Circuit description

Power supply (controller). Unregulated d.c. is derived from the a.c. mains by the transformer, the bridge rectifier and C_1 in Fig.3. Transistors Tr_{11} , Tr_{12} , Tr_{9} and Tr_{10} , D_{2-4} and Z_{3-6} form a simple regulator of output voltage according to the selected diodes: C_9 and C_{10} suppress any tendency to oscillate and C_8 and C_{11} control the rise and fall times of the pulsed supply. A further regulated supply line (12V) is provided by Z_1, R_3 and C_2 to power the pulse generator which is made up of Tr_{1-3} as a ramp generator, and Tr_6 and Tr_7 as a Schmitt trigger, R_{76} controlling the mark/space ratio at the output. Transistors Tr_4 and Tr_5 and their attendant components enable autorun-up to full speed and auto-rundown to stop to be selected via S_1 or S_2 respectively. Components S_3 and Z_2 form a "skid" control enabling momentary full power to be applied. A fast overload trip to safeguard the controller and associated circuitry is formed by Th_1 , R_1 and R_{75} , D_1 , L_2 and R_{32} . The action of overload is indicated by Lp_2 . The trip should be set to not less than 5A by R_{75} . Components

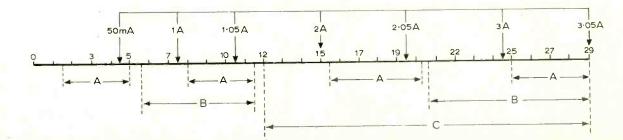
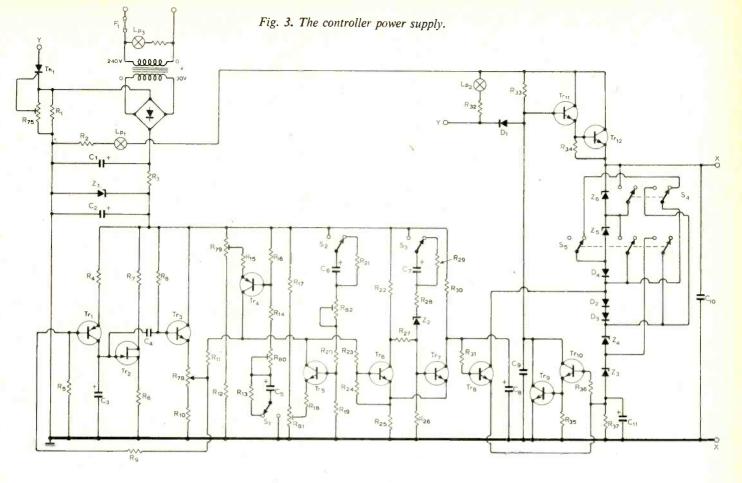


Fig. 2. Switching points recognized by the sensors of the whistle (A), the lights (B) and the locomotive motor (C).



 R_{80} and R_{82} are delay run up and down adjustments and are fitted to the front panel of the controller as are S_1 , S_2 , S_3 , S_4 , and S_5 . Switch S_4 is a a ganged micro-switch and is the whistle on/off. Switch S_5 is a 3-pole change-over rotary switch operating the lights. Transistor Tr_{12} should be fitted to a heat sink of the standard finned type (6in imes $4\frac{1}{2}$ in) with eight $1\frac{1}{2}$ in longitudinal fins. The resistor R₉ causes a slight shift in frequency from approximately 100Hz to 120Hz as loco power output is increased, which can be used to give diesel locomotives an exhaust rate effect.

Lamps (coach illumination). From Fig.2 it can be seen that the coach sensor should be able to command "lights on" from 5.5 to 11.5V. This is accomplished by Tr_{14} , R_{42} , Tr_{16} and Z_8 , in Fig. 4, the biasing of Tr_{14} being set by R_{76} , R_{43} , Z_7 and R_{41} . Turn off at 11.5V is done by Tr_{13} , biased by R_{38} , R_{39} and Z_{17} . Further reference to Fig.2 shows that lights should be on again at 21.5V (to maximum voltage of 29.5V), and this is done by Tr_{15} and R_{43} through biasing components R_{77} , R_{44} and Z_9 .

Whistle sensing and regulation circuit. This circuit, shown in Fig. 5, is similar in principle to the "lights" circuit, the correct "turn on whistle" voltages being sensed by Tr_{18} , Tr_{20} , Tr_{23} , and Tr_{26} and the "turn off whistle" voltages by Tr_{17} , Tr_{22} and Tr_{24} , The regulation of the supply to the "whistle" is achieved by dropping excess voltages across R_{50} , R_{63} and R_{64} . Components

marked with an asterisk may require small adjustments to allow for component tolerances and to achieve the correct turn on and off values as detailed in Fig. 2.

Whistle. The circuit is that of an astable multivibrator with the drive waveform to the whistle suitably "adjusted" to make the sound from the Dictaphone earpiece sound like a "whistle". If an earpiece is unobtainable a 10Ω portable radio earpiece can be used instead.

Locomotion circuit. In this circuit (Fig. 6) care has to be taken to ensure that Tr_{28} and Tr_{31} are able to dissipate heat, prefererably through the locomotive chassis.

In practice, about 6W under full load conditions and 4.5W nominal are dissipated. The average locomotive chassis is usually more than adequate and is often even painted matt black; Hornby and Trix tender drive locomotives have been modified quite successfully. In the case of the tender drive types the power transistors Tr_{28} and Tr_{31} were mounted on the tender chassis with the rest of the circuitry built round the propulsion motor, the whistle and sensor being mounted within the locomotive body. In addition to sensing the locomotion voltage level this circuit has to work with either polarity applied. With positive on the earth rail then Tr_{27,28,29}, etc are isolated by diodes D_{13} and D_{14} .

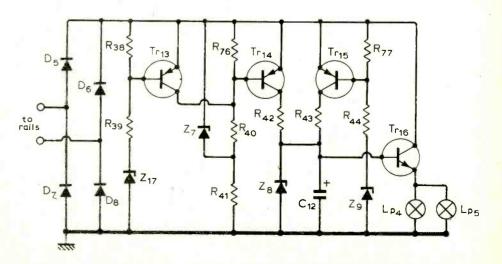


Fig. 4. Circuit diagram of the coach lights controller.

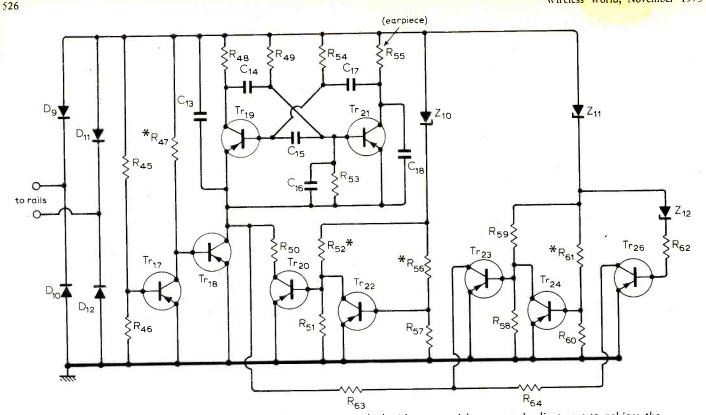


Fig. 5. Whistle level sensing and regulation circuit. Components marked with an asterisk may need adjustment to achieve the the correct switching levels.

the correct switching tereis.					
Component list					
Resis					
R_{\perp}	0.5Ω 5W	R_{42}	100Ω		
R_2	470Ω 2W	R_{43}	100Ω		
R_3	680Ω 2W	R_{44}	$(18-27k\Omega)$		
R_4	270Ω	R_{45}	$8.2k\Omega$		
$R_{\rm s}$	3.3MΩ	R_{46}	$1.5 \mathrm{k}\Omega$		
R_6	10Ω	R_{47}	$(2.7k\Omega \frac{1}{4}W)$		
R_{γ}	100Ω	R_{48}	<u>39</u> Ω		
Rs	180kΩ	R 49	$2.2k\Omega$		
<i>R</i> ,	$2.2M\Omega$	R_{50}	$100\Omega \frac{1}{2}W$		
R_{10}	1.8kΩ	R_{51}	$2.2k\Omega$		
R_{11}	$22k\Omega$	R_{52}	$(470\Omega \frac{1}{2}W)$		
R_{12}	lkΩ	R_{53}	$3.9 \mathrm{k}\Omega$		
R_{13}	10Ω	R_{54}	$2.2 \mathrm{k} \Omega$		
R_{14}	$1 k\Omega$	R_{55}	10Ω		
			"DICTAPHONE"		
			earpiece		
R_{15}	$2.2k\Omega$	R_{56}	$(1k\Omega)$		
R_{16}	$47 k\Omega$	R 57	<mark>270Ω</mark>		
R_{17}	$1 k\Omega$	R_{58}	680Ω		
R_{18}	$2.2 \mathrm{k} \Omega$	R_{59}	$1.5 k\Omega$		
R 19	$47 k\Omega$	R_{60}	680Ω		
R ₂₀	$1k\Omega$	R_{61}	$(5.1k\Omega)$		
R_{21}	10Ω	R_{62}	100Ω		
R_{22}	4.7k Ω	R_{63}	$150\Omega \frac{1}{2}W$		
R_{23}	$1 k\Omega$	R_{64}	$150\Omega \frac{1}{2}W$		
R 24	$2.2k\Omega$	R_{65}	$10k\Omega$		
R_{25}	470Ω	R_{66}	$1k\Omega \frac{1}{4}W$		
R_{26}^{-1}	$27k\Omega$	R_{67}	$100\Omega 2W$		
R ₂₇	$33k\Omega$	R_{68}	47Ω		
R_{28}	$10k\Omega$	R_{69}	47Ω		
R29	10Ω	R_{70}	4 7Ω		
R ₃₀	$4.7 \mathrm{k}\Omega$	R_{71}	47Ω		
R_{31}	$10k\Omega$	R_{72}	$100\Omega 2W$		
R_{32}	680Ω 2W	R_{73}	$10k\Omega$		
R_{33}	470Ω 2W	R_{74}	$1 k \Omega \frac{1}{4} W$		
R_{34}	470Ω	R_{75}	220 Ω pre-set		
R 35	$1k\Omega$	R_{76}	$10k\Omega$		
R 36	100Ω	R_{77}	$2.7k\Omega$		
R_{37}^{10}	100Ω	R_{78}	$5k\Omega$, 3W lin		
R 38	$10k\Omega$	R_{79}	500 Ω pre-set		
R 39	$(5.6-10k\Omega)$	R 80	$470k\Omega$ pre-set		
R_{40}	39kΩ	R_{81}^{0}	500 Ω pre-set		
R40	39kΩ	R_{81}	500 Ω pre-set		
R_{41}^{40}	$4.7k\Omega$	R_{82}	470k Ω pre-set		
+1		02			

All resistors are $\frac{1}{8}$ W, unless otherwise indicated. The values of those in brackets may need adjustment, as mentioned in the text.

Capa	citors		
C_{\perp}	6,600µF, 50V,	C_{11}	$10\mu F 6V$
	4A ripple		
C_{2}	50μF 15V 2μF tantalum	C_{12}	50µF 6.4V
C_3	2µF tantalum	C_{13}	320µF 6V
	12V		
C_{\downarrow}	220nf	C_{14}	220nF tantalum
			12V
C	$100\mu F 12V$	C_{15}	100nF
C_{6}	$100\mu F 12V$	C_{16}	330nF
C	10 μ F 12V	C_{17}	220nF tantalum
			12V
C	$2\mu F 12V$	C_{18}	330nF
	220nF	C_{19}^{10}	10nF 25V
	100nF	• • • •	
10	metallized		
	paper		

Diodes	
D_1	5D02 (International Rectifier)
D_{2-4}	1N916
D_{5-13}	5D02
$D_{14,15}$	30\$1
D_{16}	5D02
Z	12V, 1W
Ζ,	4V7 400mW
Z,	2-6V8 400mW
ZA	3V 400mW
Z,	5V1 400mW
Z ₆	3V3 400mW
Z,	5V1 400mW
Zx	5V1 400mW
Z_9	15V 400mW
Z_{10}	6V2 400mW
Z_{11}	12V 400mW
Z_{12}	11V 400mW
Z_{13}	11V 400mW
Z14	10V-400mW
Z_{15}	10V 400mW
Z_{16}	11V 400mW
Z_{17}	9V1 400mW
Transis	tors

2N3702, ZTX50	$\begin{array}{c} Tr_1, \ Tr_4, \ Tr_{13}, \ Tr_{15}, Tr_{17}, \\ Tr_{18}, \ Tr_{19}, \ Tr_{20}, \ Tr_{21}, \\ Tr_{22}, \ Tr_{23}, \ Tr_{24}, \ Tr_{26}, \\ Tr_{27}. \end{array}$
	$1r_{27}$.

2N3704, ZTX303 Tr3, Tr5, Tr6, Tr7, Tr8, Tr_{33} . Tr_{9} , Tr_{11} , Tr_{16} , Tr_{28} , TIP31A Tr_{29} . TIP32A Tr_{31} , Tr_{32} . Tr_{14} TIP31, TIP29 Tr₂ TIS43 Tr_{10} **ZTX107A** $\frac{Tr_{12}}{IRC10(1A)}$ 2N3055 Th_1

Switches

single-pole changeover (0.5A) S_1, S_2

- microswitch S_3
- Two-pole changeover microswitch S_4
- S_5 Three-pole rotary changeover

Miscellaneous Ln. 12V 60mA 24V 1W Lp_2 LP_3 240V neon indicator 5V, 50-60mA (3.5mm dia.) $Lp_{4,5}$ F_1 F_2 1A anti-surge 5A anti-surge Mains transformer. Douglas M20AT 2A suppression choke L_1 Motor. "Milliperm Special Super 12V, 5-pole" (R. MARX-LUDER, 7121 Gemmrigheim, Neckar, Germany.)

Earpiece. Danavox (G.B.) Ltd, "Broadlands", Bagshot Road, Sunninghill, Ascot, Berks.

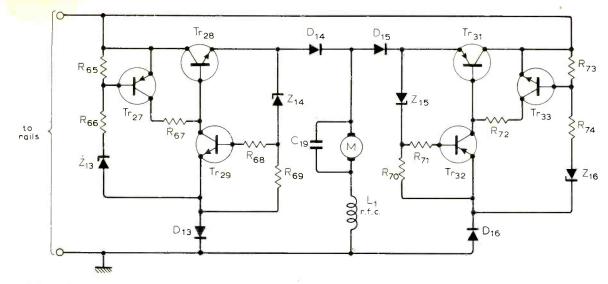


Fig. 6. Motor drive unit.

Transistors $Tr_{3_{2},3_{1},3_{3}}$ etc are operational. With negative on the earthing rail the reverse occurs, $Tr_{3_{1},3_{2},3_{3}}$ being isolated and $Tr_{27,28,29}$ etc. being operational. Resistors R_{65} and R_{73} may have to be adjusted slightly to take account of component tolerances.

General Notes

When ordinary magnet-and-pole-piece locomotives are modified to take this system the pulse supply makes the locomotives noisy in operation. A simple modification is possible to stop this and consists of sawing out the armature "slot" to take a circular ferrite magnet of the type fitted to "Hornby" locomotives and other miniature electric motors. The air gap should be kept small as large air gaps cause an increase in running current and heat dissipated by the motor, although, air gaps as large as $\frac{1}{16}$ in have been found satisfactory. This modification immensely improves the slow start and running response.

Other locomotives fitted with magnet and pole pieces are best refitted with five-pole ring field motors in order to get the best from this or any other "pulse" system.

Locomotives fitted with plastic body shells will usefully augment the noise from the whistle and not so usefully augment noise from tender drive units. The tender drive units can be suitably "silenced" by lining the interior with $\frac{1}{32}$ -in thick lead sheet which can be made from $\frac{1}{8}$ -in roof lead by rolling or by taking the $\frac{1}{8}$ -in thick lead to a sheet metal works who will usually do the job for a few pence. The imitation coal in tender drive units can usefully have small holes ($\frac{1}{32}$ -in dia) drilled in the coal department in order to assist air circulation. The holes are not noticeable after drilling without very careful examination.

The layout of components has not been found critical, most of the circuitry being made up on 0.1-in Veroboard or similar. The power supply ramp generator should be kept clear of pulse-carrying wires and parts, and the normal good practices applied. The power supply output waveform should be checked for slow rise and

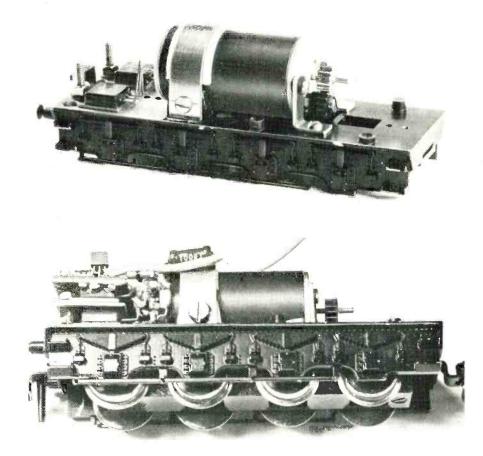


Fig. 7. Motor and control mounted in the tender.

fall times (0.2-0.5ms) on an oscilloscope before use. Too fast edges will damage C10, which should be metallized paper or polystyrene of at least 200V working. All other components are uncritical. The ganged microswitch will probably have to be made up, and it is worth noting that it does not matter if both switches do not switch at exactly the same time so long as they are free in operation. (Ganged microswitches are, however, commercially available from Bulgin.) The bridge rectifiers fitted to the "coach" and whistle sensor units are there to make it immaterial which way round the coaches are placed on the rails and what polarities are placed on the rails. (Reversing

the loco by reversing the supply has no effect on lights or whistle.) When setting up the system it is best to use only one meter for all measurements. Slight adjustment to all output voltages can be made by varying R_{17} in the range 47-100 Ω . The coach lighting sensor regulator transistor Tr_{4} should be fitted to a small heat sink (1in \times lin) or more conveniently the mild steel ballast plate that is supplied with some commercial coaches (Trix). In practice the system adds considerable realism to the model railway "train" which, in my opinion, they sadly lack at the moment. It only remains to add an efficient load sensing smoke unit to make the system complete.

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News of the Month

"Donald Duck" eliminators for U.S. Navy

The United States Navy is buying British systems capable of overcoming the "Donald Duck" effect which oxy-helium gas has on deep-sea divers' speech. The systems, worth, with spares, a total of £23,000, were developed for the Royal Navy by Marconi Space and Defence Systems Limited, a GEC-Marconi Electronics company, from Admiralty Research Laboratories designs.

The "Donald Duck" effect results from divers having to breathe an oxy-helium mixture in depths of greater than 600 feet, where air cannot be used safely. The mixture, being much less dense than air, produces changes in the speed of sound, and therefore in the pitch of a speaker's voice. This rises to an extent where it becomes completely unintelligible to the listener. In emergency situations, the lack of effective communications can mean life or death to the diver.

The Marconi system, designated the Type 023, was developed from designs started in late 1968. It has already been in service in the Admiralty Experimental Diving Unit and the Royal Naval Physiological Laboratory, and is currently being evaluated, with favourable results, in a series of medical research dives of up to 1000 feet by the Smithsonian Institute in the U.S.A. It operates on a principle where each sound is digitally analyzed, and the significant portion, typically about one third, is reconstructed at a slower rate, while the rest is rejected. This has the effect of lowering the frequency to about a third of its transmitted value, and thus creating full intelligibility.

Largest solid-state image sensor

RCA have demonstrated what is claimed to be the largest solid-state image sensor announced to date. The sensor — which is a charge coupled device (c.c.d.) — is a silicon chip the size of a small coin, containing over 120,000 electronic elements. Manufacturable c.c.d. image sensors of at least this size are essential if all-solid-state TV cameras are to have the resolution to satisfy a broad range of applications. Possible future TV cameras employing c.c.ds could be the size of a cigarette package or smaller, and would be rugged, highly reliable and potentially low in cost. When an image is focused on the c.c.d., the sensor's electronic elements transform the picture into individual electrical charge packets. These packets are then read out very rapidly by charge transfer techniques. The resulting information can be processed and displayed as a TV picture.

Component tester for relay systems

Electronics and radio research scientists of the Measuring Systems Design Department of Bell Laboratories in the United States have developed a new kind of test set with several valuable features for use in testing components of f.m. radio relay systems.

The new test set measures delay distortion, insertion loss (or gain), and return loss. The overall shapes of all three transmission characteristics are displayed. simultaneously on two large-screen oscilloscopes. This mode of operation allows the test set to approach the accuracy of point-by-point measurement while still displaying the characteristic over the entire frequency band. An operator can adjust the component being tested and instantly observe the effect over the entire frequency band. (Previously, measurements of this accuracy were obtained by taking several measurements over the frequency band and plotting the results manually to determine the overall shape.)

The 50 to 100MHz scanner, called the f.m. scanner, was designed primarily to measure characteristics of f.m. radio system components.

Travelling scholarship

An I.E.E.E. travelling scholarship of £300 is being offered for a visit or visits to foreign electrical or electronic research or manufacturing establishments by a postgraduate student. The purpose is to promote an exchange of research and technological ideas and to foster a closer relationship between young engineers in different countries. Candidates must submit a programme for their visit(s) by December 31, 1973, and the award will be made to the candidate whose programme is judged most likely to promote the objects of the scholarship.

The scholarship is financed by the U.K. and Republic of Ireland Section of the Institute of Electrical and Electronics

Engineers, which is acting in collaboration with the Institution of Electrical Engineers and the Institution of Electronic and Radio Engineers. Entrants must be student or graduate members of one of these three institutions. Further information and entry forms are obtainable from Prof. C. W. Turner, Dept. of Electrical & Electronic Engineering, King's College, Strand, London WC2R 2LS.

Venture for speech recognition

EMI Limited, London, and Threshold Technology Incorporated, Cinnaminson, N.J., U.S.A., have announced their intention of forming a joint venture company in Britain to market, over much of the world, electronic systems for recognizing spoken words and converting them into signals for controlling machines or instructing computers.

A major area of Threshold's operations is in the security field. It is currently testing a system which can identify a speaker's voice and compare it with voice patterns in a memory bank of "authorized" voices.

Physics exhibition obituary

The Council of The Institute of Physics has decided that the Physics Exhibition should be discontinued. The next exhibition provisionally arranged for 1975 will not take place.

In recent years the number of exhibitors, particularly industrial firms, has fallen substantially, as has the number of visitors. This gives confirmation to a widely held belief that generalized scientific exhibitions without a unifying theme are unattractive to both exhibitors and visitors.

The Institute's knowledge and expertise in the exhibition field will now be concentrated on smaller specialized events.

The exhibition was first held by The Physical Society in 1905; the last one, in 1973, was the fifty-seventh in the series.

Briefly

B.A.S.C. gets going. The principals of five major U.K. u.h.f. aerial manufacturers met in Bristol in September to reconstitute the British Aerial Standards Council, which, although formed as long ago as 1963, confined itself primarily to technical interchange. Recent developments have prompted it to extend its activities considerably, with the object of promoting high standards of performance, design and construction in television and v.h.f. radio aerials available to the public.

Frequency change for Northern Radio 4. The Radio 4 medium-wave service in North East England, which is at present transmitted on 261 metres (1151kHz), changed its wavelength on Saturday September 29 to 330 metres (908kHz). The two transmitters concerned are those at Stagshaw (near Hexham) and Scarborough.

Multi-flash Trigger Unit

Instrument triggers up to five flash units at intervals from 11ms to 11s

by Ralph Lewis

There are many times when the output of commercial stroboscopic flash units is completely inadequate to deal with a particular photographic problem. I am thinking essentially of cases similar to one described by Victor Blackman in his "Cameravaria" column in Amateur Photographer when he was required to take sequence photographs of a springboard diver in flight. To have used a strobe flash, even of a power considered high for strobe circuits, would have necessitated the pool being in complete darkness, otherwise ambient illumination would have obliterated the flash images. Because it was obviously dangerous to attempt a dive under those conditions, he ended up making a montage from photographs taken during separate dives.

Stroboscopic flash design to deliver the same amount of energy per flash as the high power single flash units (often 1,000 to 5,000 joules) in use in many studios today, is impracticable because of problems encountered in cooling the flash tube and building up energy in the capacitor rapidly enough. The usual way out of this difficulty, where short sequences are required and it is not essential for the light to issue from exactly the same point each time, is to arrange for a number of capacitors to be charged simultaneously and discharged in succession; each one through a separate flashtube; often, but not necessarily, mounted in one reflector.

A simpler and less expensive method is to make use of conventional commercial single flash units and connect them to a device that will trigger them in the required manner. Making use of standard designs means that they can be obtained as and when needed from the several firms offering equipment hire facilities.

The circuit of such a device, which will trigger up to five flash units at equal increments of time throughout periods of 11 seconds to 11 milliseconds, is illustrated in this article. The periods are continuously variable to suit the duration of the event to be photographed.

Circuit operation

Transistors Tr_1 , Tr_2 and Tr_3 (Fig. 1) with their associated components make up a monostable multivibrator which is switched from the stable to the unstable state by a negative pulse applied to the base of Tr_2 . This is provided by the closing of the camera shutter contacts which connect to the socket labelled sync. The pulse causes the collector current of Tr_2 to rise and switch on the thyristor SCR_1 , which in turn triggers the first flash of the sequence connected to FL₁. If C_1 were directly connected to the collector of Tr_2 , it would, together with the input resistance of Tr_3 , greatly increase the rise time of the collector potential of Tr_2 .

To overcome this, an emitter follower Tr_1 is inserted between Tr_2 collector and C_1 which provides a much lower impedance for C_1 and Tr_3 to shunt. To begin with, C_1 is charged to the supply voltage minus the base potential of Tr_3 . When Tr_2 is switched on, its collector rises almost to the voltage of the positive rail carrying the emitter of Tr_1 with it. Because the charge on C_1 cannot change instantaneously, the base of Tr_3 is taken to almost twice the potential of the positive rail above earth which cuts off its collector current until such time as the charge has sufficiently leaked away via R_5

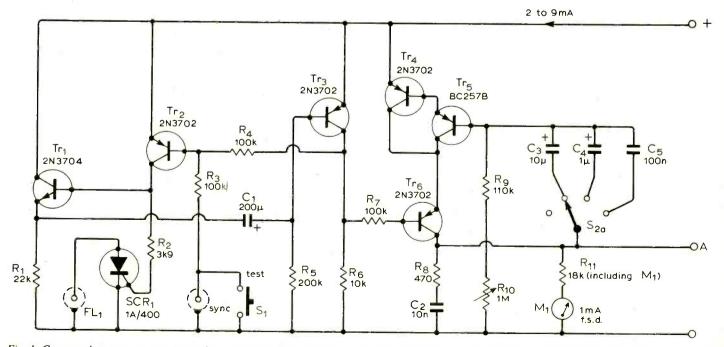
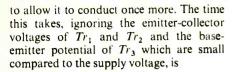


Fig. 1. Camera shutter contacts trigger the monostable circuit which turns on the thyristor to provide the first flash trigger. If C_1 were directly connected to Tr_2 collector, rise time would be too great. Timing circuit provides ramp output at A.

Wireless World, November 1973



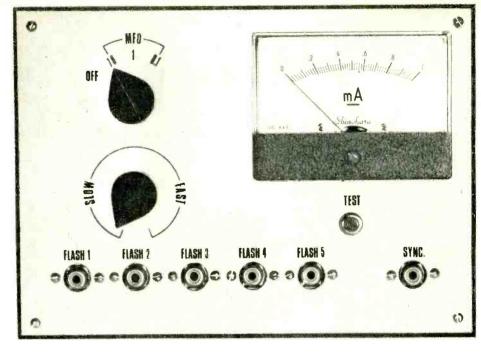
$$a \approx C_1 R_5 \log_e (2V_{cc}/V_{cc}) \approx 0.69 C_1 R_5$$

When the base of Tr_3 is biased to cut off its collector falls to earth potential and negatively biases the base of Tr_2 , holding it in the conducting state. When the charge on C_1 has sufficiently leaked away to allow Tr_3 to conduct once more, its collector rises until it is within 0.2 volts of the positive rail, which is sufficient to cut off Tr_2 through R_4 . The circuit now holds this condition until another negative pulse is applied to Tr_2 base.

The timing circuit is a transistor version of a Blumlein integrator, more usually referred to as a Miller integrator. A basic circuit is shown in Fig. 2 using an n-p-n transistor for ease of explanation although the final circuit makes use of p-n-ps so that a positive going ramp is obtained.

At the start, the switch S is open, the capacitor C is charged to a potential of $V_{cc} - V_{eb}$ and a current flows through R equal to $(V_{cc} - V_{eb})/R$. When the switch is closed the immediate tendency is for a collector current to flow through R_L equal to $(V_{cc} - V_{ce} \text{ sat.})/R_L$, provided the current in R is large enough to cause saturation in the transistor, and for the collector to take up a position about 0.2 volts above the negative rail. If that were to happen, the collector current would be cut off because the voltage across C cannot change instantaneously and any change in collector potential is immediately transferred to the base. Obviously this is impossible, so a condition develops where the base potential is just sufficiently positive to allow C to discharge through the transistor, which allows the collector voltage to fall slowly in a linear manner. This occurs for the following reason. Electron current flows away from the base via R and into the base from C. The result is a difference current which is the base current during the discharge.

The greater the current gain in the transition, the smaller the change in base current required to satisfy the voltage change at the



collector as the capacitor discharges. The base current is thus very small compared to I_R and changes very little during the discharge. The smaller the base current is, the smaller the difference between I_R and I_C and the more constant V_{eb} . A constant voltage across R produces a constant current through it; therefore the nearer I_c approaches I_R the closer it comes to constancy. As constant current flowing into or out of a capacitor raises or lowers the potential across it, according to the basic expression V = It/C, it follows that the voltage across C falls linearly with respect to time. As one plate is connected to a hardly changing V_{ab} and the other plate is joined to the collector, the collector voltage must fall in like manner.

When the capacitor is completely discharged, the collector potential is equal to V_{eb} , the base current is again provided by R only and the collector falls a fraction further to V_{ce} sat.

If the switch is now opened, C recharges via the base of the transistor and R_L .

The time for the linear portion of the voltage ramp can be expressed essentially by

$$t = \frac{VC}{I_c} \approx \frac{(V_{cc} - V_{eb})C}{(V_{cc} - V_{eb})/R}$$
$$\approx CR \text{ seconds, as } I_c \approx I_{eb}$$

Because linearity is dependent upon a high value of beta, a Darlington pair is used in the final circuit and Tr_6 acts as the switch. Leakage in the capacitor, represented by R_c in Fig. 2, must be kept to a minimum because it provides a shunt negative feedback path, bypassing the capacitive loop; reducing the gain of the amplifier and consequently the linearity of the ramp. For this reason, tantalum capacitors are recommended for C_3 and C_4 if the expense of polyester types is considered prohibitive.

Linearity also depends on a high voltage gain which is a product of $h_{FE}i_bR_L$. This makes the choice of R_L a compromise as h_{FE} and R_L are interdependent. Too large a resistance could limit the collector current to a value which would seriously reduce the

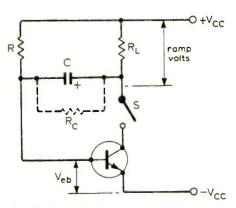
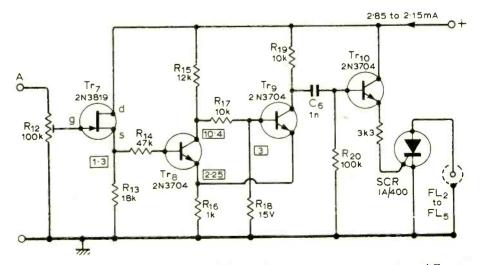
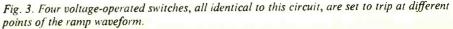


Fig. 2. Basis of the timing circuit is a Blumlein (Miller) integrator, the linear portion of the ramp being about CR seconds long.





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current gain factor. This is especially so in the present circuit where the collector current of Tr_5 can only be a fraction of that of Tr_4 . The effective load resistance of Tr_4 and Tr_5 is made up of R_{11} and four R_{12} s in parallel and works out at approximately 10.5k Ω , giving adequate linearity for the purpose with the transistors shown, though no doubt others would give an equal or even better performance. The ones chosen had the merit of being inexpensive and were close to hand.

The meter provides a quick check of the correct functioning (or otherwise) of the timer; enables, on the 10μ F range, the time of the ramp to be compared with the duration of the event to be photographed; and facilitates the setting up of the voltage level switches.

The circuit of a switch is shown in Fig. 3 and as four are required the components are labelled A to D. The switches are arranged to operate sequentially at equal intervals during the ramp. Transistors Tr_8 and Tr_9 are connected as a Schmitt trigger and the potential at A is applied to the base of Tr_8 via an f.e.t. source follower which serves to isolate the switches one from another and prevents variable shunting of R_{11} by the change in input resistance of Tr_8 as it changes state.

With A at zero potential, Tr_8 is nonconducting and Tr_9 is in saturation. Tr_8 emitter potential is provided by the emitter current of Tr_9 flowing through R_{16} and is normally about 2.25 volts. When the voltage at the base of Tr_8 is sufficient to initiate conductance, its first effect is to raise the emitter voltage (emitter follower action). but this tends to bias off Tr_9 thus reducing the current which provided the voltage in the first place. As Tr₈ base continues to rise, its collector voltage falls, reducing the base voltage of Tr_9 and consequently its emitter current. This reduces the emitter voltage of Tr_8 which causes still heavier conduction until such time as saturation occurs and its collector potential is very little more than its emitter. When this state is reached, Tr_9 base is at a lower potential than its emitter, due to the divider action of R_{17} and R_{18} , and is cut off.

Because the action is regenerative, the collector of Tr_9 can be raised from 2.3 volts to 19.5 volts when the base of Tr_8 reaches a critical point on the ramp which is set by adjustment of R_{12} . This voltage change is converted to a current pulse by C_6 , R_{20} and the emitter follower Tr_{10} . Gate resistor limits the current peak to a value that will reliably turn on the thyristor.

A circuit that relies for its operation upon somewhat precise voltage levels obviously requires a stable supply voltage. The circuit of the battery supply and voltage regulator is shown in Fig. 4 and follows common practice. The quiescent battery current is 16mA rising to 21mA during the timing period. It is left to the constructor as to whether he fits PP3s or PP6s as a lot depends on how much one plans to use it.

Construction

If tantalum capacitors are used for C_3 and C_4 their values should be measured as the tolerance of some of them is as wide as

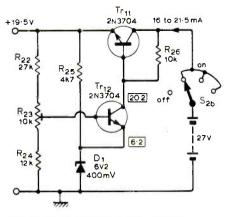


Fig. 4. Stable battery supply circuit.

electrolytics in general (+100 - 10%) and can double the time of the ramp if one is not careful. If a bridge is not available, it would be advisable, though more expensive, to use polyester types if anything like the suggested times are looked for.

The period $0.70C_1R_5$ must be longer than the period of the longest timing run, i.e. 11 seconds, for the ramp to reach maximum before Tr_6 is turned off. It can with advantage be twice as long to aid the setting of the voltage level switches and the rail voltage. Because the leakage resistance of electrolytic capacitors aids their discharge, a capacitor of 200μ F is used which works out at 28 seconds but in practice gives about 20 seconds.

The circuits are made up on individual pieces of 0.15-in Veroboard (see Fig. 5) and board wiring diagrams are available from the editorial office at W.W.

Use is made of mounting tags broken out of a length of tag strip to secure the Veroboard to the front panel. The timer and voltage regulator assemblies are secured by means of the meter studding and the switches by the nuts and screws used to fasten the phono sockets, see Fig. 5.

When making panels for instruments I usually make a layout on a piece of white board in black drawing ink and label it with Letraset. I then make a fine negative of it and from that, a single weight bromide enlargement to the size required. A brief exposure to a 15-watt lamp at 6 to 7 feet is given to the paper before development and a light grey print with black lettering results. This is fixed to a piece of 14 s.w.g. aluminium with dry mounting tissue and a coat of clear polyurethane "varnish" is applied to the surface of the paper. When dry, the holes are cut out and the panel trimmed to size, but before trimming, the boundary lines of the panel are scored through to the aluminium surface with a sharp knife, so that a neat edge is obtained by filing as close to the line as possible. Holes are drilled small and enlarged to size with forward strokes of a file only, to avoid lifting the top surface of the paper. After cleaning off the swarf and filings with a cloth moistened with methylated spirit, I give it a final coat of polyurethane, paying particular attention to the edges of the panel and the insides of the holes. In this way, a neat, durable, and professional appearance is given to the finished product if a little care is taken.

Setting up

To set the rail voltage, select the $0.1-\mu$ F range and press the test button. The meter will move rapidly to full scale and hold for about 20 seconds. This gives time to adjust R_{23} so that the needle rests just short of the far stop which represents approximately 18.5 volts.

Setting up the switches is most easily done if a small electronic flash unit is used. Firstly, select the 10- μ F range, and to enable a more precise observation of the exact point at which the switch triggers, connect an 8- μ F capacitor in parallel, temporarily. Press the button and make sure that the ramp time does not exceed the turn on time of Tr_6 . If

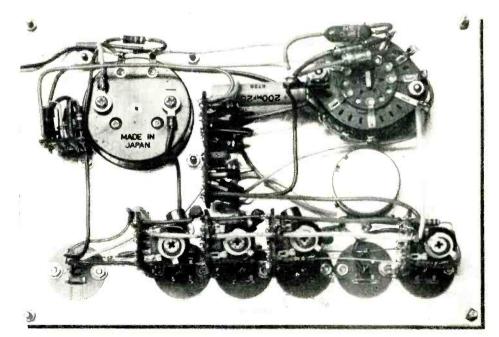


Fig. 5. Four circuit boards of voltage-operated switches are mounted vertically above the trigger sockets. Send s.a.e. to WW for board wiring diagrams.

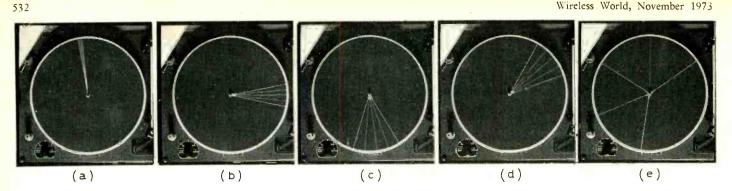


Fig. 6. To check linearity of $0.1-\mu F$ and $1.0-\mu F$ ranges the five flash units were used to photograph a string tied between spindle and rim of a 78 rev/min turntable. For the $0.1-\mu F$ range, R_{10} was set at min., mid. and max. settings (a, b and c) and at min. and mid. settings for the $1.0-\mu F$ range (d and e).

it does, connect a value somewhat smaller than $8-\mu F$.

With the flash connected to FL_2 , initiate the ramp with the test button and observe the point at which it fires on the meter. Repeat this, adjusting R_{12} , until firing takes place at precisely 0.25mA. Connect the flash in turn to FL_3 , FL_4 and FL_5 and adjust resistors 12 so that it fires at 0.5, 0.75 and 1.0mA respectively.

Checking the linearity on the $10-\mu$ F range can be done by inserting a microammeter in series with C_3 and observing that the discharge current, which should be in the region of 15.5μ A, is maintained with an almost imperceptible change until the 1mA point is reached on the meter. A change would indicate excessive leakage in C_3 or a low beta in Tr_4 or Tr_5 . In the original the change is less than 0.5% with a tantalum capacitor.

Linearity on the 0.1 μ F and part of the 1.0- μ F ranges can be checked by connecting five flash units and photographing, at various settings of R_{10} , a string tied between the spindle and rim of a gramophone turntable rotating at 78 rev/min. This of course takes into account the accuracy with which the switch trigger levels were set. See photographs in Fig. 6.

The resistor and capacitor, R_8 and C_2 , are to prevent a transient pulse triggering the 0.25mA switch when Tr_6 is turned on. The voltage readings given in the diagram are for guidance only, especially the source potential of Tr_7 which can differ markedly from the value in Fig. 4 because of the wide spreads in the characteristics of presently available f.e.t.s. Those given were measured with a 50k Ω /V meter with the point A at chassis potential.

And finally; if used with flash trigger circuits in which the voltage on the sync. contacts is not extinguished upon firing, the s.c.rs will remain conducting unless the plugs are momentarily pulled from FL_1 to FL_5 . This doesn't happen in portable units where a capacitor is discharged through the primary of a tesla coil, directly connected to the sync. contacts, but might occur if a slave relay circuit were used.

Letters to the Editor

The Editor does not necessarily endorse opinions expressed by his correspondents

Hi-fi equipment standards

We were interested in your editorial comment "The Educated Ear" (October issue) and disappointed that we were unable to provide you beforehand with full information on British work equivalent to DIN 45 5000. BSI is in fact working on a series of specifications for domestic hi-fi equipment. The specifications which have already been issued for comment in draft form deal with equipment such as amplifiers, microphones, record players, loudspeakers, headphones and combinations of equipment. The intention is to cover as much of the field of hi-fi as can be objectively approached.

Your regret at our apparent inaction would appear to be justified since Britain is indisputably a world leader in this field. We can only comment that the industry in this country only felt the need for guidance in these matters about two years ago and BSI responded immediately.

You will be glad to know that Britain

also leads in the field of specifying, and the forthcoming British Standard has already been proposed to the International Electrotechnical Commission as the basis for an international standard. Terry Hammond,

British Standards Institution, London, W.1.

Your editorial of October does an extreme disservice to those representatives of the U.K. audio industry who had been working since 1968 on the preparation of a U.K. based specification for the performance of high-fidelity equipment. Organizations participating in the early work included BREMA, FBA, APAE and RECMF, who were represented on an informal body, the Audio Specification Co-ordinating Committee. In 1970 the work had advanced far enough for an approach to be made to the British Standards Institution, which resulted in the setting up of Technical Committee TLE/26. For the record, a press release was sent by the Co-ordinating Committee to some twenty leading British electronics journals, announcing the completion of the preliminary work, but only two, not including *Wireless World*, felt moved to print it.

Since 1970, TLE/26 has met about thirty-six times and has prepared draft specifications for seven of the components of high-fidelity systems, viz. amplifiers, tuners, loudspeakers, microphones, record playing units, headphones and combinations. In order to further the goal of an internationally accepted specification for high fidelity equipment - infinitely preferable to a host of differing national standards - most of these drafts have been submitted to the International Electrotechnical Commission, and are under consideration by the newly set up Working Group 12 of sub-committee SC29B, which has at present one U.K. member and may have more in the future.

Most significant is the divergence of attitude between British audio engineers and the technical press to the German specification. One of the kindest descriptions applied to it by the leading "hi-fi purist" types is "a charter for mid-fi". One prominent manufacturer proclaims the ease with which its requirements may be exceeded, even with relatively modestly

priced equipment. The British audio engineer (or Dutch, French or Danish, for that matter) who is prepared to regard it, as it stands, as an acceptable criterion for the thin red line that divides highfidelity equipment from everything else, has yet to be encountered.

It really is high time that the technical press properly supported the work of British engineers in this and other fields of standardization. I have had occasion to write similarly to another journal on the same subject within the past year. A standard is useless if it is not used: it will not be used if it is not accepted by engineers and buyers in general and it will not be accepted if it is not publicized. Inaccurate editorials in the country's leading popular electronics journals nullifying the efforts of British engineers and publicizing a highly deprecated foreign standard are simply and completely unfair! J. M. Woodgate,

Chislehurst,

Kent.

Editor's note: We shall be glad to publicize the British standard when it is issued.

Radiating coaxial cables

I am writing in relation to J. R. Avery's letter (September letters) to point out that the radiating coaxial cable system he describes does not produce a "field variation of an inverse r^4 nature". The two straight lines shown on his graph are incorrectly designated as they actually show an inverse r and an inverse r^2 relationship of field strength with distance and not inverse r^2 and inverse r^4 as indicated.

With this correction in mind it seems that the fall off in radiation with increasing distance from the cable corresponds more nearly to that experienced with what is usually termed the "induction field" and the advantages claimed for radiating cable systems appear to be no more attractive at medium frequencies than those of induction loop systems. Admittedly at v.h.f. and u.h.f. the radiating cable system has its advantages, particularly in tunnel and mine applications, and where the cable can be used for both receiving and transmitting.

It is interesting to note that inexpensive coaxial cable with open-weave braiding is not very effectively screened and at m.f. produces results similar to those obtained with specially designed radiating cables, except that more r.f. power is required to provide the same field strength. This has been shown by field tests and, as a result, the cheaper coaxial cable is currently being installed experimentally for a university radio installation.

The proposed Scottish university system referred to is unlikely to produce any improvement over a well-designed induction loop system which would also not cause any significant interference beyond the perimeter of the campus. However, a radiating cable system which employs cable ducts below the ground is liable to induce currents at r.f. into any neighbouring cables (e.g. telephone cables) and, although this may have the dubious advantage of effectively increasing the broadcast coverage, the interference potential to the telephone system may be significant.

Finally, it should be added that the experimental or permanent operation of any radiating or induction system, irrespective of the rate of attenuation of field strength with distance, requires a licence from the Minister of Posts and Telecommunications and such a licence will only be issued after careful consideration of the practical circumstances and, in particular, the potential for interference to other services. M. Goddard,

Ministry of Posts and Telecommunications, London, S.E.1.

Mr Avery replies:

May I reply to the various points raised by Mr Goddard in his response to my letter published in the September issue on radiating coaxial cables?

He is, of course, quite correct in pointing out the error in the designation of the two straight lines in my graph. These should accurately be labelled "inverse r" and " r^{2} " as the ordinate of the graph is field strength. This error arose from Mr Moore's initial reference to field variations as inverse r^2 for transverse electromagnetic fields, and inverse r^4 for radiomagnetic fields.

The problem is one of units of measurement. If an aerial with a numeric gain ratio of G over isotropic is placed in an electromagnetic field with a field strength of E volts per metre and a wavelength of λ metres, then the power in watts available at the aerial terminals, assuming no mismatch or finite conductivity losses, is given by the expression:

 $P = G\left(\frac{\lambda^2}{4\pi}\right)\left(\frac{E^2}{120\pi}\right)$

If the distance d from the originating source is varied then this power increases or decreases according to an inverse square law ratio given by:

 $\left(\frac{\lambda}{4\pi d}\right)^2$

This gives a field strength variation of an inverse d nature, not a d^2 . However, the straight lines in my graph do correctly depict electromagnetic and magnetic induction field variations, according to Mr Moore's original definition, although the mathematical designation is as Mr Goddard points out incorrect.

The similarity of coverage provided between radiating cables and induction loop systems is not difficult to explain as both propagate by a similar mechanism. The loop carries radio frequency current which sets up an induction field within and adjacent to the loop, and is fed from both ends of the loop as a closed system. The radiating coaxial cable also carries surface radio frequency currents which are continuously coupled from inside the cable to the outer surface via the coupling mechanism (holes, slots, loose braid, etc.). However, the coaxial cable is fed from one end only, the other end being terminated in a matched load. This fundamental difference is one major attraction of radiating cables, as in some situations it is difficult to cover the desired area using loops. This is the case in the cited Scottish University system, where, due to the campus layout, approximately 20 loops, one on each building, would have been required to provide adequate coverage. Each loop has to be fed by a separate amplifier to achieve adequate coverage, and the signal distribution and impedance matching becomes very complex.

The use of a radiating cable will alleviate the problem by cutting the equipment down to one transmitter, but siting of the cable is important as the field is still inductive in nature and falls away rapidly with increasing distance from the cable. This is even more important if the coaxial cable used is of the loose braid type, as it is susceptible to the contamination effects of dirt and moisture. This may not be too important at medium wave frequencies, but at v.h.f. and u.h.f. frequencies, where only radiating coaxial cables can be used, as loops are too inefficient, the attenuation of loose braid cable increases and a better cable construction is necessary.

May I thank Mr Goddard for his valued comments, and his colleagues at the Ministry of Posts and Telecommunications, who carried out the measurements on the radiating cable from whose results my graph was compiled, for their valued assistance. Anyone interested in operating a radiating cable system at any frequency should contact the M.P.T. for approval and a technical and development licence, as radiating cable systems are still very much in the investigation phase.

J. R. Avery.

Using c.m.o.s. devices

I can quite understand Peter Seddon's trepidation after reading (Oct. Letters) the warnings about breakdown damage in c.m.o.s.; I was nearly frightened off by the apparent difficulties in handling and use, and came to the conclusion that c.m.o.s. devices were the answer to an engineer's prayer provided that one did not wish to unpack them, plug them in and switch-on!

Fortunately I was seduced, by the claims of low power consumption coupled with high noise immunity, into trying some, and would like to offer some words of comfort to Mr Seddon, based on my experiences during more than a year's use of c.m.o.s. devices.

I have come to the conclusion that, apart from a few elementary precautions, c.m.o.s. devices are more robust than the makers would have us believe. The main things to avoid are contact with plastics such as expanded polystyrene, which are capable of developing extremely high voltages due to friction (nylon lab. coats may come into this category), and the application of voltages outside the maxima specified from power supplies, unearthed soldering irons and test equipment. With the exception of these main points I have not found any other precautions necessary (the image of Mr Seddon chained to his bench is intriguing but hardly practicable).

My prime source of device destruction was my failure to appreciate the devastating effect of floating inputs when the device was "on supply". In the case of hex buffers and inverters, e.g. R.C.A. CD4010 and CD4009, a floating input to a spare element will assume a potential of about $\frac{1}{2} V_{cc}$, causing both complementary output transistors to conduct. This quickly results in failure due to the high current so taken.

This problem is not likely to occur in the final circuit since the few spare inputs there are will, if the designer has done his job properly, be suitably tied to 0V or V_{cc} . During "lash-ups", however, it is very easy to overlook the odd spare input and burn the device out (and sometimes burn one's own fingers, literally!).

In the case of a two input gate, e.g. R.C.A. CD4011, doing duty as an inverter/ buffer, I find the simplest thing to do is to strap the two inputs, thereby remaining the need to find a suitable "V" or " V_{cc} " point.

So far I have not experienced a failure traceable to gate breakdown and have even had devices survive reverse insertion in their sockets.

I should like to offer Mr Seddon the following advice: (1) Ensure all spare inputs are suitably tied. (2) Keep within the operating voltages recommended. (3) Check soldering iron and test gear earths. (4) Avoid contact with non-conducting plastics. (5) Plug the devices in the right way round. (6) Set power-supply current limiting to the lowest practicable level. These six points are applicable to any semiconductor device and do not make c.m.o.s. any more difficult than t.t.l.

Finally, Mr. Seddon, have a go; c.m.o.s. is fairly cheap now and the rewards are well worth the odd few bob (sorry, five new pence pieces)! David S. Williams,

Walsall,

Staffs.

Novice licence

You are so right in asking (page 516 of W.W. Oct. 1973) "Should there be a U.K. novice licence?" There is a need for such and has been for many years. Pre-war there was the A.A. licence which put so many of today's "G"s where they are.

The radio controlled model people are also worthy of consideration. What an advantage it would be to them to use limited power communication on airfields etc. There are many such persons keen enough in this branch of radio experimenting and research but who are not in the least interested in becoming a "G" and calling someone at the other side of the world "old man", each to his own liking.

The frequency allocated will, we understand, be made unusable by misuse or at least this is the opinion of "G's" — but if we listen to some of the "amateur bands" there is sometimes cause for concern.

I feel that at least holders of model "pulse" licences should be granted a frequency for speech communication. Ray Williams,

Grantham,

Lincs.

Projection television

The letter from America by G. W. Tillett (September issue) and the letter from H. Ibbotson (October) bring memories to me with feelings of nostalgia.

It is a great pity that after a very promising start the development of projection television stopped. I firmly believed then and still do that a form of projection television will be evolved which will include stereo sound and 3D reproduction.

Within very restricted limitations I continued development of colour projection television. The results, although promising, will require a fair amount of work, particularly to improve brightness. The colour and picture quality is comparable with a 26in shadow mask tube. Where projection fails is insufficient brightness, and it must be viewed in total darkness.

The main difficulty is that, of necessity, I had to use black and white MW6/2 tubes with colour filters. Mullard's did at one time produce blue, green and yellow tubes. These, with a red filter on the yellow tube, produced acceptable results; however, the loss of light was considerable.

I saw the French optical system demonstrated in Paris early in the 1950s but did not think the results as good as the Philips/Mullard unit.

In adapting the standard projection system to colour it was necessary to re-design the deflection coil assembly to accommodate convergence coils. The whole assembly is similar to that used with shadow mask tubes.

There is still a fair amount of development work to be done, so get cracking you *Wireless World* experimenters! V. Valchera,

Valradio Ltd, Feltham, Middlesex.

Sale of "walkie-talkies"

I would draw your attention to the adverts for "walkie-talkies" in a popular publication. The information is attached on a separate sheet. |Extracts from *Exchange* and Mart sent.]

To the best of my knowledge these units operate in the 29.9-31.00MHz area and as such it would be most unlikely that permission to operate them in the United Kingdom would be granted by the M.P.T.

I certainly have no wish to restrict the commercial activities of the concerns

www.americanradiohistory.com

selling these items but in all fairness I do feel that some reputable authority should make some investigations into the sale and obvious use of them.

As all these units are imported it would seem that some regulation could be exercised by H.M. Customs and Excise. There already exists an import restriction covering similar units operating in the 26.1–29.7MHz and 88–108MHz bands and maybe this could be extended.

I should add that I am a radio amateur (G3LWM) and it is certain'ly not a case of "sour grapes" but an effort to prevent unsuspecting people becoming liable to prosecutions under the Wireless Telegraphy Act. On numbers of occasions I have been asked by the police to produce my licence. This has usually been on the tops of wind-swept hills, on misty nights to take advantage of good v.h.f. conditions!

J. D. Harris, Bishop's Stortford, Herts.

VAT and prices

Despite your publishing my letter in the September issue there are 41 advertisements in the October issue which have no indication whether VAT applies or not. Together with Mr Dykes (Oct. issue), I hope that the matter will improve. Perhaps some editorial guidance is necessary. These 41 firms will of course not get any of the ± 100 I spend monthly with your advertisers — just the same as those firms who offer long lists of transistors they do not have in stock.

Do these people think we do not remember poor deliveries, wrong items sent, poor packaging and procrastination? Those who do not quote prices at all are the worst of course; possibly they have large office staffs to answer queries — I don't have time, I merely go elsewhere. W. B. Henniker,

Henniker & Kerr, Edinburgh.

Frequency shifter for "howl" suppression

Some of your readers may not be aware that the frequency shifter designed by M. Hartley Jones and described in your July issue, can be adapted to provide a very acceptable imitation of "tape phasing", much sought after in popular music. All that is required is a mixer to add direct and frequency shifted sound. The result is a series of nulls running through the audio spectrum at a rate determined by the frequency shift.

For best effect a frequency shift of about 0.2Hz is required, which is not difficult to achieve with that particular circuit. A good explanation of phasing is given in the *Journal of the Audio Engineering Society of America*, December 1970, vol. 18, No 6, pp.674-5.

A. G. Falla, Radcliffe on Trent, Notts.

Dual-polarity Digital Voltmeter

2 — Construction and calibration

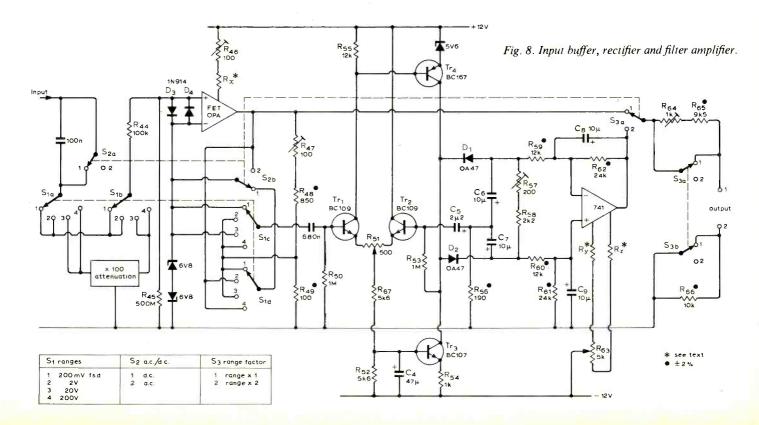
by A. J. Ewins

A.c./d.c. input stages. The sensitivity of the basic d.v.m. is, as already stated, 2 volts d.c., with an input impedance of $20k\Omega$. It was required that the d.v.m. should have a maximum sensitivity of 200mV a.e. and d.c., and as high an input impedance as possible. It was also required that the a.c. response should extend up to 100kHz so that the voltages of all signals encountered in audio circuits (tape-recorder bias and erase oscillators operate around 100kHz) could be accurately measured. These requirements call for an input amplification stage with a voltage gain of ten, a frequency response from 0 to 100kHz and a high input impedance. The temperature stability of the amplifier stage must also be good for d.c. measurements, because a maximum sensitivity of 200mV implies a resolution of $100\mu V$. To achieve these objectives it was decided to use a f.e.t. operational amplifier as the input buffer stage. The one used by the author is supplied by RS Components Ltd, the FET-OPA, which at £5.80 trade may be thought rather expensive. However, an alternative device with similar characteristics is one supplied by Ancom Ltd, type 15A-37. This is priced at £4.95 retail and, though still expensive, is thought worth it. It has an input impedance of $5 \times 10^{10}\Omega$ and an offset temperature stability of $50\mu V/^{\circ}C$, which is satisfactory. Although the f.e.t. op. amp. provides an accurate gain of ten at d.c., its frequency response at this gain level does not extend, accurately, to 100k Hz. However, its unity gain frequency response does extend beyond 100k Hz and it was not found difficult to design a rectifying circuit with an overall voltage gain of ten and a frequency response beyond 100k Hz.

Fig. 8 shows the circuit diagram of the complete a.c./d.c. input stages of the d.v.m., including the a.c. rectifier circuit. Using this in front of the basic d.v.m. extends the ranges of the d.v.m. to 200mV, 400mV, 2V, 4V, 20V, 40V, 200V and 400V, a.c. and d.c., and provides an input impedance of the order of 500M Ω on all ranges up to, and including, 4V, and about 10M Ω in parallel with 10pF for all ranges above 4V. In the d.c. mode, the f.e.t. op. amp. has a voltage gain of either ten or unity. In the a.c. mode,

the op. amp. has a fixed unity voltage gain and the rectifier circuit is either connected directly to the output of the op. amp. or via $a \times 10$ attenuator. The rectifier circuit itself has a voltage gain of five and is followed by a differential-amplifier filter circuit with a voltage gain of two.

