# Wireless World 

ELECTRONICS


# Wireless World 

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## Over the Hump

THIS month the 60 th anniversary is being celebrated of one of the most famous and, let us face it, controversial events in the history of wireless communication. It was in December, 1901, that Marconi announced that he had been able to receive at St. Johns, Newfoundland, the succession of triple dots sent out by the $20-\mathrm{kW}$ spark station at Poldhu on a daily schedule from 3 p.m. G.M.T. onwards. The signals were heard at 12.30 p.m., 1.10 p.m. and 1.20 p.m. local time on 12th December and again less distinctly on the following day. On the 14th December Marconi abandoned further experiment owing to the weather, cabled the news of his success to his Company and informed the Press.

The whole project had been carried through under a certain amount of stress-of time (in order to ensure priority over possible rivals) and of weather. Widespread gales had brought down the original Poldhu aerial and a smaller temporary aerial had to be used; the balloons and kites used instead of tall masts at St . Johns had proved to be well nigh unmanageable in the winds then prevailing, and the variation of capacitance with the pitching of the kites prevented the use of the latest syntonic (tuned) receiver. The experimenters did have, however, a variety of sensitive coherers (detectors). These included "microphone" types consisting of loose carbon granules or a mixture of carbon dust and cobalt filings (Marconi's own formulation) and a sensitive self-restoring type, due originally to Tomassina and later used by the Italian navy, in which a globule of mercury was contained between carbon and iron electrodes. All these were used in series with a battery and a telephone earpiece-a far more sensitive arrangement than the earlier "tapper" coherer, relay and morse inker.

The news which Marconi gave to the world was received with astonishment and by his competitors with incredulity. But his confidence was unshaken. Within three months he had set out to repeat the experiment, this time on board the s.s. Philadelphia, outward bound, using this time the syntonic receiver and the self-restoring Italian navy coherer. In daylight signals from Poldhu could be received only up to 700 miles, but at night messages were recorded on tape up to 1,550 miles, and the letter $S$ signals up to 2,099 miles.

So the scientific sceptics, whose calculations of diffraction over a curved surface had predicted failure of any attempt to span the Atlantic, were refuted. The Canadian Government was sufficiently confident to advance $£ 16,000$ for a transmitting station at Glace Bay and by successive increases of wavelength and power during the next year or two
good contact was established at night, but it was not until the summer of 1905 that reliable signals were recorded at Poldhu from Glace Bay, with both stations in daylight. Eventually the Clifden station took over the transmission from this side of the Atlantic and a limited public telegraph service was opened in October, 1907, and an unlimited service from February, 1908, continued until the Clifden station was burnt down in 1922.

Looking back to that boisterous day in 1901 , with our present knowledge of radio propagation and of the trials and difficulties which followed, we must be grateful for the fluke which gave Marcons the optimism and courage to persist. He was extremely lucky. No one then knew that daylight was the worst time to conduct such experiments, but this "mistake" was offset by the fact that he could not have chosen a better year than 1901, which was at sunspot minimum, or a better month of that year, when the absorbing D layer of the ionosphere was to all intents and purposes non-existent. The difficulties in repeating the initial success could be partly accounted for by the rise in sunspot activity in the following years and it was probably not until increasing absorption had been overtaken by the rate of increase of powers and wavelengths, that the fruits of the 1901 experiment were safely gathered.
To commemorate the anniversary the Science Museum, South Kensington, is arranging an exhibition of early Marconi apparatus which will be on view from 13th December.to 25th January, and on the 12th December the Cornish Group of the R.S.G.B. in conjunction with the Newfoundland Radio Club are planning to exchange messages on the amateur bands between Signal Hill and Poldhu. This is a most imaginative gesture, and we congratulate all concerned in advance on what will undoubtedly be a successful and enjoyable event. Would it be asking too much to suggest that on a future occasion, near sunspot minimum, they endeavour with the permission of the P.M.G. to repeat the contact on some wavelength between 1,000 and 2,000 metres, using at the receiving end all the modern techniques, but making the transmitted power as near as can be estimated to that of the original Poldhu? It is unlikely that the powers that be would take kindly to a $20-\mathrm{kW}$ spark but might be lenient towards a temporary c.w. transmitter of equivalent and therefore lower spectral power level. The results would be illuminating and would, we think, give added force to Sir Oliver Lodge's assessment of Marconi's achievement that "it constituted an epoch in human history on its physical side, and was itself an astonishing and remarkable feat."

# THE PILKINGTON COMMITTEE 

## Dear Coumilter

CONCERNED as you are to advise about the future of our broadcasting service you will doubtless have looked closely at its past. And having done so you may have concluded that the technical means by which broadcasting is consummated has been a dominant factor in determining the ends to which it has been put. Assuming this is an agreeable conclusion then it follows that the future of broadcasting will be shaped, in large measure, by the available technical facilities. The acceptance of this important generality should excuse the intromission of one who was a Founding Father of the B.B.C. and who, circa 1925, as the B.B.C.'s first Chief Engineer, planned a technical system for programme distribution which accorded with the ideological policies laid down by Lord Reith.

The creation of the B.B.C. was not, as some have pompously stated, "a wise measure of sociological planning " it was in fact a means to solve an intractable technical problem. The original demands from private enterprise to be given channels for the purpose of advertising greatly exceeded the number which could be used simultaneously without mutual interference. In these circumstances it was decided to grant a monopoly to one prganization which was ordered to do broadcasting "to the satisfaction of the Postmaster General." This organization was to be known as the British Broadcasting Company, later on it became the British Broadcasting Corporation.

A strange beast this B.B.C.! By civil service, out of compromise, tended in its youth by rich uncles, handed over in adolescence to public trustees, obedient to a constitution which defies a basic principle of democracy, it yet became the fervent supporter of free speech; strongly opposed to radio advertising yet making large profits through a publications department, sailing on "heedless of the gulls screaming round its mast," and as sensitive to criticism as a newly fledged debutante, the B.B.C. (may it live for ever!) is quintessentially British; and it came into being solely because of the limitations of communications technology.

## Is a Monopoly Desirable?

But the B.B.C. no longer enjoys a complete monopoly; to the great sorrow of many sincere folk commerce has taken over part of the service (television) and is now insinuating its persuasions to have a similar control over a parallel soundbroadcasting service; it is up to you to recommend what to do, whether to give or to withhold.

In this connection you are in my.opinion asked to answer an unanswerable question, namely, is a vicious principle justified by an admirable practice?

