## Tuner-amplifier survey

 Model railway control system


PORTABLE INSTRUMENTS

These highly accurate instruments incorporate many useful features, including long battery life. All A type models have $3 \frac{1}{4}$ " scale meters, and case sizes 5 " $\times 7^{\prime \prime} \times 5^{\prime \prime}$. B types have 5 " mirror scale meters and case sizes 7 " $\times 10^{\prime \prime} \times 6^{\prime \prime}$.


## A.C. MICROVOLTMETERS

VOLTAGE \& db RANGES : $15 \mu \mathrm{~V}, 50 \mu \mathrm{~V}, 150 \mu \mathrm{~V} \ldots 500 \mathrm{~V}$ f.s.d Acc. $\pm 1 \% \pm 1 \%$ f.s.d. $\pm 1 \mu \mathrm{~V}$ at $1 \mathrm{kHz}, 100,-90 \ldots+50 \mathrm{~dB}$ scale $-20 \mathrm{~dB} /+6 \mathrm{~dB}$ rel. to $1 \mathrm{~mW} / 600 \Omega$. RESPONSE : $\pm 3 \mathrm{~dB}$ from 1 Hz to $3 \mathrm{MHz}, \pm 0.3 \mathrm{~dB}$ from 4 Hz to 1 MHz above $500 \mu \mathrm{~V}$. Type TM38 can be set to a restricted B.W. of 10 Hz to 10 kHz or 100 kHz . INPUTIMPEDANCE: Above $50 \mathrm{mV}:>4.3 \mathrm{M} \Omega<20$ pf. On $50 \mu V$ to $50 \mathrm{mV}:>5 \mathrm{M} \Omega<50 \mathrm{pf}$. AMPLIFIER OUTPUT: 150 mV at f.s.d

## $\mathbf{f 4 9}_{\text {wixin }} \mathbf{f 6 3} \underset{\text { wixa }}{ }$

## D.C. MICROVOLTMETERS

VOLTAGE RANGES: $30 \mu \mathrm{~V}, 100 \mu \mathrm{~V}, 300 \mu \mathrm{~V} . .300 \mathrm{~V}$. Acc. $\pm 1 \%, \pm 2 \%$ f.s.d., $\pm 1 \mu \mathrm{~V}$. CZscale.
CURRENT RANGES: $30 \mathrm{pA}, 100 \mathrm{pA}, 300 \mathrm{pA}, 300 \mathrm{~mA}$.
Acc. $\pm 2 \%, \pm 2 \%$ f.s.d., $\pm 2$ pA. CZ scale.
LOGARITHMIC RANGE:
$\pm 5 \mu V$ at $\pm 10 \%$ f.s.d., $\pm 5 \mathrm{mV}$ at $\pm 50 \%$ f.s.d., $\pm 500 \mathrm{mV}$ at f.s.d. RECORDER OUTPUT: $\pm 1 \mathrm{~V}$ at f.s.d. into $>1 \mathrm{k} \Omega$

£55
ty̆pe TM10 (appearance similar to type TM9B)

## D.C. MULTIMETERS

VOLTAGERANGES: $3 \mu \mathrm{~V}, 10 \mu \mathrm{~V}, 30 \mu \mathrm{~V} \ldots 1 \mathrm{kV}$
Acc. $\pm 1 \% \pm 1 \%$ f.s.d. $\pm 0 \cdot 1 \mu \mathrm{~V}$. LZ \& CZ scales.
CURRENT RANGES : $3 \mathrm{pA}, 10 \mathrm{pA}, 30 \mathrm{pA} \ldots 1 \mathrm{~mA}$ ( 1 A for TM9BP) Acc. $\pm 2 \% \pm 1 \%$ f.s.d. $\pm 0 \cdot 3 p A$. LZ \& CZ scales.
RESISTANCE RANGES: $3 \Omega, 10 \Omega, 30 \Omega \ldots 1 \mathrm{kM} \Omega 2$ linear. Acc. $\pm 1 \%, \pm 1 \%$ f.s.d. up to $100 \mathrm{M} \Omega$.
RECORDER OUTPUT: 1 V at f.s.d. into $>1 \mathrm{k} \Omega$ on LZ ranges

## £75 TM9A <br> $\mathbf{f 8 9}{ }_{\substack{\text { țм9 } \\ \text { тмя }}}$ <br> f93

## BROADBAND VOLTMETERS

H.F. VOLTAGE\&dBRANGES: $1 \mathrm{mV}, 3 \mathrm{mV}, 10 \mathrm{mV}, 3 \mathrm{f} . \mathrm{s} . \mathrm{d}$.

Acc. $\pm 4 \% \pm 1 \%$ of f.s.d. at $30 \mathrm{MHz},-50 \mathrm{~dB},-40 \mathrm{~dB},-30 \mathrm{~dB}$
to +20 dB . Scale $-10 \mathrm{~dB} /+3 \mathrm{~dB}$ rel. to $1 \mathrm{~mW} / 50 \Omega . \pm 07 \mathrm{~dB}$
from 1 MHz to $50 \mathrm{MHz} . \pm 3 \mathrm{~dB}$ from 300 kHz to 400 MHz . $\pm 0.7 \mathrm{~dB}$
L.F.RANGES : As TM3 except for the omission of $15 \mu \mathrm{~V}$ and $150 \mu \mathrm{~V}$

AMPLIFIER OUTPUT : Square wave at 20 Hz on H.F. with
amplitude proportional to square of input. As TM3 on L.F.


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# Gardne line up 

# Line MatchingTransformers from Standard to Super Fidelity 

It's easy to choose the right Line Matching Transformer from the five Gardners ranges.

The Super Fidelity Series, with a frequency response of 10 Hz to $80 \mathrm{kHz}-0.5 \mathrm{~dB}$, gives the widest possible bandwidth for high accuracy instrumentation and recording applications.

Then there's the Wide and Extra Wide-band ranges. Outstanding performers with a frequency range 30 Hz 20 kHz or more - for the 0.5 dB points. Used a lot by broadcasting and recording companies throughout the world.

The Miniature and Standard ranges provide excellent bandwidth for most purposes, 30 Hz 22 kHz for the 1.0 dB points.

Except for the very smallest in the range, all Gardners Line Matching Transformers are fully magneti-

cally shielded, giving very high hum rejection ratios.
Prices start from $£ 3.19$ (recommended retail price) and all types are usually available from stock.

Complete technical information is given in brochure GT. 5 'Audio Frequency Transformers' which we'll be glad to send on request.

So accurate is the balancing of the windings on some of these transformers that, when used as pairs in a hybrid circuit (as illustrated) we can guarantee a rejection of better than $-55 d B$ over the frequency range 50 Hz to 10 kHz and normal rejection of up to $-75 d B$ may be expected.

Specialists in Electronic Transformers and Power Supplies

# GARDNERS 

TRANSFORMERS LIMITED
Gardners Transformers Limited, Christchurch, Hampshire, BH23 3PN Tel: Christchurch 2284 (STD 02015 2284) Telex: 41276 GARDNERS XCH.

# is this the price you pay? 

Probably if you're still using an ordinary soldering iron Ordinary soldering irons can cause damage to transistors and integrated circuits - damage which wastes time and costs money. Now, with the unique ANTEX $\times 25$ and CCN low leakage soldering irons no harm can come to the most delicate equipment, even when soldered 'Live'. (You could be making quite a saving). All prices include V.A.T. at $10 \%$




# Anotheradvanced Hi-Fi stereo tape recorder/amplifier from Philips. 

3 heads.Solenoid-operated.Tip-touch controls. $2 \times 12$ watt RMS amplifier usable with the DC motors switched off. Two built-in loudspeaker enclosures.

This is the N4418, number two in the Philips range of advanced $\mathrm{Hi}-\mathrm{Fi}$ stereo tape recorders. In producing this range, Philips have drawn on decades of experience in professional tape recording installations for studios, computers and airports the world over.

Each machine easily meets the DIN 45500 standard for Hi-Fi tape recorders. Sophisticated design gives precise control, simple operation, and great reliability. Here are the main features:

4 tracks. 3 speeds $-7 \frac{1}{2}, 3 \frac{3}{4}, 1 \frac{7}{8} \mathrm{ips}$.
Suitable for stereo and mono recording and playback, multiplay, echo during recording, A-B monitoring.
$2 \times 12$ watt RMS Hi-Fi amplifier usable with recorder's motors and tape transport switched off.

Three motors - two DC motors for reel drive, one DC capstan motor electronically governed to keep tape speed constant.

Tape tension comparators for constant winding torque.

Three magnetic heads - one each for recording, playback and erase.

Detachable lower head cover for easy editing and cleaning.

For control of transport functions and recording mode, illuminated tip-touch controls are linked to solenoids - giving easier, quieter and more reliable operation.

Remote control unit (extra) with
same tip-touch buttons as recorder.
Sliding switches for function selection-selected function illuminated.

Precise sliding faders for two microphones and another signal source.

Recording stand-by (level adjustable with tape stationary).

Two illuminated calibrated VU type meters for recording/playback.

4-digit counter, zero reset, and on/off Autostop to halt tape at predetermined position.

Sockets for headphones and microphones easily accessible at front, concealed under sliding lid.

Built-in acoustical boxes giving $2 \times 6$ watts via $6^{\prime \prime} \times 4^{\prime \prime}$ loudspeakers.

Reels lockable by means of metal hub locks.

Removable transparent lid.
Amplifier detachable in one unit leaving recorder functioning.
Frequency response:
$40-20,000 \mathrm{~Hz}$ at $7 \frac{1}{2} \mathrm{ips}$ $40-16,000 \mathrm{~Hz}$ at $7 \frac{1}{2} \mathrm{ips}$ with built-in stereo interference filter.

DIN 45500
$40-15,000 \mathrm{~Hz}$ at $3_{4}^{3} \mathrm{ips}$ $60-8,000 \mathrm{~Hz}$ at $1 \frac{7}{8} \mathrm{ips}$
Wow and Flutter $<0 \cdot 15 \%$ at $7 \frac{1}{2}$ ips.
See your Philips dealer for a demonstration. And for a free book on all Philips Hi-Fi stereo tape recorders, write to Philips Electrical Limited, Dept SP, Century House, Shaftesbury Avenue, London WC2H 8AS.


## AnDER5 MEAIS METERS...

## REGAL RANGE

- New $100^{\circ}$ arc high quality meters at low prices.
- Rugged taut band construction - pivot and jewel available to order

Sensitivities to $10 \mu \mathrm{~A}$Very competitively priced for OEM quantities

- Modern styled meters in matt black plastic cases with flattened arc giving long scale.

TWO MODELS
R55 $2.5 \mathrm{in}(63.5 \mathrm{~mm})$ Scale length
R65 3.2in ( 81.3 mm ) Scale length

Anders provide what is probably the largest range of meters available from a single source in Europe: MC/MI, dynamometer, vibrating reed, electrostatic, etc. in over 100 case styles and sizes, a few of which are shown below.


Popular models and ranges are stocked in depth while a specially equipped instrument department enables swift production of non-standard ranges and scales, to suit individual customer requirements, in large or small quantities.


Vulcan Moving Iron. 4 models, $1 \cdot 5^{\prime \prime}, 1 \cdot 8^{\prime \prime}, 2 \cdot 7^{\prime \prime}$, $3 \cdot 7^{\prime \prime}$ scales. Voltmeters, ammeters and motor starting meters.


Kestrel Clear Front. 7 models, 1:3"-5•25" scales. DC moving coil, AC moving coil rectified, $A C$ moving iron.


Profile 350 edgewise $4 \cdot 3^{\prime \prime}$ scale
DC moving coil and AC moving coil rectified. Horizontal or vertical mounting.


Oxford Long Scale $240^{\circ}$. 2 models, $5 \cdot 5^{\prime \prime}, 8^{\prime \prime}$ scales. DC moving coil and AC moving coil rectified.


Stafford Long Scale 240 6 models, $3.5^{\prime \prime}-11 \cdot 5^{\prime \prime}$ scales. DC moving coil, AC moving coil rectified, AC moving iron. Alsp 98 scale.


Models KE1 and KE2
Miniature Edgewise
Meters. Nominal scale lengths $1.2^{\prime \prime}$ and $2^{\prime \prime}$. Available in sensitivities from 50 microamps Moving Coil.


Lancaster Long Scale 240 . 2 models, $4^{\prime \prime}, 5 \cdot 5^{\prime \prime}$ scales. DC moving coil and $A C$ moving coil rectified.

RIDERS ELECTROMILS LIMITED ${ }_{48 / 56}$ Bayham Pace, Bayham Street. London, N.w.1. Telephone $01-3879092$.
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B \& W are not playing hard to get. Far from it.
We've appointed - very selectively - a national network of Authorised B \& W Dealers to demonstrate, install and service our famous loudspeakers.

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Ask to hear B \& W speakers where you see the sign; it could be the beginning of a totally rewarding experience.

B \& W loudspeakers are in great demand abroad. So much so. we have been honoured with the Queens Award to Industry for export achievement.

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Contact us at Mullard for all your 'communications' components... components for telecoms, broadcasting, radar and navaids. We have unique resources for their development and production, and have devoted literally millions of pounds to meeting the component needs of manufacturers of
communications equipment.
Some of our products are well-established favourites, others are at the forefront of current technology.
Some are made on an extremely large scale, some are customer specials. Please let us know of your own particular requirement.

## VARACTOR <br>  <br> 

New tuning and multiplier types amnounced

Tuning Varactors
Three new silicon varactor diodes, all with a wide electronically tuned capacitance range, have been introduced by Mullard. Designated types BXY53, BXY54 and BXY55, they have total capacitance ratios of $4.0,6.5$ and 7.0 respectively. Typical capacitances at -4 V are $1.0,4.7$ and 15pF. Reverse ratings are 60 V at $10 \mu \mathrm{~A}$. Low insertion loss, another important feature, is $0.8,0.5$ and 0.25 dB for the three types respectively (this is under small signal conditions with the diode at the end of a $50 \Omega$ transmission line, and measured at 2 GHz for the BXY53 and BXY54, and at 1 GHz for the BXY55).

The new tuner and multiplier varactors come in the same type of standard microwave package.

Multiplier Varactors
Two silicon multiplier varactors have also been announced. These are high efficiency types BXY56 and BXY57, and are intended for use in both low and high order multiplier circuits with output frequencies in the range 3 to 8 GHz . Cut-off frequencies at -6 V are 160 and $140 \mathrm{GH}_{3}$ respectively. Power ratings are 5.2 and 6.6 W , and the reverse rating is 60 V for both types. For further information on all five of these new varactors please use reader enquiry service no. WW 100 .

\title{

Unique transistors-unique performance

\section*{forTV transposer

## forTV transposer service

The very strict requirements that have to be met by power amplifiers in TV transposers are reflected in the performance that is expected of individual transistors.

Mullard transposer transistors are available which are unique in being designed, specified and guaranteed for this special application. The d.c. safe operating area is exceptionally large compared with earlier types, making for completely safe operation at high powers in class A and ensuring extremely low intermodulation distortion. Furthermore, they are $100 \%$ individually tested for intermodulation in the manner prescribed by transposer manufacturers.

An advanced diffusion process is employed in which arsenic is used as an emitter dopant. This allows the
depth of diffusion to be very accurately controlled and a very thin base is obtained giving a minimum $\mathrm{f}_{\mathrm{T}}$ of 2 GHz . The maintenance of high performance over a long operating life is assisted by the employment of a sophisticated gold metallisation system.
At 860 MHz , the most powerful member of the Mullard transposer transistor family, the BLX98, has a power gain of typically $5 \cdot 0 \mathrm{~dB}$, giving a minimum output of 3.5 W with intermodulation distortion better than 60 dB . For data on this device please use reader enquiry service no. WW 101.

## FREQUENCY AGILITY...



Radar jamming, both unintentional and deliberate, can be overcome by the use of frequency agile systems. This well-known fact has tended to obscure the many other important advantages which frequency agile radars offer.
They greatly facilitate the detection of fluctuating echoes and so give increased range. They reduce the effects of 'glint', or interference between echoes from different parts of the target, and so enhance tracking accuracy. They provide for decorrelation of the target from clutter. And they completely eliminate early or 'second-time-round' echoes.

The key components for such systems-frequency agile magnetrons and voltage-controlled local oscillators-have been developed by Mullard against the background of a thorough study of fast AFC and related system requirements.

The Mullard magnetrons are spin-tuned, the internal tuning element being rotated via a magnetic
coupling through the vacuum envelope. A rapid and truly random variation of frequency over the operating band is obtained. A typical 100 kW X-band magnetron being made at Mitcham sweeps through 450 MHz in $500 \mu \mathrm{~s}$. Other types can be supplied, including those for J-band, and preset frequency locks can also be provided.

Mullard local oscillators for this type of application are realised in the form of microstrip integrated circuits, and a typical LO comprises a linearised varactor-tuned transistor oscillator multiplier. A salient feature of the device and its control system is, of course, its ability to follow the magnetron's large and rapid frequency variations.

A good introduction to this whole subject is provided by Frequency Agile Radar-a review of techniques and advantages. Write to Dept. CMS/C14 at Mullard House for a free copy.

## Mobile design... WHY DO IT THE HARD WAY?

A visitor to our Application Laboratory recently couldn't believe his eyes when we showed him one of our u.h.f. wideband amplifier modules. He held the inch-long pack in the palm of his hand, and it took a demonstration to convince him that it could be taken straight from its wrapping and cover the band 380 to 512 MHz without any tuning or 'tweaking up' whatsoever. In fact


Mullard u.h.f. modules are completely encapsulated and the question of tuning or trimming simply does not arise.

They have outputs of 2.5, 7.0 and 17 W . And if you want to couple them together there are no problems: they all have $50 \Omega$ input and output impedances. There are many other features attractive to the equipment designer. They will withstand load mismatch, they will accept input overdrive and they will remain stable even when the supply voltage sinks to 10.5 V or rises to 16.5 V .

Naturally they cost somewhat more than the sum of the discrete components, but this is more than outweighed by the time you save on design, manufacture and test. All very well for the designer, but also very well for the user and maintenance engineer. For data please use reader enquiry service no. WW 102.

> Latest broadband transistors boost performance of TV distribution systems

The excellent broadband performance of Mullard transistors such as the BFY90 and BFW16A has led to their widespread use in TV aerial amplifier and distribution systems.

These well known types are now being supplemented by a new family which, thanks to an advanced diffusiontechnology, has an eyen higher performance. It comprises types BFR90, $91,92,93,94 \& 96$ which are ideally suited for operation from 40 to 900 MHz and give an output of up to 1 V across $75 \Omega$. All are individually tested for essential parameters such as intermodulation and crossmodulation distortion.

Using BFR94s, for instance, a push-pull amplifier can be made with a bandwidth of 40 to 300 MHz , and featuring 12 -channel cross-modulation distortion of only -98 dB at an output of 32 dBmV . The 3.5 GHz transition frequency of the BFR94 results in an amplifier with high power gain and a noise figure which is almost independent of frequency.

For data on transistors in the new family please use reader enquiry service no. WW 103.



## If the answer's'yes' think Ferroxcube and contact Mullard.

Full data for RM and pot transformer cores is given in the Mullard Technical Handbook (Book 3, Part 2). Use reader enquiry service no. ... for a Handbook order form and descriptive leaflet.

## FOUR ADVANCED PLUMBICON TUBES MARK 10TH ANNIVERSARY

Four new Plumbicon tubes, the most advanced yet, are being announced this year, the tenth anniversary of the introduction of this kind of TV camera tube. Plumbicon tubes are now regarded internationally as 'standard'-in fact $90 \%$ of the world's colour TV cameras are fitted with them.

The four new tubes are additions to the Mullard 1-inch XQ1080 family. They feature a unique anti-comettail gun and bias light pipe, and antihalation discs are fitted as standard. Output capacitance is low and ensures optimal signal-to-noise ratio.

All four new types have an ex-
*Registered trademark for TV camera tubes

# Simplergigahertz amplifiers with new transistor 

A new n-p-n silicon transistor featuring a very high transition frequency and low noise has been announced by Mullard. With a noise figure of $4 \cdot 0 \mathrm{~dB}$ at 2 GHz and a power gain of 8 dB this new device, the $551 \mathrm{BFY} / \mathrm{A}$, considerably simplifies u.h.f. and microwave repeater station design.

Broadband amplifiers with centre frequencies of up to 2 or 3 GHz can be designed relatively easily by taking advantage of the high gain of the 551BFY/A. With it microwave re-
tended red response and are intended for monochrome and red chrominance channels. The spectral response cut-off of broadcast tube XQ1083 and its industrial counterpart XQ1084 is 900 nm . Broadcast tube XQ1085 and its industrial counterpart XQ1086 are of similar construction but have infrared filters giving cut-off at 750 nm .

peaters can be made to operate on a 'straight through' basis, there being no need for conversion down to an intermediate frequency.

In radar systems, too, and ultra high-speed data communications systems operating at gigahertz bit rates the $551 \mathrm{BFY} / \mathrm{A}$ is an extremely attractive device. An interesting military application is in electronic warfare countermeasures where it can replace travelling wave tubes in octave band amplifiers.

The typical transition frequency of the $551 \mathrm{BFY} / \mathrm{A}$ (at $\mathrm{f}=500 \mathrm{MHz}$ ) is $5 \mathrm{GHz} . \mathrm{V}_{\mathrm{CBO}}$ max. is 20 V , and $\mathrm{I}_{\mathrm{C}}$ max. 25 mA . Total permissible powerdissipation up to ambient temperatures of $60^{\circ} \mathrm{C}$ is 300 mW . A miniature ceramic encapsulation is used which is compatible with strip-line and microstrip circuits. For data please use reader enquiry service no. WW104.

## Contact Colimn

AGOOD'BUYIN'
The case for buying in sub-systems or sub-assemblies instead of working with discrete components is not always indisputable. But in many areas there are clear-cut savings to be made on development and production costs and, quite frequently, there are size and performance advantages. The modules for mobile transmitters described in this 'Contact' are a case in point. The microwave field is another.
The Mullard company is particularly well placed for this kind of microwave activity. Not only does it have the resources to design and manufacture microwave sub-systems, it designs and makes the discrete components as well. There is complete vertical integration of the whole activity, and consequent economic and technical advantages.

Much of this Mullard work has in the past involved conventional 'three dimensional' components and waveguide technology, but microwave integrated circuits using microstrip technology are now assuming greater importance.

With the tremendous advances being made in discrete microwave devices, it is not surprising that thin film circuits are more appropriate for many sub-systems. A Gunn diode of micron dimensions, for instance, is incongrous when used with 3 cm waveguide plumbing. And with transistors having an $\mathrm{f}_{\mathrm{T}}$ of 5 GHz allied solid-state techniques must be used for the circuitry.

However, the customer's first need is to know whether a 'subsystem approach' is viable for his particular project. This he can find out by supplying Mullard with a 'black box' specification. A technical appraisal will be prepared and sent to him in about three weeks.

By 'Electron'

## Voretexínin

50/70 WATT ALL SILICON AMPLIFIER WITH BUILT-IN 4-WAY MIXER USING F.E.T.s.

This is a high fidelity amplifier ( $0.3 \%$ intermodulation distortion) using the circuit of our $100 \%$ reliable 100 Watt Amplifier with its elaborate protection against short and overload, etc. To this is allied our latest development of F.E.T. Mixer Amplifier, again fully protected against overload and completely free from radio breakthrough


The mixer is arranged for $2-30 / 60 \Omega$ balanced line microphones, 1 -HiZ gram input and 1 -auxiliary input followed by bass and treble controls. 100 volt balanced line output or $5 / 15 \Omega$ and 100 volt line.

## 50/70 WATT ALL SILICON AMPLIFIER WITH BUILT-IN 5-WAY MIXER USING F.E.T.S This is similar to the 4 -way version but with 5 inputs and bass cut controls on each of the three low impedance balanced line microphone stages, and a high impedance ( 10 meg ) gram stage with bass and treble controls plus the usual line or tape input. All the input stages are protected against overload by back to back low noise, low intermodulation distortion of mains supply fluctuations and another stabilised supply for the driver stages is arranged to cut off when the output is overloaded or over temperature. The output is $75 \%$ efficient and 100 V balanced line or $8-16 \Omega$ output are selected by means of a rear panel switch which has a locking plate indicating the output impedance selected. The Mixer section has an additional emitter follower output for driving a slave amplifier, phones or tape recorder, output 3 V out on 600 ohms upwards.

100 WATT ALL SILICON AMPLIFIER. A high quality amplifier with 8 ohms- 15 ohms or 100 volt line output for A.C. Mains. Protection is given for short and open circuit output over driving and over temperature. Input 0.4 V on 100 K ohms.

THE 100 WATT MIXER AMPLIFIER with specification as above is here combined with a 4-channel F.E.T. mixer, $2-30 / 60 \Omega$ balanced microphone inputs. $1-\mathrm{HiZ}$ gram input and 1 -auxiliary input with tone controls and mounted in a standard robust stove enamelled steel case. A stabilised voltage supply feeds the tone controls and pre amps, compensating for a mains voltage drop of over $25 \%$ and the output transistor biasing compensates for a wide range of voltage and temperature. Also available in rack panel form.

CP50 AMPLIFIER. An all silicon transistor 50 watt amplifier for mains and 12 volt battery operation, charging its own battery and automatically going to battery if mains fail. Protected inputs, and overload and short circuit protected outputs for 8 ohms- 15 ohms and 100 volt line. Bass and treble controls fitted.

Models available with 1 gram and 2 low mic. inputs, 1 gram and 3 low mic. inputs or 4 low mic. inputs.

200 W.ATT AMPLIFIER. Can deliver its full audio power at any frequency in the range of $30 \mathrm{c} / \mathrm{s}-20 \mathrm{Kc} / \mathrm{s}$ $\pm 1 \mathrm{~dB}$. Less than $0.2 \%$ distortion at $1 \mathrm{Kc} / \mathrm{s}$. Can be used to drive mechanical devices for which power is over 120 watt on continuous sine wave. Input 1 mW 600 ohms. Output $100-120 \mathrm{~V}$ or $200-240 \mathrm{~V}$. Additional matching transformers for other impedances are available.

20/30 WATT MIXER AMPLIFIER. High fidelity all silicon model with F.E.T. input stages to reduce intermodulation distortion to a fraction of normal transistor input circuits. The response is level 20 to $20,000 \mathrm{cps}$ within 2 dB and over 30 times damping factor. At 20 watts output there is less than $0.2 \%$ intermodulation even over the microphone stage at full gain with the treble and bass controls set level. Standard model 1 -low mic. balanced and 1 auxiliary input.

Every Tannoy "Monitor Gold" dualconcentric loudspeaker is individually tested and given its own serial number. Every "Monitor-Gold" has a frequency curve taken on Brüel \& Kjaer measuring equipment, and a copy of this curve will, in future, be provided with every unit.

|  | $10^{\prime \prime}$ | $12^{\prime \prime}$ | $15^{\prime \prime}$ |
| :--- | :---: | :---: | :---: |
| Power Handling Capacity | 25 W | 35 W | 50 W |
| Frequency Response | $27-20,000 \mathrm{HZ}$ | $25-20,000 \mathrm{HZ}$ | $23-20,000 \mathrm{HZ}$ |
| Intermodulation Products | less than $2 \%$ | less than $2 \%$ | less than $2 \%$ |
| Impedance via <br> Crossover network | 8 ohms <br> (5 ohms min.) | 8 ohms <br> (5 ohms min.) | 8 ohms <br> (5 ohms min.) |

The whole range of Tannoy Dual-Concentric units sounds very similar, depending on the selected enclosure, and the different types are ideal for combinations in Quadraphonic systems.


Response curve of $12^{\prime \prime}$ Monitor Gold mounted on Works test Enclosure
Norwood Road, West Norwood, London SE27 9AB Tel: 01-670 1131


Electronic valves (a comprehensive range) semi-conductors (a wide variety) integrated circuits... and now a comprehensive range of Hybrid Microcircuits. Prices on request.

Teonex offers more than 3,000 devices. They are competitively priced and they are superlative in performance because the company imposes strict quality control. Teonex concentrates entirely on export and now operates in more than sixty countries on Government or private contract. All popular types in the Teonex range are nearly always available for immediate delivery. Write now for technical specifications and prices: Teonex Limited, 2a Westbourne Grove Mews, London W11 2RY, England. Cables: Tosuply London W11. Telex : 262256 $\qquad$ AVAILABLE ONLY FOR EXPORT

## New automatic digital bridge from Wayne Kerr



Wayne Kerr's new 8900 is one of the best value-for-money bridges in the world.

It is universal, has a wide range, and gives immediate digital readout of resistive and reactive terms-simultaneously.

On all ten ranges, for every type of measurement available, the displays provide a complete indication of the numerical value (up to 19999), polarity, decimal points and units-automatically and in half a second.

Direct measurements of $Q$, dissipation and dc volts. 2,3,\& 4-terminal. Automatic lead compensation. 4- Quadrant: + ve or - ve C, L, 1/C, G and R. Overall coverage:

$$
\begin{array}{lll}
10 \mu \Omega-200 \mathrm{M} \Omega & 1 \mathrm{nH} & -20 \mathrm{kH} \\
0.001 \mathrm{pF}-20,000 \mu \mathrm{~F} & 10 \mathrm{p} v & -200 v
\end{array}
$$ Accuracy: $0.1 \%(10 \Omega-200 \mathrm{M} \Omega), 0.3 \%(10 \mathrm{~m} \Omega-10 \Omega)$ in all quadrants. Frequency: 1 kHz Outputs: Analog and TTL.

For more information phone Bognor (02433) 25811, or fill in the coupon.

## - Unilits

Nat KEF ELECTRONICS LIMITED TOVIL MAIDSTONE ME15 6QP Tel 062257258

Reg in England No 702392

Research based on the premise that loudspeakers could be made to reproduce sound more accurately by the efficient utilisation of plastics and metal alloys has enabled KEF engineers to evolve the current range of chassis speakers.

Results of research on these materials plus spin-off from other technologies has enabled KEF to achieve precise quality control in production, reliability and accurate sound reproduction under wide extremes of operating conditions.

Many of the world's leading manufacturers recognise these salient points and insist on using KEF drive units in their equipment.

Full details of chassis speakers and dividing networks are available on request.


WW-014 FOR FURTHER DETAILS

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| BY127 |  | 1250 V |  | IA |  |  |  | OA8 |  | 7p |
| BZYIO |  | 800 V |  | 6A |  |  |  | OA90 |  | 5p |
| BZil3 |  | 200 V |  | 6A |  |  |  | OA9 |  | 5 P |
| IN400\| |  | 50 V |  | IA |  | p |  | OA2 |  | 7p |
| IN 4004 |  | 400 V |  | 1 A |  | p |  | IN41 |  | 5p |
| - N4007 |  | -1000V |  | IA |  |  |  | BAll |  | 8p |
| BRUSHED ALUMINIUM PANELS$12 \mathrm{in} \times 6 \mathrm{in}, 25 \mathrm{p} ; 12 \mathrm{in} \times 2 \frac{1}{2} \mathrm{in}, 10 \mathrm{p} ; 9 \mathrm{in} \times 2 \mathrm{in}, 7 \mathrm{p}$ |  |  |  |  |  |  | THERMISTORS |  |  |  |
|  |  |  |  |  |  |  |  | $1055 S$ |  | 15p |
| SLIDER POTENTIOMETERS |  |  |  |  |  |  |  |  |  | $\begin{array}{r} 15 p \\ 61.35 \end{array}$ |
| $86 \mathrm{~mm} \times 9 \mathrm{~mm} \times 16 \mathrm{~mm}$, length of track 59 mm . <br> SINGLE IOK, 25 K , IOOK log. or lin. 40p. |  |  |  |  |  |  |  |  |  |  |
| DUAL GANG, IOK + loK etc. log. or lin. 60p. <br> KNOB FOR ABOVE, 12 p . <br> FRONT PANEL, 65p. |  |  |  |  |  |  | THY | RISTO |  |  |
|  |  |  |  |  |  |  |  | 506050 | 0.8A | 30p |
| 18 Gauge panel 12 in $\times 4$ in with slots cut for use with |  |  |  |  |  |  |  | 5064200 | 0.8A | 47p |
| slider pots. Grey or matt black finish complete |  |  |  |  |  |  |  | F 50V |  | 40p |
| with fixings for 4 pots. |  |  |  |  |  |  | 10 | D 400 V | 4A | 55p |

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# Wireless World 

Electronics, Television, Radio, Audio

November 1973
Volume 79 Number 1457


This month's cover picture shows the sealing in of the "works" of a digital wristwatch, including a Monsanto l.e.d. display seen as the dark rectangle in the middle.

## In our next issue

(publication date November 19)
Active filters used with loudspeakers can provide greater flexibility and overcome inherent disadvantages of the passive crossover network.
Using opto-couplers. An investigation into the noise behaviour of these devices used in conjunction with transistors.

## Contents

523 Integrated Circuits in the U.K.
524 Model Railway Control System by P. Cowan
528 News of the Month
"Donald Duck" eliminators
Largest solid-state image sensor
Component tester for relay systems
529 Multi-flash Trigger Unit by R. Lewis
532 Letters to the Editor
Hi-fi equipment standards
Using c.m.o.s. devices
Radiating coaxial cables
535 Dual-polarity Digital Voltmeter - 2 by A. J. Ewins
540 November Meetings
541 Entertainment Electronics at Berlin
545 Audio Fair Preview
547 An Automatic Noise Limiter by P. Hinch
548 Sound Recorder uses P.C.M.
550 World of Amateur Radio
551 Tuners and Tuner Amplifiers by Basil Lane
557 Circards - 11: Basic logic circuits by J. Carruthers, J. H. Evans, J. Kinsler \& P. Williams

559 H.F. Predictions
560 Circuit Ideas
Adjustable current regulator
Deflection amplifier
Simulating electrolytics
561 10-2 Metre Amateur Transverter by D. R. Bowman
566 Sixty Years Ago
567 Linear Voltage-controlled Oscillator by J. L. Linsley Hood
569 Books Received
570 Which Way does Current Flow? by "Cathode Ray"
571 New Products
A116 APPOINTMENTS VACANT
A142 INDEX TO ADVERTISERS

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## Integrated Circuits in the U.K.

About six years ago we took a look at the British integrated circuits industry (Leader, Dec. 1967) and declared that 1968 may well be remembered as the year in which "the British electronics industry finally kept its national identity or became predominantly American controlled". This of course referred to control of equipment design through control of the design and marketing of integrated circuits. In fact there was not a particular critical year in which everything happened, but since 1968 we have seen the American and other foreign companies progressively increasing their hold over the U.K. integrated circuits market, until now the British i.c. manufacturers jointly have only 10-15 per cent of the market. In 1968 there were six wholly Britishowned i.c. firms in operation; now there are only three, Ferranti, G.E.C. and Plessey. The greater part of the i.cs used by British equipment manufacturers is imported from about 18 American companies (led by Texas, Motorola, Fairchild, National Semiconductor and Signetics) and four European owned companies (the Philips group which has Mullard in the U.K. Valvo in Germany and R.T.C. in France - and Siemens, SGS-ATES and SESCOSEM).

What happened after 1968 was a period of over-production of i.cs and a worldwide price war, resulting from the 1970-71 depression in trade, which caused the prices of i.cs to fall from pounds to pence. The British firms were unable to compete and only the large American companies were able to sustain the low prices. The duplication of effort on such things as the 7400 series of devices did not help matters.

There was one development after 1968, however, which we hinted would help the British i.c. industry and which did in fact take place. This was the increase in demand from equipment manufacturers for special i.cs, tailor-made for particular applications - as distinct from "off-the-shelf" devices. This type of product requires close cooperation between the i.c. and equipment makers, and in Britain this obviously works best when both parties are British, since discussions on whether to manufacture the i.cs do not have to be referred back to headquarters in some other country. It is for this kind of operation that the Government, through the D.T.I., is helping financially to support a research and development programme - up to $£ 10 \mathrm{~m}$ spread over 6-7 years. There may be additional, but probably smaller, support from the Ministry of Defence.
The trouble is that this kind of money will not go very far in present conditions. Such is the rate at which integrated circuit technology is changing - complete new classes of device appearing every few months - that any manufacturer needs a continuous injection of money into research and development just in order to stay in the race, let alone moving ahead of his competitors.

Now that we are in the Common Market it may seem inappropriate to show concern for the fate of a particular industry in a particular country: after all, we are all Europeans now. But the fact remains that our national standard of living still depends on the performance of our national manufacturing industries. Maybe we can still live by exporting woollen goods and Scotch whisky, but to neglect the huge potertialities of the world electronics market - which is expected to reach an annual $£ 40,000 \mathrm{~m}$ by about 1980 - is one way of helping the British to become what has already been suggested. "the peasants of Europe".

# A two-rail layout fitted with working whistle, speed control and coach interior illumination. 

by P. Cowan

The system of model train control to be described is such that any chosen function does not interact with nor is dependent on any other function. No interconnections of rolling stock are necessary. High frequency a.c. is not used, removing problems in connection with interference. All commands are operable from a trackside controller and no sequential actions are necessary.

The system uses d.c. levels for each function and in the case of the locomotive the level is switched with deliberately slow ( $0.2-0.5 \mathrm{~ms}$ ) rising and falling edges at 100 Hz , each piece of rolling-stock and the locomotive being fitted with a simple "level sensor". The "inertia" of the system is such that the slow rising and falling edges are not evident in practice except in that they remove interference with other apparatus - a problem which is evident when high frequency a.c. is applied to a model railway layout. The use of d.c. levels enables quite high powers to be transmitted down the rails without having to resort to tuned filters and/or large capacitors. The circuits are also easy to make and set up.

Fig. 1 shows a typical train movement. Here. the whistle is allocated 3 V , the lights 6 V and the locomotive 12 V . Init ially, with a complete train at rest and all functions off at $T=0$, the whistle is sounded (a). At (b) the train moves off slowly with whistle still on and at (c) the whistle is turned off and the train continues moving forward slowly. At (d) the driver turns on the coach lights (the train still moving forward slowly), at (e) the whistle is sounded, coach lights are on and the train is picking up speed. At (f) the whistle is off, the locomotive and train are coasting, leaving only the lights turned on.

In practice it is better to arrange for the "voltage separation per function" to increase with increasing current demand from the train to make an allowance for volts dropped down the rails as the train moves away from the power connection point. The system described has worked without trouble on a Club layout 35 feet by 10 feet, including several points and crossovers with attendant contacts.

The power diagram in Fig. 2 shows how the voltage separation per function is arranged in the practical controller cir-

cuit and details of each function's operating voltage. It can be seen that each function operates over a particular range of voltage about a correct voltage level, allowing for volts dropped down the rails and, within limits, keeping the system in sync. For example, the whistle operates at 19.5 V when blown with the loco running but will still work correctly down to 16 V , giving 3.5 V safety margin. Fig. 2 also shows the voltage levels that each sensor must accept; and those that are to be rejected, together with details of the output current that the controller must supply.

## Circuit description

Power supply (controller). Unregulated d.c. is derived from the a.c. mains by the transformer, the bridge rectifier and $C_{1}$ in Fig.3. Transistors $\operatorname{Tr}_{11}, \operatorname{Tr}_{12}, T r_{9}$ and $T r_{10}$, $D_{2-4}$ and $Z_{3-6}$ form a simple regulator of output voltage according to the selected diodes. $C_{9}$ and $C_{10}$ suppress any tendency to oscillate and $C_{\vee}$ and $C_{11}$ control the rise and fall times of the pulsed supply. A further regulated supply line ( 12 V ) is provided by $Z_{1}, R_{3}$ and $C_{2}$ to power the pulse generator which is made up of $T r_{1-3}$ as a ramp generator, and $T r_{6}$ and $T r_{7}$ as a Schmitt trigger, $R_{76}$ controlling the mark/space ratio at the output. Transistors $\operatorname{Tr}_{4}$ and $\operatorname{Tr}_{5}$ and their attendant components enable auto-run-up to full speed and auto-rundown to stop to be selected via $S_{1}$ or $S_{2}$ respectively. Components $S_{3}$ and $Z_{2}$ form a "skid" control enabling momentary full power to be applied. A fast overload trip to safeguard the controller and associated circuitry is formed by $T h_{1}, R_{1}$ and $R_{75}$, $D_{1}, L_{2}$ and $R_{32}$. The action of overload is indicated by $L p_{2}$. The trip should be set to not less than 5 A by $R_{75}$. Components

Fig. 1. A complete train movement, showing all functions operating.


Fig. 2. Switching points recognized by the sensors of the whistle (A), the lights (B) and the locomotive motor (C).

$R_{80}$ and $R_{82}$ are delay run up and down adjustments and are fitted to the front panel of the controller as are $S_{1}, S_{2}, S_{3}, S_{4}$, and $S_{5}$. Switch $S_{4}$ is a a ganged micro-switch and is the whistle on/off. Switch $S_{5}$ is a 3-pole change-over rotary switch operating the lights. Transistor $\operatorname{Tr}_{12}$ should be fitted to a heat sink of the standard finned type ( 6 in $\times$ $4 \frac{1}{2}$ in) with eight $1 \frac{1}{2}$ in longitudinal fins. The resistor $R_{9}$ causes a slight shift in frequency from approximately 100 Hz to 120 Hz as loco power output is increased, which can be used to give diesel locomotives an exhaust rate effect.

Lamps (coach illumination). From Fig. 2 it can be seen that the coach sensor should be able to command "lights on" from 5.5 to 11.5 V . This is accomplished by $T r_{14}, R_{42}, T r_{16}$ and $Z_{8}$, in Fig. 4, the biasing of $T_{14}$ being set by $R_{76}, R_{43}$, $Z_{7}$ and $R_{4}$. Turn off at 11.5 V is done by $T_{13}$, biased by $R_{38}, R_{39}$ and $Z_{17}$. Further reference to Fig. 2 shows that lights should be on again at 21.5 V (to maximum voltage of 29.5 V ), and this is done by $\operatorname{Tr}_{15}$ and $R_{43}$ through biasing components $R_{77}, R_{44}$ and $Z_{9}$.

Whistle sensing and regulation circuit. This circuit, shown in Fig. 5, is similar in principle to the "lights" circuit, the correct "turn on whistle" voltages being sensed by $T r_{18}$, $T r_{20}, T r_{23}$, and $T r_{26}$ and the "turn off whistle " voltages by $T r_{17}, T r_{22}$ and $T r_{24}$, The regulation of the supply to the "whiste" is achieved by dropping excess voltages across $R_{50}, R_{63}$ and $R_{64}$. Components
marked with an asterisk may require small adjustments to allow for component tolerances and to achieve the correct turn on and off values as detailed in Fig. 2.

Whistle. The circuit is that of an astable multivibrator with the drive waveform to the whistle suitably "adjusted" to make the sound from the Dictaphone earpiece sound like a "whistle". If an earpiece is unobtainable a $10 \Omega$ portable radio earpiece can be used instead.

Locomotion circuit. In this circuit (Fig. 6) care has to be taken to ensure that $\operatorname{Tr}_{28}$ and $T r_{31}$ are able to dissipate heat, prefererably through the locomotive chassis.

In practice, about 6 W under full load conditions and 4.5 W nominal are dissipated. The average locomotive chassis is usually more than adequate and is often even painted matt black; Hornby and Trix tender drive locomotives have been modified quite successfully. In the case of the tender drive types the power transistors $\operatorname{Tr}_{28}$ and $T r_{31}$ were mounted on the tender chassis with the rest of the circuitry built round the propulsion motor, the whistle and sensor being mounted within the locomotive body. In addition to sensing the locomotion voltage level this circuit has to work with either polarity applied. With positive on the earth rail then $\operatorname{Tr}_{27}{ }_{28}{ }_{28}, 29$, etc are isolated by diodes $D_{13}$ and $D_{14}$.


Fig. 4. Circuit diagram of the coach lights controller.


Fig. 5. Whistle level sensing and regulation circuit. Components marked with an asterisk may need adjustment to achieve the the correct switching levels.

## Component list

## Resistors

|  |  |  |  |
| :---: | :---: | :---: | :---: |
| $R_{1}$ | $0.5 \Omega 5 \mathrm{~W}$ | $R_{\text {d2 }}$ | $100 \Omega$ |
| $R_{2}$ | $470 \Omega 2 \mathrm{~W}$ | $R_{4}$ | 100 2 |
| $R_{3}$ | $680 \Omega 2 \mathrm{~W}$ | $R_{14}$ | (18-27k $\Omega$ ) |
| $R_{4}$ | $270 \Omega$ | $R_{4}$ | $8.2 \mathrm{k} \Omega$ |
| $R_{\text {s }}$ | $3.3 \mathrm{M} \Omega$ | $R_{46}$ | $1.5 \mathrm{k} \Omega$ |
| $R_{6}$ | $10 \Omega$ ? | $R_{47}$ | ( $2.7 \mathrm{k} \Omega \frac{1}{4} \mathrm{~W}$ ) |
| $R_{7}$ | $100 \Omega$ | $R_{48}$ | 39, |
| $R_{\text {g }}$ | $180 \mathrm{k} \Omega$ | $R_{89}$ | $2.2 \mathrm{k} \Omega$ |
| $R_{9}$ | $2.2 \mathrm{M} \Omega$ | $R_{\text {s0 }}$ | $100 \Omega \frac{1}{2} \mathrm{~W}$ |
| $R_{10}$ | $1.8 \mathrm{k} \Omega$ | $R_{51}$ | $2.2 \mathrm{k} \Omega$ |
| $R_{11}$ | $22 \mathrm{k} \Omega$ | $R_{52}$ | (470 $\left.2 \frac{1}{2} \mathrm{~W}\right)$ |
| $R_{12}$ | $1 \mathrm{k} \Omega$ | $R_{53}$ | $3.9 \mathrm{k} \Omega$ |
| $R_{13}$ | $10 \Omega$ | $R_{\text {St }}$ | $2.2 \mathrm{k} \Omega$ |
| $R_{1+}$ | $1 \mathrm{k} \Omega$ | $R_{\text {s }}$ | $10 \Omega$ <br> "DICTAPHONE" <br> earpiece |
| $R_{15}$ | $2.2 \mathrm{k} \Omega$ | $R_{56}$ | (1kS) |
| $R_{16}$ | $47 \mathrm{k} \Omega$ | $R^{37}$ | $270 \Omega$ |
| $R_{17}$ | $1 \mathrm{k} \Omega$ | $R_{\text {sy }}$ | $680 \Omega$ |
| $R_{18}$ | $2.2 \mathrm{k} \Omega$ | $R_{\text {s, }}$ | $1.5 \mathrm{k} \Omega$ |
| $R_{19}$ | $47 \mathrm{k} \Omega$ | $R_{60}$ | $680 \Omega$ |
| $R_{20}$ | $1 \mathrm{k} \Omega$ | $R_{61}$ | ( $5.1 \mathrm{k} \Omega$ ) |
| $R_{21}$ | $10 \Omega$ | $R_{62}$ | $100 \Omega$ |
| $R_{22}$ | $4.7 \mathrm{k} \Omega$ | $R_{63}$ | $150 \Omega \frac{1}{2} \mathrm{~W}$ |
| $R_{2,}$ | $1 \mathrm{k} \Omega$ | $R_{64}$ | $150 \Omega \frac{1}{2} \mathrm{~W}$ |
| $R_{24}$ | $2.2 \mathrm{k} \Omega$ | $R_{65}$ | $10 \mathrm{k} \Omega$ |
| $R_{25}$ | $470 \Omega$ | $R_{66}$ | $1 \mathrm{k} \Omega \frac{1}{4} \mathrm{~W}$ |
| $R_{26}$ | $27 \mathrm{k} \Omega$ | $R_{67}$ | $100 \Omega 2 \mathrm{~W}$ |
| $R_{27}$ | $33 \mathrm{k} \Omega$ | $R_{68}$ | 47S |
| $R_{28}$ | $10 \mathrm{k} \Omega$ | $R_{69}$ | $47 \Omega$ |
| $R_{29}$ | $10 \Omega$ | $R_{70}$ | $47 \Omega$ |
| $R_{30}$ | $4.7 \mathrm{k} \Omega$ | $R_{71}$ | $47 \Omega$ 1000 $2 W$ |
| $R_{31}$ | $10 \mathrm{k} \Omega$ | $R_{72}$ | $100 \Omega 2 \mathrm{~W}$ |
| $R_{32}$ | $680 \Omega 2 \mathrm{~W}$ | $R_{73}$ | $10 \mathrm{k} \Omega$ |
| $R_{33}$ | $470 \Omega 2 \mathrm{~W}$ | $R_{74}$ | $1 \mathrm{k} \Omega \frac{1}{4} \mathrm{~W}$ |
| $R^{3+}$ | $470 \Omega$ | $R_{75}$ | $220 \Omega$ pre-set |
| $R_{35}$ | $1 \mathrm{k} \Omega$ | $R_{76}$ | $10 \mathrm{k} \Omega$ |
| $R_{36}$ | $100 \Omega$ | $R_{77}$ | $2.7 \mathrm{k} \Omega \mathrm{W}$ |
| $R_{3}{ }^{\text {? }}$ | $100 \Omega$ | $R_{78}$ | $5 \mathrm{k} \Omega, 3 \mathrm{~W}$ lin |
| $R_{38}$ | 10k $\Omega$ | $R_{79}$ | $500 \Omega$ pre-set |
| $R_{39}$ | (5.6-10k $\Omega$ ) | $R_{80}$ | $470 \mathrm{k} \Omega$ pre-set |
| $R_{40}$ | $39 \mathrm{k} \Omega$ | $R_{\text {s }}$ | $500 \Omega$ pre-set |
| $R_{40}$ | $39 \mathrm{k} \Omega$ | $R_{81}$ | $500 \Omega$ pre-set |
| $R_{4}$ | $4.7 \mathrm{k} \Omega$ | $R_{82}$ | $470 \mathrm{k} \Omega$ pre-set |

All resistors are $\frac{1}{8} \mathrm{~W}$, unless otherwise indicated. The values of those in brackets may need adjustment, as mentioned in the text.