The principle of operation of the rectifier circuit is as shown in Fig. 9. A diode/ capacitor rectifying bridge circuit is used instead of a full diode bridge. In the author's opinion, this is a more useful type of rectifier circuit than the full diode bridge since it has a voltage doubling action whilst, at the same time, the capacitors provide a first order filtering action to the unwanted a.c. component. For this type of circuit, V_{o} equals R_L . I_m where I_m equals I_L (peak)/ π . The feedback voltage, $V_f = V_{in}$. Thus, the voltage gain of the circuit, V_o/V_f , equals $(R_L/R_f)(I_{L peak}/I_L\pi)$. If the d.v.m. is to be calibrated in terms of r.m.s. values for sinewave inputs, $I_{L(peak)} = \sqrt{2} I_L$ and the voltage gain of the circuit will therefore be; $(R_L/R_f)(\sqrt{2/\pi})$. Therefore, for a voltage gain of 5, R_L equals 11.11 R_f . In the circuit of Fig. 8, R_L is equivalent to R_{58} in series with R_{57} , paralleled by R_{59} and R_{60} (which are effectively in series), i.e. $R_L = 24$ (2.2+0.2)/(24+2.2+0.2). R_L is thus adjustable from about $2k\Omega$ to $2.2k\Omega$, which, if $R_f = 190\Omega$, allows an adjustment to the voltage gain of the rectifier circuit from about 4.78 to 5.17. The maximum input voltage to the a.c. rectifier circuit is 400mV r.m.s. and therefore the output stage of the amplifier must be able to handle a peak-topeak voltage swing in excess of about 6 volts and provide a peak current of about 3mA. An op. amp. would therefore appear to be the ideal choice for this stage. However, neither the well-known 741 or 709 have a sufficiently high frequency response. It was therefore decided to design a suitable amplifier using discrete components on the



principle that simplicity sometimes produces the best results. The output stage is made to have an extremely high output impedance by using a constant current source as the load. This, together with the large amount of negative feedback available, overcomes the non-linearity of the diodes to such an extent that the linearity of the d.v.m. to a.c. measurements is accurate to plus or minus one digit down to 1% of full-scale. The overall frequency response is also good, being flat to within $\pm 0.5\%$ from 30Hz to over 100kHz.

A d.v.m. designed on the dual-slope integrating principle provides a degree of filtering action to alternating voltages by virtue of its design. It can be shown that the filtering action takes the form of an attenuation of 6dB/octave above a frequency whose period is equivalent to the integrating time of the d.v.m. In addition, at frequencies which are an exact multiple of the integrating frequency, the attenuation is theoretically infinite. The integrating period of this design (approximately 100ms) is equivalent to a frequency of 10Hz. Thus frequencies of a multiple of 10, i.e. 10, 20, 30Hz and etc., will be infinitely attenuated and those in between by not less than 6dB/octave above 10Hz. Thus, the filtering action of the integrator itself, together with the filtering action of the capacitors of the diode/capacitor bridge and the differential filter amplifier, provide an attenuation greater than 60dB to all frequencies above 30Hz.

The output from the circuit of Fig. 9, for connection to the circuit of Fig. 3, is via the $1k\Omega$ variable resistor R_{64} in series with R_{65} , and R_{66} to earth. When the switch, S_3 , is closed these resistors are bypassed and the ranges of the d.v.m. are 200mV, 2V, 20V, and 200V. When S_3 is open, the sensitivity of the basic circuit is effectively reduced by a factor of two, so that the ranges available become 400mV, 4V, 40V and 400V. The reading indicated by the display must therefore be multiplied by two. R_{64} allows this multiplication factor of two to be precisely adjusted.

 R_{46} and R_{63} allow the offsets of the f.e.t. and 741 op. amps. to zeroed. R_{47} allows the ×10 attenuator to be precisely adjusted. R_{51} is included so that the d.c. potential at the junction of diodes D_1 and D_2 may be

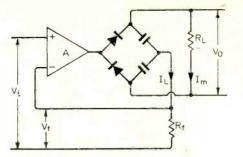


Fig. 9. Basic rectifier circuit

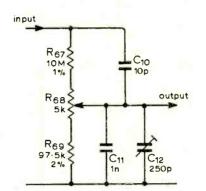
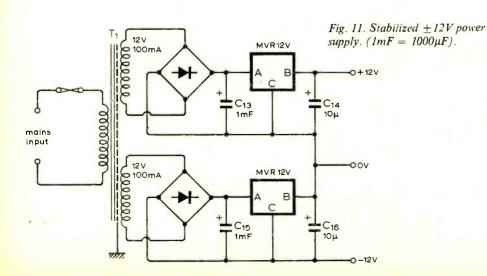


Fig. 10. Input attenuator.

adjusted to zero, preventing the two capacitors of the rectifier bridge from becoming reverse-polarised. These capacitors, together with C_8 , C_9 and C_5 are tantalum types and can accept a small reverse potential of no more than 500mV.

Fig. 10 is the circuit of the $\times 100$ attenuator. The variable resistor, R_{68} , allows the attenuator to be precisely adjusted under d.c. conditions and C_{12} allows the frequency response of the attenuator to be adjusted to an optimally flat condition. The resistor R_{69} is a parallel combination of a $100k\Omega$ and $3.9M\Omega$ resistor.

Power supplies. The power supply requirements for the d.v.m. are 5 volts at about 1 amp. (for the t.t.l. logic circuits and seven segment digital indicators) and ± 12 volts at about 50mA (for the analogue circuitry). Figs. 11 and 12 show the circuit diagrams of the power supplies and it will be seen that these are greatly simplified by the use of monolithic voltage regulators. Types MVR5V and MVR12V have been used by



the author, as supplied by RS Components Ltd. They are, respectively, rated at 5V $(\pm 0.25V)$ at 600mA and 12V $(\pm 0.6V)$ at 500mA. They have internal foldback overload and short circuit protection and are mounted in T03 cases. Alternative devices, types L005TI and L036TI (5V and 12V), may be bought from Semiconductor Supplies with identical characteristics.

Two 5V regulators are used because the total current consumption of the logic circuits and digital displays exceeds the current rating of one device. Thus one device is used to power the logic circuits and the other to power the digital displays.

The bridge rectifier for the 5V supplies may be any suitable diode bridge (or bridge of individual diodes) rated at 20, or more, p.i.v. and 1 amp. Diodes, type 1N4001, would be entirely suitable.

For the plus and minus 12V supplies, the diode bridge (or bridge of diodes) should be rated at 30, or more, p.i.v. and not less than 50mA. Diodes, type 0A200 (rated at 50 p.i.v. and 90mA) would be suitable.

Practical details

Figs. 13, 14 and 15 show the detailed layouts, on 0.1 in pitch Veroboard, of the main circuits of Figs. 3, 4 and 8, respectively. The components of the $\times 100$ attenuator (Figs. 8 and 10) are not included on the circuit board layout of Fig. 15 but should be mounted around the switch wafers $S_{1(a)}$ and $S_{1(b)}$. The layouts of the circuits are not critical (provided a logical approach is made) but are presented here as a guide to the would-be-constructor. Constructors may, of necessity, have to modify their layouts from those of the author to suit differences in components.

In Fig. 14, the layout of the digital and control logic circuit of Fig. 4, two 0.1μ F capacitors are shown, decoupling the supply rail to the t.t.l. circuits. The circuit has operated successfully without these capacitors and they may, therefore, not be needed. The rest of the layout conforms to the circuit diagram.

A number of components, used by the author in the construction of the prototype circuit boards, are fairly expensive and constructors may wish to consider cheaper alternatives. The zero offset adjustment potentiometers, R_3 and R_4 , of IC's 3 and 6 of Fig. 3 are shown, in the layout of Fig. 13, to be multi-turn pre-sets. These may be replaced by single-turn pots. of $5k\Omega$ and two fixed resistors totalling approximately $5k\Omega$, as shown for the zero offset adjustment potentiometer of the 741 of Fig. 8. The exact values of the two fixed resistors (R_v and R_z as shown in Fig. 8) will have to be found experimentally such that a zero offset is obtained when the wipers of the $5k\Omega$ pots. are approximately at the centre. In this manner it will be found that quite a fine control is produced.

In order to have sufficient control for an accurate adjustment of the two reference voltages, it will be found that R_1 and R_2 (Fig. 3) ideally need to be ten-turn pots. Alternatively, each pot. may be replaced by two single-turn pots; one of $5k\Omega$ (coarse control) and one of 500Ω (fine control). In the case of R_1 the $5k\Omega$ pot. should be placed

in the circuit as indicated and the 500Ω pot. in series with R_{13} . R_5 (Fig. 3) and R_6 and R_7 need only be single-turn pots.

For the C_1 , the author used a fairly expensive 63V, polycarbonate type but believes that a much cheaper polyester type should be just as satisfactory.

There is nothing special about the remainder of the components of Fig. 3. Z_2 is a standard 5.6V zener diode from the Mullard, BZY88 range and has a temperature coefficient of about -0.2mV/°C. This represents a change of about -0.004%/°C for the two reference voltages and should be more than adequate.

In Fig. 8, the offset adjustment for the f.e.t. op.-amp. may be either a ten-turn, $1k\Omega$ pot., or a single-turn, 100Ω pot. in series with a fixed resistor, R_x , of about 470 ohms, as shown. R_{51} need only be a single-turn pot., but R_{47} , R_{57} and R_{64} ideally need to be ten, or more, turn preset pots. (as does R_{68} in Fig. 10) since a resolution of about 1% is required. However, it is not impossible to achieve this resolution with single-turn pots., only tricky.

Nothing has been said, so far, about the type of digital and overload indicators used. For the seven-segment digital indicators the author chose "Minitrons" because, in his opinion, these are hard to beat for a combination of size, price and low current consumption. Types 3015F and 3015G have both been used and are widely available. The type 3015F indicates the digits 0 to 9 and a right-hand decimal point. The type 3015G indicates "+" and "-" signs, the digit "1" and a right-hand decimal point. One of the many, cheap l.e.ds now available is probably the obvious choice for an overload indicator, although a 6.3V filament bulb rated at 40mA is worth considering.

Construction and adjustment of circuits

The obvious place to start on the construction of the d.v.m. is with the power supplies and if the monolithic regulators are used, as

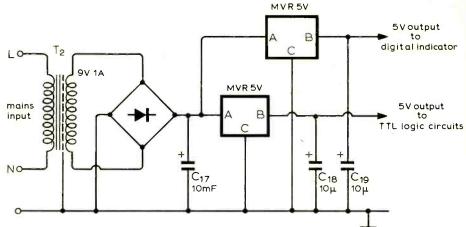


Fig. 12. Stabilized twin 5V power supply.

suggested by the author, these will present no difficulty. The circuits of Figs. 3 and 4 should then be constructed on two separate circuit boards as illustrated in Figs. 13 and 14. It is suggested that, if i.c. sockets are not used, all the i.cs should be checked for correct operation before insertion into the circuits. In particular, the input offset voltages of the 709 and 741 op.-amps. should be checked to ensure that they are within the manufacturer's tolerances. To simplify the checking and setting-up of the analogue circuit, IC_6 should initially be left out of circuit.

When the circuit of Fig. 3 has been constructed (less IC_6) it can be checked and initially adjusted. All three power supplies should be connected and the \bar{C} and "hold" inputs should be temporarily connected to the +5V line. With the power supplies switched on a few quick voltage checks can be made; in particular the reference voltage of Z_2 and the output voltages from IC_1 and IC_5 can be checked. They should be approximately +5.6V, +2V and -2V, respectively. The positive input to IC_2 and the negative inputs to IC_4 and IC_7 should also be about +2V. If these latter voltages are correct, the emitters of Tr_1 to Tr_4 should be at very nearly zero volts and may be

adjusted to precisely zero, with the V_{in} inputs shorted together, by means of R_3 . The reference levels to the two comparators, IC_8 and IC_9 , should now be adjusted. To do this, a small variable voltage source of between about -5mV and +5mV should be fed to what will be the output of IC_6 . R_7 should be adjusted so that the output from the collector of Tr_9 changes from about zero volts to about +5V when the small variable voltage source is reduced just below -3mV. The output of Tr_9 collector should revert to zero volts when the variable voltage just exceeds -1 mV. Similarly, R_6 should be adjusted so that the emitter of Tr_6 undergoes identical output voltage changes when the variable voltage source exceeds about +3mV and is reduced below about +1mV. If all is well, the operation of the switching transistors Tr_1 to Tr_4 may now be checked. Adjust the small variable voltage source to some positive value in excess of +3mV so that the emitter of Tr_6 becomes +5V. Measuring the output voltage at the junction of the emitters of Tr_1 to Tr_4 , disconnect the \overline{C} input from the + 5V line and connect to ground. The voltage reading should change from zero volts to the + 2V reference level. Reconnect the \overline{C} input to the +5V line and repeat the test with the variable

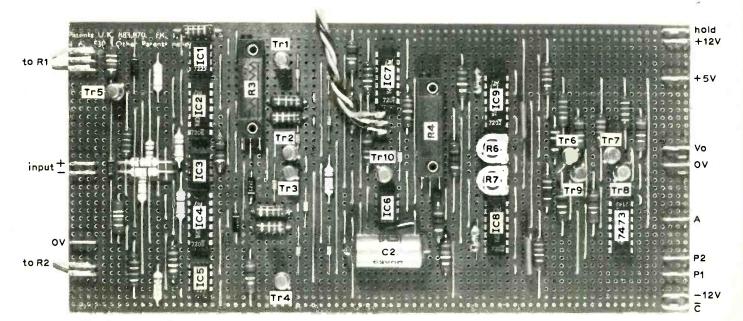


Fig. 13. Layout of analogue circuit.

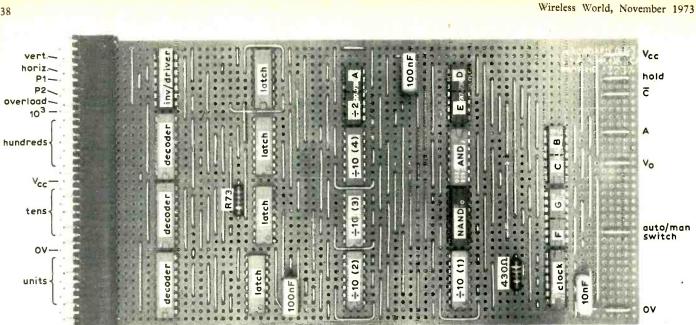


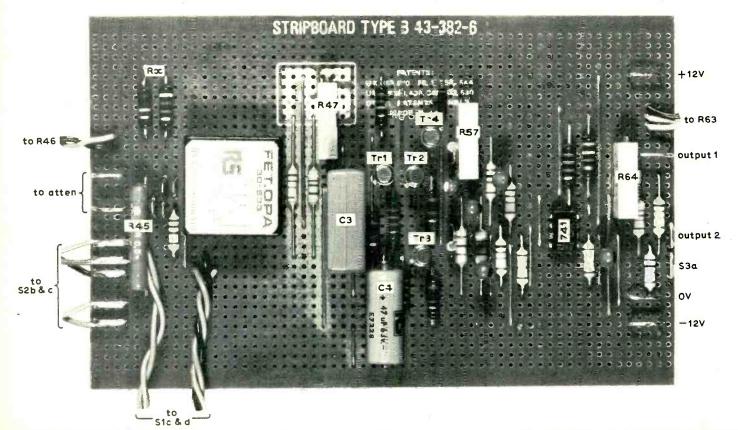
Fig. 14. Control circuitry and display logic

voltage source adjusted to some negative value below -3mV so that the collector of Tr_9 is at about +5V. The voltage reading should change from zero volts to the -2Vreference level. If all checks are satisfactory, disconnect the voltage supplies and insert IC₆ into the circuit. No more checks or adjustments can now be made until some preliminary checks have been carried out to the digital circuit board. To do these, connect the +5V supply to it and temporarily connect the "auto-Manual switch" input (see Fig. 14) to ground and the V_o input to the +5V line. With the supply switched on, the operation of the clock oscillator, the four decade counters and the

divide-by-two counter may be checked and should be observed to be running as a normal counter. The \bar{C} output should be constant at the logical "I" level, i.e. about + 5V. If the digital indicators have been connected, they should be continually indicating zero and the overload indicator should be OFF.

If the switch input is now disconnected from ground, the four decade counters and the divide-by-two flip-flop should become permanently set to zero and stop counting after three complete cycles of the main counter. The "hold" output should also become logical zero. On re-connection of the switch input to ground, the main counter

should start recounting and the "hold" output become logical "1" again. If the V_o input is now disconnected from the +5V line and connected to ground the A flip-flop should be observed dividing by two and the \overline{C} output should become constant at the logical zero level. This completes all the useful checks that can be made before interconnecting the analogue and digital circuit boards and if all the tests have proved successful, this should now be done. If not, the wiring should first be checked (this should, of course, have been done before any testing was carried out) and then an attempt made to discover any faulty components.



With the analogue, digital and power supply boards interconnected, the digital and overload indicators connected, the V_{in} inputs shorted together and the switch input connected to ground, the power supplies should be switched on. If all is working correctly, a voltage of a few millivolts, positive or negative, will probably be indicated and should be adjustable to zero by means of R_4 and/or R_5 . To test that the circuits are functioning correctly, a variable voltage source of from just under -2V to just over +2V should be applied to the V_{in} inputs. Varying this input voltage source between its limits should result in digital readings, of correct polarity, corresponding approximately to the applied voltage. Indicated readings greater in magnitude than 1999 should result in an overload indication. If reversed polarity indications are given, it is a simple matter to correct this by reversing the connections of P_1 and P_2 to the digital circuit board.

The auto/manual function can be checked by disconnecting the switch input from ground. If all is well, the display will become "frozen" and will not alter when the input voltage is varied. Upon reconnection of the switch input to ground, the digital readout should again follow the input voltage. Final adjustments to R_4 and R_5 can now be made and should be carried out in the following manner. With the V_{in} inputs shorted together, disconnect the switch input from ground to freeze the display. This effectively short circuits the output from IC_6 to its negative input. Next, connect a voltmeter between ground and the V_o output. When R_{4} is adjusted correctly, the V_{o} output will be at about +5V. As the wiper of R_4 is adjusted, positively and negatively, about this position, a point on either side will be found where the V_{a} output falls to zero volts. For a correct setting, the wiper of R_4 should be exactly mid-way between these two points. Having adjusted R_4 , reconnect the switch input to ground and adjust R_5 for a zero digital readout. The V_{a} output will be observed to be indicating about +5V with the occasional "kick" towards zero volts. The rate at which the "kicks" occur is an indication of the goodness of the zero adjustment. The less frequent the kicks, the better the adjustment. A kick once every second indicates a zero adjustment ten times better than that digitally indicated, i.e. to within $100\mu V$ of the true zero. (Remember, the least significant digit is 1mV.) Apart from the accurate adjustment of the two reference voltages, this completes the testing and setting-up of the basic digital voltmeter circuits. All that remains now is to construct and test the a.c./d.c. input stages. This should present no difficulty, and apart from the adjustment of R_{51} , final adjustment of the remaining preset controls should be left until the instrument is finally housed. When the circuit of Fig. 8 has been constructed, R_{51} should be adjusted for zero direct volts at the junctions of the collectors of Tr_3 and Tr_4 . When the instrument is complete, R_{46} becomes the zero adjustment for direct voltages, and R_{63} becomes the zero adjustment for a.c. voltages.

Before proceeding to a discussion on the calibration of the instrument there is a detail

Specification

Ranges. 200mV full-scale a.c. and d.c. 2V full-scale a.c. and d.c. 4V full-scale a.c. and d.c. 20V full-scale a.c. and d.c. 40V full-scale a.c. and d.c. 200V full-scale a.c. and d.c. 400V full-scale a.c. and d.c. (Readings multiplied by two on 400mV, 4V etc.) 400mV full-scale a.c. and d.c. (Maximum resolution $100\mu V$.)

Input impedance. 500M Ω up to 4V full-scale. 10M Ω and 10pF above 4V.

Display. $3\frac{1}{2}$ digits. Overload indication. Readings up to 2500. Polarity indication.

Accuracy. Error less than $\pm 0.1\%$ of reading, $\pm 0.05\%$ full-scale on direct voltage readings. Less than $\pm 0.5\%$ of of reading, $\pm 0.05\%$ full-scale on alternating-voltage ranges.

Frequency range. 30Hz to 100kHz.

Mode. Continuously-sampling or manual "hold".

that has not, so far, been mentioned; it is the positioning of the display's decimal point for the various ranges. This may be easily achieved by adding an additional single-pole, four-way wafer to the range switch (S_1 , Fig. 8). Thus as the range switch is altered, the appropriate decimal point of the four digital indicators is connected to the + 5V line.

Another, and final, point is the functioning of the polarity indicators when switched to the alternating voltage ranges. It is suggested that an additional pair of single-pole, 2-way contacts are added to the a.c./d.c. function switch $(S_2, Fig. 8)$. In the d.c. position, these two sections should connect the J and K inputs of the polarity flip-flop to the emitter of Tr_6 and the collector of Tr_9 , respectively. Correct polarity will be thus indicated as previously described. In the a.c. position, these contacts should connect both J and K inputs to the +5V line, with the result that an alternating, plus and minus polarity indication will be given. The rate of alternation will vary from 10Hz to 5Hz for input voltages varying from zero to full scale deflection, respectively.

Calibration

Assuming that the constructor has finally housed the circuit boards and other components, and connected them up, the first step in the calibration of the instrument is the adjustment of the two reference voltages $(R_1 \text{ and } R_2, \text{ Fig. 3})$. To do this, switch the a.c./d.c. function switch to "d.c.", the range switch to "2V" and the display switch to " \times 1". Short circuit the inputs and adjust the d.c. zero for a zero reading. Apply an accurately known direct voltage of a little less than +2V to the inputs and adjust the negative reference voltage until a digital reading exactly equal to the applied voltage is obtained. Reverse the polarity of the applied voltage and adjust the positive

reference voltage for a correct digital reading. The basic range of the d.v.m. has now been calibrated and the remaining calibration adjustments should be carried out in the following order.

1. Switch the display switch to " $\times 2$ " and apply a known voltage of a little less than +4V. Adjust R_{64} (Fig. 8) for a display reading of exactly half this applied voltage.

2. Switch the range switch to "200mV" and the display switch to " \times 1" and apply a known voltage of a little less than + 200mV. Adjust R_{47} (Fig. 8) for a display reading equal to the applied voltage.

3. Switch the range switch to "200V" and apply a known voltage of a little less than +200V. Adjust R_{68} (Fig. 10) for a display reading equal to the applied voltage. (Calibration of the ×100 attenuator may be carried out on the 20V range by applying a known voltage of just under +20V if a known voltage of the order of +200V is

not available.) 4. Switch the range switch to "2V" and the a.c./d.c. switch to "a.c." and adjust the a.c. zero for a zero reading with the inputs shorted together. Apply a known a.c. voltage of just under 2V r.m.s. at a frequency of about 1kHz and adjust R_{57} (Fig. 8) for a display reading equal to the applied voltage.

5. Switch the range switch to "200V" and apply an alternating voltage of about 300Hz, adjusting it for a digital reading of just under 200V. Vary the frequency of the signal, maintaining a constant output voltage, to about 90kHz and adjust the variable capacitor of the $\times 100$ attenuator until the original voltage is indicated. (As for the 200V d.c. range, the capacitor of the $\times 100$ attenuator may be adjusted with the range switch switched to the "20V" range and applying a variable frequency signal of just under 20V, should a 200V signal not be available.)

The accuracy of the above calibration procedure depends upon the accuracy of the known test voltages and these, ideally, should be better than $\pm 0.05\%$ for the d.c. ranges and better than $\pm 0.5\%$ for the a.c. ranges. Possibly the ideal method is to measure these test voltages with an already calibrated d.v.m. of greater accuracy than the subject of this article. Obtaining the use of such an instrument may be difficult for the amateur constructor but, in this respect, it is thought possible that some local universities *may* be willing to allow access to their electronic instruments. If not, other solutions may, hopefully, present themselves to the constructor.

Component suppliers

Ancom Ltd, Devonshire St, Cheltenham, Glos. RS Components Ltd, P.O. Box 427, 13–17 Epworth St, London EC2P 2HA.

(RS Components Ltd will only supply retailers, trade service technicians, industrial or educational users. Retailers are able to order components for private buyers.)

Semiconductor Supplies, 55 Whitehorse Road, Croydon CR0 2JG.

Vero Electronics Ltd, Industrial Estate, Chandler's Ford, Eastleigh, Hants.

(Veroboard—a similar material is available from RS Components.)

November Meetings

Tickets are required for some meetings: readers are advised therefore to communicate with the society concerned

LONDON

18th Oct. RTS - "Advanced electronic editing systems" by J. Southgate at 19.00 at London Weekend Television, South Bank TV Centre, Upper Ground, SE1.

25th Oct. SERT - "Some future trends in colour TV tubes" by G. R. Diacon at 19.00

at IBA, 70 Brompton Rd., SW7. Ist. IEE — "The management challenge for electrical engineers" by Dr. A. C. Copisarow at 17.30 at Savoy Pl., WC2. Ist. RTS — "Cable access at Bristol" by P.

Lewis and colleagues at 19.00 at London Weekend Television, South Bank TV Centre, Upper Ground, SE1.

2nd. IEE/IERE — Colloquium on "Mass spectro-metry at 14.30 at Savoy PL. WC2. 5th. IEE/IERE — Colloquium on "Display

technology" at 10.30 at Savoy Pl., WC2. 6th. IEE — "Performance of modern thyratrons"

by H. Menown at 17.30 at Savoy Pl., WC2. 6th. IEE — "The position of the graduate engineer in a large company" by T. Mayer at

18.30 at Imperial College, Exhibition Rd., SW7. 7th. IEE — "Some new possibilities in radar and navaids" by Prof. E. D. R. Shearman at

17.30 at Savoy Pl., WC2. 7th. BKSTS — "The changing world of the news cameraman" film at 18.15 lecture at 20.45 at the National Film Theatre. South Bank, Waterloo, SE1.

8th. SEE -"Use of dessicants in electronics and packaging" at 18.00 at Imperial College, Exhibition Rd., SW7.

13th. AES "Professional microphones their use and misuse" by Antony Askew and Angus McKenzie at 19.15 at the IEE, Savoy Pl., WC2.

14th. IERE - Colloquium on "Domestic equip ment control systems" at 14.00 at 9 Bedford Sq., WC1.

14th. IEE -"Data communication by packet switching" by Prof. P. T. Kirstein at 17.30 at Savoy Pl., WC2.

15th. IEE — "Lord Kelvin and his measuring instruments" by J. T. Lloyd at 17.30 at Savoy Pl., WC2.

15th. IEE — "Novel photo-detectors using semi-conductor interfaces" by Dr. M. J. Hampshire at 18.00 at Thames Polytechnic, Riverside House Annexe, Beresford St., SE18.

16th. IEE - "The broadcasting of traffic information to road vehicles" by R. S. Sandell at 17.30 at Savoy Pl., WC2.

20th. IEE — "High capacitance strain gauge for use at extreme temperatures" by Dr. B. E. Noltingk at 17.30 at Savoy Pl., WC2. 20th. IERE — "Developments in position measure-

ment techniques" by D. J. Phipps at 18.00 at

9 Bedford Sq., WC1. 22nd. IEE — "On the design of low-pass, linear phase, recursive digital filters" by Prof. S. C. Dutta Roy at 17.30 at Savoy Pl., WC2. 22nd. RTS — Shoenberg Memorial Lecture "The

Open University: a progress report and hopes for the future" by Dr. Walter Perry at 19.00 at the Royal Institution, Albemarle St., W1. 26th. IEE — Discussion on "Measurement, test

and quality control of fuses with particular reference to low voltage fuses" at 17.30 at Savoy Pl., WC2.

28th IEE - Discussion on "Semiconductor devices in hostile electrical environments" at 17.30 at Savoy Pl., WC2.

28th. IERE — "Design and application of active compensation circuits for servo control systems" by Dr. D. R. Wilson at 18.00 at 9 Bedford Sq., WCL.

28th. BKSTS - "Opticals in creative art" at 19.30 at Thames Television Theatre, 308-316 Euston Rd., NW1.

29th. IEE — "The development of microwave transmission systems" by Dr. P. A. Matthews at 18.30 at King's College, Strand, WC2.

ABERDEEN

6th. IERE/IEE --- "Medical and industrial elecfrom text book to shop floor" by J. G. Mitchell at 19.00 at Robert Gordon's Institute of Technology, St. Andrews St.

BELFAST

13th. IERE — "Forum on designing for reliability" at 18.30 at Main Lecture Theatre, Ashby Institute, Queen's University, Stranmillis Rd.

BIRMINGHAM

21st. IERE --- "Pin-wheels to pulses: electronics --servant of postal sorting" by S. W. Godfrey at 19.00 at City of Birmingham Polytechnic, Franchise St., Perry Barr.

BOURNEMOUTH

20th. IERE --- "Solid state microwave sources"

by H. J. Finlay at 19.00 at the Technical College. 27th. SERT — "Servicing aspects of recent Thorn colour TV receivers" by B. Hinton at 19.15

at Room B7, Bournemouth College of Technology.

BRISTOL

15th. SERT — "Television for the blind: an eye-opener into the medium" by J. Rossetti at 19.30 at Cabot House, Bristol Polytechnic, Ashley Down Rd

28th. IERE/IEE - "Video recording" by J. Jeffrey at 18.00 at Queen's Building, the University.

CARDIFF

14th IERE — "Solid state microwave power amplifiers" by G. B. Morgan at 18.30 at Dept. of Applied Physics, UWIST.

СНАТНАМ

Ist. IERE —"Electronics in the commercial vehicle industry" by G. Leonard at 19.00 at the Medway and Maidstone College of Technology.

CHELMSFORD 28th. IEE — "Telephony — past, present and future" by J. B. Terry at 18.30 at King Edward VI Grammar School, Broomfield Rd.

CHELTENHAM

20th. IERE/IEE - "Value for money in project management" by T. G. Clark at 19.30 at G.C.H.Q. Oakley.

EDINBURGH

7th. IERE/IEE - "Medical and industrial electronics — from text book to shop floor" by J. G. Mitchell at 19.00 at Napier College of Science and Technology, Colinton Rd.

GLASGOW

8th. IERE/IEE - "Medical and industrial electronics — from text book to shop floor" by J. G. Mitchell at 19.00 at Glasgow College of Technology, Hanover St.

HIGH WYCOMBE 29th. IEE — "Developments in information display systems" by R. Stafford and Dr. T. Coutts at 19.30 at High Wycombe College of Technology.

HULL

14th. SERT - "Electronics in motor cars" by L. Phoenix at 19.30 at the E. H. Bullock Lecture Theatre, College of Technology, Queens Gardens.

LIVERPOOL

14th. IERE — "The role of electronics in the movement of shipping" by K. D. Jones at 19.00 at Dept. of Electrical Engineering and Electronics, the University.

LOUGHBOROUGH

13th. IERE -- "Fourier analysis of video telephone systems" by Dr. D. E. Pearson at 19.00 at Edward Herbert Building, the University.

MANCHESTER

8th. IERE - "Marconi automatic testing" by W. J. Stickland at 18.15 at Renold Building, UMIST.

NEWCASTLE-UPON-TYNE

14th. IERE — "Codes and coding" by J. T. Kennair at 18.00 at Main Lecture Theatre, Ellison Building, the Polytechnic, Ellison Pl.

NEWPORT, l.o.W. 9th. IERE — "Colour television" by A. C. Maine at 19.00 at Isle of Wight Technical College.

PLYMOUTH

7th. RTS/AES - "Quadraphonics" by Dr. Keith Barker at 19.50 at Plymouth Polytechnic.

15th IERE/IEE — "Developments in digital transmission systems" by G. H. Bennett at 19.00 at Main Hall, the Polytechnic.

PORTSMOUTH

14th. IERE — "What's new in multilayer printed wiring board manufacture" by G. C. Wilson at 18.30 at the Polytechnic.

READING

8th, IERE/IEE — "Ambisonic reproduction of sound" by Prof. P. B. Fellgett at 19.30 at the J. J. Thomson Physical Laboratory, University of Reading, Whiteknights Park. 29th. IERE - "Digital filters" by A. R. Owen

at 19.30 at the J. J. Thomson Physical Laboratory, University of Reading, Whiteknights Park.

SHEFFIELD

28th. IERE/IEE --- "World wide communication" by R. T. Mayne at 18.30 at the University.

SOUTHAMPTON

20th. SERT - "Television receiving aerials" by R. S. Roberts at 19.30 at the Technical College.

Entertainment Electronics at Berlin

2nd International Radio & Television Exhibition

The motto of the second international radio and television exhibition in Berlin was 50 years of German radio broadcasting, but by far the biggest attraction was video equipment. With more than a dozen different formats on show for picture playback over television receivers, the choice between four surround-sound systems takes a decidedly back seat.

The Philips long-playing video disc (VLP) system was a major feature at the show. Philips technique allows a maximum playing time of 45 min, though when the system is marketed in 1975 it will probably use a 30-min playing time, from a 30-cm wear-free disc.

Because the VLP discs contain one television picture per revolution a variety of operating modes are available: fast forward play (at twice normal speed), reverse continuous still picture, frame-byframe reproduction, slow motion forward and reverse (adjustable from 40ms to 4s), as well as normal picture reproduction. A remote control unit allows any of 45,000 frames to be selected, amounting to almost immediate random access, and because frame-to-frame crosstalk is sufficiently low each frame can be completely different. This gives the VLP potential outside the entertainment and instructional fields.

At the exhibition details of the optical scanning, signal processing and control systems were released, but first a recap.

The disc is impressed with picture information in the form of a spiral "track" consisting of a series of 0.8- μm wide, 0.16- μ m deep pits of variable length and at variable intervals. The repetition rate of the pits carries the brightness signal and the length of the pits conveys the colour and sound information. The rigid disc, made from a transparent vinyl polymer $l_{\frac{1}{4}}$ mm thick, is coated on one side with a thin metal reflecting layer and information is "read off" by a beam of plane-polarized light from a 1mW helium-neon laser. Light is reflected by the record, picked up by a lens again and focused onto a photodiode, less light being received when a pit passes in front of the lens, due to diffraction, than when a smooth part does.

With a pitch of 2 μ m (for a 30-min disc), the track density is 500 turn/mm. Half-brightness spot size is about 1 μ m at the pit but is much smaller at the

transparent surface so that contamination or damage have comparatively little effect. The focused spot is located in the plane of the pits and kept there by a control system.

Another opto-electronic control system positions the beam to within $\pm 0.2 \ \mu m$ from the track centre and shifts the optical system radially at 50 $\mu m/s$, corresponding to 2 $\mu m/rev$. Rotational speed is 1500 rev/min for the PAL version (an 1800 rev/min machine for NTSC is due at the end of this year) or 25 rev/s, allowing one picture (two fields) per revolution, held to within 0.1% by a further control system.

Master records from which the moulds are made for pressing VLPs are made from glass, with a photoresist layer 100 to 160nm thick that is cut by a high power laser. This is done in real time, with the potential that a scene can be recorded directly from a video camera. The moulds are made in the usual way from the master by electroplating.

Signal processing

The photographic process used in writing information onto the master record is highly non-linear, so a digital recording technique is the only practical way of going about things. Using the VLP coding method, it turns out that at 25 rev/s the maximum video bandwidth is 3MHz at the inner part of the record (10cm diameter). Thus if the normal PAL video signal was used as modulation all of the colour information would be lost, this being carried either side of 4.43MHz. So the colour subcarrier frequency is reduced to 1.46MHz, with a bandwidth of ± 500kHz. For stereo sound, two f.m. carriers are used, one at 350kHz and one at 650 kHz, (Fig. 1) with $\pm 50 \text{kHz}$ deviation.

Brightness information, limited in bandwidth to 3MHz, frequency modulates a 6MHz, carrier with a modulation index of less than unity. This gives first-order sidebands wider than the deviation and extending \pm 3MHz either side. These signals — brightness, colour and sound — are added in the amplitude ratios of 20:4:1, symmetrically limited and then recorded. Limiting provides rectangular pulses in which brightness is contained as frequency modulation, while colour and sound give a symmetrical width



Fig. 1. If the normal PAL video signal modulated the VLP disc carrier directly, colour information encoded at 4.43MHz would be lost as video bandwidth is about 3MHz. Therefore the colour information is transposed down to 1.46MHz, while luminance information frequency modulates the 6-MHz carrier, only the first lower sideband being recorded.

modulation of the pulses (Fig. 2). In effect, the sound and colour signals are singlesideband modulation of the brightness signal as the carrier and symmetrical limiting produces the upper sidebands — at the expense of power in the lower sidebands, of course.

In the recording unit, the brightness information is taken from the PAL video signal by a 3MHz low-pass filter prior to modulating the frequency of a multivibrator circuit. This gives rectangular pulses whose harmonics must then be filtered out so that the f.m. brightness signal has a sufficiently low rise time to show pulse width modulation (by the colour and sound signals) after combination and limiting.

The colour signal from the original video signal is filtered out and fed to a variable-gain amplifier to maintain constant level of colour signal, as derived from the bursts, and then reduced to 1.46MHz.

The playback unit has several interesting features. Apart from demodulating the brightness and sound signals it must restore the colour subcarrier frequency to 4.43MHz for playback on domestic TV receivers.

Originally, the recorded colour subcarrier frequency was 1MHz, and the PAL subcarrier at 4.43MHz was restored using a double mixing technique together with a $\div 64$ phase-locked loop to synchronize a 1MHz oscillator to the line sync frequency. The current system is different, in that the colour carrier is changed to 1.46MHz — to allow an increase in modulation depth — and the colour-burst frequency is used as a reference instead of the line sync frequency. To recreate the PAL colour signal with the requisite stability, two signals are formed; one containing the required colour modulation and the other having the appropriate stability. These two signals are made 4.43MHz different and they are both given the same frequency shift due to speed changes; thus subtractive mixing gives the reconstituted PAL colour signal.

In practice, a 1.46-MHz oscillator is gated by the 4.43-MHz colour burst, plus errors in frequency, and locked with a kind of flywheel sync circuit, so that the 1.46-MHz signal takes up the errors. This is mixed with a 4.43-MHz crystal oscillator to give a 5.89-MHz carrier, which apart from the errors due to speed changes is otherwise stable. Finally, this is mixed with the colour signal from the record i.e. a modulated 1.46MHz plus drift. The modulated difference signal, with no drift and the stability of the crystal, is the PAL colour signal.

A useful feature is the drop-out detection circuit. Here information below 2.5MHz is detected for drop-out. If a pit is missing, the detector responds to the lowered frequency by operating a switch for 3 μ s to allow the brightness of the preceding line to be used instead. (A 64 μ s delay line holds this.) In practice this switch operates before the signal gets to the f.m. demodulation circuits. When drop-outs occur the colour information is switched out. Because of the averaging with the signal in the previous line in PAL receivers, the missing colour fragments appear at half saturation, thus preventing spikes. There is also a sample and hold circuit in the sound channel used to counteract changes in signal level during a drop-out.

Control systems

Constraints on the optical system result in a wide aperture and hence small depth of focus. As the depth of focus is 1 μ m and the vertical record position may differ by up to 500 μ m from a true plane, you can see the need for this to be accurately controlled!

Displacements are detected by measuring capacitance between the metallized surface of the record and a 1 cm^2 electrode bonded to the objective lens. At a distance of 100 μ m an accuracy of 1% is sufficient to determine the objective position by 1 μ m. The lens is suspended in springs and driven by a coil in a radial magnetic field, rather like a moving coil loudspeaker. Capacitance is measured using an oscillator and f.m. ratio detector.

Two control systems are used to follow the pit track, one for slow tracking of the spiral and the other for rapidly centring the spot in presence of eccentricity. To keep the spot on the track, it can be moved radially by a mirror and coil pivoted in a magnetic field behind the objective lens. Control signals are obtained with two auxiliary light beams focused on either side of the track and reflected from the record surface onto two photodiodes. The difference between photodiode outputs controls the pivoting mirror.

For fast, slow, reverse-motion and stationary pictures. a rapid movement during the field flyback period is needed. The mirror movement can behave like a ballistic galvanometer as the opened control loop has a low resonant frequency; the jump is effected therefore by opening the loop, applying an accelerating current pulse through the coil followed by retarding a pulse, and then closing the loop. The average current in the mirror coil controls the radial transport mechanism to move the optical system across the record.

Record speed is held to $25Hz \pm 0.1\%$ by a further control system that operates from a tachogenerator coupled to the turntable shaft.

Optical systems

In "reading out" information from the track pits, a lens is used with a numerical aperture of 0.4. Spot size is about the theoretical minimum at this aperture, and diffraction, together with the radial Gaussian intensity distribution at the lens entrance pupil, produces an half-intensity diameter of 0.9 μ m. Because the pit size is smaller than this, light is diffracted and falls largely outside the lens aperture. Maximum light is transmitted to the photodetector when pits are absent.

As the laser beam is linearly polarized, a quarter-wave plate and polarizing mirror ensure that incident and reflected light beams are effectively separated (Fig. 3).

For maximum modulation of the photodetector current, reflected light from a pit must have a phase difference of 180° from that reflected from the surface in the vicinity of the pit. This is arranged by making the pit a quarter-wavelength deep. The two intensities should be equal of course, and this is achieved by dimensioning spot and pit sizes so that the same amount of light falls outside a pit as falls into it. (Modulation depth achieved at the inner-most part of the track and at 7MHz pit frequency, is 15%.)

Despite this constraint, the most important thing in determining spot size is the highest recorded pit frequency, nominally 6.5MHz. This can be altered by an intermediate lens (Fig. 3) which can make the Gaussian beam distribution at the entrance pupil of the main lens wider or narrower. The greater the homogeneity in the light distribution the smaller the spot and thus the higher the maximum recorded pit frequency.

The trade off is power in the laser beam and the particular compromise chosen means that 80% of laser power is used. The remaining inhomogeneity of the beam results in a bandwidth $92\frac{1}{2}\%$ of the theoretical maximum. If 99% of laser power were used the bandwidth would be 16% smaller.

Crosstalk from neighbouring tracks is readily assessed because they have different pit frequencies. A crosstalk level of -50dB has been measured for $1-\mu m$ track widths which is said to be in good agreement with a level calculated by Fourier analysis.

Wireless World, November 1973

With all this complexity the VLP player is not going to be cheap, about the cost of a colour receiver, Philips say. Nor do we expect two other optical (laser) systems (MCA Disco-Vision and one by Thomson-CSF) to be any cheaper. To make biggest impact, video systems will need to be much less expensive than that and even the Teldec TED player is costly at £200 (DM1148). The TED system will be sold in Germany from January, with Scandinavia and the U.K. to follow later. The TED disc catalogue lists well over 100 titles with discs priced between DM10 and 25.

Philips are already talking with potential licensees as well as having discussions over standardization with MCA in the USA. Clearly, the existence of competing systems is going to seriously weaken video disc potential. Its quite unlike the $33\frac{1}{3}$ -45 rev/min situation or the surround-sound systems competition where the same mechanism is common to all systems. This situation will also hold back penetration of video cassette/cartridge systems, as many potential buyers will presumably hold back if a disc system with its attraction of lower-cost programmes is not too far off.

There would appear to be potential in the VLP for wide bandwidth sound coding. As the VLP system is digital, presumably the p.c.m. technique would be a possibility (see, for instance, page 548). Then we could have colour pictures and high quality multi-channel sound off the same mechanism; with amplitude response down to as low as you like, no wow and flutter, no rumble, no tracing distortion, and no distortion due to tracking error. Alternatively, one could use the wide bandwidth solely for frequency-division multiplexing with the capability of storing 30 programmes on one disc. Roll on ALP!

Magnetic video disc

Whether other systems being developed will offer lower-cost players remains to be seen, but another technique, using a magnetic disc, promises low-cost hardware presumably at the expense of higher disc cost as a result of the more expensive duplicating process. This is the Rabe-Bogen magnetic disc recorder (MDR) mentioned briefly last issue. Here the idea is to make use of the turntable already present in many homes. Unlike the optical and mechanical systems, it allows home recording.

A mechanical system is used to guide the magnetic record and playback head using the stylus-in-groove system. The newly developed head, with its effective gap width of 250 to 350nm, glides across the specially treated record surface. The magnetic material is chromium dioxide with a microstructure of the order of the recorded wavelength (500nm).

A rotational speed of 156 rev/min (giving a linear velocity varying from 1.63 to 2.42m/s at 20 and 30cm diameter respectively) and a track spacing of $25 \,\mu m$ results in a playing time of 12 min per side. Bogen are currently working to reduce this to 78 rev/min to give

24 min per side. Storage density is 1.57×10^9 bits per side with a track spacing of 50 μ m and 3.14×10^9 bits per side at 25 μ m — very high compared to the nominal 20,000 bits /in² mentioned in our video tape cassette survey (Dec. 1972 page 580). Bogen claim that turntable speed variations are not a problem as monochrome receivers have a synchronization range of around $\pm 10\%$.

How convertible existing turntable mechanisms without a 78 rev/min speed are we're not sure, but even if they are not, this method would still probably have a cost advantage. At $33\frac{1}{3}$ rev/min, eight audio channels become feasible, with a playing time of 56 min per side.

Video cassettes

The Electronics Industries Association of Japan has recently decided to adopt three video cassette systems as standards for video tape recorders. This is an addition to the existing CP-508 standard for cartridge video machines. This last standard covers a 1.3cm $(\frac{1}{2}in)$ tape cartridge system (the EIAJ define a cartridge as containing one tape reel and a cassette as having two) initially developed by Matsushita in 1971. Marketing of equipment for this system has been held back until now, and as a result the standard for cartridge video recorders was agreed before market introduction. Since then National have been joined by Sanyo, Toshiba, Shiba Electric, General Corporation, Victor Company, Mitsubishi and Hitachi.

Matsushita have three variants of their NTSC machine; one for record and playback, o_{He} including a TV tuner, and one for playback only. The NV5120E shown was a PAL version of the record / playback model (see photograph). The 1.3cm tape used in these machines is interchangeable with that used on open-reel video tape recorders.

With cassette machines, both 1.9cm $(\frac{3}{4}in)$ and 1.3cm tape systems have been adopted. The three systems are: the 1.9cm system^{*} adopted by Sony, Matsushita and the Victor Company of Japan (now joined by TEAC and Nippon Electric Company); the 1.3cm system of Philips (now adopted by 15 European manufacturers, one in the U.S.A. and Hitachi/Shibaden in Japan); and the 1.3cm system of Sanyo.

For the 1.9cm cassette, the reels are positioned in a similar way to an audio or digital tape cassette with the two reels in the same plane, Fig.4a. Here the tape needs to be slanted in relation to the head. As with most cassette systems the tape has to be extracted by a complex mechanism but fast winding must be done when the tape has been returned to its cassette. In the Philips 1.3cm cassette the two reels are concentric,

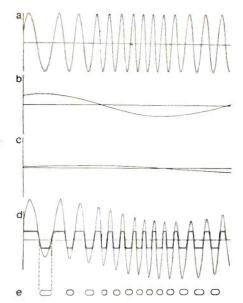


Fig.2. In coding the VLP, symmetrically limiting signals for luminance (a), colour (b) and sound (c), and combining in the ratios 20:4:1, produces a train of rectangular pulses whose frequency represents brightness and whose duty cycle carries colour and sound information.

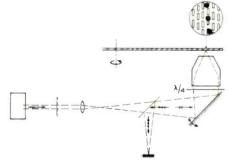


Fig. 3. In the VLP optical system, electromagnetic transducers are attached to the objective lens for focusing and to the mirror for centring and tracking. Laser beam is split by a diffraction grating to provide the two auxiliary spots before and after the main spot. Detectors either side of the main beam sense the reflected auxiliary beams to provide control signals for mirror movement.

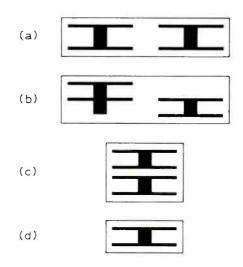


Fig. 4 Four reel arrangements now standardized by the EIAJ for domestic video cassette/cartridge systems.

Fig.4c (see also page 582 December 1972 issue), but as the tape is already slanted, the loading mechanism is simpler. In contrast to the 1.9-cm cassette, fast winding is done around the head wheel. Both head wheel and tape move in the same direction to alleviate problems of the chromium dioxide tape sticking to the head wheel, making recorded tapes incompatible with open-reel machines.

In the Sanyo cassette, Fig.5b, tape loading is similar to the 1.9-cm system, except that the capstan itself withdraws the tape. Fig.5d depicts the cartridge for comparison.

Bell & Howell, who market JVC video equipment in Germany, Italy, Scandinavia and the U.K., will be selling the new 1.9cm U-VCR machines made by JVC. Two PAL versions will be sold in Europe, the CR6000E recorder /player and the CR5000E player, both with remote control units.

RCA, who showed their MagTape SelectaVision video cassette system, have eliminated the complicated tape withdrawal mechanism used in most other cassette systems. The 1.9cm tape remains in the cassette and when inserted into the player, contact is made with the heads by the headwheel entering the cassette, allowing a 90° tape wrap. But this simplification hasn't produced a low-cost machine. The recorder/player costing \$795, and a camera costing \$300, will be marketed early next year. The player includes receiver circuitry for recording television programmes.

Another notable video machine is the VTC 7100 Sanyo 1.3cm cassette recorder. Weighing 5.5kg with batteries it is a portable machine made for the C.C.I.R. norm and is accompanied by a hand-held camera weighing 2.3kg. The cassette measures $155 \times 107 \times 25$ mm and plays for 20 min. It uses two heads normally and four for slow-motion playback.

Sanyo will be selling a PAL version of the colour recorder VTC7200 in August next year.

So the current total of video playback systems announced so far seems to be: five disc systems, four cassette tape systems, one cartridge tape system, four film players, as well as various open-reel tape machines. (Two systems have recently disappeared — Cartrivision and Ampex Instavideo.)

Surround sound

It was good to see Nippon Columbia publicly demonstrating their UMX system. This was devised by Duane Cooper of the University of Illinois and development of it has been taken up by Nippon Columbia. It arose out of considering which was the best way to transmit directional information, and theoretical analysis by Dr Cooper, using an harmonic synthesis approach, has turned up a universe of matrix systems, called UMX.

What comes out of the analysis is a two-channel phasor matrix system, called BMX, in which full mono compatibility is guaranteed, unlike QS and SQ, by deriving a truly omnidirectional signal (in

^{*}We have recently heard from Action Video Ltd that they are modifying N.T.S.C. versions of the $\frac{3}{2}$ in U-VCR Sony designed cassette recorders to the PAL system. Action Video are at 45 Great Marlborough Street, London W1.

the horizontal plane) and in which a difference signal, of the same level, has a phase shift that lags the mono signal by an amount equal to the source angle measured from a certain norm. Simple sum and difference matrixing produces left and right signals whose amplitude coefficients are the same as for the QS system (see page 56 February 1972 issue), but the phase shifts are distributed in lots of 45° rather than zero or 90° .

The chief property of the matrix is that the phase relations between speaker outputs in four-speaker playback are rotationally symmetrical, the crosstalk components of a corner sound having a phase of -45° and $+45^{\circ}$ relative to the wanted corner sound. Experiments have shown 45° phase differences to be less "oppressive" than 90° phase differences. As well, localization is aided by this phase arrangement.

More interesting than this is the way in which the two base-band channels can be augmented by further channels to improve "directivity" and reduce sensitivity to listener position. Two supplementary channels, both phase-encoded omnidirectional channels, can be added to the base matrix at the consumers discretion, assuming they are present in the transmission media. This in fact is Nippon Columbia's proposal in essence that the carrier channels are there for the taking, the baseband channels giving a better surround-sound capability in themselves than other basic two-channel matrix systems.

The total of four channels provides a "discrete" system, but it has been found that a discrete effect is obtained with narrow-bandwidth carrier channels of around 3 or 4kHz. These frequencies modulate a 30kHz carrier with a deviation of ± 6 kHz and at a carrier level of 35.4mm/s. The maximum frequency of 36kHz means that a much wider range of pickups can be used with this system. Additionally, noise reduction techniques are not used, with the potential of cheaper decoders, and special stylus shapes and record materials are not necessary. Ordinary cutting equipment (Neumann SX68) can be used for manufacturing, according to Nippon Columbia, using half-speed cutting with tracing distortion correction. Even 17cm (7in) discs can be made.

It seems a great pity that this elegantly superior system is not available yet on the market, although Nippon Columbia have equipment at the ready. Maybe the uncommitted record companies, like Decca and Polygram, are looking to video disc techniques! But as there are three other surround-sound systems being marketed we think this one is deserving of at least an equal place in the market.

There is also a Qmx technique for surround-sound tape cassettes, which has a signal-to-noise ratio advantage over the proposal to divide the cassette tape into eight separate tracks. This is now more than a proposal as JVC are showing their four-channel cassette machine (noted on page 460, September issue) which claims a 48dB signal-to-noise ratio with the JVC automatic noise reduction system.

Sansui were demonstrating integratedcircuit versions of their Variomatrix QS/RM circuitry. Three Hitachi chips will be available shortly in production quantities and they report considerable interest from European companies for their system. SQ is making inroads on the Continent, with Blaupunkt, Braun, Elac, Grundig, Körting, Loewe-Opta, Philips, Revox, Saba, Sharp, Siemens, Telefunken and Wega building in decoders. Connaught Equipment (Tate) announced an improved SQ automatic control technique that reportedly gives an all round 20dB separation, but details are not being released vet.

National were demonstrating fourchannel broadcasting by distributing composite f.m. transmissions at 103.5MHz to the Dorren Quadraplex system for reception by exhibitors. Dorren has also produced a chip for CD-4 demodulation. Claimed to be the biggest consumer i.c. produced, it is an l.s.i. 28-pin circuit with 320 transistors on the chip, and will be available in December.

But the most striking surround-sound demonstration at Berlin was the Sennheiser dummy-head stereo documentary disc. Intended for open-air headphones it sounds excellent with the closed type too. With it, one can apparently perceive sound images over three dimensions with astonishing realism using merely a dummy head containing two microphones, ordinary stereo equipment and stereo headphones. The record must be heard to be believed[†]. There didn't seem to be any ambiguity, although the frontal images weren't quite as convincing as the back ones. During the exhibition stereo transmissions were made from RIAS, Berlin using this technique, and many press reports in Germany were calling this the sensation of the exhibition. Production of the record followed some interesting psychoacoustic work at the Heinrich-Hertz-Institut, on which we hope to report later.

Cassette machines

In this tenth year of the compact audio cassette one might have expected Philips to commemorate it in some way. Talk in recent years about four-channel, eighttrack cassettes led one to suspect that Philips may have overcome the problems associated with dividing down the track into eight sections, plus guard bands. Problems like reduced signal-to-noise ratio, worsened crosstalk, worsened tape wander and more critical tape/head alignment. But instead JVC have announced the very thing, using their automatic noise reduction system of DC-4 fame - a compatible competitor to the Dolby "B" system.

Grundig have adopted the Philips dynamic noise limiter in their CN710 and 720 machines, which both incorporate CrO_2 tape switches, and claim a 50-dB s/n ratio with CrO_2 tape and d.n.l. A number of new Dolby "B" machines were seen, including the Telefunken

C2200, Trio KX-700, Sharp RT-480H, Uher CG360 with Dolby i.c. and 10-watts per channel output power, Aiwa AD-1500 with a wow and flutter of 0.07% r.m.s. weighted (similar to Teac A-450 mechanism?) and 60dB s/n ratio with Gr0₂ tape, B & O Beocord 1700 with a claimed 61dB s/n ratio, and Dual C901 with wow and flutter of 0.09% r.m.s. weighted (0.12% DIN). Latest Dolby licensees are Garrard and Nordmende. A reported world shortage of chromium dioxide is slowing down penetration of the BASF Dolby cassettes and, while they were in evidence at Berlin, they are not expected to be marketed in the U.K. until late next year. Hitachi have a new machine, model D-4500, with a combined record and playback head, claimed to be the first of its kind and using a three-motor, dual-capstan system. They claim the astonishingly low wow and flutter figures of 0.035 to 0.05% r.m.s. weighted. Most interesting open-reel tape recorder was the new Revox A700, which will no doubt be seen at London's Audio Fair along with their digital-readout receiver and some other products we haven't

To round off, here are some things that won't be at Olympia. Like television sets with headphones - one by Nordmende uses an infra-red link and many have sockets for connecting external audio amplifiers, elaborate ultrasonic remote controls, and in-line picture tubes, digital channel identification superimposed briefly on the screen on channel changing (Blaupunkt), a "stereo-quadro superthing" by Blaupunkt reportedly containing 650 transistors, 35 i.cs and 127 l.e.ds and with no moving parts; SECAM/PAL converters by Grundig and Blaupunkt; a colour projection system by Sony based on the Trinitron tube; and plenty of European-made portable colour sets.

included.

As this report is entitled entertainment electronics we must mention the ITT-Shaub Lorenz Odyssee game device. This is a way of using a c.r.t. display to play games, in a similar way to the devices now appearing in some public houses. The ITT one is much better; it uses the domestic television receiver via the antenna input. The equipment includes waveform and video generators, programme cards that determine the display for one of ten games, modulator and sync circuits, vertical and horizontal movement controls for two players together with "ball" speed controls. When a "ball" and "player" meet ball direction is reversed. In some games, a coloured foil is attached to the screen to provide boundaries or tracks in the case of a track-following exercise. Options are table tennis, lawn tennis, volleyball, ice hockey, football, and five other amusements. Price is DM 400.

[†] We hope to demonstrate this record on the *Wireless World* stand during the Audio Fair at Olympia. It is available from Sennheiser's U.K. agent Hayden Laboratories Ltd. 17 Chesham Road, Amersham, Bucks, price 50p.