The vicious principle is that which gives a single authority control over a powerful medium of propaganda, the admirable practice is demonstrated by the way the B.B.C. performs its duties.

But suppose that technical advances have abolished the channel shortage, what then! It might be said that, in these circumstances, the justification for the B.B.C. no longer exists and private enterprise might just as well take over. Assuming the abolition of channel shortage I am sure that the abolition of the B.B.C. would be an altogether retrograde step; while the B.B.C.'s institution was fortuitous its demonstrations have earned it a respect which should ensure its continuance.

It is of course possible and moreover, in my opinion, essential to preserve the B.B.C. but not necessarily by a continuance of its sound-broadcasting monopoly. It is my belief that freedom, in all its implications, is more important than the certainty of its abuse; the price of liberty is high but worth paying. If the channel shortage could be abolished or alleviated then broadcasting could be refreshed from more and more contrasted sources and would therefore match the pattern of liberal democracy more closely than it can today.

## Criteria for a Democratic Service

When, some 35 years ago, I was acting as the authority's first Chief Engineer, I laid down certain principles and, with the limited means at our disposal, did my best to see them put into practice. These principles, which I consider to be sound even today, were that the transmission service should be planned so that
(1) everyone receiving the programmes should be assured of a reproduction of them free from interference;
(2) the quality of reproduction, in its faithfulness to the original, should, given a good receiver, be capable of reaching a high standard;
(3) that the listeners (in today's set-up the viewer as well) should be given a wide range of choice between contrasted types of programme. This implies that the claims of minorities are of paramount importance.
It may be of some interest to examine today's broadcasting service in the light of these principles.

## Interference

As to clear reception, reception that is free from interference, my own experience makes me say that while there is a vast improvment now that the v.h.f. service for sound broadcasting has been instituted the very fact that quality has greatly
improved makes the occasional unwanted noise and variabilities that accompany reception the more annoying. Passing motors too often cause plucking fingers to tweak my loudspeaker, passing aeroplanes pulse-modulate reproduction, a local electric motor sometimes imposes a whine while the mains hum drugs the ears. I use a low-priced receiver, which I suppose is typical of that used by a majority and so my judgment is not that of the high-fidelity enthusiast which could well be more favourable. I do not own a television set but often, by courtesy of friends and relations, watch the programmes. From time to time I am annoyed by the sudden intrusion of snow storms bloting out the picture; it could all be better, it has all been worse.

## Quality of Reproduction

Still making it quite clear that I get my reception of sound programmes by the use of a low-priced receiver I would say that the quality of reproduction, while it gives a potent reminder of music in the original does not allow critical judgment of performance. Speech is clear and, apart from occasional interference and continuous hum, the latter being no fault of the sender, all reproduction has a silent background.

The small screen of a television set is its handicap. Because of its more comprehensive technical characteristics the larger cinema screen and the associated tricks of loudspeaker placing and conditioning makes a contrast to television in its more convincing effects upon an audience. This is not to say that television is necessarily second rate, it is to say that its technical limitations impose a greater strain upon the producer to get his effects than were more abundant facilities available.

## Range of Choice Between Programmes

Coming to my third principle, that demanding a greater number of and a greater contrast between the character of programmes, it seems to me that the present lack of choice and the consequent failure to cater for minorities, in anything like the degree I would favour, constitutes the major criticism of the existing set-up.

There is a large and respectable body of opinion which denies the justification for the wide range of choice that I believe to be desirable. Strange, is it not, to hear the same voices deploring the shrinking of the provincial press and at the same time denying the need for local broadcasting? The liberal mind is often open but, when it receives an impression, it is inclined to snap shut and not let go; like those flowers which catch flies. It is wrong to assume that an increase of facility must imply an increase of futility; it can also favour serious causes. Those likely to turn up a scornful nose at what they consider would be the vulgarities which would invade a more provident technical system of broadcasting will be more likely to welcome the suggestion to increase the time given to, for instance, educational programmes. My occasional overhearing and overseeing these programmes has convinced me of their value and, believing as I do, that the most important aim of present day sociological organization should be in furthering education, in the full meaning of that term, I therefore believe that the provision of more channels and their use for education would
be a major contribution to the community's eventual health and happiness.

The B.B.C. has given us a fine example in catering for a minority by its institution of the Third Programme, but it is sad that lack of channels makes it necessary to use the Third Programme wavelength for other purposes. Not that these other rurposes are inferior, they too cater for minorities, but if only there were more channels there would be no reason to dilute one type of programme by another and another by one.

Is it not true that there is constant compromise with respect to the demands of Welsh cultural bodies to possess an exclusive channel for their use, and is it not desirabie that they should?

The vu:garities which wouid doubtless invade other channels would seem to me to be an inevitable consequence of satisfying a majority. Why bauik the fact that the majority is not cu.tured and why not see that the problem of making it more appreciative is much deeper than shoving "cuitchar" at it? The way to abolish the gutter press is to abolish the gutter, not the press.

## Summary of Desirable Characteristics

Summarizing the examination of contemporary practice in the light of my three principles shows that interference, whiie not a serious matter, too often diates the pleasures of looking and listening, that the quality of reproduction given by an ordinary set, while adequate, leaves a good deal to be desired and that the range of contrasted types of programmes available for choice is woefuliy limited. Thus we could make an embracing summary by saying that what is needed is the provision of not only more channels but channels relative'y clear of interference to which are coup.ed receivers which do more justice to the potentiaities of good quaity, inherent in the transmission, than do the average types in use today. How to achieve these aims demands some clear thinking.

## Wire Broadcasting

It is obvious that the use of conductors (wire networks) to join the output from microphone (or camera and microphone) to the househoid receiver has potential merit. Interference can be virtually done away with, aeroplanes cannot moduate waves passing in conductors, induced voltages from domestic machines are of such relatively low intensity as to be dominated by the wanted signais, while the authority responsible for the design and maintenance of the receiver can assure the user good quaity reproduction. A further merit of the use of wires is that the number of channels that can be made available is certainly greater than that provided by radio as it exists today. These are pureiy technical advantages; there are contrasting disadvantages.

## Objections to Wire Broadcasting

Concerned only with technical issues the disadvantage of the use of conducting networks for the dissemination of programmes is that the wires will not reach economically beyond the confines of a densely populated area. Concerned with commercial vested interests there is opposition to wire brcad-
casting by those who profit from the manufacture and sale of radio receivers.