## Capacitors

| $C_{1}$ | $\begin{aligned} & 6,600 \mu \mathrm{~F}, 50 \mathrm{~V} \\ & 4 \mathrm{~A} \text { ripple } \end{aligned}$ | $C_{11}$ | $10 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| :---: | :---: | :---: | :---: |
| $C_{2}$ | $50 \mu \mathrm{~F} 15 \mathrm{~V}$ | $C_{12}$ | $50 \mu \mathrm{~F} 6.4 \mathrm{~V}$ |
| $\mathrm{C}_{3}$ | $2 \mu \mathrm{~F}$ tantalum 12 V | $C_{13}$ | $320 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| $C_{4}$ | 220 nf | $C_{14}$ | 220 nF tantalum 12 V |
| C | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ | $C_{15}$ | 100 nF |
| $C_{6}$ | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ | $C_{16}$ | 330nF |
| C | $10 \sim \mathrm{~F} 12 \mathrm{~V}$ | $C_{1}$ : | 220 nF tantalum |
|  |  |  | 12 V |
| $C^{8}$ | $2 \mu \mathrm{~F} 12 \mathrm{~V}$ | $C_{18}$ | 330 nF |
| $\mathrm{C}_{9}$ | 220 nF | $C_{19}$ | 10 nF 25 V |
| $C_{10}$ | 100 nF metallized paper |  |  |


| Diodes |  |
| :--- | :--- |
| $D_{1}$ | 5D02 (International Rectifier) |
| $D_{2-4}$ | 1N916 |
| $D_{5-13}$ | 5 D 02 |
| $D_{14,15}$ | 30 S 1 |
| $D_{16}$ | 5 D 02 |
| $Z_{1}$ | $12 \mathrm{~V}, 1 \mathrm{iW}$ |
| $Z_{2}$ | 4 V 7400 mW |
| $Z_{3}$ | $2-6 \mathrm{~V} 8400 \mathrm{~mW}$ |
| $Z_{4}$ | 3 V 400 mW |
| $Z_{5}$ | 5 V 1400 mW |
| $Z_{6}$ | 3 V 3400 mW |
| $Z_{7}$ | 5 V 1400 mW |
| $Z_{8}$ | 5 V 1400 mW |
| $Z_{9}$ | 15 V 400 mW |
| $Z_{10}$ | 6 V 2400 mW |
| $Z_{11}$ | 12 V 400 mW |
| $Z_{12}$ | 11 V 400 mW |
| $Z_{13}$ | 11 V 400 mW |
| $Z_{14}$ | 10 V 400 mW |
| $Z_{15}$ | 10 V 400 mW |
| $Z_{16}$ | 11 V 400 mW |
| $Z_{17}$ | 9 V 1400 mW |

## Transistors

2N3702, ZTX50

2N3704, ZTX303 $\quad T r_{3}, T r_{5}, T r_{6}, T r_{7}, T r_{8}$,

| TIP31A | $\begin{aligned} & \operatorname{Tr}_{33} \\ & \operatorname{Tr}_{9}, \operatorname{Tr}_{11}, \operatorname{Tr}_{16}, \operatorname{Tr}_{28} \\ & \operatorname{Tr}_{29} \end{aligned}$ |
| :---: | :---: |
| TIP32A | $\operatorname{Tr}_{31}, \operatorname{Tr}_{32}$. |
| TIP31, TIP29 | Tr ${ }_{14}$ |
| TIS43 | Tr ${ }_{2}$ |
| ZTX107A | $T r_{10}$ |
| 2N3055 | $T r_{12}$ |
| Th | IRC10 (1A) |
| Switches |  |
| $S_{1}, S_{2}$ singl | e changeover (0.5A) |
| $S_{3}$ micr |  |
| $S_{+} \quad$ Two | changeover microswitch |
| $S_{5} \quad$ Thre | e rotary changeover |

## Miscellaneous

| $L p_{1}$ | 12 V 60 mA |
| :--- | :--- |
| $L p_{2}$ | 24 V 1W |
| $L P_{3}$ | 240 V neon indicator |
| $L p_{4}, 5$ | $5 \mathrm{~V}, 50-60 \mathrm{~mA}$ ( 3.5 mm dia.) |
| $F_{1}$ | 1 A anti-surge |
| $F_{2} \quad 5 \mathrm{~A}$ anti-surge |  |
| Mains transformer. Douglas M20AT |  |
| $L_{1} \quad$ 2A suppression choke |  |
| Motor. "Milliperm Special Super $12 \mathrm{~V}, 5$-pole" |  |
| (R. MARX-LUDER, 7121 Gemmrigheim, |  |
| Neckar, Germany.) |  |
| Earpiece. Danavox (G.B.) Ltd, "Broadlands", |  |
| Bagshot Road, Sunninghill, Ascot, Berks. |  |



Fig. 6. Motor drive unit.

Transistors $\operatorname{Tr}_{32,311_{33}}$ etc are operational. With negative on the earthing rail the reverse occurs, $T r_{31}, 3_{2}, 3_{3}$ being isolated and $T r_{27,28,29}$ etc. being operational. Resistors $R_{65}$ and $R_{73}$ may have to be adjusted slightly to take account of component tolerances.

## General Notes

When ordinary magnet-and-pole-piece locomotives are modified to take this system the pulse supply makes the locomotives noisy in operation. A simple modification is possible to stop this and consists of sawing out the armature "slot" to take a circular ferrite magnet of the type fitted to "Hornby" locomotives and other miniature electric motors. The air gap should be kept small as large air gaps cause an increase in running current and heat dissipated by the motor, although, air gaps as large as $\frac{1}{16}$ in have been found satisfactory. This modification immensely improves the slow start and running response.

Other locomotives fitted with magnet and pole pieces are best refitted with five-pole ring field motors in order to get the best from this or any other "pulse" system.

Locomotives fitted with plastic body shells will usefully augment the noise from the whistle and not so usefully augment noise from tender drive units. The tender drive units can be suitably "silenced" by lining the interior with $\frac{1}{32}$-in thick lead sheet which can be made from $\frac{1}{8}$-in roof lead by rolling or by taking the $\frac{1}{8}$-in thick lead to a sheet metal works who will usually do the job for a few pence. The imitation coal in tender drive units can usefully have small holes ( $\frac{1}{32}$ in dia) drilled in the coal department in order to assist air circulation. The holes are not noticeable after drilling without very carcful examination.

The layout of components has not been found critical, most of the circuitry being made up on 0.1 -in Veroboard or similar. The power supply ramp generator should be kept clear of pulse-carrying wires and parts, and the normal good practices applied. The power supply output waveform should be checked for slow rise and


Fig. 7. Motor and control mounted in the tender.
fall times ( $0.2-0.5 \mathrm{~ms}$ ) on an oscilloscope before use. Too fast edges will damage $\mathrm{C}_{10}$, which should be metallized paper or polystyrene of at least 200 V working. All other components are uncritical. The ganged microswitch will probably have to be made up, and it is worth noting that it does not matter if both switches do not switch at exactly the same time so long as they are free in operation. (Ganged microswitches are, however, commercially available from Bulgin.) The bridge rectifiers fitted to the "coach" and whistle sensor units are there to make it immaterial which way round the coaches are placed on the rails and what polarities are placed on the rails. (Reversing
the loco by reversing the supply has no effect on lights or whistle.) When setting up the system it is best to use only one meter for all measurements. Slight adjustment to all output voltages can be made by varying $R_{37}$ in the range 47-100!2. The coach lighting sensor regulator uansistor $T r_{4}$ should be fitted to a small heat sink ( $\mathrm{in} \times$ lin) or more conveniently the mild steel ballast plate that is supplied with some commercial coaches (Trix). In practice the system adds considerable realism to the model railway "train"which, in my opinion, they sadly lack at the moment. It only remains to add an efficient load sensing smoke unit to make the system complete.

## News of the Month

## "Donald Duck" eliminators for U.S. Navy

The United States Navy is buying British systems capable of overcoming the "Donald Duck" effect which oxy-helium gas has on deep-sea divers' speech. The systems, worth, with spares, a total of $£ 23,000$, were developed for the Royal Navy by Marconi Space and Defence Systems Limited, a GEC-Marconi Electronics company, from Admiralty Research Laboratories designs.

The "Donald Duck" effect results from divers having to breathe an oxy-helium mixture in depths of greater than 600 feet, where air cannot be used safely. The mixture, being much less dense than air, produces changes in the speed of sound, and therefore in the pitch of a speaker's voice. This rises to an extent where it becomes completely unintelligible to the listener. In emergency situations, the lack of effective communications can mean life or death to the diver.

The Marconi system, designated the Type 023, was developed from designs started in late 1968. It has already been in service in the Admiralty Experimental Diving Unit and the Royal Naval Physiological Laboratory, and is currently being evaluated, with favourable results, in a series of medical research dives of up to 1000 feet by the Smithsonian Institute in the U.S.A. It operates on a principle where each sound is digitally analyzed, and the significant portion, typically about one third, is reconstructed at a slower rate, while the rest is rejected. This has the effect of lowering the frequency to about a third of its transmitted value, and thus creating full intelligibility.

## Largest solid-state image sensor

RCA have demonstrated what is claimed to be the largest solid-state image sensor announced to date. The sensor - which is a charge coupled device (c.c.d.) - is a silicon chip the size of a small coin, containing over 120,000 electronic elements. Manufacturable c.c.d. image sensors of at least this size are essential if all-solid-state TV cameras are to have the resolution to satisfy a broad range of applications. Possible future TV cameras employing c.c.ds could be the size of a cigarette package or smaller, and would be rugged, highly reliable and potentially low in cost.

When an image is focused on the c.c.d., the sensor's electronic elements transform the picture into individual electrical charge packets. These packets are then read out very rapidly by charge transfer techniques. The resulting information can be processed and displayed as a TV picture.

## Component tester for relay systems

Electronics and radio research scientists of the Measuring Systems Design Department of Bell Laboratories in the United States have developed a new kind of test set with several valuable features for use in testing components of f.m. radio relay systems.

The new test set measures delay distortion, insertion loss (or gain), and return loss. The overall shapes of all three transmission characteristics are displayed. simultaneously on two large-screen oscilloscopes. This mode of operation allows the test set to approach the accuracy of point-by-point measurement while still displaying the characteristic over the entire frequency band. An operator can adjust the component being tested and instantly observe the effect over the entire frequency band. (Previously, measurements of this accuracy were obtained by taking several measurements over the frequency band and plotting the results manually to determine the overall shape.)

The 50 to 100 MHz scanner, called the f.m. scanner, was designed primarily to measure characteristics of f.m. radio system components.

## Travelling scholarship

An I.E.E.E. travelling scholarship of $£ 300$ is being offered for a visit or visits to foreign electrical or electronic research or manufacturing establishments by a postgraduate student. The purpose is to promote an exchange of research and technological ideas and to foster a closer relationship between young engineers in different countries. Candidates must submit a programme for their visit(s) by December 31, 1973, and the award will be made to the candidate whose programme is judged most likely to promote the objects of the scholarship.

The scholarship is financed by the U.K. and Republic of Ireland Section of the Institute of Electrical and Electronics

Engineers, which is acting in collaboration with the Institution of Electrical Engineers and the Institution of Electronic and Radio Engineers. Entrants must be student or graduate members of one of these three institutions. Further information and entry forms are obtainable from Prof. C. W. Turner, Dept. of Electrical \& Electronic Engineering, King's College, Strand, London WC2R 2LS.

## Venture for speech recognition

EMI Limited, London, and Threshold Technology Incorporated, Cinnaminson, N.J., U.S.A., have announced their intention of forming a joint venture company in Britain to market, over much of the world, electronic systems for recognizing spoken words and converting them into signals for controlling machines or instructing computers.

A major area of Threshold's operations is in the security field. It is currently testing a system which can identify a speaker's voice and compare it with voice patterns in a memory bank of "authorized" voices.

## Physics exhibition obituary

The Council of The Institute of Physics has decided that the Physics Exhibition should be discontinued. The next exhibition provisionally arranged for 1975 will not take place.

In recent years the number of exhibitors, particularly industrial firms, has fallen substantially, as has the number of visitors. This gives confirmation to a widely held belief that generalized scientific exhibitions without a unifying theme are unattractive to both exhibitors and visitors.

The Institute's knowledge and expertise in the exhibition field will now be concentrated on smaller specialized events.

The exhibition was first held by The Physical Society in 1905; the last one, in 1973, was the fifty-seventh in the series.

## Briefly

B.A.S.C. gets going. The principals of five major U.K. u.h.f. aerial manufacturers met in Bristol in September to reconstitute the British Aerial Standards Council, which, although formed as long ago as 1963, confined itself primarily to technical interchange. Recent developments have prompted it to extend its activities considerably, with the object of promoting high standards of performance, design and construction in television and v.h.f. radio aerials available to the public.

Frequency change for Northern Radio 4. The Radio 4 medium-wave service in North East England, which is at present transmitted on 261 metres ( 1151 kHz ), changed its wavelength on Saturday September 29 to 330 metres ( 908 kHz ). The two transmitters concerned are those at Stagshaw (near Hexham) and Scarborough.

# Instrument triggers up to five flash units at intervals from 11 ms to 11 s 

by Ralph Lewis

There are many times when the output of commercial stroboscopic flash units is completely inadequate to deal with a particular photographic problem. I am thinking essentially of cases similar to one described by Victor Blackman in his "Cameravaria" column in Amateur Photographer when he was required to take sequence photographs of a springboard diver in flight. To have used a strobe flash, even of a power considered high for strobe circuits, would have necessitated the pool being in complete darkness, otherwise ambient illumination would have obliterated the flash images. Because it was obviously dangerous to attempt a dive under those conditions, he ended up making a montage from photographs taken during separate dives.
Stroboscopic flash design to deliver the same amount of energy per flash as the high power single flash units (often 1,000 to 5,000 joules) in use in many studios today, is impracticable because of problems encountered in cooling the flash tube and building up energy in the capacitor rapidly enough. The usual way out of this difficulty, where short sequences are required and it is not
essential for the light to issue from exactly the same point each time, is to arrange for a number of capacitors to be charged simultaneously and discharged in succession; each one through a separate flashtube; often, but not necessarily, mounted in one reflector.
A simpler and less expensive method is to make use of conventional commercial single flash units and connect them to a device that will trigger them in the required manner. Making use of standard designs means that they can be obtained as and when needed from the several firms offering equipment hire facilities.
The circuit of such a device, which will trigger up to five flash units at equal increments of time throughout periods of 11 seconds to 11 milliseconds, is illustrated in this article. The periods are continuously variable to suit the duration of the event to be photographed.

## Circuit operation

Transistors $T r_{1}, T r_{2}$ and $T r_{3}$ (Fig. 1) with their associated components make up a monostable multivibrator which is switched
from the stable to the unstable state by a negative pulse applied to the base of $\operatorname{Tr}_{2}$. This is provided by the closing of the camera shutter contacts which connect to the socket labelled sync. The pulse causes the collector current of $\mathrm{Tr}_{2}$ to rise and switch on the thyristor $S C R_{1}$, which in turn triggers the first flash of the sequence connected to $\mathrm{FL}_{1}$. If $C_{1}$ were directly connected to the collector of $T r_{2}$, it would, together with the input resistance of $\mathrm{Tr}_{3}$, greatly increase the rise time of the collector potential of $T r_{2}$.

To overcome this, an emitter follower $T r_{1}$ is inserted between $T_{2}$ collector and $C_{1}$ which provides a much lower impedance for $C_{1}$ and $T r_{3}$ to shunt. To begin with, $C_{1}$ is charged to the supply voltage minus the base potential of $T r_{3}$. When $T r_{2}$ is switched on, its collector rises almost to the voltage of the positive rail carrying the emitter of $T r_{1}$ with it. Because the charge on $C_{1}$ cannot change instantaneously, the base of $\mathrm{Tr}_{3}$ is taken to almost twice the potential of the positive rail above earth which cuts off its collector current until such time as the charge has sufficiently leaked away via $R_{5}$


Fig. I. Camera shutter contacts trigger the monostable circuit which turns on the thyristor to provide the first flash trigger. If $C_{1}$ were directly connected to $T r_{2}$ collector, rise time would be too great. Timing circuit provides ramp output at $A$.
to allow it to conduct once more. The time this takes, ignoring the emitter-collector voltages of $T r_{1}$ and $T r_{2}$ and the baseemitter potential of $T r_{3}$ which are small compared to the supply voltage, is

$$
t \approx C_{1} R_{5} \log _{e}\left(2 V_{\mathrm{cc}} / V_{\mathrm{cc}}\right) \approx 0.69 C_{1} R_{5}
$$

When the base of $T r_{3}$ is biased to cut off its collector falls to earth potential and negatively biases the base of $T r_{2}$, holding it in the conducting state. When the charge on $C_{1}$ has sufficiently leaked away to allow $T_{r_{3}}$ to conduct once more, its collector rises until it is within 0.2 volts of the positive rail, which is sufficient to cut off $\mathrm{Tr}_{2}$ through $R_{4}$. The circuit now holds this condition until another negative pulse is applied to $T r_{2}$ base.
The timing circuit is a transistor version of a Blumlein integrator, more usualiy referred to as a Miller integrator. A basic circuit is shown in Fig. 2 using an n-p-n transistor for ease of explanation although the final circuit makes use of $\mathrm{p}-\mathrm{n}$-ps so that a positive going ramp is obtained.
At the start, the switch $S$ is open, the capacitor $C$ is charged to a potential of $V_{c c}-V_{e b}$ and a current flows through $R$ equal to $\left(V_{c s}-V_{c b}\right) / R$. When the switch is closed the immediate tendency is for a collector current to flow through $R_{L}$ equal to ( $V_{\text {cc }}-V_{\text {ce }}$ sat.) $/ R_{L}$, provided the current in $R$ is large enough to cause saturation in the transistor, and for the collector to take up a position about 0.2 volts above the negative rail. If that were to happen, the collector current would be cut off because the voltage across $C$ cannot change instantancously and any change in collector potential is immediately transferred to the base. Obviously this is impossible, so a condition develops where the base potential is just sufficiently positive to allow $C$ to discharge through the transistor, which allows the collector voltage to fall slowly in a linear manner. This occurs for the following reason. Electron current flows away from the base via $R$ and into the base from $C$. The result is a difference current which is the base current during the discharge.

The greater the current gain in the transition, the smaller the change in base current required to satisfy the voltage change at the

collector as the capacitor discharges. The base current is thus very small compared to $I_{R}$ and changes very little during the discharge. The smaller the base current is, the smaller the difference between $I_{R}$ and $I_{C}$ and the more constant $V_{e b}$. A constant voltage across $R$ produces a constant current through it; therefore the nearer $I_{c}$ approaches $I_{R}$ the closer it comes to constancy. As constant current flowing into or out of a capacitor raises or lowers the potential across it, according to the basic expression $V=I t / C$, it follows that the voltage across $C$ falls linearly with respect to time. As one plate is connected to a hardly changing $V_{e h}$ and the other plate is joined to the collector, the collector voltage must fall in like manner.
When the capacitor is completely discharged, the collector potential is equal to $V_{e b}$, the base current is again provided by $R$ only and the collector falls a fraction further to $V_{c e}$ sat.
If the switch is now opened, $C$ recharges via the base of the transistor and $R_{f}$.

The time for the linear portion of the voltage ramp can be expressed essentially by

$$
\begin{aligned}
& t=\frac{V C}{I_{C}} \approx \frac{\left(V_{c c}-V_{e b}\right) C}{\left(V_{c \mathrm{c}}-V_{e b}\right) / R} \\
& \approx C R \text { seconds, as } I_{c} \approx I_{R} .
\end{aligned}
$$

Because linearity is dependent upon a high value of beta, a Darlington pair is used in the final circuit and $T_{6}$ acts as the switch. Leakage in the capacitor, represented by $R_{C}$ in Fig. 2, must be kept to a minimum because it provides a shunt negative feedback path, bypassing the capacitive loop; reducing the gain of the amplifier and consequently the linearity of the ramp. For this reason, tantalum capacitors are recommended for $C_{3}$ and $C_{ \pm}$if the expense of polyester types is considered prohibitive.
Linearity also depends on a high voltage gain which is a product of $h_{F E} i_{t} R_{L}$. This makes the choice of $R_{L}$ a compromise as $h_{F E}$ and $R_{L}$ are interdependent. Too large a resistance could limit the collector current to a value which would seriously reduce the


Fig. 2. Basis of the timing circuit is a Blumlein (Miller) integrator, the linear portion of the ramp being about $C R$ seconds long.


Fig. 3. Four voltage-operated switches, all identical to this circuit, are set to trip at different points of the ramp waveform.
current gain factor. This is especially so in the present circuit where the collector current of $T r_{s}$ can only be a fraction of that of $T r_{4}$. The effective load resistance of $T r_{4}$ and $T r_{5}$ is made up of $R_{11}$ and four $R_{12} \mathrm{~s}$ in parallel and works out at approximately $10.5 \mathrm{k} \Omega$, giving adequate linearity for the purpose with the transistors shown, though no doubt others would give an equal or even better performance. The ones chosen had the merit of being inexpensive and were close to hand.

The meter provides a quick check of the correct functioning (or otherwise) of the timer; enables, on the $10 \mu \mathrm{~F}$ range, the time of the ramp to be compared with the duration of the event to be photographed; and facilitates the setting up of the voltage level switches.

The circuit of a switch is shown in Fig. 3 and as four are required the components are labelled A to D. The switches are arranged to operate sequentially at equal intervals during the ramp. Transistors $T r_{8}$ and $T r_{9}$ are connected as a Schmitt trigger and the potential at A is applied to the base of $T r_{8}$ via an f.e.t. source follower which serves to isolate the switches one from another and prevents variable shunting of $R_{11}$ by the change in input resistance of $T r_{8}$ as it changes state.

With A at zero potential, $\operatorname{Tr}_{8}$ is nonconducting and $T r_{9}$ is in saturation. $\operatorname{Tr}_{8}$ emitter potential is provided by the emitter current of $T r_{9}$ flowing through $R_{16}$ and is normally about 2.25 volts. When the voltage at the base of $T r_{8}$ is sufficient to initiate conductance, its first effect is to raise the emitter voltage (emitter follower action), but this tends to bias off $T r_{g}$ thus reducing the current which provided the voltage in the first place. As Tr $_{8}$ base continues to rise, its collector voltage falls, reducing the base voltage of $T_{r}$, and consequently its emitter current. This reduces the emitter voltage of $T r_{8}$ which causes still heavier conduction until such time as saturation occurs and its collector potential is very little more than its emitter. When this state is reached, $\operatorname{Tr}_{9}$ base is at a lower potential than its emitter, due to the divider action of $R_{17}$ and $R_{18}$, and is cut off.

Because the action is regenerative, the collector of $\mathrm{Tr}_{9}$, can be raised from 2.3 volts to 19.5 volts when the base of $T r_{8}$ reaches a critical point on the ramp which is set by adjustment of $R_{12}$. This voltage change is converted to a current pulse by $C_{6}, R_{20}$ and the emitter follower $\operatorname{Tr}_{10}$. Gate resistor limits the current peak to a value that will reliably turn on the thyristor.

A circuit that relies for its operation upon somewhat precise voltage levels obviously requires a stable supply voltage. The circuit of the battery supply and voltage regulator is shown in Fig. 4 and follows common practice. The quiescent battery current is 16 mA rising to 21 mA during the timing period. It is left to the constructor as to whether he fits PP3s or PP6s as a lot depends on how much one plans to use it.

## Construction

If tantalum capacitors are used for $C_{3}$ and $C_{4}$ their values should be measured as the tolerance of some of them is as wide as


Fig. 4. Stabie battery supply circuit.
electrolytics in general $(+100-10 \%)$ and can double the time of the ramp if one is not careful. If a bridge is not available, it would be advisable, though more expensive, to use polyester types if anything like the suggested times are looked for.
The period $0.70 C_{1} R_{5}$ must be longer than the period of the longest timing run, i.e. 11 seconds, for the ramp to reach maximum before $T r_{6}$ is turned off. It can with advantage be twice as long to aid the setting of the voltage level switches and the rail voltage. Because the leakage resistance of electrolytic capacitors aids their discharge, a capacitor of $200 \mu \mathrm{~F}$ is used which works out at 28 seconds but in practice gives about 20 seconds.

The circuits are made up on individual pieces of 0.15 -in Veroboard (see Fig. 5) and board wiring diagrams are available from the editorial office at $W \cdot W$.

Use is made of mounting tags broken out of a length of tag strip to secure the Veroboard to the front panel. The timer and voltage regulator assemblies are secured by means of the meter studding and the switches by the nuts and screws used to
fasten the phono sockets, see Fig. 5.
When making panels for instruments I usually make a layout on a piece of white board in black drawing ink and label it with Letraset. I then make a fine negative of it and from that, a single weight bromide enlargement to the size required. A brief exposure to a 15 -watt lamp at 6 to 7 feet is given to the paper before development and a light grey print with black lettering results. This is fixed to a piece of 14 s.w.g. aluminium with dry mounting tissue and a coat of clear polyurethane "varnish" is applied to the surface of the paper. When dry, the holes are cut out and the panel trimmed to size, but before trimming, the boundary lines of the panel are scored through to the aluminium surface with a sharp knife, so that a neat edge is obtained by filing as close to the line as possible. Holes are drilled small and enlarged to size with forward strokes of a file only, to avoid lifting the top surface of the paper. After cleaning off the swarl and filings with a cloth moistened with methylated spirit, I give it a final coat of polyurethane, paying particular attention to the edges of the panel and the insides of the holes. In this way, a neat, durable, and professional appearance is given to the finished product if a little care is taken.

## Setting up

To set the rail voltage, select the $0.1-\mu \mathrm{F}$ range and press the test bution. The meter will move rapidly to full scale and hold for about 20 seconds. This gives time to adjust $R_{23}$ so that the needle rests just short of the far stop which represents approximately 18.5 volts.

Setting up the switches is most easily done if a small electronic flash unit is used. Firstly, select the $10-\mu \mathrm{F}$ range, and to enable a more precise observation of the exact point at which the switch triggers, connect an $8-\mu \mathrm{F}$ capacitor in parallel, temporarily. Press the button and make sure that the ramp time does not exceed the turn on time of $T_{6}$. If


Fig. 5. Four circuit boards of voltage-operated switches are mounted vertically above the trigger sockets. Send s.a.e. to WW for board wiring diagrams.


Fig. 6. To check linearity of $0.1-\mu F$ and $1.0-\mu F$ ranges the five flash units were used to photograph a string tied between spindle and rim of a 78 rev/min turntable. For the 0.1- $\mu$ F range, $R_{10}$ was set at min., mid. and max. settings $(a, b$ and $c$ ) and at min. and mid. settings for the $1.0-\mu F$ range ( $d$ and $e$ ).
it does, connect a value somewhat smaller than $8-\mu \mathrm{F}$.

With the flash connected to $\mathrm{FL}_{2}$, initiate the ramp with the test button and observe the point at which it fires on the meter. Repeat this, adjusting $R_{12}$, until firing takes place at precisely 0.25 mA . Connect the flash in turn to $\mathrm{FL}_{3}, \mathrm{FL}_{4}$ and $\mathrm{FL}_{5}$ and adjust resistors 12 so that it fires at $0.5,0.75$ and 1.0 mA respectively.

Checking the linearity on the $10-\mu \mathrm{F}$ range can be done by inserting a microammeter in series with $C_{3}$ and observing that the discharge current, which should be in the region of $15.5 \mu \mathrm{~A}$, is maintained with an almost imperceptible change until the 1 mA point is reached on the meter. A change
would indicate excessive leakage in $C_{3}$ or a low beta in $\mathrm{Tr}_{4}$ or $T r_{5}$. In the original the change is less than $0.5 \%$ with a tantalum capacitor.

Linearity on the $0.1 \mu \mathrm{~F}$ and part of the $1.0-\mu \mathrm{F}$ ranges can be checked by connecting five flash units and photographing, at various settings of $R_{10}$, a string tied between the spindle and rim of a gramophone turntable rotating at $78 \mathrm{rev} / \mathrm{min}$. This of course takes into account the accuracy with which the switch trigger levels were set. See photographs in Fig. 6.

The resistor and capacitor, $R_{8}$ and $C_{2}$, are to prevent a transient pulse triggering the 0.25 mA switch when $T i_{6}$ is turned on.

The voltage readings given in the diagram
are for guidance only, especially the source potential of $\mathrm{Tr}_{7}$ which can differ markedly from the value in Fig. 4 because of the wide spreads in the characteristics of presently available f.e.t.s. Those given were measured with a $50 \mathrm{k} \Omega / \mathrm{V}$ meter with the point A at chassis potential.

And finally; if used with flash trigger circuits in which the voltage on the sync. contacts is not extinguished upon firing, the s.c.rs will remain conducting unless the plugs are momentarily pulled from $\mathrm{FL}_{1}$ to $\mathrm{FL}_{5}$. This doesn't happen in portable units where a capacitor is discharged through the primary of a tesla coil, directly connected to the sync. contacts, but might occur if a slave relay circuit were used.

## Letters to the Editor

The Editor does not necessarily endorse opinions expressed by his correspondents

## Hi-fi equipment standards

We were interested in your editorial comment "The Educated Ear" (October issue) and disappointed that we were unable to provide you beforehand with full information on British work equivalent to DIN 455000 . BSI is in fact working on a series of specifications for domestic hi-fi equipment. The specifications which have already been issued for comment in draft form deal with equipment such as amplifiers, microphones, record players, loudspeakers, headphones and combinations of equipment. The intention is to cover as much of the field of hi-fi as can be objectively approached.

Your regret at our apparent inaction would appear to be justified since Britain is indisputably a world leader in this field. We can only comment that the industry in this country only felt the need for guidance in these matters about two years ago and BSI responded immediately.

You will be glad to know that Britain
also leads in the field of specifying, and the forthcoming British Standard has already been proposed to the International Electrotechnical Commission as the basis for an international standard.
Terry Hammond,
British Standards Institution,
London, W.1.

Your editorial of October does an extreme disservice to those representatives of the U.K. audio industry who had been working since 1968 on the preparation of a U.K. based specification for the performance of high-fidelity equipment. Organizations participating in the early work included BREMA, FBA, APAE and RECMF, who were represented on an informal body, the Audio Specification Co-ordinating Committee. In 1970 the work had advanced far enough for an approach to be made to the British Standards Institution, which resulted in the setting up of

Technical Committee TLE/26. For the record, a press release was sent by the Co-ordinating Committee to some twenty leading British electronics journals, announcing the completion of the preliminary work, but only two, not including Wireless World, felt moved to print it.

Since 1970, TLE/26 has met about thirty-six times and has prepared draft specifications for seven of the components of high-fidelity systems, viz. amplifiers, tuners, loudspeakers, microphones, record playing units, headphones and combinations. In order to further the goal of an internationally accepted specification for high fidelity equipment - infinitely preferable to a host of differing national standards - most of these drafts have been submitted to the International Electrotechnical Commission, and are under consideration by the newly set up Working Group 12 of sub-committee SC29B, which has at present one U.K. member and may have more in the future.

Most significant is the divergence of attitude between British audio engineers and the technical press to the German specification. One of the kindest descriptions applied to it by the leading "hi-fi purist" types is "a charter for mid-fi". One prominent manufacturer proclaims the ease with which its requirements may be exceeded, even with relatively modestly
priced equipment. The British audio engineer (or Dutch, French or Danish, for that matter) who is prepared to regard it, as it stands, as an acceptable criterion for the thin red line that divides highfidelity equipment from everything else, has yet to be encountered.

It really is high time that the technical press properly supported the work of British engineers in this and other fields of standardization. I have had occasion to write similarly to another journal on the same subject within the past year. A standard is useless if it is not used: it will not be used if it is not accepted by engineers and buyers in general and it will not be accepted if it is not publicized. Inaccurate editorials in the country's leading popular electronics journals nullifying the efforts of British engineers and publicizing a highly deprecated foreign standard are simply and completely unfair! J. M. Woodgate,

Chislehurst,
Kent.
Editor's note: We shall be glad to publicize the British standard when it is issued.

## Radiating coaxial cables

I am writing in relation to J. R. Avery's letter (September letters) to point out that the radiating coaxial cable system he describes does not produce a "field variation of an inverse $r^{4}$ nature". The two straight lines shown on his graph are incorrectly designated as they actually show an inverse $r$ and an inverse $r^{2}$ relationship of field strength with distance and not inverse $r^{2}$ and inverse $r^{4}$ as indicated.

With this correction in mind it seems that the fall off in radiation with increasing distance from the cable corresponds more nearly to that experienced with what is usually termed the "induction field" and the advantages claimed for radiating cable systems appear to be no more attractive at medium frequencies than those of induction loop systems. Admittedly at v.h.f. and u.h.f. the radiating cable system has its advantages, particularly in tunnel and mine applications, and where the cable can be used for both receiving and transmitting.

It is interesting to note that inexpensive coaxial cable with open-weave braiding is not very effectively screened and at m.f. produces results similar to those obtained with specially designed radiating cables, except that more r.f. power is required to provide the same field strength. This has been shown by field tests and, as a result, the cheaper coaxial cable is currently being installed experimentally for a university radio installation.
The proposed Scottish university system referred to is unlikely to produce any improvement over a well-designed induction loop system which would also not cause any significant interference beyond the perimeter of the campus. However, a radiating cable system which employs cable ducts below the ground is liable to
induce currents at r.f. into any neighbouring cables (e.g. telephone cables) and, although this may have the dubious advantage of effectively increasing the broadcast coverage, the interference potential to the telephone system may be significant.

Finally, it should be added that the experimental or permanent operation of any radiating or induction system, irrespective of the rate of attenuation of field strength with distance, requires a licence from the Minister of Posts and Telecommunications and such a licence will only be issued after careful consideration of the practical circumstances and, in particular, the potential for interference to other services. M. Goddard,

Ministry of Posts and Telecommunications, London, S.E.1.

Mr Avery replies
May 1 reply to the various points raised by Mr Goddard in his response to my letter published in the September issue on radiating coaxial cables?
He is, of course, quite correct in pointing out the error in the designation of the two straight lines in my graph. These should accurately be labelled "inverse $r$ " and " $r{ }^{2}$ " as the ordinate of the graph is field strength. This error arose from Mr Moore's initial reference to field variations as inverse $r^{2}$ for transverse electromagnetic fields, and inverse $r^{4}$ for radiomagnetic fields.

The problem is one of units of measurement. If an aerial with a numeric gain ratio of $G$ over isotropic is placed in an electromagnetic field with a field strength of $E$ volts per metre and a wavelength of $\lambda$ metres, then the power in watts available at the aerial terminals, assuming no mismatch or finite conductivity losses, is given by the expression:

$$
P=G\left(\frac{\lambda^{2}}{4 \pi}\right)\left(\frac{E^{2}}{120 \pi}\right)
$$

If the distance $d$ from the originating source is varied then this power increases or decreases according to an inverse square law ratio given by:

$$
\left(\frac{\lambda}{4 \pi d}\right)^{2}
$$

This gives a field strength variation of an inverse $d$ nature, not a $d^{2}$. However, the straight lines in my graph do correctly depict electromagnetic and magnetic induction field variations, according to Mr Moore's original definition, although the mathematical designation is as Mr Goddard points out incorrect

The similarity of coverage provided between radiating cables and induction loop systems is not difficult to explain as both propagate by a similar mechanism. The loop carries radio frequency current which sets up an induction field within and adjacent to the loop, and is fed from both ends of the loop as a closed system. The radiating coaxial cable also carries surface radio frequency currents which are continuously coupled from inside the cable to the outer surface via the coupling mechanism (holes, slots, loose braid, etc.).

However, the coaxial cable is fed from one end only, the other end being terminated in a matched load. This fundamental difference is one major attraction of radiating cables, as in some situations it is difficult to cover the desired area using loops. This is the case in the cited Scottish University system, where, due to the campus layout, approximately 20 loops, one on each building, would have been required to provide adequate coverage. Each loop has to be fed by a separate amplifier to achieve adequate coverage, and the signal distribution and impedance matching becomes very complex.

The use of a radiating cable will alleviate the problem by cutting the equipment down to one transmitter, but siting of the cable is important as the field is still inductive in nature and falls away rapidly with increasing distance from the cable. This is even more important if the coaxial cable used is of the loose braid type, as it is susceptible to the contamination effects of dirt and moisture. This may not be too important at medium wave frequencies, but at v.h.f. and u.h.f. frequencies, where only radiating coaxial cables can be used, as loops are too inefficient, the attenuation of loose braid cable increases and a better cable construction is necessary.
May I thank Mr Goddard for his valued comments, and his colleagues at the Ministry of Posts and Telecommunications, who carried out the measurements on the radiating cable from whose results my graph was compiled, for their valued assistance. Anyone interested in operating a radiating cable system at any frequency should contact the M.P.T. for approval and a technical and development licence, as radiating cable systems are still very much in the investigation phase.
J. R. Avery.

## Using c.m.o.s. devices

I can quite understand Peter Seddon's trepidation after reading (Oct. Letters) the warnings about breakdown damage in c.m.o.s.; I was nearly frightened off by the apparent difficulties in handling and use, and came to the conclusion that c.m.o.s. devices were the answer to an engineer's prayer provided that one did not wish to unpack them, plug them in and switch-on!

Fortunately I was seduced, by the claims of low power consumption coupled with high noise immunity, into trying some, and would like to offer some words of comfort to Mr Seddon, based on my experiences during more than a year's use of c.m.o.s. devices.

I have come to the conclusion that, apart from a few elementary precautions, c.m.o.s. devices are more robust than the makers would have us believe. The main things to avoid are contact with plastics such as expanded polystyrene, which are capable of developing extremely high voltages due to friction (nylon lab. coats may come into this category), and the application of voltages outside the maxima specified from power supplies, unearthed soldering irons and test equipment. With the exception of these main points I have not
found any other precautions necessary (the image of Mr Seddon chained to his bench is intriguing but hardly practicable).

My prime source of device destruction was my failure to appreciate the devastating effect of floating inputs when the device was "on supply". In the case of hex buffers and inverters, e.g. R.C.A. CD4010 and CD4009, a floating input to a spare element will assume a potential of about $\frac{1}{2} V_{c c}$, causing both complementary output transistors to conduct. This quickly results in failure due to the high current so taken.

This problem is not likely to occur in the final circuit since the few spare inputs there are will, if the designer has done his job properly, be suitably tied to 0 V or $V_{\text {cc }}$ During "lash-ups", however, it is very easy to overlook the odd spare input and burn the device out (and sometimes burn one's own fingers, literally!).

In the case of a two input gate, e.g. R.C.A. CD4011, doing duty as an inverter/ buffer, I find the simplest thing to do is to strap the two inputs, thereby remaining the need to find a suitable " 0 V " or " $V_{c c}$ " point.

So far I have not experienced a failure traceable to gate breakdown and have even had devices survive reverse insertion in their sockets.

I should like to offer Mr Seddon the following advice: (1) Ensure all spare inputs are suitably tied. (2) Keep within the operating voltages recommended. (3) Check soldering iron and test gear earths. (4) Avoid contact with non-conducting plastics. (5) Plug the devices in the right way round. (6) Set power-supply current limiting to the lowest practicable level. These six points are applicable to any semiconductor device and do not make c.m.o.s. any more difficult than t.t.l.

Finally, Mr. Seddon, have a go; c.m.o.s. is fairly cheap now and the rewards are well worth the odd few bob (sorry, five new pence pieces)!
David S. Williams,
Walsall,
Staffs.

## Novice licence

You are so right in asking (page 516 of W.W. Oct. 1973) "Should there be a U.K. novice licence?" There is a need for such and has been for many years. Pre-war there was the A.A. licence which put so many of today's " G " s where they are.

The radio controlled model people are also worthy of consideration. What an advantage it would be to them to use limited power communication on airfields etc. There are many such persons keen enough in this branch of radio experimenting and research but who are not in the least interested in becoming a " $G$ " and calling someone at the other side of the world "old man", each to his own liking.

The frequency allocated will, we understand, be made unusable by misuse or at least this is the opinion of "G's" - but if we listen to some of the "amateur
bands" there is sometimes cause for concern.
I feel that at least holders of model "pulse" licences should be granted a frequency for speech communication.
Ray Williams,
Grantham,
Lincs.

## Projection television

The letter from America by G. W. Tillett (September issue) and the letter from H. Ibbotson (October) bring memories to me with feelings of nostalgia.

It is a great pity that after a very promising start the development of projection television stopped. I firmly believed then and still do that a form of projection television will be evolved which will include stereo sound and 3D reproduction.

Within very restricted limitations I continued development of colour projection television. The results, although promising, will require a fair amount of work, particularly to improve brightness. The colour and picture quality is comparable with a 26 in shadow mask tube. Where projection fails is insufficient brightness, and it must be viewed in total darkness.

The main difficulty is that, of necessity. I had to use black and white MW6/2 tubes with colour filters. Mullard's did at one time produce blue, green and yellow tubes. These, with a red filter on the yellow tube, produced acceptable results; however, the loss of light was considerable.

I saw the French optical system demonstrated in Paris early in the 1950s but did not think the results as good as the Philips / Mullard unit.

In adapting the standard projection system to colour it was necessary to re-design the deflection coil assembly to accommodate convergence coils. The whole assembly is similar to that used with shadow mask tubes.

There is still a fair amount of development work to be done, so get cracking you Wireless World experimenters!
V. Valchera,

Valradio Ltd, Feltham, Middlesex.

## Sale of "walkie-talkies"

I would draw your attention to the adverts for "walkie-talkies" in a popular publication. The information is attached on a separate sheet. |Extracts from Exchange and Mart sent.|

To the best of my knowledge these units operate in the $29.9-31.00 \mathrm{MHz}$ area and as such it would be most unlikely that permission to operate them in the United Kingdom would be granted by the M.P.T.
l certainly have no wish to restrict the commercial activities of the concerns
selling these items but in all fairness I do feel that some reputable authority should make some investigations into the sale and obvious use of them.

As all these units are imported it would seem that some regulation could be exercised by H.M. Customs and Excise. There already exists an import restriction covering similar units operating in the $26.1-29.7 \mathrm{MHz}$ and $88-108 \mathrm{MHz}$ bands and maybe this could be extended.

I should add that I am a radio amateur (G3LWM) and it is certainly not a case of "sour grapes" but an effort to prevent unsuspecting people becoming liable to prosecutions under the Wireless Telegraphy Act, On numbers of occasions I have been asked by the police to produce my licence. This has usually been on the tops of wind-swept hills, on misty nights to take advantage of good v.h.f. conditions!

## J. D. Harris,

Bishop's Stortford,
Herts.

## VAT and prices

Despite your publishing my letter in the September issue there are 41 advertisements in the October issue which have no indication whether VAT applies or not. Together with Mr Dykes (Oct. issue), I hope that the matter will improve. Perhaps some editorial guidance is necessary. These 41 firms will of course not get any of the $£ 100$ I spend monthly with your advertisers - just the same as those firms who offer long lists of transistors they do not have in stock.

Do these people think we do not remember poor deliveries, wrong items sent, poor packaging and procrastination? Those who do not quote prices at all are the worst of course; possibly they have large office staffs to answer queries -I don't have time, I merely go elsewhere.
W. B. Henniker,

Henniker \& Kerr,
Edinburgh.

## Frequency shifter for "howl" suppression

Some of your readers may not be aware that the frequency shifter designed by M. Hartley Jones and described in your July issue, can be adapted to provide a very acceptable imitation of "tape phasing", much sought after in popular music. All that is required is a mixer to add direct and frequency shifted sound. The resuit is a series of nulls running through the audio spectrum at a rate determined by the frequency shift.
For best effect a frequency shift of about 0.2 Hz is required. which is not difficult to achieve with that particular circuit. A good explanation of phasing is given in the Journal of the Audio Engineering Society of America, December 1970, vol. 18, No 6, pp.674-5.
A. G. Falla,

Radcliffe on Trent,
Notts.

# Dual-polarity Digital Voltmeter 

# 2 - Construction and calibration 

by A. J. Ewins

A.c./d.c. input stages. The sensitivity of the basic d.v.m. is, as already stated, 2 volts d.c., with an input impedance of $20 \mathrm{k} \Omega$. It was required that the d.v.m. should have a maximum sensitivity of 200 mV a.c. and d.c., and as high an input impedance as possible. It was also required that the a.c. response should extend up to 100 kHz so that the voltages of all signals encountered in audio circuits (tape-recorder bias and erase oscillators operate around 100 kHz ) could be accurately measured. These requirements call for an input amplification stage with a voltage gain of ten, a frequency response from 0 to 100 kHz and a high input impedance. The temperature stability of the amplifier stage must also be good for d.c. measurements, because a maximum sensitivity of 200 mV implies a resolution of $100 \mu \mathrm{~V}$. To achieve these objectives it was decided to use a f.e.t. operational amplifier as the input buffer stage. The one used by the author is supplied by RS Components Ltd, the FET-OPA, which at $£ 5.80$ trade may be thought rather expensive. However, an alternative device with similar character-
istics is one supplied by Ancom Ltd. type $15 \mathrm{~A}-37$. This is priced at $£ 4.95$ retail and, though still expensive, is thought worth it. It has an input impedance of $5 \times 10^{10} \Omega$ and an offset temperature stability of $50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$, which is satisfactory. Although the f.e.t. op . amp provides an accurate gain of ten at d.c., its frequency response at this gain level does not extend, accurately, to 100 kHz . However, its unity gain frequency response does extend beyond 100 kHz and it was not found difficult to design a rectifying circuit with an overall voltage gain of ten and a frequency response beyond 100 kHz .

Fig. 8 shows the circuit diagram of the complete a.c./d.c. input stages of the d.v.m., including the a.c. rectifier circuit. Using this in front of the basic d.v.m. extends the ranges of the d.v.m. to $200 \mathrm{mV}, 400 \mathrm{mV}, 2 \mathrm{~V}$, $4 \mathrm{~V}, 20 \mathrm{~V}, 40 \mathrm{~V}, 200 \mathrm{~V}$ and 400 V , a.c. and d.c., and provides an input impedance of the order of $500 \mathrm{M} \Omega$ on all ranges up to, and including, 4 V , and about $10 \mathrm{M} \Omega$ in parallel with 10 pF for all ranges above 4 V . In the d.c. mode, the f.e.t. op. amp. has a voltage gain of either ten or unity. In the a.c. mode,
the op. amp. has a fixed unity voltage gain and the rectifier circuit is either connected directly to the output of the op. amp. or via $a \times 10$ attenuator. The rectifier circuit itself has a voltage gain of five and is followed by a differential-amplifier filter circuit with a voltage gain of two.

The principle of operation of the rectifier circuit is as shown in Fig. 9. A diode/ capacitor rectifying bridge circuit is used instead of a full diode bridge. In the author's opinion, this is a more useful type of rectifier circuit than the full diode bridge since it has a voltage doubling action whilst, at the same time, the capacitors provide a first order filtering action to the unwanted acc. component. For this type of circuit, $V_{o}$ equals $R_{L} \cdot I_{m}$ where $I_{m}$ equals $I_{L}$ (peak) $/ \pi$. The feedback voltage, $V_{f}=V_{i n}$. Thus, the voltage gain of the circuit, $V_{o} / V_{f}$, equals $\left(R_{L} / R_{f}\right)\left(I_{L \text { peak }} / I_{L} \pi\right)$. If the d.v.m. is to be calibrated in terms of r.m.s. values for sinewave inputs, $I_{L \text { (peak })}=\sqrt{2 . I_{L}}$ and the voltage gain of the circuit will therefore be; $\left(R_{L} / R_{f}\right)(\sqrt{2 / \pi})$. Therefore, for a voltage gain of 5, $R_{L}$, equals $11.11 R_{f}$. In the circuit of Fig. 8, $R_{L}$ is equivalent to $R_{58}$ in series with $R_{57}$, paralleled by $R_{59}$ and $R_{60}$ (which are effectively in series), i.e. $R_{L}=24$ $(2.2+0.2) /(24+2.2+0.2) . R_{L}$ is thus adjust able from about $2 \mathrm{k} \Omega$ to $2.2 \mathrm{k} \Omega$, which, if $R_{f}=190 \Omega$, allows an adjustment to the voltage gain of the rectifier circuit from about 4.78 to 5.17 . The maximum input voltage to the a.c. rectifier circuit is 400 mV r.m.s. and therefore the output stage of the amplifier must be able to handle a peak-topeak voltage swing in excess of about 6 volts and provide a peak current of about 3 mA . An op. amp. would therefore appear to be the ideal choice for this stage. However, neither the well-known 741 or 709 have a sufficiently high frequency response. It was therefore decided to design a suitable amplifier using discrete components on the

principle that simplicity sometimes produces the best results. The output stage is made to have an extremely high output impedance by using a constant current source as the load. This, together with the large amount of negative feedback available, overcomes the non-linearity of the diodes to such an extent that the linearity of the d.v.m. to a.c. measurements is accurate to plus or minus one digit down to $1 \%$ of full-scale. The overall frequency response is also good, being flat to within $\pm 0.5 \%$ from 30 Hz to over 100 kHz .
A d.v.m. designed on the dual-slope integrating principle provides a degree of filtering action to alternating voltages by virtue of its design. It can be shown that the filtering action takes the form of an attenuation of 6 dB /octave above a frequency whose period is equivalent to the integrating time of the d.v.m. In addition, at frequencies which are an exact multiple of the integrating frequency, the attenuation is theoretically infinite. The integrating period of this design (approximately 100 ms ) is equivalent to a frequency of 10 Hz . Thus frequencies of a multiple of 10 , i.e. 10,20 , 30 Hz and etc., will be infinitely attenuated and those in between by not less than 6 dB / octave above 10 Hz . Thus, the filtering action of the integrator itself, together with the filtering action of the capacitors of the diode/capacitor bridge and the differential filter amplifier, provide an attenuation greater than 60 dB to all frequencies above 30 Hz .

The output from the circuit of Fig. 9, for connection to the circuit of Fig. 3, is via the $1 \mathrm{k} \Omega$ variable resistor $R_{64}$ in series with $R_{65}$, and $R_{66}$ to earth. When the switch, $S_{3}$, is closed these resistors are bypassed and the ranges of the d.v.m. are $200 \mathrm{mV}, 2 \mathrm{~V}, 20 \mathrm{~V}$, and 200 V . When $S_{3}$ is open, the sensitivity of the basic circuit is effectively reduced by a factor of two, so that the ranges available become $400 \mathrm{mV}, 4 \mathrm{~V}, 40 \mathrm{~V}$ and 400 V . The reading indicated by the display must therefore be multiplied by two. $R_{64}$ allows this multiplication factor of two to be precisely adjusted.
$R_{46}$ and $R_{63}$ allow the offsets of the f.e.t. and 741 op . amps. to zeroed. $R_{47}$ allows the $\times 10$ attenuator to be precisely adjusted. $R_{51}$ is included so that the d.c. potential at the junction of diodes $D_{1}$ and $D_{2}$ may be


Power supplies. The power supply requirements for the d.v.m. are 5 volts at about 1 amp . (for the t.t.1. logic circuits and seven segment digital indicators) and $\pm 12$ volts at about 50 mA (for the analogue circuitry). Figs. 11 and 12 show the circuit diagrams Figs. 11 and 12 show the circuit diagrams
of the power supplies and it will be seen that these are greatly simplified by the use of monolithic voltage regulators. Types MVR5V and MVR12V have been used by
adjusted to zero, preventing the two capacitors of the rectifier bridge from becoming tors of the rectifier bridge from becoming
reverse-polarised. These capacitors, together with $C_{8}, C_{9}$ and $C_{5}$ are tantalum types and can accept a small reverse potential of no more than 500 mV

Fig. 10 is the circuit of the $\times 100$ attenuator. The variable resistor, $R_{68}$, allows the attenuator to be precisely adjusted under d.c. conditions and $C_{12}$ allows the under d.c. conditions and $C_{12}$ allows the
frequency response of the attenuator to be adjusted to an optimally flat condition. The
resistor $R_{0}$ is a parallel combination of a adjusted to an optimally flat condition. The
resistor $R_{69}$ is a parallel combination of a resistor $R_{69}$ is a parallel combination of a
$100 \mathrm{k} \Omega$ and $3.9 \mathrm{M} \Omega$ resistor.


Fig. 9. Basic rectifier circuit


Fig. IO. Input attenuator. -
in the circuit as indicated and the $500 \Omega$ pot in series with $R_{13} . R_{5}$ (Fig. 3) and $R_{6}$ and $R_{7}$ need only be single-turn pots.

For the $C_{1}$, the author used a fairly expensive 63 V , polycarbonate type but believes that a much cheaper polyester type should be just as satisfactory.
There is nothing special about the remainder of the components of Fig. 3. $Z_{2}$ is a standard 5.6 V zener diode from the Mullard, BZY88 range and has a temperature coeflicient of about $-0.2 \mathrm{mV} / \mathrm{C}$. This represents a change of about $-0.004 \% /{ }^{\circ} \mathrm{C}$ for the two reference voltages and should be more than adequate.

In Fig. 8, the offset adjustment for the f.e.t. op.-amp. may be either a ten-turn, $1 \mathrm{k} \Omega$ pot., or a single-turn, $100 \Omega$ pot. in series with a fixed resistor, $R_{x}$, of about 470 ohms, as shown. $R_{51}$ need only be a single-turn pot., but $R_{47}, R_{57}$ and $R_{64}$ ideally need to be ten, or more, turn preset pots. (as does $R_{68}$ in Fig. 10) since a resolution of about $1 \%$ is required. However, it is not impossible to achieve this resolution with single-turn pots., only tricky
Nothing has been said, so far, about the type of digital and overload indicators used. For the seven-segment digital indicators the author chose "Minitrons" because, in his opinion, these are hard to beat for a combination of size, price and low current consumption. Types 3015 F and 3015G have both been used and are widely available. The type 3015 F indicates the digits 0 to 9 and a right-hand decimal point. The type 3015G indicates " + " and " -" signs, the digit " 1 " and a right-hand decimal point. One of the many, cheap le.ds now available is probably the obvious choice for an overload indicator, although a 6.3 V filament bulb rated at 40 mA is worth considering.

## Construction and adjustment of circuits

The obvious place to start on the construction of the d.v.m. is with the power supplies and if the monolithic regulators are used, as


Fig. 12. Stabilized twin $5 V$ power supply.
suggested by the author, these will present no difficulty. The circuits of Figs. 3 and 4 should then be constructed on two separate circuit boards as illustrated in Figs. 13 and 14. It is suggested that, if i.c. sockets are not used, all the i.cs should be checked for correct operation before insertion into the circuits. In particular, the input offset voltages of the 709 and 741 op.-amps. should be checked to ensure that they are within the manufacturer's tolerances. To simplify the checking and setting-up of the analogue circuit, $1 C_{6}$ should initially be left out of circuit.