International Audio Fair

Olympia, October 23rd to 28th

An increased number of exhibitors over previous years will be at the Audio Fair this year. A list of the brand names at the show is printed overleaf and some of the equipment which will be shown for the first time is also described briefly. The show is to open from 10 a.m. to 9 p.m. except the final day, Sunday, from 11 a.m. to 7 p.m. Cost of admission will be 45p. *Wireless World* has again organized five of the lectures which will run during the course of the show.

Admission for the lectures is free, but tickets must be obtained beforehand, either from the information kiosk or through an exhibitor.

Lecture demonstration programme

Tues. 23rd Oct.

2 p.m. Sound synthesis for the amateur by Douglas Shaw

4 p.m. Quadraphony and music by Mike Thorne

6 p.m. High fidelity loudspeakers — fact or fiction? by Frank Jones

8 p.m. The available signal by Angus McKenzie (W.W. presentation)

Wed. 24th Oct.

2 p.m. Multi-channel sound recording systems by Dr. Keith Barker

4 p.m. Magazines — the technical interpreter by Basil Lane (W.W. presentation)

6 p.m. The progress of sound reproduction by Ralph West

8 p.m. Repeat of 6 p.m. lecture

Thurs. 25th Oct.

2 p.m. Keep it clean by Donald Aldous

4 p.m. Sound waves in rooms by Roger Driscoll

6 p.m. Test results and performance can they be related? by Dr. Arthur Bailey (W.W. presentation)

8 p.m. What goes on in a recording studio by Adrian Hope

Fri. 26th Oct.

2 p.m. A fresh look at audio noise reduction systems by David Rees (W.W. presentation)

4 p.m. The objective and subjective assessment of loudspeakers *by Gareth Jefferson*

6 p.m. A musical programme on how a record show is produced and presented *by John McGinn*

8 p.m. Quadraphony and music by Mike Thorne

Sat. 27th Oct.

2 p.m. The music scene and the recording heard

by Joan Coulson

4 p.m. Audio advertising by Rex Baldock

6 p.m. Practical limitations of audio equipment by J. L. Linsley Hood (W.W. presentation)

8 p.m. A live concert of contemporary music presented by Capricorn

Sun. 28th Oct.

2 p.m. New motional feedback loudspeaker system by Roger Driscoll

4 p.m. The record risibility factor by Donald Aldous

Special Event

On Tuesday 23rd at 11 a.m. there is the annual prize giving and presenting of trophies to winners of the British Amateur Tape Recording Contest, 1973.

Exhibition Briefs

The Shure V15 Mk III cartridge, introduced earlier this year has a new laminated magnetic core structure and a stylus assembly with a 25% reduction of tip mass.

A speaker system of interest from Eagle is a six-way system —two tweeters, two mid range and two bass units — the AA42.

The series 3400X stereo recorder will be shown by Tandberg. This is based on the recently introduced 3300X tape deck but includes 15W per channel amplifiers, integral speakers and linear motion output potentiometers.

A new amplifier introduced by Sinclair is the System 4000, providing 17W continuous power, both channels driven into 8ρ . Varicap tuning and a four-pole ceramic filter i.f. section are incorporated in the matching 4000 tuner.

Two recently announced Garrard automatic turntable units with belt drive (available in November) are the Zero 100SB and the 86SB. Both are powered by a screened four-pole synchronous motor fitted with a two-step pulley. The 100SB incorporates the tangential tracking arm of the earlier model plus an automatic record counter to monitor stylus wear. A turntable unit QZ100SC with a built-in fourchannel decoder for either CD-4 or SQ recordings will also be on show.

A new company at the Audio Fair will be N.E.A.L. (North East Audio Limited) who are producing a cassette model 102 which combines the 3M Wollensak transport mechanism with circuitry incorporating Dolby B, solid-state switching, twin p.p.ms, separate low noise, high overload margin input amplifiers for microphone, low level line and high level line (f.e.t.) inputs and separate switched recording and playback circuits for equalization of ferric and chrome tapes. The transport features bi-peripheral drive.

Philips will be demonstrating their motional feedback loudspeaker system, the principle of which was described in *Wireless World*, September 1973, pp.425-426.





New cassette recorder introduced by N.E.A.L. See overleaf exhibition brief.

Model 104 "reference" loudspeaker from KEF. The system has a new 8in mid-range/ bass unit, the voice coil of which operates safely up to 250°C, providing the new unit with a handling capacity of 50W. A B139 is coupled acoustically to the 8in driver.

ADC AKG Acoustic Research Agfa Akai Alba Alba Alpha Altec Amstrad Amtron Antiference Ateka Audio Packs Audio -Technica Audiotronics

BASF B&O BSR Macdonald B&W Bib Binatone Bose Brahms Braun Bush Arena

Calyx Cambridge Audio Connoisseur

Darby Decca Diamond Stylus Dynatron

Eagle Electrokit Empire Encore Era/De Banks

Ferguson Ferranti Ferrograph Gabraphone Gale Garrard Goldring Goodmans Grundig H.M.V. Hacker Hi Fi Aids Howland West

I.T.T. International Artists

J. Beam J. B. L. J. V. C.

Josty Kit KEF Keletron

Koss

Leak Murphy Learjet Marantz

Marconiphone Markovits Metrosound Musitapes Musonic

N.E.A.L. National Panasonic Nu-Way Onkyo

Paddock Tidy Philips Pioneer Plustronics Precision Tapes Pye Q.A.S. Quad Quadrasonics Revox Rola Celestion Rotel

SME Saba Sanvo Scan Dyna Securette Servosound Sharp Sherwood Shure Siemens Sinclair Sonab Sonotone Sonv Soundesign Sound-Picture Stax/Era Steepletone TDK Tandberg

Tannoy Tate Teac Teledyne Toshiba Trio Tripletone

U.D.T. Uher Ultra

Van der Molen Videosonic Videotone

Weltron

Wharfedale

Yamaha

Harrogate

Audio Show

"Audio 73", housed in over four floors of the Hotel Majestic, Harrogate, from August 31st to September 2nd offered an opportunity to examine some of those products unlikely to appear at the London show.

Among these, Ampex have devised a simple solution to the problem of residual tape head magnetisation, comprising demagnetising arrangements within a cassette cleaning tape. Available from Tape Music Distributors Ltd of St. Albans, this is loaded and played through in the normal way. Prices are £2.20 and £2.91 respectively for cassette and cartridge formats.

Ariston Audio introduced a low mass (310g) stereo headset, type HS100, of Japanese origin. This uses a moving coil diaphragm drive, open backed to minimize colouration, and with a sensitivity of 105dB per mW and 0.5W handling, produces high level sound from low power amplifiers, the matching impedance being 4 to 32ρ . Price is £21.

Richard Allan, one of the few remaining postwar firms, has added the "Academy" i.b. enclosure to their loudspeaker range. It employs 300mm, 125mm and 20mm diameter drive units to cover the audio band, each assembled from basic parts within the Richard Allan organisation to ensure uniformity and quality of production. Costing £75, the speaker occupies 4 cu.ft and weighs 60lb. R.N.B.

An Automatic Noise-Limiter

A simple muting circuit for use with f.m. tuners

by P. Hinch, B. Tech.

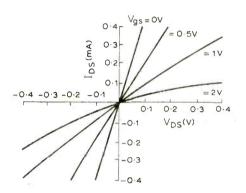
In recent years the automatic noise limiter has become an increasingly common addition to high quality f.m. receivers. Such a circuit greatly simplifies tuning of the receiver by selecting a minimum signal level below which the audio output is muted. Apart from the removal of interstation noise, a squelch circuit can also ensure that only the local transmitters of the national stations are received. With high sensitivity tuners (such as the Nelson-Jones design¹), it is not always immediately apparent when the "wrong" transmitter is being received, until the poorer signal-tonoise-ratio becomes evident. A further bonus is the removal of tuning ambiguities in the absence of a.f.c., caused by the shape of the discriminator response curve; a high level, distorted signal is received on either side of the true signal due to the i.f. falling on the wrong slope of the discriminator response.

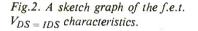
The usual method of achieving the a.n.l. function is to detect amplitude modulation of the i.f. after limiting. If noise is being received, the i.f. amplitude occasionally drops to zero due to noise cancellation. These gaps in the i.f. waveform can be detected, and used to operate the muting circuit. However, in a circuit designed to be an add-on unit for existing tuners, it was considered undesirable to make connections into the i.f. strip of the receiver. The circuit described requires no modifications to the tuner, except, in the case of monaural reception, removal of the de-emphasis capacitor.

The circuit relies on the fact that, while the signal bandwidth is restricted to a maximum of 53kHz (for stereo signals), the noise bandwith extends to over 100kHz. A third order high pass filter is used to reject the signal and yet allow noise to pass through. The resultant signal is amplified and detected, so producing a d.c. output related to the amount of noise being received. This is used to operate an f.e.t. switch, which mutes the output of the receiver. For mono reception, provision is made for adding a de-emphasis capacitor at the output.

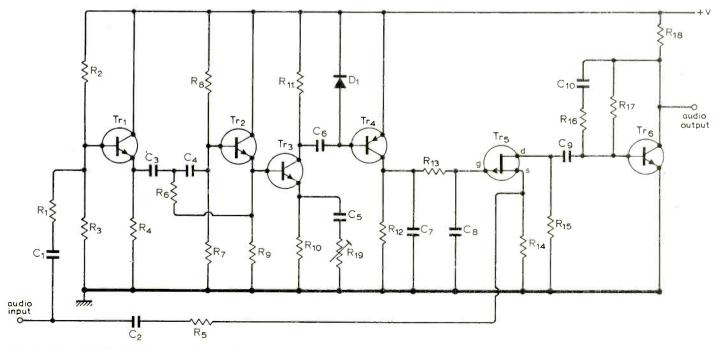
Circuit description

The first stage is an emitter follower designed to provide a high input impedance which is substantially constant with





frequency. This is important in order to avoid amplitude and phase distortion of the stereo multiplex waveform when fed from a receiver having an appreciable output impedance. The input capacitor to the emitter follower has a value of 68pF, giving a first order high-pass characteristic with a cut-off frequency of 100kHz. The variation in amplitude at the input when fed from a source impedance of $2.2k\Omega$



ericanradiohistory co

Fig. 1. Complete circuit of automatic noise limiter.

(as in the Nelson-Jones design) is then only 0.3dB from 1 to 53kHz.

The second stage is a Sallen-Key type second order high pass filter with a cut-off of 100kHz, presenting a low impedance drive to the voltage amplifier stage (Tr_3 in Fig. 1.). The detector Tr_4 switches when the amplifier output reaches about 1.4 volts peak-to-peak. The detector output passes through a low pass filter (R_{13} , C_8) which prevents accidental muting caused by brief noise spikes on an otherwise low noise signal (for example, those caused by badly suppressed car ignition systems). The muting action is performed by a p-channel junction f.e.t. used as a switch.

Design of the f.e.t. switch

If an f.e.t. is operated under conditions of low gate-source voltage and low drainsource voltage, it acts as a linear resistance, the value of which is controlled by the gatesource voltage (see Fig. 2). For the 2N3820 device used in this design, the minimum "on" resistance is typically around 400Ω . In order to avoid distortion it is clear that, in the "on" state, the drain-source signal voltage must be kept to a minimum, as also must the gate-source signal voltage. If either of these is allowed to rise, the drainsource resistance will vary over the cycle, and distortion will be generated. Thus an f.e.t. switch as shown in Fig. 3 was found to generate 0.5% distortion at 0.5V r.m.s. input. For higher input levels the distortion increased drastically. This was considered unacceptable for high quality reproduction.

The solution to this is to connect the f.e.t. (Tr_5) to the virtual earth point of a feedback amplifier, as shown in Fig. 1. At this point, signal levels are very low.

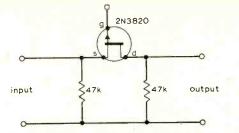


Fig.3. Elements of the f.e.t. switch used to control the receiver output.

In this curcuit, distortion was found to be 0.03% at 53kHz, and 0.5V r.m.s. input. The distortion was almost entirely second harmonic, and at low frequencies the level was reduced still further. The attenuation in the "off" state was found to be -60db relative to 0.5V r.m.s.

This design has the added advantage that de-emphasis can be added for mono reception, by connecting a 2.2nF capacitor across the base and collector of the transistor.

Constructional Details The layout is not particularly critical, but long leads should be avoided, especially to the base of Tr_1 . It is, of course, important to remember to remove the receiver de-emphasis capacitor if one was fitted for mono reception. In the case of the Nelson-Jones tuner the designer recommends replacing this component with 150pF.

Performance The circuit has been in use for some time in the author's Nelson-Jones tuner. It has proved to be highly immune to transient interference, and greatly simplifies tuning of the main national and local

Components lis	st 👘 👘
Resistors:	
R_1 1k Ω	$R_{10} 2.2 \mathrm{k} \Omega$
$R_2 47k\Omega$	R_{11} 4.7k Ω
R_{1}^{2} 47k Ω	R_{12} 47k Ω
\vec{R} , 2.2k Ω	R_{13} 220k Ω
\vec{R} , 22k Ω	$R_{14} 47 \mathrm{k}\Omega$
R_{h} 10k Ω	$R_{15} 47 \mathrm{k}\Omega$
R_{γ}° 15k Ω	$R_{10} 22k\Omega$
R_{\star} 39k Ω	R_{17} 560k Ω
$R_9 2.2 \mathrm{k} \Omega$	$R_{18}^{\prime} 2.2 \mathrm{k} \Omega$

All 5% carbon.

Potentiometer: R_{19} 1k Ω lin. preset

Capacitors:	
C_1 68pF silver mica	C, 10nF
$C_{2} 1 \mu F$	C_7 10nF
C_3 150pF silver mica	C ₈ 100nF
C_4 150pF silver mica	$C_9 1 \mu F$
C ₅ 100nF	C_{10} 470nF

All capacitors except C_1 , C_3 , C_4 , may be 20%. C_1 , C_3 , C_4 should be 5%.

 Transistors:

 Tr_1 to Tr_3 2N930

 Tr_4 BC214L

 Tr_5 2N3820

 Tr_6 2N930

Diode: D_1 1N914

stations. To enable reception of distant signals a switch has been included to short the gate of Tr_5 to ground and defeat the muting operation.

Reference

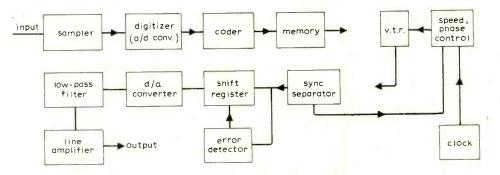
1. "F.M. Stereo Tuner" by L. Nelson-Jones, Wireless World, April-May 1971.

Sound Recorder uses P.C.M.

Or how to eliminate wow and flutter, crosstalk and modulation distortion

Pulse code modulation has been used by Nippon Columbia, the well-respected Japanese software and hardware company, for the first time for studio master tape recordings to eliminate the conventional tape recorder with its limitations. Though other techniques, in particular that of pre-distortion to reduce playback tracing error, may possibly give greater audible improvement, the use of the p.c.m. technique is outstanding in the number of problems it removes at one go.

The p.c.m. recorder, developed by Nippon Columbia in co-operation with NHK Research Laboratories, removes ghosting, wow and flutter, crosstalk and modulation distortion, at the same time



In this eight-channel p.c.m. system for making studio master recordings, fidelity already improved over conventional tape recorders as illustrated in the graphs — can be further improved by duplicating channels where only two or four are required using digital error-correcting procedures.

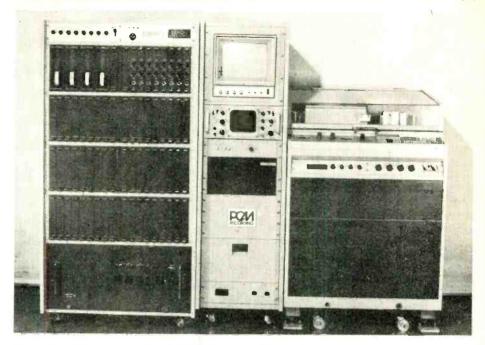
reducing harmonic distortion to 0.1%, providing a dynamic range of better than 75dB and an amplitude response extending from d.c. to 20kHz. The p.c.m. system has eight channels, is capable of half-speed reproduction (to increase cutting capacity), features an additional head to give an advance signal for variable-pitch recordings, and is equipped for automatic editing and splicing. Records made with this system are already available in Japan and additionally feature halfspeed cutting and anti-tracing-distortion cutting.

To pulse-code modulate the eight audio channels, signals are first sampled at a rate of 47.25kHz, three times the frequency of 525-line, 30-field/s horizontal sync pulses (recorded waveforms are similar to television signals enabling a video tape recorder to be used together with a monitor). The sampled signals are then quantized by an a. to d. converter, see block diagram. A linear binary coder uses 13 bits to specify the quantization levels, and together with a parity check bit for error detection and a check bit for phase shift detection, makes 120 bits per sample, for the eight channels. (Low radix coding is used in p.c.m. to improve noise immunity, the price being bandwidth - hence the video recorder.)

Synchronizing information is carried on the front and back porches of the horizontal sync signal, using a clock frequency of 7.1824MHz. The televisionlike system makes it quite different from the BBC p.c.m. transmission system, where a 14-bit code is used for each of 13 channels which, with 9-bit sync data and 5-bit data for transmitter switching, makes 196 bits per sample; sampling rate 32kHz.

On playback the signals are routed into their channels, error detected and checked for drop-outs. If a sample is missing the preceding and following signals are averaged, and when more than one sample is missing, the preceding signal is maintained. Errors can be further reduced by duplicating information. If only four channels are required, samples for channels 1 to 4 are staggered by one sample and fed to channels 5 to 8; re-ordering the signal means that larger drop-outs can be tolerated. The two samples of the same information are compared and only the correct one transmitted. If both samples are missing, the interpolation technique is used. Finally, the signals are passed through a d. to a. converter and filtered to remove the sampling frequency.

Half-speed reproduction is achieved by halving the clock frequency and low-pass filter cut-off frequency. The advantage of half-speed disc cutting was recognized some time ago (Nippon Columbia have a patent on this dating to 1956) and it's claimed that the permissible input to the cutter head can be increased by four times at h.f. This is used on Columbia* Mastersonic p.c.m. recordings



To achieve the necessary bandwidth for p.c.m. this recorder uses a conventional 525-line video tape recorder. Editing is made easier by the provision of a 30-Hz frame synchronizing signal on the control (audio) track.

(°/°)

0.5

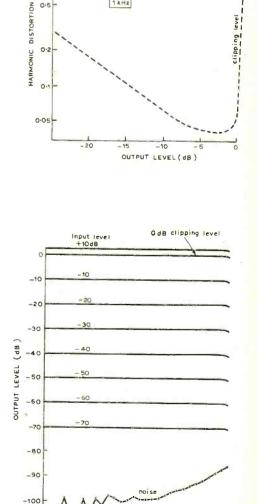
With the p.c.m. tape recorder harmonic distortion is reduced by an order of magnitude over conventional tape recorders

As well as featuring a flat amplitude response from d.c. to 20kHz, the p.c.m. technique shows excellent linearity of input-output level and a noise level that permits at least 75dB dynamic range.

as well as "non-distortion cutting". This last-mentioned technique uses a tracing simulator at the recording stage to offset the tracing distortion due to the finite size of the playback stylus, giving a reduction in distortion of an order of magnitude.

There are clearly other applications for this technique. As well as laboratory testing it will be of value for data recording where wide dynamic range, operation down to d.c., low distortion, and high stability are important e.g. in noise and vibration work, speech and music analysis and seismic studies.





1 kHz

-110 50 20 100 200 500 1k 10k 20 2 k 5k FREQUENCY (Hz)

^{*} Sold as Denon recordings outside Japan.

550

On October 15, Oscar 6 completed its first year in space. It was designed for a lifetime of about one year and there are now increasing signs of battery deterioration; as a result the 144 MHz to 28 MHz repeater is now available only on the south/north evening orbits on Mondays, Thursdays and Saturdays. It is hoped that a replacement satellite, Oscar 7, will be launched this year, possibly in the October / November period. This will carry two beacon transmitters (including one on 2304 MHz) and two repeaters: one (built in West Germany) is designed to accept signals on 432 MHz and re-transmit them on 145.9 MHz; the other will be similar to that on Oscar 6, accepting signals in the 144 MHz band and re-transmitting them in the 28MHz band. The satellite will also carry an Australian designed command system.

Barry Turner, G8CEX, is believed to be the first holder of a British Class B licence to qualify for the A.R.R.L.'s Oscar "1000" award.

Fifty years of "short waves"

Possibly the most significant date in the history of the opening of the "short waves" was November 28, 1923 when the first amateur two-way transatlantic contacts were made by Leon Deloy, 8AB, of Nice, France, and Fred Schnell, 1MO and John Reinartz, 1XAM in the United States on about 100 to 110 metres. During the summer of 1923 Deloy had visited the States where attention was turning to the use of shorter wavelengths and he arranged to go below the customary 200 metres during the 1923 transatlantic tests. On his return to Europe he carried out many tests on short waves with the British amateur E. J. Simmonds, 20D, of Gerrards Cross, and then in November cabled A.R.R.L. asking them to listen for him between 100 and 110 metres. He was heard on November 27 and excellent contact established the following night, so initiating the rush by both amateurs and commercials to the short waves. First British amateur to make two-way contact with the United States was Jack Partridge, 2KF of Merton on December 8.

One of the still-active British amateurs who took part in the early days of international h.f. operation — and is also credited with being the first British amateur to issue a QSL card — is W. E. Corsham, G2UV of Wembley, Middlesex. He has accepted an invitation to become a Vice-President of the R.S.G.B.

Technical trends

What, one is often asked, are the current trends in amateur radio equipment practice? This is by no means an easy question to answer. With so many different individuals one finds that at any given time many different approaches are being tried — while there are also very many amateurs who use the same basic equipment for many years. But it is suggested that the following are technical trends that have been attracting attention in the past year or so. A rapid growth in the amount of channelized n.b.f.m. operation on 144 MHz spurred on by the appearance on the market of many compact f.m. transceivers. Much more interest in the advantages to be obtained from effective speech processing both on s.s.b. and (for v.h.f.) a.m. coupled with greater appreciation of the reasons for carrying out s.s.b. speech clipping at r.f. rather than a.f. Increasing interest in frequency synthesis and various forms of crystal-stabilized v.f.o. (unfortunately some of the simplified forms of frequency synthesis that have been used in amateur equipment seem likely to lead to more problems than they solve, but improved systems are beginning to appear.) Much greater recognition of the importance of receivers having highly linear front-ends in order to provide good dynamic selectivity - involving the use of double-balanced diode and f.e.t. mixers. the use of power f.e.ts. in r.f. amplifiers, reduced sideband noise in oscillators and the like (this trend is equally reflected in professional communications receivers such as the Racal 1772 series). The gradual transfer of the bulk of mobile operation from 1.8 MHz to 144 MHz. The continuing trend towards beam aerials for long-distance s.s.b. operation on h.f., whereas dipole-type wire aerials remain popular for c.w. operation; for beam aerials the Quad and associated Delta-loop aerials appear to be making increasing impact although the Yagi remains by far the most popular arrangement for rotary beams. And, in common with most of electronics, a trend towards greater use of integrated circuits and a wide range of semiconductor devices.

On the bands

The R.S.G.B. has appealed to its members to adhere to the I.A.R.U. Region 1 voluntary h.f. band-plan affecting the 3.5 to 28 MHz bands, stating: "The band plan is reviewed at three-yearly intervals and is considered by the national societies to be practical and worth while. However, this view is obviously not shared by a small minority . . . one solution is to make the sub-division of each band apart of the licence regulations". It points out that if necessary the Society's MPT Liaison Committee will not hesitate to make such recommendations to the Ministry. The current problem is the increasing "intrusion" of phone stations into segments of the band voluntarily reserved for c.w. and r.t.t.y. operation.

According to the Cheltenham group newsletter, G. V. Farrance, G3KPT has worked 39 countries (including the United States, Canada and the Panama Canal Zone) on 7, 14 and 21 MHz bands using one of the low-power (2 watts) Heath HW-7 transceivers which include a direct-conversion receiver and all-transistor transmitter, using a simple inverted-L aerial 66 ft long and between 26 ft and 6 ft high.

Contacts by means of reflections from meteor trails continue to be made by British amateurs on 144 MHz with stations in Italy, Hungary, Sweden and so on, particularly during the periods of the major meteor showers.

In brief

An R.S.G.B. lecture on aerials is being given by Les Moxon, G6XN, at the I.E.E., Savoy Place, London WC2 on Thursday, November 8 . . . The amateur club station, G3SSO, of Government Communications Headquarters, Cheltenham, has won the R.S.G.B. h.f. contests championship for1972-73, based on the results of six different h.f. contests. F. Cooper, G2QT, of Ashford, Kent was runner-up . . . The annual R.S.G.B. 7 MHz contests will be held on October 20-21 (c.w.) and November 3-4 (phone) . . . The death has occurred of Harold Jones, G5ZT of Plymouth, a founder member of the Plymouth Radio Club and one of the pioneers in this country of longdistance slow-scan television (some of his results were described and illustrated in World of Amateur Radio, September 1971) . . . The phone section of the "CO world-wide contest" is on October 27 to 28 with the c.w. section on November 24 to 25.

PAT HAWKER, G3VA

Tuners and Tuner-Amplifiers

A résumé of the techniques used in modern designs and the standards upon which specifications are based

by Basil Lane

The purchase of a tuner or tuner-amplifier is often determined by the following factors; price, in terms of value for money; aesthetic appeal — since the new acquisition must integrate with the room décor and finally performance. The relative importance of each of these depends on the individual and the first two are purely matters of pocket and taste. The final factor should be a simple case of fixing a required specification and then comparing this with the appropriate product data. However, the solution is not so easily reached — as is described in the following article.

To attempt to review the progress in the design of tuners and tuner amplifiers over the past year is rather like taking a current model of the Morris Minor and reviewing it as something new. In general, the circuitry of receivers and tuners is fixed by an outline block schematic which has not changed for many years; the only differences can be seen in component detail, with an increasing usage of integrated circuits particularly in the i.f. stages — f.e.ts in the r.f. amplifier stage and ceramic filters. Even the trend towards using varicap diodes for the tuned r.f. amplifiers seems to have halted and perhaps even reversed.

Of course, quadraphony has been the biggest talking point of this last twelve months, but in as much as it raises the price of many receivers by quite a considerable amount, it has had very little effect upon the popular market place. To complicate the matter still further, there are several systems extant and every possibility of quite a prolonged battle before any one emerges as the victor. In almost all cases, the manufacturers that have opted to include quadraphonic decoders in their receivers have chosen to provide for all the major systems. Just to refresh the memory, these are the SQ matrix system of CBS, the QS matrix system of Sansui, the CD4 of RCA Victor and finally, as if that is not enough, some have opted to provide four channel synthesis from

conventional stereophonic recordings and broadcasts.

Although the matrix systems lend themselves to the conventional mass production of discs and replay systems, few proponents entirely own an equipment manufacturer, as do the Victor Company of Japan. The interests of RCA Victor are certainly reflected in the range of JVC Nivico receivers which are almost all fitted with CD4 system decoders. Such a situation will not prevail for very long as it is expected that at least the CBS licencees will show a considerable number of new products at the Audio Fair this year. Not mentioned so far and not included in the table, is the equipment end of Sansui who have not, as yet, provided details of products available but which are believed to have a number of quadraphonic receivers. Apart from the developing market for quadraphony, reflected in the increasing range available, novelty of circuit and user facilities are conspicuous by their absence. There are, however some "fine detail" improvements which can be commented upon; for example, the new Ferrograph tuner SFM1 which has a facility for varying the muting threshold to suit signal strength for the particular conditions prevailing. In addition it includes the very unusual feature of a continuously variable separation control from full stereo to mono, permitting an optimal setting for



Fig. 1. The Nikko STA Receiver showing the additional tuning indicator on left.

minimum subjective noise.

Several tuners and receivers have been improved by the addition of a tuning meter in addition to the normal "centre of channel" meter used for f.m. stations. The tuning meter makes rather more sense since it measures actual signal strength available and so can be used to assist the correct alignment of aerial arrays. Phase-lock-loop decoders are also becoming more popular, with Armstrong, Pioneer and Fisher all having models incorporating this type of circuit.

Cambridge Audio have just produced a new tuner, the T55, which not only uses phase-lock-loop stereo decoding but also modern design techniques in all other stages. The r.f. and mixer stages utilize m.o.s. transistors, and varactor diode tuning. Although any tuner which has varactor tuning can be remote controlled, few actually have the external connection point. The Cambridge tuner has such a facility plus connections for remote signal strength indication and a.f.c. switching.

With a.m. broadcasting such a well established fact and receiver design virtually static in this area, it comes as a surprise to see some sort of innovation from Philips in the RH720 receiver. Adopted from communications receivers, there is a control which permits the bandwidth to be varied to reduce interference or improve the frequency response of the tuner. Touch controls are also featured on this tuner, offering instant selection of up to six preset stations.

Two products which look obviously different are the Harmon Kardon Citation 15 and the Sherwood SEL 300. The first of these is perhaps one of the most innovative of modern tuners since not only is the tuning dial a drum type, more often to be found in laboratory instrumentation, but also a quieting and a tuning meter are incorporated. The really new item is the introduction of a Dolby 'B' noise reduction unit. For some time Dr. Dolby has advocated the use of the 'B' system as a way of increasing the area over which satisfactory stereo reception can be obtained. As yet there have been no professional broadcasts made here in the U.K. using this principle although an experiment has been made in the amateur band by G30SS, Angus McKenzie. He reported quite good results although insufficient data was obtained to determine the exact degree of improvement. However several American broadcast stations are making use of Dolby

'B' encoding and the Citation 15 was obviously designed to exploit this to the full. This tuner is also unusual in that the design of the i.f. strip appears to be a retrograde step away from integrated circuits and ceramic or crystal filters to a complex 9 pole phase linear LC network. Although this is obviously more difficult to set up at the manufacturing stage, Harmon Kardon claim that the performance justifies the technique adopted.

The Sherwood SEL 300 would appear to be unique in displaying the tuned frequency in the form of a digital display. Seven segment incandescent lamps are used, driven from a logic circuit consisting of seventeen i.c. packages, and a crystal controlled clock oscillator. The i.f. filter is even more complex than that of the Citation 15, being a 12 pole "Le Gendre" toroidal filter which is claimed to offer an even sharper cut off than the crystal types.

Two Trio products appear to have surprising features, the KR-5200 in particular, though it may be something which appears as a result of the terrible translation presumably from the Japanese original. The data sheet suggests that the f.m. i.f. strip uses a combination of mechanical filters (!) and other forms of filter, presumably LC types, to give a really sharply defined passband. Although the mechanical filter has been a feature of communications receivers for many years, it is very surprising to find them in a domestic receiver. There has been, unfortunately, no opportunity to check this against the circuit diagram and so the accuracy of the statement is open to question.

An additional circuit feature mentioned in the brochure for the KR-5200 is the double switching stereo demodulator which uses antiphase cancellation of crosstalk to improve the stereo separation. This has echoes of the Delta 75 receiver system used by Leak, where crosscoupling can be switched in by selecting one or both "quasi-stereo" buttons on the front panel to reduce background noise on weak stereo signals.

The second of the two Trio products mentioned is the KT-8005, a tuner which, if the data sheet is anything to go by has perhaps the most outstanding performance of any of those listed in the table. With a usable sensitivity of 1.5μ V, an f.m. stereo distortion of 0.3% and a capture ratio of 1.0dB, the KT-8005 must be quite a remarkable design.

Product data

The data sheet associated with any particular tuner or receiver is obviously designed to attract the potential purchase, and with the Trade Description Act hanging over the writers' heads, they cannot afford to make any claim which cannot be substantiated. However, in compiling the table for this survey it has become evident that the quantity and quality of the technical data referring to performance is extremely variable.

On the one hand there is ITT with the new TA-1-200 which has as data the barest information on power output and none on

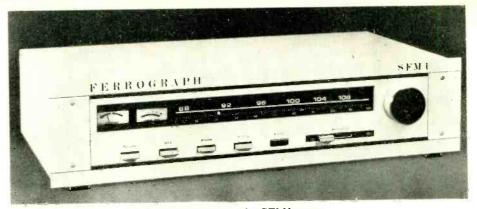


Fig. 2. The latest product from Ferrograph, the SFM1 tuner.

the performance of the tuner section at all and on the other hand, Sherwood or Trio and many others that give a profusion of detail.

For buyers, it is the comparison of performance, giving in turn some idea of value for money, which would be of considerable use in making a decision on what to buy. Even worse, when plenty of information is given, the measurement methods used by different manufacturers often invalidates comparison. The Editor, in the lead editorial for last month, brought out one aspect of this when he commented that the only national standard which assists by defining a minimum quality for hi-fi, was that produced by DIN. Two interesting points arise from this, first that although many manufacturers say that their product exceeds the DIN 45 500 specification, almost all of them quote measurements made to the old and rather dated American IHF standard. (IHF stands for Institute of High Fidelity.)

In some instances no indication is given of the measurement method and just bare figures are quoted. These must be, for many, useless and often confusing figures making comparison impossible. Criticism of the British Standards Institute for not taking some lead on this topic, evoked the response we see in the Letters column this month. The fact that the BS committee TLE/26 has been working on this standard since 1968 and still has not come up with a final proposal, is an indication that it could still

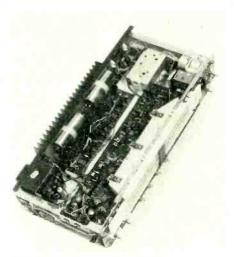


Fig. 3) An internal view of the Goodmans One-Ten.

be some time before something appears and even then it may look nothing like the proposal or, if it is not publicised, that is no guarantee that it will be used. He remarks that the press is a significant factor in the acceptance of such standards, a point which cannot be denied, but even more important is its acceptance by industry, and as we have seen this is not just a matter for the press to solve.

The BS proposals for minimum quality are, it must be emphasised, still at an early stage, but in brief the details are as follows: The measurement techniques to be used are those specified in BS 4054:1966, which it is to be noted does not acknowledge the existence of stereophonic systems! The frequency response measured at 30% utilisation (the stereo term for deviation) to 1 kHz modulation should be $\pm 3 \text{ dB}$ between 40Hz and 12.5kHz and ±2dB from 250Hz to 6.3kHz. The disparity between channels between 250Hz and 6.3kHz is limited to 2dB. Details of the minimum requirements for sensitivity, distortion and so on are contained within Part 2 of these proposals which, unfortunately, were not available at the time of going to press. It is known however, that there is some similarity in these proposals with those of the DIN 45 500 but the notable exception is in the test signals used. Modulation for the DIN sensitivity test is 15kHz and the sensitivity is expressed at the 26dB quieting point. The remainder of the test procedures relating to the tuner section of a receiver and tuners are similar. The more popular IHF standard differs in many ways from both the DIN and the proposed BS standard. Again, the test signal varies, being a carrier modulated to 100% by a 400Hz tone and in addition, the usable sensitivity is considered to be the point which separates total distortion (including hum and noise), from the audio output of the tuner produced by the test signal, by 30dB.

Despite the existence of the DIN and the IHF standards, some manufacturers still persist in quoting sensitivity to other levels of quieting and to other deviations. Examples of these are to be found in the table at the end of this article.

Many of these problems of comparison would be alleviated if manufacturers used a standard graphical presentation which would enable purchasers to make a total assessment of the sensitivity, noise and

harmonic distortion capability of the tuner.

Sadly, the most important aspect of good f.m. reception is often overlooked at the design stage. This relates to the ability of the r.f. amplifier to avoid overload from high level adjacent channel signals when tuning to a comparatively weak signal. This is becoming increasingly important with the number of new f.m. local radio stations coming on the air. Evidence of the poor discrimination of the r.f. amplifier is exemplified by the presence of "birdies" when switched, particularly, to stereo broadcasts. To a certain extent this can be overcome with the use of a well placed, well designed aerial and again designers are encouraging this situation because a few quite highly priced tuners have no external aerial connectors and even more, have facilities for matching into only one impedance of feeder.

Quite recent issues of the magazines Electrical and Electronic Trader and Electrical and Radio Trading have contained details of some correspondence between the BBC and the aerial manufacturers' trade association on the subject of home-made aerials. The BBC have reprinted construction details for aerials in Information Sheet 1104, available from BBC Engineering Information, and for some reason the manufacturers took exception to this and complained vociferously. What is relevant is that the BS4054:1966 contains such information already and since manufacturers are among those represented on the committees of the BS, presumably they were party to agreeing the publication of such details. However, the fact remains that an external aerial, professional or home-made, can do much to improve the quality of reception in the face of considerably disparate signal strengths for adjacent channel stations. Useful publications from the BBC on f.m. stereo reception will be described elsewhere in a later issue of Wireless World.

Finally a point on reviews on f.m./a.m. tuners and receivers. Most of the hi-fi journals available in the U.K. publish reviews from time to time which describe the performance of a typical sample supplied by the manufacturer or distributor.



Fig. 4. A Receiver from ITT, the TA-1-200.

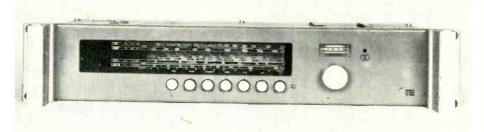


Fig. 5. A professional a.m./f.m. tuner made by Millbank.

In many instances, details of the test techniques are not published and so it still remains a difficult problem to crossrelate and compare results from magazine to magazine. In at least one of the divisions of audio, a BS proposal has been published which does lay out a standard format and test technique for the presentation of certain performance information. Perhaps it is about time that the whole field of consumer equipment is studied and some agreement obtained on presentation of data. This could well be initiated by a measure of cooperation between journals or even an acknowledgement by British Standard committees that journals have a vital place in the chain between consumer and

designer and go on to consider including standard data presentation formats suitable for use by reviewers.

With many new products appearing at the Audio Fair this year, the possibility of announced price changes and the need to incorporate information on products not described in this table, there will be a follow-up, including manufacturers' names and addresses, in the December issue.

Maker and Model	Stereo (S) or Quad (Q)	FM/AM	Tuner (T) Tuner/Amp Receiver (R)	Aerial Z(Ω)	Tuner o/p into load (Ω)	Power Output (''r.m.s.'')	F.M. Distn(%)	Sensitivity (IHF or DIN)	Price (*+ VAT)
ACOUSTIC RESEARCH AR Tuner-amp AR Tuner	S S	FM FM	R T			50W/ <mark>8</mark> Ω —	0.4 0.4	2.0μV IHF 2.0μV IHF	240.00 110.00
ADASTRA A1005 (Chassis) A1018 A1007 (Chassis)	As above b	FM ut in woode AM	T en cabinet T	75 75				10 <mark>µV for</mark> 10dB ──	
<i>AKAI</i> AT550 AT580 AA8030 AA8080	S S S S	FM/AM FM/AM FM/AM FM/AM	T T R R			25W/8Ω 40W/8Ω	<0.8 <0.8 0.8 0.6	1.8µV ІНҒ 1.6µV ІНҒ 2.5µV ІНҒ 2.0µV ІНҒ	91.62 143.30 140.48 178.07
<i>ALBA</i> UA100D UA800	S S	FM/AM FM/AM	R. T	75 75		15W/8Ω —	<1.0	2.0μV for 20dB S/N 2μV IHF	43.67 37.84

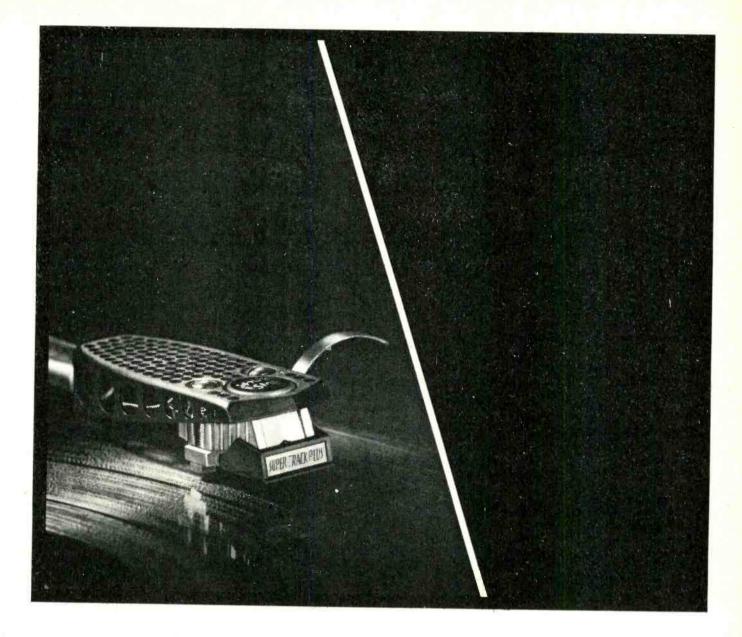
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Maker and Model	Stereo (S) or Quad (Q)	FM/AM	Tuner (T) Tuner/Amp Receiver (R)		Tuner o/p into load (Ω)	Power Output (''r.m.s.'')	F.M. Distn(%)	Sensitivity (IHF or DIN)	Price (*+ VAT)
ALPHA FR4000 FR3000 FR2000 R150 FT150 Executive 007	S S S S S S S S S S S S S S S S S S S	FM/AM FM/AM FM/AM FM/AM FM/AM	R R R T T	300 300 300 300 300 300/75	1V/? 500mV/10k 50mV/10k	20W/8Ω 15W/8Ω 10W/8Ω 15W*/8Ω	 <0.4	2μV IHF 3μV IHF 2μV IHF 3μV IHF 2.5μV IHF 1.8μV IHF	95.50° 86.60° 68.00° 59.00° 45.00° 49.50°
ARMSTRONG 623 624 625 626	s s s s s	FM/AM FM FM FM/AM	T T R R	300/75 300/75 300/75 300/75	-		<0.2 <0.2 <0.2 <0.2	1.5µV ІНҒ 1.5µV ІНҒ 1.5µV ІНҒ 1.5µV ІНҒ	79.20 59.40 110.00 132.00
ASTRONIC B2477 (Single Station) B2478 (Single Station) B2479 (4 Station tuner) B2480 (5 Station tuner)	As for B24 As for B24	AM FM 78 tuner 78 but with	T T one am static	75 201	500mV/5k		_	 10µV IHF	39.05* 39.05* 41.58* 60.06*
AUDIO DECKS CT17 CR50			T R						121.74 167.67
BANG & OLUFSEN Beomaster 901 Beomaster 1001 Beomaster 3000–2 Beomaster 4000 Beomaster 1700	S S+Synth S S+Synth S	FM	R R R R T	240/75 300/75 75 — 75	 1V/?	20W/4Ω 15W/4Ω 30W/8Ω 55W/8Ω —	<0.9 <0.4 <0.5	1.8µV DIN <3.5µV IHF 2.0µV IHF <1.4µV DIN 2.0µV IHF	100.90 96.90 164.50 193.50 60.90
<i>BUSH ARENA</i> TA2700 TA2800 TA3500	S S S	FM FM/AM FM	R R R	75 75 75		15W/3.2Ω 15W/3.2Ω 10W/4Ω		1.5µV DIN 1.5µV DIN 3.0µV DIN	85.67 89.43 74.37
DUAL CR50 CT17	S S	FM/AM FM/AM	R T	240 240	-	18W/4Ω —	 <1.0	1.5µV DIN 8µV DIN	167.67 121.74
FISHER 170 180 201 203 205 304 404	S S S S S + Q S + Q	FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM	R R R R R R R R			16W/4Ω 21W/4Ω 20W/8Ω 25W/4Ω 35W/4Ω 15W/8Ω 22W/8Ω	0.8 0.8 0.8 0.8 0.8 0.8 0.3 0.3	2.5μV IHF 2.5μV IHF 3.0μV IHF 2.5μV IHF 2.5μV IHF 1.8μV IHF 1.8μV IHF	127.60 169.40 132.44 216.70 235.40 286.00 363.00
<i>GOODMANS</i> One-ten Module 80 Module 90	S S S	FM/AM FM FM/AM	R	240/75 300 240/75	_	40W/8Ω 70W/4Ω 30W/8Ω	0.2	1μV IHF 1.5μV DIN 1.0μV IHF	130.85 87.54 112.03
<i>GRUNDIG</i> RTV800 RTV900	S S	FM/AM FM/AM		240/65 2 <mark>4</mark> 0	-	12.5W/4Ω 25W/4Ω	0.7 0.7	1.1μV DIN 1.8μV DIN	150.40 195.75
HARMON KARDON Citation 15 (Dolby) 50+ 75+ 100+ 150+ 330A 630 930	S S+00 S++00 S S	FM FM/AM FM/AV FM/AN FM/AN FM/AN	I R I R I R I R	300/75 300 300 300 300 300/75 300/75			0.35 0.9 0.7 0.7 0.7 0.6	2.0μV IHF 2.8μV IHF 2.0μV IHF 1.9μV IHF 1.8μV IHF 1.8μV IHF 1.8μV IHF	279.00 159.00 259.00 355.00 123.00 150.00 199.00
177 TA-1-200	S	FM/AN	A R	2	2	8W/4.5Ω	!		79.50
JVC/NIVICO VR5505 VR5515(L) VR5525	S S+Q S+Q	FM/AN FM/AN FM/AN	<mark>л R</mark>	300 300		25W/8Ω 15W/8Ω 18W/8Ω	0.5 0.8 0.5	2.2µV IHF 2.2µV IHF 2.2µV IHF	95.50 135.00 169.50

Maker and Model	Stereo (S or Quad (Q		Tuner (T Tuner/Am Receiver (I	p Z(Ω)			t Distn(%)	Sensitivity (IHF or DIN)	Price (*+ VAT)
VR5535 4VR1006 4MM1000 4VR5414 4VR5436 4VR5445 4VR5446	S+Q S+Q S+Q S+Q S+Q S+Q S+Q S+Q	FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM	R R R R R R R R	300 300 300 300 300 300 300/75		28W/8Ω 40W/8Ω 40W/8Ω 15W/8Ω 17W/8Ω 21W/8Ω 22W/8Ω	0.8 0.4 1.0 0.8 1.0 0.8	2.0µV IHF 2.2µV IHF 2.2µV IHF 2.0µV IHF 2.0µV IHF 2.0µV IHF 2.0µV IHF	195.00* 208.50* 146.50* 208.50* 235.00* 280.00* 280.00*
<i>KLINGER</i> KC91 KC96	S S	FM FM	T R	300/75 300/75	2.0V/10k	 25W/8Ω	_	8.0µV DIN 8.0µV DIN	41.40* 82.20*
<i>KORT/NG</i> T510 T710 310T 410T 800L Syntector 1600L	S S S S S+Synth (FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM	T T R R R R	240 240 240 240 240 240 240					47.63 80.05 66.19 81.51 140.62 191.21
<i>LEAK</i> Delta FM Delta FM/AM Delta 75	S S S	FM FM/AM FM	T T R			 35W/8Ω	< 0.5 < 0.5 < 0.5	2.5μV IHF 2.5μV IHF 2.5μV IHF	74.43 83.79 1 <mark>63.8</mark> 3
<i>LUX</i> R800 FQ990 717 700 500	S S S S S S	FM/AM FM/AM FM/AM FM/AM FM/AM	R R T T T	300/75 300/75 300/75 300/75		40W/8Ω 70W/8Ω 	0.4 0.5 0.6 0.5	1.8μV ΙΗF 2.0μV ΙΗF 2.2μV ΙΗF 2.2μV ΙΗF 1.7μV ΙΗF	205.00° 250.00° 74.00° 100.00° 160.00°
MARANTZ 2010 2220 2230 2245 2270 105 115 120 4415	S S S S S S S S S S S S S S S S S S S	FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM	R R R R T T T R	300/75 300/75 300/75 300/75 300/75 300/75 300/75 300/75 300/75		10W/8Ω 20W/8Ω 30W/8Ω 45W/8Ω 70W/8Ω 	<1.0 <0.9 <0.5 <0.3 <1.0 <0.3 <0.25 <1.0	2.8µV IHF 2.1µV IHF 2.0µV IHF 1.7µV IHF 1.4µV IHF 2.8µV IHF 1.7µV IHF 2.8µV IHF 2.8µV IHF	129.00* 169.50* 215.00* 270.00* 330.00* 95.00* 260.00* 260.00* 245.00*
<i>MILLBANK</i> Met 100k Met 500 fixed station	S	FM/AM FM	T T	300 75	100mV/? 250mV/?	=	0.2	3µV HF	71.89 50.60
<i>NIKKO</i> STA5010 STA7070 STA8080	S S S	FM/AM FM/AM FM/AM	R R R	300/75 300/75 300/75	к ———	22W/8Ω 34W/8Ω 45W/8Ω	0.5 0.5 0.5	2.5μV IHF 2.0μV IHF 2.0μV IHF	115.50 143.00 158.40
<i>ONKYO</i> 234 225	S S	FM/AM FM/AM	R R	300 300		12W/8Ω 22W/8Ω	< 0.8 < 0.8	2.5μV IHF 2.5μV IHF	120.00* 160.03*
<i>PHILIPS</i> RH621 RH690 RH720 RH702 RH702 RH901	S S S S S S	FM/AM FM/AM FM/AM FM/AM FM/AM	T T R R R	300/75 300/75 300 300 300	600mV/10k 250mV/10k 		<1.0 <4.0 <1.0 <1.5	1.0μV DIN 7.0μV (300Ω) DIN 2.0μV (300Ω) DIN 1.6μV (300Ω) DIN 1.3μV (300Ω) DIN	110.00 47.50 215.00 90.38 87.00
PIONEER QX9900 QX8000A QX4000 SX2500 SX9000 SX828 SX727 SX626 SX525 SX424 _X440A TX6200 TX7100 TX7100 TX8100 TX8100 TX9100 TX500A		FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM FM/AM	T T T	300/75 300/75 300/75		30W/8Ω 22W/8Ω 10W/8Ω 58W/8Ω 	0.5 0.8 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	1.8µV IHF 2.2µV IHF 2.2µV IHF 1.6µV IHF 1.6µV IHF 1.2µV IHF 1.3µV IHF 1.5µV IHF 1.5µV IHF 1.9µV IHF 1.9µV IHF 1.9µV IHF 1.5µV IHF 2.5µV IHF	430.24* 308.39* 216.82* 337.47* 303.26* 221.44* 285.22* 222.39* 184.74* 134.87* 106.09* 127.00 87.17* 117.20* 137.64* 185.99* 76.03*

555

Maker and Model	Stereo (S) or Quad (Q)	FM/AM	Tuner (T) Tuner/Amp Receiver (R)		Tuner o/p into load (Ω)	Power Output (''r.m.s.''	F.M. Distn(%))	Sensitivity (IHF or DIN)	Price (*+ VAT)
ROGERS Ravensbourne Series II Series II tuner-amplifier Series III tuner	S S S	FM FM FM	T R T	75 75 75	200mV/? 200mV/?	20W/8Ω	Mono <0.5 Mono <0.5 Mono <0.5	2.0μV DIN 2.0μV DIN 5.0μV DIN	61.50* 93.00* 50.00*
SABA TS80 8080 8035 Freiburg (remote control)	S S S S	FM/AM FM/AM FM/AM FM/AM	T R R R	240 240 240 240	-	30W/8Ω 12W/8Ω 40W/8Ω		1.5mV for 63dB S/N 1.5mV for 63dB S/N 1.8mV for 62dB S/N 1.1mV for 65dB S/N	
SANYO DCX 2500k DCX 2300k FMT 1400k DC 3300KA DC 3000KA	S S S+Q S+Q	FM/AM FM/AM FM/AM FM/AM FM/AM	R R T R R		_	10W/Ω 15W/8Ω —			82.79 99.75 63.01
SCAN-DYNA 2400 2000 3000 4000			R R R R						
SHERWOOD S7050 S7100A S7200 S2400 SEL 300 Digital tuner S8900A S7900A	s s + Q s s s s s	FM/AM FM/AM FM/AM FM FM FM/AM	R R T T R R	300 300 300/75 300/75 300/75 300/75	1111	22W/8Ω 40W/8Ω — 65W/8Ω 65W/8Ω	0.5 0.25 0.25 0.15 0.15 0.15	1.9μV ΙΗF 1.8μV ΙΗF 1.8μV ΙΗF 1.5μV ΙΗF 1.5μV ΙΗF 1.7μV ΙΗF	99.00* 132.00* 179.00* 122.00* 262.00*
<i>SONAB</i> R7000 R4000-2	S S	FM FM	R R	1	-	40W/8Ω 40W/8Ω	<0.5 <0.3	1.4µV DIN 2.0µV DIN	
STEEPLETONE S305 S500 STU1	S S S	FM/AM FM/AM FM/AM	R R T	75 300/75 300/75		4W/8Ω 25W/8Ω —	Ξ	 8.0μV DIN	43.30 89.99 44.66
SUGDEN R21 R51	S S	FM FM	Ŧ			-			66.00 71.50
<i>TEAC</i> AT100 AG6500 AG6000 AG7000	S S	FM FM/AM	T R	300 300/75	1V/30k —	50W/8Ω	<0.5 <0.7	2.0 _µ V 1НF 1.8 _µ V 1НF	116.60 242.00 220.00 242.00
TELETON GT202 TF50 TFS50LA TFS55	S S S S	FM/AM FM/AM FM/AM FM/AM	R R	300 300 300 300 300				1.5µV IHF 2.5µV IHF 2.5µV IHF 2.5µV IHF 2.5µV IHF	84.00 93.37 107.35 97.16
<i>TRIO</i> KR2120 KT8005 KR5200 KT1000A KR6170 KR2200 KT7001 KR3200 KT2001	<i>S</i> S S S S S S S S S S S S S S S S S S	FM/AM FM/AM FM/AM FM/AM FM/AM FM/AN FM/AN FM/AN	T R T R R T R	300/75 300/75 300/75 300/75 300/75 300/75 300/75 300/75	5 1.5V/1k 5 1.0V/2k 5 1.5V/1k 5 1.5V/1k	12W/8Ω 30W/8Ω 40W/8Ω 8W/8Ω 17W/8Ω	0.3 0.7 0.9 0.8 1.0 <0.5	2.3µV IHF 1.5µV IHF 1.8µV IHF 3.0µV IHF 1.9µV IHF 2.0µV IHF 1.5µV IHF 2.3µV IHF 2.0µV IHF	82.50 145.00 142.00 50.00 225.00 72.50
WHARFEDALE / Denton Linton Triton	S S S	FM/AN FM/AN FM/AN	1 R	300/7 300/7 300/7	5/	9W/80 17W/80 25W/80	2 <1.0	4.ΟμV IHF 2.5μV IHF 4.ΟμV IHF	95.00 107.66 160.00
<i>YAMAHA</i> CR700 CR500 CT700 CR510LS	S S S S	FM/AN FM/AN FM/AN FM/AN	1 R 1 T	300/7 300/7 300/7 300/7	5 — 5 —	40W/80 22W/80 22W/80	2 0.5 0.4	1.7µV ІНҒ 2.0µV ІНҒ 1.7µV ІНҒ 2.0µV ІНҒ	208.76 153.80 153.78 175.76



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Several years ago, we decided that our next challenge would be to go beyond the best there was. Our computers told us we had taken the existing cartridge structure and stylus assembly of the V-15 Type II Improved as far as we could, and that hereafter, any improvement in one performance parameter would be at the expense of performance in some other parameter.

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Circards — 11 Basic Logic Gates

When one and one isn't two

by J. Carruthers, J. H. Evans, J. Kinsler & P. Williams*

Logical or arithmetic processes are extensively used in systems such as industrial control, computers, electronic instrumentation and automatic telephone exchanges. These processes often involve complex functions of several variables, the desired functions being realized by switching operations in a logical manner. Although much of the design of these systems now deals with the interconnection of complex functional blocks, successful results also depend on a knowledge of the basic elements that constitute the complex functional blocks.

The basic elements of such systems are logic gates, which may perform combinational operations on their inputs. These inputs will normally be in one of two allowed states that could be, for example, two different voltages, two different currents or two different resistance values such as the limiting cases of open circuit and short circuit. Whatever form the allowed states take, a logic gate is concerned with whether certain statements about its inputs, at a given instant, are true or false. If these statements are made using normal language they become unmanageable as the number of quantities involved increases, making some form of symbolic statement highly desirable.

If a certain statement is true it is assigned the value 1 and if it is false it is given the value 0. For example, if one of the inputs to a logic gate is called A and it can be either at 5 V or 0 V then the statement "input A is at 5 V" may be true or false. If it is true than A = 1 and if it is false then A = 0. If this gate has three inputs and its output, D, is only at 5 V (D = 1) when two of its inputs, A and B, are at 5 V and its other input, C, is at 0 V, then D = 1when A = 1 AND B = 1 AND C = 0. Now C = 0 implies that C is NOT 1 i.e. $\dot{C} = 1$, where the bar indicates NOT or negation, so the above statement could be simply written as D = A AND BAND C. Using the multiplication sign of normal algebra (\times or .) to represent the AND operation this statement becomes $D = A \times B \times \tilde{C}$, or $D = A.B.\tilde{C}$, or even $D = AB\tilde{C}$ where the "multiplication"

(AND) signs are implied. This type of

algebra, based on logical statements that

TABLE 1. Properties of Boolean algebra.

2		= 0	12	Ă.A Ā+A	= 0 = 1	22	A. (B+C) A+A.B	$= A \cdot B + A \cdot C$ $= A$
4		= 1		0 + A 0.A	= A = 0		A + Ā. B A. (A + B)	= A + B = A
	0.1 0+1	= 0 = 1		1 + A 1.A	= 1 = A		(A + B).(A + C) $\overline{A + B}$	= A + B.C = Ă.B
7 8	Õ 1	= 1 = 0			= B + A = B.A		A.B	= Ā + Ē = A
	A+A A.A		-		$= A + (B + C)$ $= A \cdot (B \cdot C)$		$\overline{A + B}$ $\overline{A.B}$	= A. = A + B

are true or false, is called Boolean algebra and it is a very useful tool in the development of logical thinking and in the design of digital circuits and systems.

As well as the AND and NOT operations it is necessary to postulate the OR operation which is represented by the (+)symbol of normal algebra. For example, if a logic gate has two inputs A and B, and its output D is in the logic 1 state when either A or B is in the logic 1 state this statement can be written as D = AOR B which is represented by D = A+B.