If for no other reason than that portable sets and car radios cannot be served by the wire it would be plain silly to consider shutting down the radio senders. This must set a limit to the oppositions of vested interests, but without doubt it persists. Perhaps it may be lessened by the popularity of the transistor portable.

But some of the arguments advanced against wire broadcasting demonstrate in their futility how fearful its opponents can be. When I was proselytising wire broadcasting a serious writer, whose strictures were published in a respectable technical journal, argued how dangerous it was to suggest setting up a system which could be so easily seized by a dictator, or a would-be one. This argument neglected the point that a pirate radio station could be far more widely heard than transmissions through wires and that once a dictator had power it would not only be the broadcasting services that he commandeered. And as to the use of radio receivers to pick up encouraging messages from abroad, if the country were enemy-occupied it is certain that jamming would be used if the occupying authorities thought it to be worth while.

## Use of the Electric Power Network

R. E. H. Carpenter and I devised, circa 1930, a system for diffusing sound programmes through the electric power network. Fortunately for the Trade, it was found that an Act of 1882 forbade the practice, and in a Parliamentary debate Members demonstrated their loyalty to vested interests and refused to repeal the Act. So much for the liberty of inventors.

I see from your terms of reference that you, as a committee, are required to consider the use of wires for disseminating programmes. Well! Well!

## Use of the Telephone Network

It was suggested, circa 1930, notably by the British Post Office, that the telephone network could be used for distributing programmes. The frequencies of the carrier waves injected into the network were to be within the long-wave band, i.e. those used by radio senders such as Droitwich, Hilversum, Paris. The reception would be available on an ordinary radio set equipped with a long-wave switch which was plugged into the network. It would appear that the Italian authorities already have such a system.

The limitations of the scheme are, of course, that it is available only to telephone subscribers. I should think also that if the subscribers' telephones were served by open-wire conductors that there would be severe interference from long-wave senders of telegraph signals but I am prepared to be wrong. Also, of course, the quality of reproduction would be typical of the ordinary radio set.

## Overlapping in the Absence of Planning

The fact that the wire broadcasting method is chiefly practicable in urban areas makes one ask if it is reasonable to deny a facility to some because it cannot be given to all. The Corporation understandably considers it as a duty to spread its radio service throughout the territory for which it is
responsible, but it is questionable whether this practice need be carried so far as to cause overlapping and, therefore, in a national sense, unnecessary expenditure. In recognizing this problem I suggest in my summing up, the formation of a technical committee of all the talents to plan a national system of programme distribution, taking into account local conditions and modern technology.

## Potentialities of Centrimetric Wave Broadcasting

In contrast to the use of wire networks to increase facility it may be of interest to consider a scheme, impractical, perhaps, but worth describing, relying upon the use of centimetric-wave radio. The telecommunications engineer will agree, other problems inherent in the scheme assumed solved, that the use of centimetric waves to carry programmes would allow the simultaneous diffusion of enough programmes to satisfy the most importunate desire for increased facility. The basic problem would be to avoid shielding, meaning the casting of radio shadows by buildings, hills and so forth. There is an analogy with light. A single source of light suspended above a densely populated area would illuminate some parts but cast shadows in others. A canopy of light over the whole area would disperse the shadows and create a uniform illumination everywhere below it. Centrimetric waves would not, to their advantage, cast such clear-cut shadows as light, but the analogy is a fair one.

According to my suggestion a number of senders, transmitting centimetric waves, would be installed on high buildings, towers, hills and high ground, and would thus spray the houses of an urban area with their radiations. The sending aerials would comprise a number of half-wave types interconnected by folds of conductors not contributing to radiation and would be extremely efficient. Only the receiving aerials would be directional, looking like pudding basins and oriented to catch the strongest signal; they would be coaxially connected to the householders' receiving sets. These aerials would be less conspicuous than those picking up television transmissions today.
Interference would be negligible and quality of a high standard. The simplicity of the senders would make it practicable to leave the installation unattended as is successfully done with more complex equipment.
The disadvantage of the scheme, assuming that the effects of shielding could be wholly overcome (which is doubtful) is that the area over which the signals would be received would be limited to urban areas. But as I read the last sentence it struck me that we need not be too pessimistic about rural areas; on a clear day and standing on the heights of hills and mountains it is surprising how far one can see. Centimetric waves penetrate fog and rain and so the analogy of sight need not deny the practicability of the suggestion to serve rural as well as urban areas by these very short waves. There would be shielding everywhere but in what degree? The experts will give you the answer.

The adoption of centimetric waves would, of course, mean radical and costly changes to our present-day transmission system; perhaps in time the medium- and long-wave stations might be shut down
leaving only those using v.h.f. to serve portables and car radios.
It is said, moreover, that there are more important uses for centimetric waves than their employment in the broadcasting service-one can guess what these more important uses might be and feel that in a sane world. . . . But the world is not, in some aspects, sane.

## Television-Lines and Colour

On other issues the future of television and recommendations about lines and colour must engage your attention-I saw a comparison of pictures using 405 and 625 lines. My impression was that there was a distinction without much difference. It would seem to me to be advisable to recommend the 625 -line system for no better, but no worse reason than that the majority of other systems throughout the world use the greater number of lines-export and all that.

And colour! No sane person would argue that, other things being equal, the introduction of colour to television would be anything but desirable. But other things are not equal and should make one pause.

I was particularly struck by the implication of a polemical question put to me by an American engineer: "Would you," he asked, "pay two to three times more to see a colour film than you would to see a black and white? " I said, "Certainly not" and so drew the obvious conclusion that it was not worth paying two or three times the cost of a normal type of television receiver to get colour reproduction. If it cost no more to produce colour the debate would hinge upon the quality of the picture, but in the circumstances the cost factor is dominant.