When the circuit of Fig. 3 has been constructed (less $I C_{6}$ ) it can be checked and initially adjusted. All three power supplies should be connected and the $\bar{C}$ and "hold" inputs should be temporarily connected to the +5 V line. With the power supplies switched on a few quick voltage checks can be made; in particular the reference voltage of $Z_{2}$ and the output voltages from $I C_{1}$ and $I C_{5}$ can be checked. They should be approximately $+5.6 \mathrm{~V},+2 \mathrm{~V}$ and -2 V , respectively. The positive input to $I C_{2}$ and the negative inputs to $I C_{4}$ and $I C_{7}$ should also be about +2 V . If these latter voltages are correct, the emitters of $T r_{1}$ to $T r_{4}$ should be at very nearly zero volts and may be
adjusted to precisely zero, with the $V_{\text {in }}$ inputs shorted together, by means of $R_{3}$. The reference levels to the two comparators, $I C_{8}$ and $I C_{9}$, should now be adjusted. To do this, a small variable voltage source of between about -5 mV and +5 mV should be fed to what will be the output of $I C_{6} . R_{7}$ should be adjusted so that the output from the collector of $\operatorname{Tr}_{9}$ changes from about zero volts to about +5 V when the small variable voltage source is reduced just below -3 mV . The output of $T r_{9}$ collector should revert to zero volts when the variable voltage just exceeds -1 mV . Similarly, $R_{6}$ should be adjusted so that the emitter of $T r_{6}$ undergoes identical output voltage changes when the variable voltage source exceeds about +3 mV and is reduced below about +1 mV . If all is well, the operation of the switching transistors $\operatorname{Tr}_{1}$ to $\operatorname{Tr}_{4}$ may now be checked. Adjust the small variable voltage source to some positive value in excess of +3 mV so that the emitter of $T r_{6}$ becomes +5 V . Measuring the output voltage at the junction of the emitters of $T r_{1}$ to $T r_{4}$, disconnect the $\bar{C}$ input from the +5 V line and connect to ground. The voltage reading should change from zero volts to the +2 V reference level. Reconnect the $\bar{C}$ input to the +5 V line and repeat the test with the variable


Fig. 13. Layout of analogue circuit.


Fig. 14. Control circuitry and display logic
voltage source adjusted to some negative value below -3 mV so that the collector of $T r_{9}$ is at about +5 V . The voltage reading should change from zero volts to the -2 V reference level. If all checks are satisfactory, disconnect the voltage supplies and insert $I C_{6}$ into the circuit No more checks or adjustments can now be made until some preliminary checks have been carried out to the digital circuit board. To do these, connect the +5 V supply to it and temporarily connect the "auto-Manual switch" input (see Fig. 14) to ground and the $V_{o}$ input to the +5 V line. With the supply switched on, the operation of the clock oscillator, the four decade counters and the
divide-by-two counter may be checked and should be observed to be running as a normal counter. The $\bar{C}$ output should be constant at the logical " 1 " level, i.e. about +5 V . If the digital indicators have been connected, they should be continually indicating zero and the overload indicator should be OFF.

If the switch input is now disconnected from ground, the four decade counters and the divide-by-two flip-flop should become permanently set to zero and stop counting after three complete cycles of the main counter. The "hold" output should also become logical zero. On re-connection of the switch input to ground, the main counter
should start recounting and the "hold" output become logical " 1 " again. If the $V_{o}$ input is now disconnected from the +5 V line and connected to ground the $A$ flip-flop should be observed dividing by two and the $\bar{C}$ output should become constant at the logical zero level. This completes all the useful checks that can be made before interconnecting the analogue and digital circuit boards and if all the tests have proved successful, this should now be done. If not, the wiring should first be checked (this should, of course, have been done before any testing was carried out) and then an attempt made to discover any faulty components.


Fig. 15. Input circuit hyyou.

With the analogue, digital and power supply boards interconnected, the digital and overload indicators connected, the $V_{\text {in }}$ inputs shorted together and the switch input connected to ground, the power supplies should be switched on. If all is working correctly, a voltage of a few millivolts, positive or negative, will probably be indicated and should be adjustable to zero by means of $R_{4}$ and/or $R_{5}$. To test that the circuits are functioning correctly, a variable voltage source of from just under -2 V to just over +2 V should be applied to the $V_{\text {in }}$ inputs. Varying this input voltage source between its limits should result in digital readings, of correct polarity, corresponding approximately to the applied voltage. Indicated readings greater in magnitude than 1999 should result in an overload indication. If reversed polarity indications are given, it is a simple matter to correct this by reversing the connections of $P_{1}$ and $P_{2}$ to the digital circuit board.
The auto/manual function can be checked by disconnecting the switch input from ground. If all is well, the display will become "frozen" and will not alter when the input voltage is varied. Upon reconnection of the switch input to ground, the digital readout should again follow the input voltage. Final adjustments to $R_{4}$ and $R_{5}$ can now be made and should be carried out in the following manner. With the $V_{i n}$ inputs shorted together, disconnect the switch input from ground to freeze the display. This effectively short circuits the output from $I C_{6}$ to its negative input. Next, connect a voltmeter between ground and the $V_{o}$ output. When $R_{4}$ is adjusted correctly, the $V_{0}$ output will be at about +5 V . As the wiper of $R_{4}$ is adjusted, positively and negatively, about this position, a point on either side will be found where the $V_{o}$ output falls to zero volts. For a correct setting, the wiper of $R_{4}$ should be exactly mid-way between these two points. Having adjusted $R_{4}$, reconnect the switch input to ground and adjust $R_{5}$ for a zero digital readout. The $V_{o}$ output will be observed to be indicating about +5 V with the occasional "kick" towards zero volts. The rate at which the "kicks" occur is an indication of the goodness of the zero adjustment. The less frequent the kicks, the better the adjustment. A kick once every second indicates a zero adjustment ten times better than that digitally indicated, i.e. to within $100 \mu \mathrm{~V}$ of the true zero. (Remember, the least significant digit is 1 mV .) Apart from the accurate adjustment of the two reference voltages, this completes the testing and setting-up of the basic digital voltmeter circuits. All that remains now is to construct and test the a.c./d.c. input stages. This should present no difficulty, and apart from the adjustment of $R_{51}$, final adjustment of the remaining preset controls should be left until the instrument is finally housed. When the circuit of Fig. 8 has been constructed, $R_{51}$ should be adjusted for zero direct volts at the junctions of the collectors of $\operatorname{Tr}_{3}$ and $T r_{4}$. When the instrument is complete, $R_{46}$ becomes the zero adjustment for direct voltages, and $R_{63}$ becomes the zero adjustment for a.c. voltages.
Before proceeding to a discussion on the calibration of the instrument there is a detail

## Specification <br> Ranges. 200 mV full-scale a.c. and d.c. 2 V full-scale a.c. and d.c. 4 V full-scale a.c. and d.c. 20 V full-scale a.c. and d.c. 40 V full-scale a.c. and d.c. 200 V full-scale a.c. and d.c. 400 V full-scale a.c. and d.c. (Readings multiplied by two on $400 \mathrm{mV}, 4 \mathrm{~V}$ etc.) 400 mV full-scale a.c. and d.c. (Maximum resolution $100 \mu \mathrm{~V}$.)

Input impedance. $500 \mathrm{M} \Omega$ up to 4 V fullscale. $10 \mathrm{M} \Omega$ and 10 pF above 4 V .

Display. $3 \frac{1}{2}$ digits. Overload indication. Readings up to 2500 . Polarity indication.

Accuracy. Error less than $\pm 0.1 \%$ of reading, $\pm 0.05 \%$ full-scale on direct voltage readings. Less than $\pm 0.5 \%$ of of reading, $\pm 0.05 \%$ full-scale on alter-nating-voltage ranges.

Frequency range. 30 Hz to 100 kHz .
Mode. Continuously-sampling or manual "hold".
that has not, so far, been mentioned; it is the positioning of the display's decimal point for the various ranges. This may be easily achieved by adding an additional single-pole, four-way wafer to the range switch ( $S_{1}$, Fig. 8). Thus as the range switch is altered, the appropriate decimal point of the four digital indicators is connected to the +5 V line.

Another, and final, point is the functioning of the polarity indicators when switched to the alternating voltage ranges. It is suggested that an additional pair of single-pole, 2 -way contacts are added to the a.c./d.c. function switch ( $S_{2}$, Fig. 8). In the d.c. position, these two sections should connect the $J$ and $K$ inputs of the polarity flip-flop to the emitter of $\operatorname{Tr}_{6}$ and the collector of $T r_{9}$, respectively. Correct polarity will be thus indicated as previously described. In the a.c. position, these contacts should connect both $J$ and $K$ inputs to the +5 V line, with the result that an alternating, plus and minus polarity indication will be given. The rate of alternation will vary from 10 Hz to 5 Hz for input voltages varying from zero to full scale deflection, respectively.

## Calibration

Assuming that the constructor has finally housed the circuit boards and other components, and connected them up, the first step in the calibration of the instrument is the adjustment of the two reference voltages ( $R_{1}$ and $R_{2}$, Fig. 3). To do this, switch the a.c./d.c. function switch to "d.c.", the range switch to " 2 V " and the display switch to " $\times 1$ ". Short circuit the inputs and adjust the d.c. zero for a zero reading. Apply an accurately known direct voltage of a little less than +2 V to the inputs and adjust the negative reference voltage until a digital reading exactly equal to the applied voltage is obtained. Reverse the polarity of the applied voltage and adjust the positive
reference voltage for a correct digital reading. The basic range of the d.v.m. has now been calibrated and the remaining calibration adjustments should be carried out in the following order.

1. Switch the display switch to " $\times 2$ " and apply a known voltage of a little less than +4 V . Adjust $R_{64}$ (Fig. 8) for a display reading of exactly half this applied voltage.
2. Switch the range switch to " 200 mV " and the display switch to " $\times 1$ " and apply a known voltage of a little less than +200 mV . Adjust $R_{47}$ (Fig. 8) for a display reading equal to the applied voltage.
3. Switch the range switch to " 200 V " and apply a known voltage of a little less than +200 V . Adjust $R_{68}$ (Fig. 10) for a display reading equal to the applied voltage.
(Calibration of the $\times 100$ attenuator may be carried out on the 20 V range by applying a known voltage of just under +20 V if a known voltage of the order of +200 V is not available.)
4. Switch the range switch to " 2 V " and the a.c./d.c. switch to "a.c." and adjust the a.c. zero for a zero reading with the inputs shorted together. Apply a known a.c. voltage of just under 2 V r.m.s. at a frequency of about 1 kHz and adjust $R_{57}$ (Fig. 8) for a display reading equal to the applied voltage.
5. Switch the range switch to " 200 V " and apply an alternating voltage of about 300 Hz , adjusting it for a digital reading of just under 200 V . Vary the frequency of the signal, maintaining a constant output voltage, to about 90 kHz and adjust the variable capacitor of the $\times 100$ attenuator until the original voltage is indicated. (As for the 200 V d.c. range, the capacitor of the $\times 100$ attenuator may be adjusted with the range switch switched to the " 20 V " range and applying a variable frequency signal of just under 20 V , should a 200 V signal not be available.)

The accuracy of the above calibration procedure depends upon the accuracy of the known test voltages and these, ideally, should be better than $\pm 0.05 \%$ for the d.c. ranges and better than $\pm 0.5 \%$ for the a.c. ranges. Possibly the ideal method is to measure these test voltages with an already calibrated d.v.m. of greater accuracy than the subject of this article. Obtaining the use of such an instrument may be difficult for the amateur constructor but, in this respect, it is thought possible that some local universities may be willing to allow access to their electronic instruments. If not, other solutions may, hopefully, present themselves to the constructor.

## Component suppliers

Ancom Ltd, Devonshire St, Cheltenham, Glos. RS Components Ltd, P.O. Box 427, 13-17 Epworth St, London EC2P 2HA.
(RS Components Ltd will only supply retailers, trade service technicians, industrial or educational users. Retailers are able to order components for private buyers.)
Semiconductor Supplies, 55 Whitehorse Road, Croydon CR0 2JG.
Vero Electronics Ltd, Industrial Estate, Chandler's Ford, Eastleigh, Hants.
(Veroboard-a similar material is available from RS Components.)

## November Meetings

Tickets are required for some meetings: readers are advised therefore to communicate with the society concerned

## LONDON

18th Oct. RTS - "Advanced electronic editing systems ${ }^{n}$ by J. Southgate at 19.00 at London Weekend Television, South Bank TV Centre, Upper Ground, SE1.

25th Oct. SERT - "Some future trends in colour TV tubes" by G. R. Diacon at 19.00 at IBA, 70 Brompton Rd., SW7.

Ist. IEE - "The management challenge for electrical engineers" by Dr. A. C. Copisarow at 17.30 at Savoy P1., WC2.

1st. RTS - "Cable access at Bristol" by P. Lewis and colleagues at 19.00 at London Weekend Television, South Bank TV Centre, Upper Ground, SEI.

2nd. IEE/IERE-Colloquium on "Mass spectrometry at 14.30 at Savoy Pl.. WC2.
Sth. IEE/IERE - Colloquium on "Display technology" at 10.30 at Savoy Pl., WC2.

6th. IEE - "Performance of modern thyratrons" by H. Menown at 17.30 at Savoy PI., WC2.
6th. IEE - "The position of the graduate engineer in a large company" by T. Maycr at 18.30 at Imperial College, Exhibition Rd., SW7.

7th. IEE - "Some new possibilities in radar and navaids" by Prof. E. D. R. Shearman at 17.30 at Savoy Pl., WC2.

7th. BKSTS - "The changing world of the news cameraman" film at 18.15 lecture at 20.45 at the National Film Theatre. South Bank, Waterloo. SE 1
8th. SEE - "Use of dessicants in electronics and packaging" at 18.00 at Imperial College, Exhibi tion Rd., SW7.
13th. AES -- "Professional microphones their use and misuse" by Antony Askew and Angus McKenzie at 19.15 at the IEE, Savoy Pl., WC2.

14th. IERE - Colloquium on "Domestic equip ment control systems" at 14.00 at 9 Bedford Sq., WCl 1 .

14th. IEE - "Data communication by packet switching" by Prof. P. T. Kirstein at 17.30 at Savoy Pl., WC2.

15th. IEE - "Lord Kelvin and his measuring instruments" by J. T. Lloyd at 17.30 at Savoy Pl., WC2.

15 th. IEE - "Novel photo-detectors using semi conductor interfaces" by Dr. M. J. Hampshire at 18.00 at Thames Polytechnic, Riverside House Annexe. Beresford St., SE18.

16th. IEE - "The broadcasting of traffic information to road vehicles" by R. S. Sandell at 17.30 at Savoy Pl.. WC2.

20th. IEE - "High capacitance strain gauge for use at extreme temperatures" by Dr. B. E. Noltingk at 17.30 at Savoy Pl., WC2.

20th. IERE - "Developments in position measure ment techniques" by D. J. Phipps at 18.00 at 9 Bedford Sq., WCl.

22nd. IEE - "On the design of low-pass, linear phase, recursive digital filters" by Prof. S. C. Dutta Roy at 17.30 at Savoy Pl.. WC2.

22nd. RTS - Shoenberg Memorial Lecture "The Open University: a progress report and hopes for the future" by Dr. Walter Perry at 19.00 at the Royal Institution, Albemarle St., W 1.

26th. IEE - Discussion on "Measurement, test and quality control of fuses with particular reference to low voltage fuses" at 17.30 at Savoy PI., WC2.

28th IEE - Discussion on "Semiconductor devices in hostile electrical environments" at 17.30 at Savoy Pl., WC2.

28th. IERE - "Design and application of active compensation circuits for servo control systems" by Dr. D. R. Wilson at 18.00 at 9 Bedford Sq., WC1.

28th. BKSTS - "Opticals in creative art" at 19.30 at Thames Television Theatre, 308-316 Euston Rd., NWI.
29th. IEE - "The development of microwave transmission systems" by Dr. P. A. Matthews at 18.30 at King's College, Strand, WC2.

## ABERDEEN

6th. IERE/IEE - "Medical and industrial electronics - from text book to shop floor" by J. G. Mitchell at 19.00 at Robert Gordon's Institute of Technology, St. Andrews St.

## BELFAST

13th. IERE - "Forum on designing for reliability" at 18.30 at Main Lecture Theatre, Ashby Institute, Queen's University, Stranmillis Rd.

## BIRMINGHAM

21 st. IERE - - "Pin-wheels to pulses: electronics servant of postal sorting" by S. W. Godfrey at 19.00 at City of Birmingham Polytechnic, Franchise St., Perry Barr.

## BOURNEMOUTH

2Hh. IERE - "Solid state microwave sources" by H. J. Finlay at 19.00 at the Technical College.
27th. SERT - "Servicing aspects of recent Thorn colour TV receivers" by B. Hinton at 19.15 at Room B7, Bournemouth College of Technology.

## BRISTOL

15th. SERT - "Television for the blind: an eye opener into the medium" by J. Rossetti at 19.30 at Cabot House, Bristol Polytechnic, Ashley Down Rd.

28th. IERE/IEE - "Video recording" by J. Jeffrey at 18.00 at Queen's Building, the University.

## CARDIFF

14th IERE - "Solid state microwave power amplifiers" by G. B. Morgan at 18.30 at Dept. of Applied Physics, UWIST

## CHATHAM

1st. IERE -"Electronics in the commercial vehicle industry" by G. Leonard at 19.00 at the Medway and Maidstone College of Technology

## CHELMSFORD

28th. IEE - "Telephony - past; present and future" by J. B. Terry at 18.30 at King Edward VI Grammar School, Broomfield Rd.

## CHELTENHAM

20th. IERE/IEE - "Value for money in project management" by T. G. Clark at 19.30 at G.C.H.Q. Oakley.

## EDINBURGH

7th. IERE/IEE - "Medical and industrial elec tronics - from text book to shop floor" by J. G. Mitchell at 19.00 at Napier College of Science and Technology, Colinton Rd.

## GlASGOW

8th. IERE/IEE - "Medical and industrial electronics - from text book to shop floor" by J. G. Mitchell at 19.00 at Glasgow College of Technology, Hanover St

## HIGH WYCOMBE

29th. IEE - "Developments in information display systems" by R. Stafford and Dr. T. Coutts at 19.30 at High Wycombe College of Technology.

## HULL

14th. SERT - "Electronics in motor cars" by L. Phoenix at 19.30 at the E. H. Bullock Lecture Theatre, College of Technology, Queens Gardens.

## LIVERPOOL

14th. IERE - -The role of electronics in the movement of shipping" by K. D. Jones at 19.00 at Dept. of Electrical Engineering and Electronics, the University.

## LOUGHBOROUGH

13th. IERE -"Fourier analysis of video telephone systems" by Dr. D. E. Pearson at 19.00 at Edward Herbert Building, the University.

## MANCHESTER

8th. IERE - "Marconi automatic testing" by W. J. Stickland at 18.15 at Renold Building, UMIST

## NEWCASTLE-UPON-TYNE

14th. IERE - "Codes and coding" by J. T. Kennair at 18.00 at Main Lecture Theatre, Ellison Building, the Polytechnic, Ellison P|

## NEWPORT, l.o.W.

9th. IERE - "Colour television" by A. C Maine at 19.00 at Isle of Wight Technical College.

## PLYMOUTH

7th. RTS/AES - "Quadraphonics" by Dr. Keith Barker at 19.50 at Plymouth Polytechnic.

15th IERE/IEE - "Developments in digital transmission systems" by G. H. Bennett at 19.00 at Main Hall, the Polytechnic.

## PORTSMOUTH

14th. IERE - "What's new in multilayer printed wiring board manufacture" by G. C. Wilson at 18.30 at the Polytechnic.

## READING

8th. IERE/IEE - "Ambisonic reproduction of sound" by Prof. P. B. Fellgett at 19.30 at the J. J. Thomson Physical Laboratory, University of Reading. Whiteknights Park.
29th. IERE -- "Digital filters" by A. R. Owen at 19.30 at the J. J. Thomson Physical Laboratory, University of Reading, Whiteknights Park.

## SHEFFIELD

28th. IERE/IEE - "World wide communication" by R. T. Mayne at 18.30 at the University

## SOUTHAMPTON

20th. SERT - "Television receiving aerials" by R. S. Roberts at 19.30 at the Technical College.

# Entertainment Electronics at Berlin 

## 2nd International Radio \& Television Exhibition

The motto of the second international radio and television exhibition in Berlin was 50 years of German radio broadcasting, but by far the biggest attraction was video equipment. With more than a dozen different formats on show for picture playback over television receivers, the choice between four surround-sound systems takes a decidedly back seat.

The Philips long-playing video disc (VLP) system was a major feature at the show. Philips technique allows a maximum playing time of 45 min , though when the system is marketed in 1975 it will probably use a $30-\mathrm{min}$ playing time, from a $30-\mathrm{cm}$ wear-free disc.
Because the VLP discs contain one television picture per revolution a variety of operating modes are available: fast forward play (at twice normal speed), reverse continuous still picture, frame-byframe reproduction, slow motion forward and reverse (adjustable from 40 ms to 4 s ), as well as normal picture reproduction. A remote control unit allows any of 45,000 frames to be selected, amounting to almost immediate random access, and because frame-to-frame crosstalk is sufficiently low each frame can be completely different. This gives the VLP potential outside the entertainment and instructional fields.

At the exhibition details of the optical scanning, signal processing and control systems were released, but first a recap.

The disc is impressed with picture information in the form of a spiral "track" consisting of a series of $0.8-\mu \mathrm{m}$ wide, $0.16-\mu \mathrm{m}$ deep pits of variable length and at variable intervals. The repetition rate of the pits carries the brightness signal and the length of the pits conveys the colour and sound information. The rigid disc, made from a transparent vinyl polymer $1 \frac{1}{4} \mathrm{~mm}$ thick, is coated on one side with a thin metal reflecting layer and information is "read off" by a beam of plane-polarized light from a 1 mW helium-neon laser. Light is reflected by the record, picked up by a lens again and focused onto a photodiode, less light being received when a pit passes in front of the lens, due to diffraction, than when a smooth part does.

With a pitch of $2 \mu \mathrm{~m}$ (for a $30-\mathrm{min}$ disc), the track density is $500 \mathrm{turn} / \mathrm{mm}$. Half-brightness spot size is about $1 \mu \mathrm{~m}$ at the pit but is much smaller at the
transparent surface so that contamination or damage have comparatively little effect. The focused spot is located in the plane of the pits and kept there by a control system.

Another opto-electronic control system positions the beam to within $\pm 0.2 \mu \mathrm{~m}$ from the track centre and shifts the optical system radially at $50 \mu \mathrm{~m} / \mathrm{s}$, corresponding to $2 \mu \mathrm{~m} / \mathrm{rev}$. Rotational speed is $1500 \mathrm{rev} / \mathrm{min}$ for the PAL version (an $1800 \mathrm{rev} / \mathrm{min}$ machine for NTSC is due at the end of this year) or 25 rev $/ \mathrm{s}$, allowing one picture (two fields) per revolution, held to within $0.1 \%$ by a further control system.

Master records from which the moulds are made for pressing VLPs are made from glass, with a photoresist layer 100 to 160 nm thick that is cut by a high power laser. This is done in real time, with the potential that a scene can be recorded directly from a video camera. The moulds are made in the usual way from the master by electroplating.

## Signal processing

The photographic process used in writing information onto the master record is highly non-linear, so a digital recording technique is the only practical way of going about things. Using the VLP coding method, it turns out that at $25 \mathrm{rev} / \mathrm{s}$ the maximum video bandwidth is 3 MHz at the inner part of the record $(10 \mathrm{~cm}$ diameter). Thus if the normal PAL video signal was used as modulation all of the colour information would be lost, this being carried either side of 4.43 MHz . So the colour subcarrier frequency is reduced to 1.46 MHz , with a bandwidth of $\pm 500 \mathrm{kHz}$. For stereo sound, two f.m. carriers are used, one at 350 kHz and one at 650 kHz , (Fig. 1) with $\pm 50 \mathrm{kHz}$ deviation.
Brightness information, limited in bandwidth to 3 MHz , frequency modulates a 6 MHz carrier with a modulation index of less than unity. This gives first-order sidebands wider than the deviation and extending $\pm 3 \mathrm{MHz}$ either side. These signals - brightness, colour and sound
are added in the amplitude ratios of $20: 4: 1$, symmetrically limited and then recorded. Limiting provides rectangular pulses in which brightness is contained as frequency modulation, while colour and sound give a symmetrical width


Fig. 1. If the normal PAL video signal modulated the VLP disc carrier directly, colour information encoded at 4.43 MHz would be lost as video bandwidth is about 3 MHz . Therefore the colour information is transposed down to 1.46 MHz , while luminance information frequency modulates the $6-\mathrm{MHz}$ carrier, only the first lower sideband being recorded.
modulation of the pulses (Fig. 2). In effect, the sound and colour signals are singlesideband modulation of the brightness signal as the carrier and symmetrical limiting produces the upper sidebands - at the expense of power in the lower sidebands, of course.
in the recording unit, the brightness information is taken from the PAL video signal by a 3 MHz low-pass filter prior to modulating the frequency of a multivibrator circuit. This gives rectangular pulses whose harmonics must then be filtered out so that the f.m. brightness signal has a sufficiently low rise time to show pulse width modulation (by the colour and sound signals) after combination and limiting.
The colour signal from the original video signal is filtered out and fed to a variable-gain amplifier to maintain constant level of colour signal, as derived from the bursts, and then reduced to 1.46 MHz .

The playback unit has several ínteresting features. Apart from demodulating the brightness and sound signals it must restore the colour subcarrier frequency to 4.43 MHz for playback on domestic TV receivers.

Originally, the recorded colour subcarrier frequency was 1 MHz , and the PAL subcarrier at 4.43 MHz was restored using a double mixing technique together with a $\div 64$ phase-locked loop to synchronize a 1 MHz oscillator to the line sync frequency. The current system is different, in that the colour carrier is changed to 1.46 MHz - to allow an increase in modulation depth - and the colour-burst
frequency is used as a reference instead of the line sync frequency. To recreate the PAL colour signal with the requisite stability, two signals are formed; one containing the required colour modulation and the other having the appropriate stability. These two signals are made 4.43 MHz different and they are both given the same frequency shift due to speed changes; thus subtractive mixing gives the reconstituted PAL colour signal.

In practice, a $1.46-\mathrm{MHz}$ oscillator is gated by the $4.43-\mathrm{MHz}$ colour burst, plus errors in frequency, and locked with a kind of flywheel sync circuit, so that the $1.46-\mathrm{MHz}$ signal takes up the errors. This is mixed with a $4.43-\mathrm{MHz}$ crystal oscillator to give a $5.89-\mathrm{MHz}$ carrier, which apart from the errors due to speed changes is otherwise stable. Finally, this is mixed with the colour signal from the record i.e. a modulated 1.46 MHz plus drift. The modulated difference signal, with no drift and the stability of the crystal, is the PAL colour signal.

A useful feature is the drop-out detection circuit. Here information below 2.5 MHz is detected for drop-out. If a pit is missing, the detector responds to the lowered frequency by operating a switch for $3 \mu$ s to allow the brightness of the preceding line to be used instead. (A $64 \mu$ s delay line holds this.) In practice this switch operates before the signal gets to the f.m. demodulation circuits. When drop-outs occur the colour information is switched out. Because of the averaging with the signal in the previous line in PAL receivers, the missing colour fragments appear at half saturation, thus preventing spikes. There is also a sample and hold circuit in the sound channel used to counteract changes in signal level during a drop-out.

## Control systems

Constraints on the optical system result in a wide aperture and hence small depth of focus. As the depth of focus is $1 \mu \mathrm{~m}$ and the vertical record position may differ by up to $500 \mu \mathrm{~m}$ from a true plane, you can see the need for this to be accurately controlled!

Displacements are detected by measur ing capacitance between the metallized surface of the record and a $1 \mathrm{~cm}^{2}$ electrode bonded to the objective lens. At a distance of $100 \mu \mathrm{~m}$ an accuracy of $1 \%$ is sufficient to determine the objective position by $1 \mu \mathrm{~m}$. The lens is suspended in springs and driven by a coil in a radial magnetic field, rather like a moving coil loudspeaker. Capacitance is measured using an oscillator and f.m. ratio detector.

Two control systems are used to follow the pit track, one for slow tracking of the spiral and the other for rapidly centring the spot in presence of eccentricity. To keep the spot on the track, it can be moved radially by a mirror and coil pivoted in a magnetic field behind the objective lens. Control signals are obtained with two auxiliary light beams focused on either side of the track and reflected from the record surface onto two photodiodes. The difference between photodiode
outputs controls the pivoting mirror. For fast, slow, reversemotion and stationary pictures, a rapid movement during the field flyback period is needed. The mirror movement can behave like a ballistic galvanometer as the opened control loop has a low resonant frequency; the jump is effected therefore by opening the loop, applying an accelerating current pulse through the coil followed by retarding a pulse, and then closing the loop. The average current in the mirror coil controls the radial transport mechanism to move the optical system across the record.

Record speed is held to $25 \mathrm{~Hz} \pm 0.1 \%$ by a further control system that operates from a tachogenerator coupled to the turntable shaft.

## Optical systems

In "reading out" information from the track pits, a lens is used with a numerica! aperture of 0.4 . Spot size is about the theoretical minimum at this aperture, and diffraction, together with the radial Gaussian intensity distribution at the lens entrance pupil. produces an half-intensity diameter of $0.9 \mu \mathrm{~m}$. Because the pit size is smaller than this, light is diffracted and falls largely outside the lens aperture. Maximum light is transmitted to the photodetector when pits are absent.

As the laser beam is linearly polarized, a quarter-wave plate and polarizing mirror ensure that incident and reflected light beams are effectively separated (Fig. 3).

For maximum modulation of the photodetector current, reflected light from a pit must have a phase difference of $180^{\circ}$ from that reflected from the surface in the vicinity of the pit. This is arranged by making the pit a quarter-wavelength deep. The two intensities should be equal of course, and this is achieved by dimensioning spot and pit sizes so that the same amount of light falls outside a pit as falls into it. (Modulation depth achieved at the inner-most part of the track and at 7 MHz pit frequency, is 15\%.)

Despite this constraint, the most important thing in determining spot size is the highest recorded pit frequency, nomin ally 6.5 MHz . This can be altered by an intermediate lens (Fig. 3) which can make the Gaussian beam distribution at the entrance pupil of the main lens wider or narrower. The greater the homogeneity in the light distribution the smaller the spot and thus the higher the maximum recorded pit frequency.

The trade off is power in the laser beam and the particular compromise chosen means that $80 \%$ of laser power is used. The remaining inhomogeneity of the beam results in a bandwidth $92 \frac{1}{2} \%$ of the theoretical maximum. If $99 \%$ of laser power were used the bandwidth would be $16 \%$ smaller.

Crosstalk from neighbouring tracks is readily assessed because they have dif ferent pit frequencies. A crosstalk level of -50 dB has been measured for $1-\mu \mathrm{m}$ track widths which is said to be in good agreement with a level calculated by Fourier analysis.

With all this complexity the VLP player is not going to be cheap, about the cost of a colour receiver, Philips say. Nor do we expect two other optical (laser) systems (MCA Disco-Vision and one by Thomson-CSF) to be any cheaper. To make biggest impact, video systems will need to be much less expensive than that and even the Teldec TED player is costly at $£ 200$ (DM1148). The TED system will be sold in Germany from January, with Scandinavia and the U.K. to follow later. The TED disc catalogue lists well over 100 titles with discs priced between DM 10 and 25.

Philips are already talking with potential licensees as well as having discussions over standardization with MCA in the USA. Clearly, the existence of competing systems is going to seriously weaken video disc potential. Its quite unlike the $33 \frac{1}{3}-$ $45 \mathrm{rev} / \mathrm{min}$ situation or the surroundsound systems competition where the same mechanism is common to all systems. This situation will also hold back penetration of video cassette/cartridge systems. as many potential buyers will presumably hold back if a disc system with its attraction of lower-cost programmes is not too far off.

There would appear to be potential in the VLP for wide bandwidth sound coding. As the VLP system is digital, presumably the p.c.m. technique would be a possibility (see, for instance, page 548). Then we could have colour pictures and high quality multi-channel sound off the same mechanism; with amplitude response down to as low as you like, no wow and flutter, no rumble, no tracing distortion, and no distortion due to tracking error. Alternatively, one could use the wide bandwidth solely for frequency-division multiplexing with the capability of storing 30 programmes on one disc. Roll on ALP!

## Magnetic video disc

Whether other systems being developed will offer lower-cost players remains to be seen, but another technique, using a magnetic disc, promises low-cost hardware presumably at the expense of higher disc cost as a result of the more expensive duplicating process. This is the RabeBogen magnetic disc recorder (MDR) mentioned briefly last issue. Here the idea is to make use of the turntable already present in many homes. Unlike the optical and mechanical systems, it allows home recording.

A mechanical system is used to guide the magnetic record and playback head using the stylus-in-groove system. The newly developed head, with its effective gap width of 250 to 350 nm , glides across the specially treated record surface. The magnetic material is chromium dioxide with a microstructure of the order of the recorded wavelength $(500 \mathrm{~nm})$.

A rotational speed of $156 \mathrm{rev} / \mathrm{min}$ (giving a linear velocity varying from 1.63 to $2.42 \mathrm{~m} / \mathrm{s}$ at 20 and 30 cm diameter respectively) and a track spacing of $25 \mu \mathrm{~m}$ results in a playing time of 12 min per side. Bogen are currently working to reduce this to $78 \mathrm{rev} / \mathrm{min}$ to give

24 min per side. Storage density is 1.57 $\times 10^{9}$ bits per side with a track spacing of $50 \mu \mathrm{~m}$ and $3.14 \times 10^{9}$ bits per side at $25 \mu \mathrm{~m}$ - very high compared to the nominal 20,000 bits $/ \mathrm{in}^{2}$ mentioned in our video tape cassette survey (Dec. 1972 page 580 ). Bogen claim that turntable speed variations are not a problem as monochrome receivers have a synchroniza tion range of around $\pm 10 \%$.

How convertible existing turntable mechanisms without a $78 \mathrm{rev} / \mathrm{min}$ speed are we're not sure, but even if they are not, this method would still probably have a cost advantage. At $33 \frac{1}{3} \mathrm{rev} / \mathrm{min}$, eight audio channels become feasible, with a playing time of 56 min per side.

## Video cassettes

The Electronics Industries Association of Japan has recently decided to adopt three video cassette systems as standards for video tape recorders. This is an addition to the existing CP-508 standard for cartridge video machines. This last standard covers a $1.3 \mathrm{~cm}\left(\frac{1}{2}\right.$ in) tape cartridge system (the EIAJ define a cartridge as containing one tape reel and a cassette as having two) initially developed by Matsushita in 1971. Marketing of equipment for this system has been held back until now, and as a result the standard for cartridge video recorders was agreed before market introduction. Since then National have been joined by Sanyo, Toshiba, Shiba Electric, General Corporation. Victor Company, Mitsubishi and Hitachi.
Matsushita have three variants of their NTSC machine; one for record and playback, ore including a TV tuner, and one for playback only. The NV5120E shown was a PAL version of the record/ playback model (see photograph). The 1.3 cm tape used in these machines is interchangeable with that used on openreel video tape recorders.
With cassette machines, both 1.9 cm ( $\frac{3}{4} \mathrm{in}$ ) and 1.3 cm tape systems have been adopted. The three systems are: the 1.9 cm system* adopted by Sony, Matsushita and the Victor Company of Japan (now joined by TEAC and Nippon Electric Company); the 1.3 cm system of Philips (now adopted by 15 European manufacturers, one in the U.S.A. and Hitachi/Shibaden in Japan); and the 1.3 cm system of Sanyo.

For the 1.9 cm cassette, the reels are positioned in a similar way to an audio or digital tape cassette with the two reels in the same plane, Fig.4a. Here the tape needs to be slanted in relation to the head. As with most cassette systems the tape has to be extracted by a complex mechanism but fast winding must be done when the tape has been returned to its cassette. In the Philips 1.3 cm cassette the two reels are concentric,

- We have recently heard from Action Video Ltd that they are modifying N.T.S.C. versions of the $\frac{3}{4}$ in U-VCR Sony designed cassette recorders to the PAL system. Action Video are at 45 Great Marlborough Street, London W 1.


Fig.2. In coding the VLP, symmetrically limiting signals for luminance (a), colour (b) and sound (c), and combining in the ratios 20:4:1, produces a train of rectangular pulses whose frequency represents brightness and whose duty cycle carries colour and sound information.


Fig.3. If the VLP optical system, electromagnetic transducers are attached to the objective lens for focusing and to the mirror for centring and tracking. Laser beam is split by a diffraction grating to provide the two auxiliary spots before and after the main spot. Detectors either side of the main beam sense the reflected auxiliary beams to provide control signals for mirror movement.
(a)

(b)

(c)

(d)


Fig. 4 Four reel arrangements now standardized by the EIAJ for domestic video cassette/cartridge sustems.

Fig.4c (see also page 582 December 1972 issue). but as the tape is already slanted. the loading mechanism is simpler. In contrast to the $1.9-\mathrm{cm}$ cassette. fast winding is done around the head wheel. Both head wheel and tape move in the same direction to alleviate problems of the chromium dioxide tape sticking to the head wheel, making recorded tapes incompatible with open-reel machines.

In the Sanyo cassette, Fig.5b, tape loading is similar to the $1.9-\mathrm{cm}$ system. except that the capstan itself withdraws the tape. Fig.5d depicts the cartridge for comparison.

Bell \& Howell, who market JVC video equipment in Germany, Italy, Scandinavia and the U.K., will be selling the new 1.9 cm U-VCR machines made by JVC. Two PAL versions will be sold in Europe, the CR6000E recorder /player and the CR5000E player, both with remote control units.

RCA, who showed their MagTape SelectaVision video cassette system, have eliminated the complicated tape withdrawal mechanism used in most other cassette systems. The 1.9 cm tape remains in the cassette and when inserted into the player, contact is made with the heads by the headwheel entering the cassette, allowing a $90^{\circ}$ tape wrap. But this simplification hasn't produced a low-cost machine. The recorder/player costing $\$ 795$, and a camera costing $\$ 300$, will be marketed early next year. The player includes receiver circuitry for recording television programmes.

Another notable video machine is the VTC 7100 Sanyo 1.3 cm cassette recorder. Weighing 5.5 kg with batteries it is a portable machine made for the C.C.I.R. norm and is accompanied by a hand-held camera weighing 2.3 kg . The cassette measures $155 \times 107 \times 25 \mathrm{~mm}$ and plays for 20 min . It uses two heads normally and four for slow-motion playback.
Sanyo will be selling a PAL version of the colour recorder VTC 7200 in August next year.
So the current total of video playback systems announced so far seems to be: five disc systems, four cassette tape systems, one cartridge tape system, four film players, as well as various open-reel tape machines. (Two systems have recently disappeared - Cartrivision and Ampex Instavideo.)

## Surround sound

It was good to see Nippon Columbia publicly demonstrating their UMX system. This was devised by Duane Cooper of the University of Illinois and development of it has been taken up by Nippon Columbia. It arose out of considering which was the best way to transmit directional information, and theoretical analysis by Dr Cooper, using an harmonic synthesis approach, has turned up a universe of matrix systems, called UMX.

What comes out of the analysis is a two-channel phasor matrix system, called BMX, in which full mono compatibility is guaranteed, unlike QS and SQ, by deriving a truly omnidirectional signal (in
the horizontal plane) and in which a difference signal, of the same level, has a phase shift that lags the mono signal by an amount equal to the source angle measured from a certain norm. Simple sum and difference matrixing produces left and right signals whose amplitude coefficients are the same as for the QS system (see page 56 February 1972 issue), but the phase shifts are distributed in lots of $45^{\circ}$ rather than zero or $90^{\circ}$.
The chief property of the matrix is that the phase relations between speaker outputs in four-speaker playback are rotationally symmetrical, the crosstalk components of a corner sound having a phase of $-45^{\circ}$ and $+45^{\circ}$ relative to the wanted corner sound. Experiments have shown $45^{\circ}$ phase differences to be less "oppressive" than $90^{\circ}$ phase differences. As well, localization is aided by this phase arrangement.

More interesting than this is the way in which the two base-band channels can be augmented by further channels to improve "directivity" and reduce sensitivity to listener position. Two supplementary channels, both phase-encoded omnidirectional channels, can be added to the base matrix at the consumers discretion, assuming they are present in the transmission media. This in fact is Nippon Columbia's proposal in essence - that the carrier channels are there for the taking, the baseband channels giving a better surround-sound capability in themselves than other basic two-channel matrix systems.

The total of four channels provides a "discrete" system, but it has been found that a discrete effect is obtained with narrow-bandwidth carrier channels of around 3 or 4 kHz . These frequencies modulate a 30 kHz carrier with a deviation of $\pm 6 \mathrm{kHz}$ and at a carrier level of $35.4 \mathrm{~mm} / \mathrm{s}$. The maximum frequency of 36 kHz means that a much wider range of pickups can be used with this system. Additionally, noise reduction techniques are not used, with the potential of cheaper decoders, and special stylus shapes and record materials are not necessary. Ordinary cutting equipment (Neumann SX68) can be used for manufacturing, according to Nippon Columbia, using half-speed cutting with tracing distortion correction. Even 17 cm ( 7 in ) dises can be made.

It seems a great pity that this elegantly superior system is not available yet on the market, although Nippon Columbia have equipment at the ready. Maybe the uncommitted record companies, like Decca and Polygram, are looking to video disc techniques! But as there are three other surround-sound systems being marketed we think this one is deserving of at least an equal place in the market.

There is also a Qmx technique for surround-sound tape cassettes, which has a signal-to-noise ratio advantage over the proposal to divide the cassette tape into eight separate tracks. This is now more than a proposal as JVC are showing their four-channel cassette machine (noted on page 460 , September issue) which claims a 48 dB signal-to-noise ratio with
the JVC automatic noise reduction system.
Sansui were demonstrating integratedcircuit versions of their Variomatrix QS/RM circuitry. Three Hitachi chips will be available shortly in production quantities and they report considerable interest from European companies for their system. SQ is making inroads on the Continent, with Blaupunkt, Braun, Elac, Grundig, Körting, Loewe-Opta, Philips, Revox, Saba, Sharp, Siemens, Telefunken and Wega building in decoders. Connaught Equipment (Tate) announced an improved SQ automatic control technique that reportedly gives an all round 20 dB separation, but details are not being released yet.

National were demonstrating fourchannel broadcasting by distributing composite f.m. transmissions at 103.5 MHz to the Dorren Quadraplex system for reception by exhibitors. Dorren has also produced a chip for CD-4 demodulation. Claimed to be the biggest consumer i.c. produced, it is an l.s.i. 28-pin circuit with 320 transistors on the chip, and will be available in December.

But the most striking surround-sound demonstration at Berlin was the Sennheiser dummy-head stereo documentary disc. Intended for open-air headphones it sounds excellent with the closed type too. With it, one can apparently perceive sound images over three dimensions with astonishing realism using merely a dummy head containing two microphones, ordinary stereo equipment and stereo headphones. The record must be heard to be believed $\dagger$. There didn't seem to be any ambiguity, although the frontal images weren't quite as convincing as the back ones. During the exhibition stereo transmissions were made from RIAS, Berlin using this technique, and many press reports in Germany were calling this the sensation of the exhibition. Production of the record followed some interesting psychoacoustic work at the Heinrich-Hertz-Institut, on which we hope to report later.

## Cassette machines

In this tenth year of the compact audio cassette one might have expected Philips to commemorate it in some way. Talk in recent years about four-channel, eighttrack cassettes led one to suspect that Philips may have overcome the problems associated with dividing down the track into eight sections, plus guard bands. Problems like reduced signal-to-noise ratio, worsened crosstalk, worsened tape wander and more critical tape/head alignment. But instead JVC have announced the very thing, using their automatic noise reduction system of DC-4 fame -a compatible competitor to the Dolby "B" system.

Grundig have adopted the Philips dynamic noise limiter in their CN710 and 720 machines, which both incorporate $\mathrm{CrO}_{2}$ tape switches, and claim a $50-\mathrm{dB}$ $\mathrm{s} / \mathrm{n}$ ratio with $\mathrm{CrO}_{2}$ tape and d.n.l. A number of new Dolby " $B$ " machines were seen, including the Telefunken

C2200, Trio KX-700, Sharp RT-480H, Uher CG360 with Dolby i.c. and 10-watts per channel output power, Aiwa AD- 1500 with a wow and flutter of $0.07 \%$ r.m.s. weighted (similar to Teac A-450 mechanism?) and $60 \mathrm{~dB} \mathrm{~s} / \mathrm{n}$ ratio with $\mathrm{GrO}_{2}$ tape, $\mathrm{B} \& \mathrm{O}$ Beocord 1700 with a claimed $61 \mathrm{~dB} \mathrm{~s} / \mathrm{n}$ ratio, and Dual C901 with wow and flutter of $0.09 \% \quad$ r.m.s. weighted $(0.12 \%$ DIN). Latest Dolby licensees are Garrard and Nordmende. A reported world shortage of chromium dioxide is slowing down penetration of the BASF Dolby cassettes and, while they were in evidence at Berlin. they are not expected to be marketed in the U.K. until late next year.

Hitachi have a new machine, model D-4500, with a combined record and playback head, claimed to be the first of its kind and using a three-motor, dual-capstan system. They claim the astonishingly low wow and flutter figures of 0.035 to $0.05 \%$ r.m.s. weighted. Most interesting open-reel tape recorder was the new Revox A700, which will no doubt be seen at London's Audio Fair along with their digital-readout receiver and some other products we haven't included.

To round off, here are some things that won't be at Olympia. Like television sets with headphones - one by Nordmende uses an infra-red link and many have sockets for connecting external audio amplifiers, elaborate ultrasonic remote controls, and in-line picture tubes. digital channel identification superimposed briefly on the screen on channel changing (Blaupunkt), a "stereo-quadro superthing" by Blaupunkt reportedly containing 650 transistors, 35 i.cs and 127 l.e.ds and with no moving parts; SECAM/PAL converters by Grundig and Blaupunkt; a colour projection system by Sony based on the Trinitron tube; and plenty of European-made portable colour sets.

As this report is entitled entertainment electronics we must mention the ITTShaub Lorenz Odyssee game device. This is a way of using a c.r.t. display to play games, in a similar way to the devices now appearing in some public houses. The ITT one is much better; it uses the domestic television receiver via the antenna input. The equipment includes waveform and video generators, programme cards that determine the display for one of ten games, modulator and sync circuits, vertical and horizontal movement controls for two players together with "ball" speed controls. When a "ball" and "player" meet ball direction is reversed. In some games. a coloured foil is attached to the screen to provide boundaries or tracks in the case of a track-following exercise. Options are table tennis, lawn tennis, volleyball, ice hockey, football, and five other amusements. Price is DM 400 .
+We hope to demonstrate this record on the Wireless World stand during the Audio Fair at Olympia. It is available from Sennheiser's U.K. agent Hayden Laboratories Ltd. 17 Chesham Road, Amersham, Bucks, price 50p.

## International Audio Fair

## Olympia, October 23rd to 28th

An increased number of exhibitors over previous years will be at the Audio Fair this year. A list of the brand names at the show is printed overleaf and some of the equipment which will be shown for the first time is also described briefly. The show is to open from 10 a.m. to $9 \mathrm{p} . \mathrm{m}$. except the final day, Sunday, from 11 a.m. to 7 p.m. Cost of admission will be 45 p . Wireless World has again organized five of the lectures which will run during the course of the show.
Admission for the lectures is free, but tickets must be obtained beforehand, either from the information kiosk or through an exhibitor.

## Lecture demonstration programme

Tues. 23rd Oct.
2 p.m. Sound synthesis for the amateur by Douglas Shaw

4 p.m. Quadraphony and music by Mike Thorne

6 p.m. High fidelity loudspeakers - fact or fiction?
by Frank Jones
8 p.m. The available signal
by Angus McKenzie (W.W. presentation)

## Wed. 24th Oct.

2 p.m. Multi-channel sound recording systems
by Dr. Keith Barker
4 p.m. Magazines - the technical
interpreter
b.' Basil Lane (W.W. presentation)

6 p.m. The progress of sound reproduction by Ralph West

8 p.m. Repeat of 6 p.m. lecture
Thurs. 25th Oct.
2 p.m. Keep it clean
by Donald Aldous

4 p.m. Sound waves in rooms
by Roger Driscoll
6 p.m. Test results and performance can they be related?
by Dr. Arthur Bailev (W.W. presentation)
8 p.m. What goes on in a recording studio by Adrian Hope

## Fri. 26th Oct.

2 p.m. A fresh look at audio noise reduction systems
by David Rees (W.W. presentation)
4 p.m. The objective and subjective assessment of loudspeakers
by Gareth Jefferson
6 p.m. A musical programme on how a record show is produced and presented by John McGinn

8 p.m. Quadraphony and music by Mike Thorne

## Sat. 27th Oct.

2 p.m. The music scene and the recording heard
by Joan Coulson
4 p.m. Audio advertising
by Rex Baldock
6 p.m. Practical limitations of audio equipment
by J. L. Linsley Hood (W.W. presentation)
8 p.m. A live concert of contemporary music presented by Capricorn

## Sun. 28th Oct.

2 p.m. New motional feedback loudspeaker system
by Roger Driscoll
4 p.m. The record risibility factor
by Donald Aldous

## Special Event

On Tuesday 23rd at 11 a.m. there is the annual prize giving and presenting of trophies to winners of the British Amateur Tape Recording Contest, 1973.

## Exhibition Briefs

The Shure V15 Mk III cartridge, introduced earlier this year has a new laminated magnetic core structure and a stylus as sembly with a $25 \%$ reduction of tip mass.

A speaker system of interest from Eagle is a six-way system -two tweeters, two mid range and two bass units - the AA42.

The series 3400 X stereo recorder will be shown by Tandberg. This is based on the recently introduced 3300 X tape deck but includes 15 W per channel amplifiers, integral speakers and linear motion output potentiometers.

A new amplifier introduced by Sinclair is the System 4000 , providing 17 W continuous power, both channels driven into $8 \Omega$. Varicap tuning and a four-pole ceramic filter i.f. section are incorporated in the matching 4000 tuner.

Two recently announced Garrard automatic turntable units with belt drive (available in November) are the Zero 100SB and the 86 SB . Both are powered by a screened four-pole synchronous motor fit ted with a two-step pulley. The 100SB incorporates the tangential tracking arm of the earlier model plus an automatic record counter to monitor stylus wear. A turntable unit QZ100SC with a built-in fourchannel decoder for either CD-4 or SQ recordings will also be on show.

A new company at the Audio Fair will be N.E.A.L. (North East Audio Limited) who are producing a cassette model 102 which combines the 3M Wollensak transport mechanism with circuitry incorporat ing Dolby B , solid-state switching, twin p.p.ms, separate low noise, high overload margin input amplifiers for microphone, low level line and high level line (f.e.t.) inputs and separate switched recording and playback circuits for equalization of ferric and chrome tapes. The transport features bi-peripheral drive.

Philips will be demonstrating their motional feedback loudspeaker system, the principle of which was described in Wireless World, September 1973, pp. 425 426.


New cassette recorder introduced by N.E.A.L. See overleaf exhibition brief.