A logic gate is an example of a basic logical circuit, called a combinational circuit, the output of which at a given instant is determined by the state of its inputs. Irrespective of its complexity, certain relationships, laws and simplification rules of Boolean algebra can be used to represent or investigate the behaviour of a combinational circuit. Using up to three variables, Table 1 shows some of the properties of this algebra some of which are the same as ordinary algebra. In Boolean algebra. division and subtraction have no meaning and the variables can only have the values 0 or 1. Table 2 shows the Boolean algebra theorems relating the values 0 and 1 in terms of relay contacts that are either open (logic 0) or closed (logic 1). Table 3 illustrates the Boolean algebra theorems in one variable A in similar terms, where A can have either of the states 0 (Acontact open) or 1(A-contact closed). In Table 1 relations 26 & 27 together are known as De Morgan's theorem and 20 & 30 are identical with 26 & 27 except that the variables have been negated (or inverted or complemented).

Combinational logic circuits may take many different forms, one of which employs relay contacts which is useful for illustrating some of the simple Boolean
 Table 2. Boolean theorems in terms of relay contacts.

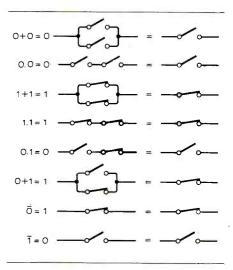
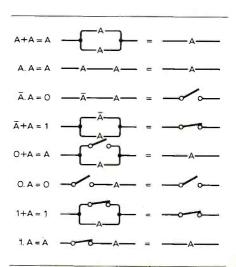


Table 3. Boolean theorems in one variable.



^{*}All with Paisley College of Technology.

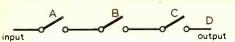
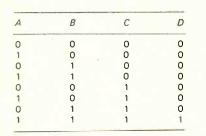


Fig. 1. D = 1 when contacts A AND BAND C are closed, represented by D = A.B.C.

TABLE 4. Truth table for Fig. 1



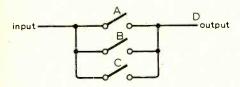


Fig. 2. D = 1 when A OR B OR C are closed, represented by D = A + B + C.

TABLE 5. Truth table for Fig. 2 '

GATE

A	В	С	D
0	0	0	0
1	0	0	1
0	1	0	1
1	1	0	1
0	0	1	1
1	0	1	1
.0	1	1	1
1	1	1	1

relations. For example, in Figs 1 & 2, A, B and C are contacts operated by relay coils (not shown) to complete a path between input and output. Thus, we are concerned with the statement "the connection between input and output is complete".

When this statement is true D = 1and when it is false D = 0. In Fig 1, D = 1 only when contacts A AND B AND C are closed simultaneously so the Boolean representation is D = A.B.C.Hence, series-connected contacts of the same type provide the AND operation. In Fig. 2, D = 1 when contacts A OR B or C are closed so the situation may be represented by D = A + B + C. If more than one contact is closed the above statement is still true, i.e. D = 1. Thus, parallel-connected contacts of the same type provide the OR (or "inclusive" OR) operation and the order in which they are wired or considered does not affect the truth of the statement.

The validity of a Boolean statement representing the behaviours of a combinational logic gate can be checked by means of a truth table, which is a tabular listing of all possible logic combinations of the variables and the resulting output logic, Tables 4 & 5 are the truth tables for Figs 1 & 2 respectively and they show that a complete truth table requires 2n rows to represent a gate having n variables. Table 6 is a listing of the truth tables for the commonly-used combinational logic operations and shows the names given to the logic gates used to realize these operations. The NOR (NOT OR) gate performs the complement of the OR function and the NAND (NOT AND) gate the complement of the AND function.

and $\stackrel{A}{\stackrel{}{\underset{c}}}$ $\stackrel{A}{\stackrel{}{\underset{c}}}$ $\stackrel{A}{\stackrel{}{\underset{c}}}$ $\stackrel{B}{\stackrel{}{\underset{c}}}$ $\stackrel{B}{\overset{}{\underset{c}}}$ $\stackrel{B}{\overset{}}$ $\stackrel{}{\underset{}}$ $\stackrel{B}{\overset{}}$ $\stackrel{}}{\overset{}}$ $\stackrel{}{\underset{}}$ $\stackrel{}}{\overset{}}$ $\stackrel{}}{\overset{}}$ $\stackrel{}}{\underset{}}$ $\stackrel{}}{\overset{}}$ $\overset{}}{\overset{}}$ $\overset{}}{\overset{}}$ $\overset{}}{\overset{}$

SYMBOLS

Fig. 3. Some of the symbols used for logic gates.



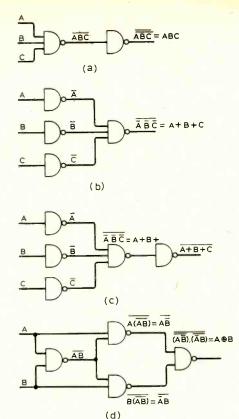


Fig. 4. Logic operations of AND (a), OR (b), NOR (c) and exclusive OR (d), can be realized using only NAND gates.

Unlike the OR gate, the "exclusive" OR gate only makes D = 1 when either A = 1 OR B = 1 but not when A = B = 1. The exclusive OR operation is used so frequently that it is given the symbol +. Thus, D = AB + AB = A + B.

Examples have been given of basic logical operations realized by means of relay contacts but this technique can become unwieldly. A more general diagrammatic representation of logic gates is desirable as the logic diagram should be independent of the circuit techniques employed in their realization. Unfortunately, there is no universally accepted symbol* to represent a particular logic gate, some of the different types of symbols that have been used being shown in Fig. 3.

While the operation indicated by a logic gate symbol is independent of the circuitry used, it should be realized that as there are two allowed states the user must decide which state is to represent the logical 1 condition. For example, if the two states are represented by voltage levels, one may be positive and the other 0 V, one may be negative and the other 0 V, one may be positive and the other negative, both may be positive or both negative. Irrespective of the values of these voltage levels, the system is said to use positive logic if the logical 1 state is represented by the more positive level and is said to use negative logic if the logical 1 state is represented by the more negative voltage level.

*Following a majority decision of the I.E.C., the B.S.I. have opted for the rectangular logic gate symbols (not shown in Fig. 3). BS3939 section 21 is currently being amended. — Ed.

TABLE 6. Truth tables for common combinational logic operations.

INP	UTS			OUTPUT D =		
A	В	A.B	A+B	A + B	A.B	A+B
0	0	0	0	1	1	0
1	0	0	1	0	1	1
0	1	0	1	0	1	1
1	1	1	1	0	0	0
NAME	OF GATE	AND	OR	NOR	NAND	EXCLUSIVE

Although all the combinational logic gates appearing in Table 6 are available in various forms of hardware, it is possible to build complete logic systems with either only NOR gates or only NAND gates. Fig. 4 shows how the AND, OR, NOR and exclusive-OR operations may be realized using only NAND gates and Fig. 5 shows the sole use of NOR gates to realize the AND, OR, NAND and exclusive-OR operations. These illustrations also show the application of some of the relations given in Table 1. Figs 4(a) & 4(b) use relations 28 & 30 respectively on the output function and relation 30 is also used on the output from the threeinput NAND gate in Fig. 4(c). In Fig. 4(d), relations 27, 21 & 11 are used in turn on both inputs to the final gate and relation 30 used on its output function. Figs 5(a) & 5(b) use relations 29 & 28 respectively on the output function, relation 29 also being used on the output of the three-input NOR gate in Fig. 5(c). In Fig. 5(d) relation 29 is used on the input to the final gate and relations 27, 26, 21 & 11 used in turn on its output function.

These examples show that more gates of a given type are required to realize any other particular simple logic function. Although this point has been illustrated by simple Boolean expressions, in the design of more complicated systems the algebra may be cumbersome and other techniques such as Karnaugh mapping

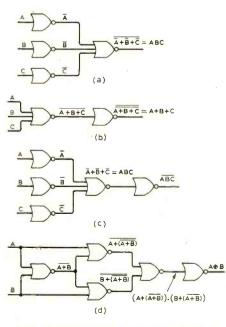


Fig. 5. NOR gates can realize the logic operations of AND (a), OR (b), NAND (c) and exclusive OR (d).

would be used to obtain a minimal solution. To synthesize a complex system it may be advisable to use gates of one type because of their availability and cost.

Many different types of solid-state electronic logic-gate realizations are available such as resistor-transistor logic (r.t.l.), diode-transistor logic (d.t.l.), directcoupled transistor logic (d.c.t.l.), transistor-transistor (t.t.l.), logic emittercoupled logic (e.c.l.) compleand mentary metal oxide transistor logic (c.m.o.s.). These families of gates have different characteristics and one family may prove to be more suitable than another in a particular application. For example, the prime consideration may be highest possible speed of operation or lowest power consumption or greatest immunity to external noise or the simplicity of interfacing the gates with other circuitry. The successful design of a digital system therefore requires a working knowledge of the capabilities of the various types of electronic gates available.

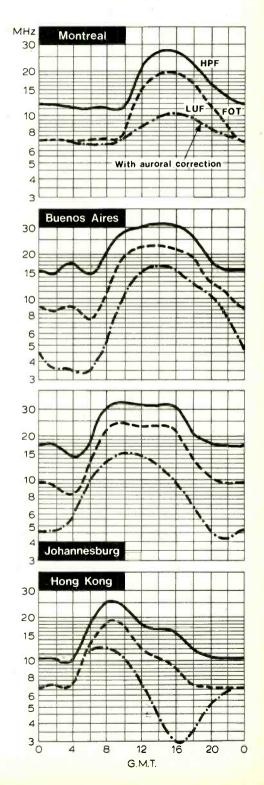
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11 Basic logic gates
Subsequent issues will cover wideband amplifiers, alarm circuits, digital counters, pulse modulators. Introductory articles

Subsequent issues will cover wideband amplifiers, alarm circuits, digital counters, pulse modulators. Introductory articles in *Wireless World* indicate availability of Circards, which are normally ready for despatch on the 14th of the month, and the Circard concept was outlined in the October 1972 issue, pages 469/70.

H.F. Predictions for November

LUF (lowest usable frequency) curves are for reception in the U.K. of point-to-point telegraphy services using medium power and directional aerials. LUFs for domestic reception of high power broadcasting stations would be about the same, while those for the amateur service would be a few megahertz higher particularly at noon.

Commercial working frequencies are kept below FOT (optimum traffic frequency) to allow for day-to-day ionospheric variations and seasonal trend over the month. Amateur "openings" can be expected on bands up to HPF (highest probable frequency).

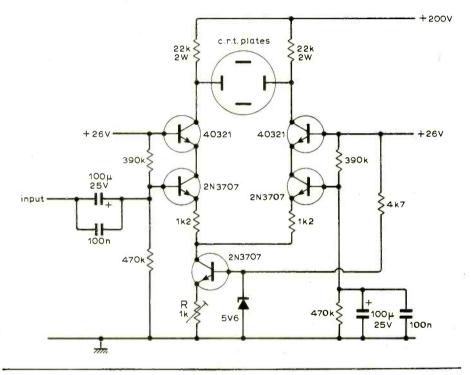


Circuit Ideas

560

Deflection amplifier

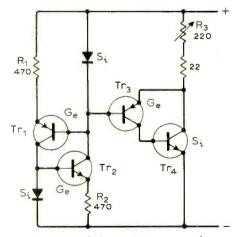
The amplifier is designed for use with an electrostatically deflected tube, and combines the frequency-response of a cascode amplifier with the linearity of a constant current-fed long-tailed pair. Adjust the value of R to give 3mA through each load resistor. The output transistors need small heat sinks. G. A. Johnston, Stechford, Birmingham.



Two-terminal current controller

This is an adaptation of Williams' well-known ring-of-two to produce an adjustable current regulator or limiter for use in test circuits or incorporation into power supplies. Its particularly low minimum voltage drop, around 1.4V, is obtained by combining germanium alloy transistors and forward-biased silicon diodes.

The ring-of-two uses transistors Tr_1 and Tr_2 drawing a nearly constant current over a wide range of voltage. If only a small controllable current is required, this may be adjusted by varying either R_1 or R_2 or both. It is desirable to keep the ring-of-two transistors as cool as possible, and so Tr_3 and Tr_4 are added. The current in this pair is adjusted by means of R_3 . Transistor Tr_4 is heavier transistor and carries the



major part of the total current whereas Tr_3 , like Tr_1 and Tr_2 , operates at low current for stability. J. P. Holland, London SW15.

Simulating high-capacitance electrolytics

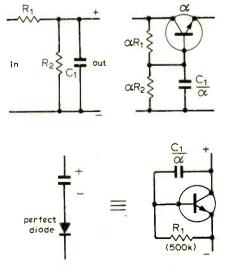
The first two circuits below are nearly equivalent, excepting that the drain of current is drastically reduced in the second. For small-scale applications, a BC107 with h_{FE} of about 300 can be used, with up to 300mW dissipation.

Either can be used to feed an a.f. preamplifier, or to partially stabilize a battery supply (e.g a car battery), but the second has very little drain on the battery. By having a capacitor of about 100μ F with a BC107, an apparent capacitance of about 3000μ F is put across the output. The second circuit is cheaper and far less bulky than the first. I used this with certain audio equipment and it has completely eliminated the tendency of the preamp to "motor-boat".

The last two circuits are also almost exactly equivalent. Resistor R_1 is to cut down the leakage current of the circuit, and can be a very high value. The leakage current of the second circuit is now about $10\mu A$, using a BC 107 and $100\mu F$.

I found the second circuit useful in switch-on-protection of loudspeakers.

Other circuits, using higher rating transistors (e.g. 2N3055) or p-n-p transistors, can be used. Even bearing in mind that h_{FE}



for 2N3055 is only about 30, a cost saving of about 40% can be obtained. R. M. Brady, Urmston, Manchester.

10–2 Metre Amateur Transverter

Design and construction of a unit which can be used with most 100W output 10-metre transceivers

by D. R. Bowman, G3LUB

The aim of this article is to describe the design and construction of a 10 to 2 metre transverter. This unit is compatible with the transceiver published in *Wireless World*¹ and the two pieces of equipment combine to produce an elegant 2 metre s.s.b. transmitter/receiver. The transverter can be used with most 100W output transceivers which have the facility of operating on 10 metres. The unit can be used with all other transmission modes at a reduced power level.

Methods of generating v.h.f. s.s.b.

There are two basic methods of generating a single-sideband suppressed-carrier signal within the 2 metre band². The first method uses a high frequency phasing system at any frequency in the 5-25MHz region which is then heterodyned into the 2 metre band. This technique has gained support recently and when carefully built is capable of producing a high quality signal. The second method uses a transverter (heterodyne unit) in conjunction with a commercially built h.f. band s.s.b. transceiver. It is the availability of these transceivers rather than their ultimate performance on 2 metres which has been the reason for the popularity of the transverter technique.

The second method mentioned above has some serious drawbacks. The spectral clarity of the output of an h.f. transmitter rarely exceeds 50dB. This means that inband spurious signals no more than 50dB below the peak output of the required signal are present. Many h.f. transceivers do not even achieve this figure and, whereas these spurious signals cause minimal interference on the h.f. bands (80-20m), on 2 metres they can be objectionable. The reason is plain when one realizes that the dynamic range of received signals at v.h.f. can be 80dB, whereas on the congested h.f. bands the range rarely exceeds 40dB.

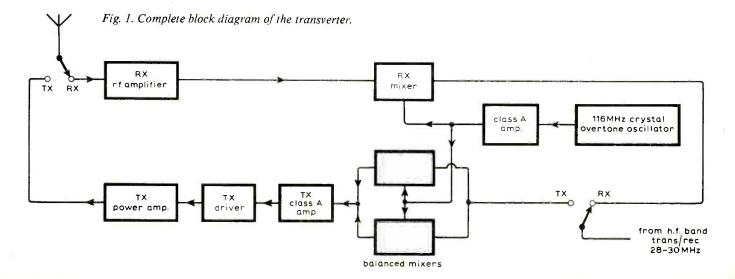
There is one small mitigating effect and that is the variable amplitude of many of these spurious signals. Many of them follow the speech waveform and therefore have extremely low average signal levels. This demonstrates the point that very great care is required when operating h.f. transmitters via transverters on the v.h.f. bands. One must not be scared off by the problem, but should design to minimize it.

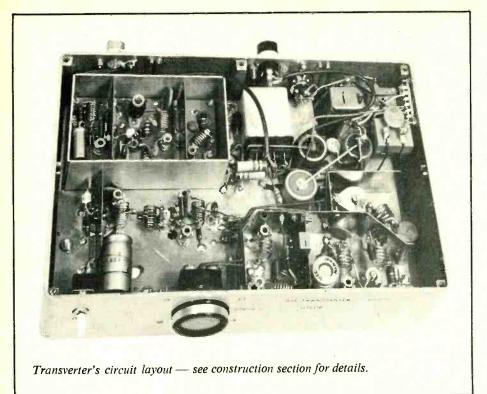
The transverter is equally suited for use with any of the available commercial transceivers but the spectral purity of the v.h.f. signal will of course be mainly determined by the performance of the h.f. exciter. These inband unwanted signals are 50dB down in the case of "The Cumbrian Transceiver" at least¹ and there are very few of them. This situation can be further improved by introducing a selective 28MHz pretunable filter between the exciter and the transverter in Fig. 5. It was decided that these levels were adequate, remembering that an aerial filter (high Q break) can be expected to contribute a further 20dB and the aerial at least 10dB to the reduction of spurious out-of-band signals.

Transverter in principle

The transceiver circuit can be divided into two basic units. These are the receiver's 2 to 10 metre converter and the transmitter's 10 metre to 2 metre transverter with its appropriate power amplifier. The receiver's converter consists of an r.f. amplifier feeding a mixer which requires a local oscillator with a frequency of 116MHz. The transmitter transverter consists of a balanced mixer requiring a local oscillator of the same frequency followed by a multistage power amplifier. A considerable saving can be made by using one source of local oscillator voltage for both transmit and receive mixers.

Fig. 1 shows the complete block diagram of the "Westmorland Transverter". As signal flow is in opposite directions on transmit and receive isolation is increased between the 2 metre aerial socket and the 10 metre transceiver, keeping 10 metre i.f. breakthrough to a minimum. The only drawback to this system is that two possible paths for internal self oscillation may exist. If 2 metre noise should appear at the output of the power amplifier, under certain conditions this can be amplified and frequency changed to 10 metres where it will find its way into



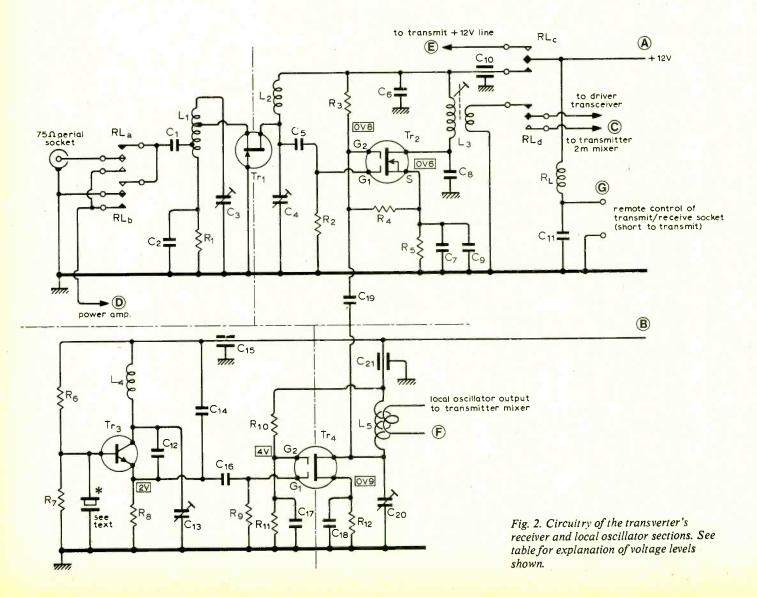


the input of the transmitter mixer, thus setting up an oscillatory path. Good relay isolation might be enough to eliminate this effect, but there is a further danger point via the common local oscillator feed line.

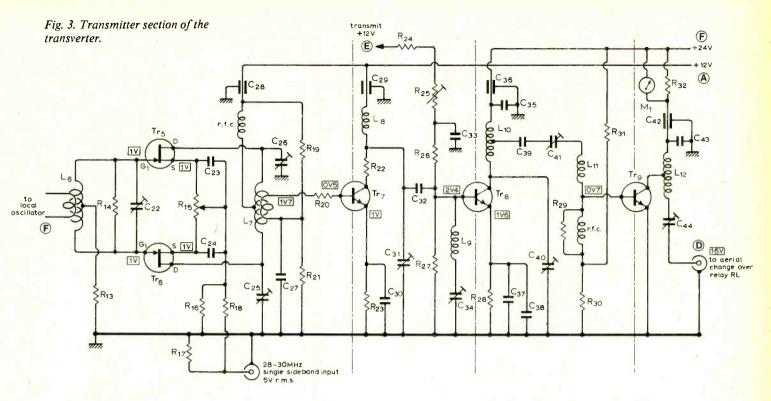
The simplest method of overcoming this problem is to switch the relevant receive and transmit stages in phase with the main transmit/receive operation of the exciting transceiver, but allowing the overtone oscillator to run continuously. This also eliminates the first feedback path and avoids any necessity to use high isolation transmit/receive relays. The block diagram shows the l.o. source simply as a 116MHz crystal oscillator.

However carefully a low-frequencyderived multiplier chain is designed, large numbers of spurious frequencies will be present in the output. One method of overcoming this problem is to use an LC oscillator phase-locked to a low frequency crystal, but this is rather complex and a more simple if less elegant system is to use an overtone oscillator with an appropriate crystal.

No mention has so far been made concerning the reasons for using 10 metres rather than any of the other bands found on most transceivers. This is simply that the 2 metre band is 2MHz wide as in the 10 metre range. Although there is



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some advantage in using 14MHz (from the spurious signal reduction point of view), image problems are considerably greater.

Practical circuitry

The Receiver section

The receiver section consists of two stages, namely a 2 metre r.f. amplifier followed by a mixer which converts the received 2 metre signal to 10 metres which is compatible with the associated transceiver. It was decided to use a common-baseconnected f.e.t. in the r.f. amplifier $(Tr_1,$ Fig. 2). This circuit was chosen in view of its unconditional stability at all frequencies to at least 500MHz. The maintenance of overall stability is usually the most difficult problem for the amateur constructor and for this reason a dual gate device was not used.

The noise performance is in the region of 2dB and the gain is adequate to mask inevitable mixer noise. The r.f. circuitry situated between the aerial relay and the source connection of TR_1 has a low value of loaded Q and the source coil tapping point should be adjusted for minimum noise. This adjustment is not critical and it may be easier to find the point of maximum signal strength, the difference in noise level being small.

The effective G_m of the f.e.ts varies considerable within any device type and therefore the value of R_1 has to be found for each case. A multimeter should be connected across the resistor R_1 the value of which is adjusted until the calculated current flow is about 5mA.

A source current $Tr_1 = \text{meter voltage} \div R_1$.

No special r.f. overload protection has been included in the circuit. Over a long period of time using both a high power linear amplifier as well as the transistor power amplifier to be described, no incidents of r.f. transistor damage have occurred. With frequencies as high as 150MHz it is difficult to design protection circuits that do not produce some performance deprivation and as junction f.e.t. devices are inherently robust no such protection is considered necessary.

Receiver mixer

The circuit of this mixer uses a dualgate m.o.s. f.e.t. (Tr_2 type 40673 or its equivalent). This is probably an appropriate point to warn any prospective constructor against the use of the earlier unprotected dual gate devices which were particularly prone to static generated gate electrode breakdown.

The 40673 f.e.t. is extremely well suited to use as a mixer as it couples very small local oscillator drive requirements with considerable isolation between the signal and *l.o.* paths. It also presents a high impedance to the r.f. amplifier

.

Voltage table			
Circuit Point	D.C. Voltage (Volts)	R.M.S. Voltage (Volts)	
Across $R_1 220 \Omega$ Tr_2 Gate 2 Tr_2 Source Tr_3 across R_{19} (osc. disabled). Tr_4 gate 2 Tr_6 gate 1	5mA (see text) 0.8 0.6 2 4	1 r.f.	
$Tr_{\rm s}$ gate 1 r.f. in across $R_{\rm s}$	1.7	measured relative to ground. 5 r.f.	
L_7 secondary T_7 base r.f. drive Tr_7 emitter Tr_8 base Tr_9 emitter	1 2.4 1.6	.5 r.f. 1 r.f.	
Tr_9 base Output measured across a 50 Ω dummy load	.7 approx	2.5 r.f. 16 r.f.	

All post mixer r.f. voltages are those measured when the transceiver is driven with an intermittent whistle i.e. the base of Tr_7 onwards.

output, helping to maintain the Q of the r.f. tuned circuits. The transfer characteristics of these devices are substantially square-law, minimizing the generation of unwanted signals. The l.o. drive level is non-critical and any level between 0.2 to 1V r.m.s. works well. As the measurement of 116MHz r.f. voltages is rather difficult, no figure has been quoted.

Local oscillator

To achieve the correct frequency conversions a source of extremely stable 116MHz oscillations is required. Transistor Tr_3 is connected in an overtone crystal oscillator circuit. Almost all crystals with frequency markings in excess of 20MHz are intended for overtone operation, but this mode must not be mistaken for harmonic operation as it is quite different. A harmonic oscillator operated on the fundamental (lowest) resonant frequency of the crystal and a resonant circuit tuned to the required (higher) frequency is incorporated in the circuit. This selects the output frequency and at the same time attenuates to some extent the other harmonics which in this context can be considered to be spurious signals. Although these other harmonics are reduced in level they are still present and are liable to generate unwanted signals in the receiver's output.

The overtone oscillator relies upon the fact that all crystals have a number of harmonically related resonances. These occur at odd multiples of the crystal's fundamental frequency and the circuit is designed to excite the crystal in the range of the required overtone. In practice the highest multiple that is usable is the seventh or possibly ninth overtone.

The oscillator is followed by an isolation amplifier which is necessary as the mixer load appearing in parallel with the oscillator output varies considerably from the transmit to receive mode. This amplifier (Tr_4) uses a dual-gate f.e.t. which is extremely stable in operation partly as a result of the resistive input circuit.

Transmitter mixer

The transmit mixer circuit consists of two cheap junction f.e.ts (Tr_5 and Tr_6) 2N3819 connected in a balanced configuration. The local oscillator voltage is fed in pushpull to the two gate electrodes while the 28MHz s.s.b. is parallel-connected to the source electrodes. This arrangement is used as the harmonics of the 10 metre s.s.b. are balanced and therefore attenuated. This helps to reduce the fifth harmonic of the input s.s.b. which tunes across the range 140-150MHz. Variable resistor R_{15} in association with C_{25} and C_{26} should be carefully adjusted to minimize this harmonic. The local oscillator harmonics are not reduced by the balancing procedure but as these signals are harmonically related to 116MHz, they are well clear of the 2 metre band and therefore are easily eliminated by the various resonant circuits.

Two-metre linear power amplifier

The output of the transmitter mixer is at a very low level and a linear amplifier is required to increase this level to about 5W p.e.p. The 5W level was determined mainly by the availability of v.h.f. power transistors. The R.C.A. overlay silicon transistors do not readily lend themselves to large signal v.h.f. linear amplification and for this reason the 2N3375 used is underrun. A cheaper alternative to the 2N3375 is the 2N3866 which has no mounting stud and therefore will require some heat sink arrangement. Possibly a simple pushfit heat sink over the transistor would be adequate if care is taken to limit the continuous drive tune-up periods.

The 2N3375 is forward biased and operates in what is really class B. The quiescent current is set to between 20 and 50mA, by adjusting the resistance value of R_{31} .

The driver stage makes use of a 2N3866 which is forward biased only during the transmit period. This stage operates in class A and therefore its collector current should show no variations as a result of the speech waveform. The standing current of the driver stage is measured by reading the direct voltage appearing across the emitter resistor R_{28} (33 ohms) and should be set to between 50 and 80mA by adjusting R_{25} . A small heat sink should be mounted on the transistor can to keep the collector temperature below 70°C;

 L_9 and C_{34} constitute a series trap which should be tuned to 116MHz. This circuit helps to reduce l.o. feedthrough that is inevitable even after careful balancing of the mixer circuit comprising Tr_5 and Tr_6 .

The first stage of the linear amplifier, Tr_7 , provides considerable gain, but its output is still at a low level. The BFY 90 common-emitter-connected class A amplifier is capable of delivering up to about 50mW with a low level of distortion. This transistor type is notoriously unstable but as long as the circuit values are copied and the layout shown in the photograph duplicated exactly, no difficulties should be experienced. C_{31} should be adjusted for maximum 2 meter drive to the p.a. as should C_{41} .

Aerial changeover relay

The aerial changeover relay is a standard RS Components type 21. This relay has a 12V d.c. coil and four changeover contacts. One of these contacts is used to switch the aerial while another connects the redundant input/output line to earth. The normal practice of using a coaxial relay is not necessary as the relay is mounted so close to the output transistor tank circuit that the spring contacts in the relay become part of the tuned output matching circuit. As a result the power losses are minimal.

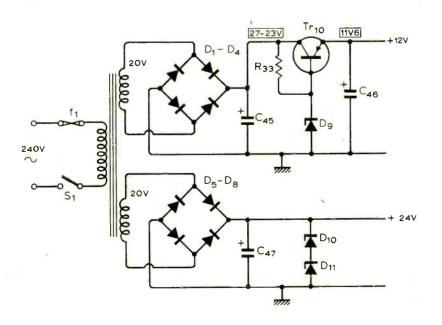


Fig. 4. Power supply circuit. See components list for transformer details.

The other pair of changeover contacts is used to switch the h.t. to the appropriate sections and switch the 10 metre input/ output line from the converter/receiver to the transmitter/transverter. The control of this transmit/receive relay is via a jack socket mounted on the transverter box. A short circuit across this jack socket energizes the relay and changes the transverter from receive to the transmit mode.

Power supply

In the unit constructed by the author there was very little room left for the power supply. As a result the circuit is very simple and uses a heavily overrun transformer. This does have the advantage of increasing the reliability of the output power transistor as the h.t. voltage drops considerably when continuous high current is taken from the supply. The transformer has two 3VA 20V windings, one of which supplies the p.a. at +24Vand the other at +12V.

The 12V supply has no short-circuit protection but does incorporate a very simple series stabilizer. The 24V supply has no stabilizer but uses a zener diode to clamp the voltage, thereby preventing a high voltage occurring at very low load currents. The use of separate secondaries helps to provide supply isolation which, in turn, makes the maintenance of stability easier. The peak current, as indicated by the p.a. meter, is about 250mA. while the 12V supply provides about 120mA.

Construction

The construction technique used for the Westmorland Transverter is slightly unusual. The complete circuit is built on to a 8.5 \times 5.25in piece of glass-fibre copper laminate board. The circuitry is almost completely mounted on the copper side. This board is in turn mounted within a 8.75 \times 5.5 \times 2.125in die-cast box with only the input, output, transmit / receive control socket and mains input terminations mounted on the rear wall. The front carries a miniature meter indicating p.a. collector current and a miniature mains on/off switch. The receiver converter and overtone oscillator are mounted on a separate, copper uppermost board within a small aluminium screening box. This precaution is probably unnecessary but occurred as the converter was separately built quite a time before the rest of the transverter.

Various other screens can be seen in the photograph and, with the exception of the roughly laid out power supply, the author would suggest that any prospective constructor use a similar layout. This arrangement is in the form of a loop which follows the block diagram closely, allowing minimum path lengths between stages and helping to maintain r.f stability. The only underboard wiring is the screened lead carrying the s.s.b. from the relay to the transmit balance mixer and the r.f. bypassed h.t. lines.

The balanced mixer is symmetrically built (very important as it helps the maintenance of r.f. balance).

One important note of warning is in order. The author succeeded in destroying a number of output transistors before he realized that an intermittent short circuit on C_{41} was allowing 24V to be directly connected to the base of Tr_{q} . The inclusion of C_{39} avoids this difficulty.

Alignment

The alignment of the converter will be dealt with first and separately from the rest of the transverter.

It may be that a prospective constructor would like to build the converter first, allowing the 2 metre band to be monitored before the extra expense of the complete unit is contemplated. The converter circuit can be simplified by bypassing Tr_4 if only the construction of a receiver converter is contemplated. The first point to align is the standing current of Tr_1 . This should be set to about 5mA by adjusting the value of R_1 in the manner that has already been described. The next step is to feed a large signal having a frequency within the 2 metre band into the converter's aerial input socket. The converter's output should be fed to an appropriately tuned 10 metre receiver. The 116MHz overtone oscillator crystal should be inserted into its socket and C_{13} carefully adjusted until the 2 metre signal can be heard. This is the most exacting part of the alignment procedure.

It will be found that when the correct position for C_{13} has been found the oscillator will be stable and is less prone to frequency pulling when either a hand or screwdriver is brought near to the Tr_3 circuitry. Next C_3 and C_5 are adjusted for maximum signal delivered to the receiver which is tuned to the centre of the 10 metre band. The variable inductor L_1 is similarly peaked for maximum output. The method of adjusting the tap position on L_1 has been dealt with earlier in this description. If Tr_4 has been included then again C_{20} should be adjusted for maximum signal to the associated receiver. If the transmitter mixer is not connected to L_5 it is possible that this stage may be unstable. If this does occur C_{20} should be detuned until the rest of the transverter is built. This concludes the alignment of the converter and now the completed transverter can be dealt with.

Before any attempt is made to run the transverter it is advisable to check all the direct voltages noted in the table. If any large discrepancies are noted these errors must be corrected by careful circuit checking before proceeding further.

The quiescent current of Tr_8 must be adjusted to somewhere between 50 and 80mA. (1.7 and 2.7V as measured across R_{28}). This adjustment has also already been described and is achieved by trimming R_{25} . Variable resistor R_5 should be roughly adjusted to the centre of its travel and the 10 metre s.s.b. from the exciting transceiver should be fed via the appropriate socket to the balance mixer. The aerial output socket must be terminated in a $50/70\Omega$ dummy load. One point to note is that to set the quiescent current of Tr_8

Components list

All resistors listed should be $\frac{1}{4}$ or $\frac{1}{8}$ watt composition or carbon types (not wire wound) with a $\pm 5\%$ tolerance except where other specifications are noted.

All capacitors have their values shown in the following manner. $.1\mu$ means $.1\mu$ F, 100p stands for 100pF and electrolytics are only used above 1μ F. The types are designated -FT stands for feed through, SM stands for silver mica, DC stands for disc ceramic or low stray inductance tubular ceramic, and all voltage ratings must be at least 12 volts except where otherwise noted. Where electrolytics are specified the actual value is relatively unimportant and there is no reason why a prospective constructor should not substitute available types.

Resistors

1	220 see text	18	150
2	220k	19	10k
3	470k	20	47
4	10k	21	3.3k
5	100	22	10
6	22k	23	100
7	10k	24	47
8	560	25	5k w.w.pot
9	220	26	180
10	68k	27	180
11	33k	28	two 68 in parallel
			(0.5W)
12	100	29	680
13	100	30	51
14	2.2k	31	1.5k
15	500 trimmer	32	0.25 see text
16	100	33	2.2k
17	75	34	50 or 75
			25-50W carbon

Capacitors

	Particip			
1	56 MC	25	10p tubular	
			trimmer	
2	.001 DC	26	10p tubular	
			trimmer	
3	5p tubular	27	470 DC	
	trimmer			
4	5p tubular	28	.001 FT	
	trimmer			
5	4.7p SM	29	.001 FT	
6	.1 DC	30	.001 DC	
7	.1 DC	31	5p tubular	
			trimmer	
8	18 SM	32	10 SM	
9	.001 DC	33	.001 FT	
10	.001 FT	34	5p tubular	
			trimmer	
11	.1 DC	35	.1 DC	
12	10 SM	36	.001 FT	
13	5p tubular	37	.1 DC	
	trimmer			
14	25 SM	38	.001 DC	
15	.001 FT	39	50 MC	
16	.5p see text	40	5 trim capacitor	
17	.001 DC	41	25 trim capacitor	
18	470 DC	42	.001 FT	
19	.5p see text	43	.1 DC	
20	5p tubular	44	25 trim capacitor	
	trimmer			
21	.001 FT	45	10 00µ/5 0V	
22	5p trim	46	600µ/20V	
23	.001 DC	47	2000µ/50V	
24	.001 DC	52	100p air spaced	
			trim	

Diodes

- 1 8100 p.i.v. rectifiers e.g. 1N4002, 300mA or greater
- 12V zeners, 2.5W e.g. BZX70-C12 10-1112V zeners, 400mW e.g. BZY88 12

Transistors

1	TIS 88	6	2N3819
2	40673	7	BFY90
3	BFY90	8	2N3866
4	40673	9	2N3375
5	2N3819	10	BFX29

Meter

1mA f.s.d. or other meter shunted by R_{18} to read 250mA f.s.d.

Additional

20V miniature mains transformer (e.g. RS Components), output 20V 3VA each 2A fuse and holder. Single pole changeover toggle switch

RS Components type 21 relay - see text

Coil details

With the exception of those stated cases all coils are wound on a .25in mandrel and mounted in a self-supporting manner.

- 1 9 turns 22 s.w.g. bare copper wire with a winding length of .5in tapped at three turns and five turns from the ground end.
- 2 8 turns 22 s.w.g. bare copper wire with a winding length of .45in.
- 3 10 metre i.f. transformer 22 turns 28 s.w.g. close wound on a .45in former and tuned with an iron dust core. The secondary consists of four turns wound over L_3 .
- 4 7 turns 22 s.w.g. bare copper wire with a winding length of .45in.
- 5 7 turns of 22 s.w.g. bare copper wire with a winding length of .4in. Also two turns of 22 s.w.g. enamel covered copper wire are pushed into the centre of L, for maximum coupling co-efficient. This two turn coil is coupled using twisted insulated leads to two turns similarly pushed into
- 6 8 turns of 22 s.w.g. bare copper wire with a winding length of .5in and provided with a centre tap.
- 7 7 turns of 22 s.w.g. bare copper wire with a winding length of .5in similarly with a centre tap. Also two turns of 28 s.w.g. enamel covered copper wire are coupled by pushing into the centre of L_7 . The two turns are connected to Tr_7 via a pair of insulated twisted leads.
- 8 4 turns of 22 s.w.g. bare copper wire with a winding length of .45in.
- 9 8 turns of 22 s.w.g. bare copper wire with a winding length of .45m.
- 10 5 turns of 18 s.w.g. bare copper wire with a winding length of .4in.
- 11 4 turns of 18 s.w.g. bare copper wire with a winding length of .3in.
- 12 5 turns of 16 s.w.g. bare copper wire with a winding length of .45in, together with a centre tap.

All r.f. chokes are constructed using .25 wavelength (at 2 metres) 34 s.w.g. enamel-covered wire, wound on home made p.t.f.e. formers. i.e. 18in of 34 s.w.g. enamel covered wire wound on these formers.

28MHz filter (Fig. 6)

- 8 turns 20 s.w.g. enamel self supporting L_1 $\frac{1}{2}$ in dia $\frac{1}{2}$ in long. L_2 8 turns as L_1 . The taps on both L_1 and L_2 should be at one turn from the earthed end of the coil. The coupling link is one turn of 20 s.w.g. enamel placed in each of L_1 and L_2 .
- $C_{\nu} C_2$ 10-50pF variable. C_{3} , C_{4} 47pF silver mica.

565

it is advisable to disable the overtone oscillator. The reason for this is that a small amount of 116MHz energy may leak through the balanced mixer and thus inflate the standing current of Tr_8 . Having set the quiescent current, the oscillator should now be enabled and the current of Tr_8 will almost certainly increase. Careful adjustment of C_{34} should allow this 116MHz leakage to be considerably reduced. The next step is to supply a 10 metre drive signal of a few volts to the transverter. If the exciting transceiver is a "Cumbrian" this drive will be obtained by switching on the audio tone and adjusting the drive level accordingly.

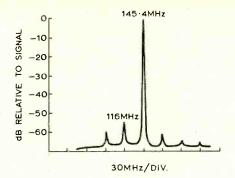
If a secondary two metre receiver happens to be available it should be tuned to receive the 2 metre output of the transverter, and C_{31} , C_{40} , C_{41} and C_{44} should be adjusted for the maximum indicated 2 metre signal. The receiver-to-transverter coupling must be progressively reduced in order that the increasing output power does not overload the auxiliary receiver. Finally C_{26} in conjunction with C_{25} can be adjusted for minimum 116MHz output while at the same time maximizing the 2 metre signal. This process requires an amount of care but will fully justify the constructor's efforts in providing a 2 metre s.s.b. signal free from spurious signals.

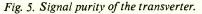
There is an alternative alignment procedure for the constructor who does not have a secondary 2 metre receiver. As the trim capacitors are adjusted, three and only three signal peaks will be found. One at 116MHz – 28MHz, i.e. 88MHz, a second at 116MHz, and the required peak at 116MHz + 28MHz, i.e. 144MHz. It is a simple matter to identify them. With no 10 metre drive, only the 116MHz peak will be present and as already explained C_{34} should null this. With 10 metre drive the correct 144MHz signal is received with minimum capacitance in circuit. As C_{31} , C_{40} , C_{41} and C_{44} are adjusted, the peak coincident with minimum capacitance should be chosen. The balance of the Tr_5 and Tr_6 circuit can be adjusted in a similar manner to that described in the previous procedure remembering that the minimumcapacitance peak must be enhanced while reducing the 116MHz by carefully balancing C_{25} and C_{26} . As the signal increases and the alignment proceeds the 10 metre drive must be reduced so as not to overheat either Tr_8 or Tr_9 .

Performance

There now follows a brief outline of the performance as measured on the author's transverter. The receiver converter exhibits a noise figure of about 2dB and a signal gain of 30dB. This noise performance will of course be degraded if the following receiver is either noisy or has a low sensitivity.

To improve the blocking performance, it would be necessary to change to a single conversion system where the i.f. filter is situated as close to the input of the receiver as possible. It would be an improvement to include a switchable attenuator between





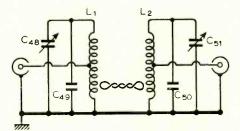


Fig. 6. High Q 28MHz filter whose use depends on the exciting transceiver used (see text).

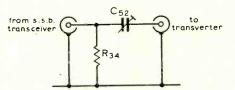


Fig. 7. Dummy load attenuator circuit. Internal layout of the transverter circuitry.

the aerial changeover relay and the r.f. amplifier.

The frequency drift is low — less than 2kHz per hour including initial switch-on drift. There are few spurious responses and those that occur are weak — an advantage of using a single frequency overtone oscillator.

Examination of Fig. 7 shows that the aim of keeping all spurious outputs from the transmitter to at least 50dB below the required output has been achieved. These spurious signals will be further reduced if the frequency sensitivity of the aerial is combined with a series high Q filter. This should drop the 116MHz to at least 80dB below the output. If the exciting transceiver is of a type other than the Cumbrian then it is advisable to include a high Qfilter circuit between the transceiver and transverter (Fig. 6).

Almost any transceiver with a 10 metre output in excess of about .5W will drive the transverter. If the transceiver used does not have an r.f. drive control then it will be necessary to attenuate the 10 metre drive using the dummy load circuit shown in Fig. 7. This can be adjusted to provide almost any level of drive out and should comfortably accept 200W p.e.p. intermittent speech. To prevent the load becoming overheated, the period of tuning should be as short as possible.

Wireless World, November 1973

The output power, in excess of 5W p.e.p., is difficult to measure as the power supply regulation will not support a continuous tone. Using a Heathkit V-7AU valve voltmeter and its associated r.f. probe at least 16V on speech peaks can be measured across a 50Ω dummy load.

power out (p.e.p.) = $\frac{V^2}{R} = \frac{16^2}{50} = 5.1$ W.

R measured in ohms, V in r.f. r.m.s. voltage.

References

1. Bowman, D. R., "10-80 Metre Amateur Transceiver", *Wireless World*, June-September 1972 (four parts).

2. "Fundamentals of S.S.B.", Collins Radio Co., 2nd ed., p 1-1

Sixty Years Ago

The throwaway perceptiveness of remarks made by some of the early experimenters gives one furiously to think on the obstacles which these pioneers faced. The progress that was made in days when it was an imaginative stroke to achieve the smallest step forward was remarkable. Dr. W. Eccles, discussing atmospherics or "Xs" in our November, 1913 issue, wrote "It is natural, but it is not scientific, to jump "It is to the conclusion that these strays are all due to lightning strokes occurring probably at great distances somewhere on the earth's surface, or possibly in the free atmosphere between one bank of ionised air and another. This, however, ignores the possibility that the source of the strays may be far outside the earth. There is nothing unreasonable in supposing that the sun, let us say, may send us occasional electric waves. For example, in the colossal movements of matter associated with the formation of a - movements that appear solar prominence to take place with enormous velocities electric discharges may be brought about of magnitude far transcending anything that can happen on the earth. These would give rise to electric waves which might reach the earth in perceptible intensity and constitute a proportion of our strays. On the other hand, we must not forget that we on the earth's surface may be protected by our ionised atmosphere from these extra-terrestrial waves. It is just such problems as these that the British Association Committee has set itself to inquire into"

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by J. L. Linsley Hood

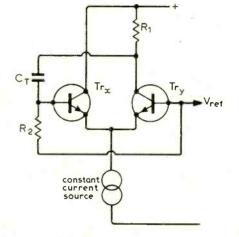
The growing use of phase locked loop systems in applications such as very high quality f.m. demodulators, in which a high degree of linearity between input frequency and output (control) voltage is sought, has focused attention on the characteristics of the available voltage controlled oscillators (v.c.os) — the linearity of the phase locked loop is mainly determined by, and cannot be better than, that of the v.c.o. contained within it. However, although the availability of a very linear v.c.o. system would allow improvements to be made in phase locked loops built around it, the usefulness of a circuit arrangement having a linear voltage/frequency characteristic extends beyond this to such applications as r.f. telemetry, "wobbulators", f.m. broadcast transmissions, and linear f.m. signal generators.

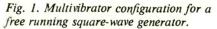
It is convenient in practice if the v.c.o. can be constructed using some form of multivibrator circuit in that this avoids the need for inductors, and, with a regard to the potential use of such a v.c.o. in an f.m. tuner demodulator system with an i.f. of 10.7MHz, it is desirable that the controlled frequency range of the circuit should extend some way above this. In view of the small lead inductances and stray capacitances which are demanded for satisfactory operation of any multivibrator circuit at these frequencies, it is helpful if the device can be constructed using some readily available high frequency linear integrated circuit, and the component arrangement has been chosen with this object in mind.

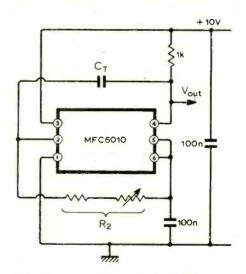
Circuit development

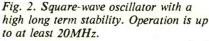
A number of multivibrator arrangements can be adapted to operate in a voltage controlled mode, but for optimum performance in high frequency applications, the non-saturating emitter-coupled systems are preferable. A suitable configuration for a free running square-wave generator is shown in Fig. 1.

In this the operation of the circuit is to switch the current available from the constant current source backwards and forwards between Tr_x and Tr_y . Resistor R_1 is the collector load of Tr_2 . When this transistor is conducting, the voltage drop across R_1 will always be constant and









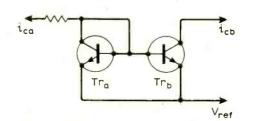


Fig. 3. "Current mimic" circuit which can be used to substitute the timing resistor, R_2 , in Fig. 2.

independent of the h.t. voltage supply, provided that this does not alter the output of the constant current source. This arrangement offers a high degree of intrinsic frequency stability and if C_T or R_2 is made variable, the "base" frequency can be altered.

A practical system is shown in Fig. 2, using a Motorola MFC6010 i.f. integrated circuit amplifier, which incorporates a long tailed pair, a constant current source and a reference voltage point. With a stabilised h.t. supply, this circuit gives a high long term frequency stability, and will operate to at least 20MHz.

This circuit arrangement can be converted into a linear and stable voltage controlled oscillator by the substitution of a "current mimic" or "current mirror" circuit for the timing resistor R_2 in Fig. 2.

Current mimic operation

The circuit configuration shown in Fig. 3 is widely used in integrated circuit manufacture, as for example in the Motorola MC3401P to provide a noninverting input on a Liniac type amplifier, or in the RCA CA3060/3080 micropower op-amps, to replace load resistors. Its attractiveness to the monolithic integrated circuit manufacturer arises from the ease with which identical pairs of transistors can be fabricated in this process.

If a given forward bias voltage is applied to the bases of an ideal identical pair of transistors, the same current will flow in the collector circuits of both. If, now, the bases of both of these transistors are joined to the collector of one of these (Tr_a) , and a certain current is drawn from this, this current will be the collector current of Tr_a plus the two base currents. Since the forward base potential of Tr_a has adjusted itself to the level required to produce the collector current of Tr_a , it will also have adjusted the base potential of Tr_b to produce the same collector current in Tr_b .

This will imply that the output ("mirror") current of Tr_b will be the same as the current drawn from the input, less the two base current contributions. If the current gains of the transistors used are high enough, or if — as will be the case in integrated circuit manufacture — the

Wireless World, November 1973

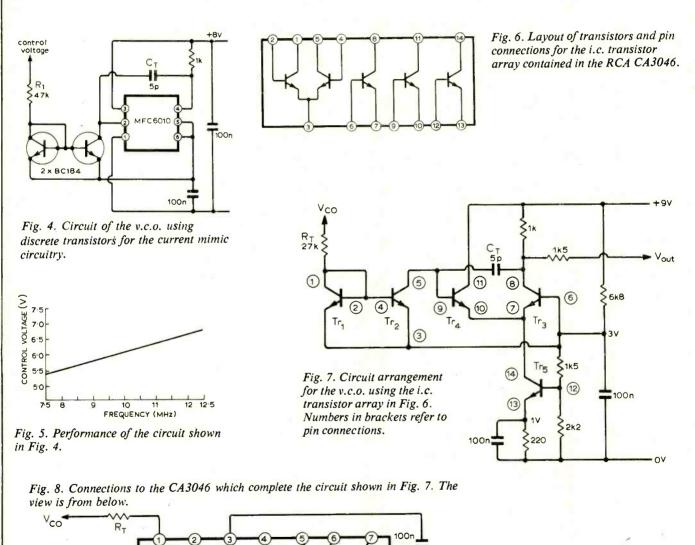
areas of the transistor junctions are trimmed to suit, the two currents (the input current and the mirror current) will be very nearly identical, and this identity will hold good over a wide current and temperature range. Although this is an integrated arrangement, discrete transistors can be used if their characteristics are reasonably closely matched.

In several circuits of the type shown in Fig. 4, the transistors used in the mimic circuit were BC184s in which the baseemitter forward voltage drop was matched by selection to about 10mV at 50μ A forward current (i.e., say 0.58V to 0.59V). This is inconvenient, but not difficult if one has a voltmeter and six or eight similar transistors to choose from. Although BC184s were used, any other similar small signal silicon devices would serve just as well.

The performance of the circuit shown in Fig. 4 is given in Fig. 5. The relationship between the control voltage and the frequency had a linearity better than 1% per MHz, and the frequency stability was as good as that of the author's signal generator during a six hour measurement period.

In view of this encouraging performance,

a means was sought for avoiding the inconvenience of having to select a matched pair of "current mimic" transistors, without the expense involved in the use of a matched-pair device. The solution was found in the use of an i.c. transistor array of the type contained in the RCA CA3046, of which the internal circuitry is shown in Fig. 6. In this particular case the array contains all the active components needed to make the v.c.o. circuit, including a matched pair of transistors. The circuit arrangement is in Fig. 7, for which the necessary interconnections across the base of the CA3046 are shown in Fig. 8.



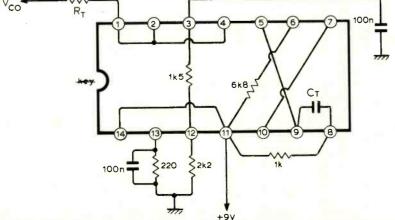
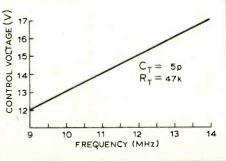


Fig. 9. Control characteristic of the v.c.o. in Fig. 7.



The performance of this circuit for a timing capacitor of 5pF, and with the other values as indicated, is shown in Fig. 9. The linearity of this arrangement is as good as that of the circuit in Fig. 4, but the long term stability of the Fig. 4 circuit is slightly better. Several CA3046 units were tried and gave identical free running operating frequencies.

Typical applications

A simple phase locked loop configuration built around this v.c.o. and suitable for use as a high quality f.m. demodulator, using an f.e.t. as a synchronous chopper type phase sensitive detector, is shown in Fig. 10. An amplitude limited input r.f. signal, of nominal 10.7MHz frequency, and of about 500mV amplitude is desirable for correct operation of the system. The output a.f. signal will be about 20mV for 75kHz deviation, with a second harmonic distortion content of about 0.07%.

An arrangement 'usable as a low distortion frequency modulated signal generator if a suitable low distortion sinewave modulation signal is applied, or as a "wobbulator" if a sawtooth input signal is provided, is shown in Fig. 11. Increasing the capacitance of the timing capacitor will provide a proportional reduction in operating frequency, allowing the system to be used, if required, down to audio frequencies, as a voltage controlled oscillator in electronic organ and similar applications.

As a final provocative thought, since it is possible to build voltage controlled oscillators (and phase locked loop demodulator systems containing these) whose linearity, over the 75kHz bandwidth normally used for f.m. transmissions, is better than 0.1%, by some margin, is not the ball now in the court of the broadcasting authorities to take note of this, and improve their f.m. transmission quality?

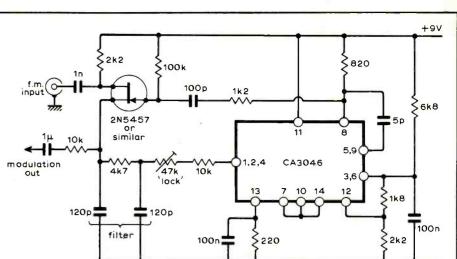


Fig. 10. Phase locked loop configuration built around the v.c.o., suitable for use as an f.m. demodulator. The f.e.t. is used as a synchronous chopper type phase sensitive detector.

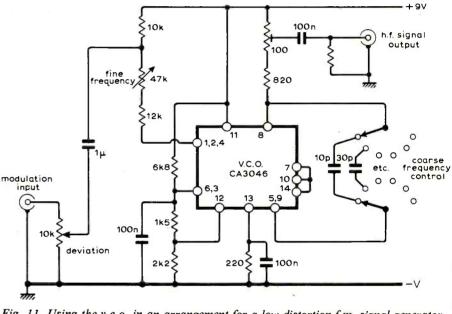


Fig. 11. Using the v.c.o. in an arrangement for a low distortion f.m. signal generator, or as a "wobbulator".

Books Received

Noise and Modulation are two books by F. R. Connor and are respectively the fifth and sixth in a series of books on introductory topics in electronics and telecommunications. They are texts designed to assist students preparing for university degree examinations or for courses at a similar level. "Noise" presents a survey of the various conditions of electrical noise followed by mathematical ideas concerning random variables. Circuit noise, noise factor and noise temperature are then considered. Finally, there is a comparative study of some important communication systems. "Modulation" provides a broad outline of the most important methods used in practice. Analogue methods such as amplitude and

frequency modulations are first considered and this is followed by phase modulation and the various types of pulse modulation. There is a final chapter on demodulation at the receiver. The material in both books is related to modern practice and a number of worked examples are included. Both books cost £1.10, and have approximately 100 pages each. Edward Arnold Ltd, 25 Hill Street, London W1X 8LL.

The Directory of Instruments, Electronics & Automation 1973 (ninth edition) contains collated information on manufacturers, trade names, equipment and components in the electronics industry. Sections come under the headings diary of events, association addresses,

who buys, U.K. agents, trade names, manufacturers' addresses and a buyers' guide. Price £7. Pp.328. Morgan-Grampian (Publishers) Ltd., 30 Calderwood Street, London SE18 6QH.

Recent additions to the Foulsham-Tab books on electronic topics and published by W. Foulsham & Co. Ltd., Yeovil Road. Slough, Bucks, are:

- How to Solve Solid State Circuit Troubles by Wayne Lemons, Price £1.75. Pp.304.
- How to Build Solid State Audio Circuits by Mannie Horowitz. Price £1.75. Pp.320.
- How to test almost everything electronic by Jack Darr. Price £1.30. Pp.160.

ΟV

Which Way Does Current Flow?

Some thoughts arising from recent correspondence

by "Cathode Ray"

I would probably be flattering myself excessively if I imagined for one moment that, when Messrs Banthorpe, Ellis and Whitehead¹ appealed for the direction of an electric current to be deemed to be the same as that of the electrons composing said current, it entered the heads of any of them to think "Well, anyway, old Cathode Ray will back us up". If, however, the question of what I would be expected to think about it had been put to them, as a minor matter of academic interest, they might confidently have claimed me as a potential ally, since in so far as I am well known at all I am well known as one who decides on circuit conventions by processes of logic and common sense rather than by what is generally accepted. They might have quoted as evidence my strong support for the heretical doctrines of M. G. Scroggie on phasor diagrams and their mass of related conventions. Beside this complex thesis, the case for abolishing the conventional direction of current flow in favour of the direction of electron flow (they would say in chorus) is simplicity itself as well as being exquisitely logical and commonsensical. So Cathode Ray could not but stand shoulder to shoulder with them.

Flows, fields and tracks

It is true that their case was severally put forward in terms that nearly brought tears to my eyes. I'm sure they meant well. And I hope they won't take it too hard when they find that their idol (self-flattery again!) has feet of clay (Daniel 2, 41-43). But it is a fact that I find myself having more in common with what Thos. Roddam divertingly proclaimed from the next bed to mine in the Geriatric Technologists' Home, as well as with the plain Yorkshire words of A. Parnham, also recorded on the p.386 already cited. I hope this revelation of my reactionariness will not cause a mass defection from the ranks of my followers (if any) - at least, not until they have read right through to the end, which is not far distant.