## Eckersley's Law

In spite of the dominance of the cost factor I go further in questioning the advisability of setting up a colour transmission service in what I consider to be the present inadequate state of its development. I cite Eckersley's law defining an enjoyment factor. The law is that the product of the value of two numerics one proportional to the fidelity of reproduction and the other to the intrinsic interest in the matter reproduced is equal to a constant. Thus delight in the fidelity of reproduction of a dull programme compensates precisely for its dullness; conversely the outpourings of transcendental talent, or the demonstrations of dramatic interest, heard through distortion, has an enjoyment constant of equal value to that derived from "dull" multiplied by "hi-fi."
The impact of an exciting programme can be considerable, colour or no colour, and if the colour is of poor quality it subtracts from not adds to excellence. I have seen silent films in black and white which have stirred far more emotion in me than the most orchidaceous all-talking, all-singing, all-dancing affairs the impact of which is made by exuberance and elaboration. "The play's the thing" and one's sensibilities can be awakened by simplicity allied with taste without need for adventitious aids. Putting aside considerations of cost and quality the potential delights of witnessing a colour television broadcast from, for instance, the Chelsea

Flower Show can be sympathetically appreciated but, as I see it, the result, in present-day colour, would be an oleographic horror; I would not pay an extra penny piece to see it. So let us wait a while, wait for technical developments reducing cost and improving quality.
These views will be unpopular but may perhaps seem the sounder when my critics are confronted by a dealer whispering the cost of a colour receiver.
In my view the efforts expended in developing colour television would be better devoted first to increasing the area of the television screen. While agreeing that there is a practical maximum to screen size I feel it has not yet been reached. I have listened with respectful attention to theories about subtended angles related to distance separating viewer and picture and have been told that a bigger screen viewed at a larger distance gives no better impression than a smaller looked at from a lesser distance, but I remain unconvinced. Has it not been said that it can be proved from a law of aerodynamics that a bumble bee cannot fly but the bee, not knowing the law, goes on flying?
Improvements in television technology, namely, colour and larger screens demand a wider sideband. Thus my basic plea for more channels, if accepted, would imply a wider total spectrum to contain all broadcast transmissions. If this spectrum were wide enough then there would be room not only for more but for wider channels; and centimetric waves would provide this wider spectrum.

## A Committee of All the Talents

Have I by now succeeded in drawing a single thread of argument through the warp and woof of my discursions? Have I convinced a reader that the potentialities of broadcasting have not yet been fully realized because of the restrictions of its technology? The sheer weight of tradition has so far confined the service within narrow limits and deprived it of a full exhibition of its powers. And if restriction has been inherent in tradition can we dismiss tradition and discover a way to expand the technical means at our disposal so as to give a new stimulus to broadcasting?
Had I my way I would attempt to gather together a technical committee of all the talents and ask it to frame a plan capable of giving a majority of listeners a multi-programme service.
The basic difficulty in achieving a plan is the rivalry of vested interests be they of prestige or profit. I see the B.B.C. is anxious to demonstrate an ability to provide local programmes and estimates that it will cost $£ 30,000$ a year to stir the blood of Bournemouth. Would not a local committee be the right authority to provide occasional local programmes and get the money to run them from local advertising? This in passing, but as an example of rivalry rather than combination.

Is it necessary to be so tender about vested interests be they of commerce or prestige? To form our technical committees we have bodies skilled in installing and running wired systems; the Independent Television Authority could surely subscribe ideas, the B.B.C. stands in its integrity as the most experienced body concerning all aspects of broadcasting, the Post Office could add its quota of experience in the linking of studio output with transmitter input; in sum could not a combination of
authorities frame a national plan of broadcasting to provide a wider range of programme distribution than exists today?

## Conclusions

In all I have said the principle that liberty is of paramount importance rules my thinking. That its abuse is often nauseating is obvious but for the sake of principle must be tolerated. The B.B.C. sets an admirable example and because it must choose it must also refuse; without selection it would be formless. I doubt very much whether a continuing insistence upon uplift lifts up anything, but I passionately support the B.B.C.'s policy. But there
are other policies; let us benefit by them as well.
Open up the channels then and let the flood of opinion, the phases of art, the dichotomies of politics, the shocks of minority opinion be diffused to the public and broadcasting will be the greater for it. But find the best advice how to achieve these ends technically.

Yours sincerely,


## BEGINNINGS OF THE B.B.C.

The History of Broadcasting in the United Kingdom: Vol. 1.-The Birth of Broadcasting. By Asa Briggs. Pp. $425+$ xiii; 50 illustrations. Oxford University Press, Amen House, Warwick Square, London, E.C.4. Price 42s.

This is the first volume of a projected series on the history of broadcasting which will carry the story up to the ending of the B.B.C. monopoly in 1955. The present book covers the background, origins, organization and administration of the service up to the end of 1926, when the British Broadcasting Company became the Corporation.

In writing this volume Professor Briggs has drawn on much unpublished material, including Lord Reith's diary. He has produced a highly detailed and extremely well-documented study which puts order into the confused and confusing story of how broadcasting started.

Even before the B.B.C. was formed at the end of 1922, opposition had come from every conceivable quarter; the press and news agencies, the Services, the entertainment industry, the gramophone companies and others voiced their objections. The opposition "displayed a remarkable variety of fears and prejudices". Just as America had "blundered into chaos". so, it seemed, "British broadcasting was to be forced into a strait jacket". Highly restrictive rules were either proposed or put into effect at various stages; for example, the ban on controversy and on the broadcasting of news which had not already been published in the press. Hours of transmission were severely
restricted and frequent breaks in programmes were required.

There were money troubles as well. The Company was "arbitrarily and inequitably financed", partly by a share of the licence fees and partly from royalties on receivers sold by member-firms. But "piracy" was widespread; for this the public was not entirely to blame, as there was great confusion over the different forms of licence, particularly that for home constructors.

In the face of all these difficulties a lesser man than the first General Manager might well have given up the struggle. "Reith did not make broadcasting, but he did make the B.B.C." He emerges from this book, not as the ruthless autocrat of popular fancy in the mid-1920's, but as the skilful, patient and resilient negotiator and administrator who set the pattern for the public corporation while the B.B.C. was still a commercial company.

If Reith (ably backed on the technical side by P. P. Eckersley, the B.B.C.'s first chief engineer) emerges as the hero of the book, it is pleasing to observe that Prof. Briggs finds no real villain, though clearly he considers the Post Office control to have been at times rather heavy-handed. Of the radio-electric companies who put up the money at the start, he says: "For bearing [the risk of initiating a broadcast service] the 'Big Six' received no concessions. Together they made up a monopoly, but it was a monopoly which enjoyed no monopoly profits and few monopoly privileges. It was the Post Office who did best financially out of the deal ".
H. F. S.

## "RADIO AND ELECTRONIC

THE widening sphere of activities encompassed by the term "radio experimenter" is reflected in the title of the seventh edition of this very popular work. "Radio and Electronic Laboratory Handbook," by M. G. Scroggie, B.Sc., M.I.E.E., is a completely revised and enlarged version of the earlier editions. The no-nonsense approach is retained, and although the discussion is as thorough and complete as in many more self-consciously "long-haired" books, the treatment is considerably more lucid and unobscured by jargon than is usually the case.