Model 104 "reference" loudspeaker from KEF. The system has a new 8 in mid-range/ bass unit, the voice coil of which operates safely up to $250^{\circ} \mathrm{C}$, providing the new unit with a handling capacity of 50 . A B139 is coupled acoustically to the 8in driver.

| ADC | Gabraphone | Revox |
| :---: | :---: | :---: |
| AKG | Gale | Rola Celestion |
| Acoustic Research | Garrard | Rotel |
| Agfa | Goldring |  |
| Akai | Goodmans |  |
| Alba Grundig |  |  |
| Alpha H.M.V. |  | Saba Sanyo |
| Altec | Hacker | Scan Dyna |
| Amstrad | Hi Fi Aids | Securette |
| Arntron | Howland West | Servosound |
| Antiference |  | Sharp |
| Ateka | I.T.T. | Sherwood |
| Audio Packs | International | Shure |
| Audio-Technica | Artists | Siemens |
| Audiotronics |  | Sinclair |
|  | J. Beam | Sonab |
| BASF | J.B.L | Sonotone |
| B \& 0 | J.V.C. | Sony |
| BSR Macdonald | Josty Kit | Soundesign |
| B \& W | KEF | Sound-Picture |
| Bib | Keletron | Stax/Era |
| Binatone | Koss | Steepletone |
| Bose |  |  |
| Brahms | Leak Murphy |  |
| Braun | Learjet | Tandberg |
| Bush Arena | Marantz | Tannoy |
|  | Marconiphone | Tate |
|  | Markovits | Teac |
| Cambridge Audio | Metrosound | Teledyne |
| Connoisseur | Musitapes | Toshiba |
|  | Musonic | Trio |
|  |  | Tripletone |
| Darby | N.E.A.L |  |
| Decca | National Panasonic | U.D.T. |
| Diamond Stylus | Nu-Way | Uher |
| Dynatron | Onkyo | Ultra |
| Eagle | Paddock Tidy Philips | Van der Molen |
| Electrokit | Philips | Videosonic |
| Empire | Plustronics | Videotone |
| Encore | Precision Tapes |  |
| Era/De Banks | Pye | Weltron |
| Ferguson | Q.A.S. | Wharfedale |
| Ferranti | Quad |  |
| Ferrograph | Quadrasonics | Yamaha |

## Harrogate

## Audio Show

"Audio 73", housed in over four floors of the Hotel Majestic, Harrogate, from August 31st to September 2nd offered an opportunity to examine some of those products unlikely to appear at the London show.
Among these, Ampex have devised a simple solution to the problem of residual tape head magnetisation, comprising demagnetising arrangements within a cassette cleaning tape. Available from Tape Music Distributors Ltd of St. Albans, this is loaded and played through in the normal way. Prices are $£ 2.20$ and $£ 2.91$ respectively for cassette and cartridge formats.

Ariston Audio introduced a low mass ( 310 g ) stereo headset, type HS 100 , of Japanese origin. This uses a moving coil diaphragm drive, open backed to minimize colouration, and with a sensitivity of 105 dB per mW and 0.5 W handling, produces high level sound from low power amplifiers, the matching impedance being 4 to $32 \Omega$. Price is $£ 21$.

Richard Allan, one of the few remaining postwar firms, has added the "Academy" i.b. enclosure to their loudspeaker range. It employs $300 \mathrm{~mm}, 125 \mathrm{~mm}$ and 20 mm diameter drive units to cover the audio band, each assembled from basic parts within the Richard Allan organisation to ensure uniformity and auality of production. Costing $£ 75$, the speaker occupies 4 cu.ft and weighs 60 lb .
R.N.B.

# A simple muting circuit for use with f.m. tuners 

by P. Hinch, B.Tech.

In recent years the automatic noise limiter has become an increasingly common addition to high quality f.m. receivers. Such a circuit greatly simplifies tuning of the receiver by selecting a minimum signal level below which the audio output is muted. Apart from the removal of interstation noise, a squelch circuit can also ensure that only the local transmitters of the national stations are received. With high sensitivity tuners (such as the NelsonJones design ${ }^{1}$ ), it is not always immediately apparent when the "wrong" transmitter is being received, untii the poorer signal-to-noise-ratio becomes evident. A further bonus is the removal of tuning ambiguities in the absence of a.f.c., caused by the shape of the discriminator response curve; a high level, distorted signal is received on eithet side of the true signal due to the i.f. falling on the wrong slope of the discriminator response.

The usual method of achieving the a.n.l. function is to detect amplitude modulation of the i.f. after limiting. If noise is being received, the i.f. amplitude occasionally drops to zero due to noise cancellation. These gaps in the i.f. waveform can be
detected, and used to operate the muting circuit. However, in a circuit designed to be an add-on unit for existing tuners, it was considered undesirable to make connections into the i.f. strip of the receiver. The circuit described requires no modifications to the tuner, except, in the case of monaural reception, removal of the de-emphasis capacitor.

The circuit relies on the fact that, while the signal bandwidth is restricted to a maximum of 53 kHz (for stereo signals), the noise bandwith extends to over 100 kHz . A third order high pass filter is used to reject the signal and yet allow noise to pass through. The resultant signal is amplified and detected, so producing a d.c. output related to the amount of noise being received. This is used to operate an f.e.t. switch, which mutes the output of the receiver. For mono reception, provision is made for adding a de-emphasis capacitor at the output.

## Circuit description

The first stage is an emitter follower designed to provide a high input impedance which is substantially constant with


Fig.2. A sketch graph of the f.e.t. $V_{D S}=I D S$ characteristics.
frequency. This is important in order to avoid amplitude and phase distortion of the stereo multiplex waveform when fed from a receiver having an appreciable output impedance. The input capacitor to the emitter follower has a value of 68 pF . giving a first order high-pass characteristic with a cut-off frequency of 100 kHz . The variation in amplitude at the input when fed from a source impedance of $2.2 \mathrm{k} \Omega$


Fig. 1. Complete circuit of automatic noise limiter.
(as in the Nelson-Jones design) is then only 0.3 dB from 1 to 53 kHz .

The second stage is a Sallen-Key type second order high pass filter with a cut-off of 100 kHz , presenting a low impedance drive to the voltage amplifier stage ( $T r_{3}$ in Fig. 1.). The detector $\mathrm{Tr}_{4}$ switches when the amplifier output reaches about 1.4 volts peak-to-peak. The detector output passes through a low pass filter" ( $R_{13}, C_{8}$ ) which prevents accidental muting caused by brief noise spikes on an otherwise low noise signal (for example, those. caused by badly suppressed car ignition systems). The muting action is performed by a p-channel junction f.e.t. used as a switch.

## Design of the f.e.t. switch

If an f.e.t. is operated under conditions of low gate-source voltage and low drainsource voltage, it acts as a linear resistance, the value of which is controlled by the gatesource voltage (see Fig. 2). For the 2N3820 device used in this design, the minimum "on" resistance is typically around $400 \Omega$. In order to avoid distortion it is clear that, in the "on" state, the drain-source signal voltage must be kept to a minimum, as also must the gate-source signal voltage. If either of these is allowed to rise, the drainsource resistance will vary over the cycle, and distortion will be generated. Thus an f.e.t. switch as shown in Fig. 3 was found to generate $0.5 \%$ distortion at 0.5 V r.m.s. input. For higher input levels the distortion increased drastically. This was considered unacceptable for high quality reproduction.

The solution to this is to connect the f.e.t. $\left(T r_{s}\right)$ to the virtual earth point of a feedback amplifier, as shown in Fig. 1. At this point, signal levels are very low.


Fig.3. Elements of the f.e.t. switch used to control the receiver output.

In this curcuit, distortion was found to be $0.03 \%$ at 53 kHz , and 0.5 V r.m.s. input. The distortion was almost entirely second harmonic, and at low frequencies the level was reduced still further. The attenuation in the "off" state was found to be -60 db relative to 0.5 V r.m.s.
This design has the added advantage that de-emphasis can be added for mono reception, by connecting a 2.2 nF capacitor across the base and collector of the transistor.

Constructional Details The layout is not particularly critical, but long leads should be avoided, especially to the base of $T r_{1}$. It is, of course, important to remember to remove the receiver de-emphasis capacitor if one was fitted for mono reception. In the case of the Nelson-Jones tuner the designer recommends replacing this component with 150 pF .

Performance The circuit has been in use for some time in the author's Nelson-Jones tuner. It has proved to be highly immune to transient interference, and greatly simplifies tuning of the main national and local

Components list
Resistors:
$R_{1} 1 \mathrm{k} \Omega$
$R_{2} 47 \mathrm{k} \Omega$
$R_{3} 47 \mathrm{k} \Omega$
$R_{4} 2.2 \mathrm{k} \Omega$
$R_{5} 22 \mathrm{k} \Omega$
$R_{6} 10 \mathrm{k} \Omega$
$R_{7} 15 \mathrm{k} \Omega$
$R_{\mathrm{y}} 39 \mathrm{k} \Omega$
$R_{9} 2.2 \mathrm{k} \Omega$
All 5\% carbon.
Potentiometer:
$R_{19} 1 \mathrm{k} \Omega$ lin. preset
Capacitors:
$C_{1} 68 \mathrm{pF}$ silver mica
$C_{6} 10 \mathrm{nF}$
$C_{2} 1 \mu \mathrm{~F}$
$C_{3} .150 \mathrm{pF}$ silver mica
$C_{7} 10 \mathrm{nF}$
$C_{4} 150 \mathrm{pF}$ silver mica
$C_{8} 100 \mathrm{nF}$
C 5100 nF
$C_{y} 1 \mu \mathrm{~F}$

All capacitors except $C_{1}, C_{3}, C_{4}$, may be $20 \% C_{1}, C_{3}, C_{4}$ should be $5 \%$.
Transistors:
$T r_{1}$ to $\operatorname{Tr}_{8} \quad$ 2N930
$T r_{+} \quad$ BC214L
$\operatorname{Tr}_{5} \quad$ 2N3820
$T_{6} \quad$ 2N930
Diode:
$D_{1} \quad$ IN914
stations. To enable reception of distant signals a switch has been included to short the gate of $T r_{5}$ to ground and defeat the muting operation.

## Reference

1. "F.M. Stereo Tuner" by L. Nelson-Jones, Wireless World, April-May 1971.

## Sound Recorder uses P.C.M.

## Or how to eliminate wow and flutter, crosstalk and modulation distortion

Pulse code modulation has been used by Nippon Columbia, the well-respected Japanese soft ware and hardware company, for the first time for studio master tape recordings to eliminate the conventional tape recorder with its limitations. Though other techniques, in particular that of pre-distortion to reduce playback tracing error, may possibly give greater audible improvement, the use of the p.c.m. technique is outstanding in the number of problems it removes at one go.

The p.c.m. recorder, developed by Nippon Columbia in co-operation with NHK Research Laboratories, removes ghosting. wow and flutter. crosstalk and modulation distortion, at the same time


In this eight-channel p.c.m. system for making studio master recordings, fidelity already improved over conventional tape recorders as illustrated in the graphs - can be further improved by duplicating channels where only two or four are required using digital error-correcting procedures.
reducing harmonic distortion to $0.1 \%$, providing a dynamic range of better than 75 dB and an amplitude response extending from d.c. to 20 kHz . The p.c.m. system has eight channels, is capable of half-speed reproduction (to increase cutting capacity), features an additional head to give an advance signal for variable-pitch recordings, and is equipped for automatic editing and splicing. Records made with this system are already available in Japan and additionally feature halfspeed cutting and anti-tracing-distortion cutting.

To pulse-code modulate the eight audio channels, signals are first sampled at a rate of 47.25 kHz , three times the frequency of 525 -line, 30 -field $/ \mathrm{s}$ horizontal sync pulses (recorded waveforms are similar to television signals enabling a video tape recorder to be used together with a monitor). The sampled signals are then quantized by an a. to d. converter, see block diagram. A linear binary coder uses 13 bits to specify the quantization levels, and together with a parity check bit for error detection and a check bit for phase shift detection, makes 120 bits per sample, for the eight channels. (Low radix coding is used in p.c.m. to improve noise immunity, the price being bandwidth - hence the video recorder.)
Synchronizing information is carried on the front and back porches of the horizontal sync signal, using a clock frequency of 7.1824 MHz . The televisionlike system makes it quite different from the BBC p.c.m. transmission system, where a 14-bit code is used for each of 13 channels which, with 9 -bit sync data and 5 -bit data for transmitter switching, makes 196 bits per sample; sampling rate 32 kHz .

On playback the signals are routed into their channels, error detected and checked for drop-outs. If a sample is missing the preceding and following signals are averaged, and when more than one sample is missing, the preceding signal is maintained. Errors can be further reduced by duplicating information. If only four channels are required, samples for channels, 1 to 4 are staggered by one sample and fed to channels 5 to 8; re-ordering the signal means that larger drop-outs can be tolerated. The two samples of the same information are compared and only the correct one transmitted. If both samples are missing, the interpolation technique is used. Finally, the signals are passed through a d. to a. converter and filtered to remove the sampling frequency.

Half-speed reproduction is achieved by halving the clock frequency and low-pass filter cut-off frequency. The advantage of half-speed disc cutting was recognized some time ago (Nippon Columbia have a patent on this dating to 1956) and it's claimed that the permissible input to the cutter head can be increased by four times at h.f. This is used on Columbia* Mastersonic p.c.m. recordings

[^3]

To achieve the necessary bandwidth for p.c.m. this recorder uses a conventional 525-line video tape recorder. Editing is made easier by the provision of a $30-\mathrm{Hz}$ frame synchronizing signal on the control (audio) track.

With the p.c.m. tape recorder harmonic distortion is reduced by an order of magnitude over conventional tape recorders

As well as featuring a flat amplitude response from d.c. to 20 kHz , the p.c.m. technique shows excellent linearity of input-output level and a noise level that permits at least $75 d B$ dynamic range.
as well as "non-distortion cutting". This last-mentioned technique uses a tracing simulator at the recording stage to offset the tracing distortion due to the finite size of the playback stylus, giving a reduction in distortion of an order of magnitude.

There are clearly other applications for this technique. As well as laboratory testing it will be of value for data recording where wide dynamic range, operation down to d.c., low distortion, and high stability are important e.g. in noise and vibration work, speech and music analysis and seismic studies.


on h.f., whereas dipole-type wire aerials remain popular for c.w. operation; for beam aerials the Quad and associated Delta-loop aerials appear to be making increasing impact although the Yagi remains by far the most popular arrangement for rotary beams. And, in common with most of electronics, a trend towards greater use of integrated circuits and a wide range of semiconductor devices.

## On the bands

The R.S.G.B. has appealed to its members to adhere to the I.A.R.U. Region 1 voluntary h.f. band-plan affecting the 3.5 to 28 MHz bands, stating: "The band plan is reviewed at three-yearly intervals and is considered by the national societies to be practical and worth while. However, this view is obviously not shared by a small minority . . one solution is to make the sub-division of each band apart of the licence regulations". It points out that if necessary the Society's MPT Liaison Committee will not hesitate to make such recommendations to the Ministry. The current problem is the increasing "intrusion" of phone stations into segments of the band voluntarily reserved for c.w. and r.t.t.y. operation.

According to the Cheltenham group newsletter, G. V. Farrance, G3KPT has worked 39 countries (including the United States, Canada and the Panama Canal Zone) on 7,14 and 21 MHz bands using one of the low-power ( 2 watts) Heath HW-7 transceivers which include a direct-conversion receiver and all-transistor transmitter, using a simple inverted-L aerial 66 ft long and between 26 ft and 6 ft high.

Contacts by means of reflections from meteor trails continue to be made by British amateurs on 144 M Hz with stations in Italy, Hungary, Sweden and so on, particularly during the periods of the major meteor showers.

## In brief

An R.S.G.B. lecture on aerials is being given by Les Moxon, G6XN, at the I.E.E., Savoy Place, London WC2 on I hursday, November 8 . . . The amateur club station, G3SSO. of Government Communications Headquarters, Cheltenham, has won the R.S.G.B. h.f. contests championship for 1972-73, based on the results of six different h.f. contests. F. Cooper, G2QT, of Ashford, Kent was runner-up The annual R.S.G.B. 7 MHz contests will be held on October 20-21 (c.w.) and November 3-4 (phone) . . . . The death has occurred of Harold Jones, G5ZT of Plymouth, a founder member of the Plymouth Radio Club and one of the pioneers in this country of longdistance slow-scan television (some of his results were described and illustrated in World of Amateur Radio, September 1971)

The phone section of the "CQ world-wide contest" is on October 27 to 28 with the c.w. section on November 24 to 25 .

PAT HAWKER, G3VA

# Tuners and Tuner-Amplifiers 

# A résumé of the techniques used in modern designs and the standards upon which specifications are based 

by Basil Lane


#### Abstract

The purchase of a tuner or tuner-amplifier is often determined by the following factors; price, in terms of value for money; aesthetic appeal - since the new acquisition must integrate with the room décor and finally performance. The relative importance of each of these depends on the individual and the first two are purely matters of pocket and taste. The final factor should be a simple case of fixing a required specification and then comparing this with the appropriate product data. However, the solution is not so easily reached - as is described in the following article.


To attempt to review the progress in the design of tuners and tuner amplifiers over the past year is rather like taking a current model of the Morris Minor and reviewing it as something new. In general, the circuitry of receivers and tuners is fixed by an outline block schematic which has not changed for many years; the only differences can be seen in component detail, with an increasing usage of integrated circuits particularly in the i.f. stages - f.e.ts in the r.f. amplifier stage and ceramic filters. Even the trend towards using varicap diodes for the tuned r.f. amplifiers seems to have halted and perhaps even reversed.

Of course, quadraphony has been the biggest talking point of this last twelve months, but in as much as it raises the price of many receivers by quite a considerable amount, it has had very little effect upon the popular market place. To complicate the matter still further, there are several systems extant and every possibility of quite a pro longed battle before any one emerges as the victor. In almost all cases, the manufacturers that have opted to include quadraphonic decoders in their receivers have chosen to provide for all the major systems. Just to refresh the memory, these are the SQ matrix system of CBS, the QS matrix system of Sansui, the CD4 of RCA Victor and finally, as if that is not enough, some have opted to provide four channel synthesis from
conventional stereophonic recordings and broadcasts.

Although the matrix systems lend themselves to the conventional mass production of dises and replay systems, few próponents entirely own an equipment manufacturer, as do the Victor Company of Japan. The interests of RCA Victor are certainly reflected in the range of JVC Nivico receivers which are almost all fitted with CD4 system decoders. Such a situation will not prevail for very long as it is expected that at least the CBS licencees will show a considerable number of new products at the Audio Fair this year. Not mentioned so far and not included in the table, is the equipment end of Sansui who have not, as yet, provided details of products available but which are believed to have a number of quadraphonic receivers. Apart from the developing market for quadraphony, reflected in the increasing range available, novelty of circuit and user facilities are conspicuous by their absence. There are, however some "fine detail" improvements which can be commented upon; for example, the new Ferrograph tuner SFMl which has a facility for varying the muting threshold to suit signal strength for the particular conditions prevailing. In addition it includes the very unusual feature of a continuously variable separation control from full stereo to mono. permitting an optimal setting for


Fig. 1. The Nikko STA Receiver showing the additional tuning indicator on left.
minimum subjective noise.
Several tuners and receivers have been improved by the addition of a tuning meter in addition to the normal "centre of channel" meter used for f.m. stations. The tuning meter makes rather more sense since it measures actual signal strength available and so can be used to assist the correct alignment of aerial arrays. Phase-lock-loop decoders are also becoming more popular, with Armstrong, Pioneer and Fisher all having models incorporating this type of circuit.

Cambridge Audio have just produced a new tuner, the T55, which not only uses phase-lock-loop stereo decoding but also modern design techniques in all other stages. The r.f. and mixer stages utilize m.o.s. transistors, and varactor diode tuning. Although any tuner which has varactor tuning can be remote controlled. few actually have the external connection point. The Cambridge tuner has such a facility plus connections for remote signal strength indication and a.f.c. switching.

With a.m. broadcasting such a well established fact and receiver design virtually static in this area, it comes as a surprise to see some sort of innovation from Philips in the RH720 receiver. Adopted from com munications receivers, there is a control which permits the bandwidth to be varied to reduce interference or improve the frequency response of the tuner. Touch controls are also featured on this tuner, offering instant selection of up to six preset stations.

Two products which look obviously different are the Harmon Kardon Citation 15 and the Sherwood SEL 300. The first of these is perhaps one of the most innovative of modern tuners since not only is the tuning dial a drum type, more often to be found in laboratory instrumentation, but also a quieting and a tuning meter are incorporated. The really new item is the introduction of a Dolby ' $B$ ' noise reduction unit. For some time Dr. Dolby has advocated the use of the ' $B$ ' system as a way of increasing the area over which satisfactory stereo reception can be obtained. As yet there have been no professional broadcasts made here in the U.K. using this principle although an experiment has been made in the amateur band by G30SS, Angus McKenzie. He reported quite good results although insufficient data was obtained to determine the exact degree of improvement. However several American broadcast stations are making use of Dolby
' $B$ ' encoding and the Citation 15 was obviously designed to exploit this to the full. This tuner is also unusual in that the design of the i.f. strip appears to be a retrograde step away from integrated circuits and ceramic or crystal filters to a complex 9 pole phase linear LC network. Although this is obviously more difficult to set up at the manufacturing stage, Harmon Kardon claim that the performance justifies the technique adopted.

The Sherwood SEL 300 would appear to be unique in displaying the tuned frequency in the form of a digital display. Seven segment incandescent lamps are used, driven from a logic circuit consisting of seventeen i.c. packages, and a crystal controlled clock oscillator. The i.f. filter is even more complex than that of the Citation 15 , being a 12 pole "Le Gendre" toroidal filter which is claimed to offer an even sharper cut off than the crystal types.

Two Trio products appear to have surprising features, the KR-5200 in particular, though it may be something which appears as a result of the terrible translation presumably from the Japanese original. The data sheet suggests that the f.m. i.f. strip uses a combination of mechanical filters (!) and other forms of filter, presumably $L C$ types, to give a really sharply defined passband. Although the mechanical filter has been a feature of communications receivers for many years, it is very surprising to find them in a domestic receiver. There has been, unfortunately, no opportunity to check this against the circuit diagram and so the accuracy of the statement is open to question.

An additional circuit feature mentioned in the brochure for the KR-5200 is the double switching stereo demodulator which uses antiphase cancellation of crosstalk to improve the stereo separation. This has echoes of the Delta 75 receiver system used by Leak, where crosscoupling can be switched in by selecting one or both "quasi-stereo" buttons on the front panel to reduce background noise on weak stereo signals.

The second of the two Trio products mentioned is the KT-8005, a tuner which, if the data sheet is anything to go by has perhaps the most outstanding performance of any of those listed in the table. With a usable sensitivity of $1.5 \mu \mathrm{~V}$, an f.m. stereo distortion of $0.3 \%$ and a capture ratio of 1.0 dB , the KT- 8005 must be quite a remarkable design.

## Product data

The data sheet associated with any particular tuner or receiver is obviously designed to attract the potential purchase, and with the Trade Description Act hanging over the writers' heads, they cannot afford to make any claim which cannot be substantiated. However, in compiling the table for this survey it has become evident that the quantity and quality of the technical data referring to performance is extremely variable.

On the one hand there is ITT with the new TA-1-200 which has as data the barest information on power output and none on


Fig. 2. The latest product from Ferrograph, the SFM1 tuner.
the performance of the tuner section at all and on the other hand, Sherwood or Trio and many others that give a profusion of detail.

For buyers, it is the comparison of performance, giving in turn some idea of value for money, which would be of considerable use in making a decision on what to buy. Even worse, when plenty of information is given, the measurement methods used by different manufacturers often invalidates comparison. The Editor, in the lead editorial for last month, brought out one aspect of this when he commented that the only national standard which assists by defining a minimum quality for hi-fi, was that produced by DIN. Two interesting points arise from this, first that although many manufacturers say that their product exceeds the DIN 45500 specification, almost all of them quote measurements made to the old and rather dated American IHF standard. (IHF stands for Institute of High Fidelity.)

In some instances no indication is given of the measurement method and just bare figures are quoted. These must be, for many, useless and often confusing figures making comparison impossible. Criticism of the British Standards Institute for not taking some lead on this topic, evoked the response we see in the Letters column this month. The'fact that the BS committee TLE/26 has been working on this standard since 1968 and still has not come up with a final proposal, is an indication that it could still


Fig. 3 An internal view of the Goodmans One-Ten.
be some time before something appears and even then it may look nothing like the proposal or, if it is not publicised, that is no guarantee that it will be used. He remarks that the press is a significant factor in the acceptance of such standards, a point which cannot be denied, but even more important is its acceptance by industry, and as we have seen this is not just a matter for the press to solve.

The BS proposals for minimum quality are, it must be emphasised, still at an early stage, but in brief the details are as follows: The measurement techniques to be used are those specified in BS 4054:1966, which it is to be noted does not acknowledge the existence of stereophonic systems! The frequency ${ }^{2}$ response ${ }^{4}$ measured at $30 \%$ utilisation (the stereo term for deviation) to 1 kHz modulation should be $\pm 3 \mathrm{~dB}$ between 40 Hz and 12.5 kHz and $\pm 2 \mathrm{~dB}$ from 250 Hz to 6.3 kHz . The disparity between channels between 250 Hz and 6.3 kHz is limited to 2 dB . Details of the minimum requirements for sensitivity, distortion and so on are contained within Part 2 of these proposals which, unfortunately, were not available at the time of going to press. It is known however, that there is some similarity in these proposals with those of the DIN 45500 but the notable exception is in the test signals used. Modulation for the DIN sensitivity test is 15 kHz and the sensitivity is expressed at the 26 dB quieting point. The remainder of the test procedures relating to the tuner section of a receiver and tuners are similar. The more popular IHF standard differs in many ways from both the DIN and the proposed BS standard. Again, the test signal varies, being a carrier modulated to $100 \%$ by a 400 Hz tone and in addition, the usable sensitivity is considered to be the point which separates total distortion (including hum and noise), from the audio output of the tuner produced by the test signal, by 30 dB .
Despite the existence of the DIN and the IHF standards, some manufacturers still persist in quoting sensitivity to other levels of quieting and to other deviations. Examples of these are to be found in the table at the end of this article.

Many of these problems of comparison would be alleviated if manufacturers used a standard graphical presentation which would enable purchasers to make a total assessment of the sensitivity, noise and
harmonic distortion capability of the tuner.
Sadly, the most important aspect of good f.m. reception is often overlooked at the design stage. This relates to the ability of the r.f. amplifier to avoid overload from high level adjacent channel signals when tuning to a comparatively weak signal. This is becoming increasingly important with the number of new f.m. local radio stations coming on the air. Evidence of the poor discrimination of the r.f. amplifier is exemplified by the presence of "birdies" when switched, particularly, to stereo broadcasts. To a certain extent this can be overcome with the use of a well placed, well designed aerial and again designers are encouraging this situation because a few quite highly priced tuners have no external aerial connectors and even more, have facilities for matching into only one impedance of feeder.

Quite recent issues of the magazines Electrical and Electronic Trader and Electrical and Radio Trading have contained details of some correspondence between the BBC and the aerial manufacturers' trade association on the subject of home-made aerials. The BBC have reprinted construction details for aerials in Information Sheet 1104, available from BBC Engineering Information, and for some reason the manufacturers took exception to this and complained vociferously. What is relevant is that the BS4054:1966 contains such information already and since manufacturers are among those represented on the committees of the BS, presumably they were party to agreeing the publication of such details. However, the fact remains that an external aerial, professional or home-made, can do much to improve the quality of reception in the face of considerably disparate signal strengths for adjacent channel stations. Useful publications from the BBC on f.m. stereo reception will be described elsewhere in a later issue of Wireless World.

Finally a point on reviews on f.m./a.m. tuners and receivers. Most of the hi-fi journals available in the U.K. publish reviews from time to time which describe the performance of a typical sample supplied by the manufacturer or distributor.


Fig. 4. A Receiver from ITT, the TA-1-200.


Fig. 5. A professional a.m./f.m. tuner made by Millbank.

In many instances, details of the test techniques are not published and so it still remains a difficult problem to crossrelate and compare results from magazine to magazine. In at least one of the divisions of audio, a BS proposal has been published which does lay out a standard format and test technique for the presentation of certain performance information. Perhaps it is about time that the whole field of consumer equipment is studied and some agreement obtained on presentation of data. This could well be initiated by a measure of cooperation between journals or even an acknowledgement by British Standard committees that journals have a vital place in the chain between consumer and
designer and go on to consider including standard data presentation formats suitable for use by reviewers.

With many new products appearing at the Audio Fair this year, the possibility of announced price changes and the need to incorporate information on products not described in this table, there will be a follow-up, including manufacturers' names and addresses, in the December issue.

| Maker and Model | $\begin{gathered} \text { Stereo (S) } \\ \text { or ( } \mathrm{O} \text { ) } \end{gathered}$ | FM/AM | Tuner ( T ) Tuner/Amp Receiver (R) | Aerial $Z(\Omega)$ | Tuner o/p into load $(\Omega)$ | Power Output ("r.m.s.") | $\begin{gathered} \text { F.M. } \\ \text { Distn(\%) } \end{gathered}$ | Sensitivity (IHF or DIN) | $\begin{gathered} \text { Price } \\ \left(\dot{+}+{ }^{+}\right. \\ \text {(AT) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ACOUSTIC RESEARCH |  |  |  |  |  |  |  |  |  |
| AR Tuner-amp | S | FM | R |  |  | 50W/8ת | 0.4 |  |  |
| AR Tuner | S | FM | T |  | - |  | 0.4 | $2.0 \mu \mathrm{~V}$ IHF | 110.00 |
| ADASTRA |  |  |  |  |  |  |  |  |  |
| A1005 (Chassis) | FM ${ }_{\text {F }}^{\text {F above but in wooden cabinet }}$ |  |  | 75 - |  |  |  |  |  |
| A1018 ${ }_{\text {A1007 }}$ (Chassis) |  |  |  |  |  |  |  |  |  |
| A1007 (Chassis) |  |  |  | 75 |  |  |  | Tor for 10dB |  |
| AKAI |  |  |  |  |  |  |  |  |  |
| AT550 | S | FM/AM | T | 75/300 | $1.8 \mathrm{~V} /$ ? | - |  |  |  |
| AT580 | S | FM/AM | T | 75/300 | $1.8 \mathrm{~V} /$ ? |  | <0.8 | $1.8 \mu \mathrm{~V} \mathrm{HF}$ | 91.62 143.30 |
| AA8030 | S | FM/AM | R | 75/300 |  | 25W/8ת | 0.8 |  | 140.48 |
| AA8080 | S | FM/AM | R | 75/300 | - | $40 \mathrm{~W} / 8 \Omega$ | 0.6 | $2.5 \mu \mathrm{VIFF}$ |  |
| ALBA |  |  |  |  |  |  |  |  |  |
| UA100D | S | FM/AM |  |  |  | $15 \mathrm{~W} / 8 \Omega$ |  |  |  |
| UA800 | S | FM/AM | T | 75 | $400 \mathrm{mV} / 2 \mathrm{k}$ |  | $<1.0$ | $2.0 \mu \vee \mathrm{Vor}$ | 37.84 |


| Maker and Model | $\begin{gathered} \text { Stereo (S) } \\ \text { or ( } \mathrm{O} \text { (uad } \end{gathered}$ | FM／AM | Tuner（ T ） <br> Tuner／Amp <br> Receiver（R） | Aerial $Z(\Omega)$ | Tuner o／p into load $(\Omega)$ | Power Output （＂r．m．s．＂） | $\begin{gathered} \text { F.M. } \\ \text { Distn }(\%) \end{gathered}$ | Sensitivity （IHF or DIN） | $\begin{aligned} & \text { Price } \\ & \text { VAT) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { ALPHA } \\ & \text { FR4000 } \\ & \text { FR3000 } \\ & \text { FR2000 } \\ & \text { R150 } \\ & \text { FT150 } \end{aligned}$ | $\begin{aligned} & \mathrm{S} \\ & \mathrm{~S} \\ & \mathrm{~S} \\ & \mathrm{~S} \\ & \mathrm{~S} \end{aligned}$ | $\mathrm{FM} / \mathrm{AM}$ $\mathrm{FM} / \mathrm{AM}$ $\mathrm{FM} / \mathrm{AM}$ $\mathrm{FM} / \mathrm{AM}$ $\mathrm{FM} / \mathrm{AM}$ FM | $\begin{aligned} & R \\ & R \\ & R \\ & R \\ & R \\ & T \\ & T \end{aligned}$ | 300 300 300 300 300 $300 / 75$ | $\begin{aligned} & \text { - } \\ & \overline{1 \mathrm{~V} / ?} \\ & \{500 \mathrm{mV} / 10 \mathrm{k}\} \end{aligned}$ | 20W／8 <br> $15 W / 8 \Omega$ <br> $10 \mathrm{~W} / 8 \Omega$ <br> $15 \mathrm{~W}^{*} / 8 \Omega$ $\qquad$ <br> － | － － － ＜ 0.4 | $2 \mu \mathrm{~V}$ IHF $3 \mu \mathrm{~V}$ IHF $2 \mu \mathrm{~V}$ IHF $3 \mu \mathrm{~V}$ IHF $2.5 \mu \mathrm{~V} \mathrm{HF}$ $1.8 \mu \mathrm{~V}$ IHF | 95．50＊ <br> $86.60^{*}$ $68.00^{*}$ $59.00^{\circ}$ 45．00＊ $49.50^{\circ}$ |
| Executive 007 | S | FM |  | 300／75 | $50 \mathrm{mV} / 10 \mathrm{k}\}$ | － | ＜0．4 | $1.8 \mu \mathrm{~V}$ IHF |  |
| $\begin{aligned} & \text { ARMSTRONG } \\ & 623 \\ & 624 \\ & 625 \\ & 626 \end{aligned}$ | $\begin{aligned} & S \\ & S \\ & S \\ & S \\ & S \end{aligned}$ | $\begin{aligned} & \text { FM/AM } \\ & \text { FM } \\ & \text { FM } \\ & \text { FM/AM } \end{aligned}$ | $\begin{aligned} & T \\ & T \\ & R \\ & R \end{aligned}$ | $\begin{aligned} & 300 / 75 \\ & 300 / 75 \\ & 300 / 75 \\ & 300 / 75 \end{aligned}$ | 二 | － <br> $40 \mathrm{~W} / 8 \Omega$ $40 \mathrm{~W} / 8 \Omega$ | $\begin{aligned} & <0.2 \\ & <0.2 \\ & <0.2 \\ & <0.2 \end{aligned}$ | $\begin{aligned} & 1.5 \mu V \mathrm{IHF} \\ & 1.5 \mu \mathrm{IHF} \\ & 1.5 \mu \mathrm{~V} \mathrm{HF} \\ & 1.5 \mu \mathrm{IHF} \end{aligned}$ | $\begin{array}{r} 79.20 \\ 59.40 \\ 110.00 \\ 132.00 \end{array}$ |
| ASTRONIC <br> B2477（Single Station） <br> B2478（Single Station） <br> B2479（4 Station tuner） <br> B2480（5 Station tuner） | As for B247 As for B247 | AM FM 8 tuner 8 but with | $T$ <br> one am station | $\overline{75}$ | $500 \mathrm{mV} / 5 \mathrm{k}$ | － | － | $\overline{10} \mu \mathrm{~V}$ IHF | $\begin{aligned} & 39.05^{*} \\ & 39.05^{\circ} \\ & 41.58^{\circ} \\ & 60.06^{\circ} \end{aligned}$ |
| AUDIO DECKS CT17 <br> CR50 |  |  | $\begin{aligned} & T \\ & R \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & 121.74 \\ & 167.67 \end{aligned}$ |
| BANG \＆OLUFSEN <br> Beomaster 901 <br> Beomaster 1001 <br> Beomaster 3000－2 <br> Beomaster 4000 <br> Beomaster 1700 | $\begin{aligned} & S \\ & S+\text { Synth } 0 \\ & S \\ & S+\text { Synth } 0 \\ & S \end{aligned}$ | FM／AM <br> FM <br> FM <br> FM <br> FM | $\begin{aligned} & R \\ & R \\ & R \\ & R \\ & R \\ & T \end{aligned}$ | $\begin{gathered} 240 / 75 \\ 300 / 75 \\ 75 \\ 75 \end{gathered}$ | － － $1 \mathrm{~V} /$ ？ | $\begin{aligned} & 20 \mathrm{~W} / 4 \Omega \\ & 15 \mathrm{~W} / 4 \Omega \\ & 30 \mathrm{~W} / 8 \Omega \\ & 55 \mathrm{~W} / 8 \Omega \end{aligned}$ | $\begin{aligned} & -0.9 \\ & <0.4 \\ & <0.5 \end{aligned}$ | $\begin{aligned} & 1.8 \mu \vee \mathrm{DIN} \\ & <3.5 \mu \mathrm{~V} \mathrm{HF} \\ & 2.0 \mu \mathrm{~V} \mathrm{HF} \\ & <1.4 \mu \mathrm{DIN} \\ & 2.0 \mu \mathrm{~V} \mathrm{HF} \end{aligned}$ | $\begin{array}{r} 100.90 \\ 96.90 \\ 164.50 \\ 193.50 \\ 60.90 \end{array}$ |
| $\begin{aligned} & \text { BUSH ARENA } \\ & \text { TA2700 } \\ & \text { TA2800 } \\ & \text { TA3500 } \end{aligned}$ | $\begin{aligned} & \mathrm{S} \\ & \mathrm{~S} \\ & \mathrm{~S} \end{aligned}$ | $\begin{aligned} & \text { FM } \\ & \text { FM/AM } \\ & \text { FM } \end{aligned}$ | $\begin{aligned} & R \\ & R \\ & R \end{aligned}$ | $\begin{aligned} & 75 \\ & 75 \\ & 75 \end{aligned}$ | 二 | $15 W / 3.2 \Omega$ $15 W / 3.2 \Omega$ $10 \mathrm{~W} / 4 \Omega$ | － | $1.5 \mu \mathrm{~V}$ DIN $1.5 \mu \mathrm{~V}$ DIN $3.0 \mu \mathrm{~V}$ DIN | $\begin{aligned} & 85.67 \\ & 89.43 \\ & 74.37 \end{aligned}$ |
| $\begin{aligned} & \text { DUAL } \\ & \text { CR50 } \\ & \text { CT17 } \end{aligned}$ | $\begin{aligned} & \mathrm{S} \\ & \mathrm{~S} \end{aligned}$ | FM／AM FM／AM | $\begin{aligned} & R \\ & T \end{aligned}$ | $\begin{aligned} & 240 \\ & 240 \end{aligned}$ | － | $18 \mathrm{~W} / 4 \Omega$ | ＜1．0 | $\begin{aligned} & 1.5 \mu V \text { DIN } \\ & 8 \mu V \text { DIN } \end{aligned}$ | $\begin{aligned} & 167.67 \\ & 121.74 \end{aligned}$ |
| FISHER 170 180 201 203 205 304 404 | $\begin{aligned} & S \\ & S \\ & S \\ & S \\ & S \\ & S+Q \\ & S+Q \end{aligned}$ | FM／AM <br> FM／AM <br> FM／AM <br> FM／AM <br> FM／AM <br> FM／AM <br> FM／AM | $R$ $R$ $R$ $R$ $R$ $R$ $R$ $R$ $R$ |  | － － － － | $\begin{aligned} & 16 \mathrm{~W} / 4 \Omega \\ & 21 \mathrm{~W} / 4 \Omega \\ & 20 \mathrm{~W} / 8 \Omega \\ & 25 \mathrm{~W} / 4 \Omega \\ & 35 \mathrm{~W} / 4 \Omega \\ & 15 \mathrm{~W} / 8 \Omega \\ & 22 \mathrm{~W} / 8 \Omega \end{aligned}$ | 0.8 0.8 0.8 0.8 0.8 0.3 0.3 | $2.5 \mu \mathrm{VIHF}$ <br> $2.5 \mu \mathrm{~V}$ IHF <br> $3.0 \mu \mathrm{~V} \mathrm{IHF}$ <br> $2.5 \mu \mathrm{VIHF}$ <br> $2.5 \mu \mathrm{~V}$ IHF <br> $1.8 \mu \mathrm{~V}$ IHF <br> $1.8 \mu \mathrm{VIHF}$ | $\begin{aligned} & 127.60 \\ & 169.40 \\ & 132.44 \\ & 216.70 \\ & 235.40 \\ & 286.00 \\ & 363.00 \end{aligned}$ |
| GOODMANS <br> One－ten <br> Module 80 <br> Module 90 | $\begin{aligned} & \mathrm{S} \\ & \mathrm{~S} \\ & \mathrm{~S} \end{aligned}$ | $\begin{aligned} & \text { FM/AM } \\ & \text { FM } \\ & \text { FM/AM } \end{aligned}$ | $\begin{aligned} & R \\ & R \\ & R \end{aligned}$ | $\begin{aligned} & 240 / 75 \\ & 300 \\ & 240 / 75 \end{aligned}$ | － | $40 \mathrm{~W} / 8 \Omega$ <br> $70 W / 4 \Omega$ <br> $30 W / 8 \Omega$ | $\begin{gathered} 0.2 \\ -0.5 \end{gathered}$ | $1 \mu \mathrm{~V}$ IHF $1.5 \mu V$ DIN $1.0 \mu \mathrm{VIHF}$ | $\begin{array}{r} 130.85 \\ 87.54 \\ 112.03 \end{array}$ |
| GRUNDIG RTV800 RTV900 | $\begin{aligned} & \mathrm{S} \\ & \mathrm{~S} \end{aligned}$ | FM／AM FM／AM | $\begin{aligned} & R \\ & R \end{aligned}$ | $\begin{aligned} & 240 / 65 \\ & 240 \end{aligned}$ | － | $\begin{aligned} & 12.5 \mathrm{~W} / 4 \Omega \\ & 25 \mathrm{~W} / 4 \Omega \end{aligned}$ | $\begin{aligned} & 0.7 \\ & 0.7 \end{aligned}$ | $1.1 \mu \mathrm{~V}$ DIN $1.8 \mu \vee \operatorname{DIN}$ | $\begin{aligned} & 150.40 \\ & 195.75 \end{aligned}$ |
| $\begin{aligned} & \text { HARMON KARDON } \\ & \text { Citation } 15 \text { (Dolby) } \\ & 50+ \\ & 75+ \\ & 100+ \\ & 150+ \\ & 330 A \\ & 630 \\ & 930 \end{aligned}$ | $\begin{aligned} & S \\ & S+Q \\ & S+Q \\ & S+Q \\ & S+Q \\ & S \\ & S \end{aligned}$ | FM <br> FM／AM <br> FM／AM <br> FM／AM <br> FM／AM <br> FM／AM <br> FM／AM | $\begin{aligned} & T \\ & R \\ & R \\ & R \\ & R \\ & R \\ & R \\ & R \\ & R \end{aligned}$ | $\begin{aligned} & 300 / 75 \\ & 300 \\ & 300 \\ & 300 \\ & 300 \\ & 300 / 75 \\ & 300 / 75 \end{aligned}$ | $\min 2 \mathrm{~V} / ?$ $=$ $=$ $=$ $=$ $=$ | $12 \mathrm{~W} / 8 \Omega$ <br> $18 \mathrm{~W} / 8 \Omega$ <br> $24 W / 8 \Omega$ <br> $30 \mathrm{~W} / 8 \Omega$ <br> 30W／8 <br> $45 W / 8 \Omega$ | 0.35 0.9 0.7 0.7 - 0.7 0.6 | $2.0 \mu \mathrm{~V}$ IHF <br> $2.8 \mu \vee \mathrm{IHF}$ <br> $2.0 \mu \mathrm{~V}$ IHF <br> $1.9 \mu \mathrm{VIHF}$ <br> $1.8 \mu \mathrm{~V}$ IHF <br> $1.9 \mu \mathrm{~V}$ IHF <br> $1.8 \mu \mathrm{VIHF}$ | $\begin{aligned} & 279.00^{*} \\ & 159.00^{*} \\ & 259.00^{\circ} \\ & 309.00^{*} \\ & 355.00^{*} \\ & 123.00^{*} \\ & 150.00^{*} \\ & 199.00^{*} \end{aligned}$ |
| $\begin{aligned} & \text { ITT } \\ & \text { TA-1-200 } \end{aligned}$ | S | FM／AM | 1 R |  | ． | $8 W / 4.5 \Omega$ |  |  | 79.50 |
| $\begin{aligned} & \text { JVC/NIVICO } \\ & \text { VR5505 } \\ & \text { VR5515(L) } \\ & \text { VR5525 } \end{aligned}$ | $\begin{aligned} & S \\ & S+Q \\ & S+Q \end{aligned}$ | $\begin{aligned} & \text { FM/AM } \\ & \text { FM/AM } \\ & \text { FM/AM } \end{aligned}$ | $\begin{array}{ll} \Lambda & R \\ \Lambda & R \\ \Lambda & R \end{array}$ | $\begin{array}{r} 300 \\ 300 \\ \hline \end{array}$ | － | $\begin{aligned} & 25 \mathrm{~W} / 8 \Omega \\ & 15 \mathrm{~W} / 8 \Omega \\ & 18 \mathrm{~W} / 8 \Omega \end{aligned}$ | $\begin{aligned} & 0.5 \\ & 0.8 \\ & 0.5 \end{aligned}$ | $\begin{aligned} & 2.2 \mu V \text { IHF } \\ & 2.2 \mu V \text { IHF } \\ & 2.2 \mu V \text { IHF } \end{aligned}$ | $\begin{array}{r} 95.50^{*} \\ 135.00^{\circ} \\ 169.50^{*} \end{array}$ |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Maker and Model \& Stereo（S） or Quad（Q） \& ） \(\mathrm{FM} / \mathrm{AM}\) \& \begin{tabular}{l}
Tune \\
Tuner \\
Receiv
\end{tabular} \& \[
\begin{array}{ll}
\text { ) } \& \text { Aerial } \\
\text { R) } \& Z(\Omega)
\end{array}
\] \& Tuner o／p into load （ \(\Omega\) ） \& Power Output （＂r．m．s．＂） \& \[
\text { , } \begin{gathered}
\text { F.M. } \\
\text { Distn(\%) }
\end{gathered}
\] \& Sensitivity （IHF or DIN） \& Price （＊ VAT） \\
\hline VR5535 \& \(\mathrm{S}+\mathrm{Q}\) \& FM／AM \& R \& － \& － \& \& \& \& \\
\hline 4VR1006 \& S＋Q \& FM／AM \& R \& 300 \& － \& \(40 \mathrm{~W} / 8 \Omega\) \& 0.8
0.4 \& \[
\begin{aligned}
\& 2.0 \mu \mathrm{~V} \text { IHF } \\
\& 2.2 \mathrm{uV} \mathrm{HFF}
\end{aligned}
\] \& \[
\begin{aligned}
\& 195.00 \text { * } \\
\& 20850
\end{aligned}
\] \\
\hline 4MM1000 \& \(\mathrm{S}+\mathrm{Q}\) \& FM／AM \& R \& 300 \& － \& \(40 \mathrm{~W} / 8 \Omega\) \& 0.4 \&  \& \[
208.50
\] \\
\hline 4VR5414 \& S＋O \& FM／AM \& R \& 300 \& － \& \(15 \mathrm{~W} / 8 \Omega\) \& 1.0 \& \(2.2 \mu \mathrm{~V} / \mathrm{HF}\)
\(2.0 \mu \mathrm{lHF}\) \& \[
\begin{aligned}
\& 146.50^{*} \\
\& 20850^{*}
\end{aligned}
\] \\
\hline 4VR5436 \& \(\mathrm{S}+\mathrm{Q}\) \& FM／AM \& R \& 300 \& － \& \(17 \mathrm{~W} / 8 \Omega\) \& 1.0 \& \(2.0 \mu \mathrm{~V}\) lHF
\(2.0 \mu \mathrm{lHF}\) \& \[
\begin{aligned}
\& 208.50 \\
\& 23500
\end{aligned}
\] \\
\hline 4VR5445 \& \(\mathrm{S}+\mathrm{O}\) \& FM／AM \& R \& 300 \& － \& 21W／8s \& 1.0 \& \(2.0 \mu \mathrm{~V}\) lHF
\(2.0 \mu \mathrm{VIHF}\) \& \[
\begin{aligned}
\& 235.00^{*} \\
\& 280.00
\end{aligned}
\] \\
\hline 4VR5446 \& S＋Q \& FM／AM \& R \& 300／75 \& － \& 22W／8』 \& 1.8
0.8 \& \(2.0 \mu \mathrm{~V}\) IHF
\(2.0 \mu \mathrm{VIHF}\) \& \[
\begin{aligned}
\& 280.00 \\
\& 280.00^{*}
\end{aligned}
\] \\
\hline \multicolumn{10}{|l|}{KLINGER} \\
\hline KC91 \& S \& FM \& T \& 300／75 \& 2．0V／10k \& － \& － \& \& \\
\hline KC96 \& S \& FM \& R \& 300／75 \& 2．0V／10k \& 25W／8® \& － \& \(8.0 \mu \mathrm{~V}\) DIN \& \[
\begin{aligned}
\& 41.40^{*} \\
\& 82.20^{*}
\end{aligned}
\] \\
\hline \multicolumn{10}{|l|}{KORTING} \\
\hline T510 \& S \& FM／AM \& T \& 240 \& \& \& \& \& \\
\hline T710 \& S \& FM／AM \& T \& 240 \& － \& － \& － \& － \& \begin{tabular}{l}
47.63 \\
80.05
\end{tabular} \\
\hline 310 T \& S \& FM／AM \& R \& 240 \& 二 \& \(5 \mathrm{~W} / 8 \Omega\) \& 二 \& 二 \& 80.05
66.19 \\
\hline 4107 \& S \& FM／AM \& R \& 240 \& 二 \& \(10 \mathrm{~W} / 8 \Omega\) \& － \& 二 \& 66.19
81.51 \\
\hline 800 L \& S \& FM／AM \& \(R\) \& 240 \& \& \(16 \mathrm{~W} / 8 \Omega\) \& \& \& 81.51
140.62 \\
\hline Syntector 1600L \& S＋Synth 0 \& FM／AM \& R \& 240 \& － \& \(40 \mathrm{~W} / 8 \Omega\) \& － \& 二 \& \[
\begin{aligned}
\& 140.62 \\
\& 191.21
\end{aligned}
\] \\
\hline \multicolumn{10}{|l|}{LEAK} \\
\hline Delta FM \& S \& FM \& T \& － \& － \& － \& \(<0.5\) \& \& \\
\hline Delta FM／AM \& S \& FM／AM \& T \& － \& — \& － \& \(<0.5\) \& \& \\
\hline Delta 75 \& S \& FM \& R \& － \& 二 \& \(35 \mathrm{~W} / 8 \Omega\) \& \[
\begin{aligned}
\& <0.5 \\
\& <0.5
\end{aligned}
\] \& \[
\begin{aligned}
\& 2.5 \mu \mathrm{~V} \text { IHF } \\
\& 2.5 \mu \mathrm{IHF}
\end{aligned}
\] \& \[
\begin{array}{r}
83.79 \\
163: 83
\end{array}
\] \\
\hline \multicolumn{10}{|l|}{LUX} \\
\hline R800 \& S \& FM／AM \& R \& － \& － \& \(40 \mathrm{~W} / 8 \Omega\) \& 0.4 \& \& \\
\hline FQ990 \& S \& FM／AM \& R \& 300／75 \& － \& \(70 \mathrm{~W} / 8 \Omega\) \& 0.5 \& \(2.0 \mu \mathrm{~V}\) IHF \& \(250.00^{*}\) \\
\hline 717 \& S \& FM／AM \& T \& 300／75 \& \(1 \mathrm{~V} /\) ？ \& \& 0.6 \& \(2.2 \mu \mathrm{~V}\) IHF \& 74．00＊ \\
\hline 700 \& S \& FM／AM \& T \& 300／75 \& \(750 \mathrm{mV} / ?\) \& － \& 0.6 \& \(2.2 \mu \mathrm{~V}\)
\(2.2 \mu \mathrm{VHF}\) \& 100．00＊＊ \\
\hline 500 \& S \& FM／AM \& T \& 300／75 \& \(450 \mathrm{mV} /\) ？ \& － \& 0.5 \& \(1.7 \mu \vee \mathrm{IHF}\) \& \(160.00^{*}\) \\
\hline \multicolumn{10}{|l|}{MARANTZ} \\
\hline 2010 \& S \& FM／AM \& R \& 300／75 \& － \& 10W／8， \& \(<1.0\) \& \& \\
\hline 2220 \& S \& FM／AM \& R \& 300／75 \& － \& 20W／8® \& ＜ 0.9 \& \(2.1 \mu \mathrm{~V} \mathrm{HHF}\) \& 169.50 ＊ \\
\hline 2245 \& S \& FM／AM \& R \& 300／75 \& \& \(30 \mathrm{~W} / 8 \Omega\) \& \(<0.5\) \& \(2.0 \mu \mathrm{~V}\) IHF \& \(215.00^{*}\) \\
\hline 2245 \& S \& FM／AM \& R \& 300／75 \& \& 45W／8』 \& \(<0.3\) \& \(1.7 \mu \mathrm{~V} \mathrm{IHF}\) \& 270.00 ＊ \\
\hline 105 \& S \& FM／AM \& R \& 300／75 \& － \& 70W／8® \& \(<0.3\) \& \(1.4 \mu \mathrm{VIHF}\) \& 330.00 ＊ \\
\hline 115 \& S \& FM／AM \& T \& \(300 / 75\)
\(300 / 75\)
\(300 / 75\) \& － \& － \& \(<1.0\) \& \(2.8 \mu \mathrm{VIHF}\) \& \(95.0{ }^{*}\) \\
\hline 120 \& S \& FM／AM \& T \& \(300 / 75\)
\(300 / 75\) \& － \& － \& ＜0．3 \& \(1.7 \mu \vee \mathrm{IHF}\) \& 145．00＊＊ \\
\hline 4415 \& \(\mathrm{S}+\mathrm{Q}\) \& FM／AM \& R \& 300／75 \& － \& \(\overline{60 W} / 8 \Omega\) \& \(<0.25\)
\(<1.0\) \& \(1.4 \mu \mathrm{VIHF}\)
\(2.8 \mu \mathrm{~V}\) IHF \& \[
\begin{aligned}
\& 260.00^{*} \\
\& 245.00^{*}
\end{aligned}
\] \\
\hline \multicolumn{10}{|l|}{MILLBANK} \\
\hline Met 100k \& S \& FM／AM \& T \& 300 \& \(100 \mathrm{mV} /\) ？ \& － \& \& \& \\
\hline Met 500 fixed station \& － \& FM \& T \& 75 \& \(250 \mathrm{mV} /\) ？ \& － \& 0.2 \& －\({ }^{\text {a }}\) \& 50．60 \\
\hline \multicolumn{10}{|l|}{NIKKO} \\
\hline STA5010 \& S \& FM／AM \& \(R\) \& \& － \& \& \& \& \\
\hline STA7070 \& S \& FM／AM \& R \& 300／75 \& － \& \(34 \mathrm{~W} / 8 \Omega\) \& 0.5 \& \& \\
\hline STA8080 \& S \& FM／AM \& R \& 300／75 \& － \& 45W／8の \& 0.5
0.5 \& \(2.0 \mu \mathrm{~V} \mathrm{IHF}\)
\(2.0 \mu \mathrm{HF}\) \& \[
\begin{aligned}
\& 143.00 \\
\& 158.40
\end{aligned}
\] \\
\hline \multicolumn{10}{|l|}{ONKYO} \\
\hline 234 \& S \& FM／AM \& R \& 300 \& \& \& \& \& \\
\hline 225 \& S \& FM／AM \& \(\stackrel{R}{R}\) \& 300 \& － \& \[
\begin{aligned}
\& 12 \mathrm{~W} / 8 \Omega \\
\& 22 \mathrm{~W} / 8 \Omega
\end{aligned}
\] \& \(<0.8\)
\(<0.8\) \& \[
\begin{aligned}
\& 2.5 \mu \vee \mathrm{IHF} \\
\& 2.5 \mu \mathrm{VHF}
\end{aligned}
\] \& \[
\begin{aligned}
\& 120.00 \\
\& 160.03^{*}
\end{aligned}
\] \\
\hline \multicolumn{10}{|l|}{PHILIPS} \\
\hline RH621 \& S \& FM／AM \& T \& 300／75 \& \(600 \mathrm{mV} / 10 \mathrm{k}\) \& －＜ \& ＜1．0 \& \& \\
\hline RH690 \& S \& FM／AM \& T \& 300／75 \& \(250 \mathrm{mV} / 10 \mathrm{k}\) \& － \& ＜4．0 \& \[
7.0 \mu \mathrm{~V}(300 \Omega) \mathrm{DIN}
\] \& 110.00
47.50 \\
\hline \[
\begin{aligned}
\& \text { RH720 } \\
\& \text { R } 4720
\end{aligned}
\] \& S \& FM／AM \& R \& 300 \& － \& \& ＜1．0 \& \(3.0 \mu \mathrm{~V}\)（300ת）DIN \& 215.00 \\
\hline \multirow[t]{2}{*}{RH901} \& S \& FM／AM \& R \& 300
300 \& － \& \(15 \mathrm{~W} / 4 \Omega\) \& ＜1．5 \& \(1.6 \mu \mathrm{~V}(300 \Omega) \mathrm{DIN}\) \& 215.00
90.38 \\
\hline \& S \& FM／AM \& R \& 300 \& － \& \(8 \mathrm{~W} / 4 \Omega\) \& － \& \(1.3 \mu \mathrm{~V}\)（300 ）DIN \& 87.00 \\
\hline \& \multicolumn{9}{|r|}{，3pV（300』）Din 81.00} \\
\hline \multicolumn{10}{|l|}{PIONEER} \\
\hline Qx9900 \& \(\mathrm{S}+\mathrm{O}\) \& FM／AM \& \& －－ \& － \& \& \& \& \\
\hline Qx8000A \& \(\mathrm{S}+\mathrm{Q}\) \& FM／AM \& R \& － \& － \& 22W／8® \& 0．5 \& \(1.8 \mu \mathrm{~V} / \mathrm{HF}\)
\(2.2 \mu \mathrm{~V} / \mathrm{HF}\) \& \[
\begin{aligned}
\& 430.24^{*} \\
\& 30839^{*}
\end{aligned}
\] \\
\hline Qx4000
S \(\times 2500\) \& \(S_{S}+0\) \& FM／AM \& R \& － \& － \& \(10 \mathrm{~W} / 8 \Omega\) \& 0.8 \& \(2.2 \mu \mathrm{~V}\) IHF
\(2.2 \mu \mathrm{HF}\) \& 308.39