Roddam argues against reversing the usual convention (i.e., "current" opposite to electron flow) on the grounds that (a) to do so would cause a great upset (at which he hints by pointing out that among other things it would make nonsense of all diode and transistor symbols), and (b) (although one suspects that he personally might find such an upset quite amusing) there is really no need for it if only we stopped bothering our heads unnecessarily with charge carriers, which can safely be left to the electronic device makers, and dealt simply in fields and "current tracks".

But you may not be ripe for accepting such a revolutionary plan (and I wouldn't blame you). In that case you must meditate on the fact that not all electric charge carriers are electrons. In this respect electricity differs fundamentally from air and water, held up by Banthorpe as examples for it to copy. And although Ellis may not be able to satisfy his commendably inquisitive students on why there are two kinds of current (unless he has a hot line to the Creator) he cannot deny the fact. A great many carriers are holes and positive ions. So the choice of which to regard as positive for the purpose of specifying direction of current flow is arbitrary anyway. Even if we yielded to the entreaties of the enemies of the current (in two senses) convention and overthrew it we would not rid ourselves of the anomaly of some charge carriers flowing the wrong way.

The answer that would undoubtedly emerge from Messrs Banthorpe, Ellis and Whitehead is that, as practical current carriers, electrons are in a large majority, having in metallic circuits at least a virtual monopoly; and that should decide the matter. The sacred cause of Democracy and all that. Students would still have to face the fact of current carriers flowing in the opposite direction to the currents they carried, but less often than at present, and every little helps. Whether that little would be enough to justify reversing very nearly all the books is a big question, however.

Perhaps it would help to answer it if we went on to a point that the current revolutionaries don't seem to have considered, or if they have then not enough. Suppose we did what they said and agreed to call the positive direction of electric current the direction in which the electrons composing that current were flowing, or, if the flow was of positive carriers, the opposite direction. Would students be any less confused than they are now if they were told that the positive direction of current was the direction in which negative charges were flowing, or opposite to the direction in which positive charges were flowing? Or that (as suggested by Banthorpe) current flows from negative (i.e., a deficit) to positive (surplus), like water doesn't flow from the bottom of a well to the top of a hill?

Too much, too late

On the reasonable assumption that the students would be even more confused by this, the revolutionaries would be driven to deciding to call electrons positive charges. That would have been an excellent idea 75 years ago when electrons were discovered. But now? The imagination boggles. As my fellow geriatric has pointed out, all rectifier, diode and transistor symbols would need to have their arrow heads reversed. The electric fields would have to be changed around too. All those + and things in books on electronics would have to be interchanged. There would be great fun in deciding whether your car battery had been made before or after R Day and so whether red should be taken to mean black and vice versa, or not. And what about Fleming's right and left hand rules? And the corkscrew rule? Would we have to reverse magnetic field conventions? As in the administration of VAT, problems would multiply as one went along. Before we were finished, the operation of changing Britain over to the right-hand rule of the road would look simple and straightforward.

Believe me, I'm truly sorry to be numbered with the reactionaries, but in this matter (as the key worker says when he downs tools for a 50% rise) I have no alternative.

Reference

¹Wireless World June, 1973, p294 and August, 1973, p.386.

New Products

Reverberation unit

A variable decay reverberation system suitable for control room or portable use has been introduced by Feldon Audio Ltd. Manufactured by Quad-Eight Electronics of California, the RV-10 features a patented new approach to mechanical reverberation simulation which is claimed to provide a clean, transparent sound comparing favourably with existing devices or chambers.

The creation of totally new effects can be achieved by four different initial delays developed by independent transmission lines and the full delay pattern is released after 55 milliseconds. The reverberation runs in four continuous trains of multiples of the delay times with a signal to noise ratio of 60dB. Immunity to external noise is better than 55dB which makes the RV-10 ideal for use in control rooms under high-level monitor conditions. It also features 3 steps of low frequency roll-off which are 100Hz, 250Hz, 500Hz at 18dB per octave. Completely self contained, the unit is $19 \times 3\frac{1}{2} \times 10\frac{1}{2}$ in and 17 lb in weight.

Distortion in the drive and recovery system is under 0.25% up to full output level of +18dBm maximum. The input sensitivity is +4dBm and is continuously variable down to -20dBm with internal trim pot. Input/output impedance is 600Ω , transformer isolated and floating. The effective bandpass of the RV-10 reverberation system is 100Hz to 7kHz which is independent of the variable decay time setting. The overall frequency response has been limited to the useful reverberation bandwidth. This is claimed to be good industry practice and in conjunction with built-in filters eliminates the need for external filtering. Input and output connections are Jones barrier strip, and power requirements are 117V a.c. at 12W. Professional Equipment Division, Feldon Audio Ltd, 126 Great Portland Street, London W1N 5PH.

WW 309 for further details

17in storage c.r.t.

The direct-view storage cathode-ray tube type E722A manufactured by English Electric Valve Co. Ltd., provides very bright displays of information, ranging



forms to half-tone pictures. Designed primarily for use in air traffic control radars, it is equally useful for medical, tabular display or other applications involving viewing under high ambient light conditions.

A new type of annular flood gun is used in the E722A which gives a uniform high brightness level across the whole of the display area. The useful viewing screen area is 153 square inches (995 sq cm). A storage time of two to three minutes is normal with only ten per cent degradation of contrast. Storage can be extended by electronic methods to ten minutes or longer.

The image can be completely erased in a fraction of a second and selective erasure of information such as aircraft identification labels is possible. English Electric Valve Co. Ltd., Chelmsford, Essex CM1 20U.

WW 310 for further details

TV sweep generator

A high frequency-setting accuracy of better than 1.0% combined with a broad frequency range extending from 3-860MHz is provided by the PM5334 Philips TV sweep generator from Pye Unicam Ltd of Cambridge. Featuring eight front-panel selected sweep ranges that employ individual oscillators, the PM5334 covers all the frequencies needed for TV-set i.f. chroma and sound alignment, those for similar f.m.-receiver i.fs and TV bands I, III, IV and V, and f.m. band II. Fixed frequency markers are employed at important frequencies (5.5, 10.7 and 38.9MHz) and a variable one is available for use on any of the ranges.

The instrument also provides a continuously adjustable sweep width on each range with an additional control permitting the selected frequency width to be centred on the range scale. A further facility permits the sweep frequency to be adjusted in the range 8-50Hz.

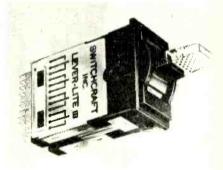
The output on the PM5334 is stabilized and can be adjusted 80dB down from a maximum of 200mV, with the additional possibility of modulating this output with a 1kHz signal. It is also possible for signals to be provided at this output which represent any of the fixed marker frequencies \pm the variable-marker frequency (modulated or unmodulated), and a further output provides just the fixed marker frequencies as carrier signals.

A further feature of this instrument is its built-in bias-voltage source (0-30V floating) which eliminates the need for a separate supply for this purpose in radio or television (both monochrome and colour) alignment work. It basically means that only the PM 5334 and a dual-trace oscilloscope, such as Philips PM3110, are needed for complete alignment of, for example, TV-set i.f. and subcarrier stages.

A front-panel colour-coding system is provided which associates a given function with its specified operation of the instrument. Pye Unicam Ltd., Cambridge. WW 311 for further details

Illuminated lever switch

The Lever Lite III, from Souriau, is a part of the Switchcraft range of illuminated switches. It is available with three switching functions with alternatives up to eight pole double throw switching and giving a different colour of lever in each position.



Non-locking and locking (momentary) types are available. The contact springs are silver plated phosphor bronze with precious metal contact and the housing and lever of moulded plastic. Souriau (U.K.) Ltd, Shirley Avenue, Vale Road, Windsor, Berkshire.

WW 312 for further details

Desoldering braid

The use of pure copper desoldering braid is accepted as an easy and effective aid to the desoldering of electronic components. But there has always been a severe disadvantage to its use because previously available desoldering braids usually contain a highly corrosive flux which is activated when used with a soldering

instrument. A new desoldering braid available from GDS Sales Ltd, does not contain a corrosive flux. Instead, a new formula flux is used which is based on resin and organic compounds. Adcola desoldering braid is available from GDS in three sizes: AA (1.5×0.4 mm); AB (1.7×0.7 mm); BB (2.8×0.7 mm). Each type costs £6 per box of ten spools. GDS (Sales) Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Bucks. WW 307 for further details

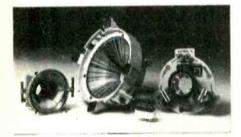
110° deflection yokes

A range of colour TV deflection vokes has been announced by General Instrument Europe. It includes the type XP7311, XP731213 and 19194 Series assembly for use with 67mm colour picture tube type A67-150X.

Facilities for rotating the yoke within the housing are provided for picture souaring. A decuate axial movement for the yoke is provided for "red balling" prior to clamping the yoke in its optimum position for good beam landing.

The auto wound toroidal horizontal and vertical windings are laid into grooves formed in the plastic end caps mounted on the front and rear ends, of the ferrite voke core. This precision turns placement ensures good and consistent convergence standards comparable to those currently being obtained on 90° receivers using conventional saddle coils.

The plastic housings are moulded from self extinguishing material conforming to at least U.L. SE1 standards, whilst the terminal panels are of flame retardant s.r.b.p. material.



With the deflection vokes, G.I. has announced a radial convergence/purity panel designed for mounting on the rear of the 110° PST deflection yoke type XP 7311 etc. The coil assemblies contain windings for dynamic horizontal and vertical convergence control together with additional windings for electro-magnetic static shift. These assemblies are mounted on a flame retardant etched copper clad phenolic laminated panel conforming to BS 3888 (PPCD), DIN 40802 (C) and NEMA L1-1-1971 (FR2). A self extinguishing plastic mount to UL SE1 standards secures the purity magnets. The convergence assembly can be supplied with or without the integral purity correction magnets. Where dynamic blue width correction is not required, use of the G.I. blue lateral/purity device type 19194-1 is recommended. This last device is mainly constructed in plastic material conforming

Auto ranging multimeter

Keithley Instruments have introduced a $3\frac{1}{2}$ digit autoranging multimeter using l.e.d. display. The Model 165 has autorange and automatic polarity switching facilities; manual ranging is also provided for all functions.

As a d.c. voltmeter, the Model 165 covers measurements from 10V to 1000V with six full-scale ranges. Most d.c. voltage ranges offer +0.1% reading accuracy plus a nominal digitization error. On the six a.c. voltage ranges, the 165 permits measurements over a frequency range of 20Hz to 20kHz with specified mid-band accuracies of 0.7% to 0.9%. Useful measurements may be made beyond these limits from 10Hz to 100kHz.

The a.c. current ranges cover five decades from 100nA resolution to 2A, with the same frequency range as a.c. voltage. The d.c. current ranges span seven full-scale decades, with overall sensitivity of 1nA to 2A. Full range voltage drop is only 10mV on all except the 1A range where it is 100mV. Resistance ranges also cover seven decades, with 0.1Ω to 200M Ω sensitivity. Keithley Instruments Ltd, 1 Boulton Road, Reading, Berks. WW 306 for further details



to UL SE1 standards. A plastic knob moves two sliding plates, containing fixed magnets, in opposite directions to control the lateral movements of the blue and rcd/green beams. The purity magnet rings are mounted at the rear of the main assembly. General Instrument Europe S.p.A. 20149 Milano P.22a Amendola 9. WW 301 further details

Panel mounting potentiometers

The T162P6 is a cermet 4-in rectilinear potentiometer. It is fitted with an adapter manufactured from Delrin 500 and is bolted to the front panel giving accessibility to the screwhead for easier adjustment. Compared to a plain hole this mounting provides positive screwdriver location, a dust sealed panel and a much neater appearance. Other advantages of this product are said to be the high strength of the component to adapter joint with a push out minimum of 10-lbf, and an anti-rotation threaded bush, with washer and nut which locks the component firmly to the panel. The dimensions of the basic potentiometer are increased by a minimal amount, the remainder of the specification being the same as for the basic potentiometer type T162P. Also available are the T62P6, 3-in rectilinear and the T72P6, 1-in rectilinear potentiometers with wirewound elements. Electrosil Ltd, Pallion Works, Sunderland, Co. Durham.

WW 305 for further details

Variable-phase generator

A low-frequency limit of 0.1Hz is provided in the latest addition to Philips range of l.f. equipment, available from Pye Unicam Ltd of Cambridge. Known as the PM5161, this 0.1Hz to 1MHz variable-phase generator also has low signal distortion, this being typically 0.06% between 100Hz and 50kHz.

It is intended primarily for use as a sine-wave signal source in analogue-type simulator systems, such as those employed in process control and biomedical work, and also in audio and stereo work. An important feature is its dual-output system that permits the first output to be employed as the reference for the second so that a defined phase relationship can be maintained between the two. This phase difference can be adjusted in 30° steps up to 360°, and continuous phase adjustment is possible over the range of each step.

Apart from this, the PM5161 has two outputs, one with a 50 Ω impedance and the other with a 600 Ω one, and both can provide a 10V_{eff} output signal unloaded. The unit's outputs are short-circuit proof and each output can be attenuated using the 0/20/40dB attenuation control.

Among its other characteristics the PM5161 has a stability of better than 550 p.p.m./24hrs long-term and better than 100 p.p.m./15mins short term. Its phase error is less than 3.5° up to 100kHz and 7° to 1MHz, and frequency accuracy better than 3% to 100kHz and 5% to 1MHz. Pye Unicam Ltd, Cambridge. WW 303 for further details



WW-094 FOR FURTHER DETAILS

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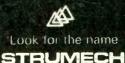
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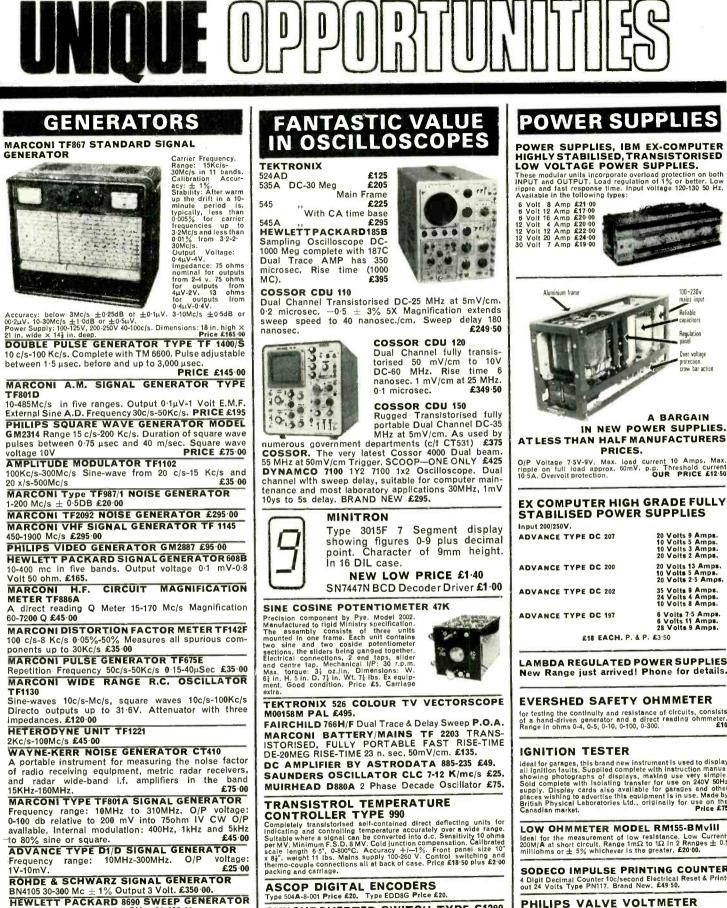
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Max, 300mV, 1000Hz-30MHz.

PRICE £30.0

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ASCOP DIGITAL ENCODERS Type 504A-8-001 Price £20. Type EDD8G Price £20.

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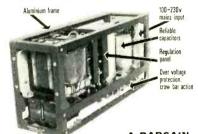
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20 Volts 9 Amps. 10 Volts 5 Amps. 10 Volts 3 Amps. 20 Volts 2 Amps. 20 Volts 13 Amps. 10 Volts 5 Amps. 20 Volts 2.5 Amps. 35 Volts 9 Amps. 24 Volts 4 Amps. 10 Volts 8 Amps. 6 Volts 7-5 Amps 6 Volts 11 Amps. 28 Volts 9 Amps.

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for testing the continuity and resistance of circuits, consists of a hand-driven generator and a direct reading ohmmeter. Range in ohms 0-4, 0-5, 0-10, 0-100, 0-300.

ideal for parages, this brand new instrument is used to display all ignition faults. Supplied complete with instruction manua showing photographs of displays, making use very simple Sold complete with isolating transfer for use on 240V 50Hz supply. Display cards also available for parages and other places wishing to advertise this equipment is in use. Made by British Physical Laboratories Ltd., originally for use on the Canadian market.

LOW OHMMETER MODEL RM155-BMvill Ideal for the measurement of low resistance. Low Current 200M/A at short circuit. Range $1m\Omega$ to 1Ω in 2 Ranges \pm 0.5 milliohms or \pm 5% whichever is the greater. **£20:00**.

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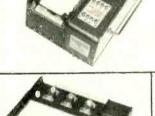




MINIATURE PEN RECORDER

MINIAIUKE PEN ALLUNUEN Provides permanent record of DC currents up to 1mA. Eminently suitable for use where space is limited. Separate time marker pen provided. Chart width 80mm Chart length 40ft. Chart speeds: Slow 20-60-180 mm/hour. Fast 600-1800-5400 mm/hour. Fast 600-120x285mm. Weight 7.7 lbs. (3.5 Kg). Price complete with accessories

£39.00



SINGLE CHANNEL HIGH SPEED RECORDER

Chart length 175ft, Footage indicator. Width of recording channel 80mm. Chart speeds (selected by push buttons) 1.2-6-12-30-60-120-300-60m per minute. Full deflection current 8mA. per minute. Fuil deflection current office. Internal impedance 210 ohms. External impedance 800 ohms. Dimensions 320x340x175mm. Weight 35 lbs. Price complete with accessories





EVENT RECORDER

Designed fo EVENT RECORDER Designed for recording sequences of up to ten different operations, e.g. sequence of machine tool operation, switching sequences, etc. Record is presented in the form of square "pulses". When energised, pen moves by approxi-mately 4mm, to the right of zero line. Response time 100 milliseconds. Chart width 110mm. Chart length 50/h. Inv. capacity 72 hours. Chart speeds 20:60-180-600-1800-5400 mm/hour. Size 160:160x255mm. Weight 9 lbs. n auences of Size 160x160x255mm, vvery Price complete with accessories 160x160x255mm, Weight 9 lbs





PORTABLE AC/DC RECORDING VOLTAMMETER Fitted with separate zero-marking pen-Accuracy 1.5% DC, 2.5% AC. Measure-ments ranges — AC and DC: 5-15-150-250-500mA 1.5-5 Amps 5-15-50-150-250-500/M 1.5-5 Amps 5-15-50-150-250-500/ DC only 150mV. Frequency range 45 to 1000 c/s. Chart width 100mm. Chart speeds 20-60-180-60 1800-5400 mm/hour. Weight 22 lbs. Price complete with accessories

£78.00



THREE CHANNEL HIGH SPEED RECORDER

Strip Chart Recorder, Chart length 175ft Footage Indicator Width of recording channel 80mm. Chart speeds (selected by pushbuttons) 1.2-12-30.60-120-300-600-3000 mm, per minute. Full deflection current 8mA. Internal impe-dance 210 ohms. External impedancer 800 ohms. Dimensions 510x345x175 mm. Weight 44 lbs. Price complete with accessories

£90.00



4-RANGE GENERAL PURPOSE TEMPERATURE RECORDER Type 01

Specially designed compact self-contained instrument for recording temperatures up to 500°C. The main design objectives were for an easy-to-use, robust instrument suitable for use in the laboratory and in the field. The four ranges are 10°C, 50°C, 100°C and 500°C. These are selected by push buttons allowing full use of the 3" wide chart. Two chart speeds 1" and 6" per hour are provided by the 240V 50Hz synchronous chart drive.

£95.00 plus £5.00 packing and carriage



ully transistorised for measurement or Fully transistorised for measurement of overall distortion of signals with frequencies between 10 Hz and 1 MHz. Built-in electronic votimeter can also be used separately for measuring AC voltage: basic noise, gain or attenua-tion over a wide frequency range.

 Millivoltmeter:
 Iess than 0.3% (50 Hz . . . 30 KHz).

 Voltage range (in 12 ranges): from 1 mv
 Squarewave output:--

 to 300 V f.s d. Level range (ret to 0 776
 Frequency range (in 4 ranges): from 10 V): from + 52 d8 to - 75 dB. Frequency range (from 10 Hz to 2 MHz 8andwidth within 3 d8): up to 8 MHz Accuracy: 75 Ohm constant. Risetime: less than 10 Vp. Output impedance:

 within 3 d8): up to 8 MHz Accuracy: 75 Ohm constant. Risetime: less than 5%. Input impedance: 2
 10n S.

 Mohm: 50 pF approx
 £249.00

 £249.00

M.FM

GENERATOR

Type AF 1065

£225.00

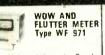


Transistorised generator providing wide range of squarewave and sinewave signals. Suitable for measuring distortion, gain or attenuation when testing the frequency response of low-frequency

RCL BRIDGE

Type P 966

2101 -1 2 3 a.



Solid state, high stability unit. Can be preset for either the European standard at 3150 Hz or the American standard at 3000 Hz. Provided with built-in 3000

3000 Hz. Provided with bullt-in oscillator. Specifications: DIN and CCIR. Input Signal: 20 mV rms to 20 V rms approx. Frequencies (switchable): 3150 Hz and 3000 Hz. Ranges (flutter): $\pm/-$ 0.1% $\pm/-$ 0.3% $\pm/-$ 1% f.s.d. Drift indication: $\pm/-$ 2% max. Input impedence: 10mOhm max. Built-in oscillator: 3000 Hz or 3150 Hz switchable. Stability: better than 0.1% Shifts for calibration: $\pm/-$ 0.1% dynamic, 50 Hz \pm 2% static calibration: + 2% static.

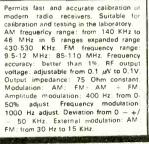
£225.00



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Suitable for alignment of tuned circults in television sets. Incorporates a sweep generator, a market generator and a crystal-controlled oscillator operating at 5.5 MHz. Sweep frequency range 1-30 MHz, 170-260 MHz Fund. 470-780 MHz Harmonic. Marker frequency range once MH 480-800 MHz 2-266 MHz. 480-800 MHz

£195.00



Permits fast and accurate calibration of

Resistance: from 0.1 Ohm to 11 MOhm. Capacitance: from 1 pF to 1100 µF. Inductance: from 10 µH to 1100 µF. Accuracy: +/- 1%. Dissipation factor D: from 1.10.³ to 50. Quality factor Q: from 0.02 to 1000. Internal oscillator: 1 KHz.



Designed for for use in one hand, the 690 ammeter makes use

Designed for use in one hand, the Ampertest 690 ammeter makes use of the familiar clamp or 'pincer' system to measure without breaking the circuit the current flowing in a conductor. It has six current ranges from 3 A to 600 A f.s.d., with the first division at 100 mA. The ranges can be extended by means of a 10-to-1 current transformer that is subnied with the instrument. means of a 10-to-1 current transformer that is supplied with the instrument, providing ranges from 300 mA to 60 A f.s.d. with the first division at 10 mA. Two a.c. voltage ranges of 250 V and 600 V f.s.d. are provided. The con-nections for voltage measurements are made by means of two leads and probes that plug into the base of the instrument. instrument

range -10 to -12 dB. Accuracy (% of F.S.D.):—DC and resistance measurements +2.5. Price with test leads, and £39.50 inc. leather case

Specification Specification Measurement ranges: — Current 10-25-100-250-500 Amps. Volt-age 300, 600 V. Accuracy 4%. Scale length 60mm. Overall dimensions 283 x 94 x 36mm. Weight 1.5 lbs.

£10.50

MULTIMETER

MULLINTELER 0.1-1-10-1000mA. 2.5-10-20-250-500-1000V AC/ DC. Sensitivity AC and DC all ranges except 10V-10.000 Ohm/V. Dimensions 212 x 118 x 75mm Weight 2.9 lbs. Price complete with steel carrying crease and text leads. case and test leads

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AC/DC MULTIMETER taut band suspension movement. Sensitivity 20,000 ohms per volt on DC

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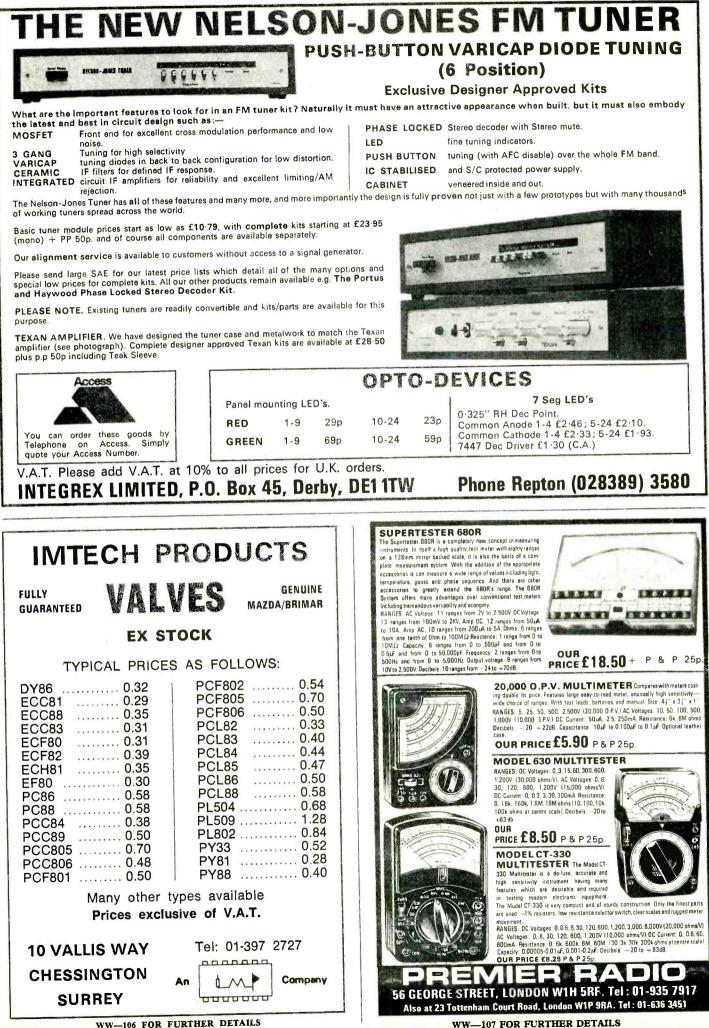
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		N VO	LTAGE TRA	D/OR 24 VOLT RAN	GE
Ref. No.	Amps. 12V 24V	lb oz	Size cm.	Secondary Windings	P&P
111 213 71	0.5 0.25 1.0 0.5 2 1	1 4	4·8× 2·9× 3·5 6·1× 5·8× 4·8	0-12V at 0-25A × 2 0-12V at 0-5A × 2	€ p 1.02 22 1.22 22
18	4 2 6 3	1 12 2 12 3 8	7.0× 6.4× 6.1 8.3× 7.7× 7.0 8.9× 8.0× 7.7	0-12V at 1A × 2 0-12V at 2A × 2 0-12V at 3A × 2	1.60 22 2.24 36
108	8 4 10 5	5864	9·9× 8 9× 8·6 9·9× 9·6× 8·6	0-12V at 3A × 2 0-12V at 4A × 2 0-12V at 5A × 2	2 70 42 3 00 52 3 55 52
116 17	12 6 16 8	6 12 8 12	9·9×10·2×8·6 12·1× 9 9×10·2	0-12V at 5A×2 0-12V at 8A×2	4·30 52 5·48 52
115 187	20 10 30 15	18 8 15 8	14.0× 9.6×11.8 14.0×12.1×11.8	0-12V at 10A × 2 0-12V at 15A × 2	6-89 67 12-90 82
226	60 30	32 0	17·2×15·3×14·0 30		23.72 *
Ref No. 112	Amps. 0.5	Weight Ib oz 1 4	Size cm. 6·1× 5-8× 4·8	Secondary Taps	₽&₽ € p 1·22 22
79	1.0	2 4 3 4	7.0×6.7×6.1 8.9×7.7×7.7	0-12-15-20-24-30∨	1.62 36
20 21	3·0 4·0	4 8 6 4	9·9× 8·3× 8·6 9·9× 9·6× 8·6	88 88 88 88 88 88	2·43 36 2·99 42 3·55 52
51 117	5·0 6·0	6 12 8 0	12.1 × 8.6 × 10.2 12.1 × 9.3 × 10.2	11 D	4·42 52 5·28 52
88 89	8.0 10.0	12 0 13 12	12·1×11·3×10·2 14·0×10·2×11·8	23 23, 27 24	6·82 67 8·36 67
Ref. No.	Amps.	Weight	Size cm.	50 VOLT RANGE Secondary Taps	P&P
102	0.5	1 12 2 12	7·0× 6·4× 6·1 8·3× 7·4× 7·0	0-19-25-33-40-50V	£ p 1.60 30
104	2.0	5 8 6 12	9·9× 8·9× 8·6 9·9×10·2× 8·6	11 12	2·34 36 3·25 42
106	4-0 6-0	10 0 12 0	$12.1 \times 10.5 \times 10.2$	11 11 11 11	4·41 52 5·84 52 8·63 67
118 119	8·0 10·0	18 0 25 0	14.0×10.2×11.8 14.0×12.7×11.8 17.2×12.7×14.0	77 FF	11·27 97 14·13 *
Ref. No.	Amps.	Weight Ib oz	Size cm.	80 VOLT RANGE	₽& ₽ £ ₽
124 126 127	0.5	2 4 3 4	7.0× 6.7× 6.1 8.9× 7.7× 7.7	0-24-30-40-48-60V	1-62 36 2-26 36
125	2·0 3·0 4·0	6 4 8 12 13 12	9.9×9.6×8.6 12.1×9.5×10.2	11 11	3·55 42 5·41 52
40	5-0	12 00 15 8	12.1×11.8×10.2 14.0×10.2×11.8 14.0×12.1×11.8	12 12	6 98 67 8 22 67 10 12 82
121	8-0	25 00 25 0	14.0×14.7×11.8 17.2×12.7×14.0	FF FF	10·12 82 11·40 • 16·75 •
189		29 00	17-2×14-0×14-0 E TRANSFORMER	S WITH SCREENS	18.75 *
Ref. No.	Amps.	Weight Ib oz	Size cm.	VOLTS	₽ ≜ P € p
238	200 1A 1A	1 4	2·8×2·6×2·0 6·1×5·8×4·8	3-0-3 0-6 0-6	1·10 10 1·27 22
13 235 207	100 330, 330	4 4	3.9×2.6×2.9 4.8×2.9×3.5	9-0-9 0-9, 0-9	64 10 1·27 10
208 236	500, 500 1A, 1A 200, 200	1 00 1 12 4	6·1×5·4×4·8 7·0×6·4×6·1 4·8×2·9×3·5	0-8-9, 0-8-9 0-8-9, 0-8-9 0-15, 0-15	1.70 22 2.28 30 1.27 10
214 221	300, 300 700 (D,C	1 4 .) 1 8	61×58×48 70×61×61	0-20, 0-20 20-12-0-12-20	1 34 22 1 20 30
206 203	1A, 1A 500, 500	2 12 2 4	8·3×7·7×7·0 8·3×7·0×7·0 8·9×7·7×7·7	0-15-20, 0-15-20 0-15-27, 0-15-27 0-15-27, 0-15-27	3 08 38 2 36 38
204	1A, 1A	3 4 B/	ATTERY CHARGE	RTYPES	2.39 38
PRIMA Ref. No.	RY 200-250 Amps.	Weight	(Secondary 2V, 6V Size cm.	, 12V)	P&P
45	1·5 4·0	1 0Z 1 8 3 4	7.0× 6.1× 6.1 8.9× 7.7× 7.7	Please note these	£ p 1.61 30
86 146	6·0 8·0	6 4 6 12	9.9× 9.6× 8.6 9.9×10.2× 8.6	Please note, these units do not In- clude rectifiers	2·45 42 3·70 52 4·22 52
50	12.5	12 0	14·0×10·2×11·8 /	clude rectifiers n: open with solder tags	6.29 67
impregn	ation.				
Also	stocke	d d	SEMICONDU		
	VOM				
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PLE	ASE A	DD 1	0% FOR V.A	.T. including F	P. & P.
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20		11		ctron	Tee
			IEC IO	NDON EC:	3N 1R.
	E MI	NOR	$LO_1 LOI$		
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,TH	TELE	EPH	ONE: 01-	488 3316	/8
,TH	TELE	EPH	ONE: 01-		/8
,TH	TELE	EPH	ONE: 01-	488 3316	/8
,TH	TELE St tue	EPH BE STA	ONE: 01-	488 3316 Gate & Liverp	/8
,TH	TELE St tue	EPH BE STA	ONE: 01-	488 3316 Gate & Liverp	/8
,TH	TELE ST TUE WV	EPH BE STA	ONE: 01-	488 3316 Gate & Liverp	/8

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WW-115 FOR FURTHER DETAILS

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The GNT Range of Automatic Morse Equipment is now manufactured in the U.K. and comprises complete equipment for Morse Training Schools and for Automatic Morse Transmission. Models available include :

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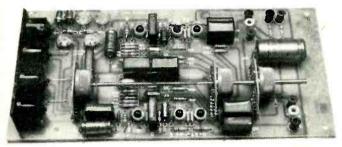
WW-116 FOR FURTHER DETAILS



Wireless World, November 1973

HART ELECTRONICS

Audio Kits



This is our Bailey/Burrows Stereo pre-amp front end. We think it is the best engineered kit of the best pre-amp circuit available, and there is a back end/tone-control unit of similar advanced design to go with it which is only $1\frac{1}{2}$ " deep so it fits almost anywhere, but of course it's at its best in a Hart universal amplifier metalwork with a couple of Hart Bailey 30 watt power amps to keep it company. That's a recipe for real Hi-Fi with electronics you'll be too proud to cover up.

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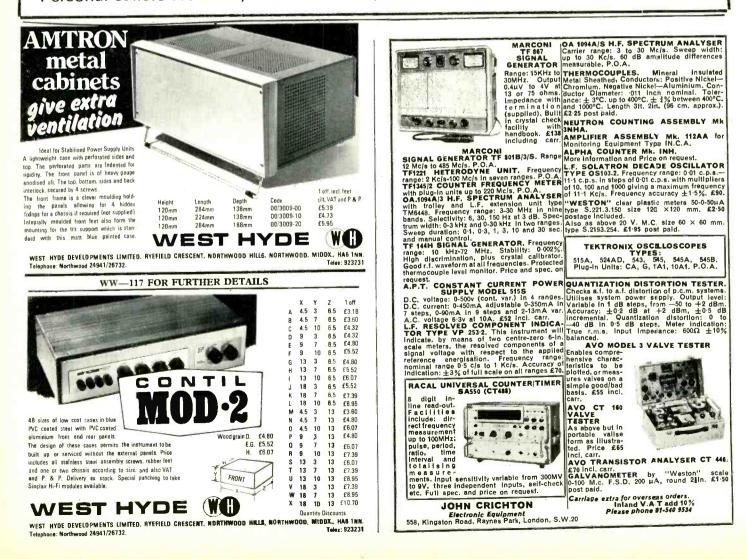
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Wireless World, November 1973





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Pack	I.	Price
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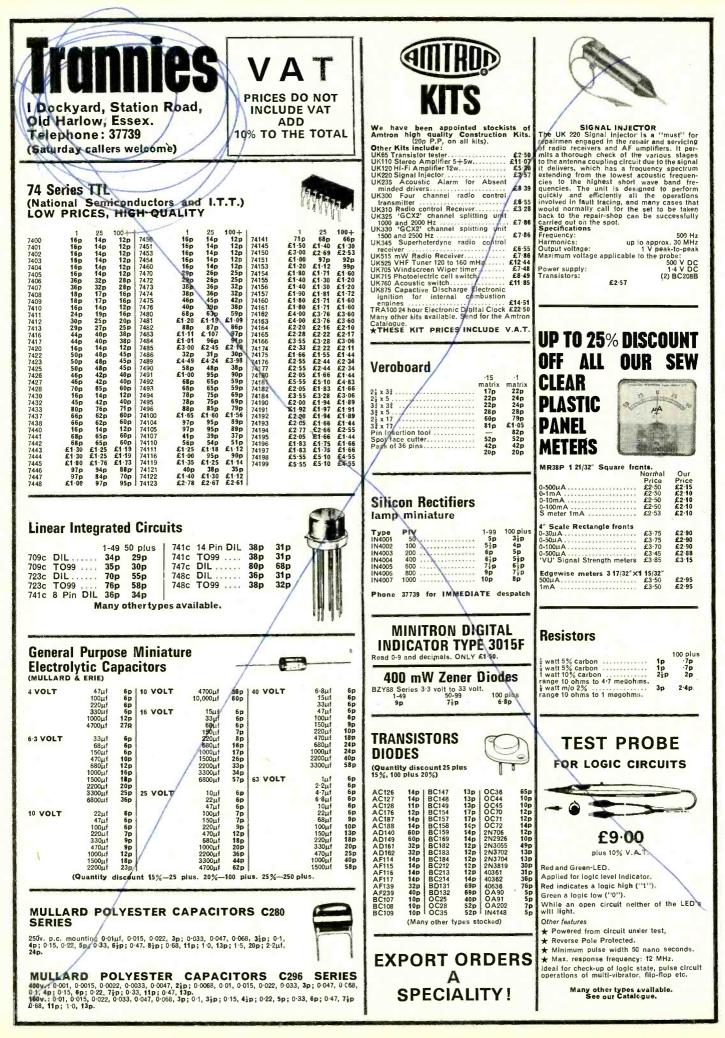
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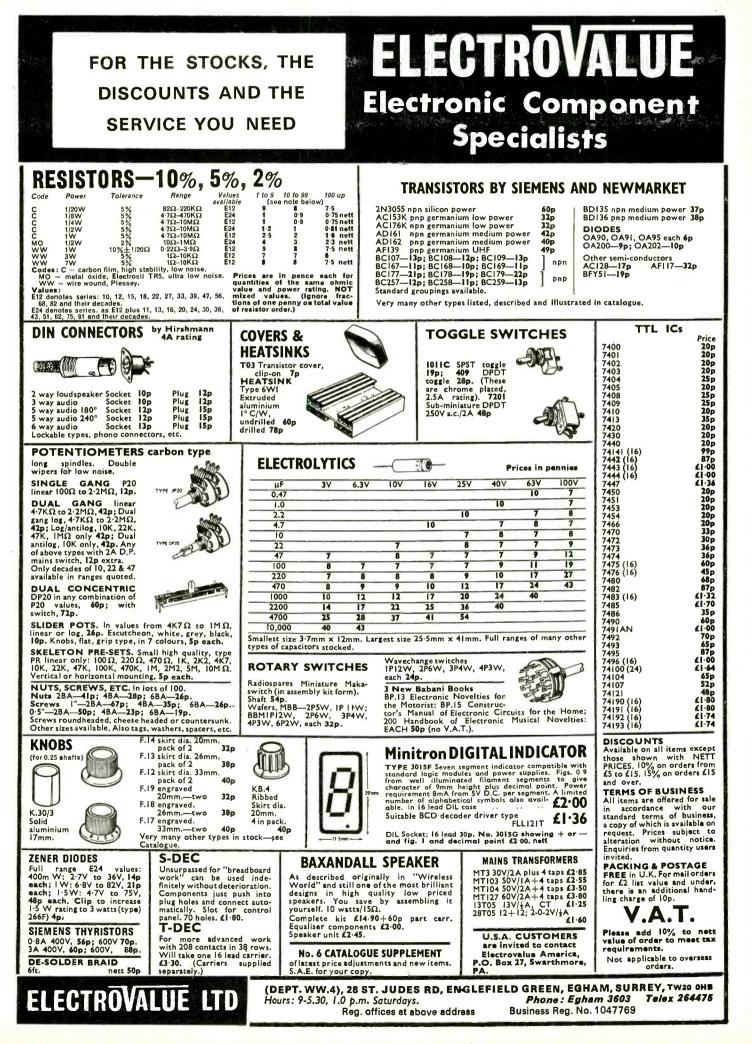
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Wireless World, November 1973





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0.32 EF40 0.45 EF41 0.40 EF83 0.29 EF85 0.28 EF86 0.30 EF89 1.08 EF91 0.37 EF92 0.90 EF95 1.08 EF183	0.62 0.25 0.60 0.31 0.27 0.25 0.27 0.25 0.31 0.31 0.26	PCF200 PCF201 PCF801 PCF802 PCF805 PCF806 PCF808 PCF808 PCH200 PCL81	0.80 0.60 0.44 0.45 0.80 0.85 0.85 0.65 0.65 0.50 0.30	U191 U301 UABC80 UAF42 UBC41 SPECIA O9J T	0.68 0.70 0.30 0.50 0.48	UL41 UL84 UU5 UY41 UY85 VR105/30	0.60 0.85 0.65 0.45 0.35 0.35	2K25 3A4 3D6 3Q4 384 3V4	7.50 0.40 0.15 0.55 0.33 0.48	6AH6 6AK5 6AK8 6AL5 6AL5W 6AM6 6AN8	0.50 0.35 0.80 0.18 0.35 0.35 0.35 0.60	6BG6G 6BJ6 6BQ7A 6BR7 6BW6 9BW7	0·47 0·45 0·43 1·09 0·80 0·80	6J5GT 6J6 6J7G 6J7M 6K6GT 6K7	0-80 0-25 0-80 0-85 0-55 0-40	68L7GT 68N7GT 68Q7 68Q7GT 6V6G 6V6G 6V6GT 6X4 6X5G 6X5GT	0.35 0.35 0.45 0.80 0.15 0.85 0.33 0.25 0.35	30C15 30C17 30C18 30F5 30FL1 30FL12 30FL14 30L15 30L17	£ 0.70 0.85 0.75 0.80 0.70 0.95 0.80 0.80 0.80	6057 6060 6064 6065 6080 6148 8020 9001 9001	£ 0.55 0.50 0.45 0.65 1.55 1.75 8.75 0.15 0.40
1 08 EF184 0 27 EF1201 0 46 EL34 0 20 EL41 0 45 EL84 0 50 EL85 0 27 EL86 0 36 EL90 0 40 EL95 0 27 EL500 0 27 EL504	0.31		0 60 0 35 0 40 0 43 0 60 0 50 0 40 0 35 0 36 0 36 0 30 0 62	P 4 OA5 OA10 OA70 OA71 OA73 OA74 OA79	2 0.20 0.25 0.10 0.10 0.07 0.07		5 0·12 0·20 0·30 0·25 0·25 0·20 0·20	1N702-72 1N823A 1N4785 1ZMT5 1ZMT10 1ZT5 1ZT10	£	3N139 3N140 3N154 3N159 6FR5 12FR60 40954	\$ 1.75 0.97 0.95 1.45 0.45 0.73 1.25	ASY67 BAW19 BC107 BC108 BC113 BC118 BCY72	\$ 0-48 0-28 0-10 0-10 0-10 0-20 0-15	CR83/40 C82A CV102 GET103 GET115 GET116 GEX66	\$ 0.50 0.65 0.25 0.23 0.45 0.50 1.50	6¥6G 6-30L2 6Z4 7B7 7¥4 9D6 11E2 12AT6 12AT7	0.35 0.40 0.50 0.60 0.30 3.70 0.35 0.35	30P12 30P19 30PL1 30OL13 30PL14 35L6GT 35W4 36Z4GT 50C5	0.75 0.70 0.90 0.85 0.50 0.30 0.55 0.45	9003 9004 9006 C.R. Tube VCR97 VOR517F VCR517C 88D 88J	0.45 0.12 0.12 4.00 1.5.00
0.25 EM31 0.25 EM80 0.27 EM84 0.36 EM87 0.80 EY51 0.39 EY86 0.39 EY88 0.31 EZ41 0.31 EZ80	0.22 0.36 0.31 0.63 0.36 0.40 0.40 0.40 0.40 0.45 0.22	PL504 PL508 PL509 PL802 PX4 PY33 PY80 PY81 PY82	0.62 0.70 1.05 0.88 2.50 0.55 0.35 0.35 0.30	(6D15) OA81 OA91 OA200 OA202 OA2200 OAZ201 OC22 OC25	0.08 0.07 0.07 0.10 0.55 0.50 0.50 0.50 0.40	OC81DM OC82 OC82DM OC83B OC83B OC84 OC122 OC139 OC140 OC170 OC171	0.20 0.25 0.30 0.25 0.15 0.25 0.50 0.25 0.40 0.25 0.30	2G385 2G403 2N918 2N1304 2N1306 2N1307 2N2147 2N2411 2N2904A \$\mathbf{p}2N2989 2N3053	0.51 0.51 0.22 0.25 0.25 0.64 1.50 0.25 4.00 0.25	40595 40636 40668 40669 AC126 AC127 AC128 AC176 ACY17 ACY18 AD149	1.25 1.25 1.25 1.40 0.25 0.25 0.20 0.20 0.20 0.25 0.17 0.50	BF115 BF173 BFY51 BFY52 BS BS2 BSY29 BU100 BYZ13 BYZ16 CRS1/10	0.25 0.20 0.20 0.45 0.45 0.47 0.25 1.80 0.25 0.63 0.25	NKT222 NKT304 RAS310AJ SD918 SD928 SD928 SD94 SD988 V405A Z2A51CF	0.20 0.50 F 0.33 0.26 0.31 0.32 0.21 0.46 0.40 0.78	12A17 12AU7 12AV6 12AX7 12BA6 12BE6 12BH7 12C8 12E1 12K5	0.24 0.40 0.25 0.25 0.35 0.35 0.23 0.30 2.85	50CD6G 50EH5 75 76 78 80 723A/B 803 803 805	1.10 0.55 0.50 0.55 0.50 0.55 7.00 5.50 12.00	88L Photo Tu CMG25 931A 6097C Special Vi	8-10 bes 2-50 4-75 16-00
0-67 EZ81 0-56 GZ34 0-25 KT86 0-40 KT88 0-40 N78 0-40 OA2	0:24 0:52 0:63 2:30 2:25 1:60 0:38 RANS	PY83 PY88 PY800 PY801 QQVO 3-10	0.85 0.32 0.35 0.45 1.10	OC26 OC28 OC29 OC35 OC36 OC38 OC44 OC45 OC70	0.25 0.60 0.60 0.50 0.56 0.42 0.17 0.12 0.12	OC172 OC200 OC201 OC206 IN21B IN25 IN43 IN70 IN677	0.37 0.40 0.75 0.95 0.30 0.60 0.10 0.07 0.12	2N3054 2N3055 2N3730 2N3731 2N4172 82303 3F100 3FR5 3N128	0.50 0.64 0.50 2.75 0.50 0.50 0.62 0.32 0.87	AD161 AD162 AF118 AF127 AF139 AF178 AF186 ASY26 ASY28	0-35 0-35 0-50 0-20 0-30 0-48 0-48 0-40 0-25 0-25	CR81/20 OR81/30 CR81/35 OR81/40 OR83/05 OR83/20 OR83/30 CR825/02	0-38 0-40 0-43 0-48 0-30 0-38 0-38 0-48 0-48 5 0-55	ZR11 ZR21 ZR22 ZENER DIODES All prefe voltag	0.33 0.46 0.42	12K5 12K7GT 12K8GT 12Q7GT 128G7 1487 19AQ5 19G8	0.95 0.45 0.40 0.40 0.40 0.40 0.70 0.40 5.75 5.75	807 813 832A 866A 931A 954 955 956 957	0 50 4 00 2 70 1 25 4 75 0 35 0 35 0 30 0 35	JP9/7D K301 K305 K308 K337 KRN2A WL417A 3J/92/E	35.00 4.50 11.00 14.50 14.50 8.15 1.35 35.00
hone enqui	ries fo etall 7	r valves, 43 4946;			and and	COTHERS ecial valves. for each ad	πĸ	POSTAGI	C QUAT I	ES free. DD	107 07	is value		1W 1·5W 7W	0.87 0.25 0.40	19H4 20P4 25L6GT	5.25 1.00 0.50	991 2051 5933	0.40 0.70 1.00	5C22 714AY 725A	22.00 8.60 22.50

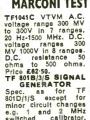


TF 1400S DOUBLE PULSE GENERATOR WITH TM 6600/S SECONDARY PULSE UNIT. For testing radar, nucleonics, 'scopes, counters, filters elc. SPEC. TF 1400S. Rec. frequ. 10Hz to 100 kHz, pulse width 0'1 to 100µ sec., delsy -15 to +3000µ sec., fras time < 30N sec. SPEC. TM 6600/S. As for TF1400S except pulse width 0'5 to 25µ sec, delay 0 to + 300µ sec. £230.



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MARCONI TEST EQUIPMENT

e.g. 1 and 2 Mi switched calibrate P.O.A.

TF 801D/1/S SIGNAL GENERATOR. Range 10-485 MHz in five ranges. R.F. Output 0-1 W-1V Source e.m.f. Dial calibrated in volts, decibels and power relative to thermal noise. Piston type attenuator. SoGa output impedance. Internai modulation at 1 kHz at up to 90% depth, also external sine and pulse modulation. Bullt-in 5MHz crystal calibrator. Separate R.F. and mod. meters. P.O.A. TF \$52B13 Openillation

TF 562B/3 Oscillator and Detector Unit. TF 1226B | TF 1226B | TF 1226A } White Noise Test Set. TM 577A |

TM 577A [TF 1258 VHF SPECTRUM ANALYSER for analysis and measurement of Radar Equipment. Frequency range 190 to 230MHz with crystal check points. Sweep width 0.5 to 5MHz, output pulse delay (a) 85-175 LiSec, (b) 0.7-1.4 mSec with x1 and x2 multiplier and -2, x1, x2 multiplier. Output 2µV to 20mV with x10 multiplier. £200.

Ind -2, x1, x2 multiplier. Cutput 24/V Ti SmV with x10 multiplier. £200. HEWLETT--PACKARD ISSA 800 WITH ISSA DUAL TRACE PLUG-IN. Full spec. and P.O.A. S248 COUNTER FREQUENCY MEASUREMENT: 10/Hz to 10/10/Hz. Accuracy 1 count. Only for the seconds, moling of dollar, count. Period mea-suirgimento 4/10/Hz, reads in seconds, molint automatically positioned. Display on 5 neon lamp decades and 2 meters. Complete with manual and following to application. S40B TRANSFER OSCILLATOR. S40B TRANSFER O

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etc. £123. **516B SHF SIGNAL GENERATOR.** Freq. range 1,75GHz-4.2GHz, Mod.: F.M., C.W. Pulse and Ext. A.M., output. 0,1uV-200mW. Price on application.

TF 894 AUDIO TESTER. Combined A.F. Generator (0-25kHz), Output meter (up to 2W. at 500, 15 and $\Omega_{\rm C}$) and valve voltmeter (0-800V.), with stepped and variable attenuators. £60.

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TYPECA1094 Freq. range: 3 to 30MHz in 9 bands. Selectivity: 6 30 and 150Hz. at 3db. Spec-trum width: 0-30kHz. Sweep Duration: 0.1, 0.3, 1, 3, 10 4 30 eecs.

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SOLARTRON DO 905 STABILISED AM-PLITUDE SIGNAL GENERATOR. Freq. range 350kHz-500MHz £70. TF 1370 R-C OSCILLATOR. SQUARE AND SINE WAYE. Freq.: Sinewave 10Hz-10MHz, squarewave: 0-73.2pp 10Hz-10HzHz. Direct output: sinewave: 0-73.2pp 10Hz-10HzHz. Altenu-squarewave: 0-73.2pp 10Hz-100kHz. Altenu-stor range. -50d8 to +10dB. Impedance: 75,100,500Ω. Price upon application.

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separate P.S.U. £150 511A - UMHZ, solid state, compact, 561A-10MHz, solid state, compact, takes the following plugs-Ins: X, Y, differential, sampling, spectrum ana-

differential, sampling, spectrum, an-lyser. PLUG-IN UNITS GA-24 MHz dual trace 50MV-20V. G-20 MHz differential 50MV-20V. D-High gain differential 10MV-50V. N 600MHz sampling 10MV-cm. R Transistor measurement. P type calibration, SB3-Delayed swasp time base. EQUIPMENT 162 wave form generator. 163 Pulse generator.

500/250W MEDIUM WAVE BROAD-CAST TRANSMITTERS. Price and details on application.

M.O. for ET 4336 TX (see description in previous issues) £8:50. P. & P. £1:50. ARSE SPARES. We hold the largest stock in U.K. Write for list. 3 PHASE AUTO TRANSFORMER, wys input 4000, wys output 241,5[230[218.5% S0C 18kVA. Made by Westinghouse of USA. Brand new in original cases £80.00 including UK transport.



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TELEPHONE TYPE "J" (Tropicalised) 10 line MAGNETO TELEPHONE SWITCHBOARD

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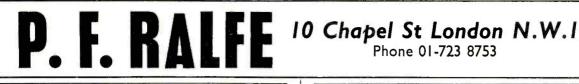
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BEST PRICES PAID FOR TEST AND COMMUNICATION EQUIPMENT, Single items or quantities. Private or Industrial. SPECTRUM ANALYSER. TYPEOA1094 Freq. 18000



TELEVISION SWEEP GENERATOR

by Sweep systems type 505. Frequency coverage 450-940MHz. (Channels 15-80). Markers at 465/ 565/660/750/830 and 900MHz. Attenuated output in eight, five db steps and fine 0-10 db. Sweep width adjustable from 1-15MHz. The instrument is completely solid-state using variator diodes and transistors throughout. Dims: $19 \times 12 \times 5$ ins. Wt.: 20lbs. Supplied in good working order, price £59.50 + 50p carriage.

AFRIAL CHANGE/OVER RELAYS

AERIAL CHANGE/OVER RELAYS of current manufacture designed espec-ially for mobile equipments, coil voltage [2v., frequency up to 250 MHz at 50 watts. Small size only, 2 in. × ¥ in. Offered brand new, boxed. Price **£1:50**, inc. P.&P.

ALCAD' Sealed rechargeable Nickel-cadmium batteries. Type W3.5, 1.2V at 3.5 Ah. Size as 'U2'. Offered new in packs supplying 12V, £15. Or separately at £1.25. Automatic Constant current electronic battery chargers specially designed for nickel cad-mium cells. Metered and fused. Up to weive cells can be charged up to tweive cells can be charged up to 750mA, variable 0-750mA, Size 7x6xSins. Brand new units. Price each £17.

Smiths Ltd Weight indicators, self powered, measures 0 to 20 cwts in 1 cwt divisions on a 4" cirscale meter indicator, 30 feet of cable and heavy duty load cell use with bell crank or actual reading is 5 cwt for F.S.D. brand new units special price £7:50 post 50p.

CossorElectronic Invertors type CRA 200. A high quality device for producing a 115V 400HZ single phase output. Incorporating the following features: Input 23-28V D.C. * Full overload protection. \$ Sing autonometry for the second seco

- Full overload protection.
 Sine wave output.
 Remote control facilities.
 Completely Solid State (Silicon transistors).
 Built to Aircraft specifications.
 I80VA of output continuous.
 May be run in series operation for 3 phase requirements. Offered brand new boxed units. Price £17:50 Carriage 50p.

AUDIO OSCILLATORS AMERICAN TS-382/U Covers 20 c/s-200 Kc/s in four ranges. Output voltage I micro volt to 10 v. in seven ranges. Built in calibrator. Sine wave O.P. is excellent over complete range. Supplied with transmit case, adaptors and circuits and transformer for 240 A.C. £20.

MINIATUREAEIUNISELECTORS 12 position × 3 bank 250 ohm coils, 1 bridging and 2 non-bridging wipers avail-able now—Type 2200A complete with bases. Price £4.

BRAND NEW DIGITAL PANEL VOLTMETERS VOLTMETERS 10MV-1-99VV. 199 Measuring points. Input impedance 100Mohm. Automatic zeroing. Measurements: 155mm × 72mm × 72mm. List price was £52-00. OUR PRICE £24-50.

DIGITAL MEASUREMENT Type 2003 Digital Voltmeter. 34 Digit display. Measuring up to 1000 Volts. display. Meas AS NEW £65.

Noise Generator Model CT-82 Range ISkHz to I60MHz very useful noise for factor measurements of receivers/wide band LF, amplifiers etc., the instrument is directly calibrated in noise factor and displayed on panel meter, also output meter calibrated in dbs, for 115-250 vac operation offered in good used condition, small size low price only £8 Carr. 50p.

H. W. SULLIVAN STANDARD AIR SPACED CONDENSERS Capaditance range 0 to 100 pf fully screened with engraved vernier sub-divided into 100 equal divisions com-plete with vernier index and original manufacturers seal offered brand new, at only £25 each.

High torque geared motors. 20RPM. 6-9V. operation. Built-in gearbox. Overall size 2ins. long by lin. diameter. Current drain at 6V only 8mA. These are precision, Swiss made geared motors. Original price was over £6 each. Our price each is only £1.50 (plus 10p each post and packing).

DIGITAL FREQUENCY

METER type 'FT300'—reads as frequency meter up to 99.99KHz in three ranges or as tachometer, 99,990 RPM. Solid-state instrument. Clear read-out. Size only 8in. by 5in. by 24in. Weight 44 lbs. BCD V. AC. Made by famous manufac-turer. These units are brand new in original makers cartons. Our price: £55.

Cossor Radio Telephones Type CC303

All Solid State except for O-P Valves 25 Watt A.M. offered brand new for high bond applications boot control console. Complete manual supply. Prices £75 each + V.A.T.

SCHOMANDL PRECISION FREQUENCY METER TYPE FDI WITH FDMI ADAPTOR GPO approved equipment for Radio Telephone Marine servicing etc., offered in as new condition with calibration certificate.

G.E.C. Uniselectors, 8-banks, 25 position full wipe. 75 ohm coil. Not new but excellent working condition. Each €2.

Brand new GEC 3 banks of 25 position uniselectors with fitted suppressor. £2.50 each.