The author discusses the setting-up of an experimental laboratory, with suggestions for the choice of relevant instruments. The latest types of measuring instruments are described, with many references to commercial pro-

## LABORATORY HANDBOOK'"

dücts, and several circuits for items of test gear are included. A chapter on the provision and use of standards is followed by discussions of the measurement of circuit parameters, equipment characteristics and signal measurements, at all frequencies up to v.h.f. The recording, examination and interpretation of experimental results are dealt with, and an extremely comprehensive, 80 -page reference section contains most of the information that one never seems to be able to find when it is wanted. New sections include those on digital equipment, and the testing of semiconductors and f.m. receivers.

The book is published for "Wireless World" by Iliffe" Books Ltd., and costs 55s.

New Distortion Criterion discussed in an article under this title by E. R. Wigan in the April and May 1961 issues of Electronic Technology is that the subjective unpleasantness of a distorted sound is assessed from the rate of deviation (with time) of the distorted sound from what the listener considers to be a normal undistorted sound. If we interpret this criterion simply as the rate of change of the difference berween the distorted and undistorted signals, the unpleasantness should increase both with signal frequency and amplitude and both these effects were confirmed (the latter indirectly). The effect on the criterion of the listener's opinion of normality was shown by presenting him with a distorted background. This he took to be normal, thus reducing the subjective unpleasantness of other more distorted sounds. When, with an unknown-language, very little opinion of normality was possible, listeners found it very difficult to make any assessment of the distortion. By changing the background, the memory time for such impressions of normality was found to be of the order of four seconds. A subjective grading of unpleasantness suggested that this was proportional to the square of the rate of deviation from normality. A suggested mathematical criterion which is consistent with these and other results is $C_{t}=n^{2}\left(p_{n}-t\right) \%$ summed for all terms from $n=2$ onwards for which $p_{n}>t$, where $n$ is the harmonic number, $p_{n}$ the percentage amplitude of the $n$th harmonic compared with the undistorted signal, and $z$ the just audible percentage harmonic distortion (under the conditions of the experiment). The rate at which the individual terms decrease due to a finite $t$ can be found by comparing signals of different bandwidth. In this way the minimum audible $500 \mathrm{c} / \mathrm{s}$ distortion was estimated as $0.3 \%$.

Fire and Water, especially salt water, are two of the classic elements which are usually regarded as fatal to electronic apparatus. But this is not necessarily true, as has been recorded in the February 1961 issue of the American Naval Research Reviews. The first step in the process is the immersion of the equipment which has been damaged by fuel oil, smoke and tars from fires or salt water in an emulsion of chemicals containing a hydrocarbon solvent (to remove the "greasy" substances) and water (to dilute and carry away the salt water). A surface active agent holds the solvent and water in emulsion until an oilfouled surface is contacted when the
solvent is released. Ultrasonic agitation is employed to "scrub" the apparatus and, when psimary cleaning is complete, the emulsion is flushed away either by a water sprayer or again by ultrasonic agitation in an immersion rank.

The majority of the flushing water is then blown out by oil-free compressed air and the remainder is removed by a water-displacing compound. This either physically displaces the water or, in deep interstices, combines with it to form a substance known as an azeotrope, which has a lower boiling point than water and, when it evaporates, carries off the water with it. A drying period in a warm "oven" completes the process and the waterdisplacing composition leaves behind a corrosion- and moisture-resistant film. More than 90 per cent of equipment damaged by fire but not actually burned in the U.S.S. Constellation is being recovered satisfactorily by this rehabilitation process.
"Aperture Distortion" occurring in television systems causes lack of sharpness in the picture: the effect is due to the finite width of the camera spot "gradually" moving across a black-white boundary and so "slowly" changing the output signal from black through grey to white. This is corrected by electronic artificial sharpening of transitions, but usually the technique is applied only to the higher frequencies, that is, those representing vertical transitions. In fournal of the S.M.P.T.E. for June 1960 W. G. Gibson and A. C. Schroeder suggest correction for the effect of the aperture in the vertical direction, i.e. on horizontal edges.

Correction is achieved by deriving a "detail" signal by subtraction of adjacent lines from each other (thus leaving only the change that has occurred between the lines), and this signal is mixed with the original signal so as to reinforce the transition. Naturally, this involves the delaying of whole lines of the picture so that the detail signal can be derived and used: quartz-crystal mechanical lines are used, operating at about $30 \mathrm{Mc} / \mathrm{s}$.

The technique does not suffer from some of the defects inherent in correction for vertical edges: for instance, the signal-to-noise ratio is not markedly degraded. Also it has the advantage that it can be used on a composite signal (including colour) so that only one unit is required for all signal sources at a station. The authors hold out the hope that the system may help to reduce the
" lininess" of images by compensating at the transmitter for a dispiaytube spot expanded in the vertical direction.

First Colour TV Receivers available for sale from the Zenith Radio Corporation in U.S.A. use a new colour demodulator system. This employs two "sheet-beam" valves (Type 6 JH 8 ) which have, additional to the usual valve structure focus, accelerator and deflector electrodes and two ancdes. The electron beam, controled in intensity by the first grid, is forced into flat or sheet-like form by the focusing section and speeded up by the positive potential on the accelerator. Potentials applied to the deflectors switch the beam from one anode to the other.
For colour demodulation two colour-difference signals, R-Y and B$Y$, are applied to the control grids of the two valves. These signals are, of course, on the $3.58 \mathrm{Mc} / \mathrm{s}$ subcarrier and are in phase-quadrature ( $90^{\circ}$ difference) with one another. The deflector plates are energized from the local oscillator synchronized with the "burst," or colour phasereference, signal, the $\mathrm{R}-\mathrm{Y}$ stage with a direct push-pull output, and the B-Y with a push-pull quadrature output. Thus the beams modulated with the colour difference amplitudes are switched from one anode to the other of the sheet-beam valves, so giving outputs which are of opposite polarity. The four outputs consist of $B-Y$ and $R-Y$ signals direct and two "negative" signals, from which G-Y is obtained, for application to the c.r.t. control grids. The luminance or Y signal is applied to the c.r.t. cathode. The use of the sheetbeam valves saves two waveform inverter stages which are otherwise necessary to obtain the G-Y signal.