216.82 <br>
\hline SX2500
S $\times 9000$ \& S \& FM／AM \& R \& －－ \& － \& $58 \mathrm{~W} / 8 \Omega$ \& 0.5 \& 1．6 $\mathrm{V}^{\text {V }} \mathrm{lHF}$ \& $337.47^{*}$ <br>
\hline SX6000 \& － \& － \& － \& － \& － \& － \& － \& － \& 303.26 ＊ <br>
\hline S×828 \& S \& FM／AM \& R \& \& \& 54W／80 \& 0.5 \& \& 221．44＊＊ <br>
\hline SX727 \& $\mathrm{S} \quad \mathrm{F}$ \& FM／AM \& R \& 二． \& － \& 54W／8ת \& 0.5 \& $1.7 \mu \vee 1 \mathrm{HF}$ \& 285．22＊＊ <br>
\hline SX626 \& $S$ F \& FM／AM \& R \& － \& － \& 37W／8® \& 0.5 \& $1.2 \mu \mathrm{VIHF}$ \& 222．39＊＊ <br>
\hline SX525 \& $S$ F \& FM／AM \& R \& － \& － \& 20W／8® \& 0.5 \& $1.3 \mu \vee 1 H F$ \& 184．74＊＊ <br>
\hline SX424 \& $S$ F \& FM／AM \& R \& － \& － \& 13W／8的 \& 0.8
$<10$ \& $1.5 \mu \vee \mathrm{IHF}$ \& $134.87^{*}$ <br>
\hline LX440A \& $S$ F \& FM／AM \& R \& － \& － \& $12 \mathrm{~W} / 8 \Omega<$ \& ＜1：0 \& $1.5 \mu \mathrm{~V}$ IHF \& 106．09＊ <br>
\hline TX6200 \& $S$ F \& FM／AM \& T \& 300／75 \& $0.775 \mathrm{~V} / 10 \mathrm{k}$ \& $14 W / 8 \Omega<$ \& $<1.0$ \& $2.5 \mu \mathrm{~V}$ IHF \& 127.00 <br>
\hline TX7100 \& $S$ F \& FM／AM \& T \& 300／75 \& \& －$<0$ \& $<0.4$ \& $1.9 \mu \mathrm{~V}$ IHF \& 87．17＊ <br>
\hline TX8100 \& $S$ F \& FM／AM \& T \& $300 / 75$ \& $0.775 \mathrm{~V} / 10 \mathrm{k}$
$0.775 \mathrm{~V} / 10 \mathrm{k}$ \& －＜ \& $<0.4$ \& $1.9 \mu \vee \mathrm{IHF}$ \& $117.20^{*}$ <br>
\hline TX9100 \& $S$ F \& FM／AM \& T \& 300／75 \& 0．775V／10k \& －＜ \& $<0.4$ \& $9.8 \mu \mathrm{VIHF}$ \& $137.64 *$ <br>
\hline TX500A \& $S$ F \& FM／AM \& T \& $300 / 75$ \& $0.775 \mathrm{~V} / 10 \mathrm{k}$
$0.775 \mathrm{~V} / 10 \mathrm{k}$ \& －＜ \& $<0.3$ \& $1.5 \mu \mathrm{VIHF}$ \& 185．99＊＊ <br>
\hline \& S \& FM／AM \& T \& 300／75 \& $0.775 \mathrm{~V} / 10 \mathrm{k}$ \& －＜ \& ＜0．8 \& $2.3 \mu \vee \mathrm{IHF}$ \& $76.03^{\circ}$ <br>
\hline
\end{tabular}




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$$
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& \text { Super-Track "Ples" V-15 TYPE III } \\
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\end{aligned}
$$

[^4]WW-088 FOR FURTHER DETALS

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# Circards - 11 <br> Basic Logic Gates 

When one and one isn't two

by J. Carruthers, J. H. Evans, J. Kinsler \& P. Williams*

Logical or arithmetic processes are extensively used in systems such as industrial control, computers, electronic instrumentation and automatic telephone exchanges. These processes often involve complex functions of several variables, the desired functions being realized by switching operations in a logical manner. Although much of the design of these systems now deals with the interconnection of complex functional blocks, successful results also depend on a knowledge of the basic elements that constitute the complex functional blocks.

The basic elements of such systems are logic gates, which may perform combinational operations on their inputs. These inputs will normally be in one of two allowed states that could be, for example, two different voltages, two different currents or two different resistance values such as the limiting cases of open circuit and short circuit. Whatever form the allowed states take, a logic gate is concerned with whether certain statements about its inputs, at a given instant, are true or false. If these statements are made using normal language they become unmanageable as the number of quantities involved increases, making some form of symbolic statement highly desirable.

If a certain statement is true it is assigned the value 1 and if it is false it is given the value 0 . For example, if one of the inputs to a logic gate is called A and it can be either at 5 V or 0 V then the statement "input A is at 5 V " may be true or false. If it is true than $\mathbf{A}=$ 1 and if it is false then $\mathrm{A}=0$. If this gate has three inputs and its output, $D$, is only at $5 \mathrm{~V}(\mathrm{D}=1)$ when two of its inputs, $\mathbf{A}$ and B , are at 5 V and its other input, C , is at 0 V , then $\mathrm{D}=1$ when $\mathrm{A}=1$ AND $\mathrm{B}=1$ AND $\mathrm{C}=0$.

Now $\mathrm{C}=0$ implies that C is NOT 1 i.e. $C=1$, where the bar indicates NOT or negation, so the above statement could be simply written as $\mathrm{D}=\mathrm{A}$ AND B AND C. Using the multiplication sign of normal algebra ( $X$ or .) to represent the AND operation this statement becomes $\mathrm{D}=\mathrm{A} \times \mathrm{B} \times \overline{\mathrm{C}}$, or $\mathrm{D}=\mathrm{A} \cdot \mathrm{B} \cdot \overline{\mathrm{C}}$, or even $D=A B \bar{C}$ where the "multiplication" (AND) signs are implied. This type of algebra, based on logical statements that

[^5]
## TABLE 1. Properties of Boolean algebra.

| 1 | $0+0$ | $=0$ | 11 | $\overrightarrow{\mathrm{A}} . \mathrm{A}$ | $=0$ | 21 | A. $(B+C)$ | $=A \cdot B+A \cdot C$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 0.0 | $=0$ | 12 | $\bar{A}+A$ | $=1$ | 22 | $A+A . B$ | $=\mathbf{A}$ |
| 3 | $1+1$ | $=1$ | 13 | $0+A$ | $=\mathrm{A}$ | 23 | $A+\bar{A} \cdot B$ | $=\mathrm{A}+\mathrm{B}$ |
| 4 | 1.1 | $=1$ | 14 | $0 . A$ | $=0$ | 24 | $A \cdot(A+B)$ | $=\mathbf{A}$ |
| 5 | 0.1 | $=0$ | 15 | $1+A$ | $=1$ | 25 | $(A+B) \cdot(A+C)$ | $=A+B \cdot C$ |
| 6 | $0+1$ | $=1$ | 16 | $1 . A$ | $=\mathrm{A}$ | 26 | $\bar{A}+\bar{B}$ | $=\bar{A} \cdot \bar{B}$ |
| 7 | 0 | $=1$ | 17 | $A+B$ | $=B+A$ | 27 | $\bar{A} \cdot \bar{B}$ | $=\overline{\mathbf{A}}+\overline{\mathrm{B}}$ |
| 8 | 1 | $=0$ | 18 | A. $B$ | $=B \cdot A$ | 28 | $\overline{\bar{A}}$ | $=\mathrm{A}$ |
| 9 | $A+A$ | $=\mathrm{A}$ | 19 | $(A+B)$ | $=A+(B+C)$ | 29 | $\overline{A+B}$ | $=\mathrm{A}$. |
| 10 | A.A | $=\mathrm{A}$ | 20 | (A.B) ${ }^{\text {c }}$ | $=A .(B C)$ | 30 | $\overline{\text { A.B }}$ | $=A+B$ |

are true or false, is called Boolean algebra and it is a very useful tool in the development of logical thinking and in the design of digital circuits and systems.

As well as the AND and NOT operations it is necessary to postulate the OR operation which is represented by the ( + ) symbol of normal algebra. For example, if a logic gate has two inputs $A$ and $B$, and its output $D$ is in the logic 1 state when either A or B is in the logic 1 state this statement can be written as $\mathbf{D}=\mathrm{A}$ OR $B$ which is represented by $D=A$ $+B$.

A logic gate is an example of a basic logical circuit, called a combinational circuit, the output of which at a given instant is determined by the state of its inputs. Irrespective of its complexity, certain relationships, laws and simplification rules of Boolean algebra can be used to represent or investigate the behaviour of a combinational circuit. Using up to three variables, Table 1 shows some of the properties of this algebra some of which are the same as ordinary algebra. In Boolean algebra division and subtraction have no meaning and the variables can only have the values 0 or 1. Table 2 shows the Boolean algebra theorems relating the values 0 and 1 in terms of relay contacts that are either open (logic 0) or closed (logic 1). Table 3 illustrates the Boolean algebra theorems in one variable $A$ in similar terms, where A can have either of the states 0 (Acontact open) or 1 (A-contact closed). In Table 1 relations 26 \& 27 together are known as De Morgan's theorem and 20 \& 30 are identical with 26 \& 27 except that the variables have been negated (or inverted or complemented).

Combinational logic circuits may take many different forms, one of which employs relay contacts which is useful for illustrating some of the simple Boolean

Table 2. Boolean theorems in terms of relay contacts.


Table 3. Boolean theorems in one variable.



Fig. I. $D=1$ when contacts $A$ AND $B$ $A N D C$ are closed, represented by $D=$ A.B.C.

TABLE 4. Truth table for Fig. 1

| $A$ | $B$ | $C$ | $D$ |
| :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 |
| 0 | 1 | 0 | 0 |
| 1 | 1 | 0 | 0 |
| 0 | 0 | 1 | 0 |
| 1 | 0 | 1 | 0 |
| 0 | 1 | 1 | 0 |
| 1 | 1 | 1 | 1 |



Fig. 2. $D=1$ when $A$ OR $B$ OR C are closed, represented by $D=A+B+C$.

TABLE 5. Truth table for Fig. 2

| $A$ | $B$ | $C$ | $D$ |
| :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 1 |
| 0 | 1 | 0 | 1 |
| 1 | 1 | 0 | 1 |
| 0 | 0 | 1 | 1 |
| 1 | 0 | 1 | 1 |
| 0 | 1 | 1 | 1 |
| 1 | 1 | 1 | 1 |

relations. For example, in Figs $1 \& 2, A$, $B$ and $C$ are contacts operated by relay coils (not shown) to complete a path between input and output. Thus, we are concerned with the statement "the connection between input and output is complete".

When this statement is true $\mathrm{D}=1$ and when it is false $D=0$. In Fig 1, $\mathbf{D}=1$ only when contacts A AND B AND C are closed simultaneously so the Boolean representation is $\mathrm{D}=\mathrm{A} . \mathrm{B} . \mathrm{C}$. Hence, series-connected contacts of the same type provide the AND operation. In Fig. 2, $D=1$ when contacts A OR B or $C$ are closed so the situation may be represented by $D=A+B+C$. If more than one contact is closed the above statement is still true, i.e. $\mathbf{D}=1$. Thus, parallel-connected contacts of the same type provide the OR (or "inclusive" OR) operation and the order in which they are wired or considered does not affect the truth of the statement.

The validity of a Boolean statement representing the behaviours of a combinational logic gate can be checked by means of a truth table. which is a tabular listing of all possible logic combinations of the variables and the resulting output logic, Tables $4 \& 5$ are the truth tables for Figs 1 \& 2 respectively and they show that a complete truth table requires $2 n$ rows to represent a gate having $n$ variables. Table 6 is a listing of the truth tables for the commonly-used combinational logic operations and shows the names given to the logic gates used to realize these operations. The NOR (NOT OR) gate performs the complement of the OR function and the NAND (NOT AND) gate the complement of the AND function.

GATE SYMBOLS



Fig. 3. Some of the symbols used for logic gates.


Fig. 4. Logic operations of $A N D$ (a), $O R$ (b), NOR (c) and exclusive $O R(d)$, can be realized using only NAND gates.

Unlike the OR gate, the "exclusive" OR gate only makes $\mathrm{D}=1$ when either A $=1$ OR $B=1$ but not when $A=B$ $=1$. The exclusive OR operation is used so frequently that it is given the symbol + . Thus, $\mathbf{D}=\mathbf{A B}+\overline{\mathrm{A} B}=\mathbf{A}+\mathbf{B}$.

Examples have been given of basic logical operations realized by means of relay contacts but this technique can become unwieldly. A more general diagrammatic representation of logic gates is desirable as the logic diagram should be independent of the circuit techniques employed in their realization. Unforturiately, there is no universally accepted symbol* to represent a particular logic gate, some of the different types of symbols that have been used being shown in Fig. 3.

While the operation indicated by a logic gate symbol is independent of the circuitry used, it should be realized that as there are two allowed states the user must decide which state is to represent the logical 1 condition. For example, if the two states are represented by voltage levels, one may be positive and the other 0 V , one may be negative and the other 0 V , one may be positive and the other negative, both may be positive or both negative. Irrespective of the values of these voltage levels, the system is said to use positive logic if the logical 1 state is represented by the more positive level and is said to use negative logic if the logical 1 state is represented by the more negative voltage level.

[^6]TABLE 6. Truth tables for common combinational logic operations.

| INPUTS |  | OUTPUT D = |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | B | A. B | $A+B$ | $A+B$ | A. B | $A+B$ |
| 0 | 0 | 0 | 0 | 1 | 1 | 0 |
| 1 | 0 | 0 | 1 | 0 | 1 | 1 |
| 0 | 1 | 0 | 1 | 0 | 1 | 1 |
| 1 | 1 | 1 | 1 | 0 | 0 | 0 |
| NAME OF GATE |  | AND | OR | NOR | NAND | $\begin{gathered} \text { EXCLUSIVE } \\ \text { OR } \end{gathered}$ |

Although all the combinational logic gates appearing in Table 6 are available in various forms of hardware, it is possible to build complete logic systems with either only NOR gates or only NAND gates. Fig. 4 shows how the AND, OR, NOR and exclusive-OR operations may be realized using only NAND gates and Fig. 5 shows the sole use of NOR gates to realize the AND, OR, NAND and exclusive-OR operations. These illustrations also show the application of some of the relations given in Table 1. Figs 4(a) \& 4(b) use relations 28 \& 30 respectively on the output function and relation 30 is also used on the output from the threeinput NAND gate in Fig. 4(c). In Fig. 4(d), relations $27,21 \& 11$ are used in turn on both inputs to the final gate and relation 30 used on its output function. Figs 5(a) \& 5(b) use relations 29 \& 28 respectively on the output function, relation 29 also being used on the output of the three-input NOR gate in Fig. 5(c). In Fig. 5 (d) relation 29 is used on the input to the final gate and relations $27,26,21 \&$ 11 used in turn on its output function.

These examples show that more gates of a given type are required to realize any other particular simple logic function. Although this point has been illustrated by simple Boolean expressions, in the design of more complicated systems the algebra may be cumbersome and other techniques such as Karnaugh mapping


Fig. 5. NOR gates can realize the logic operations of $A N D(a), O R(b), N A N D$ (c) and exclusive $O R$ (d).
would be used to obtain a minimal solution. To synthesize a complex system it may be advisable to use gates of one type because of their availability and cost.

Many different types of solid-state electronic logic-gate realizations are available such as resistor-transistor logic (r.t.l.), diode-transistor logic (d.t.l.), directcoupled transistor logic (d.c.t.l.), tran-sistor-transistor logic (t.t.l.), emittercoupled logic (e.c.l.) and complementary metal oxide transistor logic (c.m.o.s.) These families of gates have different characteristics and one family may prove to be more suitable than another in a particular application. For example, the prime consideration may be highest possible speed of operation or lowest power consumption or greatest immunity to external noise or the simplicity of interfacing the gates with other circuitry. The successful design of a digital system therefore requires a working knowledge of the capabilities of the various types of electronic gates available.

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Subsequent issues will cover wideband amplifiers, alarm circuits, digital counters, pulse modulators. Introductory articles in Wireless World indicate availability of Circards, which are normally ready for despatch on the 14th of the month, and the Circard concept was outlined in the October 1972 issue, pages 469/70.

## H.F. Predictions for November

LUF (lowest usable frequency) curves are for reception in the U.K. of point-to-point telegraphy services using medium power and directional aerials. LUFs for domestic reception of high power broadcasting stations would be about the same, while those for the amateur service would be a few megahertz higher particularly at noon.

Commercial working frequencies are kept below FOT (optimum traffic frequency) to allow for day-to-day ionospheric variations and seasonal trend over the month. Amateur "openings" can be expected on bands up to HPF (highest probable frequency).




## Circuit Ideas

## Deflection amplifier

The amplifier is designed for use with an electrostatically deflected tube, and combines the frequency-response of a cascode amplifier with the linearity of a constant current-fed long-tailed pair. Adjust the
value of $R$ to give 3 mA through each load resistor. The output transistors need small heat sinks.
G. A. Johnston,

Stechford,
Birmingham.


## Two-terminal current controller

This is an adaptation of Williams' well-known ring-of-two to produce an adjustable current regulator or limiter for use in test circuits or incorporation into power supplies. Its particularly low minimum voltage drop, around 1.4 V , is obtained by combining germanium alloy transistors and forward-biased silicon diodes.

The ring-of-two uses transistors $T r_{1}$ and $T r_{2}$ drawing a nearly constant current over a wide range of voltage. If only a small controllable current is required, this may be adjusted by varying either $R_{1}$ or $R_{2}$ or both. It is desirable to keep the ring-of-two transistors as cool as possible, and so $\operatorname{Tr}_{3}$ and $T r_{4}$ are added. The current in this pair is adjusted by means of $R_{3}$. Transistor $\operatorname{Tr}_{4}$ is heavier transistor and carries the

major part of the total current whereas $T r_{3}$, like $T r_{1}$ and $T r_{2}$, operates at low current for stability.
J. P. Holland,

London SW15.

## Simulating high-capacitance electrolytics

The first two circuits below are nearly equivalent, excepting that the drain of current is drastically reduced in the second. For small-scale applications, a BC107 with $h_{F E}$ of about 300 can be used, with up to 300 mW dissipation.

Either can be used to feed an a.f. preamplifier, or to partially stabilize a battery supply (e.g a car battery), but the second has very little drain on the battery. By having a capacitor of about $100 \mu \mathrm{~F}$ with a BC 107, an apparent capacitance of about $3000 \mu \mathrm{~F}$ is put across the output. The second circuit is cheaper and far less bulky than the first. I used this with certain audio equipment and it has completely eliminated the tendency of the preamp to "motor-boat".

The last two circuits are also almost exactly equivalent. Resistor $R_{1}$ is to cut down the leakage current of the circuit, and can be a very high value. The leakage current of the second circuit is now about $10 \mu \mathrm{~A}$, using a BC 107 and $100 \mu \mathrm{~F}$.

I found the second circuit useful in switch-on-protection of loudspeakers.

Other circuits, using higher rating transistors (e.g. 2 N 3055 ) or p-n-p transistors, can be used. Even bearing in mind that $h_{F E}$

for 2 N 3055 is only about 30 , a cost saving of about $40 \%$ can be obtained. R. M. Brady,

Urmston,
Manchester.

# 10-2 Metre Amateur Transverter 

# Design and construction of a unit which can be used with most 100W output 10 -metre transceivers 

by D. R. Bowman, G3LUB

The aim of this article is to describe the design and construction of a 10 to 2 metre transverter. This unit is compatible with the transceiver published in Wireless World ${ }^{1}$ and the two pieces of equipment combine to produce an elegant 2 metre s.s.b. transmitter/receiver. The transverter can be used with most 100W output transceivers which have the facility of operating on 10 metres. The unit can be used with all other transmission modes at a reduced power level.

## Methods of generating v.h.f. s.s.b.

There are two basic methods of generating a single-sideband suppressed-carrier signal within the 2 metre band ${ }^{2}$. The first method uses a high frequency phasing system at any frequency in the $5-25 \mathrm{MHz}$ region which is then heterodyned into the 2 metre band. This technique has gained support recently and when carefully built is capable of producing a high quality signal. The second method uses a transverter (heterodyne unit) in conjunction with a commercially built h.f. band s.s.b. transceiver. It is the availability of these transceivers rather than their ultimate performance on 2 metres which has been the reason for the popularity of the transverter technique.
The second method mentioned above has some serious drawbacks. The spectral clarity of the output of an h.f. transmitter rarely exceeds 50 dB . This means that
inband spurious signals no more than 50 dB below the peak output of the required signal are present. Many h.f. transceivers do not even achieve this figure and. whereas these spurious signals cause minimal interference on the h.f. bands $(80-20 \mathrm{~m})$, on 2 metres they can be objectionable. The reason is plain when one realizes that the dynamic range of received signals at v.h.f. can be 80 dB , whereas on the congested h.f. bands the range rarely exceeds 40 dB .

There is one small mitigating effect and that is the variable amplitude of many of these spurious signals. Many of them follow the speech waveform and therefore have extremely low average signal levels. This demonstrates the point that very great care is required when operating h.f. transmitters via transverters on the v.h.f. bands. One must not be scared off by the problem, but should design to minimize it.

The transverter is equally suited for use with any of the available commercial transceivers but the spectral purity of the v.h.f. signal will of course be mainly determined by the performance of the h.f. exciter. These inband unwanted signals are 50 dB down in the case of "The Cumbrian Transceiver" at least' and there are very few of them. This situation can be further improved by introducing a selective 28 MHz pretunable filter between the exciter and the transverter in Fig. 5. It was decided that these levels
were adequate, remembering that an aerial filter (high $Q$ break) can be expected to contribute a further 20 dB and the aerial at least 10 dB to the reduction of spurious out-of-band signals.

## Transverter in principle

The transceiver circuit can be divided into two basic units. These are the receiver's 2 to 10 metre converter and the transmitter's 10 metre to 2 metre transverter with its appropriate power amplifier. The receiver's converter consists of an r.f. amplifier feeding a mixer which requires a local oscillator with a frequency of 116 MHz . The transmitter transverter consists of a balanced mixer requiring a local oscillator of the same frequency followed by a multistage power amplifier. A considerable saving can be made by using one source of local oscillator voltage for both transmit and receive mixers.

Fig. 1 shows the complete block diagram of the "Westmorland Transverter". As signal flow is in opposite directions on transmit and receive isolation is increased between the 2 metre aerial socket and the 10 metre transceiver, keeping 10 metre i.f. breakthrough to a minimum. The only drawback to this system is that two possible paths for internal self oscillation may exist. If 2 metre noise should appear at the output of the power amplifier, under certain conditions this can be amplified and frequency changed to 10 metres where it will find its way into



Transverter's circuit layout - see construction section for details.
the input of the transmitter mixer, thus setting up an oscillatory path. Good relay isolation might be enough to eliminate this effect, but there is a further danger point via the common local oscillator feed line.

The simplest method of overcoming this problem is to switch the relevant receive and transmit stages in phase with the main transmit/receive operation of the exciting transceiver, but allowing the overtone oscillator to run continuously. This also eliminates the first feedback path and avoids any necessity to use high isolation transmit/receive relays. The block diagram shows the l.o. source simply as a 116 MHz crystal oscillator.

However carefully a low-frequencyderived multiplier chain is designed, large numbers of spurious frequencies will be present in the output. One method of overcoming this problem is to use an LC oscillator phase-locked to a low frequency crystal, but this is rather complex and a more simple if less elegant system is to use an overtone oscillator with an appropriate crystal.

No mention has so far been made concerning the reasons for using 10 metres rather than any of the other bands found on most transceivers. This is simply that the 2 metre band is 2 MHz wide as in the 10 metre range. Although there is


Fig. 2. Circuitry of the transverter's receiver and local oscillator sections. See table for explanation of voltage levels shown.

some advantage in using 14 MHz (from the spurious signal reduction point of view), image problems are considerably greater.

## Practical circuitry

## The Receiver section

The receiver section consists of two stages, namely a 2 metre r.f. amplifier followed by a mixer which converts the received 2 metre signal to 10 metres which is compatible with the associated transceiver. It was decided to use a common-baseconnected f.e.t. in the r.f. amplifier ( $\operatorname{Tr}_{1}$, Fig. 2). This circuit was chosen in view of its unconditional stability at all frequencies to at least 500 MHz . The maintenance of overall stability is usually the most difficult problem for the amateur constructor and for this reason a dual gate device was not used.
The noise performance is in the region of 2 dB and the gain is adequate to mask inevitable mixer noise. The r.f. circuitry situated between the aerial relay and the source connection of $T R_{1}$ has a low value of loaded $Q$ and the source coil tapping point should be adjusted for minimum noise. This adjustment is not critical and it may be easier to find the point of maximum signal strength, the difference in noise level being small.

The effective $G_{m}$ of the f.e.ts varies considerable within any device type and therefore the value of $R_{1}$ has to be found for each case. A multimeter should be connected across the resistor $R_{1}$ the value of which is adjusted until the calculated current flow is about 5 mA .
A source current $T r_{1}=$ meter voltage $\div R_{1}$.
No special r.f. overload protection has been included in the circuit. Over a long period of time using both a high power linear amplifier as well as the transistor power amplifier to be described, no incidents of r.f. transistor damage have
occurred. With frequencies as high as 150 MHz it is difficult to design protection circuits that do not produce some performance deprivation and as junction f.e.t. devices are inherently robust no such protection is considered necessary.

## Receiver mixer

The circuit of this mixer uses a dualgate m.o.s. f.e.t. ( $\operatorname{Tr}_{2}$ type 40673 or its equivalent). This is probably an appropriate point to warn any prospective constructor against the use of the earlier unprotected dual gate devices which were particularly prone to static generated gate electrode breakdown.
The 40673 f.e.t. is extremely well suited to use as a mixer as it couples very small local oscillator drive requirements with considerable isolation between the signal and l.o. paths. It also presents a high impedance to the r.f. amplifier

| Voltage table |  |  |
| :---: | :---: | :---: |
| Circuit Point | D.C. Voltage (Volts) | R.M.S. Voltage (Volts) |
| Across $R_{1} 220$ S | 5 mA (see text) |  |
| Tr ${ }_{2}$ Gate 2 | 0.8 |  |
| $\mathrm{Tr}_{2}$ Source | 0.6 |  |
| $T_{3}$ across $R_{19}$ (osc disabled). | 2 |  |
| $T r_{4}$ gate 2 | 4 |  |
| Tr $r_{5}$ gate 1 |  |  |
|  |  | measured |
|  |  | relative to |
|  |  | ground. |
| Tr $r_{6}$ gate 1 |  |  |
| r.f. in across $R_{5}$ |  | $5 \mathrm{r} . \mathrm{f}$ |
| $L_{7}$ secondary | 1.7 |  |
| $T_{7}$ base r r f. drive |  | $5 \mathrm{r} . \mathrm{f}$. |
| Tr $r_{7}$ emitter | 1 |  |
| Tr ${ }_{8}$ base | 2.4 | 1 r.f. |
| Tr $r_{8}$ emitter | 1.6 |  |
| Trg base | 7 approx | 2.5 r.f. |
| Output measured across a $50 \Omega$ dummy load |  | 16 r.f. | a $50 \Omega$ dummy load

16 r.f. All post mixer r.f. voltages are those measured when the transceiver is driven with an intermittent whistle i.e. the base of $\mathrm{Tr}_{\mathrm{r}}$ onwards.
output, helping to maintain the $Q$ of the r.f. tuned circuits. The transfer characteristics of these devices are substantially square-law, minimizing the generation of unwanted signals. The l.o. drive level is non-critical and any level between 0.2 to IV r.m.s. works well. As the measurement of 116 MHz r.f. voltages is rather difficult, no figure has been quoted.

## Local oscillator

To achieve the correct frequency conversions a source of extremely stable 116 MHz oscillations is required. Transistor $\mathrm{Tr}_{3}$ is connected in an overtone crystal oscillator circuit. Almost all crystals with frequency markings in excess of 20 MHz are intended for overtone operation, but this mode must not be mistaken for harmonic operation as it is quite different. A harmonic oscillator operated on the fundamental (lowest) resonant frequency of the crystal and a resonant circuit tuned to the required (higher) frequency is incorporated in the circuit. This selects the output frequency and at the same time attenuates to some extent the other harmonics which in this context can be considered to be spurious signals. Although these other harmonics are reduced in level they are still present and are liable to generate unwanted signals in the receiver's output.

The overtone oscillator relies upon the fact that all crystals have a number of harmonically related resonances. These occur at odd multiples of the crystal's fundamental frequency and the circuit is designed to excite the crystal in the range of the required overtone. In practice the highest multiple that is usable is the seventh or possibly ninth overtone.

The oscillator is followed by an isolation amplifier which is necessary as the mixer load appearing in parallel with the oscillator output varies considerably from the
transmit to receive mode. This amplifier ( $T_{4}$ ) uses a dual-gate f.e.t. which is extremely stable in operation partly as a result of the resistive input circuit.

## Transmitter mixer

The transmit mixer circuit consists of two cheap junction f.e.ts ( $T r_{5}$ and $T r_{6}$ ) 2N3819 connected in a balanced configuration. The local oscillator voltage is fed in pushpull to the two gate electrodes while the 28 MHz s.s.b. is parallel-connected to the source electrodes. This arrangement is used as the harmonics of the 10 metre s.s.b. are balanced and therefore attenuated. This helps to reduce the fifth harmonic of the input s.s.b. which tunes across the range $140-150 \mathrm{MHz}$. Variable resistor $R_{15}$ in association with $C_{25}$ and $C_{26}$ should be carefully adjusted to minimize this harmonic. The local oscillator harmonics are not reduced by the balancing procedure but as these signals are harmonically related to 116 MHz , they are well clear of the 2 metre band and therefore are easily eliminated by the various resonant circuits.

## Two-metre linear power amplifier

The output of the transmitter mixer is at a very low level and a linear amplifier is required to increase this level to about 5 W p.e.p. The 5 W level was determined mainly by the availability of v.h.f. power transistors. The R.C.A. overlay silicon transistors do not readily lend themselves to large signal v.h.f. linear amplification and for this reason the 2 N 3375 used is underrun. A cheaper alternative to the 2 N 3375 is the 2 N 3866 which has no mounting stud and therefore will require some heat sink arrangement. Possibly a simple pushfit heat sink over the transistor would be adequate if care is taken to limit the continuous drive tune-up periods.

The 2N3375 is forward biased and operates in what is really class B. The quiescent current is set to between 20 and 50 mA , by adjusting the resistance value of $R_{31}$.

The driver stage makes use of a 2 N 3866 which is forward biased only during the transmit period. This stage operates in class A and therefore its collector current should show no variations as a result of the speech waveform. The standing current of the driver stage is measured by reading the direct voltage appearing across the emitter resistor $R_{28}$ ( 33 ohms ) and should be set to between 50 and 80 mA by adjusting $R_{25}$. A small heat sink should be mounted on the transistor can to keep the collector temperature below $70^{\circ} \mathrm{C}$ :
$L_{9}$ and $C_{34}$ constitute a series trap which should be tuned to 116 MHz . This circuit helps to reduce l.o. feedthrough that is inevitable even after careful balancing of the mixer circuit comprising $\operatorname{Tr}_{5}$ and $\operatorname{Tr}_{6}$.
The first stage of the linear amplifier, $T r_{7}$, provides considerable gain, but its output is still at a low level. The BFY 90 common-emitter-connected class A amplifier is capable of delivering up to about 50 mW with a low level of distortion. This transistor type is notoriously unstable but as long as the circuit values are copied and the layout shown in the photograph duplicated exactly, no difficulties should be experienced. $C_{31}$ should be adjusted for maximum 2 meter drive to the p.a. as should $C_{40}$ and $C_{41}$.

## Aerial changeover relay

The aerial changeover relay is a standard RS Components type 21. This relay has a 12 V d.c. coil and four changeover contacts. One of these contacts is used to switch the aerial while another connects the redundant input/output line to earth. The normal practice of using a coaxial relay is not necessary as the relay is mounted so close to the output transistor tank circuit that the spring contacts in the relay become part of the tuned output matching circuit. As a result the power losses are minimal.


Fig. 4. Power supply circuit. See components list for transformer details.

The other pair of changeover contacts is used to switch the h.t. to the appropriate sections and switch the 10 metre input/ output line from the converter/receiver to the transmitter/transverter. The control of this transmit/receive relay is via a jack socket mounted on the transverter box. A short circuit across this jack socket energizes the relay and changes the transverter from receive to the transmit mode.

## Power supply

In the unit constructed by the author there was very little room left for the power supply. As a result the circuit is very simple and uses a heavily overrun transformer. This does have the advantage of increasing the reliability of the output power transistor as the h.t. voltage drops considerably when continuous high current is taken from the supply. The transformer has two 3 VA 20 V windings, one of which supplies the p.a. at +24 V and the other at +12 V .

The 12 V supply has no short-circuit protection but does incorporate a very simple series stabilizer. The 24 V supply has no stabilizer but uses a zener diode to clamp the voltage, thereby preventing a high voltage occurring at very low load currents. The use of separate secondaries helps to provide supply isolation which, in turn, makes the maintenance of stability easier. The peak current, as indicated by the p.a. meter, is about 250 mA . while the 12 V supply provides about 120 mA .

## Construction

The construction technique used for the Westmorland Transverter is slightly unusual. The complete circuit is built on to a $8.5 \times 5.25 \mathrm{in}$ piece of glass-fibre copper laminate board. The circuitry is almost completely mounted on the copper side. This board is in turn mounted within a $8.75 \times 5.5 \times 2.125$ in die-cast box with only the input, output, transmit / receive control socket and mains input terminations mounted on the rear wall. The front carries a miniature meter indicating p.a. collector current and a miniature mains on /off switch. The receiver converter and overtone oscillator are mounted on a separate, copper uppermost board within a small aluminium screening box. This precaution is probably unnecessary but occurred as the converter was separately built quite a time before the rest of the transverter.

Various other screens can be seen in the photograph and, with the exception of the roughly laid out power supply, the author would suggest that any prospective constructor use a similar layout. This arrangement is in the form of a loop which follows the block diagram closely, allowing minimum path lengths between stages and helping to maintain r.f stability. The only underboard wiring is the screened lead carrying the s.s.b. from the relay to the transmit balance mixer and the r.f. bypassed h.t. lines.
The balanced mixer is symmetrically built (very important as it helps the maintenance of r.f. balance).

One important note of warning is in order. The author succeeded in destroying a number of output transistors before he realized that an intermittent short circuit on $C_{41}$ was allowing 24 V to be directly connected to the base of $T r_{9}$. The inclusion of $C_{39}$ avoids this difficulty.

## Alignment

The alignment of the converter will be dealt with first and separately from the rest of the transverter.

It may be that a prospective constructor would like to build the converter first, allowing the 2 metre band to be monitored before the extra expense of the complete unit is contemplated. The converter circuit can be simplified by bypassing $T r_{4}$ if only the construction of a receiver converter is contemplated. The first point to align is the standing current of $T r_{1}$. This should be set to about 5 mA by adjusting the value of $R_{1}$ in the manner that has already been described. The next step is to feed a large signal having a frequency within the 2 metre band into the converter's aerial input socket. The converter's output should be fed to an appropriately tuned 10 metre receiver. The 116 MHz overtone oscillator crystal should be inserted into its socket and $C_{13}$ carefully adjusted until the 2 metre signal can be heard. This is the most exacting part of the alignment procedure.
It will be found that when the correct position for $C_{13}$ has been found the oscillator will be stable and is less prone to frequency pulling when either a hand or screwdriver is brought near to the $T r_{3}$ circuitry. Next $C_{3}$ and $C_{5}$ are adjusted for maximum signal delivered to the receiver which is tuned to the centre of the 10 metre band. The variable inductor $L_{3}$ is similarly peaked for maximum output. The method of adjusting the tap position on $L_{1}$ has been dealt with earlier in this description. If $\operatorname{Tr}_{4}$ has been included then again $C_{20}$ should be adjusted for maximum signal to the associated receiver. If the transmitter mixer is not connected to $L_{5}$ it is possible that this stage may be unstable. If this does occur $C_{20}$ should be detuned until the rest of the transverter is built. This concludes the alignment of the converter and now the completed transverter can be dealt with.

Before any attempt is made to run the transverter it is advisable to check all the direct voltages noted in the table. If any large discrepancies are noted these errors must be corrected by careful circuit checking before proceeding further.

The quiescent current of $T r_{8}$ must be adjusted to somewhere between 50 and 80 mA . ( 1.7 and 2.7 V as measured across $R_{28}$. This adjustment has also already been described and is achieved by trimming $R_{25}$. Variable resistor $R_{5}$ should be roughly adjusted to the centre of its travel and the 10 metre s.s.b. from the exciting transceiver should be fed via the appropriate socket to the balance mixer. The aerial output socket must be terminated in a $50 / 70 \Omega$ dummy load. One point to note is that to set the quiescent current of $T r_{8}$

## Components list

All resistors listed should be $\frac{1}{4}$ or $\frac{1}{8}$ watt composition or carbon types (not wire wound) with a $\pm 5 \%$ tolerance except where other specifications are noted.

All capacitors have their values shown in the following manner. . $1 \mu$ means $.1 \mu \mathrm{~F}, 100 \mathrm{p}$ stands for 100 pF and electrolytics are only used above $1 \mu \mathrm{~F}$. The types are designated FT stands for feed through, SM stands for silver mica, DC stands for disc ceramic or low stray inductance tubular ceramic, and "all voltage ratings must be at least 12 volts except where otherwise noted. Where electrolytics are specified the actual value is relatively unimportant and there is no reason why a prospective constructor should not substitute available types.

## Resistors

| esistors |  |  |  |
| :---: | :---: | :---: | :---: |
| 1 | 220 see text | 18 | 150 |
| 2 | 220k | 19 | 10k |
| 3 | 470k | 20 | 47 |
| 4 | 10k | 21 | 3.3k |
| 5 | 100 | 22 | 10 |
| 6 | 22k | 23 | 100 |
| 7 | 10k | 24 | 47 |
| 8 | 560 | 25 | 5k w.w.pot |
| 9 | 220 | 26 | 180 |
| 10 | 68k | 27 | 180 |
| 11 | 33k | 28 | two 68 in parallel (0.5W) |
| 12 | 100 | 29 | 680 |
| 13 | 100 | 30 | 51 |
| 14 | 2.2 k | 31 | 1.5 k |
| 15 | 500 trimmer | 32 | 0.25 see text |
| 16 | 100 | 33 | 2.2k |
| 17 | 75 | 34 | 50 or 75 |
|  |  |  | 25-50W carbon |
| Capacitors |  |  |  |
| 1 | 56 MC | 25 | 10p tubular trimmer |
| 2 | . 001 DC | 26 | 10p tubular trimmer |
| 3 | 5p tubular trimmer | 27 | 470 DC |
| 4 | 5p tubular trimmer | 28 | . 001 FT |
| 5 | 4.7p SM | 29 | . 001 FT |
| 6 | .1 DC | 30 | . 001 DC |
| 7 | .1 DC | 31 | 5p tubular trimmer |
| 8 | 18 SM | 32 | 10 SM |
| 9 | . 001 DC | 33 | . 001 FT |
| 10 | . 001 FT | 34 | 5p tubular trimmer |
| 11 | .1 DC | 35 | . 1 DC |
| 12 | 10 SM | 36 | . 001 FT |
| 13 | 5p tubular trimmer | 37 | .1 DC |
| 14 | 25 SM | 38 | . 001 DC |
| 15 | . 001 FT | 39 | 50 MC |
| 16 | .5p see text | 40 | 5 trim capacitor |
| 17 | . 001 DC | 41 | 25 trim capacitor |
| 18 | 470 DC | 42 | . 001 FT |
| 19 | . 5 p see text | 43 | .1 DC |
| 20 | $5 p$ tubular trimmer | 44 | 25 trim capacitor |
| 21 | . 001 FT | 45 | $1000 \mu / 50 \mathrm{~V}$ |
| 22 | 5 p trim | 46 | $600 \mu / 20 \mathrm{~V}$ |
| 23 | . 001 DC | 47 | 2000 $\mu / 50 \mathrm{~V}$ |
| 24 | . 001 DC | 52 | 100p air spaced trim |

## Diodes

[^7]
## Transistors

| 1 | TIS 88 | 6 | 2N3819 |
| :--- | :--- | ---: | :--- |
| 2 | 40673 | 7 | BFY90 |
| 3 | BFY90 | 8 | 2N3866 |
| 4 | 40673 | 9 | 2N3375 |
| 5 | 2N3819 | 10 | BFX29 |

## Meter

$\operatorname{lmA}$ f.s.d. or other meter shunted by $R_{18}$ to read 250 mA f.s.d.

## Additional

20 V miniature mains transformer (e.g. RS Components), output 20V 3VA each 2A fuse and holder.
Single pole changeover toggle switch
RS Components type 21 relay - see text

## Coil details

With the exception of those stated cases all coils are wound on a .25 in mandrel and mounted in a self-supporting manner.
19 turns 22 s.w.g. bare copper wire with a winding length of .5 in tapped at three turns and five turns from the ground end.
28 turns 22 s.w.g. bare copper wire with a winding length of .45 in .
310 metre i.f. transformer 22 turns 28 s.w.g. close wound on a .45 in former and tuned with an iron dust core. The secondary consists of four turns wound over $L_{3}$.
47 turns 22 s.w.g. bare copper wire with a winding tength of .45 in .
57 turns of 22 s.w.g. bare copper wire with a winding length of .4 in . Also two turns of 22 s.w.g. enamel covered copper wire are pushed into the centre of $L_{s}$ for maximum coupling co-efficient. This two turn coil is coupled using twisted insulated leads to two turns similarly pushed into $L_{6}$.
68 turns of 22 s.w.g. bare copper wire with a winding length of .5 in and provided with a centre tap.
77 turns of 22 s.w.g. bare copper wire with a winding length of .5 in similarly with a centre tap. Also two turns of 28 s.w.g. enamel covered copper wire are coupled by pushing into the centre of $L_{7}$. The two turns are connected to $T r_{7}$ via a pair of insulated twisted leads.
84 turns of 22 s.w.g. bare copper wire with a winding length of 45 in .
98 turns of 22 s.w.g. bare copper wire with a winding length of .45 m .
105 turns of 18 s.w.g. bare copper wire with a winding length of 4 in .
114 turns of 18 s.w.g. bare copper wire with a winding length of .3 in .
125 turns of 16 s.w.g. bare copper wire with a winding length of .45 in , together with a centre tap.
All r.f. chokes are constructed using .25 wavelength (at 2 metres) 34 s.w.g. enamel-covered wire, wound on home made p.t.f.e. formers. i.e. 18 in of 34 s.w.g. enamel covered wire wound on these formers.

## $\mathbf{2 8 M H z}$ filter (Fig. 6)

$L_{1} \quad 8$ turns 20 s.w.g. enamel self supporting $\frac{1}{1}$ in dia $\frac{1}{7}$ in long. $L_{2} 8$ turns as $L_{1}$. The taps on both $L_{1}$ and $L_{2}$ should be at one turn from the earthed end of the coil. The coupling link is one turn of $20 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. enamel placed in each of $L_{1}$ and $L_{2}$.
$C_{1}, C_{2} \quad 10-50 \mathrm{pF}$ variable.
$C_{3} C_{4} \quad 47 \mathrm{pF}$ silver mica.
it is advisable to disable the overtone oscillator. The reason for this is that a small amount of 116 MHz energy may leak through the balanced mixer and thus inflate the standing current of $\operatorname{Tr}_{8}$. Having set the quiescent current, the oscillator should now be enabled and the current of $T r_{8}$ will almost certainly increase. Careful adjustment of $C_{34}$ should allow this 116 MHz leakage to be considerably reduced. The next step is to supply a 10 metre drive signal of a few volts to the transverter. If the exciting transceiver is a "Cumbrian" this drive will be obtained by switching on the audio tone and adjusting the drive level accordingly.

If a secondary two metre receiver happens to be available it should be tuned to receive the 2 metre output of the transverter, and $C_{31}, C_{40}, C_{41}$ and $C_{44}$ should be adjusted for the maximum indicated 2 metre signal. The receiver-to-transverter coupling must be progressively reduced in order that the increasing output power does not overload the auxiliary receiver. Finally $C_{26}$ in conjunction with $C_{25}$ can be adjusted for minimum 116 MHz output while at the same time maximizing the 2 metre signal. This process requires an amount of care but will fully justify the constructor's efforts in providing a 2 metre s.s.b. signal free from spurious signals.

There is an alternative alignment procedure for the constructor who does not have a secondary 2 metre receiver. As the trim capacitors are adjusted, three and only three signal peaks will be found. One at $116 \mathrm{MHz}-28 \mathrm{MHz}$, i.e. 88 MHz , a second at 116 MHz , and the required peak at $116 \mathrm{MHz}+28 \mathrm{MHz}$, i.e. 144 MHz . It is a simple matter to identify them. With no 10 metre drive, only the 116 MHz peak will be present and as already explained $C_{34}$ should null this. With 10 metre drive the correct 144 MHz signal is received with minimum capacitance in circuit. As $C_{31}$, $C_{40}, C_{41}$ and $C_{44}$ are adjusted, the peak coincident with minimum capacitance should be chosen. The balance of the $\operatorname{Tr}_{5}$ and $T r_{6}$ circuit can be adjusted in a similar manner to that described in the previous procedure remembering that the minimumcapacitance peak must be enhanced while reducing the 116 MHz by carefully balancing $C_{25}$ and $C_{26}$. As the signal increases and the alignment proceeds the 10 metre drive must be reduced so as not to overheat either $\operatorname{Tr}_{8}$ or $T r_{g}$.

## Performance

There now follows a brief outline of the performance as measured on the author's transverter. The receiver converter exhibits a noise figure of about 2 dB and a signal gain of 30 dB . This noise performance will of course be degraded if the following receiver is either noisy or has a low sensitivity.

To improve the blocking performance, it would be necessary to change to a single conversion system where the i.f. filter is situated as close to the input of the receiver as possible. It would be an improvement to include a switchable attenuator between


Fig. 5. Signal purity of the transverter.


Fig. 6. High Q 28 MHz filter whose use depends on the exciting transceiver used (see text).