SIX Level A.E.I. Uniselectors miniature plug in type 2216A coil 125 ohms. non-bridging wipers with index. 12 position 6 bank. Absolutely brand new in makers cartons sold complete with base. £6:50

CAMBRIDGE PORTABLE POTENTIOMETER type 44228. The ideal tool for checking thermocouples and auxiliary temperature measuring equipment. Accuracy \pm 0.1%. BRAND NEW. £75.

TINSLEY type 4363D Vernier poten-tiometer. Good condition. Price £75.

FRIGIDAIRE, AIR-CONDITIONING UNIT. Table-top model. 4 inch diameter pipe outlet. Complete and ready for use. Price £125.

WAYNE KERR type B521 Component bridge. Accurate measurement of LC & R. £55. Excellent order throughout.

TEKTRONIX OSCILLOSCOPES

Type 545A with 'CA' plug-in. (Or 'L'). DC-30MHz. Type 561A with 3A1 and 3B3 units. DC-10MHz. Type 535 with CA plug-in unit. DC-15MHz. Type 551. Double-beam with L&G units. DC-27MHz. Also available



Dynamco D7100 with IY2 and IX2 plug-ins. Portable, DC-30MHz. Hewlett-Packard 175A. 1781 and 1755A plug-ins. DC-30MHz. Marconi TF1300. s/b. DC-15MHz. £75. Roband RO50A with 5G plug-In. DC-15MHz. Price £125. Solartron CD1400. With two CX1441 and a CX1443 units.

Extremely sensitive instrument. Twin differential inputs.

TEKTRONIX type 545A OSCILLOSCOPE. Complete with 'CA' plug-in unit. As new. Perfect condition, calibrated to manufacturers standards. Bandwidth to 30MHz. This offer is too good to miss. Price only £295 (plus V.A.T.)

SIGNAL GENERATORS

Marconi type TF801D. 10-485MHz. Excellent. P.U.R. Marconi type TF867. 15KHz-30MHz. £150.



Hewlett-Packard 616A. 1780-4000MHz. £75. Advance C2H. Spot-frequency production-line test instrument. 12 freqs. in bands 500KHz-30MHz. £25.

Rohde & Schwarz U.H.F. 990-1900MHz. P.U.R.

Rohde & Schwarz SMAF. A.M. & F.M. 4-300MHz. FM Dev. 0-100KHz in 2 ranges. Fundamental-frequency generator ideal for radiotelephone test equipment. P.U.R.

MARCONI TEST EQUIPMENT. All items have been calibrated, reconditioned and guaranteed.

Wave Analyser TF455E. Frequency range 20Hz. £105.

TF893 Audio Wattmeter. Range 20Hz-35KHz. Power range 20uW-10W. Impedance 2.5Ω to 20K Ω in 48 steps. Direct calibration in Watts and dbm. Price £45.

TF2600 Sensitive Valve Voltmeter ImV f.s.d. to 300V f.s.d. Accuracy \pm 1%. Offered as new, price £55.

TFI370A Wide-range oscillator 10Hz to 10Mz. Squarewave up to 100KHz. High output—up to 1MHz 31 Volts. 75,100 or 600 Ω output. List price pre VAT—£308. Offered as new at £125.

TF2162 MF attenuator. DC-1MHz. O-111db attenuation in .1db steps. Impedance 600 ohms unbalanced. Price £50.

TF2163 U.H.F. Attenuator. DC-I GHz. 0-142db in 1db steps. Z, 50 ohms. Max. power input 0.5W. As new Price £75.

TF80ID/I A.M. Signal Generator up to 470MHz.

TFI 106 Noise Generator 1-200MHz. £75.

TF1041B Voltmeter. 300mV-300V. 20Hz-1500MHz. £45.

TF1301 Noise Gen. 200-1700MHz. 50 ohms. £55.

TF1099 20MHz Sweep Generator as new £75.

OA1094AHF Spectrum Analyser 100KHz-30MHz. As new. TFI417 Counter, Frequency Meter 7 digits. Plus range extension unit TF1434/2 to 220MHz. As new.

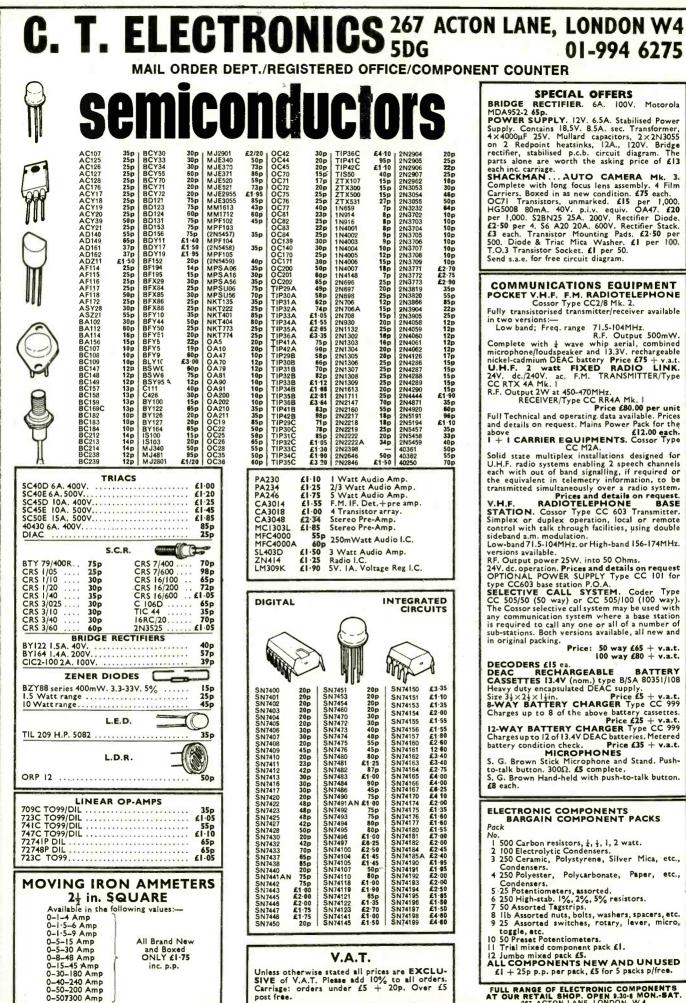
Available now-type '316' Jack-plugs, complete with leads. Good condition. Price £2 for ten.

ADVANCE AUDIO SIGNAL GENERATOR TYPE HI. 15Hz-50KHz in three ranges. Sine/square wave output. Supplied in first-class working condition. £15. Carriage £1 each.

R216 V.H.F. AM/FM Communications receivers. Coverage 19-157MHz. Film scale dial 2 frequency crystal calibrator. Plus all other facilities. Complete with A.C. power supply connecting lead. Supplied in full working order in excellent secondhand condition,

PLEASE ADD 10% V.A.T. TO THE TOTAL AMOUNT WHEN ORDERING. INCORRECT AMOUNTS WILL CAUSE DELAY IN DESPATCH. THANK YOU.

01-994 6275



SPECIAL OFFERS

RECTIFIER. 6A. 100V. Motorola

BRIDGE RECTIFIER. 6A. 100V. Motorola MDA952-2 65p. POWER SUPPLY. 12V. 6.5A. Stabilised Power Supply. Contains 18,5V. 8.5A. sec. Transformer, 4×4000µF 25V. Mullard capacitors, 2×2N3055 on 2 Redpoint heatsinks, 12A., 120V. Bridge rectifier, stabilised p.c.b. circuit diagram. The parts alone are worth the asking price of £13 each inc. carriage. SHACKMAN....AUTO CAMERA Mk. 3. Complete with long focus lens assembly. 4 Film Carriers. Boxed in as new condition. £75 each. OC71 Transistors, unmarked. £15 per 1,000. HG5008 80mA. 40V. p.iv. equiv. OA47. £20 per 1,000. S2BN25 25A. 200V. Rectifier Diode. £2:50 per 4. S6 A20 20A. 600V. Rectifier Diode. £3 each. Transistor Mounting Pads. £2:50 per 500. Diode & Triac Mica Washer. £1 per 100. T.O.3 Transistor Socket. £1 per 50. Send s.a.e. for free circuit diagram.

COMMUNICATIONS EQUIPMENT POCKET V.H.F. F.M. RADIOTELEPHONE Cossor Type CC2/8 Mk. 2. Fully transistorised transmitter/receiver available

Cossor Type CC2/8 Mk. 2. Fully transistorised transmitter/receiver available in two versions:-Low band; Freq. range 71.5-104MHz. R.F. Output 500mW. Complete with $\frac{1}{2}$ wave whip aerial, combined microphone/loudspeaker and 13.3V. rechargeable nickel-cadmium DEAC battery Price 275 + v.a.t. U.H.F. 2 watt FIXED RADIO LINK. 24V. dc./240V. ac. F.M. TRANSMITTER/Type CC RTX 4A Mk. 1 R.F. Output 2W at 450-470MHz. RECEIVER/Type CC RR4A Mk. 1 Price 280.00 per unit Full Technical and operating data available. Prices and details on request. Mains Power Pack for the above <u>£12.00 each.</u> I + I CARRIER EQUIPMENTS. Cossor Type CC MZA. Solid state multiplex installations designed for U.H.F. radio systems enabling 2 speech channels each with out of band signalling, if required or the equivalent in telemetry information, to be transmitted simultaneously over a radio system. Prices and details on request. V.H.F. RADIOTELEPHONE BASE STATION. Cossor Type CC 603 Transmitter. Simplex or duplex operation, local or remote control wich talk through facilities, using double sideband a.m. modulation. Low-band 71.5-104MHz. or High-band 156-174MHz. VER. Output power 25W. into 50 Ohms.

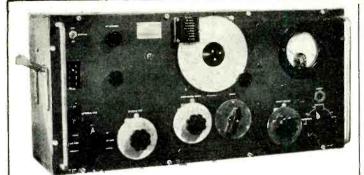
Low-band 71.5-104MHz. or High-band 156-174MHz. versions available. RF. Output power 25W. into 50 Ohms. 24V. dc. operation. Prices and details on request OPTIONAL POWER SUPPLY Type CC 101 for type CC603 base station P.O.A. SELECTIVE CALL SYSTEM. Coder Type CC 505/50 (50 way) or CC 505/100 (100 way). The Cossor selective call system may be used with any communication system where a base station is required to call any one or all of a number of sub-stations. Both versions available, all new and in original backing. in original packing. Price: 50 way £65 + v.a.t. 100 way £80 + v.a.t.

ID way £89 + V.a.t. IO way £89 + V.a.t. DEAC RECHARGEABLE BATTERY CASSETTES 13.4V (nom.) type B/SA 80351/108 Heavy duty encapsulated DEAC supply. Size 34×24×14in. Price £5 + V.a.t. 8-WAY BATTERY CHARGER Type CC 999 Charges up to 8 of the above battery cassettes. Price £35 + V.a.t. 12-WAY BATTERY CHARGER Type CC 999 Charges up to 12 of 13.4V DEAC batteries. Metered battery condition check. Price £35 + V.a.t. MICROPHONES S. G. Brown Stick Microphone and Stand. Push-to-talk button. 3002. £5 complete. S. G. Brown Hand-held with push-to-talk button. £8 each.

ELECTRONIC	COMPONENTS	
BARGAIN	COMPONENT	PACKS
Pack		

- 1 500 Carbon resistors, ‡, ‡, 1, 2 watt. 2 100 Electrolytic Condensers. 3 250 Ceramic, Polystyrene, Silver Mica, etc., Condensers. 4 250 Polyester, Polycarbonate, Paper, etc.,

FULL RANGE OF ELECTRONIC COMPONENTS AT OUR RETAIL SHOP. OPEN 9.30-6 MON.-SAT. 267 ACTON LANE, LONDON, W.4.



MARCONI SIGNAL GENERATOR TYPE TF-144G: Freq. 85 Kc/s-25 Mc/s in 8 ranges. Incremental: $\pm 1\%$ at 1 Mc/s. Output: continuously variable 1 micro-volt to 1 volt. Output Impedance: 1 microvolt to 100 millivolts, 10 ohms 100mV - 1 volt - 52.5 ohms. Internal Modulation: 400 c/s sinewave 75% depth. External Modulation: Direct or via internal amplifier. A.C. mains 200/250V, 40-100 c/s. Consumption approx. 40 watts. Measurements 29 × 12½ × 10 in. Secondhand condition. 27.50 each, Carr. 21.50.

T.1509 TRANSMITTERS (FOR EXPORT ONLY): General-purpose HF T.1509 TRANSMITTERS (FOR EXPORT ONLY): General-purpose HF communications transmitter for use in fixed or mobile ground stations. Hand or high-speed keying. Crystal or MO control, with temperature compensated MO circuit. CW, MCW and R/T. Frequency: 1.5 to 20 Mc/s. Modulation: 100 % O/put impedance: 50 ohms. Audio input: 600 ohms. Valves: Power Amplifier 2 × 813 and Modulator 2 × 813. Power requirements 200-250 volts a.c., 50 cycles. Power out put 300 watts. Dimensions 2ft. 6in. W. × 2ft. D. × 5ft. H. Weight: 800 lbs. Excellent condition, price £225.00 each. AN/ARC-27 TRANSMITTER/RECEIVER (FOR EXPORT ONLY): Frequency 225-400 mc. 1750 channels 100 Kc apart with 18 preset channels. Modulation: am. Power output 9 watts. Receiver is superheterodyne. Max. output 2 watts. Antenna: 50 ohm impedance. Power requirements 24v d.c. Complete transmitter with operating cables, control box, headphones, micro-phone. Price £250.00 each secondhand, excellent condition. POWER SUPPLY suitable for AN/ARC-27: 100 volts to 250 volts a.c. input. 24v d.c. output @ 41 amps fully smoothed. £45.00 each.

FREQUENCY METER BC-221: 125-20,000 Kc/s, complete with original calibration charts. Checked out, working order. \pounds 18:50 + \pounds 1:00 carr. BC-221 Unused as new condition complete with headset, spare valves, charts. \pounds 35:00 + £2.00 carr.

CT.52 MINIATURE OSCILLOSCOPE: Portable. Operates from 115V or 250V 50-60c/s; or 180V 500c/s. A small compact tropicalised instrument designed to meet requirements of radar and communication engineers and general electronic service. Measures 9 in. \times 8 in. \times 6 jin. Time base 10c/s-40Kc/s. Y plate sensitivity 40V per cm. Tube 2 jin. Frequency compensated amplifier up to 38dB gain. Bandwidth up to 1 Mc/s. Single sweep facilities. Complete with test leads, metal transit case. As new £27-50 each. Carr. \$1.

TUNING UNIT: 24V geared motor driving double 25pf double spaced variable capacitor. One m/c relay and 2 other relays. **£2**:50 each 30p post, good condition. UHF ASSEMBLY: (suitable for 1,000MHz conversion) including UHF valves: 2C42, 2C46, 1B40 (complete with associated capacitors and screening), 3 manual counters 0-999. Valves 6AL5 and 8×6AK5. **£10:00** plus 60p post, good condition.

MODULATOR UNIT: complete with transformer and 2×807 valves mounted in 19 in. chassis $\times 8$ in. high $\times 8$ in. deep. £4.50 secondhand cond., or £6.50 in 19 in. chassis \times 8 in new cond. Carriage £1.

RF UNIT: suitable for use with the above unit. Complete with $2 \times 3E29$ valves. Ideal for conversion to 4 metres. \$5 secondhand cond., or \$7.50 new cond. Carriage \$1.

POWER SUPPLY UNIT PN-12A: 230V a.c. input 50-60 c/s. 513V and 1025V @ 420 mA output. With 2 smoothing chokes 9H, 2 Capacitors, 10Mfd 1500V and 10Mfd 600V, Filament Transformer 230V a.c. input. 4 Rectifying Valves type 5/23. 2 x 5V windings @ 3 Amps each, and 5V @ 6 Amp and 4V @ 0.25 Amp. Mounted on steel base 19"Wx11"Hx14"D. (All connections at the rear.) Excellent condition £6 50 each, carr. £1.

AUTO TRANSFORMER: 230-115V, 50-60c/s, 1000 watts, mounted in a strong steel case $5^{\prime\prime} \times 6\frac{1}{2}^{\prime\prime} \times 7^{\prime\prime}$. Bitumen impregnated. £7 each, Carr. 75p. 230-115V, 50-60c/s, 500 watts. $7^{\prime\prime} \times 5^{\prime\prime} \times 5^{\prime\prime}$. Mounted in steel ventilated case. £4.00 each, Carr. 75p.

MODULATOR UNIT: 50 watt, part of BC-640, complete with 2 \times 811 valves, microphone and modulator transformers etc. \$7.50 each, 75p carr.

CATHODE RAY TUBE UNIT: With 3in. tube, Type 3EG1 (CV1526) colour green, medium persistence complete with nu-metal screen, £3:50 each, post 50p.

APN-1 INDICATOR METER, 270° Movement. Ideal for making rev. counter. £1.25, post 30p. AIRCRAFT SOLENOID UNIT S.P.S.T.: 24V, 200 Amps, £2 each, 30p post.

DECADE RESISTOR SWITCH: 0.1 ohm per step. 10 positions. 3 Gang, each, 0.9 ohms. Tolerance $\pm 1\%$ £3 each, 25p post. 90 ohms per step. 10 positions, total value 900 ohms. 3 Gang. Tolerance $\pm 1\%$ £3 50 each, post 30p.

TF-1041B VALVE VOLTMETER: Measures 25mV to 300V, 20 c/s to 1500 Mc/s a.c. Also 10mV to 1000V d.c. Resistance 0.02 ohms to 500 Meg. ohms. Power requirements 200-250 volts a.c. Secondhand, excellent con. £35.00. Carr. £1.

VARIAC TRANSFORMERS: Input 115V, output 0-135V at 2 Amps. £3 each 75p post.

RACK CABINETS: (totally enclosed) for Std. 19 in. Panels. Size 6 ft. high \times 21 in. wide \times 16 in. deep, with rear door. £12 each, £2.50 Carr. OR 4 ft. high \times 23 in. wide \times 19 in. deep, with rear door.£8.50, each, £2 Carr.

INSTRUMENT CABINETS: 19"W. × 16"H. × 16"D. £5.00 + £1.25 carr. 19"W. × 10"D. × 5"H. £2.50 + £1.00 carr.

TS-418/URM49 SIGNAL GENERATOR: Covers 400-1000MHz range. CW Pulse or AM emission. Power Range 0-120 dbm. £125 each. Carr. £1-50.

TN/130/APR.9 UHF TUNING UNIT: Freq. 4300-7350MHz. IF Output 160MHz with bandwidth of 20MHz and is electrically tuned by a d.c. reversible motor. £27.50 each. Carr. £1.

If wishing to call at stores, please telephone for appointment.



SIGNAL GENERATOR TS-497B/URR: (Boonton). Freq. 2-400 Mc/s in 6 bands. Internal Mod. 400 or 1000 c/s per sec. External Mod. 50 to 10,000 c/s per sec. External PM. Percent Mod. 0-30 for sine wave. Am or Pulse Carrier. O/put Voltage 0:1-100,000 microvolts cont. variable. Impedance 50Ω. Price: f_{85} each + $f_{1.50}$ carr.

CLASS "D" WAVEMETER NO. 1 MK. II: Crystal controlled heterodyne frequency meter covering 2-8MHz. Power supply 6V d.c. Good secondhand cond. £7:50 each. Post 60p.

RCA TE-149 HETERODYNE WAVEMETER: V-cut, 1MHz crystal (0.005%). Accuracy better than 0.02%. Dial directly calibrated every 1KHz from 2.5-5MHz. Useful harmonics up to 20MHz. Provision for fitting internal dry batteries. "As new" complete with Manual and Spares. £14 each. Carr. 75p.

POWER UNIT TYPE 24: (for R.216 Receiver) A.C. operated 100-125V or 200-250V, 50c/s. "As new" **£10** each. Carr. 75p.

ROTARY INVERTERS: TYPE PE.218E—input 24-28V d.c., 80 Amps. 4,800 rpm. Output 115V a.c. 13 Amp 400 c/s. 1 Ph. P.F.9. £17-50 each. Carr. £1-50. **POWER SUPPLY:** 230V a.c. input; 3000V @ 2.5mA; 4v @ 1 Amp, 300-0-300 200mA; 6V @ 7 Amp; 6V @ 3 Amp. With smoothing capacitors etc. **£10.00** each. £1.50 carr.

ACTUATOR UNIT: With 115V d.c. geared motor; o/put 12.5 rpm; torque 16 ins. oz; reversible; microswitches and potentiometer. £3.50 ea. + 40p post. DALMOTORS: 24-28V d.c. at 45 Amps, 750 watts (approx. 1hp) 12,000rpm. £5 each, 60p post.

MOTOR: 240V single phase, 2,400 rpm. 1/40 H.P. approx. Price £1.75 each, 30p post

LIST OF MOTORS AVAILABLE FOR 6p.

CONDENSERS: 30 mfd 600V wkg. d.c., **£3**·50 each, post 50p. 10 mfd 1000v wkg. **80p**, post 30p. 8 mfd 2500v **£5**, carr. 80p. 8 mfd 600v **45p**, post 15p. 8 mfd 1% 300v d.c., **£1**·25, post 25p. 4 mfd 3000v wkg. **£3**, post 50p. 4 mfd 2000v **£5**, carr. 80p. Capacitor 0·125 mfd 2700v wkg. **53**·75, post 50p. 2 5 mfd 25Kv wkg. **£20**, carr. **£3**. 2 mfd 12·5Kv wkg. TCC RL 7002-97, **£8**·50, carr. £1. 10 mfd 3Kv wkg, 55°C. TCC oil filled, **£7**·50, carr. £1. 5 x 1 mfd 3Kv wkg. 55°C. **a** - **£6**·50, carr. £1. 12 mfd 1500v d.c. wkg. **£3**·50, post 50p. 2

CONTROL PANEL: 230 v. A.C., 24 v. D.C. @ 2 amps, £2.50 each, carr. 75p. OHMITE VARIABLE RESISTOR: 5 ohms, 5[±] amps; or 40 ohms at 2.6 amps; 500 ohms, 0.55 amps. Price (either type) £2 each, 30p post each.

TX DRIVER UNIT: Freq. 100-156 Mc/s. Valves 3 × 3C24's; complete with filament transformer 230 v. A.C. Mounted in 19in. panel, £4-50 each, carr. 75p. AR88 RECEIVER: List of spares, 5p.

REDIFON TELEPRINTER RELAY UNIT NO. 12: ZA-41196 and power supply 200-250V a.c. Polarised relay type 3SEITR. 80-0-80V 25mA. Two stabi-lised valves CV 286. Centre Zero Meter 10-0-10. Size 8in. × 8in. × 8in. New condition £7.50, Carr. 75p.

WESTON INDUSTRIAL THERMOMETER MODEL 221: 0-100°C. 3in. dia. scale. Accuracy 1%. Precision made coil within-coil structure. Changes in temperature cause a totary action of the Helix turning the shaft to which the pointer is mounted. £2:80 each 30p post. Unused condition.

TRANSMITTER UNITS: Complete with 12V vibrator unit QQVO3-20A and 5 other valves with modulation transformer, etc. Two crystal controlled channels. Suitable for conversion to 2 metres. $\pounds 5 + \pounds 1$ carr.

THERMOCOUPLE METER: Scale 3.5 AE 2in. square flush mounting. $\pounds 2.50 + 25p$ post. **TS 15C/AP FLUXMETER:** Used to provide qualitative measurements of flux densities between pole faces of magnets. Range 1200-9600 gausses. $\pm 2\%$. S/hand good cond. $\pounds 25 + 60p$ post.

SYNCHRO DISTORTION AND MARGIN TEST SET: (Onwood Type 4A2) S/hand excellent cond. £85 each. Carr. £2.

MASTER SYNCHRO TEST SET T.101031 (U.S.A.): 115 volts 400 c/s. S/hand cond. £15 each + £1 carr.

MAGSLIP TESTER NO. 2 MK. I: S/hand cond. £25 each + £1 carr.

SYNCHROS: and other special purpose motors available. Send for list. S.A.E. PANORAMIC ADAPTOR TYPE ALA2: Suitable for use with APR-1, APR-4, and other Receivers having an I.F. frequency of 30 MHz. Will display signals up to 5 MHz either side of the received frequency. Power Supply 115V a.c. 400 c/s. Tube 3PB1 with nu-metal screen. £8:50 each. £1 carr. S/hand cond.

Tube 3PB1 with nu-metal screen. $\pm 6^{+}50$ each. ± 1 carr. Shand ond. **TELEPRINTER EQUIPMENT: MUIRHEAD D-514-A TRANSMISSION- MEASURING SET:** Consists of an oscillator covering audio and carrier fre-quencies, with suitable transmission measuring equipment. Power pack is contained in a separate case and operates from A.C. mains at various voltages, or from an accumulator. Power Supply 12V d.c. or 100/250V a.c. Freq. Range continuous 100-40,000Hz. Direct reading from decade dials. Accuracy $\pm 0.4\%$ $\pm 3Hz$ over whole range. Oscillator o/put 5mW ($\pm 7db$) or more inot 600Ω at any freq. Mea-surement up to 50db and down to at least 45db. Price £10 each Carr. £1.

TELEPRINTER TYPE 7B; Pageprinter 24V d.c. power supply, speed 50 bauds per min. 'as new' cond. in original packing case, £25 each; or second hand cond. (excellent order) no parts broken, £15 each. Carriage either type £2. Full list of Teleprinter equipment available for 6p.

AUTOMATIC VIBRATION EXCITER CONTROL UNIT TYPE 1016 Manufactured by Bruel & Kjoer. 5-5000 c/s. per second. S/hand very good cond. $\$90 + \pounds2$ carr. INSULATION TEST SETS: A.C. or D.C. 0-5 kV. \$22·50. S/hand cond. AND 0-3 kV. Positive and negative outputs, fine and course control. \$17·50. S/hand cond. Carr. both types $\pounds2$.

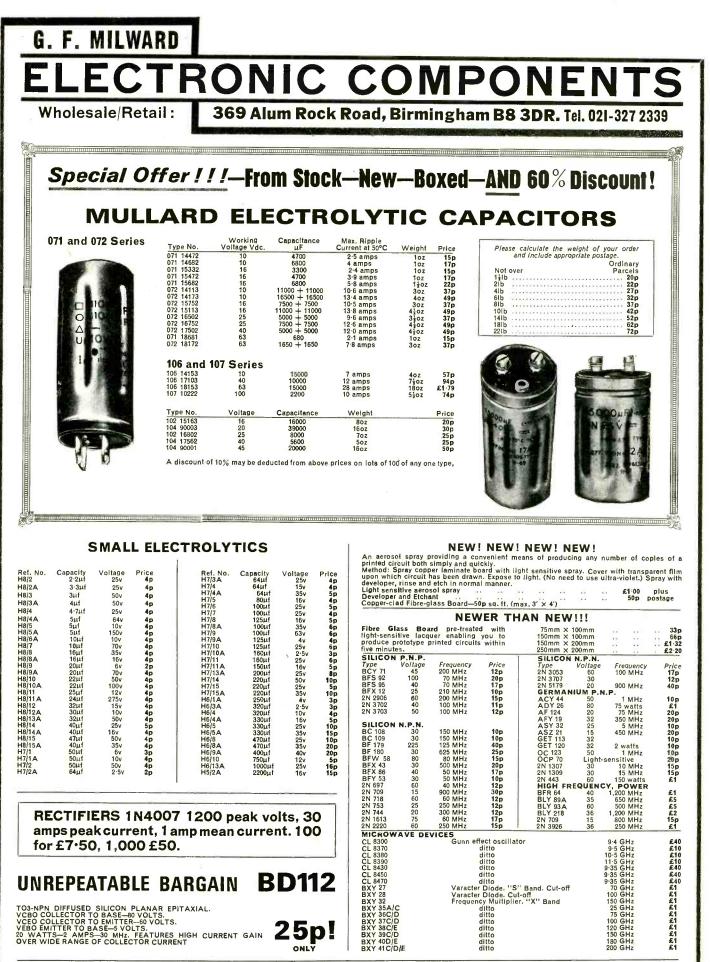
INSULATION TEST SET: 0-10 kV negative, earth with amplifier provision for checking ionisation. 110/230V a.c. input. S/hand good cond. \$30 + \$1 carr. BOONTON SIGNAL GENERATOR TYPE 202B A.M./F.M.: 54-216 MHz in three bands. Deviation 24, 80 and 240 kc/s. Attenuator is adjustable 0.1 Uv to 0.2V. As new condition. $\pounds 175 + \pounds 2$ carr. AVO FIXED ATTENUATORS: 75 ohms. $\pounds 2.50 + 20p$ post. New cond. R.F. POWER METER: 0-30 watts s/hand good cond. $\pounds 27.50 + \pounds 1$ carr.

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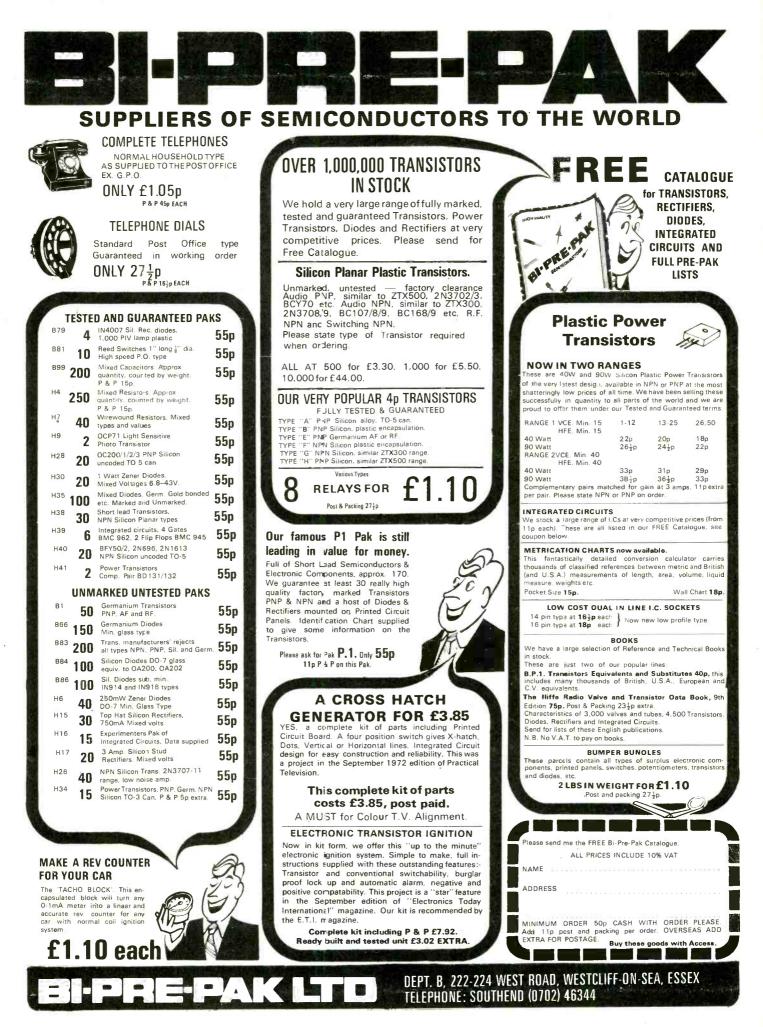
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16-929-7 Mil, 14- 146MHz and 10-00 MHz WWW, SBB, CW, AM and FM. AF output more than 1 wat.8 Meter, Squele Phone Jack. Power rejulte- ments 100/240v. A.C. 12-14v. D.C. Bize 270x 140 x310mm. OUR £155:00 Carr. PRICE Carr. PRICE Carr. PRICE Carr. PRICE Carr. PRICE Carr. Carr. PRICE CARACTERISCIPPER Fully transistoried	TYPE SD.460 46mm × 59.5mm Fronts 50µA £2:80 10mp £2:60 50-0-50µA £2:80 10mp £2:60 100µA £2:75 5 amp £2:60 200µA £2:70 50 m/L £2:60 200µA £2:70 50 m/L £2:60 500µA £2:55 200V, LC £2:60 500µA £2:60 50V, DC £2:60 500µA £2:60 50V, DC £2:60 10mA £2:60 50V, AC £2:70 10mA £2:60 15V, AC £2:70 10mA £2:60 10V, AC £2:70 10mA £2:60 10V, AC £2:70 100mA £2:60 VU Meter £2:70 100mA £2:60 VU Meter £2:70 100mA £2:60 S0V PC £2:70 100mA £2:60 S0V PC £2:70 100mA £2:60 S0V PC £2:70	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	"SEW" BAKELITE PANEL METERS TYPE MR.65 3jio. square trout. Image: State of the square trout. 1 amp. 42:60 6 amp. 42:60 30 amp. 42:60 30 amp. 42:60 50 amp. 42:60 50 amp. 42:60 50 amp. 42:60 50 amp. 42:60 50 y. D.C. 42:60 50 y. D.C. 42:60 50 y. D.C. 42:60
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OA2 0-33 6BC8 0-60 6L7(M) 0-50 12AT6 0-28 30P4MR AL60 0-78 EBL21 0-60 OB2 0-33 6BE6 0-20 6L12 0-34 12AT7 0-20 0-95 ARP3 0-35 EC53 0-49	EM83 0.75 PCC89 0.42 QP21 0.50 U33 1.50 2N3988 0.55 BA130 0.11 GET113 22 OC44 0.11 EM84 0.31 PCC189 0.46 QQV03/10 U35 0.83 28323 0.55 BA153 0.17 GET116 44 OC45 0.12
0Z4 0.44 6BG6G 1.05 6L18 0.49 12AU6 0.38 30P12 0.69 ATP4 0.40 EC54 0.50	EM85 1.00 PCF80 0.28 1.20 U37 1.75 AA119 0.17 BCY10 0.50 GET118 22 OC46 0.17 EM87 0.40 PCF82 0.30 Q875/20 U45 0.78 AA120 0.17 BCY12 0.55 GET119 27 OC65 1.24
1A5GT 0-49 6BJ6 0-39 6LD12 0-30 12AV6 0-28 30P19/ AZ31 0-46 EC88 0-39 1A7GT 0-33 6BK7A 0-60 6LD20 0-55 120AV7 0-29 30P4 0-65 AZ41 0-53 EC92 0-34	EX31 0.35 PCF84 0.40 0.63 U47 0.65 AA129 0.17 BCY33 0.22 GET573 42 OC70 0.14 EY81 0.35 PCF86 0.44 QS95/10.49 U49 0.60 AAZI3 0.20 BCY34 0.25 GET587 47 OC71 0.12
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1666 0.75 6BR8 0.75 6P28 0.70 12BE6 0.30 30PL14 0.75 CV6 0.53 ECC40 0.68 1H5GT 0.55 6BR8 0.75 6P28 0.70 12BH7 0.27 30PL3 75 CV6 0.53 ECC40 0.68	EY87/6 0.27 PCF800 58 QY04/7 0-63 U78 0.27 AC114 0-44 BC107 0-14 (BET882 55)0C75 0-12 EY88 0-40 PCF8010-40 R11 0-99 U153 0-25 AC126 0-14 BC108 0-14 (BET887 -25 OC76 0-17 EY91 0-58 PCF802 0-37 R10 1-75 U191 0-65 AC127 0-19 BC113 0-28 (BET889 -25)0C77 0-30
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184 0 33 6B26 0 49 6R7(M) 0 75 128A7GT 55 35Z3 0 50 DAC32 0 55 ECC88 0 35 185 0 22 6C4 0 28 6SA7M 0 35 128C7 0 50 DAF96 0 36 ECC88 0 35	EZ81 0.20 PCL82 0.29 R52 0.33 U282 0.40 AC157 0.28 BF154 0.28 GEX13 0.20 OC81D 0.12 EX90 0.27 PCL83 0.54 RK34 0.38 U291 0.50 AC155 0.28 BF158 0.32 GEX35 0.25 OC82 0.12 PCL84 0.28 PF156 0.32 CF156 0.34 U301 0.40 AC156 0.28 BF158 0.32 GEX35 0.25 OC82 0.12
104 0.44 0.05 0.22 6SC70T 33 12SG7 0.38 35Z50T 30 DD4 1.00 ECC804 0.55 105 0.80 6C9 1.00 6SG7(M) 39 12SH7 0.35 35Z50T 30 DD4 1.00 ECC804 0.55	1-75 PCL86 0.36 SP61 0.75 U329 0.62 AC167 0.66 BF163 0.22 GEX 45 0.36 OC83 0.22
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3Q4 0.49 6CH6 0.55 6U7G 0.76 1487 0.75 50L6GT 45 DH81 0.75 ECH21 0.63 3Q5GT 0.55 6CL6 0.46 6V4 0.19 1487 0.75 72 0.33 DK32 0.33 ECH21 0.63	GZ33 0.70 PD500 1.44 UBC41 0.45 VP2 0.53 ACY18 0.22 BFY50 0.25 MAT120 43 OC172 0.39
384 0.26 6CL8A 0.80 6V6G 0.17 19AQ5 0.42 65A2 0.43 DK40 0.55 ECH42 0.59 4CB6 0.55 6CM7 0.75 6V6GT 0.27 19BG6G 80 85A2 0.43 DK92 0.55 ECH42 0.59	GZ37 0.67 PEN45 58 UBF80 0.53 VP33 0.40 ACY20 0.20 BFY52 0.22 0.49 0.14 OC201 0.42 HABC80 PEN45 580 UBF89 0.33 VP41 0.38 ACY21 0.21 BTX34/400 0.41 0.47 OC202 0.47
5CG8 0.55 6CU5 0.75 6X4 0.27 19G6 1.40 90AG 3.38 DL92 0.26 ECH83 0.38 5B4GY 0.70 6CW4 0.70 6X5GT 0.28 19H1 2.60 90AG 3.38 DL92 0.26 ECH83 0.38	0.44 FEN45DD UBL21 0.55 V101A 0.33 ACV22 0.17 2.200A47 0.1100203 0.33 HL13C 0.20 PEN46 0.20 UC92 0.35 V1501 0.15 ACV28 0.20 BY100 0.20(0A70 0.17)0C204 0.33
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A.15 0.75 6F23 0.65 9D7 0.40 2575G 0.70 956 0.10 E180F 0.90 EF83 0.54 A.15 0.75 6F23 0.65 9D7 0.40 25Z4G 0.33 1821 0.53 F180C 0.90 EF83 0.54	KTS 1.75 PL83 0.30 UF85 0.34 X61 0.50 AF125 0.19(CG12E 0.22)(A211 0.73)Y543 0.20
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6AKS 0.30 6F28 0.60 10DE7 0.55 28D7 1.00 6060 0.30 EA76 0.88 EF91 0.17 6AL5 0.12 6F32 0.30 10F1 0.50 30A5 0.65 7193 0.53 EABC80 EF91 0.17	KT66 0.80 PL509 0.60 UL84 0.28 Z729 0.30 MATCHED TRANSISTOR SETS KT74 0.63 PL508 0.90 UM80 0.33 Z749 0.65 LP15 (AC113, AC154, AC157, AA120). 58p per pack.
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6AT6 0.30 6J7G 0.24 6AU6 0.28 6J7(M) 0.38 10P14 2.00 30FL12 0.69 10P18 0.28 6J7(M) 0.38 10P14 0.00 30FL12 0.69 10P18 0.28 50FL13 0.50	MHLD6 .75 facturers' seconds nor rejects, which are often described as "new and tested" but have a innited
6AV6 0.33 6JUSA 0.73 12A6 1.00 30FL14 0.66 AC/PEN(7) EBC91 0.33 EL32 0.50 6AW8A 0.65 6K7G 0.12 12AC6 0.55 30L1 0.29 0.98 EBF80 0.30 EL34 0.48	MU12/14 Terms of business. Cash or cheque with order. Despatch charges 100 per order up to three terms, 0.38 then each additional item 3p extra. 25p total despatch on orders between 25 and 210. Over 210
6AX4 0.55 6K8G 0.33 12 AD6 0.60 30L15 0.55 AC/TH1 50 EBF83 0.38 EL35 1.00	

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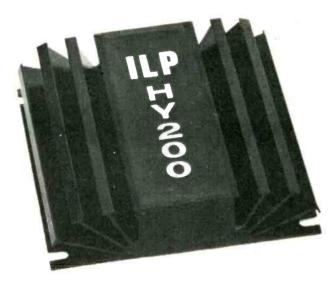
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2G303 2G306	0-25 C-30	2N3405 2N3414	0·27 0·10	40363 40389	0-88 0-46	BC135 BC136	0-11 0-15	BDY61 BDY62	1 · 25 1 · 00	BSY24 BSY25	0·20 0·15	SN7400 28p SN7401 38p	SN7430 SN7432	28p 48p	SN7472 SN7473	40p 57p
2G309 2G345B	0 30 0 25	2N3415 2N3416	0·10 0·15	40394 40395	0.56	BC137 BC138	0·15 0·24	BF115 BF117	0-23 0-43	BSY26 BSY27	0·20 0·15	SN7402 28p SN7407 56p	SN7437 SN7440	52p 20p	SN7474 SN7475	48p 96p
2G371 2G374	0·15 0·15	2N3417 2N3570	0·21 1·25	40406 40407	0.44	BC140 BC141	0·34 0·39	BF119 BF121	0.58	BSY28 BSY38	0·15 0·20	SN7410 28p SN7411 22p	SN7441 SN7442	75p 79p	SN7476 SN7481	64p £1-25
2N174 2N404	1-40	2N3571 2N3572 2N3702	1·12 0·97 0·11	40408 40409 40410	0.50 0.52 0.53	BC142 BC143 BC144	0-24 0-21 0-24	BF123 BF125 BF152	0-27 0-25 0-20	BSY39 BSY51 BSY52	0·20 0·25 0·25	SN7413 48p SN7420 20p	SN7443 SN7444	£1-04 £1-04	SN7483 SN7484	£1.00 95p
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2N457A 2N491 2N696	3-25	2N3705 2N3706	0-10	40467 40468 A	0.69	BC148 BC149	0-12	BF158 BF159	0-23	BSY56 BSY65	0.79	SN7423 52p	SN7446 SN7447	£2.00 £1.30	SN7490 SN7491	£1.00 £1.60
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2N709 2N711	0-40 0-30	2N3713 2N3714	1.95	40673 AC107	0·70 0·35	BC167B BC168B	0-11 0-13	BF177 BF178	0·29 0·35	CIII D40N3	0-53 0-55	SN 74100 £2.50 SN 74107 £0.43	SN 74153 SN 74154	£2.00	SN 74176 SN 74180	£1.50 £1.55
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2N914 2N916	0.15	2N3790 2N3791	4-21	AC126 AC127	0·25 0·20 0·20	BC171 BC172	0-13	BF183 BF184	0-40	GET119 GET120	0·35 0·25	SN 74123 £1-35 SN 74141 £0-90	SN 74164	£2.26	SN 74193 SN 74196	£1-90 £1-60
2N918 2N929	0-30 0-14 0-14	2N3792 2N3794 2N3819	5·04 0*10 0·32	AC128 AC141K AC142K	0·30 0·25	BC182 BC182L BC183	0-10 0-12 0-09	BF185 BF194 BF195	0-17 0-14 0-17	GET535 GET536 GET538	0·20 0·20 0·20	SN 74145 £1.50	SN 74167	£6-25	SN 74198	£4.60
2N930 2N1090	0-14	2N3819 2N3820 2N3823	0.47	AC151V AC152V	0.14	BC183L BC184	0.09	BF195 BF196 BF197	0.15	GET538 GET873 GET880	0-12	SN 74150 £3-35 SN 74151 £1-10	SN 74174		SN 74199	£4.00
2N1091 2N1131 2N1132	0.20	2N3824 2N3826	1.33	AC153 AC153K	0.22	BC184L BC186	0-11	BF198 BF199	0-15	GET883 GET887	0.20	NE	555 TIM	ER I.C	. 90p	
2N1302 2N1303	0-16	2N3854 2N3854A	0.16	AC154 AC176	0.20	BC187 BC207	0.25	BF200 BF224J	0-40	GET890 GET895	0-22		N D.I.L.			
2N1304 2N1305	0.20	2N3855 2N3855A	0.16	AC176K AC187K	0·20 0·20	BC208 BC212K	0-11 0-10	BF225J BF237	0.19	TIP29A TIP30A	0-49	Z	ENER	DIOD	ES	
2N1306 2N1307	0·22 0·22	2N3856 2N3856 A	0-16 0-16	AC188K ACY17	0·26 0·35	BC212L BC214L	0-18	BF238 BF244	0.22	TIP31A TIP32A	0.62	400MW—BZY88 an 1 watt—IN, IZM an				CC 25-
2N1308 2N1309	0.25	2N3858 2N3858 A	0-16	ACY18 ACY19	0·24 0·27	BC237 BC238	0.09	BF245 BF246	0.33	TIP33A TIP34A	1-01	10 watt-ZS SERIE				
2N1483 2N1507	0.90	2N3859 2N3859A	0-16	ACY20 ACY21	0-22	BC239 BC251	0·09 0·20	BF247 BF254	0.49	TIP35A TIP36A	2·90 3·70	BR	DGE R	ECTIF	IERS	
2N1613 2N1631	0.20	2N3860 2N3866	0.16	ACY22 ACY28	0-16 0-20	BC252 BC253	0.18	BF255 BF257	0-17 0-41	TIP41A TIP42A	0·79 0·90	PIV 50 1A 24p	100 26p	200 35p	400 35p	600 40p
2N1637 2N1638	0-36	2N3877 2N3877A	0·25 0·26	ACY30 ACY39	0-42	BC257 BC258	0.09	BF258 BF259	0-46	TIP2955 TIP3055	0-98	2A 32p	37p	41 p	46p	52 p
2N1701 2N1702	1·10 2·15	2N3900 2N3900A	0·20 0·21	ACY40 ACY41	0-17	BC259 BC261	0-13 0-20	BF270 BF272	0.25	ME0401 ME0402	0.18	4A 60p 6A 62p	70p 75p	75p 80p	85p £1·10	95p £1·25
2N1711 2N1893	0·22 0·34	2N3901 2N3903	0-32	ACY44 AD136V	0-31	BC262 BC263	0·18 0·23	BF273 BF274	0.25	ME0404 ME0411	0-13 0-17	DIOD	DES &	RECTI	FIERS	
2N2102 2N2147	0·30 0·70	2N3904 2N3905	0·27 0·24	AD142 AD143	0.54	BC300 BC301	0-42 0-34	BF457 BF458	0.53 0.65	ME0412 ME0413	0·18 0·14	IN5171 (1.5 amp 50 IN5172 (1.5 amp 10			(10 amp 100 p (10 amp 200 p	
2N2148 2N2192	0-94 0-40	2N3906 2N4036	0-27 0-46	AD149V AD150	0-66 0-63	BC302 BC303	0-27 0-54	BFS21A BFS28	2-30 0-92	ME1120 ME4001	0.25	IN4517 (1·5 amp 20	0 pv) 10p	CL1004	10 amp 400 p	v) 47p
2N2192A 2N2193	0-40 0-40	2N4037 2N4058	0 40	AD161 AD162	0-45	BC307 BC307A	0-10 0-10	BFS61 BFS98	0·27 0·28	ME4002 ME4003	0-11 0-14	IN5173 (1·5 amp 40 IN5176 (1·5 amp 60	0 pv) 12p		(10 amp 600 p	
2N2193A 2N2194	0·61 0·27	2N4059 2N4060	0.09	AD161 AD162	Pr. 1-05	BC308 BC308A	0.09 0.09	BFW11 BFW15	0.61	ME4101 ME4102	0·10 0·11	IN5177 (1·5 amp 80 PL4007 (1·5 amp 10			& CATHODI 35 amp 50 pv)	
2N2194A 2N2195	0·30 0·37	2N4061 2N4062 2N4302	0.11	AF109R AF114 AF115	0.40	BC308B BC309	0.09	BFX13 BFX29	0.23	ME4103 ME4104	0.10	IN5400 (3 amp 50 p IN5401 (3 amp 100			35 amp 100 pv 35 amp 200 pv	
2N2195A 2N2218A 2N2219	0.18	2N4303 2N4916	0.47	AF115 AF116 AF117	0.25	BC309A BC309B BC327	0-10	BFX30 BFX37	0.25	ME6101 ME6102	0·14 0·16	IN5402 (3 amp 200 IN5404 (3 amp 400	pv) 20p	IN1188 (35 amp 400 pv 35 amp 600 pv	v) £2·66
2N2219A 2N2219A 2N2220	0·37 0·51 0·20	2N4917 2N4918	0·20 0·17 0·50	AF118 AF121	0.50	BC328 BC337	0-24 0-22 0-19	BFX44 BFX63 BFX68	2.48	ME8002 ME8003	0.17	CL7005 (3 amp 600	pv) 25p	CATH	ODE STUD	ONLY
2N2221 2N2221 A	0.20	2N4919 2N4920	0.63	AF124 AF125	0 24	BC338 BCY30	0.19	BFX84 BFX85	0.24	M J400 M J420 M J421	0-78 0-86 0-88	CL7006 (3 amp 800 CL7007 (3 amp 100)			35 amp 800 p 35 amp 1000 p	
2N2222 2N2222 A	0-31 0-41	2N4921 2N4922	0.50	AF126 AF127	0.19	BCY31 BCY32	0.40	BFX86 BFX87	0.24	MJ430 MJ440	0.75		141 17p	BY237 BY210	121p 0A79 35p 0A81	7p 8p
2N2368 2N2369	0-11 0-15	2N4923 2N5172	0 60	AF139 AF170	0·38 0·25	BCY33 BCY34	0-34	BFX88 BFX89	0.25	M J 480 M J 481	0.75	IN916 7p B/	144 12p	BYZ11 BYZ12	32p 0A85 30p 0A90	1 O p
2N2369A 2N2646	0·17 0·70	2N5174 2N5175	0 22	AF172 AF178	0-25	BCY38 BCY39	0·53 1·05	BFY10 BFY11	0·35 0·45	M J490 M J491	0.94	AA129 15p BA	145 17p 154 12p	0A9	10p 0A91	7p 7p
2N2647 2N2711	1-20 0-12	2N5176 2N5190	0·32 0·92	AF179 AF180	0-65 0-50	BCY40 BCY42	0·50 0·15	BFY17 BFY18	0·90 0·35	M J802 M J901	14-2 2-65	BA102 25p BY	100 15p 126 15p	0A10 0A47	20p DA95 71p OA200	
2N2712 2N2713	0·12 0·17	2N5191 2N5192	0-96 1-24	A F186 A F200	0-40 0-35	BCY43 BCY58	0-15	BFY19 BFY20	0.35 0.50	M J 1001 M J 1800	2·34 1·88	BA110 25p B)	127 171p	0A70 0A73	71p 0A202 10p 0A210	
2N2714 2N2904	0.17	2N5193 2N5194	1.01	AF211 AF239	0.55	BCY59 BCY70	0.22	BFY29 BFY37	0·40 0·20	M J 2500 M J 2501	2·92 3·25	OPTOELECTRONIC		POTENT	IOMETERS	1
2N2904 A 2N2905	0.25	2N5195 2N5245	1-46	AF240 AF279	0·72 0·54	BCY71 BCY72	0.22	BFY41 BFY43	0.43	M J 2955 M J 3000	1.00 2.47	MINITRON 3015F 7 INDICATOR (16 PIN	-SEGMENT	Carbon: Log. or l	: _in., less switc	:h, 17 ło
2N2905A 2N2906	0-88	2N5457 2N5458	0.35	AF280 AFY42	0:54 0-74	BCY87 BCY88	3-47	BFY50 BFY51 BFY52	0·22 0·15	M J3001 M J3701	2·79 0·9	DRIVER SN 7447	£1 30	Log. or L	in., with swit und Pots (3W)	ch, 27p
2N2906A 2N2907 2N2907A	0·30 0·32 0·33	2N5459 3N128 3N138	0·33 0·73 1·65	AL102 AL103	0.75	BCY89 BCZ10 BCZ11	0.97	BFY52 BFY53 BFY56	0·20 0·15 0·34	M J4502 M JE340	4.44	SOCKETS TIL 209 LIGHT	20p EMITTING	Twin Ga	nged Stereo Po	
2N2907A 2N2923 2N2924	0.33	3N138 3N139 3N140	1.65	ASY26 ASY27	0·30 0·36 0·28	BCZ11 BD115 BD116	0.50 0.75 0.50	BFY56 BFY64 BFY75	0·34 0·41 0·40	MJE370 MJE371	0.73	DIOOE. (Red). 35	>	or Lin.	, 47p S (CARBON)	
N2925 N2926	0.12	3N140 3N141 3N142	0-81 0-58	ASY28 ASY29 ASY50	0·28 0·36 0·20	BD121 BD123	0.50	BFY76 BFY77	0.40	M JE520 M JE521	0.59	SCORPIO ignition 50p P. & P.	kit £10 +	0·1 Watt	t 6p VERT	ICAL
Green	0-12	3N143 3N152	0.75	ASY55	0.35	BD124 BD130	0.67	BFY78 BFY90	0.36	MJE1092 MJE1102	1-93	WIRE-WOUND RE	SISTORS	0-2 Watt 0-3 Watt	t 6p 01 t 7½p HORIZC	
Orange N3053	0.10	3N153 3N154	0-81	BC107 BC108	0.15	BD131 BD132	0-40	BRY39 BSX19	0·30 0·13	M J E2801 M J E2901 M J E2955	1-19 1-56	2.5 watt 5% (up to only), 7p			POTENTIOME 58mm, TRACK	
N3054 N3055	0 60 0 75	3-N159 3 N187	1-17	BC109 BC113	0-19 0-13	BD135 BD136	0.43	BSX20 BSX21	0.14	RETU	1-65 IRN	5 watt 5 + (up to 8	·2kΩ only),	SINGLE	GANGED, LOG	or LIN
2N3390 2N3391	0-20 0-20	3N200 3N201	2-49	BC114 BC115	0.12	BD137 BD138	0.55	BSX26 BSX27	0·49 0·34			9p 10 watt 5% (up to 3	26kΩ only),	TWIN G	to 1M. 30p ea Anged. Log	or LIN
N3391 A N3392	0-22 0-13	40050 40251	0-78 0-81	BC116 BC116A	0-15 0-18	BD139 BD140	0·71 0·83	BSX28 BSX29	0·25 0·47	POS		10p	01111		o 500k. 50p e	ach
N3393 N3394	0.12	40309 40310	0·30 0·50	BC117 BC118	0·21 0·11	BDY10 BDY11	1·25 1·50	BSX30 BSX59	0.68	SERV			UB-MIN. EL			
N3402	0-12	40313 Post & Packing	0-92 13p per	BC119 order, Europ	0.27 be 25p. Co	BDY17 mmonwealt	1.50 1 (Alr) 65p	BSX60 (Min.)	0.24		PRICES	SUBJECT TO ST	e range of va			
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Tel: 0I-452 0I6I/2/3 A. MARSHALL & SON LTD 42 CRICKLEWOOD BROADWAY, LONDON, N.W.2 AND 65 BATH STREET, GLASGOW TEL 041-332 4133 CALLERS WELCOME Hours: 9-5.30 pm Mon-Frl 9-5 pm Sat																

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With the development of the HY200, ILP bring you the first COMPLETE Hybrid Power Amplifier.

COMPLETE: because the HY200 uses no external components! COMPLETE: because the HY200 is its own heatsink!

By the use of integrated circuit technique, using 27 transistors, the HY200 achieves total component integration. The use of specially developed high thermally conductive alloy and encapsulant is responsible for its compact size and robust nature.

The module is protected by the generous design of the output circuit, incorporating 25amp transistors. A fuse in the speaker line completes protection.

Only 5 connections are provided, input, output, power lines and earth.

Output Power: 100 watts RMS; 200 watts peak music power into 8Ω Input Impedance: $10K\Omega$ Input Sensitivity: ODb (0.775volt RMS) Load Impedance: $4-16\Omega$ Total Harmonic Distortion: less than 0.1% at 100 watts typically 0.05% Signal: Noise: Better than 75Db relative to 100 watts Frequency response: $10Hz-50KHz \pm 1Db$ Supply Voltage: $\pm 45volts$ APPLICATIONS: P.A., Disco, Groups, Hi-Fi, Industrial.

PRICE: £14.90 inc. VAT & P & P

Trade applications welcomed

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SECOND GENERATION 25 WATT H YBRI

A brand new hybrid fabrication technique, recently perfected in our laboratories, has enabled us to achieve our latest range of completely integrated devices We have now finally reduced the modular amplifier to a simple input/output device

requiring only the addition of a basic unstabilized (split line) power supply. The HY50 takes medium power modules to their logical conclusion by incorporating with it a heatsink, which is designed in special high conductivity alloy, sufficient for normal audio use without additional chassis sinking. All this without significantly

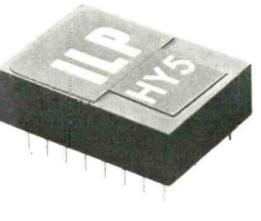
increasing the size of the module comparable in size to a packet of King-size cigarettes. Consistent with modern thinking a triple rated output circuit with a load fuse allows

for peak transient response without distortion but ensures the necessary protection. SPEC.

OUTPUT POWER LOADIMPEDANCE INPUT SENSITIVITY: INPUT IMPEDANCE: TOTAL HARMONIC DISTORTION: SIGNAL/NOISE BATIO: FREQUENCY RESPONSE: SUPPLY VOLTAGE: SIZE

25watts RMS. 50watts peak music power. 4-16 Ω into 8 Ω . Odb (0.775volts RMS). 47KΩ. Less than 0.1% at 25watts typically 0.05 better than 75db. 10Hz-50 KHz ± 1db + 2 5volts 105x50x25mm Price £5.40 mono £10.80 stereo. Price inclusive of VAT & P & P.

NEW HY5 PRE-AMPLIFIER



Unchallenged for two years, the HY5, our unique multifunction preamplifier/tone hybrid, has been brought into line with the advancements in our power hybrids. Like the HY50, the new HY5 has no external components & has been redesigned to run off a split power

line with improvements in signal/noise, overload capability & reduced distortion. The output has been increased to match the power module (Odb), and to share the same power supply. Overall size is reduced by the use of a new thin film circuitry while the device still retains all the functions

of the earlier device. When combined with the HY50 & power supply only potentiometers are required to complete a simple

mono amplifier with input & output facilities expected to be found on Hi-Fi amplifiers The combination of two HY50's two HY50's sharing a common power supply (PSU50) are linked by a balance control to form a complete stereo system.