Meter Relay-the MagTrack-introduced by the Weston Instrument Division of Daystrom increases the normally rather low contact pressure produced between a moving meter pointer and a fixed contact pointer both by attaching to the pointer a soft iron bead which is attracted by a magnet attached to the fixed pointer, and by means of a second aiding coil (suitably wound on the same frame as the measurement coil) which is energized on contact. The magnet provides sufficient force ( $\approx 30 \mathrm{mgm}$ ) to break through any insulating film which may have accumulated on the contacts and the additional pressure ( $\approx 2 \mathrm{gm}$ ) provided on contact by the aiding coil moves the flexible contact to provide a wiping action.

# I.T.A. Plan for V.H.F. and U.H.F. 

expanding the Television service and changing lines without duplication

THE Television Advisory Committee in their 1960 report emphasized the importance " of planning the use of Bands IV and V (and when the time comes the re-engineering of Bands I and III) from the start as an integrated whole." They also stated (paragraph 32) "If 625 -line standards were adopted for the higher bands then eventually they would need to be introduced into Bands $I$ and III in order to achieve a single standard. We [the Committee] consider that such a changeover is capable of àchievement given a long-term programme in which the aim and phases are made clear to all concerned and as a consequence have the full cooperation of the broadcasters, the viewers and the radio industry."

The drafting of a detailed plan did not come within the tern's of reference of the T.A.C., but there has subsequently been no lack of proposals and counter-proposals from various authorities and from industry. Some of these have been quite complex and have involved the starting of a third service in Band III, duplication of the existing services in Bands IV and V and an eventual reshuffle of these services between u.h.f. and v.h.f.

The Independent Television Authority, while not dissenting from the T.A.C. recommendations for an eventual change to 625 -line standards, has in the past advocated delay in its adoption, until a scheme could be evolved which, as it was one of the first to point out, avoided "the absurdity that, if we changed the national line system, we must approach the point at which we have emptied our best television frequencies in Bands I and III of all television." It now puts forward a scheme which permits an early start of new programmes on 625 lines (which it now positively endorses as desirable for the future), which avoids any transfer of the two established national services from Bands I and III and which gives a practicable interpretation of the T.A.C. recommendations.
The I.T.A. proposals contained in a pamphlet " $405: 625$. A plan for changing to 625 lines while retaining v.h.f. transmission" issued last month are basically as follows (and we quote):

So that we may continue to use the v.h.f. bands with their substantial advantages and avoid the duplication of services, the Authority proposes for consideration that there should be designated a " 405-625 transition period," during which existing $405-$ line sets would wear out physically. This period would last for seven to eight years. At the end of the period, all transmissions would become 625 -line, and all 405 line transmission would cease. This change would take place on an "appointed day." During this transition period, the following arrangements should be systematically introduced:
(i) At all the existing v.h.f. transmitting stations of both the B.B.C. and I.T.A., "shadow" plant, consisting of new transmitters and aerials arranged for 625-line operation on their appropriate new v.h.f.
channels, should be installed. This would enable the two existing services to be switched simultaneously and without interruption to 625 -line transmission on the appointed day.
(ii) There should be placed on sale from the start new dual standard receivers capable of 625 -line reception in v.h.f. and u.h.f., and also capable of receiving the existing services as they are today transmitted. It should be the plan that these dual standard receivers, by the normal process of replacement, should have supplanted the existing $405-$ line v.h.f. receivers by the appointed day.
(iii) As early as possible, the planning and building of a national network of u.h.f. stations should begin, and arrangements be made for the introduction area by area of one or two new programmes on 625 lines. The network of u.h.f. stations should be progressively expanded to give as much coverage as possible, making the best pace that proved practicable.

The I.T.A. point out that the pace will be governed by the success or otherwise of acquiring sites for the thisty or more u.h.f. stations, additional to those on existing v.h.f. sites, which will be needed to give national coverage. It is estimated that nine of these lie within the boundaries of National Parks and at least five more near areas of natural beauty. These are difficulties which face any extension of the television services into Bands IV and V.
Advantages claimed for the I.T.A. proposals are:
(i) The superior v.h.f. bands are retained in permanent use without interruption for two of the national services.
(ii) The temporary duplication of two services, with the formidable waste of capital, revenue, and manpower involved, is avoided. New v.h.f. transmitters and aerials must, of course, be installed at the existing v.h.f. stations to provide the "shadow" equipment eventually to be used to take over and transmit the present two services on 625 lines on their new v.h.f. channels, but this provision is far less costly than the transfer of these services to a u.h.f. network of stations, only some twenty main v.h.f. stations for each of the present two programmes needing to be so equipped compared with the sixty-four main u.h.f. stations required to give approximately the same coverage.
(iii) The permanently heavier running costs of an all-u.h.f. transmission system are avoided, and so is the liquidation of the v.h.f. stations.
(iv) Duplicated transmissions require standards conversion, which further degrades the picture quality of the already lower grade 405 -line service, and this degradation is also avoided.
(v) The transition to 625 lines could be achieved much more quickly, perhaps in half the time, for the termination of 405 -line transmission would not have to wait for the completion of coverage by the u.h.f. $625-$ line transmissions. The shadow plant could be installed comfortably within seven or eight years. It is difficult to see how the building of the u.h.f. network could take less than twelve to fifteen years.
(vi) The new type of dual standard v.h.f.-u.h.f. receiver produced during the transition would be basically similar to those required by Continental and

Commonwealth countries, so their export would be assisted. The 405 -line facility would simply be left out for export and finally, after the switch to 625 lines, it would be left out for the home market as well.

The design of the proposed new British receiver and the sequence of events in the changeover plan are envisaged in the following terms:

It is, of course, an essential part of the plan for retaining v.h.f. for the main British services that the standard receiver becomes and remains a v.h.f.-u.h.f. set if there are also to be u.h.f. services. The method of transition here proposed requires the incorporation of a small but essential additional piece of equipment in the new dual standard receiver. Over and above its ability to receive, or be converted to receive, the new 625 -line u.h.f. services, the new set must also be capable of receiving, or of being converted to receive, the present two services when, on the appointed day, they are switched to 625 lines on their new v.h.f. channels. Provided that the parameters (the visionsound carrier spacing, the width of the vestigial sideband, the polarity of vision modulation and the choice of frequency or amplitude modulation for the sound channel) adopted for the $625-$ line transmissions in both v.h.f. and u.h.f. are the same, this addition is both easy and cheap to provide, the cost being in terms of shillings rather than pounds. It involves no more than the equipment of the normal v.h.f. turret tuner with two additional "unchristened" channel positions, marked " X " and " Y ," not initially fitted with coils. During a period of a year or more before the appointed day for changing the present two services to 625 lines on their new v.h.f. channels, local dealers would progressively clip in to these "X" and "Y" positions the coils or "biscuits" needed for the two new 625 -line v.h.f. channels to be used in the area of the set. The task of the dealers would be eased by arranging for the "shadow" 625-line transmitters to radiate trade test transmissions on their new v.h.f. channels each morning, instead of the $405-$ line transmitters as at present, this practice being put into operation in all areas a year or so in advance of the appointed day. This is no new process for dealers. They have already experienced it several times on a smaller scale for, when the I.T.A. has opened new transmitting stations, many thousands of so-called multi-channel sets in the new area needed coils to be clipped in to unequipped positions on their v.h.f. turret tuners to enable them to receive the new channel. In these areas the dealers were able to accomplish this task in a few weeks, but no one will wish to underestimate the careful and efficient planning, by manufacturers and dealers alike, necessary to repeat the process on a national scale. Indeed, the feasibility of the plan rests on this particular operation. It would be a substantial alleviation that all receivers sold a few years before the appointed day would already have had their " X " and " Y " positions fitted with the necessary coils by the manufacturers, for the new channels would by then have been made known to them.

Whatever method of transition is chosen, it is little use to pretend that the complications will not be painful for the broadcasters, the manufacturers and the public alike. Equally, whatever method is chosen, the operation will be expensive. These considerations make it all the more important that, when the end is reached, it should be the ideal end, and not the second best end, shortsightedly determined by the choice of what might seem the easiest way out during the transition. History already contains a bitter lesson for us. Our present dilemma is the direct result of the great technical catastrophe of sixteen years ago, when television broadcasting was resumed on 405 lines at a time when refined line systems were perfectly feasible. The choice of the relatively coarse
line system with which we are already technically dissatisfied then seemed the easiest way out. It will now cost many millions to correct matters. It would be tragic to fall into a second error by finding ourselves, at the end of the period of transition, with a broadcasting system that was still technically defective. If we are to make the change at all, we should steadily ask what it is we wish to have in the end, and we should accept whatever transitional complications are necessary in order to reach it. This end, it is the argument of this present paper, is a 625 -line broadcasting system making full and continuous use of the v.h.f. bands, in which the two main services have been uninterruptedly contained.

We do not go all the way with the I.T.A. in condemning the restarting of television in 1946 on 405 lines. Nor are we convinced that the advantages of a change now to 625 lines will outweigh the disadvantages of the "expensive and painful complications" which will bear heavily on all concernednot least on the public. It is true that we might have adopted a higher standard in 1946, but we could not have been expected to guess that the figure of 625 would be the one to find favour. If any other standard than 405 had been adopted it would have been the American 525, the only other higher standard then in the running.

Whatever may be the final conclusions about our line standards, we have no doubts about the desirability of extending the television services by the provision of more channels, the case for which has been so ably stated by Capt. Eckersley elsewhere in this issue. This will certainly cost a lot of money, and if the need for larger pictures and a higher line standard are part of the bargain, then there can be little doubt that the I.T.A.'s latest proposals provide the best solution so far advanced.


FRAME-GRID AERIALS?-These five helical aerials have been designed by Cossar Radar \& Electronics and are for use by the War Office at the Guided Weapons Trials Establishment on the coast of Anglesey. They will operate in the frequency ronge $100-400 \mathrm{Mc} / \mathrm{s}$ employing circular polarization and will be for telemetering missiles.

# AIRBORNE HOMING SYSTEM 

USE OF A PHASE-SHIFTING NETWORK

BY H. M. BOYLE,* B.Sc., A.Inst.P.

THE principle of measuring phase difference to provide direction finding information is well known. A new method for achieving the measurement was developed by Johnson and Berestord of R.A.E. in 1952 and is covered by Brtish Parent No. 787,894 . It involves the use of a phase-shifting network between two aerials used for the reception of the transmission on which it is required to home. Subsequent developments by the Plessey Co. have used the phase-shifting network principle in airborne homing equipments but the associated circuitry, both of the phase-difference measurement and of the equipment as a whole, has been much simplified and is described below.


Fig. 1. Circuit for modulating a receiver carrier to provide homing information

The method of phase measurement takes the following form, the circuit being shown in Fig. 1. The doodes MR1 and MR2 are made to conduct alternately by the application of a low frequency switching waveform. The r.f. output can therefore be expressed as:

$$
\begin{align*}
& \cos (\omega t)+\cos \left(\omega t+\phi+\phi^{\prime}\right)- \\
& \text { Diode MR2 } \operatorname{conducting}  \tag{1}\\
& \cos \left(\omega t+\phi^{\prime}\right)+\cos (\omega t+\phi)- \\
& \text { Dode MR1 conducting } \tag{2}
\end{align*}
$$ where $\omega$ refers to the carrier frequency of the received transmission, $\phi$ is the phase delay of the signal at the port aerial relative to that at the star-

[^1]board aerial and $\phi^{\prime}$ is the delay contributed by the phase shifi network. This results in a square wave modulation of the carrier at the switching frequency and at a depth depending on $\phi$. When $\phi=0$ the two expressions abuve are equal and the modulation depth is zero. For any other value of $\phi$, positive or negative, the modulation depth will increase, and the modulation is in phase, or in anti-phase, with the switching waveform according to the sign of $\phi$. Thus the phase difference has been transformed into a modulation of the carrier and homing information provided. This can be seen by expanding expressions (1) and (2) above:
\[

$$
\begin{align*}
& \text { i.e. } 2 \cos \frac{\left(2 \omega t+\phi+\phi^{\prime}\right)}{2} \cos \left[-\frac{\left(\phi+\phi^{\prime}\right)}{2}\right]  \tag{3}\\
& \text { and } 2 \cos \frac{\left(2 \omega t+\phi+\phi^{\prime}\right)}{2} \cos \left[-\frac{\left(\phi-\phi^{\prime}\right)}{2}\right] \tag{4}
\end{align*}
$$
\]