Fig. 7. Dummy load attenuator circuit. Internal layout of the transverter circuitry.
the aerial changeover relay and the r.f. amplifier.

The frequency drift is low - less than 2 kHz per hour including initial switch-on drift. There are few spurious responses and those that occur are weak - an advantage of using a single frequency overtone oscillator.

Examination of Fig. 7 shows that the aim of keeping all spurious outputs from the transmitter to at least 50 dB below the required output has been achieved. These spurious signals will be further reduced if the frequency sensitivity of the aerial is combined with a series high $Q$ filter. This should drop the 116 MHz to at least 80 dB below the output. If the exciting transceiver is of a type other than the Cumbrian then it is advisable to include a high $Q$ filter circuit between the transceiver and transverter (Fig. 6).

Almost any transceiver with a 10 metre output in excess of about .5 W will drive the transverter. If the transceiver used does not have an r.f. drive control then it will be necessary to attenuate the 10 metre drive using the dummy load circuit shown in Fig. 7. This can be adjusted to provide almost any level of drive out and should comfortably accept 200 W p.e.p. intermittent speech. To prevent the load becoming overheated, the period of tuning should be as short as possible.

The output power, in excess of 5 W p.e.p., is difficult to measure as the power supply regulation will not support a continuous tone. Using a Heathkit V-7AU valve voltmeter and its associated r.f. probe at least 16 V on speech peaks can be measured across a $50 \Omega$ dummy load.
power out (p.e.p.) $=\frac{V^{2}}{R}=\frac{16^{2}}{50}=5.1 \mathrm{~W}$.
$R$ measured in ohms, $V$ in r.f. r.m.s. voltage.

## References

1. Bowman, D. R., " $10-80$ Metre Amateur Transceiver", Wireless World, June-September 1972 (four parts).
2. "Fundamentals of S.S.B.", Collins Radio Co., 2nd ed., p 1-1

## Sixty Years Ago

The throwaway perceptiveness of remarks made by some of the early experimenters gives one furiously to think on the obstacles which these pioneers faced. The progress that was made in days when it was an imaginative stroke to achieve the smallest step forward was remarkable. Dr. W. Eccles, discussing atmospherics or "Xs" in our November, 1913 issue, wrote . . . . 'It is natural, but it is not scientific, to jump to the conclusion that these strays are all due to lightning strokes occurring probably at great distances somewhere on the earth's surface, or possibly in the free atmosphere between one bank of ionised air and another. This, however, ignores the possibility that the source of the strays may be far outside the earth. There is nothing unreasonable in supposing that the sun, let us say, may send us occasional electric waves. For example, in the colossal movements of matter associated with the formation of a solar prominence - movements that appear to take place with enormous velocities electric discharges may be brought about of magnitude far transcending anything that can happen on the earth. These would give rise to electric waves which might reach the earth in perceptible intensity and constitute a proportion of our strays. On the other hand, we must not forget that we on the earth's surface may be protected by our ionised atmosphere from these extra-terrestrial waves: It is just such problems as these that the British Association Committee has set itself to inquire into.

The BSR McDonald 810 costs around $£ 40$ (excluding cartridge). But you may be tempted to spend $£ 20$ more on a transcription turntable that doesn't do any more for you. In fact, the 810 offers you more sophisticated features than most other turntables at this price.
Its pre-programmed sequential cam system outdates conventional cam gear and swinging plate mechanisms to bring you a new experience in smoothness, quietness and featherlight operation The professional low mass transcription tonearm floats in a concentric gimbal arm mount, reducing tracking pressures to a minimum, and has a precise zerc balance adjustment over the full range of cartridge and stylus masses.
The $6^{3 / 2}$ lb turntable is driven by a high torque synchronous dynamically balanced 4-pole motor. The wide selection of operating modes are all featherweight push-button controlled.
Other technical innovations include an automatic tonearm lock to eliminate accidental
damage to the stylus or record, a variable pitch control, rotating stub spindle, dualrange bias compensator, stylus position gauge, stylus cleaning brush, micro-gear stylus pressure control, slide-in cartridge carrier and viscous-damped cue and pause with exclusive friction clutch to keep the tonearm cued over the exact groove.
The ADC K3E (elliptical) magnetic cartridge is recommended as an optional extra.
We'll explain all the finer details when you send for our free illustrated brochure.


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# A novel configuration which utilizes an i.c. transistor array and is capable of a linearity better than $1 \%$ per MHz 

by J. L. Linsley Hood

The growing use of phase locked loop systems in applications such as very high quality f.m. demodulators, in which a high degree of lineariţy between input frequency and output (control) voltage is sought, has focused attention on the characteristics of the available voltage controlled oscillators (v.c.os) - the linearity of the phase locked loop is mainly determined by, and cannot be better than, that of the v.c.o. contained within it. However, although the availability of a very linear v.c.o. system would allow improvements to be made in phase locked loops built around it, the usefulness of a circuit arrangement having a linear voltage/frequency characteristic extends beyond this to such applications as r.f. telemetry, "wobbulators", f.m. broadcast transmissions, and linear f.m. signal generators.

It is convenient in practice if the v.c.o. can be constructed using some form of multivibrator circuit in that this avoids the need for inductors, and, with a regard to the potential use of such a v.c.o. in an f.m. tuner demodulator system with an i.f. of 10.7 MHz , it is desirable that the controlled frequency range of the circuit should extend some way above this. In view of the small lead inductances and stray capacitances which are demanded for satisfactory operation of any multivibrator circuit at these frequencies, it is helpful if the device can be constructed using some readily available high frequency linear integrated circuit, and the component arrangement has been chosen with this object in mind.

## Circuit development

A number of multivibrator arrangements can be adapted to operate in a voltage controlled mode, but for optimum performance in high frequency applications, the non-saturating emitter-coupled systems are preferable. A suitable configuration for a free running square-wave generator is shown in Fig. 1.

In this the operation of the circuit is to switch the current available from the constant current source backwards and forwards between $T_{x}$ and $T r_{y}$. Resistor $R_{1}$ is the collector load of $\mathrm{Tr}_{2}$. When this transistor is conducting, the voltage drop across $R_{1}$ will always be constant and


Fig. 1. Multivibrator configuration for a free running square-wave generator.


Fig. 2. Square-wave oscillator with a high long term stability. Operation is up to at least 20 MHz .


Fig. 3. "Current mimic" circuit which can be used to substitute the timing resistor, $\mathbf{R}_{2}$, in Fig. 2.
independent of the h.t. voltage supply, provided that this does not alter the output of the constant current source. This arrangement offers a high degree of intrinsic frequency stability and if $C_{T}$ or $R_{2}$ is made variable, the "base" frequency can be altered.

A practical system is shown in Fig. 2, using a Motorola MFC6010 i.f. integrated circuit amplifier, which incorporates a long tailed pair, a constant current source and a reference voltage point. With a stabilised h.t. supply, this circuit gives a high long term frequency stability, and will operate to at least 20 MHz .

This circuit arrangement can be converted into a linear and stable voltage controlled oscillator by the substitution of a "current mimic" or "current mirror" circuit for the timing resistor $R_{2}$ in Fig. 2.

## Current mimic operation

The circuit configuration shown in Fig. 3 is widely used in integrated circuit manufacture, as for example in the Motorola MC3401P to provide a noninverting input on a Liniac type amplifier, or in the RCA CA3060/3080 micropower op-amps, to replace load resistors. Its attractiveness to the monolithic integrated circuit manufacturer arises from the ease with which identical pairs of transistors can be fabricated in this process.

If a given forward bias voltage is applied to the bases of an ideal identical pair of transistors, the same current will flow in the collector circuits of both. If, now, the bases of both of these transistors are joined to the collector of one of these ( $\operatorname{Tr}_{a}$ ), and a certain current is drawn from this, this current will be the collector current of $T r_{a}$ plus the two base currents. Since the forward base potential of $T r_{a}$ has adjusted itself to the level required to produce the collector current of $T r_{a}$, it will also have adjusted the base potential of $\operatorname{Tr}_{b}$ to produce the same collector current in $T r_{b}$.
This will imply that the output ("mirror") current of $T r_{b}$ will be the same as the current drawn from the input, less the two base current contributions. If the current gains of the transistors used are high enough, or if - as will be the case in integrated circuit manufacture - the
areas of the transistor junctions are trimmed to suit, the two currents (the input current and the mirror current) will be very nearly identical, and this identity will hold good over a wide current and temperature range. Although this is an integrated arrangement, discrete transistors can be used if their characteristics are reasonably closely matched.

In several circuits of the type shown in Fig. 4, the transistors used in the mimic circuit were BC184s in which the baseemitter forward voltage drop was matched by selection to about 10 mV at $50 \mu \mathrm{~A}$ forward current (i.e., say 0.58 V to 0.59 V ).

This is inconvenient, but not difficult if one has a voltmeter and six or eight similar transistors to choose from. Although BCl 84 s were used, any other similar small signal silicon devices would serve just as well.

The performance of the circuit shown in Fig. 4 is given in Fig. 5. The relationship between the control voltage and the frequency had a linearity better than $1 \%$ per MHz , and the frequency stability was as good as that of the author's signal generator during a six hour measurement period.

In view of this encouraging performance,
a means was sought for avoiding the inconvenience of having to select a matched pair of "current mimic" transistors, without the expense involved in the use of a matched-pair device. The solution was found in the use of an i.c. transistor array of the type contained in the RCA CA3046, of which the internal circuitry is shown in Fig. 6. In this particular case the array contains all the active components needed to make the v.c.o. circuit, including a matched pair of transistors. The circuit arrangement is in Fig. 7, for which the necessary interconnections across the base of the CA3046 are shown in Fig. 8.


Fig. 4. Circuit of the v.c.o. using discrete transistors for the current mimic circuitry.


Fig. 5. Performance of the circuit shown in Fig. 4.


Fig. 6. Layout of transistors and pin connections for the i.c. transistor array contained in the RCA CA3046.


Fig. 8. Connections to the CA3046 which complete the circuit shown in Fig. 7. The view is from below.


Fig. 9. Control characteristic of the v.c.o. in Fig. 7.


The performance of this circuit for a timing capacitor of 5 pF , and with the other values as indicated, is shown in Fig. 9. The linearity of this arrangement is as good as that of the circuit in Fig. 4, but the long term stability of the Fig. 4 circuit is slightly better. Several CA3046 units were tried and gave identical free running operating frequencies.

## Typical applications

A simple phase locked loop configuration built around this v.c.o. and suitable for use as a high quality f.m. demodulator, using an f.e.t. as a synchronous chopper type phase sensitive detector, is shown in Fig. 10. An amplitude limited input r.f. signal, of nominal 10.7 MHz frequency, and of about 500 mV amplitude is desirable for correct operation of the system. The output a.f. signal will be about 20 mV for 75 kHz deviation, with a second harmonic distortion content of about $0.07 \%$.

An arrangement usable as a low distortion frequency modulated signal generator if a suitable low distortion sinewave modulation signal is applied, or as a "wobbulator" if a sawtooth input signal is provided, is shown in Fig. 11. Increasing the capacitance of the timing capacitor will provide a proportional reduction in operating frequency, allowing the system to be used, if required, down to audio frequencies, as a voltage controlled oscillator in electronic organ and similar applications.

As a final provocative thought, since it is possible to build voltage controlled oscillators (and phase locked loop demodulator systems containing these) whose linearity, over the 75 kHz bandwidth normally used for f.m. transmissions, is better than $0.1 \%$, by some margin, is not the ball now in the court of the broadcasting authorities to take note of this, and improve their f.m. transmission quality?


Fig. 10. Phase locked loop configuration built around the v.c.o., suitable for use as an f.m. demodulator. The f.e.t. is used as a synchronous chopper type phase sensitive detector.


Fig. 11. Using the v.c.o. in an arrangement for a low distortion f.m. signal generator, or as a "wobbulator".

## Books Received

Noise and Modulation are two books by F. R. Connor and are respectively the fifth and sixth in a series of books on introductory topics in electronics and telecommunications. They are texts designed to assist students preparing for university degree examinations or for courses at a similar level. "Noise" presents a survey of the various conditions of electrical noise followed by mathematical ideas con cerning random variables. Circuit noise, noise factor and noise temperature are then considered. Finally, there is a comparative study of some important communication systems. "Modulation" provides a broad outline of the most important methods used in practice. Analogue methods such as amplitude and
frequency modulations are first considered and this is followed by phase modulation and the various types of pulse modulation. There is a final chapter on demodulation at the receiver. The material in both books is related to modern practice and a number of worked examples are included. Both hooks cost $£ 1.10$, and have approximately 100 pages each. Edward Arnold Ltd, 25 Hill Street, London W IX 8LL.

The Directory of Instruments, Electronics \& Automation 1973 (ninth edition) contains collated information on manufacturers. trade names, equipment and components in the electroniss industry. Sections come under the headings diary of events, association addresses.
who buys, U.K. agents, trade names, manufacturers' addresses and a buyers' guide. Price £7. Pp.328. Morgan-Grampian (Publishers) Ltd., 30 Calderwood Street, London SE18 6QH.

Recent additions to the Foulsham-Tab books on electronic topics and published by W . Foulsham \& Co. Ltd., Yeovil Road. Slough, Bucks, are:

How to Solve Solid State Circuit Troubles by Wayne Lemons, Price $£ 1.75$. Pp. 304.
How to Build Solid State Audio Circuits by Mannie Horowitz. Price £1.75. Pp. 320.
How to test almost everything electronic by Jack Darr. Price £1.30. Pp. 160.

# Which Way Does Current Flow? 

## Some thoughts arising from recent correspondence

by "Cathode Ray"

I would probably be flattering myself excessively if I imagined for one moment that, when Messrs Banthorpe, Ellis and Whitehead ${ }^{1}$ appealed for the direction of an electric current to be deemed to be the same as that of the electrons composing said current, it entered the heads of any of them to think "Well, anyway, old Cathode Ray will back us up". If, however, the question of what I would be expected to think about it had been put to them, as a minor matter of academic interest, they might confidently have claimed me as a potential ally, since in so far as I am well known at all I am well known as one who decides on circuit conventions by processes of logic and common sense rather than by what is generally accepted. They might have quoted as evidence my strong support for the heretical doctrines of M. G. Scroggie on phasor diagrams and their mass of related conventions. Beside this complex thesis, the case for abolishing the conventional direction of current flow in favour of the direction of electron flow (they would say in chorus) is simplicity itself as well as being exquisitely logical and commonsensical. So Cathode Ray could not but stand shoulder to shoulder with them.

## Flows, fields and tracks

It is true that their case was severally put forward in terms that nearly brought tears to my eyes. I'm sure they meant well. And I hope they won't take it too hard when they find that their idol (self-flattery again!) has feet of clay (Daniel 2, 41-43). But it is a fact that I find myself having more in common with what Thos. Roddam divertingly proclaimed from the next bed to mine in the Geriatric Technologists' Home, as well as with the plain Yorkshire words of A. Parnham, also recorded on the p. 386 already cited. I hope this revelation of my reactionariness will not cause a mass defection from the ranks of my followers (if any) - at least, not until they have read right through to the end, which is not far distant.

Roddam argues against reversing the usual convention (i.e., "current" opposite to electron flow) on the grounds that (a) to do so would cause a great upset (at which he hints by pointing out that among other things it would make nonsense of all diode and transistor symbols), and (b) (although
one suspects that he personally might find such an upset quite amusing) there is really no need for it if only we stopped bothering our heads unnecessarily with charge carriers, which can safely be left to the electronic device makers, and dealt simply in fields and "current tracks".

But you may not be ripe for accepting such a revolutionary plan (and I wouldn't blame you). In that case you must meditate on the fact that not all electric charge carriers are electrons. In this respect electricity differs fundamentally from air and water, held up by Banthorpe as examples for it to copy. And although Ellis may not be able to satisfy his commendably inquisitive students on why there are two kinds of current (unless he has a hot line to the Creator) he cannot deny the fact. A great many carriers are holes and positive ions. So the choice of which to regard as positive for the purpose of specifyjng direction of current flow is arbitrary anyway. Even if we yielded to the entreaties of the enemies of the current (in two senses) convention and overthrew it we would not rid ourselves of the anomaly of some charge carriers flowing the wrong way.

The answer that would undoubtedly emerge from Messrs Banthorpe, Ellis and Whitehead is that, as practical current carriers, electrons are in a large majority, having in metallic circuits at least a virtual monopoly; and that should decide the matter. The sacred cause of Democracy and all that. Students would still have to face the fact of current carriers flowing in the opposite direction to the currents they carried, but less often than at present, and every little helps. Whether that little would be enough to justify reversing very nearly all the books is a big question, however.

Perhaps it would help to answer it if we went on to a point that the current revolutionaries don't seem to have considered, or if they have then not enough. Suppose we did what they said and agreed to call the positive direction of electric current the direction in which the electrons composing that current were flowing, or, if the flow was of positive carriers, the opposite direction. Would students be any less confused than they are now if they were told that the positive direction of current was the direction in which negative charges were flowing, or
opposite to the direction in which positive charges were flowing? Or that (as suggested by Banthorpe) current flows from negative (i.e., a deficit) to positive (surplus), like water doesn't flow from the bottom of a well to the top of a hill?

## Too much, too late

On the reasonable assumption that the students would be even more confused by this, the revolutionaries would be driven to deciding to call electrons positive charges. That would have been an excellent idea 75 years ago when electrons were discovered. But now? The imagination boggles. As my fellow geriatric has pointed out, all rectifier, diode and transistor symbols would need to have their arrow heads reversed. The electric fields would have to be changed around too. All those + and - things in books on electronics would have to be interchanged. There would be great fun in deciding whether your car battery had been made before or after $R$ Day and so whether red should be taken to mean black and vice versa, or not. And what about Fleming's right and left hand rules? And the corkscrew rule? Would we have to reverse magnetic field conventions? As in the administration of VAT, problems would multiply as one went along. Before we were finished, the operation of changing Britain over to the right-hand rule of the road would look simple and straightforward.

Believe me, I'm truly sorry to be numbered with the reactionaries, but in this matter (as the key worker says when he downs tools for a $50 \%$ rise) I have no alternative.

## Reference

${ }^{1}$ Wireless World June, 1973, p294 and August, 1973, p. 386.

## New Products

## Reverberation unit

A variable decay reverberation system suitable for control room or portable use has been introduced by Feldon Audio Ltd. Manufactured by Quad-Eight Electronics of California, the RV-10 features a patented new approach to mechanical reverberation simulation which is claimed to provide a clean, transparent sound comparing favourably with existing devices or chambers.

The creation of totally new effects can be achieved by four different initial delays developed by independent transmission lines and the full delay pattern is released after 55 milliseconds. The reverberation runs in four continuous trains of multiples of the delay times with a signal to noise ratio of 60 dB . Immunity to external noise is better than 55 dB which makes the RV-10 ideal for use in control rooms under high-level monitor conditions. It also features 3 steps of low frequency roll-off which are $100 \mathrm{~Hz}, 250 \mathrm{~Hz}, 500 \mathrm{~Hz}$ at 18 dB per octave. Completely self contained, the unit is $19 \times 3 \frac{1}{2} \times 10 \frac{1}{2}$ in and 17 lb in weight.

Distortion in the drive and recovery system is under $0.25 \%$ up to full output level of +18 dBm maximum. The input sensitivity is +4 dBm and is continuously variable down to -20 dBm with internal trim pot. Input/output impedance is $600 \Omega$, transformer isolated and floating. The effective bandpass of the RV-10 reverberation system is 100 Hz to 7 kHz which is independent of the variable decay time setting. The overall frequency response has been limited to the useful reverberation bandwidth. This is claimed to be good industry practice and in conjunction with built-in filters eliminates the need for external filtering. Input and output connections are Jones barrier strip, and power requirements are 117 V a.c. at 12 W . Professional Equipment Division, Feldon Audio Ltd, 126 Great Portland Street, London W1N 5PH.
WW 309 for further details

## 17in storage c.r.t.

The direct-view storage cathode-ray tube type E722A manufactured by English Electric Valve Co. Ltd., provides very bright displays of information, ranging

from single transients and recurrent waveforms to half-tone pictures. Designed primarily for use in air traffic control radars, it is equally useful for medical, tabular display or other applications involving viewing under high ambient light conditions.

A new type of annular flood gun is used in the E722A which gives a uniform high brightness level across the whole of the display area. The useful viewing screen area is 153 square inches ( 995 sq cm ). A storage time of two to three minutes is normal with only ten per cent degradation of contrast. Storage can be extended by electronic methods to ten minutes or longer.

The image can be completely erased in a fraction of a second and selective erasure of information such as aircraft identification labels is possible. English Electric Valve Co. Ltd., Chelmsford, Essex CMI 2QU.
WW 310 for further details

## TV sweep generator

A high frequency-setting accuracy of better than $1.0 \%$ combined with a broad frequency range extending from $3-860 \mathrm{MHz}$ is provided by the PM5334 Philips TV sweep generator from Pye Unicam Ltd of Cambridge. Featuring eight front-panel selected sweep ranges that employ individual oscillators, the PM5334 covers all the frequencies needed for TV-set i.f. chroma and sound alignment, those for similar f.m.-receiver i.fs and TV bands I, III, IV and V, and f.m. band II. Fixed frequency markers are employed at important frequencies (5.5, 10.7 and 38.9 MHz ) and a variable one is available for use on any of the ranges.

The instrument also provides a continuously adjustable sweep width on each range with an additional control permitting the selected frequency width to be centred on the range scale. A further facility permits the sweep frequency to be adjusted in the range $8-50 \mathrm{~Hz}$.

The output on the PM5334 is stabilized and can be adjusted 80 dB down from a maximum of 200 mV , with the additional possibility of modulating this output with a 1 kHz signal. It is also possible for signals to be provided at this output which represent any of the fixed marker frequencies $\pm$ the variable-marker frequency (modulated or unmodulated), and a further output provides just the fixed marker frequencies as carrier signals.

A further feature of this instrument is its built-in bias-voltage source ( $0-30 \mathrm{~V}$ floating) which eliminates the need for a separate supply for this purpose in radio or television (both monochrome and colour) alignment work. It basically means that only the PM 5334 and a dual-trace oscilloscope, such as Philips PM3110, are needed for complete alignment of, for example, TV-set i.f. and subcarrier stages.
A front-panel colour-coding system is provided which associates a given function with its specified operation of the instrument. Pye Unicam Ltd., Cambridge. WW 311 for further details

## Illuminated lever switch

The Lever Lite III, from Souriau, is a part of the Switchcraft range of illuminated switches. It is available with three switching functions with alternatives up to eight pole double throw switching and giving a different colour of lever in each position.


Non-locking and locking (momentary) types are available. The contact springs are silver plated phosphor bronze with precious metal contact and the housing and lever of moulded plastic. Souriau (U.K.) Ltd, Shirley Avenue, Vale Road, Windsor, Berkshire.
WW 312 for further details

## Desoldering braid

The use of pure copper desoldering braid is accepted as an easy and effective aid to the desoldering of electronic components. But there has always been a severe disadvantage to its use because previously available desoldering braids usually contain a highly corrosive flux which is activated when used with a soldering
instrument. A new desoldering braid available from GDS Sales Ltd, does not contain a corrosive flux. Instead, a new formula flux is used which is based on resin and organic compounds. Adcola desoldering braid is available from GDS in three sizes: AA $(1.5 \times 0.4 \mathrm{~mm})$; $\mathrm{AB}(1.7 \times$ $0.7 \mathrm{~mm}) ; \mathrm{BB}(2.8 \times 0.7 \mathrm{~mm})$. Each type costs $£ 6$ per box of ten spools. GDS (Sales) Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Bucks.
WW 307 for further details

## $110^{\circ}$ deflection yokes

A range of colour TV deflection yokes has been announced by General Instrument Europe. It includes the type XP7311, XP731213 and 19194 Series assembly for use with 67 mm colour picture tube type A67-150X.

Facilities for rotating the yoke within the housing are provided for picture sauaring. A deauate axial movement for the yoke is provided for "red balling" prior to clamping the yoke in its optimum position for good beam landing.

The auto wound toroidal horizontal and vertical windings are laid into grooves formed in the plastic end caps mounted on the front and rear ends. of the ferrite yoke core. This precision turns placement ensures good and consistent convergence standards comparable to those currently being obtained on $90^{\circ}$ receivers using conventional saddle coils.

The plastic housings are moulded from self extinguishing material conforming to at least U.L. SE1 standards, whilst the terminal panels are of flame retardant s.r.b.p. material.


With the deflection vokes. G.I. has announced a radial convergence/purity panel designed for mounting on the rear of the $110^{\circ}$ PST deflection voke type XP 7311 etc. The coil assemblies contain windings for dynamic horizontal and vertical convergence control together with additional windings for electro-magnetic static shift. These assemblies are mounted on a flame retardant etched copper clad phenolic laminated panel conforming to BS 3888 (PPCD), DIN 40802 (C) and NEMA L1-1-1971 (FR2). A self extinguishing plastic mount to UL SE1 standards secures the purity magnets. The convergence assembly can be supplied with or without the integral purity correction magnets. Where dynamic blue width correction is not reouired, use of the G.I. blue lateral/purity device type 19194-1 is recommended. This last device is mainly constructed in plastic material conforming

## Auto ranging multimeter

Keithley Instruments have introduced a $3 \frac{1}{2}$ digit autoranging multimeter using l.e.d. display. The Model 165 has autorange and automatic polarity switching facilities; manual ranging is also provided for all functions.

As a d.c. voltmeter, the Model 165 covers measurements from 10 V to 1000 V with six full-scale ranges. Most d.c. voltage ranges offer $+0.1 \%$ reading accuracy plus a nominal digitization error. On the six a.c. voltage ranges, the 165 permits measurements over a frequency range of 20 Hz to 20 kHz with specified mid-band accuracies
of $0.7 \%$ to $0.9 \%$. Useful measurements may be made beyond these limits from 10 Hz to 100 kHz .

The a.c. current ranges cover five decades from 100 nA resolution to 2 A , with the same frequency range as a.c. voltage. The d.c. current ranges span seven fullscale decades, with overall sensitivity of $\ln \mathrm{A}$ to 2 A . Full range voltage drop is only 10 mV on all except the 1 A range where it is 100 mV . Resistance ranges also cover seven decades, with $0.1 \Omega$ to $200 \mathrm{M} \Omega$ sensitivity. Keithley Instruments Ltd, 1 Boulton Road, Reading, Berks.
WW 306 for further details

to UL SEl standards. A plastic knob moves two sliding plates, containing fixed magnets, in opposite directions to control the lateral movements of the blue and red/green beams. The purity magnet rings are mounted at the rear of the main assembly, General Instrument Europe S.p.A. 20149 Milano P.22a Amendola 9. WW 301 further detalls

## Panel mounting potentiometers

The T162P6 is a cermet 4 -in rectilinear potentiometer. It is fitted with an adapter manufactured from Delrin 500 and is bolted to the front panel giving accessibility to the screwhead for easier adjustment. Compared to a plain hole this mounting provides positive screwdriver location, a dust sealed panel and a much neater appearance. Other advantages of this product are said to be the high strength of the component to adapter joint with a push out minimum of 10 -lbf. and an anti-rotation threaded bush, with washer and nut which locks the component firmly to the panel. The dimensions of the basic potentiometer are increased by a minimal amount, the remainder of the specification being the same as for the basic potentiometer type T162P. Also available are the T62P6, $\frac{3}{-}$-in rectilinear and the T72P6, 1 -in rectilinear potentiometers with wirewound elements. Electrosil Ltd, Pallion Works, Sunderland, Co. Durham.
WW 305 for further details

## Variable-phase generator

A low-freauency limit of 0.1 Hz is provided in the latest addition to Philips range of L.f. eauipment. available from Pye Unicam Ltd of Cambridge. Known as the PM5161, this 0.1 Hz to 1 MHz variable-phase generator also has low signal distortion, this being typically $0.06 \%$ between 100 Hz and 50 kHz .

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| 30 K | Coivern. | 24021 | ${ }_{\text {E1.50 }}$ |
| 50 K | Reliance | . 07.10 | ${ }^{2} 2.25$ |
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| 50 K | Foxes |  |  |
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| 10 | Beckman | ${ }^{\text {A }}$ | ${ }_{\text {E }}^{\text {E3.00 }}$ |
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| $\begin{aligned} & 300 . \\ & 1 K . \end{aligned}$ | Fockman |  | ${ }_{\text {E2 } 2.25}^{\text {c2 }}$ |
| 10 K | Peckman | C.ss. | ${ }_{\substack{\text { c2.25 } \\ \text { c2 } 25}}$ |
| $20 \mathrm{~K} / 2 \mathrm{OK}$ | Beckman | c. | ${ }_{\text {c3 }} \mathbf{2} 20$ |
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Full range E24 values: each; $1 \mathrm{~W}: 6.8 \mathrm{~V}$ to $82 \mathrm{~V}, 21 \mathrm{p}$ each; $1.5 \mathrm{~W}: 4.7 \mathrm{~V}$ to 75 V , 48 p anch. Clip to increase 1.5 W rating to 3 wates (type) 266 F) 4p.
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BRIDGE RECTIFIER. 6A. IOOV. Motorola MDA952-2 65P. Supply. Contains 18,5V. 8.5A. sec. Transformer, $4 \times 4000 \mu \mathrm{~F} 25 \mathrm{~V}$. Mullard capacitors, $2 \times 2 \mathrm{~N} 3055$ on 2 Redpoint heatsinks, 12A., 120V. Bridge rectifier, stabilised p.c.b. circuit diagram. The
parts alone are worth the asking price of $£ 13$
each inc. carriage. Complete with long focus lens assembly. 4 Film Carriers. Boxed in as new condition. $£ 75$ each. HG5008 80 mA . 40 V . p.i.v. equiv. $\mathrm{OA} 47, \mathrm{f} 20$ per 1,000 . 52BN25 25A. 200V. Rectifier Diode. $\mathbf{£ 2 . 5 0}$ per 4. S6 A20 20A. 600 V . Rectifier Stack. $\mathbf{£ 3}$ each. Transistor Mounting Pads. $£ 2.50$ per 500 . Diode $\&$ Triac Mica Washer. $£ 1$ per 100 . Send s.a.e. for free circuit diagram.

## COMMUNICATIONS EQUIPMENT

 POCKET V.H.F. F.M. RADIOTELEPHONE Cossor Type CC2/8 Mk. 2.in two versions:-
Low band; Freq. range $71.5-104 \mathrm{MHz}$.
Low band; Freq. range $71.5-104 \mathrm{MHz}$.
R.F. Output 500 mW . Complete with $\frac{1}{4}$ wave whip aerial, combined microphone/loudspeaker and 13.3V. rechargeable nickel-cadmium DEAC battery Price $£ 75$ + v.a.t.
U.H.F. 2 watt FIXED RADIO LINK. 24 V . dc. 240 V . ac. F.M. TRANSMITTER/Type CC RTX 4 A Mk. R.F. Output 2 W at $450-470 \mathrm{MHz}$.

RECEIVER/Type CC RR4A Mk. Full Technical and operating Price $\mathbf{6 8 0 . 0 0}$ per unit and details on request. Mains Power Pack for the above
I I CARRIER EQUIPMENTS. Cossor Type CCM2A.
Solid state multiplex installations designed for U.H.F. radio systems enabling 2 speech channels the equivalent in telemetry information, to be transmitted simultaneously over a radio system.
V.H.F. RADIOTELEPHONE BAD RASE STATION. Cossor Type CC 603 Transmitter. Simplex or duplex operation, local or remote control with talk through facilities, using double sideband a.m. modulation.
Low-band $71.5-104 \mathrm{MHz}$. or High-band $156-174 \mathrm{MHz}$. RF. Output powe
RF. Out put power 25 W . into 50 Ohms. 24V.de. Operation. Prices and details on request
OPTIONAL POWER SUPPLY Type CC 101 for type CC603 base station P.O.A.
SELECTIVE CALL SYSTEM. Coder TYpe $C C 505 / 50$ ( 50 way) or CC $505 / 100$ ( 100 way).
The Cossor selective call system may be used with The Cossor selective call system may be used with any communication system where a base station is required to call any one or all of a number of
sub-stations. Both versions available, all new and in original packing. Price: 50 way $\mathbf{6 5}+$ v.a.t DECODERS 615 ea 100 way $£ 80+$ v.a.t. DEAC RECHARGEABLE BATTERY CASSETTES $13.4 V$ (nom.) type B/SA 80351/108 Heavy duty encapsulated DEAC supply. Size $3 \frac{1}{2} \times 2 \frac{1}{2} \times 1 \frac{1}{2}$ in.
8-W PA
PATTERY CHARGER Type CC
999 Charges up to 8 of the above battery cassettes. I2-WAY BATTERY CHARGER Type CC 999 Charges up to 12 of $13.4 \vee D E A C$ batteries. Metered Charges up to 2 of 13.4 ck . ${ }^{2}$ batteries. Metered
battery condition check. $£ 35+$ v.a.t. MICROPHONES S. G. Brown Stick Microphone and
to-talk button. $300 \Omega$. $E 5$ complete.
S. G. Brown Hand-held with push-to-talk button. 48 each.

ELECTRONIC COMPONENTS Pack BARGAIN COMPONENT PACKS
No. 500 Carbon resistors, $\frac{1}{4}, \frac{1}{2}, 1,2$ watt.
2100 Electrolytic Condensers.
3250 Ceramic, Polystyrene, Silver Mica, etc.,
Condensers.
4250 Polyester, Polycarbonate, Paper, etc., Condensers.
5.25 Potentiometers, assorted.

6250 High-stab. $1 \%, 2 \%, 5 \%$ resistors.
750 Assorted Tagstrips.
8 llb Assorted nuts, bolts, washers, spacers, etc. 25 Assorted switches, rotary, lever, micro, 10 toggle, atc.
50 Proset Potentiometers.
II Trial mixed component pack $£ 1$.
12 Jumbo mixed peck $\notin 5$.
ALL COMPONENTS AND UNUSED
$\mathrm{fl}+25 \mathrm{p}$ p.p. per pack, $\& 5$ for 5 packs p/free.
FULL RANGE OF ELECTRONIC COMPONENTS
AT OUR RETAIL SHOP. OPEN $9.30-6$ MON.-SAT.


MARCONI SIGNAL GENERATOR TYPE TF-144G: Freq. $85 \mathrm{Kc} / \mathrm{s}-25 \mathrm{Mc} / \mathrm{s}$ in 8 ranges. Incremental: $\pm 1 \%$ at $1 \mathrm{Mc} / \mathrm{s}$. Output: continuously variable 1 microvolt to 1 volt. Output Impedance: 1 microvolt to 100 millivolts, 10 ohms 100 mV volt - 52.5 ohms. Internal Modulation: $400 \mathrm{c} / \mathrm{s}$ sinewave $75 \%$ depth. External Modulation: Direct or via internal amplifier. A.C. mains $200 / 250 \mathrm{~V}, 40-100 \mathrm{c} / \mathrm{s}$ condition. $\mathbf{2} 27.50$ each, Carr. 11 1-50.
T. 1509 TRANSMITTERS (FOR EXPORT ONLY): General-purpose HF communications transmitter for use in fixed or mobile ground stations. Hand or high-speed keying. Crystal or Mre control, with temperat/re. Modulation: $100 \%$ circuit.CW, MCW and R/T. Frequency: 1.5 to Mm M/s. Modulation. Amplifier $2 \times 813$ and Modulator $2 \times 813$. Power requirements $200-250$ volts a.c., 50 cycles. Power out put 300 watts. Dimensions 2 ft . 6 in. W $\mathbb{W} \times 2 \mathrm{ft}$. D. $\times$

AN/ARC-27 TRANSMITTER/RECEIVER (FOR EXPORT ONLY): Frequency $225-400 \mathrm{mc} .1750$ channels 100 Kc apart with 18 preset channels Modulation: am. Power output 9 watts. Receiver is superheterodyne. Max output 2 watts. Antenna: 50 ohm impedance. Power requirements 24 v d.c. Completc transmitter with operating cables, control box, headphones, microphone. Price $\neq 250.00$ each secon and exce-27. 100 volts
input. 24 v d.c. output @ 41 amps fully smoothed. $£ 45.00$ each.
FREQUENCY METER BC-221: $125-20,000 \mathrm{Kc} / \mathrm{s}$, complete with origina calibration charts. Checked out, working order. $\notin 18.50+\chi_{1} 100$ cars $£ 35 \cdot 00$ Unused as

CT. 52 MINIATURE OSCILLOSCOPE: Portable. Operates from 115 V or $250 \mathrm{~V} 50-60 \mathrm{c} / \mathrm{s}$; or $180 \mathrm{~V} 500 \mathrm{c} / \mathrm{s}$. A small compact tropicalised instrument designed to meet requirements of radar and communication engineers and general electronic service. Measures 9 in . Tube 2 in in. Frequency compensated amplifier up to 38 dB gain. Bandwidth up to $1 \mathrm{Mc} / \mathrm{s}$. Single sweep facilities. Complete with test leads, metal transit case. As new $\mathbf{£ 2 7 - 5 0}$ each. Carr. $£ 1$.

TUNING UNIT: 24 V geared motor driving double 25 pf double spaced variable capacitor. One $\mathrm{m} / \mathrm{c}$ relay and 2 other relays. $£ 2 \cdot 50$ each 30 p post, good condition. UHF ASSEMBLY: (suitable for $1,000 \mathrm{MHz}$ conversion) including UHF valves counters $0-999$. Valves 6 AL 5 and $8 \times 6 \mathrm{AK} 5 . £ 10.00$ plus 60 p post, good condition. MODULATOR UNIT: complete with transformer and $2 \times 807$ valves mounted in 19 in . chassis $\times 8 \mathrm{in}$. high $\times 8 \mathrm{in}$. deep. $\mathbf{£ 4} 40$ secondhand cond., or $£ 6.50$ new cond. Carriage $\times 8$
RF UNIT: suitable for use with the above unit. Complete with $2 \times 3 \mathrm{E} 29$ valves Ideal for conversion to 4 metres. $£ 5$ secondhand cond., or $£ 7.50$ new cond Carriage £1.
POWER SUPPLY UNIT PN-12A: 230V a.c. input $50-60 \mathrm{c} / \mathrm{s}$. 513V and 1025V @ 420 mA output. With 2 smoothing chokes $9 \mathrm{H}, 2$ Capacitors, 10 Mfd 1500 V and 10 Mfd 600 V . Filament Transformer 230 V a.c. input. 4 Rectifying Valves type $5 \mathrm{Z3}$. ${ }^{2} \times 5 \mathrm{~V}$ windings @ 3 Amps each, and $5 \mathrm{~V} @ 6 \mathrm{Amp}$ and $4 \mathrm{~V} @ 0.25 \mathrm{Amp}$. Mounted $2 \times 5 \mathrm{~V}$ windings @ 3 Amps each, and 5 V @ 6 Amp and $4 \mathrm{~V} @ 0.25 \mathrm{Amp}$. Mounted

AUTO TRANSFORMER: $230-115 \mathrm{~V}, 50-60 \mathrm{c} / \mathrm{s}, 1000$ watts, mounted in a strong steel case $5^{\prime \prime} \times 6 \frac{2^{\prime \prime}}{2^{\prime}} \times 7^{n}$. Bitumen impregnated. £7 each, Carr. 75 p . $230-115 \mathrm{~V}$, $50-60 \mathrm{c} / \mathrm{s}, 500$ watts. $7^{*} \times 5^{\prime \prime} \times 5^{\prime \prime}$. Mounted in steel ventilated case. $\mathbf{~} 4.00$ each, Carr. 75p.
MODULATOR UNIT: 50 watt, part of BC-640, complete with $2 \times 811$ valves, microphone and modulator transformers etc. $£ 7.50$ each, 75 p carr.
CATHODE RAY TUBE UNIT: With 3in. tube, Type 3EG1 (CV1526) colour green, medium persistence complete with nu-metal screen, $£ 3 \cdot 50$ each, post 50 p. APN-1 INDICATOR METER, $270^{\circ}$ Movement. Ideal for making rev. counter. ع1-25, post 30 p
AIRCRAFT SOLENOID UNIT S.P.S.T.: $24 \mathrm{~V}, 200 \mathrm{Amps}, \mathbf{\varepsilon} 2$ each, $\mathbf{3 0}$ p post. DECADE RESISTOR SWITCH: 0.1 ohm per step. 10 positions 3 Gang, each, 0.9 ohms. Tolerance $\pm 1 \%$ £3 each, 25 p post. 90 ohms per step. 10
total value 900 ohms. 3 Gang. Tolerance $\pm 1 \% £ 3.50$ each, post 30 p.

TF-1041B VALVE VOLTMETER: Measures 25 mV to $300 \mathrm{~V}, 20 \mathrm{c} / \mathrm{s}$ to 1500 $\mathrm{Mc} / \mathrm{s}$ a.c. Also 10 mV to 1000 V d.c. Resistance 0.02 ohms to 500 Meg . ohms. Power requirements $200-250$ volts a.c. Secondhand, excellent con. $£ 35 \cdot 0 \mathrm{C}$. Carr. $£ 1$
VARIAC TRANSFORMERS: Input 115 V , output $0-135 \mathrm{~V}$ at 2 Amps . £ 3 each 75p pos
RACK CABINETS: (totally enclosed) for Std. 19 in . Paneis. Size 6 ft . high $\times 21$ in. wide $\times 16 \mathrm{in}$. deep, with rear door. $£ 12$ each, $£ 2.50$ Ca
in. wide $\times 19 \mathrm{in}$. deep, with rear door. $£ 8.50$, each, $£ 2$ Carr
INSTRUMENT CABINETS: $19^{\prime \prime} \mathrm{W} . \times 16^{\prime \prime} \mathrm{H} . \times 16^{\circ} \mathrm{D}, £ 5.00+£ 1.25 \mathrm{carr}$. $19^{\prime \prime}$ W. $\times 10^{0} \mathrm{D} . \times 5^{\prime \prime} \mathrm{H}$. $\quad £^{2 \cdot 50}+£ 1 \cdot 00$ carr
TS-418/URM49 SIGNAL GENERATOR: Covers $400-1000 \mathrm{MHz}$ range. CW Pulse or AM emission. Power Range 0-120 dbm. £125 each. Carr. £.1.50. TN/130/APR. 9 UHF TUNING UNIT: Freq. $4300-7350 \mathrm{MHz}$. IF Output 160 MHz with bandwidth of 20 MHz and is electrically tuned by a d.c. reversible
ALL U.K. ORDERS SUBJECT TO $10 \%$ VALUE ADDED TAX. THIS

SIGNAL GENERATOR TS-497B/URR: (Boonton). Freq. $2-400 \mathrm{Mc} / \mathrm{s}$ in 6 bands. Internal Mod. 400 or $1000 \mathrm{c} / \mathrm{s}$ per sec. External Mod. 50 to $10,000 \mathrm{c} / \mathrm{s}$ per sec. External PM. Percent Mod. $0.1-100,000$ microvolts cont. variable. Impedance $50 \Omega$. Price O/put Voltage
65 each +61.50 carr.
CLASS "D" WAVEMETER NO. 1 MK . II: Crystal controlled heterodyne cequency meter covering $2-8 \mathrm{MHz}$. Power supply 6 V d.c. Good secondhand cond $£ 7.50$ each. Post 60 p
RCA TE-149 HETERODYNE WAVEMETER: V-cut, 1 MHz crystal ( $0.005 \%$ ) Accuracy better than $0.02 \%$. Dial directly calibrated every 1 KHz from $2.5-5 \mathrm{MHz}$ Accuracy better than Useful harmonics up to 20 MHz . Provision for fitting internal dry batteries. "As new" complete with Manual and Spares. £14 each. Carr. 75p
POWER UNIT TYPE 24: (for R. 216 Receiver) A.C. operated 100-125V or 200-250V, 50c/s."As new" 110 each. Carr. 75p
ROTARY INVERTERS: TYPE PE.218E-input $24-28 \mathrm{~V}$ d.c., 80 Amps

POWER SUPPLY: 230 V a.c. input; 3000 V @ 2.5 mA ; 4 v @ $1 \mathrm{Amp}, 300-0-300$ 200 mA ; 6 V

ACTUATOR UNIT: With 115 V d.c. geared motor; o/put 12.5 rpm ; torque
16 ins. oz; reversible; microswitches and potentiometer. E 3.50 ea. +40 p post. 16 ins. oz; reversible; microswitches and potentiometer. 83.50 ea. +40 p post.
DALMOTORS: $24-28 \mathrm{~V}$ d.c. at $45 \mathrm{Amps}, 750$ watts (approx. 1 hp ) $12,000 \mathrm{rpm}$ \& 5 each, 60 p post.
MOTOR: 240 V single phase, $2,400 \mathrm{rpm}$. $1 / 40 \mathrm{H}$.P. approx. Price $£ 1.75$ each, 30p post.
LIST OF MOTORS AVAILABLE FOR 6 .
CONDENSERS: 30 mfd 600 V wkg. d.c., $£ 3.50$ each, post 50 p .10 mfd 1000 v wkg. 80 p , post $30 \mathrm{p} .8 \mathrm{mfd} 2500 \mathrm{v} £ 5$, carr. 80 p .8 mfd 600 v 45 p , post 15 p .8 mfd $1 \% 300 \mathrm{v}$ d.c., $£ 1.25$, post 25 p .4 mfd 3000 v wkg. $£ 3$, post 50 p . $4 \mathrm{mfd} 2000 \mathrm{v} £ 2$, post $40 \mathrm{p} .4 \mathrm{mfd} 600 \mathrm{v}, 2$ for $£ 1.00$, post 30 p . Capacitor $0 \cdot 125 \mathrm{mfd} 27,000 \mathrm{v}$ wkg. $\notin 3.75$, post 50 p .225 mfd 25 Kv wkg . $£ 20$, carr. $£ 3.2 \mathrm{mfd} 12.5 \mathrm{Kv}$ wkg. TCC RI
 CONTROL PANEL: 230 v. A.C., 24 v . D.C. @ 2 amps , $\mathbf{~} 2.50$ each, carr. 75 p OHMITE VARIABLE RESISTOR: 5 ohms , $5 \frac{1}{2} \mathrm{amps}$; or 40 ohms at 2.6 amps 500 ohms, 0.55 amps. Price (either type) $£ 2$ each, 30 p post each
TX DRIVER UNIT: Freq. $100-156 \mathrm{Mc} / \mathrm{s}$. Valves $3 \times 3 \mathrm{C} 24$ 's; complete with filament transformer 230 v . A.C. Mounted in 19in. panel, ©4.50 each, carr. 75p. AR88 RECEIVER: List of spares, 5 p.
REDIFON TELEPRINTER RELAY UNIT NO. 12: ZA-41196 and power supply $200-250 \mathrm{~V}$ a.c. Polarised relay type 3 SEITR. $80-0-80 \mathrm{~V} 25 \mathrm{~mA}$. Two stabi2 ondition $£ 7.50$, Carr. 75p.
WESTON INDUSTRIAL THERMOMETER MODEL 221: 0-100 ${ }^{\circ} \mathrm{C}$. 3 in. dia. scale Accuracy 1\%. Precision made coil within-coil structure. Changes in dia. scale. Accuracy 1\%. Precision made coil within-coil structure. Changes in is mounted. $£ 2 \cdot 80$ each 30 p post. Unused condition.
TRANSMITTER UNITS: Complete with 12 V vibrator unit QQVO3-20A and 5 other valves with modulation transformer, etc. Two crystal controlled channels. Suitable for conversion to 2 metres. $£ 5+£ 1$ carr.
THERMOCOUPLE METER: Scale 3.5 AE 2 in . square flush mounting. ${ }^{6} 2 \cdot 50+25 p$ post.
TS 15C/AP FLUXMETER: Used to provide qualitative measurements of flux densities between pole faces
good cond. $£ 25+60 \mathrm{p}$ post.
SYNCHRO DISTORTION AND MARGIN TEST SET: (Onwood Type 4A2) S/hand excellent cond. $£ 85$ each. Carr. $£^{2}$.
MASTER SYNCHRO TEST SET T. 101031 (U.S.A.): 115 volts $400 \mathrm{c} / \mathrm{s}$. S/hand cond. $£ 15$ each $+£ 1$ carr.
MAGSLIP TESTER NO. 2 MK. I: S/hand cond. $£ 25$ each $+£ 1$ carr.
SYNCHROS: and other special purpose motors available. Send for list. S.A.E. PANORAMIC ADAPTOR TYPE ALA2: Suitable for use with APR-1, APR-4, and other Receivers having an ceived frequency Power Supply 115 V a.c. $400 \mathrm{c} / \mathrm{s}$. Tube 3PB1 with nu-metal screen. $£ 8.50$ each. $£ 1$ carr. $\mathrm{S} / \mathrm{hand}$ cond.
TELEPRINTER EQUIPMENT: MUIRHEAD D-514-A TRANSMISSIONMEASURING SET: Consists of an oscillator covering audio and carrier frequencies, with suitable transmission measuring equipment. Power pack is contained in a separate case and operates from A.C. mains at various voltages, or from an $100-40,000 \mathrm{~Hz}$. Direct reading from decade dials. Accuracy $\pm 0.4{ }^{\circ}$ continuous $100-40,000 \mathrm{~Hz}$. Direct reading from decade dials. Accuracy $\pm 0 \cdot 4 \% \frac{ \pm 3 \mathrm{~Hz}}{} \mathrm{mver}$
whole range. Oscillator o/put $5 \mathrm{~mW}(+7 \mathrm{db})$ or more inot $600 \Omega$ at any freq. Meawhole range. Oscilator surement up to 50 db and down to at least 45 db . Price $£ 10$ each Carr. £1.
TELEPRINTER TYPE 7B; Pageprinter 24 V d.c. power supply, speed 50 bauds per min. 'as new' cond. in original packing case, $£ 25$ each; or second hand cond per min. as new cond. in oroginal $($ excellent order) no parts broken, $£ 15$ each. Carriage either type $£ 2$. Full list of Teleprinter equipment available for $6 p$.
AUTOMATIC VIBRATION EXCITER CONTROL UNIT TXPE 1016 Manufactured by Bruel $\&$ \& K
very good cond.
+50
+2
carr.
INSULATION TEST SETS: A.C. or D.C. $0-5 \mathrm{kV}$, $£ 22 \cdot 50$. S/hand cond. AND $0-3 \mathrm{kV}$. Positive and negat.
INSULATION TEST SET: $0-10 \mathrm{kV}$ negative, earth with amplifier provision for checking ionisation. $110 / 230 \mathrm{~V}$ a.c. input. S/hand good cond. $£ 30+£ 1$ carr BOONTON SIGNAL GENERATOR TYPE 202B A.M./F.M.: $54-216 \mathrm{MHz}$ in three bands. Deviation 24,80 and $240 \mathrm{kc} / \mathrm{s}$. Attenuator is adjustable 0.1 U to 0.2 V . As new condition. $£ 175+\varsigma^{2}$ carr
AVO FIXED ATTENUATORS: 75 ohms. $\mathbf{~} \mathbf{2} \cdot \mathbf{5 0}+20 \mathrm{p}$ post. New cond.
R.F. POWER METER: $0-30$ watts s/hand good cond. $£ 27 \cdot 50+£_{1}$ carr.
avo valve TESTER AND CHARACTERISTIC METER: S/hand good condition. $£^{35}$ each $+£^{2}$ carr.
AVO VALVE TESTER MK. III: $£ 30+£ 2$ carr
Miscellaneous Vacuum and Pressure Gauges available. Please send for list 6 p .
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071 and 072 Series



| Type No. | Working Voltage $V \mathrm{dc}$. | Capaclitance | Max. Ripple Current at $50^{\circ} \mathrm{C}$ | Weight | Price |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 07114472 | 10 | 4700 | 2.5 mps | 102 | $15 p$ |
| 07114682 | 10 | ${ }^{6800}$ | 4 amps | 102 | 170 |
| ${ }_{071} 15742$ | ${ }_{16}^{16}$ | 3300 |  | 102 | 15 p |
| 07115682 | ${ }_{16}^{16}$ | 6800 | ${ }_{5}{ }_{5} .8 .8 \mathrm{ampmps}$ | 102 | 17 p |
| 07214143 | 10 | $11000+11000$ | 10.6 amps | ${ }_{302}$ | 37p |
| 07714173 | 10 | $16500+16500$ | 13.4 amps | 402 | 49p |
| 8721575 |  | 17500 +7500 | 10.5 amps | 302 | 37p |
| 07215502 | ${ }_{25}^{16}$ | 11000 | ${ }_{9} 9.6 \mathrm{amps}$ | ${ }_{4}^{4}$ | 49p |
| 07216752 | 25 | ${ }_{7500}+7500$ | 12.6 amps | 302 | 37p |
| 07217502 | 40 | $5000+5000$ | 12.0 amps | ${ }_{4}^{102}$ | 49p |
| 07118681 07218172 | 63 63 | $1650 \stackrel{680}{+1650}$ |  | 102 302 | 15p |
| 106 and 107 Series |  |  |  |  |  |
| 10614453 |  | 15000 | 7 mps |  |  |
| 10617103 | ${ }_{43}^{40}$ | 10000 | 12 amps | 7 fioz | 4p |
| - 10710618153 | ${ }_{10}^{63}$ | 15000 | ${ }^{28} \mathrm{amps}$ |  |  |
|  |  |  | 10 amps | ${ }^{\text {¢ }}$ | 74 |
| Type No. | Voltage | Capacitance | Weight |  | Price |
| 10215163 | 16 | 16000 | 802 |  | 20p |
| 10490003 10216802 | 20 25 | 39000 8000 | 1602 702 |  | 30 p 250 |
| 10417562 | 40 | 5600 | 502 |  | 25p |
| 10490001 | 45 | 20000 | 1607 |  | 50p |



SMALL ELECTROLYTICS

| $\begin{aligned} & \text { Ref. } \\ & \mathrm{H} 8 / 2 \mathrm{No} . \end{aligned}$ | Capacity | $\underset{\text { Volage }}{\substack{\text { 25v }}}$ | Price | Ref. No. | Capacity | Voltage | Price |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H8/2A | 3-3 3 ¢ | 25v | 4 p | H714 | 6449 | 15v | $4{ }^{4}$ |
| н8/3 | зия | 50 v | 4 p | H7/4A | ${ }^{64 \mu \mathrm{fa}}$ | 35v | 5 5 |
| H8/3A | 4 ff | 50v | 4 p | H776 |  | ${ }_{\substack{16 \mathrm{~V}}}^{165 \mathrm{y}}$ | ${ }_{50}$ |
| H814 | 4.7 \%f | $25 v$ | 40 | ${ }_{\text {H }} 777$ | ${ }_{1000 \mathrm{u}}$ | 25v | ${ }_{40}$ |
| H814A | ${ }^{5} \mathrm{u}$ f | 64 V | 4 p | H778 | ${ }^{12544}$ | 16 v | 5 p |
| H815 | 5uf | 10 y | 48 | H778A | 1004 | 35v | ${ }^{6 p}$ |
| ${ }_{\text {H }}$ |  | $\xrightarrow{150 \mathrm{~V}}$ | ${ }_{40}$ | H79 + $H$ | 125ut | ${ }_{4 \times}$ | ${ }_{60}$ |
| H817 | 1041 | 70 V | 40 | H7110 | ${ }^{125 \mu 4}$ | 25 v | $6{ }_{6}$ |
| H8, 8 | 16 LH | ${ }^{35 v}$ | 4 p | H7710A | 1 160ut | 2.5 v | 3 p |
| H8184 | 1645 | ${ }^{16 v}$ | ${ }_{4}{ }^{\text {p }}$ | H7111 | 160ut | 25v | ${ }^{6 p}$ |
| H819 | ${ }_{2015}^{2045}$ | ${ }_{70 \mathrm{~V}}^{6}$ | 2 p | H7711A | 150uf | ${ }_{\text {12v }}^{16 \mathrm{~V}}$ | 5 sp |
| H8190 | $22 \mu$ | 50 v | 4 p | H7714 | 22049 | 50v | 10 p |
| H88111 | ${ }^{224 \mu}$ | ${ }_{12 \mathrm{l}}^{100 \mathrm{~V}}$ | ${ }_{40}^{4 p}$ | H7715 | ${ }_{2}^{2204 \%}$ | 25v | 50 |
| H8/11A | 244 f | 275 | 4 p | H61/4 | ${ }^{2504}+$ | 4 y | $3{ }^{\text {p }}$ |
| H8812 | ${ }^{3247}$ | 15 v 10 v | ${ }_{40}^{40}$ | ${ }_{\text {H6/3A }}$ | 3320uf | 2.5v | 3 p |
| Н88i3A | ${ }_{\text {324 }}$ | 50 v | ${ }_{4 \mathrm{p}}$ | ${ }_{\text {H6/4A }}$ | 330uf |  | ${ }^{40}$ |
| H8/14 | 40 ff | 25v | 5p | H615 | 330 Hf | 25v | 10p |
| H8814A | 40 Hf | 16 y | 4 p | H6/5A | 330uf | ${ }_{35}$ | 15 p |
| H8115 | 47 Lt | 50v. | 4 D | H618 | 4704 | ${ }^{25 v}$ | 10 p |
| H771 | - | ${ }_{6}^{35 v}$ | ${ }_{3 \mathrm{p}}^{4 \mathrm{p}}$ | ${ }_{\text {H6i9A }}$ | 400uf | ${ }_{40 \mathrm{v}}$ | ${ }_{200}^{200}$ |
| H71/ | 50 mf | 10v | ${ }_{40}$ | H6110 | 750ut | 12v | 5 p |
| ${ }^{\text {H }} 712 \mathrm{l}$ ( ${ }^{\text {a }}$ | ${ }_{6047}$ | ¢ | ${ }_{40}^{40}$ | H6613A | ${ }^{1000}$ uf | 25v | 16 p |
|  | 64 | $2 \cdot 5$ | 2 D | H5/2A | 22004 | 16v | 15p |

RECTIFIERS 1 N4007 1200 peak volts, 30 amps peak current, 1 amp mean current. 100 for $£ 7 \cdot 50,1,000 £ 50$.