INPUTS SPEC

Magnetic Pick-up 3mV (within 1db RIAA curve) Ceramic Pick-up up to 3mV, Microphone 10mV Tuner 250mV. Auxiliary 3-100mV Input impedance 47kg 1kHz

OUTPUTS Tape 100mV Main output. Odb (0.775volts).

ACTIVE TONE CONTROLS Treble ± 12db at 10kHz Bass ± 12db at 100Hz OVERLOAD CAPABILITY (equalization stage) 40db on most sensitive input. OUTPUT NOISE LEVEL (below 10mV magnetic input) 68db. DISTORTION 0.05% at 1kHz.

SUPPLY VOLTAGE ± 16-25volts SUPPLY CURRENT 15mA.

Price £4.51 mono £9.02 stereo Price inclusive of VAT & P & P



POWER SUPPLY PSU50

The new PSU50 has a low profile look being only 24 inches high and can be used for either mono or stereo systems. SPEC.

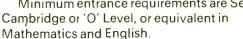
OUTPUT VOLTAGE ± 25volts. INPUT VOLTAGE 210-240volts. SIZE L. 70 D. 90 H. 60mm. Price £5.23. Price inclusive of VAT & P & P

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AD143 043 BC143 0.33 BD132 0.66 BF182 0.44 AD140 055 BC145 0.50 BD133 0.72 BF183 0.44 AD140 055 BC147 0.11 Bi)135 0.44 BF184 0.25	MPF102 046 2G339 022 2N2193 039 BY128 0.17 OA5 0.38 18021 0.11 MPF104 041 2G339A 018 2N2194 039 BY130 018 OA58L 023 18951 007	Sub-Min. 5005.60 Full Tested 1,0009.90 Ideal for Organ Builders.
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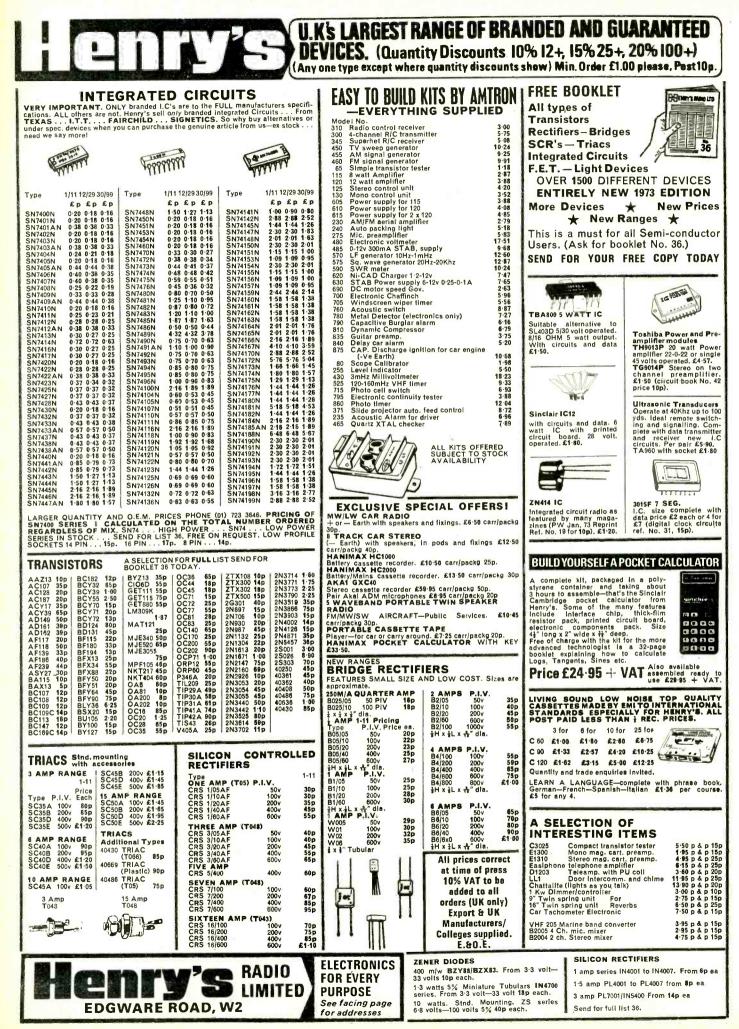
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ELECTRONIC CROSS-OVER

PORTABLE MIXER



The Mavis 3 way electronic cross-over is intended for use primarily with music and speech amplifying systems. It enables the bass range, mid-range and treble range to be separately controlled. The cross-over frequency for each range can be specified if required but will be, in the standard unit, as follows: Bass roll-off 45 c.p.s.

Bass to mid-crossing point 800 c.p.s.

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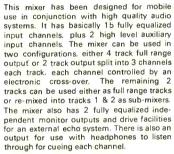
GENERAL SPECIFICATION

Size	19" x 12" deep x 7" high (standard 19"
	racking)
Weight	35lb.
Input	0 dbm 600 ohm balance
Output	+10 dbm 600 ohm balance
Power Requirements	110/230 volts 50/60 c.p.s. at 80 watts
	approx.
Optional extra	Sub plate

Optional extra PRICE - £500

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INTRODUCING THE P.A.S. 30/30



GENERAL SPECIFICATION 38" x 27" x 12" 1901b approximately

Ρ	ower Consumption
	put Impedance
C	utput Impedance
h	nput level 15 modules
b	nput level auxiliary 2 inpu
C	utput level
C	ue output level
E	qualisation range

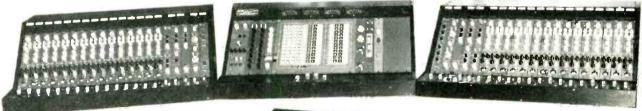
Overall noise

Channel separation

80 watts approximately 600 nhm halanced 600 ohm balanced -60 dbm -0 dbm + 10 dbm all channels 300 milliwatts - 300 millivatts ± 14 db treble ± 20 db mid ± 14 db bass ± 20 db bass peak better than - 60 db below full output better than - 80 dbm

WW—131 FOR FURTHER DETAILS

PRICE - £6,000 INCLUDING FREIGHT CASE



P.A.S. 30/30

This 30 Channel Desk is a development of the Mavis Four Group 15 Channel Mixer to meet the growing demands of modern P.A. and Studio work." It is designed such that every channel may be operated Chennel Mixer to meet the growing demands of modern Fix-an Studio work? It is designed such that every channel may be operated with total flexibility in a four channel quadraphonic setup. and for purposes of live recording it is unique in the fact that a multi-track tape machine of up to 30 tracks may be directly coupled to the channels and a 4 track Tape Machine to the mains groups. The Mixer can then at a later stage be used for mixing down to a stereo or quad-master using the main group outputs. As a compromise between a P.A. Mixer and a conventional Studio Desk. It differs from the latter in the fact that apult form the usual foldback, echo send, cueing facilities atc., only eight sub-groups and four main groups are derived directly from each channel, and are fully equipped for patching in auxiliary equipment, and may be switched before or P.A.) are equipped with fifteen channels each and a complete output arrangement including four groups and a stereo cors-over. The interd section — the routing for the tow wings and all the extra equipment needed for master quad control and mixes and a complete output arrangement including four groups and a stereo cross-over. The interd section — the routing for the tow wings and all the extra equipment needed for master quad control and mixes and all the extra equipment.

and all the extra equipment needed for master quad control and mix down into four or two track. This is dealt with in Section B of the In-struction Manual.

Using an extra stereo cross-over each wing can drive a quadraphonic P.A. system



GENERAL SPECIFICATION

GENERAL SPECIFICATION The 30/30 Mixer is divided into four parts. A Centre Desk contain-ing Routing, Foldback. Monitor, Talkback. Echo & Cueing Combiner. Oscillator and Master Quad and Pan facilities with 4 Master Faders. There also can be built-in remote control facilities for Doiby's Machine Control and Auto Tape Locators. The Centre Desk has 4 group out-puts. 4 machine inputs, two foldback outputs and 4 monitor outputs also group break. "In and out" facilities. There are also sockets to connect this desk to the two wings and a plug for the power supply. Two input wings which are mirror images, and contain 15 input

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modules, which have input trim and equalisation, also facilities which enable the module to supply a line level drive for a tape machine with or without equalisation also 4 group outputs which may be combined by switches to be used as quadraphonic output or a pan output. There are facilities for 2 monitor or effects outputs and one echo

The module has a switch which controls the output to group. off or cue

There is also a switch which enables a break socket on the rear There is also a switch which enables a break socket on the real panel for effects drive and inputs to be switched in and out The fourth unit is the power supply which powers the Centre Desk and two wings and provides a 48 volts Phantom Microphone supply to the thirty microphone inputs. 20 KG approx.

101 x 82 x 41 cm. approx. 120 Kg. approx. 100 Kg. approx. 500 watts 600 or 1200 ohms, Balanced 600 ohms, Balanced

- 60 dbm - 60 dbm 0 dbm + 10 dbm PA 0 dbm Machine 300 milliwatts + 10 dbm + 10 dbm + 10 dbm



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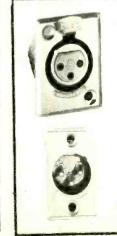
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a105

KELLNER-ELECTRONIC KG—BERLIN PRESENT electronic construction kits

SOLE DISTRIBUTORS IN THE UNITED KINGDOM A. MARSHALL & SON [LONDON] LTD. 42 CRICKLEWOOD BROADWAY, LONDON, NW2 Telephone: 01-452 0161/2/3

AMPLIFIERS

- VV1 —A simple pre-amp kit—suitable for crystal receivers, microphones etc. Price **£1**·93. P & P 20p.
- EV3 —Distortion compensated pre-amp in accordance with R.I.A.A. standards. Operating voltage: 20 volts. Current consumption approx. 1mA. Amplification factor: approx. 50db. Imput impedance: 50k ohm. Frequency response: 20Hz-40kHz. Price: £4.00. P & P 25p.
- ES3 —3 watt amplifier kit. Suitable for record players etc. Price: £3 70. P & P 20p.
- ES15—15 watt Hi-Fi amplifier kit. Two of these for an excellent stereo set. Complete with tone control network and pre-amp. Operating voltage: 30V. Max power output: 20w. Input sensitivity: 250mV with pick up. Output impedance: 4 ohm. Tone control range: Bass ±20db. Treble ±20db Price: £11.94. P & P 25p.
- ES30—30 watt Hi-Fi power amplifier kit. Can be used with most pre-amp kits. Price: £8-32. P & P 25p
- ES50—50 watt Hi-Fi power amplifier kit. A higher output version of the ES30. Price: £9 53. P & P 25p.
- AV7—An aerial amplifier kit. Connected between your aerial and receiver becomes a noise free signal booster. Operates on LW, MW, SW, VHF and T/V Channels 2-12. Requires 4-12V. Current consumptin: 2mA.
 2-25db amplification factor—input impedance 50-80 ohms. Price: £1-83. P & P 20p.

LIGHT SHOWS

LO350—A 3 channel light show construction kit. Split the output from your amplifier into 3 coloured light channels, that blend and synchronize with your favourite mood music. Maximum load per channel 500w. Operating voltage: 6 volts. Price: £13-50. P & P 20p.

LO1000—A one channel Light show module. Needs only 220V a.c. and up to a 1000 watts of lighting to translate your favourite record into synchronized light.

Price: £7.00. P & P 20p.

ST800—Strobe light constuction kit. Transform your room into a discotheque with this 120w strobe. Very bright and efficient. Operating volts: 220 V a.c. Price: £7·11. P & P 20p.

DIGITAL CLOCK

HE723—Digital clock construction kit. An extremely accurate electronic digital clock using 15 integrated circuits and one power transistor. The reference frequency is in fact 50Hz mains frequency which is an extremely accurate reference source. The estimated loss is about two seconds per year. All construction components are included and a comprehensive fault finding chart is included in the instruction booklet. The clock can be reset at any time by a push button to compensate for power cuts etc. Price: £32.58. P & P 60p.

RECEIVERS

- MUE7 A very sensitive miniature short wave and VHF receiver kit. Frequency range 25mHz to 150mHz. Uses standard batteries—7·5-12 volts. The ideal companion for kit no. UHS 70 or used on its own for short wave and VHF listening. Will drive a loudspeaker if used with kits ES2 or ES3. Price: £2·93. P & P 20p.
- WT7 Aircraft communications tuner. Connect this tuner to your medium wave radio and receive aircraft, airports and weather stations etc. Listen to pilot to control room "talk down". Hours of entertainment. Ready assembled and aligned. Price: £14.00. P & P 40p.
- DE6 Crystal set receiver construction kit. Needs only aerial and earth to operate as a superb medium wave receiver. Requires no batteries. Can be used as a noise free tape tuner. Price: £2:28. P & P 20p.

GAMES F

EW18: Electronic Dice Construction kit. Play your games the electronic way. Uses latest integrated circuit Gives random counts from one to six. Battery operated. Price £5.91. P & P 20p.

EW20: A similar kit to the above EW18. This has a proximity touch button for easier operation. Simulates the rolling of a dice. 6 volt operation current consumption: 150mA. Price: £6.64. P & P 20p.

TV2: Telephone amplifier klt. uses induction coil which is fused to back of telephone. Output 2w into 4ohms. Battery operated. Price: £5-54. P & P 30p.

POWER SUPPLIES

NT15: Mains power supply kit. 4 to 30 volts out. max power output 1-5w. Hum voltage under load: 30mV. without load. 5mVss. internal resistance less than 10ohms. Price £6-75. P & P 60p.

NT85: Mains power supply kit. 5 to 70 volts out. electronically stablised with short circuit proof facilities. Output current 1-2 amps. max power output 60W. A valuable asset to any home constructors workshop. Price £11.34. P & P 80p.

TRANSMITTERS

UHS70. An FM transmitter kit. Frequency range: 65-145mHz. Complete with microphone pre-amp. Used with your FM radio set or kit No. MUE7, as a very sensitive radio microphone. Uses standard batteries. Range about half a mile. Price £2.52 P & P 20p. A G.P.O. License is required.

W29. Emitter VFO for 2 meter band. 144-146 VFO incorporating FM modulator. 12 volts built and aligned. Price £14-00. P & P 40p.

ALARMS

- SL12. An ear piercing electronic siren kit. needs only a speaker and a 6-12 volt battery. Ideal for use in a home burglar alarm system. Price: £3-50. P & P 25p
- LS30. Light barrier construction kit. Can be used in a burglar alarm system or as a parking light switch etc. An extremely efficient photo-cell system. Price: £6.64. P & P 20p.

BG1. A 6 volt light blinker kit. Can be used in warning light systems etc. Price £1·18. P & P 20p.

D800. 800 watt light and drill speed control kit. For light dimming and light duty drill speed control. Price £2.70. P & P 20p.

NF10. LF generator construction kit. A useful 1000Hz test generator. 12 volt operation. Price: £3.91. P & P 20p.

KL150. A tone control kit used with a pre-amp to give a wide variation of tone frequencies, uses a modern integrated circuit. Price: £4.07. P & P 25p.

All prices are plus 10% VAT and plus Post and Packing.

 Text From X. 199 collisators with T 4.5. Stra And North 2, Subject 2005, Park 199, Park 1	Vo			
£50. · 150 ba.	plug-in £220; with CA plug-in £280. TEKTRONIX 538 Oscilloscope with T & CA plug-ins £285. TEKTRONIX TIME MARKERS type 181 £35. ROHDE & SCHWARZ SYNTHESIZER Model BN 44462, 30 HZ to 30 MHZ. Size 30 × 23 × 17in. MUST GO. £175. ROHDE & SCHWARZ VIDEOSCOPE BN 424101/2 £650. ROHDE & SCHWARZ Analyser BN 48302 £173. AMERICAN SWEEP GENERATOR type 422. Covers from 5 to 100 MHZ. Has built in dipley and 101 DB Push Button RF Attenua- tonin one DB staps. plus Calibrated Markor 642. Covers from 5 to 100 MHZ. Has built in dipley and 101 DB Push Button RF Attenua- tonin one DB staps. plus Calibrated Markor 643. Covers from 5 to 100 MHZ. Has built in dipley and 101 DB Push Button RF Attenua- tonin one DB staps. plus Calibrated Markor 644. Carriage £1-50. AMERICAN SWEEP GENERATOR type TRM 315 to 400 MHZ. £300. AMERICAN POWER UNITS STANDARD 250 90 HZ Input 284 40 AMP OUTPUT. Size 22 × 16 × 9in. Supplied in original transit case £25. AMERICAN AM GENERATOR type 497. 4 to 400 MHZ. Supplied with leads, etc., for 240V 50 HZ Input 284 40 AMP OUTPUT. Size 22 × 16 × 9in. Supplied in original transit case £25. AMERICAN AM GENERATOR type 497. 4 to 400 MHZ. Supplied with leads, etc., for 240V 50 HZ Operation £35. SPECIAL 40 MHZ SCOPE SOLARTRON CD1212 ONLY £30. Has to be a snag. There IS-100 nanosecs per cm. to 5 sca. per cm. In 24 calibrated ranges. 20 nanosecs per cm.	must go £723. MARCONI TF 801A AM GENERATOR 10 to 310 MHZ 545. MARCONI TF 801B. AM SIGNAL GEN- ERATOR. 12 to 470 MHZ. In good working condition £90. MARCONI TF 938 (CT44). Absorption Wattmeter 10mW to 6 Watts, Input Impedance 2:5 ohns to 20K Ohms. Freq. response flat at 20KHZ. Calibrated in volts and dbs. 5in. mirror backed meter £9:50, P. 4. P. 750. MARCONI VVM TF 1041 £22:50. MARCONI VVM TF 1041 £22:50. MARCONI TF 428C. Measures AC 100MV to 150V 20HZ to 15 MHZ. Measures DC 40MV to 300V. Complete with probe. Standard 240V operation 212:50 each. MARCONI TF 899, Measures 20MV to 2V AC. 50 HZ to 100 MHZ. £10 each. MARCONI TF 899, Measures 20MV to 2V AC. 50 HZ to 100 MHZ. £10 each. MARCONI VVM TF 1300. Measures AC 50MV to 100V, 20 HZ to 300 MHZ. DC 100MV to 300V. Ohms 50 to 5 Meg Ohm. In fine con- dition £18 each. AVO TRANSISTOR AND OIODE TESTER TYPE CT 537. In superb condition, in original crates with full instructions, circuit diagram, etc. New price £250 Plus. OUR PRICE £40 ea. Car. £1:25. EDDYSTONE 770 U. UHF RECEIVER £80. RACAL RA17 RECEIVER from £230. SSB ADAPTOR for Racal RA 17 and RA117 £60 each. MODERN TELEPHONES type 706. Two tons grey, £3.75 ea. Two-tone green £3:75 ea. Black £2.75 es. P. AP. 250 ea. Also TOPAZE YELLOW £4.50 ea. P. & P. 250. Ideal EXTENSION Telephones with standard GPO type dial, bell and postage 370. MODERN TELEPHONES type 705. Two tons grey, £3.75 ea. Two-tone green £3:75 ea. Black £2.75 es. P. & P. 750. All telephones complete with bell and dial. POTENTIOMETERS COVERN 3 watt. Brand new, 5; 10; 25; 500 ohms; 1; 2:5; 50 k all at 13p ea. MORGANITE Special Brand new, 5; 10; 25; 500 ohms; 1; 2:5; 50 k all at 13p ea. BRADD ARD 2 meg. log pots. Current type	50k and 100K 50p ea. BOURNS TRIMPOT POTENTIOMETERS. 10; 20; 50; 100; 200; 500 ohma: 1; 2; 2:5; 5; 10; 10; 20; 50; 100; 200; 500 ohma: 1; 2; 2:5; 5; 10; 25k at 35p ea. ALL BRAND NEW. RELIANCE P.C.B. mounting: 270; 470; 500 ohma; 10K at 35p ea. ALL BRAND NEW. ALMA precision resistors 200K; 400K; 497K; 908K; 1 meg-0:1% 27p ea.; 3:25k, 5:6k, 13k- 0:1% 20p ea. Diff Composition resistors 200K; 400K; 497K; 908K; 1 meg-0:1% 27p ea.; 3:25k, 5:6k, 13k- 0:1% 20p ea. Diff Composition resistors 200K; 400K; 497K; 908K; 1 meg-0:1% 27p ea.; 3:25k, 5:6k, 13k- 0:1% 20p ea. Diff Composition resistors 200K; 400K; 497K; 909 ca. 100 off	 P.C.B. PACK S & D. Quantity 2 sq. ft.—no tiny pieces. 50p plue P. & P. 20p. FIBRE GLASS as above £1 plus P. & P. 20p. S CRYSTALS 70 to 90kHz. Our choice, 25p. P. & P. 15p. MOTOR, min. synchronous, size 14 × 2 × 8in., 240V Operation 3.6 rpm, 25p each. P. & P. 5p. TRIMMER PACK, 2 Twin 50/200 pt ceramic; 2 twin 10/80 pf ceramic; 2 min strips with 4 preset 5/20 pf on ecramic; 2 min strips with 4 preset 5/20 pf on ecramic; base. ALL BRAND NEW 25p the LOT. P. & P. 10p. FLAT FACED 4" Twin Beam Tube. Type CV2133. Green Trace. Brand New. £4 each. P. & P. 5p. GRATICULES. 12 cm. by 14 cm. in High Quality plastic. 15p each. P. & P. 5p. PANEL mounting lamp holders. Red or green. 5p ea. Miniature. PANEL mounting lamp with holders—10V 15MA 5p ea. ELECTROSTATIC VOLTMETERS from 0.500 volts to 0-10KV. S.A.E. with your requirements. FIBRE GLASS PRINTED CIRCUIT BOARD. Brand new. Single sided up to 24 wide × 15" ip per sq. in. Larger pieces 1p per sq. in. Double sided. Any size 1p per sq. in. Postage 10p per order. INTEGRATED CIRCUIT test clip by AP Inc. Conjete with acutheon. Birad New Individually boxed. £1:00 ea. P. 4.P. 10p. DECADE DIAL UP SWITCH-5 DIGIT. Complete with acutheon. Bisck with windividually boxed. £1:00 ea. P. 4.P. 10p. DECADE DIAL UP SWITCH-5 DIGIT. Complete with acutheon. Bisck with windividually boxed. £1:00 ea. P. 4.P. 10p. DECADE DIAL UP SWITCH-5 DIGIT. Complete with acutheon. Bisck with with Plan. deep. Ex-Plessey. £1:40 each. P. 4.P. 15p. FIVE moving coll meters £2 P. 4.P. 37p. VISCONOL EHT CAPACITORS Size 1 × 22 ins. 0.05mid 2 :5KV 40p ea. 0.05mid 2 : 5KV 40p ea. 0.05mid 3 : 5KV 40p ea. 0.05mid 3 : 5KV 40p ea. 0.05mid 3 : 5KV 40p ea. 0.05
MAKE YOUR SINGLE BEAM SCOPE INTO A DOUBLE WITH SINE AND SQUARE WAVE GENERATOR		SCOPE INTO A DOUBLE WITH		

OUR NEW LOW PRICED SOLID STATE SWITCH. 2 HZ to 8 MHZ. Hook up a 9 volt battery and connect to your scope and have two traces for ONLY £5.50. P. & P. 25p. STILL AVAILABLE our 20 MHZ version at £9.25, P. & P. 25p.

TRANSISTOR INVERTER

12V to 1.5 KV 2MA. Size $1\frac{1}{2} \times 2\frac{1}{2} \times 4$ in. Multi tapped secondary and output level control makes possible large range of voltage and current output combinations without modification. Very flexible unit at £2.95 each. P. & P. 25p.

6V max square outputs. Completely assembled P.C. Board, ready to use. 9 to 12V supply required. £7.85 each. P & P 25p. Sine Wave only £5.85 each. P & P 25p.

In four ranges. Wien bridge oscillator thermistor stablised. Separate

independent sine and square wave amplitude controls. 3V max sine,

NEW WIDE RANGE WOBBULATOR

5 MHZ to 150 MHZ (Useful harmonics up to 1.5 GMZ) up to 15 MHZ sweep width. Only 3 controls, preset RF level, sweep width and frequency. Ideal for 10.7 or TV IF alignment, filters, receivers. Can be used with any general purpose scope. Full instructions supplied. Connect 6:3V AC and use within minutes of receiving. All this for only £5.75. P. & P. 25p. Suitable miniature transformer for 240 Volt operation £1.25.

Unless stated-please add £1.50 carriage to all units.

VALUE ADDED TAX not included in prices-please add 10%

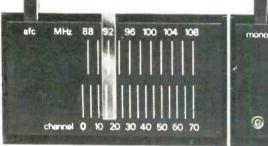
Official Orders Welcomed, Gov./Educational Depts., Authorities, etc., otherwise Cash with Order

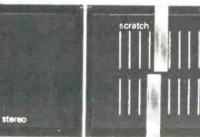
Open 9 am to 6.30 pm any day (later by arrangement.)



www.americanradiohistory.com









Project 80 tuner

Project 80 Active Filter Unit (AFU)

the slimmest, most elegant hi-fi modules ever made

Stereo decoder



Living with hi-fi takes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round; their size and presentation bring exciting new opportunities to install systems in ways hitherto only dreamed about but never before made practical. You can build a Project 80 system virtually anywhere and it is unbelievably simple to install and connect up. Everything that could possibly be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project 80 – compactness, elegantly ultra-modern styling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just a few examples of the system's fantastic versatility.

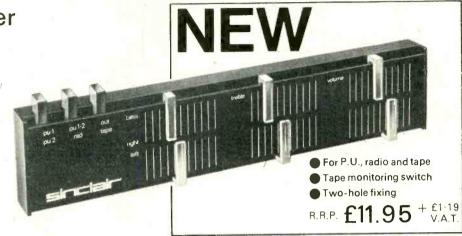


WW-097 FOR FURTHER DETAILS

Project 80 new modules

Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes drilled in the wood or plastic on which modules are to be mounted. All the electronics are contained within the 34 deep front panel! Connecting leads are taken away similarly out of sight. Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders. This enables exceptionally good environmental matching to be obtained. Provision is made for magnetic and ceramic pick-ups, radio and tape in and out. A virtual earth input stage forms part of the up-dated circuitry of the Stereo 80 to ensure the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied.



TECHNICAL SPECIFICATIONS

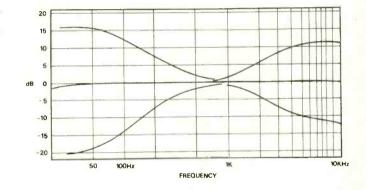
Size $-260 \times 50 \times 20$ mm ($10\frac{1}{2} \times 2 \times \frac{3}{2}$ ins) Finish - Black, with white markings

Inputs – Mag. P.U. 3mV RIAA corrected; Ceramic P.U. 300 mV Radio 300 mV; Tape 30 mV S/N ratio - 60db

Frequency range - 20Hz to 15KHz±1dB: 10Hz to 25KHz±3dB Power requirements - 20 to 35 volts

Outputs - 100mV+AB monitoring for tape

Controls - Press button for tape, radio and P.U. selection Volume, Bass+12dBto-14dB at 100Hz; Treble+11dB to-12dB at 10KHz



Project 80 FM tuner smaller, more efficient

A truly remarkable tuner in every way - its unbelievably compact size its original circuitry - its dependable performance - all this in a boldly designed modern case measuring $85 \times 50 \times 20$ mm ($3\frac{1}{2} \times 2 \times \frac{3}{4}$ ins) Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made available separately.

TECHNICAL SPECIFICATIONS

Size – $85 \times 50 \times 20$ mm (approx. $3\frac{1}{2} \times 2 \times \frac{3}{2}$ ins) Tuning range - 87 to 108 MHz Detector - I.C. balanced coincidence, for good A.M. rejection AFC - Switchable, with thermistor control to prevent from drift One 26 transistor I.C Twin dual varicap tuning Distortion - 0.3% at 1KHz for 75KHz deviation Ceramic filter in I.F. section Aerial impedance – 75 Ω or 240-300 Ω Sensitivity - 4 microvolts for 30dB quieting Power requirements - 12 to 45 volts



Making the Project 80 decoder separate from the F.M. tuner gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required. This unit gives a 40dB channel separation with an output of 150mV per channel. The gallium arsenide light emitting beacon automatically lights up to show when a stereo transmission is tuned in. Designed essentially as an integral part of Project 80 systems, this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception.

Size $-47 \times 50 \times 20$ mm (1 $\frac{1}{4} \times 2 \times \frac{1}{2}$ ins) One 19 transistor I.C.



new constructional techniques

...and again Sinclair leads the world

- 1962 Micro-miniature power amp small enough to stand on a 10p. piece. Slimline pocket receiver smaller than a 20 cigarette pack
- 1963 Micro-6 receiver, smaller than a matchbox
- 1964 Pocket F.M. receiver; PWM amp.
- 1965 Z.12 power amplifier module; PZ.3 power supply
- 1966 Stereo 25 pre-amp/control unit
- 1967 Micromatic: Q.14 loudspeaker; the first Neoteric
- 1968 IC.10, the first ever integrated circuit for constructors' use

Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80, separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment.

TECHNICAL SPECIFICATIONS

 $\begin{array}{l} \text{Size} = 108 \times 50 \times 20 \text{mm} \; (4 \frac{1}{2} \times 2 \times \frac{3}{4} \text{ins}) \\ \text{Voltage gain} = \text{minus} \; 0.2 \text{dB} \\ \text{Frequency response} = 36 \text{Hz} \; \text{to} \; 22 \text{KHz}, \; \text{controls minimum} \\ \text{Distortion} = \text{at} \; 1 \text{KHz} = 0.03\% \; \text{using} \; 30 \text{V} \; \text{supply} \\ \text{HF cut off (scratch)} = 22 \text{KHz} \; \text{to} \; 5.5 \text{KHz}, \; 12 \text{dB/oct. slope} \\ \text{L.F. cut off (rumble)} = 28 \text{dB} \; \text{at} \; 20 \text{Hz}, \; 9 \text{dB/oct. slope} \end{array}$

Z.40 & Z.60 power amplifiers totally short-circuit proof

Either of these entirely new power amplifiers is intended for use in Project 80 installations although, of course, they are readily adaptable to an even wider range of applications. Both Z.40 and Z.60 incorporate builtin protection against shortcruiting and risk of damage arising from mis-use is greatly reduced. Comprehensive instructions are supplied with each of the modules.

Z.40 Technical Specifications Size $-55 \times 80 \times 20$ mm $(2\frac{1}{8} \times 3\frac{1}{8} \times \frac{3}{8})$ 9 transistors Input sensitivity -100mV Output -15 watts RMS continuous into 8 Ω (35V). 30 watts music power into 4 Ω (30V) Frequency response -10Hz– 100KHz ± 1 dB Signal to noise ratio -64dB Distortion -at 10 watts into 8 Ω less than 0.1% Z 60 Technical Specifications Size $-55 \times 98 \times 20mm$ $(2\frac{1}{8} \times 3\frac{3}{4} \times 3\frac{1}{10})$ 12 transistors Input sensitivity -100-250mVOutput -25 watts RMS into 8 Ω (45V). 50 watts music power into 4 Ω (50V) Distortion - typically 0.03% Frequency response -10Hz to more than 200KHz $\pm 1dB$ Signal to noise ratio - better than 70dB Built-in protection against

transient overload and short circuit Load impedance – 4Ωmin: max. safe on open circuit

Sinclair power supply units PZ.8

the worlds most advanced unit in its class

Stabilised power supply unit. Reentrant current limiting makes damage from overload or even direct shorting impossible, a principle never before inorporated in a commercially available constructor module. Normal working voltage (adjustable) 45V. R.R.P. £7.98+0.79p V.A.T. Without mains transformer PZ.5 30V unstabilised R.R.P. £4.98+0.49p V.A.T.

R.R.P. £4.98+0.49p V.A.T. PZ.6 35V. stabilised R.R.P. £7.98+0.79p V.A.T.



LONDON RD., ST. IVES, HUNTINGDONSHIRE PE17 4HJ Reg. No. 699483 England

- 1969 Q.16 improved version of Q.14: Systems 2000 and 3000: Project 60 launched
- 1970 IC.12: Project 605
- 1971 Project 60 stereo FM tuner: Z.50: PZ.8
- 1972 Improvements to Project 60 with Z.50 MK.2 and PZ.8 Mk.3 The Executive Calculator: Digital multi-meter: Q.30 speaker:
- 1973 Cambridge Calculator: PROJECT 80 LAUNCHED

...and next?





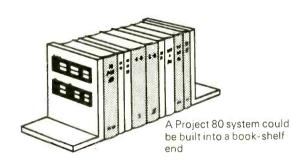
Recommended Project 80 applications

System	The Units to use	Units cost
Simple battery record player	Z. <mark>40</mark>	£5.45 +54p V.A.T.
Mains powered record player	Z.40, PZ.5	£10.43 +£1.04 V.A.T.
30W. RMS continuous sine wave stereo amp.	2×Z.40s, Stereo 80; PZ.6	£30.83 +£3.08 V.A.T
50W (8 Ω) RMS continuous sine wave de luxe stereo amp	2× Z.60s, Stereo 80; PZ.8	£33.83 +£3.38 V.A.T
Indoor P.A.	Z.60, PZ.8	£14.93 +£1.49 V.A T.
Car Radio	F.M. tuner, Z.40	£16.40 +£1.64 V.A.T.

F M Tuner, Decoder and A.F.U. may be added as required. WW---098 FOR FURTHER DETAILS

From Sinclair the worlds most advanced hi-fi modules

Sinclair Project 80 the ultra-modern non-obtrusive hi-fi





The modules mount very easily onto a playing plinth

A novel application would be to build around the base of a lampshade



Project 80 could be easily mounted onto a loudspeaker cabinet



Two Sinclair Q.16 loudspeakers suitably positioned together with Project 80 could be mounted on to a false wall.

A 23* strip along the edge

a shelf could be sufficient

to contain a complete

system

When you have seen for yourself how fantastically slim and cleverly designed these modules are, further ways will suggest themselves in which they can become a pleasing part of your particular domestic environment.

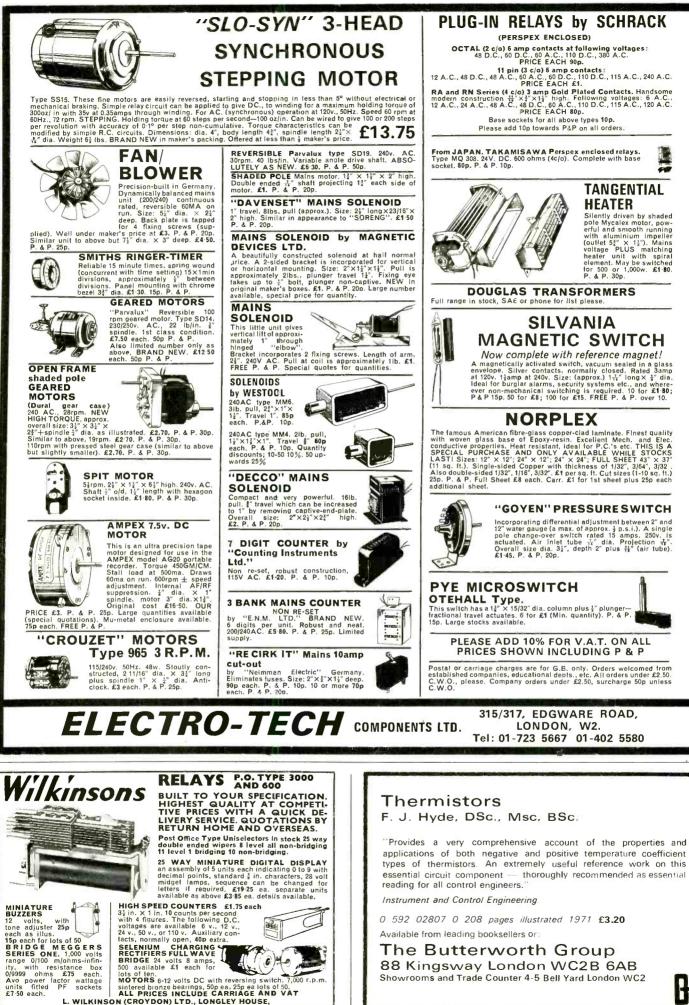
	AIR RADIONICS LTD. ST. IVES, HUNTINGDON PE	1748
Please se	nd post paid	
	1	
for which	I enclose Cash/Cheque for £including V.A.	Τ.
Name		
Address		

Guarantee

If, within 3 months of purchasing any product direct from us, you are dissatisfied with it, your money will be refunded on production of receipt of payment. Many Sinclair appointed Stockists also offer this guarantee.

Should any defect arise in normal use, we will service it without charge. For damage arising from mis-use a small charge (typically £1.00) will be made.

Sinclair Radionics Ltd. London Road, St. Ives, Huntingdon PE17 4HJ Telephone St. Ives (0480) 64311



88 Kingsway London WC2B 6AB Showrooms and Trade Counter 4-5 Bell Yard London WC2

T

L. WILKINSON (CROYDON) LTD., LONGLEY HOUSE, LONGLEY RD., CROYDON. CR0 3LH. Phone 01-684 0236. Grams: WILCO CROYDON

11

WW-120 FOR FURTHER DETAILS

des minides heart - It -



BEDFORD ELECTRONICS 7, PRIORY STREET. BEDFORD Colvern TEN TURN POTS. 500R. 5% Lin. 0.1%. £1.25 each. OSCILLOSCOPES POT CORES LA3. 40p each. CARD READER Data Products SPEEDREADER 300 Mechanism and Electronics P.O.A. each **POWER SUPPLIES** MILES HIVOLT TH25 Regulated EHT supply 100V. to 25kV. @ 1mA., voltage and current meter, overload protection. shift current metric v de final, rolitage AS NEW K150. MILES HIVOLT TH20 Similar to above buil 100V. to 20KV. @ 500uA., no meter. BRAND NEW £150. A E.I. R2202-5V to 30V @ 2A Regulated, fully adjustable supply voltage and current meters £7. Callers only. Many other L.T. & H.T. power supplies available, please inform us of your requirements. FULLY RECONDITIONED AND CALIBRATED TEST EQUIPMENT P.T.F.E.

7/0076 equipment wire to EL1930 Type A £2 per 100 yards. Please check colour and reei size availability before ordering. 51961

TEL.

MULTICORE CABLE, miniature, 35 cores of PVC 7/0076 screened overall and PVC sheathed. £2:50 for 10 yds.

PVC equipment wires from 7/0076 @ 50p/100 yds. to 70/0076 @ £1-50/100 yds. available. Colour range restricted.

Pressure transducers KDG, Type TD216. 0-1200 P.S.I. Complete with calibration chart. £5 each.

CARPENTERS polarised relay SPCO 2 x 1000R, complete with base and retainer as new. 45p each.

METERS, 3½in. diameter, sealed, 50-0-50 uA/1300R, £2:25 each. 1 mA/130R, £1:75

BALL RACES Type RCL F. Flanged in. bore 5/16in. dla. Sealed packs, 25p each.

PANEL FUSE HOLDERS with indicator lamp. The cap of these 14in. fuse holders is provided with an amber lens and min. flanged lampholder to allow a fuse failure neon to be fitted, bulb not included. 20p each.

CLEARANCE SALES of surplus equipment and components are held on equipment and components are held on the first Saturday of every month. NEXT SALE 3rd NOVEMBER 10am to 4pm

FLUID LOGIC teaching sets. These well made teaching aids contain the following components mounted on an engraved panel within a polished wooden box, 2 bistable, 1 and 3 or more logic elements, 2 press transmitters, 2 press receivers, 2 pressure regs. and gauges, 2 actuating cylinders and press. amplifiers, 4 position sensors. Suppiled complete with all accessories £37:50.



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DRILL CONTROLLER New 1kW model. Electronically changes speed from approximately 10 rev. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instruc-tions g1-65, puts 13p post and insurance. Made up model also available £2:48 plus 13p p. & p elity MIDCET

MIGHTY MIDGET Probably the finest possible radio, as described in Practical Wireless, January 73. All electronic parts £2.20 post paid. GOOD COMPANION I.C. VERSION



We can now offer these again in I.C. version using Fermuti ZN414 and Mullard AP Module 1172. Cabinet size approx. Illn. wide x 8in. high X 3in. deep. Complete assembly instructions, 26: 33 plus 257 post and ins. Excellent tone wood cabinet. I CHIP RADIO

Ferranti's latest device ZN414—gives results better than superhet. Supplied complete with technical notes and circuits £1:38 each. 10 for £11:11.

- Circuitz 21:39 calen. 10 107 21111.
 HI-Q TUNER COMPONENTS
 For experimenting with the ZN414
 Kit No. 1 Plessey Miniature Tuning Condenser with built in LW switch and 3m. Ferrit slab and litz wound MW coil 72p.
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- Kit No. 3
- wound MW and LW coils and wave exited 940. Air spaced TC with slow motion drive 8in. ferrit rod with litz wound LW and MW coils and wave change switch \$110. Permeability tuner with fast and slow motion drive and LW loading coils and wave change switch 50p. Kit No 4



Up. 12 VOLT 14 AMP POWER PACK This comprises double-wound 230/ 240V mains transformer with full wave rectifier and 2000 mf/d smoothing. Price £2:20, plus 20p post & packing. Duto t voltage adjustable

post & packing. Heavy Duty Mans Power Pack. Output voltage adjustable from 15-40V in steps maximum load 250W—that is from 6 amp at 40V to 15 amp at 15°. This really is a high power heavy duty unit with dozens of vorkahop uses. Output voltage adjustment is very quick—simply inter-change push on leads Bileon rectifiers and smoothing by 3,000mF. Price £6:33 plus 55p post.

MICRO SWITCH 5 amp changeover contacts, 11p each. 10 for 99p. 15 amp. 8.P Model 15p, changeover 17p. each



MAINS OPERATED SOLENOIDS

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D Solervoirs Model 772-small but powerful lin, pull — approx. size $1\frac{1}{2} \times 1\frac{1}{2}$ Model 4001/—jin. pull. Size $2\frac{1}{2} \times 2\frac{1}{2} \times 1\frac{1}{2}$ Size $3 \times 2\frac{1}{2} \times 2\frac{1}{2}$ Size $\frac{1}{2} \times 2\frac{1}{2} \times \frac{1}{2}$ Size post and insurance.

MAINS TRANSISTOR POWER PACK TAINS TRANSISTOR POWER PACK Designed to operate transistor sets and amplifiers. Adjust-able output 6v. 9v., 12 volts for up to 500 mÅ (class B wor-ing). Takes the place of any of the following bitteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit com-prises: mains transformer retifier, smoothing and load resistor condicensers and instructions. Real snip at only \$1.10 plus 20p postage.

00

TIME SWITCH Smith's mains driven clock with 15 amp switch, also notes showing how you can wake up with music playing, kettle boiling or come home to a warm house, warn off burglars, keep pets warm, halve your heating bill, etc. 69.95 £2.25

PRESSURE SWITCH Containing a 15 amp. change over switch operated by a diaphragm which in turn is operated by air pressure through a small metal tube. The operating pressure is ad-lustable but is set to operate in approx. 10in. of water. These are quite low pressure devices and can in fact be operated simply by blowing into the inlet tube. Original use was for washing machines to turn off water when tub has reached correct level but no doubt has many other applications. **21**:38. £1.38.

EDUCATIONAL KITS-all with pictorial instructions



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THYRISTOR LIGHT DIMMER



10 AMP DIMMER CONTROL IN AMP DIFIMER CONTROL For the control of lighting on stage or in a studio or for control of portable equipment in workshops, etc. This has two 1's amp socket outlets each is controlled by a 5 amp solid state regulator. The overall length is 17in., width 34in and depth 14in. In the end is fitted a master On/Of switch indicator, lamp and fuse. Price \$8,25.

STANDARD WAFER SWITCHES

Standard size	e 14in	wafer-	silver-pla	ted 5 a	mp. cor	tact, st	andard	in. spir	dle 2in.
Standard size long with 1 No. of Poles 1 pole 2 poles 3 poles 4 poles 5 poles 6 poles 7 poles 8 poles 9 poles 10 poles		wafer	silver-pla and nut 4 way 44p 44p 44p 77p 77p 77p 77p 77p \$1.04 \$1.04	5 way 44p 44p 77p 77p 77p 51.04 £1.04 £1.32 £1.32	6 way 44p 44p 77p 77p £1.04 £1.32 £1.32 £1.60 £1.60 £1.87	stact, st 8 way 44p 44p 77p 77p £1.04 £1.32 £1.60 £1.60 £1.60 £1.87	9 way 44p 44p 77p 77p £1.04 £1.04 £1.32 £1.60 £1.60 £1.60 £1.87	10 way 44p 77p £1.04 £1.32 £1.60 £1.87 £2.15 £2.42 £2.70 £3.00 £3.25	12 way 44p 77p £1.04 £1.32 £1.60 £1.87 £2.15 £2.42 £2.70 £3.00 £3.25
11 poles 12 poles	77p 77p	£1.04 £1.04	£1.04 £1.04	£1.32 £1.32	£1.87	£1.87	£1.87	£3.52	£3·52

TANGENTIAL HEATER UNIT

This heater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoorer and blover heaters coefficient £15 and more: We have a few only. Comprises motor, impeller, 2kW, element short likW, element allowing switching I, 2 and 3kW, and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only needs control switch. £3 55. 2kW, Model as above except 2kW. £2.75 Don't miss this. Control Switch 44p. plus VAT P. & F. 40-WALL THERMOSTATS

Don't miss this. Control Switch 44p. plus VAT P. & P. 40-WALL THERMOSTATS Made by the famous Smiths Instrument Co., called Colourstat. Wall mounting and in a hardnessme plastic case. (Gream and beige) Adjust-ationality of the state of the state of the state of the state of the around irrecting through to 50%. The slide panel is engraved and indicates (frost) (warm) (very warm) etc. The thermostat will control heaters etc. up to 15 arm path normal mains voltage and is ideal for living room, bedroom and greenhouses etc. Price **21**.65. Don't miss the

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this. **CENTRIFUGAL BLOWER** Ministure mains driven blower centrifugal type blower unit by Woods, powerdu but especially built for quiet running— driven by cuabloned induction motor with specially built low noise bearings. Orecral laize of blower is approx. $44^* \times 4^*$. When mounted by its flange air is blown into the equipment but to suck air out mount is from the centre using a claup, ideal for cooling electrical equipment, or fitting into a cooker hood, film drying cabinet or for removing flux smoke when soldering etc., etc. A real bargain at \$2.25.

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Easiest way to fanit find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio, TV, amplifier, anything—complete kit comprises two special transistors and all parts including project tube and crystal earpicce. $\pm 2:20$ —twin stethoset instead of earpicce 83p extra—post and ins. 20p.

-ELECTRIC TIME SWITCH

Made by Smiths these are A.C. mains operated. NOT CLOCKWORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. 2 completely adjustable time periods per 24 hours, 5 amp changeover contacts will switch circuit on or off during these periods. £2.75 post and ins., 23p. Additional time contacts 55p pair.

WINDSCREEN WIPER CONTROL Vary speed of your wiper to suit conditions. Al instructions to make. £2-48.

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molla form, each ready built complete with h sinks and connection tags, data supplied. Model 1153 500mW power output 272p. Model 1153 700mW power output 94p. Model EP90004 watt power output 91.60. EP9001 twin channel or stereo pre amp. £1.99. 10% discount if 10 or more ordered.



PAPST MOTORS Est. 1/40th h.p. Made for 110-120 volt working, but two of these work ideally together off our standard 240 volt mains. A really beautiful motor, extremely quiet running and reversible. £1.65 each. Postage one 23p, two 33p. 230v. model £3:30.

HORSTMANN 24-HOUR TIME SWITCH With 6 position programmer. When fitted to hot water syst stems this could

Heating

Hot Water	Central Heating
Off	no
Twice Daily	Off
All Day	Off
Twice Daily	Twice Daily
All Day	All Day
Continuously	Continuously
Continuousiy	

and hot eating Suitable of course, to programme other than central heating and water, for instance, programme updatisr and downstairs electric heat or heating and cooling or taped music and radio. In fact there is limit to the versatility of this Programmer. Mains operated. Size Sin. Sin. x 2in. deep. Price \$3 85 as illustrated but less case.

ZPM MODULATION MOTOR

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Could also be used to open ventilators, doors, valve, damper, etc. par-ticularly suitable for remote control. Made by Satchwell. Essentially a reversible geared motor fitted with internal limit switches to stop at to the suitable science. Size approx. 61n.x 61n.x 561n. and weighing approx 10 lb. An indicator on the motor graduated 0-10 shows the state of open or close. Also internally fitted is a variable resistor, wires from this to a volt meter would give a remote indication of the open or close position. Price complete with step down Transformer is £16 50.

Where postage is not stated then orders over £5 are post free. Below £5 add 30p. S.A.E. with enquiries please.



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AEKIAL with dashboard control switch—fully extendable to 40in or fully retract-able. Suitable for 12V positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. £6.35 plus 25p post and insurance.

AMPLIFIER IN CASE WITH

AMPLIFIER IN CASE WITH SPEAKER Marketed by British Relay under the name Luxistor. This is in a very neat looking cabinet and is ideal around the home or in the workshop for trouble shooting or for testing out a quick lash up. Size approx. $9\frac{1}{2} \times 6\frac{1}{4} \times 3\frac{1}{4}$ deep. Input is via a matching transformer and volume control and ampli-fier may be powered by an internal 9v battery or an external 110v source. Byeaker is an R-A eliptical 6^o x 34^o 10,000 gauss. The amplifier proper is a Newmarket model ref. P.C. 4. Price £3 85 each, 10 for £31^o50. Post and insurance 20p.



SWITCH TRIGGER MATS So thin is undetectable under carpet but will switch on with slightest pressure. For burgular alarms, shop doors, etc. 24" × 18" £1.54 13" × 10" £1.10

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RECORD PLAYBACK HEADS

RECORD PLAYBACK HEADS (TRUVOX) Individual prices of these are:— 2 track record playback heads 50p, each. 4 track record playback heads 72p each Brase heads are also available separately—2 track 33p— 4 track 55p. New metal mounting shields 39p each. 2 track-heads already fixed on heavy mounting plate with shield \$1.05.

eld £1:05. THERMOSTAT Continuoualy variable 30°-90°C. Has sensor bulk connected by 33in of fextble tubing On operation a 18 amp 250 vol: writch is opened and in addition a phrager moves through approx. Jin. This could be used to open valve on ventilator etc. £2:65 plus 23p p. & ins.



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All parts and

HIGH ACCURACY THERMOSTAT

HIGH ACCURACY THERMOSTAT Uses differential comparator 1.C with thermister as probe. Designer claims temperature control to within 1/7th of a degree. Complete kit with power pack £6 25. 6 DIGIT COUNTER Operated by 240v. A.C. mains through resident or direct from 115v. A.C. or from 80v. D.C. Made by setter-Rootf America. Metal encased for surface mounting. Size approx. 3½ × 1½ × 2½ in. Price £110 each. 10 for £9 90.

6 DIGIT COUNTER Resettable. 440 ohm coil up to 25 im-pulses per second. Ex-equipment but guaranteed perfect. £2:20 each.





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SPRING COIL LEADS As fitted to telephones, 4 core 17p each 10 for £1.53. 3 core 11p each. 10 for £1

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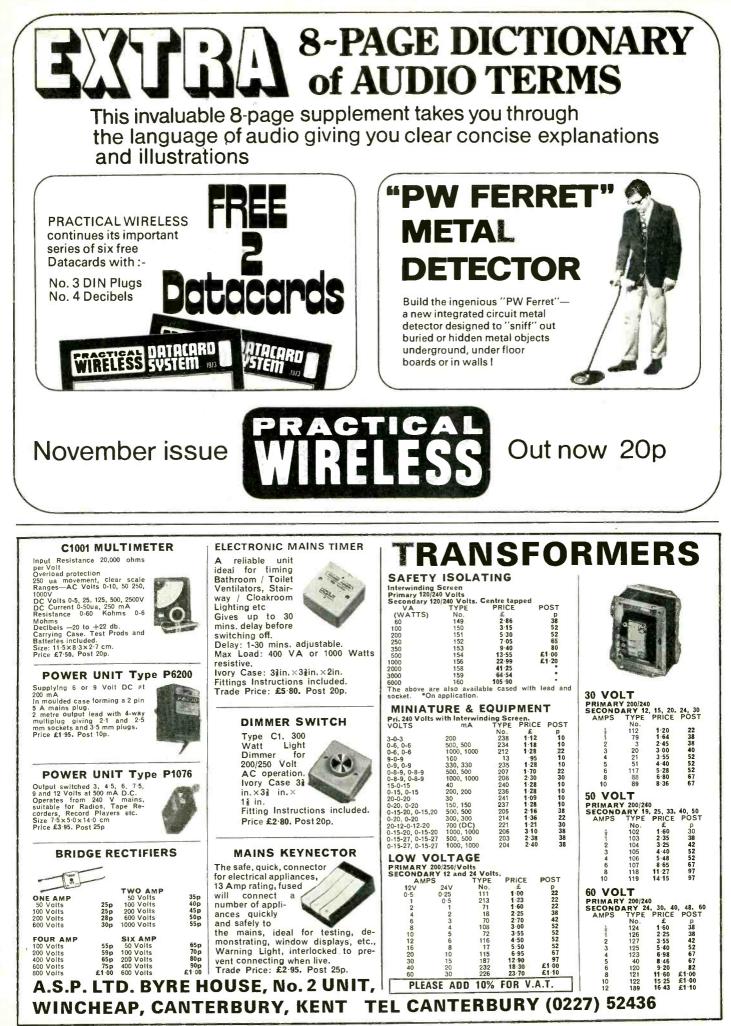
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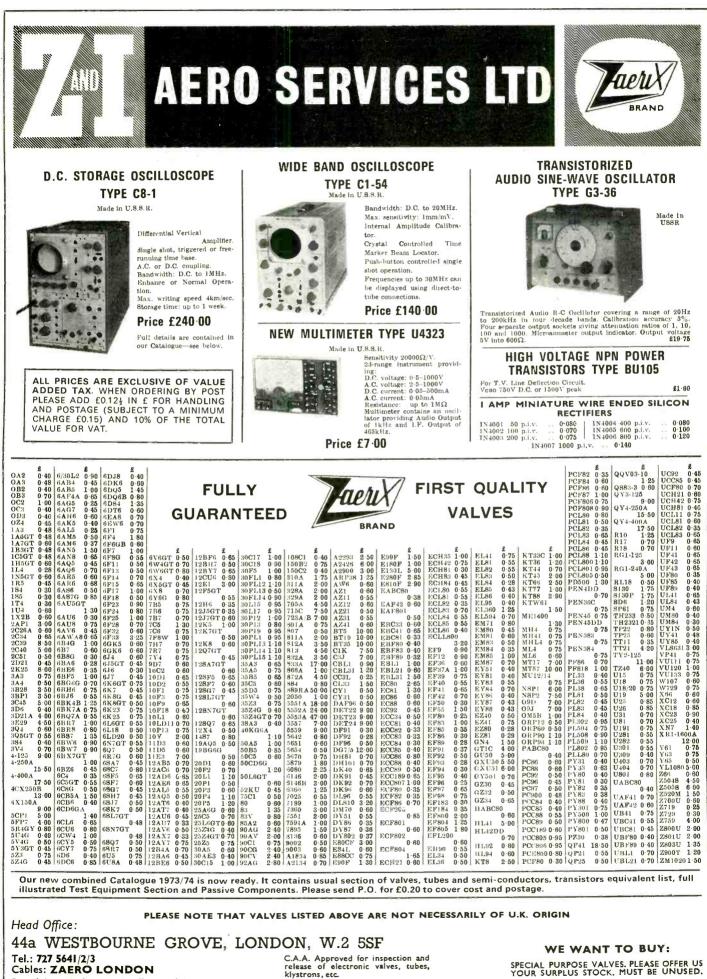
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J. BULL (ELECTRICAL) LTD.

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 for operating straight or circular tubes for shop windows, pelmet lighting etc. Each kit comprises first quality starter, tube ends, starter holder and two terry ellps to hold the tube, and circuit diagram.
 For miniature tubes, 4, 6, 8w. our Ref. PL AUI £1:38. For miniature tubes, 30, 128.
 For Autor and two terry ellps to hold the tube, and circuit diagram.
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 WHITE ROCKER SWITCHES
 Four types available, all snap in fixing through oblong hole approx 1in. x 4; in., all rated at 10 amps A.C All have white rocker except 53, which is amber.
 Our Ref. RS 51, push to make, spring return, 14p. Our Ref. RS 82, push to break, spring return, 14p. Our Ref. RS 83, push to make, spring return, 14p. Our Ref. RS 84, change over contacts, normal rocker, 26p.





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APPOINTMENTS VACANT

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Advertisement accepted up to 12 noon Thursday, November 8th for the December issue subject to space being available.

HER MAJESTY'S GOVERNMENT COMMUNICATIONS CENTRE HANSLOPE PARK, MILTON KEYNES, MK19 7BH,

has vacancies in the following fields of work

- (a) Microwaves
- (b) HF Communications
- (c) VHF/UHF Communications
- (d) Acoustics

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- (e) General Electronic Circuit Design
- Posts (a)-(f) are at Hanslope Park but posts (g) will be in London Area.

Appointments will be made within the grades of Scientific Officer, Higher Scientific Officer and Senior Scientific Officer in accordance with the following definitions:

SCIENTIFIC OFFICER

Applicants should be not more than 27 years of age and should have one of the following qualifications:

- (a) A degree in a scientific or engineering subject
- (b) Degree-standard membership of a Professional Institution
- A Higher National Certificate or (c) Higher National Diploma in scientific or engineering subject
- (d) A qualification equivalent to (c) above.

Salary Scales: £1318-£2177 with the entry point determined by qualifications and experience.

Applications stating the field of work and grade required should be made to:

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Applicants should be under 30 years of age but this requirement may be waived if special qualifications or experience can be offered. Formal qualifications are the same as for Scientific Officer above but in addition the following experience is required:

- (a) Applicants with 1st or 2nd class honours degrees-at least 2 years post-graduate experience
- experience.