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TO3-NPN DIFFUSED SILICON PLANAR EPITAXIAL
VCEO COLLECTOR TO EMITTER-60 VOLTS
VEBO EMITTRR TO BASE-S VOLTS.
20 WATTS- 2 AMPS -30 MHZ. FEATURES HIG
OVER WIDE RANGE OF COLLECTOR CURRENT


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Standard Post Office type Guaranteed in working order ONLY $27 \frac{1}{p} \mathrm{p} p$

| TESTED AND GUARANTEED PAKS |  |
| :---: | :---: |
| 879 | $4 \begin{array}{l}\text { IN4007 Sill Rec. diodes. } \\ 1.000 \text { PIV lamp plastic }\end{array}$ |

B81 $10 \begin{aligned} & \text { Reed Switches } \\ & \text { high speed P.O. type }\end{aligned}$
Mixed Capaciors Approx quantity, courted by weight. 55p
${ }^{899} 200$ P\& \& 15 p .
Mixed Resisto-s. Approx quantily, col
$P \& P 15 \mathrm{P}$.
Wirewound Resistors. Mixed
types and values
OCP71 Light Sensitiv
Photo Transistor OC200/1/2/3 PNP Silicon OC200/1/2/3 PNP
uncoded TO 5 can 1 Watt Zener Diodes. Mixed Voltages 6.8-43V
$100 \begin{aligned} & \text { Mixed Diodes. Germ Gold bond } \\ & \text { etc. Marked and Unmarked. }\end{aligned}$ Short lead Tran sisiors.
30 NPN Silicon Planar types

H39 6 | Integrated circuits. 4 Gates |
| :--- |
| BMC 962. | 20 BFY50/2.2N696, 2 N 1613 $2 \begin{aligned} & \text { Power Transistors } \\ & \text { Comp Pair BD } 131 / 132\end{aligned}$ UNMARKED UNTESTED PAKS


55p
${ }^{\text {B83 }} 200 \begin{aligned} & \text { Trans. manufacturers' rejects } \\ & \text { all types NPN. PNP. Sit and Germ. } \\ & \text { 55p }\end{aligned}$
B84 100 Silicon Diodes DO. 7 glass
-100
${ }^{\text {B }} 106 \begin{aligned} & \text { Sil. Diodes sub. min } \\ & \text { in9 } \\ & 14 \text { and IN916 types }\end{aligned}$
5
$40{ }^{250 m W}$ Zener Diodes
DO-7 Min. Glass Type
30 Top Hat Silicon Rectifiers.
15 Experimenters Pak of
Integrated Circuits, Data supplied
3 Amp Siticol Stud
NPN Silicon Trans. 2N3707-1
range, low noise amp.
$15 \begin{aligned} & \text { Power Transistors. PNP. Germ. NP } \\ & \text { Sificon } T O-3 \text { Can. } P \& P 5 p \text { extra. }\end{aligned}$
H34 15 (510.3

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\hline \multicolumn{2}{|l|}{TYPESW. $100100 \times 80 \mathrm{~mm}$} <br>
\hline - \& $100 \mu \mathrm{~A}$...... 23.95 <br>
\hline \& 100-0-100นA ${ }^{2} 38.90$ <br>
\hline \&  <br>
\hline \& 20V. D.C. ... E33 $_{50} 60$ <br>
\hline \& 50V. D.C. <br>
\hline \& 1 amp. D.C... $£ 3.60$ <br>
\hline \& 5 amp D.c... ${ }^{3} 3.80$ <br>
\hline \& $$
300 \mathrm{~V} \text { A.C. } \cdots \text { £3. }{ }^{2} 0
$$ <br>
\hline 80-0-50رA .. 23.85 \& VU Meter. ... £4.30 <br>
\hline \multicolumn{2}{|l|}{TYPE SD. $83082.5 \mathrm{~mm} \times 110 \mathrm{~mm}$ Fronts} <br>
\hline \& 10 ma ..... 89.10 <br>
\hline \& 50 mA

100 <br>
\hline \& 500 mA ….... 23.10 <br>
\hline \& $\underline{1}$ amp. ...... ${ }^{3} 3.10$ <br>
\hline \& 5 amp. ...... $83 \cdot 10$ <br>
\hline 50 HA ....... 23.40 \& 5v, D.C...... $£ 3 \cdot 10$ <br>
\hline $50-0-50 \mu \mathrm{~A}$.. $£ 3.40$ \& 10V. D.C.... $£ 3 \cdot 10$ <br>
\hline $100 \mu \mathrm{~A}$ ㄱ... $£ 3.35$ \& 20V. D.C..... $£ 3.10$ <br>
\hline 100-0-100 4 A \& 50V. D.C. ${ }^{\text {co.. }}$ ¢3.10 <br>
\hline  \&  <br>
\hline $1 \mathrm{~mA} . . . .{ }^{\text {a }}$. $83 \cdot 10$ \& 300 V. A.C.... $£ 3.30$ <br>
\hline  \& VU Meter.... $£ 3.50$ <br>
\hline \multicolumn{2}{|l|}{TYPE SD. 640 63. $6 \mathrm{~mm} \times 85 \mathrm{~mm}$ Fronts} <br>
\hline $50 \mu \mathrm{~A}$...... $£ 3.05$ \& 500 mA . . . . $£ 2.80$ <br>
\hline $50-0-50 \mu \mathrm{LA}$.. 23.05 \& 1 amp. ...... $£ 2.90$ <br>

\hline  \& $$
\begin{aligned}
& 5 \mathrm{amp} . . . . . . . \quad £ 2.90 \\
& 10 \mathrm{amp} .
\end{aligned}
$$ <br>

\hline $$
\begin{array}{ll}
100-0-100 \mu \mathrm{~A} \\
200 \mu \mathrm{~A} & \ldots 3.00 \\
£ 3
\end{array}
$$ \& \[

$$
\begin{aligned}
& 10 \mathrm{amp} . . . .{ }_{52} 90 \\
& 5 \mathrm{~V} . \mathrm{D.c.} . . . \\
& £ 2.90
\end{aligned}
$$
\] <br>

\hline $500 \mu \mathrm{~A}$ …… \& 20V. D.C..... 22.90 <br>
\hline  \& 50 V. D.C..... $£ 2.90$ <br>
\hline  \& 300V. D.C. ... 22.90 <br>
\hline  \&  <br>
\hline 100 mA ....... ${ }^{\text {2 }} 2.90$ \& VU Meter..... £3.15 <br>
\hline
\end{tabular}

| TYPE SD. 460 46mm $\times 50.5 \mathrm{~mm}$ Fronts |  |  |  |
| :---: | :---: | :---: | :---: |
| 50 HA | £2.80 | 500 ma |  |
| $50-0-50 \mu \mathrm{~A}$ | £2.80 | 1 amp . |  |
| $100 \mu \mathrm{~A}$ | £2.75 | 5 amp . | $\underline{22} 80$ |
| 100-0-100 A A | 22.75 | 10 ant | ${ }_{5} 2.80$ |
| $200 \mu \mathrm{~A}$ | 22.70 | ${ }^{51}$ 10v. D.C. | ${ }^{2} 2.60$ |
| $500 \mu \mathbf{A}$. ${ }^{\text {a }}$. | £2.55 | 20v. L.C |  |
| $1 \mathrm{~mA} . . . . .$. | £2.60 | 50 V . D. |  |
| 5 mA . | £2. 80 | 300 V . D. | 22.80 |
| $10 \mathrm{~mA} \ldots \ldots$. | £2.80 | 15 V . A.C | 22.70 |
| 50 mA | £2.80 | 300 V . A |  |
| 100mA ...... | £2.80 | vu Mieter | 22.90 |

"SEW" EDGWISE ME
TYPE P.E. 70




\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|l|}{TYPE MR.85P 4 4in. $\times 4$ din fronts.} <br>
\hline -xownem \&  <br>
\hline \&  <br>
\hline \& 500 ma

a <br>
\hline \&  <br>
\hline \&  <br>
\hline \&  <br>
\hline \&  <br>
\hline  \& 300V. D.C. ... ${ }^{\text {z3.80}}$ <br>
\hline ${ }^{50-0-5004 A}$.. ${ }^{44} 25$ \&  <br>
\hline  \&  <br>
\hline  \&  <br>
\hline ${ }_{500 \mathrm{uA}}$ …… 83.90 \&  <br>
\hline $500 \cdot 0 \cdot 500 \mu \mathrm{~A} . .53 .90$ \& 5 amp A.C. $\because .: 30$ <br>
\hline  \&  <br>
\hline  \&  <br>
\hline 5ma ........ 23.90 \& 30 amp. A.C. 83.80 <br>
\hline \multicolumn{2}{|l|}{TYPE MR.52P 2tin. square tronts.} <br>
\hline $50 \mu \mathrm{~A}$...... 23.50 \& 10V. D.C. .... 22.50 <br>
\hline 50-0-50uA .. $£ 3.05$ \& 20V.D.C. ... 22.50 <br>
\hline $100 \mu \mathrm{~A}$. . . . $£ 3.00$ \& 50V. D.C. ... £2. 50 <br>
\hline 100-0-100u A 22.95 \& ${ }^{300 \%}$ v. D.C. . 22.50 <br>
\hline  \& 15 V A.C.C. $\ldots$ £ $2 \cdot 60$ <br>
\hline  \& 300 V . A.C. . 22.80 <br>
\hline $5 \mathrm{~mA} \ldots \ldots \ldots$ £2.50 \& 8 Meter 1 mA . 22.80 <br>
\hline $10 \mathrm{~mA} . . . .{ }^{\text {2 }}$ 2. 50 \& vU Meter ... $£ 3.80$ <br>
\hline 50 mA ..... $22 \cdot 50$ \& 1 mmp . A.C.* 22.50 <br>
\hline $100 \mathrm{~mA} \ldots . .282 .50$ \& 5 amp. A.C.* 22.50 <br>
\hline $500 \mathrm{~mA} \ldots \ldots .{ }^{2} 2.50$ \& 10 amp. A.C.* £2. 50 <br>
\hline $1 \mathrm{amp} \ldots \ldots .{ }^{\text {2 }}$ 2. 50 \& 20 amp . A.C.* 22.50 <br>
\hline $6^{6} \mathrm{amp}$. ..... £2. 50 \& 30 amp . A.C.* $£ 2.50$ <br>
\hline \multicolumn{2}{|l|}{TYPE MR.65P ${ }^{3} \mathbf{i i n . ~} \times 34 \mathrm{in}$. Fronto} <br>
\hline  \& 10V. D.C.... ¢2. $200^{0}$ <br>
\hline  \& 20V. D.C. .... ${ }^{2}$ <br>
\hline ${ }_{100-0-100 \mu A}{ }^{\text {a }}$ 23-10 \& 150V. D.C. . . ${ }^{\text {E2 } 2.60}$ <br>
\hline ${ }_{5004 \mathrm{~A}}^{2004 \mathrm{~A}} \ldots \ldots .$. \&  <br>
\hline ${ }^{300-0-500 \mu \mathrm{~A}}$ (20.60 \& 50V A.C. .... 82.80 <br>
\hline (1mA \& ${ }^{150 V .}$ A.C.... 28.800 <br>
\hline 10 mA …. 22.80 \&  <br>
\hline $\begin{aligned} & 60 \mathrm{~mA} \\ & 100 \mathrm{~mA}\end{aligned} \cdots \cdots . . .{ }^{\text {che }}$ \&  <br>
\hline 800 mA …… ${ }^{2} 2.80$ \& $50 \mathrm{~mA} \mathrm{A.C.*}$ : $£ 2.80$ <br>
\hline  \&  <br>
\hline  \& 500 mA A. ${ }^{\text {a }}$. 82.80 <br>
\hline  \&  <br>
\hline  \& 10 amp A.C. 2 ER 20 <br>

\hline  \& | 20 amp . A.C." 22.80 |
| :--- |
|  | <br>

\hline \multicolumn{2}{|l|}{"SEW" EDUCATIONAL ME} <br>
\hline \& TYPE ED. 107 <br>
\hline \& 8ize overall 100 mm $90 \mathrm{~mm} \times 108 \mathrm{~mm}$. <br>
\hline \& A new
quality
range
mortng $\underset{\substack{\text { of } \\ \text { coil }}}{\text { hil }}$ <br>
\hline \& crumente lideat for <br>
\hline \& ther bench appitca. <br>
\hline \multicolumn{2}{|l|}{easily accessible to demonstrate internal working.} <br>
\hline \multicolumn{2}{|r|}{ranges} <br>
\hline \& 10 V D.C. ... 25.95 <br>
\hline \multicolumn{2}{|l|}{} <br>
\hline \multicolumn{2}{|l|}{} <br>
\hline \multicolumn{2}{|l|}{} <br>
\hline  \&  <br>
\hline
\end{tabular}

| TYPE MR. 38P $121 / 3 \mathrm{zin}$. square fronts. |  |
| :---: | :---: |
|  |  |
|  |  |
|  |  |
|  | 100V. D.C. .. 22.25 |
|  | 150V. D.C. . 28.25 |
|  |  |
| $1 \mathrm{~mA} \ldots \ldots . .{ }^{2} 2.25$ | 750v. D.C. .. 2 2.25 |
|  | 15V. A.C. 60V. D.C. |
|  | 150V. A.C. .. 22.30 |
|  | 350 V . A.C. .. 22.30 |
|  |  |
| ${ }_{100 \mathrm{~mA}}^{50 \mathrm{~mA}} \ldots \ldots .$. |  |
| TYPE MR.45P 2 in. square fronts. |  |
|  |  |
|  |  |
| ${ }_{2}^{100-0-100 \mu A}{ }^{100}$ |  |
| 5004 A ….. 52.45 | 15V. D.C. . 22.40 |
|  |  |
|  | VU Meter ... 22.70 |
|  |  |
|  |  |
| 800mA 1 1 amp |  |
|  |  |
| "SEW" BAKELITE PANEL METERS <br> TYPE MR. 65 3tin. aquare tronts. |  |
| progine |  |
|  |  |
|  | 50 mmp . .i.. 22.60 |
|  | SV. D.C. .... ${ }^{\text {E2 } 2.60}$ |
|  | 20V. D.C. .: 82.60 |
|  | (150V. D.C. .. 22.80 |
|  |  |
|  | 50v. $\triangle$ C. * $\because 28.65$ |
| $\begin{aligned} & 50 u A \\ & 50-0-50 \mu \mathrm{~A} \end{aligned} .$ |  |
|  | 500 mA A.C. 22.60 |
| ${ }^{5004}$ |  |
| $500-0-500 \mu \mathrm{~A}$ <br> 1 mA |  |
|  | 20 amp A.C. 22.60 |
|  |  |
| $\begin{aligned} & 80 \mathrm{~mA} \\ & 100 \mathrm{~mA} \\ & \cdots \end{aligned}$ | vu Meter … 23.65 |
|  | 50 mV D.C. .: 22.90 |


| TYPE S. 8080 mm Square Fronta |  |  |
| :---: | :---: | :---: |
|  | 100-0-100uA | 23.30 |
| ${ }^{50-0-50 \mu 4}$ [- 83.40 | ${ }^{50004}$ | 83.05 |
| 100 A …... $3 \cdot 40$ | 1 mA | 23.00 |
|  | ${ }_{\text {sov. D. }}$ c.... | ${ }_{23.00}^{23.00}$ |
|  | 300 V . D.C. | 23.00 |
|  | 1 mmp . D.C. | 23.00 |
|  | $\mathrm{b}_{6} \mathrm{mmp}$. D.C. | 23.00 |
|  | 300 V . A.C. | 23.00 |
|  | vu Meter | 23.70 |




## 


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$\mathrm{MP60}$
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MP60/TPD1
MP60/TPD2
HT70.....
HT70/TPD1
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BD1 Chasols
BD2/8AU2/Chassi
BDR/SAU2/P
GARRARD
${ }_{2025} 025$ Stereo
${ }_{2025}^{2025}$ TCiKBHOA
SP25
SP25 III/Acos
SP25 III
III
G800
SP25 III/G800
SP25/M75-8
AR 76
865 B
$8 \mathrm{LA5B}$
8LA5B
SL72B
SL95B
401
ZERO
ZERO
100
ZERO 100 SB
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|  |
| :--- | :--- |


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ZERO 100 M Module/Mo3E
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MP60/M44-7
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GL72/G800
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GL75/G800 GL75G800E,
GOODMANB
TD100/G800E Teak,
TD100/G800E White
LEAK
Truspee d
PHILIS
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GA180/GP200 Tea
GA:308/GP400
GA308 (less cartridge).
OA212/GP400
PIONEER
PL12D (Less cartridge)
PL15C (Less cartridge)
PL41D (Less cartridge).
PL50 (Less cartidge) PL61 (Less cartridge) PLA35 (Le
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\begin{aligned}
& \text { F. \& P. } 87 \mathrm{p} \text {. } \\
& 2 \times \mathrm{Z50/Stereo} 80 / \mathrm{Pzz8} 220 \cdot 25 . \\
& \text { P. \& P. } 37 \mathrm{p} \text {. }
\end{aligned}
$$

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|  | 75 Germanlum Gold Bonded Sub-MIn. Ilike |  |
| U4 | 40 Germanium Tranalitors like OC81, AC128 | 5 |
|  | 60200 ma Sub-Min. 8 gilicon Dlodes |  |
| U 8 | 80 811. Planar Trane K P P like BSY95 |  |
| U 7 | 16 Sil Rectifers TOP-HAT 780 mA VLTG. RANG |  |
| U8 | 30 Bli. Planar Dlodes Do-7 Glass 250 mA 1 |  |
| U-8 | 20 Mixed Yoltages, 1 Watt Zener Diodes |  |
| U10 | 20 BAY 50 charge egrage Diodes D0.7 Glass |  |
| U11 |  |  |
| U12 | 12 Billcon Rectlifere Epoxy 000 mA up to 8 |  |
| U18 | 30 PNP-NPN Sil. Tranmators OC200 \& 28104 |  |
| U14 | 150 Mixed gilicona and Germanlum Diodes |  |
| U15 | 25 SPN 811. Plamar Trans. To-5 like BFY51 |  |
|  | 103 Amp sillean Rectifers Btud Type up to 10 |  |
| U17 | 30 Gerrnariliun PNP AF Transiators TO-5 llke ACY 17 |  |
| U18 | 8 is Amp silicon Rectiffers BYZ13 Type up to 60 |  |
| U19 | 23 Bllicon NPN Transistors like BC108 |  |
|  | 121.5 Amp Billcon Rectifiers Top Hat upy to 1000 P |  |
| U21 | 30 AF. Germanlum Alloy Tranisistors 2 C 300 Series \& OC7 |  |
|  | 30 MADT's like M ${ }^{\text {a }}$ Serles PNP Tranistors |  |
| U24 | 20 Germanium 1 Amp Rectifers GJM Series up to 300 PIV |  |
| U25 | 25300 MHz SPN Sillcon Tranblators 2 N 708 , BSY 27 |  |
| U26 | 30 Fast Switching silicon Diodes like IN414 Micro-MIn |  |
| U27 | 12 NPN Germanium AF Translstors TO-1 like AC127 |  |
|  | 101 Amp BCR's TO-5 cant up to 800 P1Y CRA1/25-800 |  |
| U30 | 15 Plastic Sllicon Planar Trans, NPN 2N2426 |  |
| U91 | 20 sllicon Planir Plastic NPN Trans. Low Nolse Amp 2 |  |
| U32 | 26 Zener Diodea f00mW Do.7 cuse 3 -18 volts milred |  |
| U83 | 15 Plastlc Crae : Arip billicon Rectifera IN400n Serie |  |
| U34 | 30 silicon PNP Alloy Trape. T0-5 BCY 26 28302/4 |  |
|  | 25 Sillcon Plarar Tramitiors PNP TO-18 2 N2906 |  |
| $\pm 36$ | 25 8illion Planar NPS Tranfiftora T0-5 BFY50/51/62 |  |
|  | 30 Sillcon Alloy Trannistors 80-2 PNP OC200, 2 s 322 |  |
|  | 20 Fast switchtng Allicon Trans. NPS MHz 2N:3011 |  |
|  | 30 RF. Germ. PNP Tranisitors $2 \times 1303.5$ TO-6 |  |
| U40 |  |  |
| $\overline{1411}$ | 25 RF' Germantum Transistors TO.b. OC45, NKT72 |  |
| 4 |  |  |
| $\overline{\mathrm{U} 43}$ | 25 Sil. Trans. Pluatic TO-18 A.F. BC113/114 |  |
| U4t | 20 Bil. Trans. Plastic T0-5 BC175/XPN |  |
| U45 | 3 A SCR. T06t up to 60 | 1.10 |

[^13]BI-PAKS NEW COMPONENT SHOP NOW OPEN WITH A WIDE
RANGE OF ELECTRONIC COMPONENTS AND ACCESSORIES AT
COMPETITIVE PRICES-
qUALITY TESTED SEMICONDUCTORS
$\begin{array}{lllll} \\ 2 \mathrm{~N} 2217 & 0.24 & \text { 2N3053 } & 0.19 & \text { 2N4059 } \\ \text { 2N2218 } & 0.22 & 2 N 305 & 0.51 & 2 \mathrm{~N} 4050\end{array}$

ALITY TESTED SEMICONDUCTORS Pak no.

```
20 Red spot
```

16 White gpot R.F. Lransist

4 OC 75 transistors

+ AC 128 translitors PNP high gain
AC 126 tranaistors PNP
OC 81 type transiators
2 AC $127 / 128$ Complementary pairs PNP/NPN 3 AF 116 type transistors
3 AF 117 type translstors
3 OC 171 H.F. type translators ................
7 2N292f Bil. Epoxy trankistors mlxed colour
GET880 low nolse Germanlum t
NPV $2 \times$ BT. 141 \& $3 \times$ BT. 140
4 MADT'8 $2 \times$ MAT 100 \& $2 \times$ MAT 120
3 MADT'S $2 \times$ MAT $101 \& 1 \times$ MAT
40 OC 44 Germanlum transigtora A.F.
4 AC 127 NPN Germanium tranistor
10 NKT transistors A.F. R.F. codel

8 OADS Germanlum diodes sub-mln. IN69
10A PIV Slllcon rectifiers IB425
Billicon transistors $2 \times 2$ N696, $1 \times 2$ N 697 ,

$$
1 \times 2 \mathrm{~N} 898
$$

$$
\begin{aligned}
& \text { Silicon owitch tranifistors } 2 \times 708 \text { NPN } \\
& \text { PNP gilicon tranasistors } 2 \times 2 \mathrm{~N} 1131
\end{aligned}
$$

$$
\begin{aligned}
& \text { PNP Sill } \\
& 2 N 1132
\end{aligned}
$$

2N 1132 .......................
Slicicon NPN transistore 2 N 2969 , 500 MHz
(code P397).

$$
\begin{aligned}
& \text { (colle Par) } \mathrm{Sill} \text { ) }
\end{aligned}
$$

## 2N2905


Q38 7 NPN transiators $4 \times 2$ N3703. $3 \times 2 \mathrm{~N} 3702 \ldots 0.66$

## ELECTRONIC SLIDE-RULE

## The MK slite Rule, deslgned to slmplify Electronic cal culations features the following Balas:- Conversion of Frequency and Wavelength. Calculation of L, C and fo

## ituned Circuits. Reactance and Self-Inductance, Area

$\qquad$

NEW LOW PRICE TESTED S.C.R.'s

|  | NEW | N LO |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IV | 14 | 3 A | 5A | 5A | 7A | 10 A | 16A | 03A |
|  | T05 | 5 T066 | тоб6 | TOG4 | TO48 | TO48 | T048 | T048 |
| 50 | $0 \cdot 26$ | $6 \quad 0.28$ | $0 \cdot 39$ | 0.39 | 0.52 | 0.55 | 0.69 | 1.27 |
| 100 | 0.28 | $8 \quad 0.37$ | 0.52 | 0.52 | 0.55 | 0.64 | 0.70 | 1.54 |
| 200 | 0.39 | $9{ }^{0} 0.41$ | 0.54 | 0.54 | $0 \cdot 63$ | 0.67 | 0.83 | 1.76 |
| 400 | 0.48 | 80.52 | $0 \cdot 62$ | 0.62 | 0.74 | 0.83 | 1.03 | 1.83 |
| 00 | 0.59 | 9 0.83 | 0.75 | 0.75 | 0.85 | 1.07 | 1.38 |  |
| 00 | 0.70 | 0 0.77 | 0.88 | 0.88 | 0.99 | 1.32 | 1.65 | 4.40 |
| SIL. RECTS. TESTED |  |  |  |  |  |  |  |  |
| PIV |  | 00 mA | 750 mA | 1 K | 15A | 3 A | 10A | 30 A |
| 50 |  | 0.04 | 0.08 | 0.06 | 0.08 | 0.16 | 0.23 | 0.88 |
| 100 |  | 0.04 | 0.07 | 0.08 | 0.15 | 0.18 | 0.28 | 0.83 |
| 200 |  | 0.06 | 0.10 | 0.07 | 0.16 | 0.22 | 0.27 | 1.10 |
| 400 |  | 0.07 | 0.15 | 0.08 | 0.22 | 0.30 | 0.41 | 1.38 |
| 600 |  | 0.08 | 0.18 | 0.11 | 0.26 | 0.38 | 0.50 | 2.05 |
| 800 |  | 0.11 | 0.19 | 0.12 | 0.28 | 0.41 | 0.81 | 2.20 |
| 000 |  | 0.12 | 0.28 | 0.16 | 0.33 | 0.51 | 0.70 | 2.78 |
| 1200 |  | - | $0 \cdot 37$ |  | 0.42 | 0.63 | 0.83 |  |

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Coded GP100. BRAND NEW TO-3 CABE. POSSIBLE
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owderse with
ordued 84 or over. BRAND NEW TEXAS
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- Frequency Response 16 FHz to $100,000-1 \mathrm{~dB}$.
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- Sigral to dolse ratio 80dB.
- Overall size $63 \mathrm{~mm} \times 105 \mathrm{~mm} \times 13 \mathrm{~mm}$.

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15 watt ( $\mathbf{r}$.mas.) per channel simultaricously. Thls module latest components and circuit techniques incorporating complete shor circuit protection. With the additlon of the Mains Transformer MT80 $63 \mathrm{~mm} \times 10.5 \mathrm{~mm} \times 20 \mathrm{~mm}$. These units enable you to bultd Alid Sratems of the highest quallty- at a hitherto unobtainable price. Also ideal for many other appllcationa includlng: Disco Aysteme, Publlo
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3 hours to assemble-that's the Sinclait Cambridge pocket calculator from Henry's. Some of the many features
Include Include Interface chlp ${ }^{\text {to }}$ thick-film
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| :---: | :---: |
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Ba/BZX83. From 3.3 volt33 volts 10 p each
1.3 watts $5 \%$ Miniature Tubulars IN4700
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# mavis 

ELECTRONIC CROSS-OVER


The Mavis 3 way electronic cross-over is intended for use prim arily with music and speech amplifying systems. It enables the bass range, mid-range and treble range to be separately controlled The cross-over frequency for each range can be specified if required but will be, in the standard unit, as follows:
Bass roll-off 45 c.p.s.
Bass to mid-crossing point 800 c.p.s.
Mid to treble crossing point 5000 c.p.s.
The unit's output is balanced 600 ohm Line for each channel capable of driving six 600 ohm balance sources. The input to the cross-over is also 600 ohm balance.

GENERAL SPECIFICATION

Size
Weight
Input
Output
Power Requirements
Optional extra

## PRICE - $£ 500$

WW-130 FOR FURTHER DETAILS
$19^{\prime \prime} \times 12^{\prime \prime}$ deep $\times 7^{\prime \prime}$ high (standard $19^{\prime}$ racking)
35 lb .
0 dbm 600 ohm balance
+10 dbm 600 ohm balance
$110 / 230$ volts $50 / 60 \mathrm{c}$. p.s. at 80 watts approx.
Sub plate

## INTRODUCING THE P.A.S. 30/30

PORTABLE MIXER


This mixer has been designed for mobile use in conjunction with high quality audio systems. It has basically 15 fully equalized input channels. plus 2 high level auxiliary input channels. The mixer can be used in two configurations, either 4 track full range output or 2 track output split into 3 channels each track, each channel controlled by an electronic cross-over. The remaining 2 tracks can be used either as full range tracks or re-mixed into tracks $1 \& 2$ as sub-mixers. The mixer also has 2 fully equalized indeThe mixer also has 2 fuls equaizedidependent monitor outputs and drive faclities for an external echo system. There is also an output for use for cueing each channel through for cueing each channel.

GENERALSPECIFICATION
Size
Weight
Power Consumption
hiput Impedance
Output impecance
Input ievel 15 modules Input level auxitiary 2 inputs Output level
Cue output level
Equalisation range
$38 \times 27^{19016} \times 12$ 80 watts approximately 80 watts approximate
600 nhm halancerl 600 ohm balanced -60 dbm
-0 dbm
+10 dbm all channels
-300 milliwatts
$\pm 14 \mathrm{db}$ treble
+20 db mid
$\pm 14 \mathrm{db}$ bass
$\pm 20 \mathrm{db}$ bass peak

| better than - 60 db below full output |
| :--- |
| better than |
| 0 |

Overall noise
PRICE - $£ 6,000$ including freight case WW-131 FOR FURTHER DETAILS

P.A.S. 30/30

This 30 Channel Desk a development of the Mavis four Group 15 Channel Mixer to meet the growing demands of modern P.A. and with forexibility in a four channel quadraphonic setup. and for purpes of live recording it is unique in the fact a multi-track tape machine of up to 30 tracks may be directly coupled to the channels and a 4 track Tape Machine to the mains groups. The Mixer can then at a later stage be used for mixing down to a stereo or quacmaster using the main group outputs.
As a compromise between a P.A. Mixer and a conventional Studio Desk. it ditfers trom the latter in the fact that apart from the usual foldback. echo send. cueing facilities etc.. only eight sub-groups and four main groups are employed when the desk is used in total: the line drives for recording are derived direcily rom each channel. and are fully equipped for patching in an ${ }^{\text {be switched before or after the channels "Eection. }}$
be switched before or after the channels
The desk is built in threa sections. Two wings (which may be used independently in stereo for P.A.) are equipped with fitteen channels each and a complete output arrangement inchuding four groups and a stereo cross-over. The imrd section - the routing tor the two wings and all the extra equipment needed for master quad control and mixdown into four or two track. This is dealt with in Section B of the Instruction Manual.
Using an extra stereo cross-over each wing can drive a quadraphonic P.A. system.

## GENERALSPECIFICATION

The $30 / 30$ Mixer is divided into tour pans. A Cente Desk contain. ing Routing, Foldback. Monitor. Talkback. Echo \& Cueing Combina, Oscillator and Master Quad and Pan facilities with 4 Master Faders. There also can be built-in remote control tacilities for Doiby's Machine Control and Auro Tape Locators. The Centre Desk has 4 group outputs. 4 machine inputs, two foldback outputs and 4 monitor outputs also group braak in and out Two input wings which are mirror images, and contain 15 input

## 11a SHARPLESHALL ST., LONDON, N.W. 1

Tel. 01-722 7161/2/3/4 Telex: London 27655
modules, which have input trim and equalisation, also facilites which enable the module to supply a line level drive for a tape machine with or without equalisation also 4 group outputs which may be combined There are facilities for 2 monitor or effects outputs and one echo output. The module has a switch which controls the output to group off or cue.
There is also a switch which enables a break socket on the rear panel for effects drive and inputs to be switched in and out The fourth unit is the power supply which powers the Centre Desk and two wings and provides a 48 volts Phantom Microphone supply to the thirty microphone inputs.
Wing and Centre Desk Size $\quad 101 \times 82 \times 41 \mathrm{~cm}$. approx.

Weight Wina
Cower Consumption
Input Impedance
Output Impedance
Maximum Input Sensitivity

## Microphone Input

Machine Input Nominal Output Nominal Outpu: Monitor Outpur Monitor Ourput Echo Outpu:

120 Kg approx
100 Kg. app
500 watts.
500 watts. 1200 ohms. Balanced 600 ohms. Balanced
$-60 \mathrm{dbm}$
0 dbm
+10 dbm PA
Odbm Machin
0 dbm Machin
300 milliwatts
300 milliw
+10 dbm
$+10 \mathrm{dbm}$
+10 dm
+10 dbm

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These multi-purpose Auto Transformers, wit large centre aperture, can be used as a Doubl 10 wound current Transtormer, Auto Transforme,
H.T. or L.T. Transtormer, by simply hand wind ing the required number of turns through the c
 give 8 V @ $12 \frac{1}{2} \mathrm{Amp}, 4 \mathrm{~V}$. @ 25 Amp or 2 V . @ 50 Amp ., etc. RT. 100 VA 3.18 turns per volt, $£ 3.00$. Post 35 p .
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M.f. to highest W.D. spec. Auto wound, and tapped $0-130$, $160-200-250$ at least $2 K V A$. Can also be used as $230-240 \mathrm{~V}$. input,
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Will handle liquids or gases up to 7 p.s.i. Forged b.s.p. inlet/outlet. Precision made. British PRICE: 1 1.75. Post 25p. Special
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Suitable for Motors, Drills, etc., etc.
5 amp. 250 Volt. Price 75 p. Post 15 p .

PARVALUX
TYPE:SDI.S/86896/0J
230/250v. A.C. 50 r.p.m. 7 lb/ins
Continuousiy rated Continuously rated, Incl. bas
Post 30 p. New and unused.

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 GLAS TRIACS10 amp. Glass passivated plastic Triac. Latest device from
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Each bank comprises of a change-over
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A/clock. Spindie. 10 mm . iong. 3 mm . dia. Motor only Suitable for above colour whe

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Two Two tull octaves (less
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| 52 | 4-6 | 6M | 60 p | 700 | 35 |  |  |
|  |  |  |  | 700 | -164 | $1 \mathrm{c} / \mathrm{OH}$ |  |
|  | 6-12 | $4 \mathrm{c} / 0$ | 80 p |  | 16-24 |  |  |
| 280 | 8 8-16 | 2 6 | 60 | 700 1250 | 20-30 | 6 clo |  |
| 410 | 10-18 | $4 \mathrm{c} / \mathrm{O}$ | 70 p | 2500 | ${ }_{36-45}$ |  |  |
|  | 12-24 | 2 clo | 60 p | 2400 | 30-48 | 4 c |  |
|  | 16-24 | 4 M 2 B | ${ }^{60} \mathrm{p}$ | 9000 |  |  |  |
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| Three sets clo contacts rated at 5 amps |  |  |  |  |  |  |  |
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 4 BANK 3 C/O PUSH BUTTON Complete with black

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HE723-Digital clock construction kit. An extremely accurate electronic digital clock using 15 integrated circuits and one power transistor. The reference frequency is in fact 50 Hz mains frequency which is an extremely accurate reference source. The estimated loss is about two seconds per year. All construction components are included and a comprehensive fault finding chart is included in the instruction booklet. The clock can be reset at any time by a push button to compensate for power cuts etc.
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MUE7 A very sensitive miniature short wave and VHF receiver kit. Frequency range 25 mHz to 150 mHz . Uses standard batteries- $7 \cdot 5-12$ volts. The ideal companion for kit no. UHS 70 or used on its own for short wave and VHF listening. Will drive a louds peaker if used with kits ES2 or ES3. Price: £2.93. P \& P 20p.
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[^14]
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D800. 800 watt light and drill speed control kit. For light dimming and light duty drill speed control. Price £2.70. P \& P 20p.

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 <br> <br> MARCONI TF 1028 Fr(Low frequency version).}

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Project 80 Active Filter Unit (AFU)
the slimmest,most elegant hi-fi modules ever made


Living with hi-fi takes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round; their size and presentation bring exciting new opportunities to install systems in ways hitherto only dreamed about but never before made practical. You can build a Project 80 system virtually anywhere and it is unbelievably simple to install and connect up. Everything that could possibly be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project $\$ 0$ - compactness, elegantly ultra-modern styling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just a few examples of the system's fantastic versatility.


## Project 80 new modules

## Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes drilled in the wood or plastic on which modules are to be mounted. All the electronics are contained within the $\frac{3}{4}$ " deep front panel! Connecting leads are taken away similarly out of sight. Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders. This enables exceptionally good environmental matching to be obtained. Provision is made for magnetic and ceramic pick-ups, radio and tape in and out. A virtual earth input stage forms part of the up-dated circuitry of the Stereo 80 to ensure the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied

TECHNICAL SPECIFICATIONS
Size $-260 \times 50 \times 20 \mathrm{~mm}$ ( $\left.10 \frac{1}{4} \times 2 \times \frac{3}{4} \mathrm{ins}\right)$
Finish - Black, with white markings
Inputs-Mag.P.U. 3 mV RIAA corrected; Ceramic P.U. 300 mV
Radio 300 mV : Tape 30 mV
S/N ratio - 60db
Frequency range -20 Hz to $15 \mathrm{KHz} \pm 1 \mathrm{~dB}: 10 \mathrm{~Hz}$ to $25 \mathrm{KHz} \pm 3 \mathrm{~dB}$
Power requirements -20 to 35 volts
Outputs $-100 \mathrm{mV}+\mathrm{AB}$ monitoring for tape
Controls - Press button for tape, radio and P.U selection Volume, Bass +12 dB to -14 dB at 100 Hz ; Treble +11 dB to -12 dB at 10 KHz


## Project 80 FM tuner

## smaller, more efficient

A truly remarkable tuner in every way - its unbelievābly compact size its original circuitry - its dependable performance - all this in a boldly designed modern case measuring $85 \times 50 \times 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \times 2 \times \frac{3}{3} \mathrm{ins}$ ). Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made available separately

TECHNICALSPECIFICATIONS
Size $-85 \times 50 \times 20 \mathrm{~mm}$ (approx. $3 \frac{1}{2} \times 2 \times \frac{3}{3} \mathrm{ins}$ )
Tuning range -87 to 108 MHz
Detector-1.C. balanced coincidence, for good A.M rejection
AFC - Switchable, with thermistor control to prevent from drift
One 26 transistor I.C
Twin dual varicap tuning
Distortion $-0.3 \%$ at 1 KHz for 75 KHz deviation
Ceramic filter in I.F. section
Aerial impedance $-75 \Omega$ or 240-300 $\Omega$
Sensitivity - 4 microvolts for 30 dB queeting
Power requirements - 12 to 45 volts

## Project 80 stereo decoder

[^16]

## new constructional techniques

. . .and again Sinclair leads the world

1962 Micro-miniature power amp small enough to stand on a 10p. piece. Slimline pocket receiver smaller than a 20 cigarette pack
1963
1964
1965 Z. 12 power amplifier module: PZ. 3 power supply
1966 Stereo 25 pre-amp/control unit
1967 Micromatic: 0.14 loudspeaker; the first Neoteric
1968 IC. 10. the first ever integrated circuit for constructors' use

## Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80, separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment

## TECHNICAL SPECIFICATIONS

Size $-108 \times 50 \times 20 \mathrm{~mm}\left(4 \frac{1}{4} \times 2 \times \frac{3}{4}\right.$ ins $)$
Voltage gain-minus 0.2 dB
Frequency response -36 Hz to 22 KHz , controis minimum
Distortion - at $1 \mathrm{KHz}-0.03 \%$ using 30 V supply
HF cut off (scratch) -22 KHz to $5.5 \mathrm{KHz}, 12 \mathrm{~dB} /$ oct. slope
L.F. cut off (rumble) -28 dB at $20 \mathrm{~Hz}, 9 \mathrm{~dB} / \mathrm{oct}$. slope

## Z. 40 \& Z. 60 power amplifiers totally short-circuit proof

Either of these entirely new power amplifiers is intended for use in Projec 80 installations although, of course, they are readily adaptable to an even wider range of applications. Both $Z .40$ and $Z .60$ incorporate built in protection against shortcircuiting and risk of damage arsing from mis-use is greatly reduced. Comprehensive instructions are supplied with each of the modules

## Z.40 Technical Specifications

 Size $-55 \times 80 \times 20 \mathrm{~mm}$( $2 \frac{1}{8} \times 3 \frac{1}{8} \times \frac{3}{4}$ ins) 9 transistors Input sensitivity -100 mV
Output -15 watts RMS continuous into $8 \Omega(35 \mathrm{~V}) .30$ watts music power into $4 \Omega(30 \mathrm{~V})$
Frequency response - 10 Hz $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Signal to noise ratio -64 dB
Distortion - at 10 watts into $8 \Omega$
less than 0.1\%
Power requirements - $12-35$ volts

Z 60 Technical Specifications
Size $-55 \times 98 \times 20 \mathrm{~mm}$
( $2 \frac{1}{8} \times 3 \frac{3}{4} \times \frac{3}{3}$ ins) 12 transistors Input sensitivity-100-250mV Output - 25 watts RMS into $8 \Omega(45 \mathrm{~V}) .50$ watts music power into $4 \Omega(50 \mathrm{~V})$
Distortion - typically 0 03\% Frequency response -10 Hz to more than $200 \mathrm{KHz} \pm 1 \mathrm{~dB}$ Signal to noise ratio - better than 70dB
Built-in protection againsṭ transient overload and short circuit
Load impedance $-4 \Omega \min$ : max safe on open circuil

## Sinclair power supply units

the worlds most
advanced unit in its class
Stabilised power supply unit. Re entrant current limiting makes dam age from overload or even direct shorting impossible, a principle never before inorporated in a commercially available constructor module. Normal working voltage (adjustable) 45 V .
R.R.P. $£ 7.98+0.79$ p V.A.T

Without mains transformer PZ. 5 30V unstabilised
R.R.P. $£ 4.98+0.49$ p V.A. T

PZ. 6 35V. stabilised
R.R.P. $£ 7.98+0.79$ p V.A.T


LONDON RD., ST. IVES, HUNTINGDONSHIRE PE174 4 HJ Reg. No. 699483 England

1969 Q. 16 -improved version of Q. 14 : Systems 2000 and 3000 Project 60 launched
1970 IC. 12 : Project 605
1971 Project 60 stereo FM tuner: Z.50: PZ. 8
1972 Improvements to Project 60 with Z. 50 MK. 2 and PZ. 8 Mk. 3 The Executive Calculator: Digital multi-meter 0.30 speaker:

1973 Cambridge Calculator:
PROJECT 80 LAUNCHED
. and next?


| System | The Units to use | Units cost |
| :---: | :---: | :---: |
| Simple battery record player | 2.40 | $\begin{aligned} & £ 5.45 \\ & +54 \mathrm{p} \vee \mathrm{~A} . \mathrm{T} . \end{aligned}$ |
| Mains powered record player | Z.40, PZ. 5 | $\begin{aligned} & £ 10.43 \\ & +£ 1.04 \text { V.A.T. } \end{aligned}$ |
| 30W. RMS continuous sine wave stereo amp | $\begin{aligned} & 2 \times Z .40 \mathrm{~s}, \text { Stereo } \\ & 80 ; P Z .6 \end{aligned}$ | $\begin{aligned} & £ 30.83 \\ & +£ 3.88 \text { V.A.T. } \end{aligned}$ |
| 50W ( $8 \Omega$ ) RMS continuous sine wave de luxe stereo amp | $\begin{aligned} & 2 \times Z .60 \text { s, Stereo } \\ & 80 ; P Z .8 \end{aligned}$ | $\begin{aligned} & £ 33.83 \\ & +£ 3.38 \vee \text {.A.T. } \end{aligned}$ |
| Indoor P.A. | Z.60, PZ.8 | $\begin{aligned} & £ 14.93 \\ & +£ 1.49 \text { V.AT. } \end{aligned}$ |
| Car Radio | $\begin{aligned} & \text { F.M. tuner, } \\ & \text { Z.40 } \end{aligned}$ | $\begin{aligned} & \mathrm{£} 16.40 \\ & +£ 1.64 \mathrm{~V} . \mathrm{A} . \mathrm{T} . \end{aligned}$ |

## From Sinclair <br> the worlds most advanced hi-fi modules

Sinclair Project 80 the ultramomedern non-otrusus en hif

 a shelf could be sufficient


Two Sinclair 0.16 loudspeakers
suitably positioned together
with Project 80 could be
mounted on to a false wall.

Project 80 could be easily
mounted onto a loudspeaker cabinet

A novel application would be to build around the base of a lampshade


When you have seen for yourself how fantastically slim and cleverly designed these modules are. further ways will suggest themselves in which they can become a pleasing part of your particular demestic environment.


## Guarantee

If, within 3 months of purchasing any product direct from us, you are dissatisfied with it. your money will be refunded on production of receipt of payment. Many Sinclair appointed Stockists also offer this guarantee.

Should any defect arise in normal use. we will service it without charge. For damage arising from ris-use a small charge (typically $£ 1.00$ ) will be made.



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Type SS15. These fine motors are easily reversed, starting and stopping in less than $5^{\circ}$ without electrical or $300 z /$ in with $35 v$ at 0.35 amps through winding. For $A C$. (synchronous) aperation at 120 v , 50 Hz . Speed 60 rpm a $60 \mathrm{~Hz}, 72 \mathrm{rpm}$. STEPPING. Holding torque at 60 steps per second- $100 \mathrm{oz} / \mathrm{lin}$. Can be wired to give 100 or 200 step



FAN BLOWER
Precision-built in Germany
Dynamically balanced mains unit ( 2001240 ) continuous rated reversible 60 MA on
run. Size: 5 n " $^{\prime \prime}$ dia. deep. Back plate is tapped



SMITHS RINGER-TIMER Reliable 15 minute times, spring wound divislons, approximately $\frac{y^{\prime \prime}}{2 \prime}$ between divisions. Panel mounting with chrome


GEARED MOTORS "Parvalux" Reversible 100
rom geared motor. Type SD14,
2301250 v . AC. 22 lb/in. ${ }^{2}=1$
 Also limited number only as
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OPEN FRAME shaded pol GEARED MOTORS
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40 AC. 28 rpm . NEW
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 imilar to above, 19 rpm . $£ 2.70$. P. \& P. P. 30 p . \& P. 30p 10 rpm with pressed stee gear case (sim
out slightly smaller), $£ 2.70$. P. \& P. 30 D .