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ADMINISTRATION OFFICER, HM GOVERNMENT COMMUNICATIONS CENTRE, HANSLOPE PARK,

HANSLOPE

MILTON KEYNES, MK19 7BH.

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(f) Design and development of small mechanisms

(g) Operational Analysis. For these posts applicants should be experienced scientists/engineers who have moved into Operational Analysis rather than the inverse.

> Applicants should be at least 25 and under 32 years of age, although the upper age limit may be waived if experience of special value can be offered.

> Applicants should have obtained a 1st or 2nd class honours degree and have had a minimum of four years appropriate postgraduate experience.

> Scale: £2615-£3640. Entry will Salary normally be at the minimum of the scale but applicants with experience of special value may be entered above the minimum.

> > [3127

FIELD SERVICE ENGINEERS

Applications are invited from men who like working with the minimum of supervision and who have self discipline to make effective use of their time.

Preference will be given to those living in North London with experience of Public Address and Sound Systems. A clean driving licence is essential. Apply by letter or telephone to:

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APPOINTMENTS

Advanced Communications...

Radio Equipment Design and Development



PLESSEY HAVANT (S. Coast/Hants/Sussex Borders)

Experienced Radio Engineers

Continued expansion of radio communications business in Plessey Avionics & Communications calls for engineers with some experience in the design of equipment for mobile and static applications to lead small and large teams at Plessey, Havant.

The laboratories are situated in the grounds of a country house, three miles from Chichester Harbour and close to the South Downs and several seaside resorts. The area is well placed for housing, shopping, schools, sailing, golf, flying and other recreational and cultural facilities.

A policy of controlled expansion ensures real opportunities for individual career promotion and high levels of job satisfaction.

We offer excellent salaries, conditions of employment, fringe benefits, generous relocation expenses and a stimulating environment.

If you have two or more years' experience in any of the following techniques:-

HF, VHF or UHF Medium Power Transmitter Design HF, VHF or UHF Receiver Design MODEMS Design - Digital and Analogue Digital Synthesisers RF Signal Switching Techniques Mobile Environment Equipment Design Radio Communications System Design

---and if you have academic qualifications equivalent to a university degree or membership of a professional institution,

Fill in the coupon or ring Havant (0701 2) 6391 Extension 200, and we will be happy to consider you for a range of appointments carrying salaries of up to $\pounds 4,000$ p.a. There are also opportunities for engineers with lesser experience or qualifications to take up other appointments.

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To: L. Wise, Manpower Manager, The Plessey Comp Hants.	pany Limited, Martin Road, West Leigh, Havant,
Please send me, in confidence, an application form and	l details of Radio Opportunities.
Name	Age
Address	Home telephone no.
Qualifications	
Areas of interest	ECCEV

There is scope, variety and responsibility as a

Radio Technician

Join the National Air Traffic Services of the Civil Aviation Authority as a Radio Technician and you have the prospect of a steadily developing career in a demanding and ever expanding field.

ENTRANCE QUALIFICATIONS You should be 19 or over, with at *least one year's practical experience in telecommunications.* Preference will be given to those having ONC or qualifications in Telecommunications.

Once appointed and trained, you will be doing varied and vital work on some of the world's most advanced equipment including computers, radar and data extraction, automatic landing systems, communications and closed circuit television.

Vacancies exist at locations near London (Heathrow), London (Gatwick) and Stansted Airports and for suitably qualified people at the Signals Training Establishment, Milton Keynes, Bucks.

Salary: £1383 (at 19) to £1836 (at 25 or over); scale maximum £2158 (higher rates at Heathrow). Some posts attract shift-duty payments. Promotion prospects are excellent and ample opportunity and assistance is given to study for higher qualifications.

To: Arthur Robert F. Simor Traffic Services, S.T.E. (Re Bletchley Park, Bletchley,	ecruitment),
Please send me applicati entry as Radio Technicia	
Name	
Address	
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onal Air Traffic Services	

RANK RADIO INTERNATIONAL

ENGINEERING OPPORTUNITIES

We are manufacturers of the famous range of Leak and Wharfedale Hi-Fi products which include the Design Centre Award Winning Isodynamic Headphones.

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These opportunities in the Acoustics Engineering Development Division include:

Development Engineers — Branded Products Headphones

Advanced Development

Vacancies are also available for Circuit Engineers and Production Methods Engineers.

Candidates should ideally have had some experience or interest in $\ensuremath{\mathsf{Hi}}\xspace{-}\ensuremath{\mathsf{Fi}}\xspace{-}\x$

To obtain a job description and further details, salaries etc. for any of the positions mentioned will you please apply in writing giving brief details of your educational qualifications, career to date and current salary to:



Mr. J. R. Murgatroyd. Personnel Officer, Rank Radio International. Bradford Road, Idle,

BRADFORD BD10 8SF 3169

RANK RADIO INTERNATIONAL

SPANISH FIRM NEAR MADRID

is looking for design and development engineers with a minimum of three years of experience in the field of P.C.M. equipment to be used by the telephone industry.

Areas of interest are encoders and decoders, P.C.M. multiplexers and R.F. equipment to transmit P.C.M. data. Salary open.

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Fernando el Católico, 63 Madrid 15 SPAIN

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APPOINTMENTS



The continual expansion in all aspects of life in Zambia presents vacancies for qualified personnel. All the posts

Ministry of Power, Transport and Works Post Office

Equipment Technician

(Various)

For maintenance and installation work. Applicants should have minimum 4 years experience with Telecommunications Administration and City & Guild's final certificate in Telecommunications or equivalent. Applicants from British Post Office will be taken at Technical Officer grade. Should have held a current driving licence for 2 years for driving Government transport.

Supervising Line Technician

To control staff and labour on overhead line, underground development and maintenance work. Supervise and test; also all necessary duties to maintain services anywhere in Zambia. Applicants ideally under 45 years of age with minimum 10 years Telecommunications external experience, including overhead line and underground cable construction knowledge.

Assistant Telecommunications Engineer (Power & Accommodation)

Applicants should hold Intermediate City & Guild's Certificate in Telecommunications or equivalent. Also have equal grade of Assistant Executive Engineer or Technical Officer (A) in British Post Office and a current driving licence. To work on design of telecommunications buildings, air-conditioning systems, provision of mains and stand-by power supplies. Preparation of specifications and engineering instruction.

Telecommunications Engineer (H. F. Radio)

With minimum of 10 years experience, including a responsible position with Telecommunication organisation. Majority of experience in installation and maintenance of H.F. radio equipment. Should have final City & Guilds certificate in Telecommunications and hold grade or equivalent of Assistant Executive Engineer in British Post Office. Responsible for International Radio Transmitting and Receiving Stations. Including installing and maintaining new equipment and staff supervision. listed below offer attractive salaries, 3 year contracts, free passages for appointed candidates and their families, baggage allowances, furnished accommodation at 15% of basic salary, and in many cases substantial fringe benefits. All salaries earn 25% gratuity and generous leave allowances. This is an opportunity to widen your professional experience, to assist in the challenging work of developing a young nation – and all in the year-round sunshine.

Line Technician

For installation, maintenance and development duties of either subscribers apparatus including PABX's or jointing and laying of lead and PVC covered cables or construction and maintenance of openwire routes. Applicants should have at least 4 years suitable experience, and a current driving licence for 2 years. Two 'A' City & Guild's certificates desirable.

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Apprenticed mechanical engineers with 5 years experience, ONC or equivalent City & Guild's certificate. Duties involve running an organisation or GPO headquarters workshop in Ndola. General mechanical, carpentry, paint and light electrical work. Supervisory experience desirable. Emphasis on Mechanical Engineering.

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Applicants should possess 8 years training and practical experience in the servicing and maintenance of Semi-Automatic Message Switching and Tape Relay Equipment and associated peripheral equipment, including T100 Page Printers and T108 Tape Readers. Duties will include the maintenance of such equipment at Zambian Airports.

Civil Aviation

Radio Engineer

At least 8 years relevant experience plus I.C.A.O. Cert. is required. The duties will include the installation and maintenance of ground terminal radio communication equipment and navigational aids. Knowledge of medium powered H.F. transmitters and their ancillary equipment and of V.H.F. A.M. equipment is therefore essential.



Please apply by sending full personal and professional details and indicating the position which interests you to: Recruitment Officer,

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As a Radio Operator with the Post Office Maritime Service you can continue your career ashore in an interesting and expanding service. And earn over £2,000 a year, including compulsory pension contributions, at 25 years of age working only a 41-hour week of shift duties —with overtime this could rise to £2,300 and possibly more.

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APPOINTMENTS

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To apply you need to be 21 or over and to hold a 1st class or General Certificate issued by the MPT or an equivalent certificate issued by a Commonwealth administration or the Irish Republic.

If you would like to know more, please write to the Inspector of Wireless Telegraphy, Post Office, IMTR/WTS1.1.3, Union House, St. Martin's-le-Grand, London EC1A 1AR. L 53



Voice of Kenya Maintenance Engineer

(Broadcast Transmitter)

Required to introduce a revised maintenance system and assist in its implementation, to instruct staff and compile a maintenance instruction manual; to give occasional lectures on maintenance to engineering trainees.

Candidates, 30-50 years, must hold a degree or diploma in Engineering with extensive practical experience in organising and undertaking maintenance of sound transmission equipment, medium wave, short wave and VHF transmitters. Experience as an Instructor in maintenance techniques would be an advantage.

Commencing salary including Supplement will be in the range of £2,970 to £3,280 according to qualifications and experience. A substantial gratuity is payable on completion of engagement. Because of lower rates of Income Tax in Kenya the gross emoluments are roughly equivalent to a UK salary of £4,450 to £4,650 for a single man and £4,750 to £4,950 for a married man with two children.

Other benefits include—Subsidised Accommodation; Education Allowances; Holiday Visit Passages; Free Family Passages; Appointment Grant £100/£200. 30 Month Tour.

The post described is partly financed by Britain's programme of aid to the developing countries administered by the Overseas Development Administration of the Foreign and Commonwealth Office.

For further particulars you should apply, giving brief details of experience, to:



M Division, 4 Millbank, London SWIP 3JD, quoting reference number M2K/730923/WF. [3150

SPANISH Communications Equipment Manufacturer

Applications are invited from qualified design engineers specialized on:

a) Ground/Air Communications

b) TV Colour Transmitters

c) Side Band Transmitters

At least 5 years experience desirable. Company located in Madrid. Salary open.

Send resumé to: NORTRON Fernando el Católico, 63 Madrid 15 SPAIN 91

APPOINTMENTS

Are you equipped to engineer the future?

a121

As an experienced engineer, with a background in the electronics industry you'll be interested in the jobs listed below.

Most are newly created positions—an indication of the progress and development which has led to our current expansion programme.

Needless to say, all these positions carry salaries, which though negotiable, reflect the responsibilities of the task.

Our reputation spreads to over 70 countries—a reputation for producing some of the most sophisticated electronic equipment in the world, from custom built staff location systems to complex radio communications installations.

Chief Systems Engineer

This is a key position and calls for a man with experience of the development, design and commissioning of telecommunications or data systems. He should have a background in telephone line or switching equipment and be capable of leading the company's systems development programme. Some mobile radio communications systems experience would be an added advantage, and the position requires qualifications to degree or HNC standard.

Receiver/ Transmitter Development Engineers

These positions involve the development of highly sophisticated communications receivers and transmitters and offer plenty of scope for creativity and challenge. Applicants should have a relevant degree or equivalent and at least 3 years experience of equipment design.

Group Leader Receiver Development

To lead a group of engineers engaged in the design and development of high performance subminiature radio receivers. At least five years experience of equipment development in the mobile radio industry or a closely related field is essential. This post would be of interest to someone who has already successfully led a team in equipment development and is now seeking to advance his career and broaden his horizons.

A degree or similar qualification is essential. Engineers aged less than 30 are unlikely to have adequate experience for this, a key position.

For all these vacancies' please reply with relevant details of experience and qualifications, stating which position interests you, to:

Test Equipment Development Engineer

Duties involve designing and building test equipment for our Production and Test Departments. The activities range from simple jigs for testing small components to complex automatic fault diagnosis equipment. Applicants should have a thorough knowledge of solid state circuitry and integrated circuits and be familiar with radio receivers and transmitters. They must be able to follow a project through from inception to installation, designing printed circuits etc., ensuring high product reliability.

Senior Development Engineer

We need a Senior Development Engineer to design and develop products of a very advanced and complex nature. In addition to a degree or HNC, applicants should have at least five years experience of general low frequency design, with a bias towards digital techniques.

A future with Multitone makes sound sense

ww.americanradiohistory.com

Personnel Manager, Multitone Electric Co. Ltd. 10-28, Underwood Street, London, N.1. 3141

APPOINTMENTS



Electronics (Chigwell) Limited is the Audio division of the Thorn Group of Companies and in order to Thorn Consumer satisfy the continuing increase in demand for our products, both at home and abroad, it has become necessary to undertake an expansion programme. A new audio factory has been established at Harold Hill in Essex, which will ultimately be the largest manufacturing unit of its kind in Europe using sophisticated production techniques.

An exceptional opportunity occurs for a suitably qualified man to join the new organisation, which will be involved in quantity volume production of high wattage unit audio equipment, as Chief Inspector.

The job will be concerned with all aspects of the inspection, test and troubleshoot functions associated with the flowline production of the units. In addition, close liaison, with the Training Department in forward planning and training requirements will be necessary.

The successful candidate will hold suitable electronics qualifications, have experience of high volume production methods, be a capable staff motivator and will possess the drive and enthusiasm which the job will demand.

Written applications. setting out brief career details to date and current salary to:

a122



THE PERSONNEL MANAGER, THORN CONSUMER ELECTRONICS, 62/70 FOWLER ROAD, HAINAULT, ILFORD, ESSEX

A member of the Thorn Group THORN

3172

Southall College of Technology Beaconsfield Road, Southall, Middx.

Two Laboratory **Technicians**

required for Intermediate & Advanced Electronics Laboratory & Radio/Television Laboratory. Experience in maintaining electronic equipment desirable Salary on scale £1521-£1749 per annum inclusive.

Applications to be returned to the Registrar at the College by 19th October.



3194

Design and Development Engineers Come to Bournemouth

Here is an opportunity to live and work in the young and exciting atmosphere of Britain's most sought after sun spot. We manufacture the finest Commercial and Entertainment audio equipment and Hotel Service Systems in Europe, and are continually expanding both our comprehensive product range and market coverage.

We are now increasing our Design and Development Team and require a number of young high calibre engineers to initiate, design and complete new products in various markets. Successful candidates will have some experience in RF or A techniques (or digital/analogue switching) and should be qualified to at least HNC standard.

Self-motivation and a determination to succeed in a rapidly expanding company is of equal importance to formal qualifications. Salary will be very attractive and will be commensurate with experience.

For full details please contact SNS Electronics Group, 851 Ringwood Road, Bournemouth, Hants, Telephone Northbourne (02016) 5331/4 * Telex 41419

LONDON BOROUGH OF HOUNSLOW EDUCATION DEPARTMENT

AUDIO AND VISUAL AIDS TECHNICIAN (T. 1/3)

required at Chiswick Polytechnic, Bath Road, W.4, to join a team of two others to service five departments. Applicants should preferably have experience of modern teaching aids including closed circuit television but persons with an interest in educational technology will be considered. 36-hour week with some evening duties required. Salary scale £672-£1644 plus £105 London weighting.

Applications forms from The Principal, Chiswick Polytechnic, Bath Road, Chiswick, W.4. Tel: 01-995 3801, Ext. Road. 535. Closing date: 29th October, 1973. [3117

TECHNICAL AUTHORS

With electronic, electrical, computer or mechanical experience required by Engineering and Technical Publications (Derby) Ltd., 45 Friar Gate, Derby. Telephone 0332-41261. [3164

Board of Governors King's College Hospital.

Electronics Technician

required for an interesting project involving the application of ultrasonics to blood flow measurement. The applicant should preferably have had previous experience in prototype electronic instrument construction and will be expected to assist with clinical measurements expected to as: when required.

The appointment will be tenable for one year with a good possibility of renewal.

Minimum qualification are O.N.C. or final C and E in a relevant subject. Salary as Physics Technician Grade III.

Application forms obtainable from the Person-nel Office, King's College Hospital, Denmark Hill, S.E.25. Tel.: 01-274 6222 Ext. 2728 (Mrs. Child) should be completed and re-turned as soon as possible.

[3120

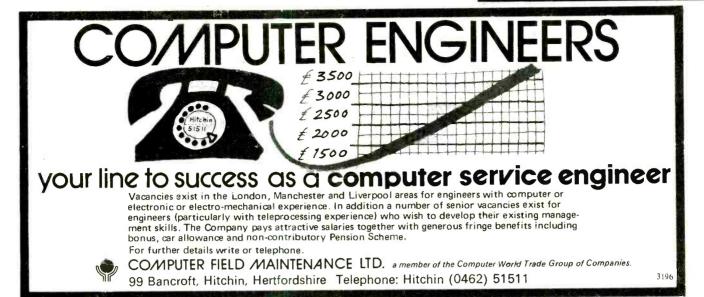
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APPOINTMENTS



Lancashire County Council **Health Department**

The Health Education Service has a vacancy for a

TECHNICIAN (TV/PHOTOGRAPHY) Grade Tech. 4

Salary £1,530-£1,803

Salary £1,330-£1,803 Television is becoming an integral part of audio visual alids in the provision of health education. T.V. studio facilities are being developed and the Health Education Service requires a technician whose duties will include the technical operation of T.V. equipment. The person appointed will, of course, be know-ledgeable in the use of normal projection equip-ment. It will be an advantage for applicants to have some expertise in camera work and photography.

have some expertise in camera work and photography. The post is full time, permanent, superannable and subject to medical clearance. Application forms obtainable from the County Medical Officer of Health, Serial No. 9693, East Cliff County Offices, Preston, to be returned by the 20th September, 1973. [3097] 13097

KEEN YOUNG MAN

interested in electronics and music, 18-20 years, to work in London recording studio. work in London recording studio. e working knowledge of audio elec-Responsible position with good Must have prospects. Phone Tony Leather on 01-499 7173. [3186

MEDICAL PHYSICS TECHNICIAN

GRADE III

with electrical and preferably some mechanical experience required to maintain cobalt, caesium and x-ray treatment units at the Royal Marsden Hospital, Fulham Road, London, S.W.3.

The person appointed will also be responsible for the development of radiation measuring instruments and will work in association with the Electronic and Workshop Groups of the Physics and Radiotherapy Departments.

Applicants should hold O.N.C., H.N.C., or similar qualification in electrical engineering or electronics and have at least 3 years' technical experience to obtain salary on scale £1,602-£2,076 p.a. plus £126 London Weighting.

Applications with details of experience and names of two referees to the Deputy Admin-istrator, Royal Marsden Hospital, Fulham Road, London, S.W.3. [3123

New Forest and Southampton Water with Racal Thermionic Ltd This is one of the most attractive areas in Southern England providing a variety of excellent recreational facilities. We are a member of the world-wide RACAL Group and are currently seeking a number of TEST ENGINEERS to join our existing team in coping with our planned expansion. Whilst formal qualifications to O.N.C. or City and Guilds standards would be an asset, previous experience in the following areas would be equally desirable. Analogue Good working knowledge of Analogue/Linear Electronics to be used on up to date Communications and Instrumentation Magnetic Recording Equipment. Digital Good working knowledge of Digital Logic Circuitry to be used on up to date Computer Peripheral Magnetic Recording Equipment. RF Good working knowledge of up to date R.F. Electronics for use on V.H.F. Transmitting Equipment using latest techniques We offer competitive salaries, good working conditions and a friendly work atmosphere. Communicate with Racal If you are interested in any of the above posts, please write or telephone for further information to The Personnel Officer, RACAL-THERMIONIC LIMITED, Shore Road, Hythe, Southampton Telephone : Hythe (04214) 3265, Ext. 66 3201 The Electronics Group

Why not live and work on the fringe of the

APPOINTMENTS

Wireless World, November 1973

THE STOCK EXCHANGE

require an additional

TELEVISION

SERVICE

ENGINEER

to maintain information display sys-

Applicants must possess appropriate television and radio servicing certifi-

cates and must be able to prove their

ability as competent Service Engineers

An attractive starting salary is offered.

In addition, there is a non-contributory pension scheme, 3 weeks holiday in a full year and Luncheon Voucehers.

Applications giving brief details of qualifications and experience should

Personnel Officer,

Council of The Stock Exchange, The Stock Exchange, London EC2N 1HP

ELECTRONIC

SERVICING

[3187

by a suitable trade test.

tems.

be sent to:

Electronics Test Engineers

a124

Pye Telecommunications of Cambridge and Haverhill have immediate vacancies for Production Test Engineers. The work entails checking to an exacting specification VHF/UHF radio-telephone equipment before customer delivery; applicants must therefore have experience of fault finding and testing electronic equipment, preferably communications equipment. Formal qualifications while desirable, are not as important as practical proficiency. Armed service experience of such work would be perfectly acceptable. Pye Telecommunications is the world's largest exporter of radio-telephone equipment and is engaged in a major expansion programme designed to double present turnover during the next five years. There are, therefore, excellent opportunities for promotion within the company. Pye also encourages its staff to take higher technical and professional qualifications.

These are genuine career opportunities in an expansionist company, so write or telephone without delay for an application form to:

Mrs A E Darkin at Cambridge Works, Elizabeth Way, Cambridge CB4 1DW. Telephone: Cambridge 51351. or Mrs C Dawe at Colne Valley Road, Haverhill, Suffolk. Telephone: Haverhill 4422.

Pye Telecommunications Ltd

96

The best young Engineers have computers in mind. Are you aged 21 to 25?

Do you want a flying start to a career in computers? Here is your chance. Train as a Field Engineer with ICL, Europe's leading computer manufacturer.

Training

You will be given thorough training on ICL electronic equipment leading to computers.

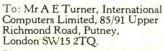
Qualifications

You should be aged between 21 and 25 and be on your final year or have attained City & Guilds electronic certificates or an HNC in electronics. You should have completed an electrical engineering apprenticeship or have at least two years' industrial experience on electronics.

Job satisfaction

As an ICL Field Engineer you have a high degree of responsibility for a customer's installation. You need technical expertise, tact and personality. So you are important as a representative of ICL.

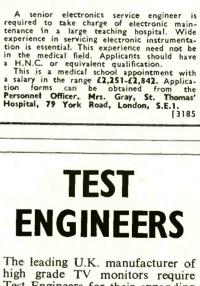
There are opportunities of starting with us in several areas in the UK. Get the full details now by completing and returning this coupon today.



Please send me an application form for job openings in Field Engineering.

Name

Address	
	1
International Computers	ICL
	(WW8)
	2589



Test Engineers for their expanding Test Department.

Situated in the Berkshire town of Maidenhead, the Company offers pleasant working conditions, good salaries and friendly environment. Duties will cover the testing and trouble-shooting of monochrome and colour TV monitors together with other ancillary sophisticated TV broadcast equipment manu-factured by the company. Previous experience of TV equipment would be an advantage. Please apply to:

PROWEST ELECTRONICS Boyn Valley Road, Maidenhead, Berks. Maidenhead 29612

[3180

ELECTRONIC ENGINEERS FOR CANADA

A well-known Canadian Company designing and manufacturing computerorientated totalisators requires electronic engineers to meet their continuous expansion.

The likely candidates should be qualified to H.N.C. standards or hold a C.G.L.I. final certificate as electronic or telecommunication technicians. Candidates with equivalent qualifications will also be considered. All candidates must have experience in the development and maintenance of computer systems. Some knowledge of programming would be an advantage. The salary is negotiable depending on qualifications and experience. Interviews will be held in the U.K. Please reply in writing to:

Attention: Managing Director. WESTERN TOTALISATOR CO. LTD., 102 Elmslie Street, Lasalle, Montreal 650, Quebec, Canada. [3179

The Polytechnic of Central London Audio Visual Aids Technician £1902-£2202

with experience in maintenance of tape recorders, amplification equipment and C.C.T.V. with the ability to operate both this and 16mm equipment,

Application form from The Establishment Officer, 309 Regent Street, London W1R 8AL. Please quote reference 885.

[3184

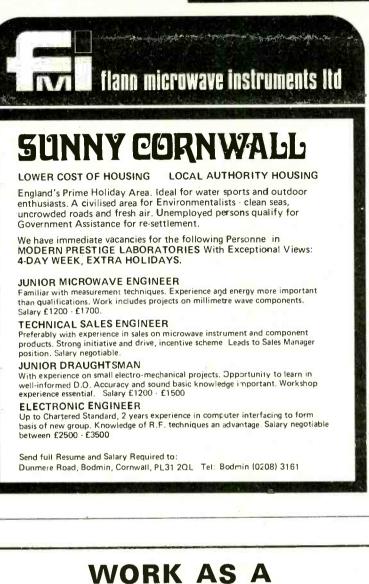
WIGGINS TEAPE RESEARCH AND DEVELOPMENT LTD. Butlers Court, Beaconsfield, Bucks.

SENIOR ELECTRONICS TECHNICIAN

Applications are invited for this post to lead a small team engaged in applying electronics to papermaking research and allied processes at the Central R. and D. Unit of an international papermaking group. Based at Beaconsfield the duties will include design, development, manufacture and maintenance of a wide variety of electronic, electro-mechanical and opto-electronic instrumentation. Applicants should be of H.N.C. standard and have several years development experience with linear and digital circuits. The salary is negotiable in the range £2,000 to £3,000. The unit provides

excellent working conditions, a pension scheme and luncheon vouchers. Application forms from Mr. A. W. Massey, Personnel Department. Tel: 0494 5652. [3091] a125

APPOINTMENTS



RADIO TECHNICIAN

ATTACHED TO SCOTLAND YARD

You'd be based at one of the Metropolitan Police Wireless Stations. Your job would be to maintain the portable VHF 2-way radios, tape recorders, radio transmitters and other electronic equipment which the Metropolitan Police must use to do their work efficiently.

We require a technical qualification such as the City & Guilds Intermediate (telecommunication's) or equivalent.

Salary scale: £1415 to £1715 according to age from 21 to 25, to a maximum £2025 p.a. (plus a London Weighting Allowance of £175 or £90 p.a.).

Promotion to Telecommunication Technical Officer will bring you more.

For details of this worthwhile and unusual job write to: Metropolitan Police, Room 733 (RT/WW), New Scotland Yard, Broadway, London, SW1H 0BG, or telephone 01-230 3122 (24-hour service).

APPOINTMENTS



9126

provision of multiple access.

- Electro-magnetic theory : radio wave propagation and aerials.
- Night vision: work on optical and detector components, the investigation of the man/ machine interface, and the assessment of systems.

Appointment may be made at Senior Scientific Officer, Higher Scientific Officer, or Scientific Officer level.

For Senior Scientific Officer appointment you must have a 1st or 2nd class honours degree with at least four years appropriate post-graduate experience. Salary scale £2615-£3640

At Higher Scientific Officer level, gualifications required are a degree, HND, or HNC, with at least 2 years post-graduate experience for the good honours graduate and 5 years for other candidates. Salary scale £2076-£2667.

For Scientific Officer appointment you should have a degree, HND, or HNC and be under 27 years old. Salary scale £1318-£2177.

3181

T.V. Studio Engineer

The Road Transport Industry Training Board has in operation at its Wembley Headquarters, a 3 camera broadcast-quality colour television studio with full telecine and video recording facilities which includes R.C.A. TR 50 and 1in. Helical Scan systems. We now wish to appoint an experienced studio engineer to join a small team working on the production of training and educational television programmes.

The applicant should not be less than 24 years of age and have a good working knowledge of the above equipment. Salary will be negotiable depending on qualifications and experience. Three weeks holiday, contributory pension and life assurance scheme.

Please send all relevant personal history stating how the above requirements are met, and quoting reference ZH335, to:



For further details,

Signals Research

Establishment,

ext. 302.

conditions of service, and an application form please

write to J. R. Mills, Director,

Christchurch, Hants, or

telephone the Personnel

Officer on Highcliffe 2361,

Mrs. H. M. Brown, Personnel Manager, **Road Transport Industry Training Board, Capitol House, Empire Way,** Wembley, Middlesex HA9 0NG.

LOUGHBOROUGH TECHNICAL COLLEGE Principal: F. Lester, B.Sc., Ph.D., F.R.I.C.

Department of Electrical Engineering LECTURER GRADE I

The person appointed will be required and Practice to Final Certificate level in Technicians' courses. Applicants should have recent trade experience and be fully conversant with broadcast receiving equipment. They should be suitably qualified and preferably be members of a Professional or Tech-nician Institution. Teaching experience and teacher training will be advantageous.

Salary will be in accordance with Scales for Teachers in Establishments for Further Education 1973 (under review), viz., Lecturing Grade, £1,500-£2,525 (plus 2 x £81 for good Honwith placing according to ours).

qualifications and experience. Further particulars may be obtained from the Principal, Loughborough Technical College, Radmoor, Lough-borough, Leicestershire, LE11 3BT, to whom completed applications should be returned within 14 days of the appearance of this advertisement. [3171

The Hatfield Polytechnic

TECHNICIAN for Psychological Laboratory

for maintenance and construction of a variety of electronic and other equipment. The person appointed will work with a Senior Technician. Applicants should preferably hold an appropriate intermediate or National Certificate, or City and Guilds qualification, but this is not essential.

Salary scale: £672-£1,242 per annum.

Application form and further details from: The Staffing Officer, The Hatfield Polytechnic, P.O. Box 109, Hatfield, Herts. Quote ref.: 270.104 P.O. Box 379/WW.

[3170

LEEDS AND BRADFORD AIRPORT **RADIO/RADAR** TECHNICIAN

REQUIRED

A vacancy occurs for a Radio/Radar Technician to undertake maintenance of all ground equipment, including radar, CRDF, ILS, etc., on a watchkeeping basis. Radar maintenance experience essential. Salary in accordance with Local Government Grade Tech-nical 5/6 (£1,926—£2,535 per annum), commencing salary, depending upon experience and qualifications, between £1,926 and £2,235, plus enhanced pay-ment for washend working. Appoints ment for weekend working. Appoint-ment subject to Local Government Superannuation Acts and medical examination.

Applications, stating age, education, and full details of experience and technical courses attended, together with the names and addresses of two people to whom reference can be made, should be sent to the Airport Dir-ector, Leeds and Bradford Airport, Yeadon, Leeds, LS19 7TZ. Tel: 08737 3391.

a127

APPOINTMENTS

University College Hospital Medical School

Neuropsychology and Metabolism Research Unit, Friern Hospital, London, N.11

ELECTRONICS TECHNICIAN

Electronics technician to assist in the establishment and subsequent running of a new research laboratory. Some experience with recorders, E.C.G., E.E.G. or data processing equipment would be an advantage but not essential.

Applicants should have O.N.C. in electrical or electronic engineering or a similar equivalent qualification. Salary on Whitley Council scale according to age and experience plus London weighting allowance.

Applications to the Secretary, University College Hospital Medical School, University Street, London, WC1E 6JJ. Quote reference F.C.2.

ENGINEER

to service ELECTRONIC ORGANS B & O AUDIO and C.T.V.

The work is interesting and varied, a Company vehicle is provided and there are vacancies in Birmingham and Manchester.

Telephone or write to: W. Swan, Jnr. or Mr. D. C. Kay, SWAN'S, 84-86 Oldham Street, Manchester M4 1LF Tel: 061-228 3821 [2959

WALSALL AND STAFFORDSHIRE TECHNICAL COLLEGE JOINT EDUCATION COMMITTEE

Principal: H. Cheetham, B.Sc.(Hon.), C.Eng., M.I.Mech.E., F.1.Prod.E., Department of Engineering

LECTURER GRADE 1

in

RADIO AND TELEVISION

Applicants will be expected to teach the subject of Radio and Television to the Final Year of the Radio and Television Mechanics Course, C.G.L.I. No. 222 and the Radio and Television Technicians Course, C.G.L.I. No. 272. A sound knowledge of the theory and practice of Colour Television Servicing would be very desirable. Applicants should possess appropriate qualifications with teaching and industrial experience.

Salary for the above post will be in accordance with the Burnham Further Education Scale, viz Lecturer Grade I £1,500 - £2,525 per annum (under review).

Application forms may be obtained from the Principal, Walsall and Staffordshire Technical College, St. Paul's Street, Walsall WS1 IXN. Applications should be returned within a fortnight of the appearance of this advertisement.

R. D. NIXON, Secretary to the Joint Education Committee.

[3125

Nigerian Telecommunications Supervisor

The Shell-BP Petroleum Development Company of Nigeria Limited has a vacancy for a qualified Nigerian Telecommunications Supervisor.

You should be academically qualified at C.E.I. Chartered Engineer level, be eligible for membership of the Nigerian Society of Engineers or hold any other qualifications acceptable to the Council of Registered Engineers of Nigeria. You must have a minimum of 5 years' total practical experience in at least two of the following:

(a) Multi-channel fixed communications systems (b) Telemetry (c) Mobile radio systems

If you are a Nigerian National returning to your country this year and are interested in this position, please telephone Pauline Ford on 01-934 2493 or write, giving details of age, qualifications and experience, to:—

Shell International Petroleum Company Ltd., Recruitment Division (GD), PNEL/41 Shell Centre, London SE1 7NA.

Are you interested in

Communal Aerial Television Systems Work?

Then read on further.....

Due to continued expansion, EMI Service, part of EMI's Electronics and Industrial Operations group of Companies, has the following vacancies for engineers at Hayes, Middlesex.

SERVICE ENGINEERS

required for bench and field work on Communal. Television Aerial equipment. Must be capable of diagnosing faults and repairing wide range of aerial amplifying and distribution equipment.

SYSTEMS PLANNING ENGINEERS

for the planning of Communal Television Aerial installations. Previous experience required to be capable of producing practical plans from building details and subsequently setting to work after installation. Attractive starting salaries. Contributory Pension Scheme. Assistance with removal expenses in appropriate cases.

WANT TO TAKE THINGS FURTHER

then write or telephone for an application form to:

R. N. L. Black, Personnel Department, EMI Limited, 135 Blyth Road, Hayes, Middlesex. 01-573 3888, Ext 2887.



International leaders in Electronics.Records and Entertainment.

3004

APPOINTMENTS

British Relay Communication and Call Systems -Speech and Visual

a128

We are acquiring an increasing volume of business in this field including many very long term contracts, and we are seeking to expand the range of our activities. Consequently, we have immediate requirements for engineers with good practical experience and ability in any of the following aspects of the work:-

> System Design **Planning and Estimating Project Control** Installation Supervision **Test and Commissioning**

Duties are varied and interesting, with frequent opportunities for travel, and for acquiring experience in new fields. Enquiries and application for interviews will be treated in strict confidence, and should be sent to:-



The General Manager, **British Relay** (Electronics) Limited, 41 Streatham High Road, London SW16 1EP Tel. 01-677 9681.

A REALLY WORTHWHILE JOB (Electrical Test Technicians/Engineers)

GEC Medical Equipment Ltd., based in North Wembley, is a world-wide leader in the manufacture of a wide range of medical diagnostic X-ray apparatus which is every day helping the sick and injured throughout the world.

Because of the ever-increasing demand for our equipment both at home and overseas and in order to maintain the high standard of reliability of our product, we need additional electronic test technicians/engineers with practical electrical/electronic experience, preferably qualified to City and Guilds or National Certificate standard.

The work involves testing and faultfinding on a wide variety of medical X-ray apparatus and associated units such as closed circuit television and image intensifiers using both orthodox and specialist test equipment.

There are excellent opportunities for career development. If you would like to know more about working with this Company please write, giving brief career details, or telephone: P. B. Blackmore, Personnel Officer, GEC Medical Equipment Ltd., East Lane, North Wembley, Middlesex, Tel: 01-904 1288. 13163

University College of North Wales, Bangor. School of Physical and Molecular Sciences.

ELECTRONICS **TECHNICIAN GRADE 5**

Applications are invited for the post of Electronics Technician Grade 5 in the above mentioned School.

The successful applicant will be concerned with the servicing and maintenance of existing electronic equipment for research and teach-ing, and with the development and construc-tion of new specialised equipment.

Applicants should have had several years practical experience in digital and linear solid state electronics, preferably in industry or the services, coupled with theoretical knowledge to about HNC standard.

Salary at an appropriate point on scale: £1,881 x 72—£2,241 per annum. (Salary Scale, at present under review).

Applications (two copies), giving full de-tails of age, qualifications and experience together with the names and addresses of two referees should be submitted to the Secretary and Registrar, University College of North Wales, Bangor, by not later than the 14th November, 1973. [3119

ELECTRONICS ENGINEER

THE OPEN UNIVERSITY

A vacancy occurs due to the setting up of a Psychological Laboratory for an Electronics Engineer. Duties will include the develop-ment of equipment for teaching and research such as a mini computer and a digital re-action timer, the maintenance of laboratory facilities and purchase of equipment in close collaboration with academic Psychologists and the Electronics Laboratory. Applicants should have at least 7 years rele-vant experience and qualifications such as City and Guilds or HNC in relevant subjects. The appointment will be made on the Tech-nician Grade 5 scale: £1,881—£2,241 per annum.

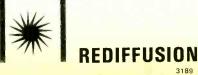
annum. Further particulars are available from the Acting Personnel Manager (EP2), The Open University, P.O. Box 75, Walton Hall, Milton Keynes, MK7 6AL. Applications should be returned as soon as

[3144

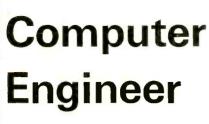
3189

ELECTRONIC ENGINEERS

required for equipment maintenance and associated engineering projects. Knowledge of professional tape recording equipment, studio operations, or high speed tape duplicating systems is desirable. Salary will be according to age and experience. Please write giving details of age, qualifications, experience and present salary to Chief Engineer, Rediffusion Reditune Ltd., Cray Avenue, Orpington, Kent.



Wireless World, November 1973



Character Generation

Rediffusion require an Engineer to maintain the above equipment in the London area. TTL experience essential. Knowledge of video circuits preferred.

Good salary plus Company car.

Telephone:

Mr. Yates 01-385 9472

Reading Education Committee Highdown School, Surley Row, Emmer Green, Reading. Telephone: Reading 475022

AUDIO VISUAL AIDS TECHNICIAN

required at the above school. Salary on scale \pounds 1,644 rising to \pounds 1,926. Extra payment for qualifications. Minimum age 25. Preference will be given to holders of C.G.L.I. Audio Visual Aids Technician's Certificate. Maintenance, servicing and operation of a wide range of A/VA equipment including CT/TV and application forms obtainable from and returnable to the Chief Education Officer. 2 Cheapside, Reading, RGI 7BA within 14 days of the appearance of this advertisement.

[3139

13202

UNIVERSITIES OF DURHAM AND LEEDS

BRITISH UNIVERSITIES AIR SHOWER PROJECT

A vacancy exists for a Technician to assist with the installation and operation of a small computer at the British Universities Air Shower Project at Haverah Park near Harrogate. The successful applicant should have a knowledge of digital electronics and/or Computer hardware and should reside in or be prepared to move to the Leeds-Bradford-Harrogate area.

Salary wilf be at an appropriate point on the University Scale for Technicians (at present under review) £1.881-£2,241 according to age and experience. The appointment will be for two years commencing 1st December, 1973 with the possibility of renewal of contract.

Applications in writing giving full details, age, ducation and experience together with copies of testimonials or names and addresses of two referees to the Personnel Office, Science Laboratories, South Road, Durham by 1st November, 1973. Interviews will be held in Leeds in November, 1973. [3168] MARCONI INSTRUMENTS LIMITED

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TECHNICIANS

are required to work on calibration, fault-finding and testing of telecommunications measuring instruments. The work is varied and will enable technicians with experience of r.f. circuits to broaden their knowledge of the latest techniques employed in the electronics and telecommunications industries by bringing them into contact with a wide range of the most advanced measuring instruments embracing all frequencies up to u.h.f.

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We require engineers with previous experience in TV (Colour and Monochrome), Radio, H-Fi, Tape/Cassette Recorders and V.T.R. products, for our Ashford and Leeds Depots.

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Pyrene House,		Sony (U.K.) Ltd.,	
Sunbury Cross,		Universal Estate,	
Sunbury-on-Thames,		Wakefield Road, Gilderse	ome,
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POSSESSION OF ONE OF THESE QUALIFIES YOU FOR CONSIDERATION FOR A RADIO OFFICER POST WITH COMPOSITE SIGNALS ORGANISATION.

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On satisfactory completion of a 7-month specialist training course, successful applicants are paid on a scale rising to $\pounds 2.527$ pa; commencing salary according to age — 25 years and over $\pounds 1.807$ pa. During training salary also by age, 25 and over $\pounds 1.350$ pa with free accommodation.

The future holds good opportunities for established status, service overseas and promotion.

Training courses commence at intervals throughout the year. Earliest possible application advised.

Applications only from British-born UK residents up to 35 years of age (40 years if exceptionally well qualified) will be considered.

Full details from

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Recruitment Officer, Government Communications Headquarters, Room A/1105 Priors Road, Oakley, Cheltenham, Glos GL52 5AJ, Telephone: Cheltenham 21491 Ext 2270

> Charing Cross Hospital (Fulham) Fulham Palace Road, London W6 8RF

ELECTRONICS TECHNICIAN FOR PATIENT MONITORING

Applications are invited for a post in a small team installing and maintaining patient monitoring equipment in this newly built hospital. The successful applicant will have an excellent opportunity to acquire experience in the application of electronics in medicine. Facilities include a new well equipped workshop.

Applicants should have at least three years experience in the electronics field, preferably in the construction of Electronic Instruments and possess an ONC or equivalent qualification.

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[3204

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Has an immediate opening for An experienced Design and Development Engineer for Audio Equipment, including Highly Professional Mixing Desks, Compressors, Limiters, Audio Monitoring Amplifiers, etc. Systems Experience is desirable. Salary open.

Send resumé to: NORTRON Fernando el Católico, 63 Madrid 15 SPAIN

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Require a **Supervisory Maintenance Engin**eer to take charge of a small specialist staff maintaining a wide range of sophisticated electronic broadcast equipment, including AVR-1 machines, flying spot telecine, HS100 Computer Controlled Editing equipment and Cassette Duplicating machinery. A broadcast background is desirable.

Applications should be made, in writing giving brief details of experience to :-

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or telephone 01-734 2511 for application form

APPOINTMENTS

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Multitone — world leaders in the electronics communications industry need an experienced Technical Author. Already established in his field, the writer we're looking for should ideally have the kind of experience generated by at least five years in the radio/ telecommunications industry.

He/or she will have complete responsibility for writing and editing technical product manuals. This is an interesting post, with plenty of scope for creative flair, and involves constant liaison with other departments, particularly with our Development Engineers.

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PERSONABLE CHEMISTS or PHYSICISTS

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Good salary subject to regular review, Ford Cortina 1600 XL, changed every 25,000 miles, modern contributory pension scheme, B.U.P.A., Life Insurance and other fringe benefits.

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ARTIFICIAL KIDNEY AND TRANSPLANT UNIT CHIEF TECHNICIAN

required to be responsible for the supervision of junior technical staff and control and maintenance of the artificial kidney equipment. Experience in Dialysis Unit an advantage but not essential. ONC, HNC, or HND in electrical or mechanical engineering, preferably with some electronics experience.

Starting salary £2,037 rising to £2,634 plus payment for on call and weekend rota.

Applications to: The House Governor, The London Hospital (Whitechapel), Whitechapel, London E1 1BB. Tel.: 01-247 5454 Extn. 388.

OPPORTUNITIES in the ELECTRONICS FIELD Men with analogue or digital qualifications/ experience seeking higher paid posts in: TEST — SERVICE — DESIGN — SALES. Phone Roger Pearce Ref. WW2. NEWMAN APPOINTMENTS 360 Oxford St., W.1. 01-629 7306 3148



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We are particularly interested in applicants with experience of writing handbooks to ATP standards and/or experience in the preparation of test specifications in ATLAS or ATLAS-type test language.

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Salaries will be up to $\pounds 2700$ dependent upon experience and ability.

Please write or telephone for an application form to:-R.N.L. Black, Personnel Department, EMI Electronics Ltd., 135 Blyth Road, Hayes, Middlesex. Tel: 01-573 3888 Ext. 2887.

APPOINTMENTS

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Technician Engineer

(Solid State Circuits)

If you know about solid state circuitry read this – then ring us – but you must be experienced in maintenance, design and construction of solid state electronic circuits, preferably in communications and CCTV.

If you are the right man – preferred age range 25/40 – you will share the responsibility for the maintenance of a wide range of sophisticated electronic devices and a radio communications network. Technical competency in your field will lead to additional design and installation responsibilities under guidance of the Company's electro-mechanical research and development group.

The job is based in Central London. If you think you can handle it, phone 01-405 5200 (reversing charges) to tell us about yourself, and to get more details.

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With good practical knowledge of Electronics and experience in Broadcasting, recording studios or quality Hi-Fi, he will be responsible for the installation of professional Audio Equipment in Studios and in the Maintenance Department. This position entails considerable travelling in the U.K. and abroad. Company Car to be provided.

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With good basic knowledge of Electronics and who has had some experience in Broadcasting, recording or Hi-Fi, he will be involved in the maintenance and installation of Studio Equipment. This can be a unique opportunity for the right person wanting to enter the professional Studio industry.

Please write giving full details to :

FELDON AUDIO LTD., 126 Great Portland Street, London, W1N 5PH Attention: Mr. W. Dyer

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ELECTRONIC ENGINEER

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The duties involved will be the performance certification, quality assessment and fault analysis of digital computer equipment, together with associated electronic test equipment. Additionally he will be required to assist generally in the day-to-day running of a small section of engineers. For this post at least three years' previous experience of digital computers and programming techniques is essential. Ideally, qualifications to a minimum of H.N.C. standard will be required. Amongst the benefits operated by the Company are:---generous Holiday Entitlement. Contributory Pension Scheme and Life Assurance and assistance with re-location expenses, where appropriate. Write giving experience, age and present salary to: The Engineering Staff Officer. Research & Engineering Department,

SMITHS INDUSTRIES LIMITED

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THE MOTOR INDUSTRY RESEARCH ASSOCIATION

Electronics Maintenance Engineer

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3182

Preferably with HNC or equivalent required. Practical experience of the maintenance of digital computers, A.D. converters etc., employing integrated circuits would be an advantage.

Applications in writing to MIRA, Watling Street, Nuneaton, Warks., giving age, experience and current earnings, quoting ref. CHGM.

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ELECTRONICS ENGINEER

A rapidly expanding company manufacturing Hi Fi equipment offers an exciting future for an Electronics Engineer with drive and ambition. He should be experienced in audio and capable of designing and making test modules.

> Apply to: MACDONALD ELECTRIC Stour House, High Street, Wollaston, Stourbridge. Tel. Stourbridge 3102. [3199

Wireless World, November 1973

APPOINTMENTS



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to work in a small enthusiastic team providing colour film recordings to broadcasters throughout the world.

Two years' experience in broadcast VTR operations and maintenance together with a sound fundamental k n o w l e d g e of colour TV systems are the essential qualifications.

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SITUATIONS VACANT A SISTANT to Technical Director required by Italian Radio Manufacturer/Distributor. The successful applicant must be a Service Engineer with Radio, TV and Audio background. A high degree of circuit knowledge is required together with the ability to work on own initiative. Commencing salary f2000/f2500 according to age and experience. Please write or telephone Mr. A. Massing, Europhon (Radio & Television) Ltd., 70 Caledonian Road, London N1 9DN. 01-837 3045/6. CREATIVE electronics engineer needed for business venture. No capital needed. No need to relinquish CREATIVE electronics engineer needed for business venture. No capital needed. No need to relinquish your job. 01-994 6264. [3192 ELECTRONICS TECHNICIAN required to join Respiratory Research Group. Work involves development and maintenance of respiratory instru-mentation in Clinical and Physiology sections of group. Experience in Analog and digital techniques desirable. Salary according to qualifications and experience. Applications to Secretary, Royal Post-graduate Medical School, DuCane Road, London W12 0HS, quoting reference 2/243/WW. [3142

Electronics Engineers

a133

lecture on computer servicing.

International Computers Limited, Europe's leading computer company, is looking for Electronics Engineers to teach the practicalities of computer servicing. At the largest training centre of its kind in Europe, ICL will first of all ground you in computer technology and education training, and then ask you to train customer engineers to such a standard that they will be able to maintain computers at optimum operational specification.

We are looking for a thorough electronics competence and the ability to put across your own first-rate knowledge. Ideally, you will have an HNC or Forces training in electronic engineering and at least three years'

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You will be based at the training centres in either Letchworth, Herts or Feltham, Middlesex. Salaries will be good. ICL depends on talent and rewards it accordingly. You will be encouraged and expected to progress; your development could be throughout the ICL group.

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Several years of experience in the design of a range of circuits, willing and able to tackle any circuit problem from first principles. Quite familiar with linear integrated circuits: a working knowledge of digital networks would be useful but is not essential. Experience in line data communications, broad rather than specialised would be advantageous.

Probably the right engineer for this job will be in the region of 28-33 years old, but age in itself is no impediment (at either end of the range)

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1-2 years experience in the design of digital logic networks using integrated circuits. We have in mind computer-type applications, but not computer design as such.

These people are required for work on a new aspect of computer-based communication systems.

Above average salaries for above average applicants.

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Mr. A. Cox

Personnel Manager Redifon Electronic Systems Ltd., P.O. Box 2, Manor Royal, Crawley, Sussex. Crawley 27074



H^{1-FI} AUDIO ENGINEERS. We require experi-enced Junior and Seniors and will pay top rates to get them. Tell us about your abilities. 01-437 4607,

UNIVERSITY COLLEGE HOSPITAL MEDICAL SCHOOL Applications are invited for the post of Audio-Visual Technician/Co-ordinator, to take charge of the Medical School's Lecture Theatres and audio-visual aids including CCTV, VTR and T/S equipment. Salary according to experience and qualifications within the range £1,077-£1,944 plus £126 London Weighting. Application forms and further particulars obtainable from The Secretary, University College Hospital Medical School, University Street, London WCIE 6JJ. [3118

Do you require Indian representation? B.Sc. Honours in Electrical Eng. Resident Delhi, Bom-bay. Willing to act as local rep. for U.K. companies. Ref. available. Write Box WW3035. E X BBC audio engineer, disillusioned by educational ability with mixers and recorders etc., will be appre-ciated and rewarded. Offers and suggestions welcomed. Yorkshire area preferred, but will travel. Box No. WW 3162.

Yorkshire area preferred, but will travel. BOX 150-WW 3162. MARINE RADIO OFFICER: (Aged 27), eight years sea service seeks employment ashore within the electronics field in either field service, sales engineering or communications. PMG Certificate (2), DTI Radar Certificate. Willing to learn new fields and travel either at home or abroad. Permanent position, preferably in Scotland. Box WW 3099. SURPLUS components and computer boards pur-chased for cash. 01-692 2009. [3108 ARTICLES.FOR SALE ARVAK ELECTRONICS. 3-channel sound-light converters, from £18. Strobes, £25. Rainbow Strobes, £132.—12A Bruce Grove, N17 6RA. 01-808 [9066.] DIVED IT in a DEWBOX quality plastic cabinet

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APPOINTMENTS-Continued on p.138

VIDEO TECHNICIAN to locate in CANADA

A Canadian company with several cable television systems in Southern Ontario is seeking an experienced broadcast technician who will assume the technical responsibilities of a small television broadcasting studio.

This is a senior technical position requiring a formal electronics training background with a strong employment background in video and audio maintenance related to television broadcast principles.

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JARMAIN CABLE SYSTEMS LTD.,

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INTERVIEWS WILL BE CONDUCTED IN LONDON, ENGLAND, AT A LATER DATE [3122

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ELECTRONICS TECHNICIAN

SALARY £1,602-£2.076

(According to qualifications and experience)

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Possession of a car essential.

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[3124

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The posts are pensionable, there is a sick pay scheme, three weeks annual paid holiday and an assisted travel scheme. There is a prospect of housing accommodation within a reasonable period for a married man, hostel accommodation is immediately available for single men.

If you have served a recognised apprenticeship or have had equivalent service training and would like to work in a beautiful part of the country, send for an application form to :

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Wireless World, November 1973

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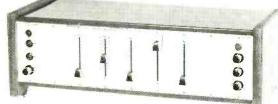
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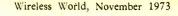
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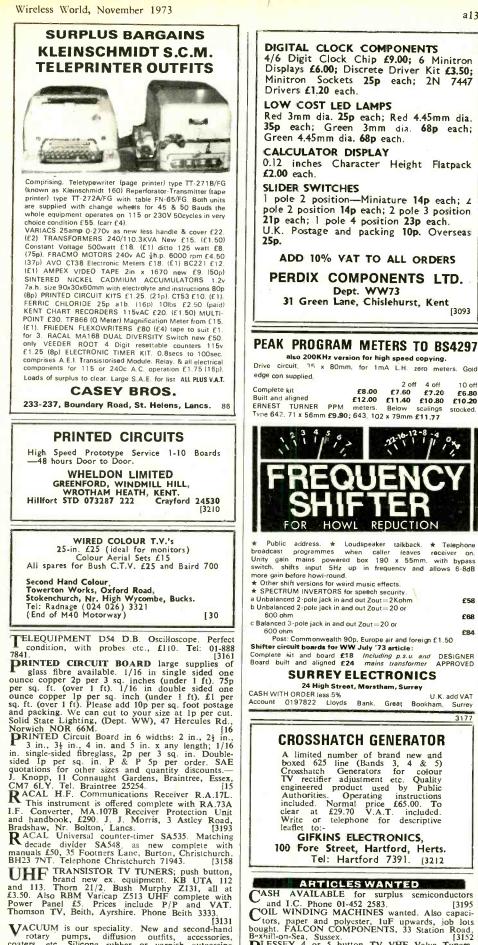
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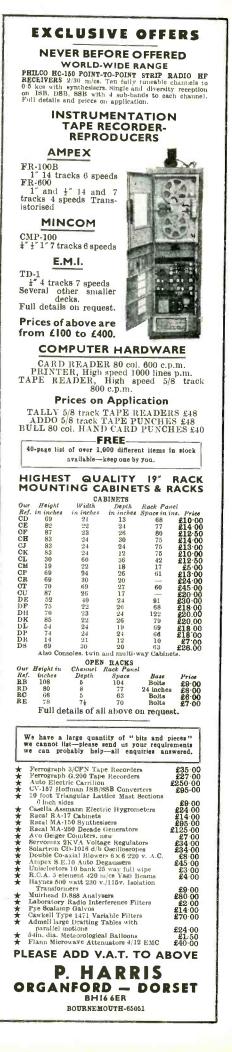
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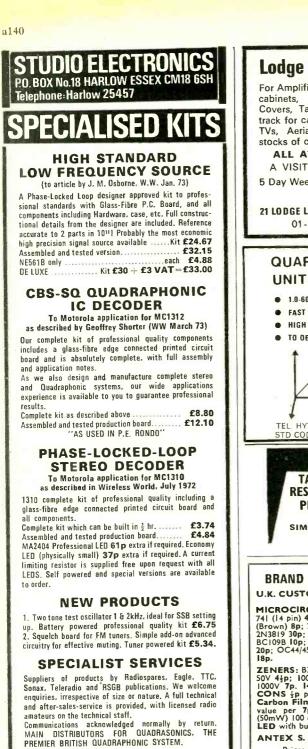


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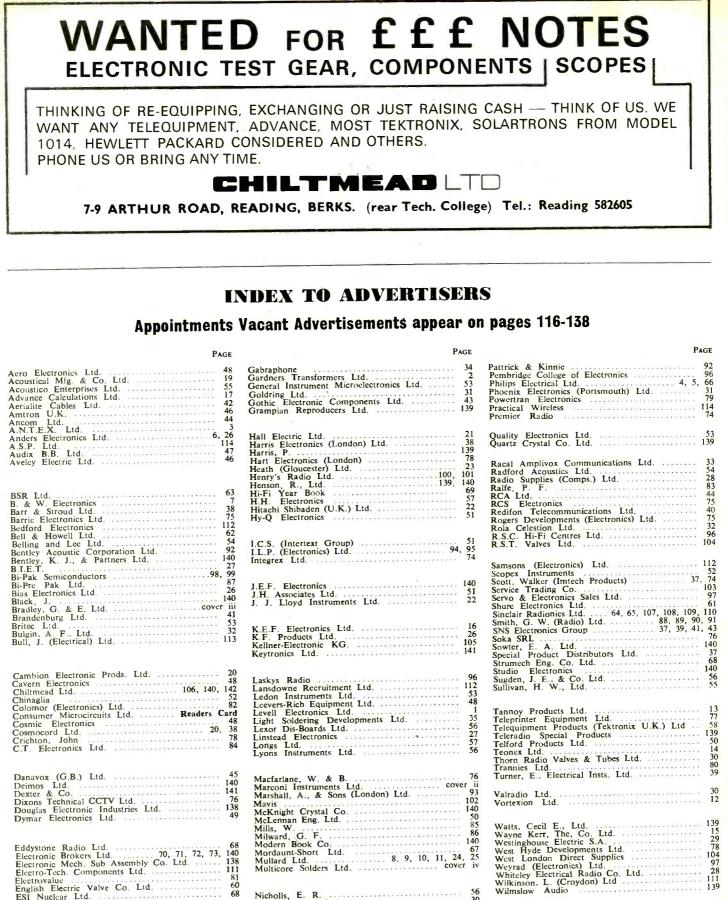
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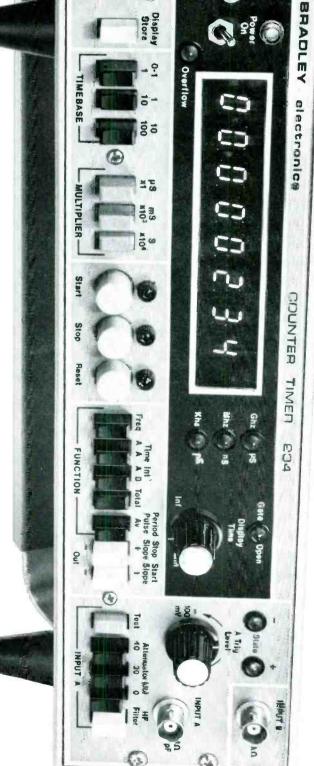
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