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| :--- |
| 102 | adjustment. Internal AF/RF

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Open frame type table top connections \(£ 25\) carr. \(£ 2\).
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3000 type, $100 \Omega 125 \mathrm{amp}$. make contact $60 \mathrm{p} .2000+130 \Omega 1$ normal $\mathrm{CO} 40 \mathrm{p} .7503 \mathrm{M}, 1 \mathrm{~B}, 1 \mathrm{CO}$ normal contacts 40 p . P. P on all relays
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We can now offer these again in 1.0
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& \text { 18 opal tube. The operating presire is ad } \\
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To control staff and labour on overhead line, underground development and maintenance work. Supervise and test; also all necessary duties to maintain services anywhere in Zambia. Applicants ideally under 45 years of age with minimum 10 years Telecommunications external experience, including overhead line and underground cable construction knowledge.

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Apprenticed mechanical engineers with 5 years experience, ONC or equivalent City \& Guild's certificate. Duties involve running an organisation or GPO headquarters workshop in Ndola. General mechanical, carpentry, paint and light electrical work. Supervisory experience desirable. Emphasis on Mechanical Engineering.

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Applicants should possess 8 years training and practical experience in the servicing and maintenance of SemiAutomatic Message Switching and Tape Relay Equipment and associated peripheral equipment, including TI00 Page Printers and Tl08 Tape Readers. Duties will include the maintenance of such equipment at Zambian Airports.

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Required to introduce a revised maintenance system and assist in its implementation, to instruct staff and compile a maintenance instruction manual; to give occasional lectures on maintenance to engineering trainees.
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These positions involve the development of highly sophisticated communications receivers and transmitters and offer plenty of scope for creativity and challenge. Applicants should have a relevant degree or equivalent and at least 3 years experience of equipment design.

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Duties involve designing and building test equipment for our Production and Test Departments. The activities range from simple jigs for testing small components to complex automatic fault diagnosis equipment. Applicants should have a thorough knowledge of solid state circuitry and integrated circuits and be familiar with radio receivers and transmitters. They must be able to follow a project through from inception to installation, designing printed circuits etc., ensuring high product reliability.

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Multitone Eectric co. Itc.
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## APPOINTMENTS

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An exceptional opportunity occurs for a suitably qualified man to join the new organisation, which will be involved in quantity volume production of high wattage unit audio equipment, as Chief Inspector.

The job will be concerned with all aspects of the inspection. test and troubleshoot functions associated with the flowline production of the units. In addition. close liaison, with the Training Department in iorward planning and training requirements will be necessary.

The successful candidate will hold suitable electronics qualifications, have experience of high volume production methods, be a capable staff motivator and will possess the drive and enthusiasm which the job will demand.

Written applications. setting out brief career details to date and current salary to:

## Thorn CONSUMER ELECTRONICS

## Southall College of Technology <br> Beaconsfield Road, Southall, Middx.

## Two Laboratory Technicians

required for Intermediate \& Advanced Electronics Laboratory \& Radio/Television Laboratory. Experience in maintaining electronic equipment desirable
Salary on scale £ 1521-£1749 per annum inclusive.
Applications to be returned to the Registrar at the College by 19th October.
 exciting atmosphere of Britain's most sought after sun spot. We manufacture the finest Commercial and Entertainment audio equipment and Hotel Service Systems in Europe, and are continually expanding both our comprehensive product range and market coverage.
We are now increasing our Design and Development Team and require a number of young high calibre engineers to initiate, design and complete new products in various markets. Successful candidates will have some experience in RF or techniques (or digital/analogue switching) and should be qualified to at least HNC standard.
Self-motivation and a determination to succeed in a rapidly expanding company is of equal importance to formal qualifications. Salary will be very attractive and will be commerisurate with experience.
For full details please contact
Mr. R.C. Jones, Technical Director,
SNS Electronics Group, 851 Ringwood Road, Bournemouth, Hants.
Telephone Northbourne (02016) 5331/4 Telex 41419

## LONDON BOROUGH OF HOUNSLOW

 EDUCATION DEPARTMENT
## AUDIO AND VISUAL AIDS TECHNICIAN

(T. 1/3)
required at Chiswick Polytechnic, Bath Road, W.4, to join a team of two others to service five departments. Applicants should preferably have experience of modern teaching aids including closed circuit television but persons with an interest in educational technology will be considered. 36 -hour week with some evening duties required. Salary scale $\mathbf{6} 672-£ 1644$ plus fl05 London weighting.
Applications forms from The Principal, Chiswick Polytechnic, Bath Road, Chiswick, W.4. Tel: 01-995 3801, Ext. 535. Closing date: 29th October, 1973.

13117

## TECHNICAL AUTHORS

With electronic, electrical, computer or mechanical experience required by Engineering and Technical Publications (Derby) Ltd., 45 Friar Gate, Derby. Telephone 0332-41261.
$[3164$

## Board of Governors

King's College Hospital.

## Electronics

## Technician

required for an interesting project involving the application of ultrasonics to blood flow measurement. The applicant should preferably have had previous experience in prototype electronic instrument construction and will be expected to assist with clinical measurements when required.
The appointment will be tenable for one year with a good possibility of renewal. Minimum qualification are O.N.C. or final C and $E$ in a relevant subject.
Salary as Physics Technician Grade III.
Application forms obtainable from the Personnel Office. KIng's College Hospital, Denmark Hitl, S.E.25. Tel.: 01-274 6222 Ext. 2728 (Mrs. Child) should be completed and re-
turned as soon as possible.

# COMPUTER ENGINEERS 



## your line to success as a computer service engineer <br> Vacancies exist in the London. Manchester and Liverpool areas for engineers with computer or

 electronic or electro-mechanical experience. In addition a number of senior vacancies exist for engineers (particularly with teleprocessing experience) who wish to develop their existing manage ment skills. The Company pays attractive salaries together with generous fringe benefits including bonus, car allowance and non-contributory Pension Scheme.For further details write or telephone.
COMPUTER FIELD MAINTENANCE LTD. a member of the Computer Worta Trade Group of Companies 99 Bancroft, Hitchin, Hertfordshire Telephone: Hitchin (0462) 51511

## Lancashire County Council Health Department <br> The Health Education Service has a vacancy for a <br> TECHNICIAN (TV/PHOTOGRAPHY)

Grade Tech. 4
Salary £1,530-£1,803
Television is becoming an integral part of audio
visual aids in the provision of visual aids in the provision of health education. Health Education Service requires a technician whose duties will include the technical operation of T.V. equipment. The person appointed will, of course, be knowledgeable in the use of normal projection equip-
ment. It will be an advantage for applicants to have some expertise in camera work and photography.
The post is full time, permanent, superannable and subject to medical clearance.
Application forms obtainable from the County Medical Officer of Health, Serial No. 9693, East Cliff County Offices. Preston, to be returned by the 20th September, 1973.
[3097

## KEEN YOUNG MAN

interested in electronics and music, 18-20 years, to work in London recording, studio. Must have working knowledge of audio elec. tronics. Responsible position with good prospects

Phone Tony Leather on 01-499 7173.
[3186

## MEDICAL PHYSICS TECHNICIAN

 GRADE IIIwith electrical and preferably some mechanical experience required to maintain cobalt, caesium and $x$-ray treatment units at the Royai Marsden Hospital, Fulham Road, London, S.W.3.
The person appointed will also be responsible for the development of radiation measuring instruments and will work in association with the Electronic and Workshop Groups of the Physics and Radiotherapy Departments.
Applicants should hold O.N.C., H.N.C., or similar qualification in electrical engineering or electronics and have at least 3 years' technica! experience to obtain salary on scale $£ 1,602$. E2,076 p.a. plus 6126 London Weighting.
Applications with details of experience and names of two referees to the Deputy Administrator, Royal Marsden Hospital, Fulham Road, London, S.W.3.

## New Forest and Southampton Water with Racal Thermionic Ltd

This is one of the most attractive areas in Southern England providing a variety of excellent recreational facilities.<br>We are a member of the world-wide RACAL Group and are currently seeking a number of

## TEST ENGINEERS

to join our existing team in coping with our planned expansion. Whilst formal qualifications to O.N.C. or City and Guilds standards would be an asset, previous experience in the following areas would be equally desirable.
Analogue
Good working knowledge of Analogue/Linear Electronics to be used on up to date Communications and Instrumentation Magnetic Recording Equipment

Digital
Good working knowledge of Digital Logic Circuitry to be used on up to date Computer Peripheral Magnetic Recording Equipment.
R.F.

Good working knowledge of up to date R.F. Electronics for use on V.H.F. Transmitting Equipment using latest techniques

We offer competitive salaries, good working conditions and a friendly work atmosphere

## Communicate with Racal

If you are interested in any of the above posts, please write or telephone for further information to
The Personnel Officer.
RACAL-THERMIONIC LIMITED,
Shore Road, Hythe, Southampion
Telephone Hythe (04214) 3265, Ext. 66

# Electronics Test Engineers 

Pye Telecommunications of Cambridge and Haverhill have immediate vacancies for Production Test Engineers. The work entails checking to an exacting specification VHF/UHF radio-telephone equipment before customer delivery; applicants must therefore have experience of fault finding and testing electronic equipment, preferably communications equipment. Formal qualifications while desirable, are not as important as practical proficiency. Armed service experience of such work would be perfectly acceptable. Pye Telecommunications is the world's largest exporter of radio-telephone equipment and is engaged in a major expansion programme designed to double present turnover during the next five years. There are, therefore, excellent opportunities for promotion within the company. Pye also encourages its staff to take higher technical and professional qualifications.
These are genuine career opportunities in an expansionist company, so write or telephone without delay for an application form to:
Mrs A E Darkin at
Cambridge Works, Elizabeth Way, Cambridge CB4 1DW.
Telephone: Cambridge 51351.
or Mrs C Dawe at
Colne Valley Road, Haverhill, Suffolk.
Telephone: Haverhill 4422.

THE STOCK EXCHANGE require an additional

## TELEVISION SERVICE ENGINEER

to maintain information display systems.
Applicants must possess appropriate television and radio servicing certificater and must be able to prove their ability as competent Service Engineers by a suitable trade test.
An attractive starting salary is offered. In addition, there is a non-contributory pension scheme, 3 weeks holiday in a full year and Luncheon Voucehers. Applications giving brief details of qualifications and experience should be sent to:

## Personnel Officer,

Council of The Stock Exchange, The Stock Exchange, London EC2N 1HP'

ELECTRONIC SERVICING

A senior electronics service engineer is required to take charge of electronic maintenance in a large teaching hospital. Wide experience in servicing electronic instrumentain the medical field. Applicants should hot be a H.N.C. or equivalent qualification.

This is a medical school appointment with a salary in the range $\mathbf{~ 2 , 2 5 1 - \{ 2 , 8 4 2 . ~ A p p l i c a . ~}$ tion forms can be obtained from the Personnel Officer, Mrs. Gray, St. Thomas' Hospital, 79 York Road, London, S.E.1.
[3185

## TEST ENGINEERS

The leading U.K. manufacturer of high grade TV monitors require Test Engineers for their expanding Test Department.
Situated in the Berkshire town of Maidenhead, the Company offers pleasant working conditions, good salaries and friendly environment. Duties will cover the testing and trouble-shooting of monochrome and colour TV monitors together with other ancillary sophisticated TV broadcast equipment manufactured by the company. Previous experience of TV equipment would be an advantage. Please apply to :

PROWEST ELECTRONICS
Boyn Valley Road,
Maidenhead, Berks.
Maidenhead 29612

## ELECTRONIC ENGINEERS FOR CANADA

A well-known Canadian Company designing and manufacturing computerorientated totalisators requires electronic engineers to meet their continuous expansion.
The likely candidates should be qualified to H.N.C. standards or hold a C.G.L.I. final certificate as electronic or telecommunication technicians, Candidates with equivalent qualifications will also be considered. All candidates must have experience in the development and maintenance of computer systems. Some knowledge of programming would be an advantage. The salary is negotiable depending on qualifications and experience. Interviews will be held in the U.K. Please reply in writing to:

Attention: Managing Director.
WESTERN TOTALISATOR CO. LTD., 102 Elmslie Street,
Lasalle, Montreal 650, Quebec, Canada.
[3179

The Polytechnlc of Central London
Audio Visual Aids Technician £1902-£2202
with experience in maintenance of tape recorders, amplification equipment and C.C.T.V. with the ability to operate both this and 16 mm equipment.
Appllcation form from The Establishment Qfficer, 309 Regent Street, London W1R 8AL. Please quote reference 885.

## WIGGINS TEAPE RESEARCH AND

 DEVELOPMENT LTD.Butlers Court, Beaconsfield, Bucks.

## SENIOR ELECTRONICS TECHNICIAN

Applications are invited for this post to lead a small team engaged in applying electronics to papermaking research and allied processes at the Central R. and D. Unit of an international papermaking group. Based at Beaconsfield the duties will include design, development, manufacture and maintenance of a wide variety of electronic, electro-mechanical and opto-electronic instrumentation.
Applicants should be of H.N.C. standard and have several years development experience with linear and digital circuits. The salary is negotiable in the range $£ 2,000$ to $£ 3,000$. The unit provides excellent working conditions, a pension scheme and luncheon vouchers.
Application forms from Mr. A. W. Massey, Personnel Department. Tel: 04945652.

## GUNNY CORNWALL

LOWER COST OF HOUSING LOCAL AUTHORITY HOUSING
England's Prime Holiday Area. ideal for water sports and outdoor enthusiasts. A civilised area for Environmentalists clean seas, uncrowded roads and fresh air. Unemployed persons qualify for Government Assistance for re-settlement.
We have immediate vacancies for the following Personne in MODERN PRESTIGE LABORATORIES With Exceptional Views: 4-DAY WEEK, EXTRA HOLIDAYS.

JUNIOR MICROWAVE ENGINEER
Familiar with measurement techniques. Experience añd energy more important than qualifications. Work includes projects on millimetre wave components. Salary $£ 1200$ - $£ 1700$.
TECHNICAL SALES ENGINEER
Preferably with experience in sales on microwave instrument and component products. Strong initiative and drive, incentive scheme Leads to Sales Manager position. Salary negotiable.
JUNIOR DRAUGHT SMAN
With experience on small electro-mechanical projects. Jppartunity to learn in well-informed D.O. Accuracy and sound basic knowledge inportant. Workshop experience essential. Salary $£ 1200-£ 1500$
ELECTRONIC ENGINEER
Up to Chartered Standard, 2 vears experience in comf uter interfacing to form basis of new group. Knowledge of R.F. techniques an advantage. Salary negotiable between $£ 2500$ - $£ 3500$

Send full Resume and Salary Required to:
Dunmere Road, Bodmin, Cornwall, PL31 20L Tel: Bodmin (0208) 3161

## WORK AS A RADIO TECHNICIAN

## ATTACHED TO SCOTLAND YARD

You'd be based at one of the Metropolitan Police Wireless Stations. Your job would be to maintain the portable VHF 2-way radios, tape recorders, radio transmitters and other electronic equipment which the Metropolitan Police must use to do their work efficiently. We require a technical qualification such as the City \& Guilds Intermediate (telecommunications) or equivalent.
Salary scale: $£ 1415$ to $£ 1715$ according to age from 21 to 25 , to a maximum £2025 p.a. (plus a London Weighting Allowance of $£ 175$ or £90 p.a.).

Promotion to Telecommunication Technical Officer will bring you more.

For details of this worthwhile and unusual job write to: Metropolitan Police, Room 733 (RT/WW), New Scotland Yard, Broadway, London, SW1H OBG, or telephone 01-230 3122 (24-hour service).


Telecommunications


Ministry of Defence Signals Research and Development Establishment, at Christchurch, Hants require scientists and engineers for work
$\square$ Signal processing and analysis ; optimising use of bandwidth and reducing error rate in communication channels.
$\square$ Assessment of design and performance of communications systems.
$\square$ Computer applications: work on systems of high integrity, and the investigation of real time software structure.
$\square$ Satellite communications: techniques for the provision of multiple access.
$\square$ Electro-magnetic theory : radio wave propagation and aerials.
$\square$ Night vision: work on optical and detector components, the investigation of the man/ machine interface, and the assessment of systems.
Appointment may be made at Senior Scientific Officer. Higher Scientific Officer, or Scientific Officer level.
For Senior Scientific Officer appointment you must have a 1 st or 2 nd class honours degree with at least four years appropriate post-graduate experience. Salary scale $£ 2615-£ 3640$. At Higher Scientific Officer level, qualifications required are a degree, HND. or HNC, with at least 2 years post-graduate experience for the good honours graduate and 5 years for other candidates. Salary scale $£ 2076$ - $£ 2667$.
For Scientific Officer appointment you should have a degree. HND. or HNC and be under 27 years old. Salary scale $£ 1318-£ 2177$.

For further details,
conditions of service, and an application form please write to J. R. Mills, Director, Signals Research Establishment.
Christchurch, Hants, or telephone the Personnel Officer on Highcliffe 2361. ext. 302.

## T.V. Studio Engineer

The Road Transport Industry Training Board has in operation at its Wembley Headquarters, a 3 camera broadcast-quality colour television studio with full telecine and video recording facilities which includes R.C.A. TR 50 and 1 in . Helical Scan systems. We now wish to appoint an experienced studio engineer to join a small team working on the production of training and educational television programmes.

The applicant should not be less than 24 years of age and have a good working knowledge of the above equipment. Salary will be negotiable depending on qualifications and experience. Three weeks holiday, contributory pension and life assurance scheme.
Please send all relevant personal history stating how the above requirements are met, and quoting reference ZH 335 , to:

Mrs. H. M. Brown, Personnel Manager, Road Transport Industry Training Board, Capitol House, Empire Way,
Wembley, Middlesex HA9 ONG.

## LOUGHBOROUGH

TECHNICAL COLLEGE
Principal
F. Lester, B.Sc., Ph.D., F.R.I.C.

Department of Electrical Engineering
LECTURER GRADE I
The person appointed will be required to teach Radio and Television Theory and Practice to Final Certificate level in Technicians' courses. Applicants should have recent trade experience and be fully conversant with broadcast receiving equipment. They should be suitably qualified and preferably be members of a Professional or Technician Institution. Teaching experience and teacher training will be advantageous.
Salary will be in accordance with Scales for Teachers in Establishments for Further Education 1973 (under review), viz., Lecturing Grade, $£ 1,500$ E2,525 (plus $2 \times$ E81 for good Honours), with placing according to qualifications and experience.
Further particulars may be obtained from the Principal, Loughborough Technical College, Radmoor, Loughborough, Leicestershire, LEll 3BT, to whom completed applications should be returned within 14 days of the appearance of this advertisement
[3171

## The Hatfield Polytechnic

TECHNICIAN for Psychological Laboratory
for maintenance and construction of
of electronic and other equipment.
The person appointed will work Senior Technician. Applicants should preferably hold an appropriate intermediate or National Certificate, or City and Guilds qualification, but this is not essential.
Salary scale: $£ 672-£ 1,242$ per annum.
Application form and further details from: The Staffing Officer, The Hatfield Polytecfinic,
P.O. Box 109, Hatfield. Herts. Quote ref: P.O. Box
$379 / W W$.

## LEEDS AND BRADFORD AIRPORT RADIO/RADAR TECHNICIAN

 REQUIREDA vacancy occurs for a Radio/Radar Technician to undertake maintenance of all ground equipment, including radar, CRDF, ILS, etc., on a watchkeeping basis. Radar maintenance experience essential. Salary in accordance with Local Government Grade Technical $5 / 6$ ( $£ 1,926-£ 2,535$ per annum) , commencing salary, depending upon experience and qualifications, between $£ 1,926$ and $£ 2,235$, plus enhanced payment for weekend working. Appointment subject to Local Government Superannuation Acts and medical examination.
Applications, stating age, education, and full details of experience and technical courses attended, together with the names and addresses of two people to whom reference can be made, should be sent to the Airport Director, Leeds and Bradford Airport, Yeadon, Leeds, LSI9 7TZ. Tel: 08737 3391.
[312]

University College Hospital Medical School

Neuropsychology and Metabolism Research Unit,
Friern Hospital, London, N. 11

## ELECTRONICS TECHNICIAN

Electronics technician to assist in the establishment and subsequent running of a new research laboratory. Some experience with recorders, E.C.G., E.E.G. or data processing equipment would be an advantage but not essential.
Applicants should have O.N.C. in electrical or electronic engineering or a similar equivalent qualification. Salary on Whitley Council scale according to age and experience plus London weighting allowance.
Applications to the Secretary, University College Hospital Medical School, University Street, London, WC1E 6JJ. Quote reference F.C.2.
[3147

## ENGINEER

to service
ELECTRONIC ORGANS $B$ \& $O$ AUDIO and C.T.V.
The work is interesting and varied, a Company vehicle is provided and there are vacancies in Birmingham and Manchester.
Telephone or write to:
W. Swan, Jnr. or Mr. D. C. Kay,

84-86 Oldham Streans
ham Street, Manchester M4 ILF
Tel : $061-2283821$

## WALSALL AND STAFFORDSHIRE TECHNICAL COLLEGE <br> JOINT EDUCATION COMMITTEE

Principal: H. Cheetham, B.Sc.(Hon.), C.Eng., M.I.Mech.E., F.I.Prod.E.,

Department of Engineering

## LECTURER GRADE 1

## in

## RADIO AND TELEVISION

 Applicants will be expected to teach the sub-ject of Radio and Television to the Final Year ject of Radio and Television to the Final Year
of the Radio and Television Mechanics Course, of the Radio and Television Mechanics Course, vision Technicians Course, C.G.L No TeleA sound knowledge of the theory and practice of Colour Television Servicing would be very desirable. Applicants should possess appropriate qualifications with teaching and industrial experience.
Salary for the above post will be in accordance with the Burnham Further Education Scale, viz Lecturer Grade I $£ 1,500-62,525$ per annum (under review).
Application forms may be obtained from the Principal, Walsall and Staffordshire Technical College, St. Paul's Street, Walsall WSI IXN. Applications should be returned within a fortnight of the appearance of this advertise ment.
R. D. NIXON,

Secretary to the Joint Education Committee.

# Nigerian Telecommunications Supervisor 

The Shell-BP Petrolcum Development Company of Nigeria Limited has a vacancy for a qualified Nigerian Telecommunications Supervisor.
You should be academically qualified at C.E.I. Chartered Engineer level, be eligible for membership of the Nigerian Society of Engineers or hold any other qualifications acceptable to the Council of Registered Engineers of Nigeria. You must have a minimum of 5 years' total practical experience in at least two of the following:
(a) Multi-channel fixed communications systems
(b) Telemetry
(c) Mobile radio systems

If you are a Nigerian National returning to your country this year and are interested in this position, please telephone Pauline Ford on OI-93+2493 or write, giving details of age, qualifications and experience, to :-

Shell International Petroleum Company Ltd., Recruitment Division (GD), PNEL/4I Shell Centre, London SEi ${ }_{7 N A}$.

## Are you interested in Communal Aerial Television Systems Work? Then read onfurther.....

Due to continued expansion, EMI Service, part of EMI's Electronics and Industrial Operations group of
Companies, has the following vacancies for engineers at Hayes, Middlesex.

SERVICE ENGINEERS
required for bench and field work on
Communal.Television Aerial equipment. Must be capable of diagnosing faults and repairing wide range of aerial amplifying and distribution equipment.

## SYSTEMS PLANNING

## ENGINEERS

for the planning of Communal Television Aerial installations. Previous experience required to be capable of producing practical plans from building details and subsequently setting to work after installation.

Attractive starting salaries. Contributory Pension Scheme. Assistance with removal expenses in appropriate cases.

## WANT TO TAKE THINGS FURTHER

then write or telephone for an application form to
R. N. L. Black, Personnel Department, EMI Limited, 135 Blyth Road, Hayes, Middlesex. oI-573 3888, Ext 2887.

## British Relay Communication and Call SystemsSpeech and Visual

We are acquiring an increasing volume of business in this field including many very long term contracts, and we are seeking to expand the range of our activities. Consequently, we have immediate requirements for engineers with good practical experience and ability in any of the following aspects of the work:-

System Design<br>Planning and Estimating Project Control Installation Supervision Test and Commissioning

Duties are varied and interesting, with frequent opportunities for travel, and for acquiring experience in new fields. Enquiries and application for interviews will be treated in strict confidence, and shoúld be sent to:-

The General Manager, British Relay (Electronics) Limited, 41 Streatham High Road, London SW16 1EP
Tel. 01-677 9681.

## A REALLY WORTHWHILE JOB

(Electrical Test Technicians/Engineers)

GEC Medical Equipment Ltd., based in North Wembley, is a world-wide leader in the manufacture of a wide range of medical diagnostic $X$-ray apparatus which is every day helping the sick and injured throughout the world.
Because of the ever-increasing demand for our equipment both at home and overseas and in order to maintain the high standard of reliability of our product, we need additional electronic test technicians/engineers with practical electrical/electronic experience, preferably qualified to City and Guilds or National Certificate standard.

The work involves testing and faultfinding on a wide variety of medical X-ray apparatus and associated units such as closed circuit television and image intensifiers using both orthodox and specialist test equipment.
There are excellent opportunities for career development. If you would like to know more about working with this Company please write, giving brief career details, or telephone: P. B. Blackmore, Personnel Officer, GEC Medical Equipment Ltd., East Lane, North Wembley, Middlesex, Tel: 019041288.

## University College of North Wales, Bangor. School of Physical and Molecular Sciences. <br> ELECTRONICS TECHNICIAN GRADE 5

Applications are invited for the post of Electronics Technician Grade 5 in the above mentioned Schoo

The successful applicant will be concerned with the servicing and maintenance of existing electronic equipment for research and teaching, and with the development and construction of new specialised equipment.

Applicants should have had several years practical experience in digital and linear solid state electronics, preferably in industry or the to about HNC standard.

Salary at an appropriate point on scale: C1,881 x 72- 62,241 per annum. (Salary Scale at present under review).

Applications (two copies), giving full details of age, qualifications and experience together with the names and addresses of two referees should be submitted to the Secretary and Registrar, University College of North Wales, Bangor, by not later than the 14 th November, 1973.

【3119

## ELECTRONICS ENGINEER

## at

THE OPEN UNIVERSITY
A vacancy occurs due to the setting up of a Psychological Laboratory for an Electronics Engineer. Duties will include the development of equipment for teaching and research such as a mini computer and a digital reaction timer, the maintenance of laboratory collaboration with academic Psychologists and the Electronics Laboratory.
Applicants should have at least 7 years relevant experience and qualifications such as City and quilds or HNC in relevant subjects. The appointment will be made on the Technician Grade 5 scale: $\mathbf{f 1 , 8 8 1 - \{ 2 , 2 4 1}$ per annum.
Further particulars are available from the Acting Personnel Manager (EP2), The Open Kniversity, P.O. Box 75. Walton Hall, Milton Apynes, MK7 6AL. possible.

## ELECTRONIC ENGINEERS

required for equipmerit maintenance and associated engineering projects. Knowledge of professional tape recording equipment, studio operations, or high speed tape duplicating systems is desirable. Salary will be according to age and experience, Please write giving details of age, qualifications, experience and present salary to Chief Engineer, Rediffusion Reditune Ltd., Cray Avenue, Orpington, Kent.

## Computer

## Engineer

## Character Generation

Rediffusion require an Engineer to maintain the above equipment in the London area. TTL experience essential. Knowledge of video circuits preferred.
Good salary plus Company car.

## Telephone:

Mr. Yates 01-385 9472

## Reading Education Committee

 Highdown School, Surley Row, Emmer Green, Reading. Telephone: Reading 475022
## AUDIO VISUAL AIDS TECHNICIAN

required at the above school. Salary on scale K1,644 rising to 61,926 . Extra payment for will be given Minimum age 25. Preference Visual Aids Technician's Certificate. Maintenance, servicing and operation of a wide range
of A/VA equipment including $C T / T V$ and reprographic equipment. Further details and application forms obtainable from and returnable to the Chief Education Officer. 2 Cheapthe appearance of this advertisement.

## UNIVERSITIES OF DURHAM AND LEEDS

BRITISH UNIVERSITIES AIR SHOWER PROJECT

A vacancy exists for a Technician to assist with the installation and operation of a small computer at the British Universities Air Shower Project at Haverah Park near Harrogate. The successful applicant should have a knowledge of digital electronics and/or Computer hardware and should reside in or be prepared to move to the Leeds-BradfordHarrogate area.
Salary will be at an appropriate point on the University Scale for Technicians (at present under review) ( $1,881-\{2,241$ according to age and experience. The appointment will be for two years commencing list December, 1973 with the possibility of renewal of contract
Applications in writing giving full details, age, education and experience together with copies of testimonial's or names and addresses of two referees to the Personnel Office, Science Laboratories, South Road, Durham by 1 st November, 1973. Interviews will be held in Leeds in November, 1973.

## MARCONI INSTRUMENTS LIMITED

## ELECTRONIC TECHNICIANS

are required to work on calibration. fault:finding and testing of telecommunications measuring instruments. The work is varied and will enable technicians with experience of r.f. circuits to broaden their knowledge of the latest techniques employed in the electronics and telecommunications industries by bringing them into contact with a wide range of the most advanced measuring instruments embracing all frequencies up to u.h.f.

Entrants may be graded as Test Technicians. Senior Test Technicians or Technician Engineers according to experience and qualifications. Our servicing and production programme, geared to our recognised export achievement. provides employment combined with prospects of advancement. not only within these grades. but into other technical and supervisory posts within the Company at Luton and St. Albans.

Salaries are attractive and conditions excellent. A Pension Scheme includes substantial life assurance cover provided by the Company. Assist ance with removal may also be given in appropriate cases. Please write or telephone. quoting reference WW178 for application form to


Mr. M. Leavens, Works Manager
Telephone: Luton 33866, or
Mr P Elsip. Personnel Officer
Marconi Instruments Ltd
Longacres. St. Albans. Herts
Telephone: St. Albans 59292
Member of GEC-Marconi Electronics


## Bench Service Engineers

We require engineers with previous experience in TV (Colour and Monochrome). Radio, H-Fi, Tape/Cassette Recorders and V.T.R. products, for our Ashford and Leeds Depots.
Preference will be given to holders of C. \& G. certificates, but sound practical knowledge may outweigh formal qualifications. Basic salary will be based on experience and practical ability.
Fringe benefits include a twice yearly bonus. L.V's. contributory pension scheme and staff purchase facilities. Hours of work 9.00 a.m.-5.30 p.m. Monday to Friday. We would be interested to hear from experienced engineers who wish to work with products which are renowned for their reliability and quality. Please write or telephone with details of past experience and salary to:

The Personnel Manager,
Sony (U.K.) Ltd.
Pyrene House,
Sunbury Cross,
Sunbury-on-Thames,
Middlesex
Tel: Sunbury 87644

OR
Regional Sales Manager,
Sony (U.K.) Ltd.,
Universal Estate,
Wakefield Road, Gildersome,
Morley, Leeds.
Tel: Morley 69421

# RADIO OFFICERS 

## DO YOU HAVE PMG I PMG II MPT <br> 2 YEARS OPERATING EXPERIENCE

possession of one of these qualifies
YOU FOR CONSIDERATION FOR A RADIO
OFFICER POST WITH COMPOSITE SIGNALS ORGANISATION.

On satisfactory completion of a 7 -month specialist training course, successful applicants are paid on a scale rising to $£ 2.527 \mathrm{pa}$; commencing salary according to age - 25 years and over $£ 1.807$ pa. During training salary also by age, 25 and over $£ 1,350$ pa with free accommodation.

The future holds good opportunities for established status, service overseas and promotion.

Training courses commence at intervals throughout the year. Earliest possible application advised.

Applications only from British-born UK residents up to 35 years of age ( 40 years if exceptionally well qualified) will be considered.

## Full details from

Recruitment Officer, Government Communications Headquarters, Room A/1105 Priors Road, Oakley, Cheltenham, Glos GL52 5AJ, Telephone: Cheltenham 21491 Ext 2270

# ELECTRONICS TECHNICIAN 

## FOR PATIENT MONITORING

Applications are invited for a post in a small team installing and maintaining patient monitoring equipment in this newly built hospital. The successful applicant will have an excellent opportunity to acquire experience in the application of electronics in medicine. Facilities include a new well equipped workshop.

Applicants should have at least three years experience in the electronics field, preferably in the construction of Electronic Instruments and possess an ONC or equivalent qualification.

Salary on the scale $\mathbf{£ 1 , 2 0 9 - £ 1 , 5 6 3}+\mathbf{£ 1 2 6}$ London Weighting. Applications quoting the names of two referees, to Mr. C. Hill, Personnel Department, telephone $748 \mathbf{2 0 5 0}$ ext 2992 from whom application form and job description are available.

## SPANISH <br> COMMUNICATIONS <br> EQUIPMENT <br> MANUFACTURER

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CLASSIFIEDS-Continued on p. 141

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CLASSIFIEDS-Continued from p. 137

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## INIEX TO ADVERTISERS

Appointments Vacant Advertisements appear on pages 116-138

| Page | Page | Page |
| :---: | :---: | :---: |
| Aero Electronics Lid 48 | Gabraphone ................................... 34 | Pattrick \& Kinnie ............................... 92 |
| Aero Electronics Lid. Lid. ................... 19 | Gardners Transformers Lid. ................. 2 | Pembridge College of Electronics |
| Acoustical Mig. \& Co. Lid. <br> Acoustico Enterprises Lid. | General Instrument Mieroelectronics Ltd. ..... 53 | Philips Electrical Ltd. ............. 4, 5, 66 |
| Advance Calculations Led. . . . . . . . . . . . . . . . . . . . . 17 | Goldring Ltd. . . . . . . . . . . . . . . . . . . . . . . 31 | Phoenix Electronics (Portsmouth) Lt |
| Aerialite Cables Ltd. . . . . . . . . . . . . . . . . . . 42 | Gothic Electronic Components Lid. .......... 439 | Powertran Electronics ........................... 114 Practical Wireless |
| Amtron U.K. . . . . . . . . . . . . . . . . . . . . . . . . . . ${ }_{46}$ | Grampian Reproducers Lid. ..................... 139 | Premier Radio .................................... |
| Ancom Ltd. . . . . . . . . . . . . . . . . . . . . . . . . . . . ${ }_{3}$ |  |  |
| A.N.T.E.X. Ltd. |  |  |
| Anders Electronics Lid. .........................6, 6 , 26 | Hall Electric Ltd. (London) Lidd. ................... ${ }_{\text {Harris Electronics }} \mathbf{3 8}$ | Quality Electronics ${ }_{\text {Quartz }}^{\text {Crystal Co. Ltd. }}$ Le.................................. 139 |
| A.S.P. Lid. Lid. ................................................... 47 | Harris Harris, $P$ Pectronics (London) Lid. .............................. $139^{139}$ |  |
| Aveley Electric Ltd. . . . . . . . . . . . . . . . . . . . 46 | Hart Electronics (London) . . . . . . . . . . . . . . . . 78 | Racal Amplivox Communications Lid. |
|  | Heath (Gloucester) Ltd. . . . . . . . . . . . . . . . $1000{ }^{23}$ |  |
|  | Henry's Radio Ltd. . . . . . . . . . . . . . . . . . . . 100,10140 | Radtord Acoustics ${ }^{\text {Radio Supplies (Comps.) Ltd. . . . . . . . . . . . . . . . . . }}$. 28 |
|  | Henson. R., Ltd. . . . . . . . . . . . . . . . . . . . . . 139, 140 |  |
| BSR Ltd. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 63 | Hi-Fi Year Book .......................... 69 | RCA Ltd. . . . . . . . . . . . . . . . . . . . . . . . . . . . . 44 |
| B. \& W. Electronics .......................... ${ }^{7}$ | H.H. Electronics | RCS Electronics . . . . . . . . . . . . . . . . . . . . 75 |
| Bart \& Stroud Ltd. ........................... 38 | Hitachi Shibaden (U.K.) Ltd. ................... ${ }_{51}$ | Redifon Telecommunications Lid. ........... 40 |
| Barrie Electronics Lid. . . . . . . . . . . . . . . . . . . . 75 | Hy-Q Electronics ............................... 51 | Rogers Developments (Electronics) Ltd. ....... 75 |
| Bedford Electronics ........................... 112 |  | Rola Celestion Lid. . ${ }^{\text {a }}$. . . . . . . . . . . . . . . . . . . 32 |
| Bell \& Howell Lid. . . . . . . . . . . . . . . . . . . . . . . 62 |  | R.S.C. Hi-Fi Centres Lid. . . . . . . . . . . . . . . . . . . 96 |
| Belling and Lee Ltd. . . . . . . . . . . . . . . . . . . 54 | I.C.S. (Intertext Group) . ........................ ${ }^{51}$ | R.S.T. Valves Lid. . . . . . . . . . . . . . . . . . . . . . 104 |
| Bentley Acoustic Corporation Ltd. ............ 92 | I.L.P. (Electronics) Ltd. . . . . . . . . . . . . . . . . . 94, 95 |  |
| Bentley, K. J., \& Partners Ltd. . . . . . . . . . . . 142 | Integrex Ltd. | Samsons (Electronics) Lid. |
| B.I.E.T. |  | Scopex Instruments |
| Bi-Pak Semiconductors .........................98, 99 |  | Scott, Walker (Imtech Products) ......... 37, 74 |
| Bi-Pre Pak Ltd. . . . . . . . . . . . . . . . . . . . . . . 26 | J.E.F. Electronics . . . . . . . . . . . . . . . . . . . . . . . . 140 | Service Trading Co. ......................... 103 |
| Bias Electronics Ltd . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $14.14{ }^{26}$ | J. H. Associates Ltd. . . . . .id. . . . . . . . . . . . . . . ${ }_{21}$ | Servo \& Electronics Sales Ltd. ................ 97 |
| Bradley, G. \& E. Lid. ...................cover iii | J. J. Lloyd Instruments Lid. .................. 22 | Shure Electronics Lid. .......... 6510710810961 |
| Brandenburg Ltd. .............................. 41 |  | Sinclair Radionics Ltd. ${ }_{\text {W }}$ (Rad $64,65,107,108,109,110$ |
| Britec Ltd. . ................................... ${ }^{3}$ | K.E.F. Electronics Ltd. . . . . . . . . . . . . . . . . . 16 | Smith, Glectronics Group $\square$ |
| Bulgin, A.F.. Ltd. | K.E.F. Products Ltd. . . . . . . . . . . . . . . . 26 | SNS Electronics Group <br> Soka SRL |
| Bull, J. (Electrical) Ltd. ....................... 113 | Kellner-Electronic KG. . . . . . . . . . . . . . . . . . . 105 | Sowter, E. A. Lid. ........................ 140 |
|  | Keytronics Lid. . . . . . . . . . . . . . . . . . . . . . . . . 141 | Special Product Distributors Lid. ............ 37 |
|  |  | Strumech Eng. Co. Ltd. . . . . . . . . . . . . . . . . . . 68 |
|  |  | Studio Electronics .................. . . . . . . . 140 |
| Cambion Electronic Prods. Ltd. ................. . 48 | Laskys Radio ............................ ..... . . 96 | Sugden, J. E., \& Co. Lid. ..................... 56 |
| Cavern Electronics <br> Chilmead Ltd. ......................... . 106, 140, 142 | Lansdowne Recruitment Ltd. . . . . . . . . . . . . . . 112 | Sullivan, H. W., Ltd. ......................... 55 |
| Chiltmead Ltd | Ledon Instruments Lid. ........................ ${ }_{4} 5$ |  |
| Colomor (Electronics) Lid. .................... 82 | Leevers-Rich Equipment Lid. ................... . 48 |  |
| Consumer Microcircuits Ltd. . . . . . . Readers Card | Levell Electronics Ltd. .................. ${ }^{1}$ |  |
| Cosmic Electronics ......................... ${ }^{\text {an }} 48$ | Light Soldering Developments Ltd. ............ ${ }^{\text {L }}$ 56 | Teleprinter Equipment Lid. <br> Telequipment Products (Tektronix U.K.) Ltd .. 58 |
| Cosmocord Ltd. ............................ 20,38 | Lexor Dis-Boards Ltd. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . ${ }^{\text {Linstead }}$ 27 | $\begin{array}{ll}\text { Telequipment Products (Tektronix U.K.) Lid ... } \\ \text { Teleradio Special Products } & 139\end{array}$ |
|  | Linstead Electronics ........................................................ 57 | Telford Products Ltd. ........................... 50 |
| C.T. Electronics Ltd. ........................... 84 | Lyons Instruments Lid. ......................................... 56 | Teonex Ltd. . . . . . . . . . . . . . . . . . . . . . . . . . . 14 |
|  |  | Thorn Radio Valves \& Tubes Ltd. ........... 30 |
| Danavox (G.B.) Ltd. . . . . . . . . . . . . . . . . . . . . 45 |  | E Flectrical |
| Danavox (G.B.) Ltd. . . . . . . . . . . . . . . . . . . . . ${ }_{140}^{45}$ | Macfarlane, W. \& B. ........................... 76 | Turner, E., Electrical |
| Deimos Lid. . . . . . . . . . . . . . . . . . . . . . . . . . . 140 | Marconi Instruments Lid. . . . . ............ cover ii |  |
| Dexter \& Co. . . ${ }^{\text {d }}$ ( 16 | Marshall, A., \& Sons (London) Lid. . . . . . . . . 93 | Valradio Ltd. . . . . . . . . . . . . . . . . . . . . . . . . . . . 30 |
| Dixons Technical CCTV Lid. .................. ${ }_{16} 76$ | Mavis ... . . . . ................................... 102 | Vortexion Ltd. |
| Douglas Electronic Industrier Lid. ............ 138 | McKnight Crystal Co. ........................ 140 |  |
| Dymar Electronics Ltd. . . . . . . . . . . . . . . . . . . 49 | MeLennan Eng. Ltd. . ............................ ${ }_{80}$ |  |
|  | Mills, W. .......................... . . . . . . . . . . . ${ }_{86} 85$ | Watts, Cecil E., Ltd. ................................. 139 |
|  | Milward, G. F. . . . . . . . . . . . . . . . . . . . . . . ${ }_{140}^{86}$ | Wayne Kerr, The, Co. Ltd. |
| Eddystone Radio Lid. . . . . . . . . . . . . 68 | Modern Book Co. . . . . . . . . . . . . . . . . . . . . . . . 140 | Westinghouse Electric S.A. ${ }_{\text {West Hyde Developments Lid. . . . . . . . . . . . . . . . . } 78} 78$ |
| Electronic Brokers Lid. ....... 70, 71, 72, 73, 140 | Mordaunt-Short Ltd. .......... 8 9, $10,11.24,25$ | West Hyde Developments Lirid ................... 104 |
| Electronic Mech. Sub Assembly Co. Lid. ...... 138 | Mullard Ltd. .......... 8, 9. 10, 11, cover iv | Weyrad (Electronics) Ltd. ..................... 97 |
| Electro-Tech. Components Lid. ................. 111 | Multicore Solders Lid. ................... Cover iv | Whiteley Electrical Radio Co. Ltd. .............. 28 |
|  |  | Wilkinson, L. (Croydon) Ltd .................. 111 |
| English Electric Valve Co. Lid. .................. 68 | Nicholls, E. R. . . . . . . . . . . . . . . . . . . . . . . . . . . . 56 | Wilmslow Audio . . . . . . . . . . . . . . . . . . . . . . . . . 139 |
| Est Nuclear Ltd | Nombrex (1969) Lid. .................................... 30 | Yates Electronics . . . . . . . . . . . . . . . . . . . . . . . . 36 |
| Farnell Instruments Ltd. ..................... 18 |  |  |
| Fi-Comp Electronics .......................... . 76 | Oison Electronics Lid. . . . . . . . . . . . . . . . . . . . . . 67 | Z. \& I. Aero Services Lid, .................... 115 |
| Future Film Developments Lid. ............... 104 | Onkyo (J. Parkar) .................................. 67 | 2. \& I. Aero Serv |

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Telex: 25583
A Lucas Company


# Multicore Solder preforms, alittle something for automatic processes. 

## Multicore Preforms.

Multicore precision made solder preforms come in virtually any shape or size.Rings. washers, discs, pellets. and lengths of solder lape - in most soft solder alloys. Designed, with or without flux cores, to make the most of automatic soldering processes.a solder preform is simple and accurate to use. It's just positioned between the parts to be soldered and the temperature of the metal surfaces raised to about $50^{\circ} \mathrm{C}$ above the melting temperature of the solder. The solder preform does the rest. Heating techniques can include gas flame, hot plate.oven conveyor. induction coils.resistance/electrode soldering hot gas and infra-red.

Multicore Solder Preforms just get on with the job. Automatically.


## Our Solder Creams,

 something else again...New Multicore Solder Creams are designed for electronics assembly where quality is vilal. Like manufacturing diodes, for instance. or making a tuner chassis. or soldering thickfilm circuits.

A finely graded solder alloy powder in a thixotropic organic. vehicle.It's often quicker, cheaper. easier and more reliable than other soldering techniques. It's different. It doesn't spit or need stirring. It can be applied by syringe, automatic dispenser or screen printing - giving instant soldering with good spread. strong joints with low contact angles. It can act as a temporary adhesive during assembly and the clear colour flux residue - without solder globules - simplifies inspection.

There are three types of Multicore Solder Cream - one of them may be just what you've been looking for.


| Mulitione <br> Product Ref. | X 1127330 |
| :---: | :---: |
| Alloy Composition | 62/36/2 Si/Ph:Ag |
| Molting Duint or Liguidus ${ }^{\circ} \mathrm{C}$ | 179 |
| Recommended Flow Temperature ${ }^{\circ} \mathrm{C}$ | 239 |
| Typical Application | Low Melting Puint Soldering of silver and mold-plated surfaces |


| XM27298 | XA127328 |
| :---: | :---: |
| 60/40 $\mathrm{Sn}^{2} / \mathrm{Pb}$ | $96 / 4 \mathrm{Sn} / \mathrm{Ag}$ |
| 188 | 221 |
| 250 | 280 |
| General purpose joints requiring | Higher temperature resistant joints. |
| high quality solder cream | Lead free. Higher joint strenglh than $\mathrm{Sn} / \mathrm{Pb}$ |



For fullinformation on these or any other Multicore products, please write on vour company's letterhead direct to: Multicore Solders Limited, Maylands Avenue, Hemel Hempstead. Hertfordshire HP2 7EP.
Tel: Hemel Hempstead 3636. Telex: 82363.


[^0]:    Celestion $\square$
    Loudspeakers for the Perfectionist ROLA CELESTION LTD. DITTON WORKS, FOXHALL ROAD, IPSWICH, SUFFOLK IP3 8JP

[^1]:    AVELEY ELECTRIC LTD.

    Roebuck Road,
    Chessington, Surrey Telex: Avel London 928479

[^2]:    Price 20p. (Back numbers 40p.)
    Editorial \& Advertising offices: Dorset House, Stamford Street, London SE1 9LU.
    Telephones: Editorial 01-261 8620; Advertising 01-261 8339.
    Telegrams/Telex, Wiworld Bisnespres 25137 London. Cables, "Ethaworld, London S.E.1."
    Subscription rates: Home, $£ 4.35$ a year. Overseas, 1 year $£ 5$; 3 years $£ 12.50$ (U.S.A. \& Canada 1 year $\$ 13$, 3 years $\$ 32.50$ ) Student rates: Home 1 year $£ 2.18,3$ years $£ 5.55$. Overseas, 1 year $£ 2.50 ; 3$ years $£ 6.25$ (U.S.A. \& Canada 1 ycar $\$ 6.50,3$ years $\$ 16.25$ ).

    Distribution: 40 Bowling Green Lane, London ECIR ONE. Telephone 0I-837 3636
    Subscriptions: Oakfield House, Perrymount Rd, Haywards Heath, Sussex RH16 3DH. Telephone 044453281. Subscriters are requested to notify a change of address four weeks in advance and to return envelope bearing previous address.

[^3]:    * Sold as Denon recordings outside Japan.

[^4]:    Shure Electronics Limited • Eccleston Road • Maidstone ME15 6AU

[^5]:    *All with Paisley College of Technology.

[^6]:    - Following a majority decision of the I.E.C., the B.S.I. have opted for the rectangular logic gate symbols (not shown in Fig. 3). BS3939 section 21 is currently being amended. - Ed.

[^7]:    1-8 $\quad 100$ p.i.v. rectifiers e.g. $1 \mathrm{~N} 4002,300 \mathrm{~mA}$ or greater
    $9 \quad 12 \mathrm{~V}$ zeners, 2.5 W e.g. $\mathrm{BZX} 70-\mathrm{C} 12$
    $10-1112 \mathrm{~V}$ zeners, 400 mW e.g. BZY88 12

[^8]:    KEYBOARD PERFORATORS for offline tape preparation
    AUTOMATIC TAPE TRANSMITTERS with speeds up to 250 w.p.m.
    MORSEINKERS specially designed for training, producing dots and dashes on tape HEAVY DUTY MORSE KEYS
    UNDULATORS for automatic record and W/T signals up to 300 w.p.m.
    CODE CONVERTERS converting from 5 -unit tape to Morse and vice versa MORSE REPERFORATORS operating up to 200 w.p.m.
    TONE GENERATORS and all Students' requirements
    CREED, MORSE EQUIPMENT, PERFORATORS, REPERFORATORS, TRANSMITTERS, PRINTERS, MARCONI UG6 UNDULATORS, BUZZERS, ALDIS LAMPS, etc.

[^9]:    (DEPT. WW.4), 28 ST. JUDES RD, ENGLEFIELD GREEN, EGHAM, SURREY, Tw 20 OHB
    Hours: 9-5.30, 1.0 p.m. Saturdays.
    Reg. offices at above address
    Phons: Egham 3603 Telex 264476
    Business Reg. No. 1047769

[^10]:    WAYNE KERR type B52I Component bridge. Accurate measurement of C \& R. 655. Excellent order throughout.

[^11]:    Output Power: 100 watts RMS: 200 watts peak music power into $8 \Omega$
    Input Impedance: $10 \mathrm{~K} \Omega$
    Input Sensitivity: ODb ( 0.775 volt RMS)
    Load Impedance: 4-16 $\Omega$
    Total Harmonic Distortion: less than $0.1 \%$ at 100 watts typically $0.05 \%$
    Signal: Noise: Better than 75 Db relative to 100 watts
    Frequency response: $10 \mathrm{~Hz}-50 \mathrm{KHz} \pm 1 \mathrm{Db}$
    Supply Voltage: $\pm 45$ volts
    APPLICATIONS: P.A., Disco, Groups, Hi-Fi, Industrial.

[^12]:    R.s.C. BMI battery elimina-
    tor completely replaces $1 . \delta \mathrm{v}$. tor completely replaces 1. 5 v .
    and
    90 v . Rad 10 batteries

[^13]:    alarge range of technical
    and data books are now
    SEND FOR FREE LIST.

[^14]:    TV2: Telephone amplifier klt. uses induction coil which is fused to back of telephone. Output $2 w$ into 4ohms. Battery operated. Price: £5.54. P \& P 30p.

[^15]:    NF10. LF generator construction kit. A useful 1000 Hz test generator. 12 volt operation. Price: £3.91. P \& P 20 p .

[^16]:    Making the Project 80 decoder separate from the F.M. tuner gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required. This unit gives a 40 dB channel separation with an output of 150 mV per channel. The gallium arsenide light emitting beacon automatically lights up to show when a stereo transmission is tuned in. Designed essentially as an integral part of Project 80 systems, this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception
    Size- $47 \times 50 \times 20 \mathrm{~mm}$ ( $1 \frac{7}{8} \times 2 \times \frac{\text { Bins }}{4}$ )
    One 19 transistor I.C.

[^17]:    ARTICLES WANTED
    CASH AVAILABLE for surplus semiconductor and I.C. Phone 01-452 2583 . 3195 COIL wINDING MACHINES wanted. Also capacitors, paper and polyester, 1 UF upwards, job lots
    ought. FALCON COMPONENTS, 33 Station Road Bexhill-on-Sea. Sussex.
    PLESSEY 4 or 5 button TV VHF Valve Tuners, any quantity. Also Pye Westminster (low band) Mobile. Thomson TV, Beith, Ayrshire. Phone Beith W Anted, all types of communications receivers and test equipment-Details to R. T. \& I. Electroniss, Ltd, Ashville Old Hall, Ashville Rd.
    $W_{\text {anted. Used }}^{\text {Anplifier }}$ bower in good condition audio tionab microphone feed, preferably with for convenuse switching. Also loud hailer type, all-weather

[^18]:    
    
     at a price in excess of the recommended maximum price shown on the cover, and that it ahall not