These can be rewritten as:

$$
\begin{equation*}
A \cos \left[\frac{\left(\phi+\phi^{\prime}\right)}{2}\right] \tag{5}
\end{equation*}
$$

and $A \cos \left[\frac{(\phi-\phi)}{2}\right]$
For negative values of $\phi$ expressions (5) and (6) may be written as:

$$
\begin{equation*}
A \cos \frac{(-\phi+\phi)}{2} \ldots \tag{7}
\end{equation*}
$$

and $A \cos \frac{(-\phi-\phi)}{2}$
which become:

$$
\begin{equation*}
A \cos \left[-\frac{\left(\phi-\phi^{\prime}\right)}{2}\right]=A \cos \frac{\left(\phi-\phi^{\prime}\right)}{2} \tag{9}
\end{equation*}
$$

and $A \cos \left[-\frac{\left(\phi+\phi^{\prime}\right)}{2}\right]=A \cos \frac{\left(\phi+\phi^{\prime}\right)}{2}$
These expressions are (5) and (6) reversed and the phase of the modulation is therefore changed for negative values of $\phi$.
For completely satisfactory operation of this circuit in the u.h.f. band ( $225-410 \mathrm{Mc} / \mathrm{s}$ ) several points were investigated and a summary of these, and their solution, is now outlined.
It can be seen that it is essential to maintain the symmetry of the circuit, so that the indication of heading zero is not affected. At these frequencies, lead inductance and stray capacitance assume major importance and it was with a view to controlling these and maintaining symmetry that a "block" form of assembly. was adopted. This method has the added advantage that the block acts as its own


Fig. 2. Practical assembly of the circuit in Fig. 1
jig during assembly. Briefly, the resistors $R_{1}$ and $R_{4}$ and the diodes $M R_{1}$ and $M R_{2}$ are mounted in holes bored in a block of aluminium, the hole dimension being chosen to give an air-spaced transmission line, in association with the components and their leads, to give optimum performance over the band. The delay line consists of a brass horseshoe embedded in a dielectric of glass fibre laminate and spaced by the dielectric from the ground plane (the aluminium block) to give the required characteristic impedance. The assembly is shown at Fig. 2.
The choice of diode in itself constituted a major problem at the time (1956). The requirements are low forward resistance and high back impedance. The Transitron T19G diode was chosen finally, having a mean forward dynamic resistance of $6 \Omega$ and a minimum back impedance of $400 \Omega$ (capacitive). Germanium diodes were found more suitable than silicon because of their lower cut-on voltage in the forward direction, which eases the requirements for the switching waveform. Failure to cut the diode on quickly will result in "holes" in the carrier at $10 \mathrm{kc} / \mathrm{s}$, which were considered undesirable.
The choice of $\phi$ and $\phi^{\prime}$ is affected by a number of factors, but in practice the aerial spacing was chosen to be 20 cm , which gives $\phi$ a value of approximately $96^{\circ}$ at $400 \mathrm{Mc} / \mathrm{s}$ at $90^{\circ}$ heading. The delay $\phi^{\prime}$ was chosen as 13.6 cm , giving $65^{\circ}$ at $400 \mathrm{Mc} / \mathrm{s}$.
Some points of interest are worth noting before leaving this part of the circuit.
The switching frequency, although uncritical, is chosen to be approx. $5.0 \mathrm{kc} / \mathrm{s}$, which is outside the normal audio pass band of the associated receiver.
The circuit introduces a certain r.f.

Fig. 3. Block diagram of homing system
loss which is of no importance except in areas of weak signal. If it is desired to restore the signal to its previous level, an r.f. amplifier of good noise figure must be incorporated. This was done in one of the Plessey developments, the amplifier being tunable and controlled by the associated transmitter-receiver.

It should be noted that the circuit in no way affects the normal intelligence on the carrier and that only very heavy modulation will affect the homing function, resulting in a loss of homing sensitivity.

The complete system is shown in Fig. 3. The $5 \mathrm{kc} / \mathrm{s}$ modulated carr er is passed into the associated receiver for demodulation. The demodulated $5 \mathrm{kc} / \mathrm{s}$ square wave is taken out via a stage provided specifically for the purpose and passed back to the Homing Unit, where the signal is fed to a phase sensitive bridge. The $5 \mathrm{kc} / \mathrm{s}$ switching waveform is also applied to the bridge, via a delay, to compensate for the phase delay suffered by the signal waveform in passing through the receiver. The resulting d.c. ouput is proportional to the amplitude of the signal wave form (provided that the signal waveform is small compared with the switching waveform) and of a polarity depending on the sign of $\phi$. The d.c. output is applied to a Standard Service I.L.S. Indicator (Type 7 or 9024 ) for display in the pilot's cabin.

The Homing equipment derives its power supplies from the associated receiver and is controlled by the receiver's control unit. The power requirements are small, being 0.37 A at 28 V for heater supplies and approx. 12 mA at 225 V h.t.

It can be seen that having chosen $\phi^{\prime}$ to be satisfactory at $400 \mathrm{Mc} / \mathrm{s}$, the phase delay introduced by the delay line is less at $225 \mathrm{Mc} / \mathrm{s}$. In addition, the fixed spacing of the port and starboard aerials means that for a given heading error, the value of $\phi$ is also less at the lower frequencies than at the high. Thus there is an inherent change in homer sensitivity (d.c. output versus heading error) over the band. Since it is desirable to have a sensibly constant output for a particular heading, regardless of operating frequency, a potentiometer has been fitted to the receiver, controlled by the frequency setting elements of that receiver. This potentiometer is used to control the gain of the $5 \mathrm{kc} / \mathrm{s}$ signal amplifier in the Homing Unit, as the carrier frequency is varied.

It should be borne in mind that the system just described is not necessarily restricted to the u.h.f. band, although modifications to the delay line length and the aerial spacing would be required.

# WORLID OF WIRELESS 

## I.E.E. and Electronics

THE scheme put forward some months ago by the I.E.E. for the reorganization of the Institution to give a stronger emphasis to its "electronics" activities has now been approved by its members. Privy Council permission has to be sought but, in the meantime, plans are going ahead for the introduction of the scheme next October.

The present four Specialized Sections (Measurement and Control, Electronics and Communications, Supply, and Utilization) will be replaced by three Divisions: (i) Electronics, (ii) Power, and (iii) Science and General. Each Division will work through about ten relatively specialized Professional Groups. The number and scope of these groups "can be modified quickly to reflect any change of emphasis in the technological scene."

## Dual-Standard TV in Eire

TELEFIS EIREANN (Irish Television Service) as already announced will ultimately adopt the 625line television standard and their first two stations will therefore be equipped for both 405-and 625line transmissions. They have placed a $£ 175,000$ contract for four 625 -line television transmitters and associated equipment with the Pye Group. At two of the Eire stations, at Mount Kippure, near Dublin, and at Truskmore Mountain in Co. Sligo, a "combining unit" will be used to allow radiation of 405and 625 -line transmissions simultaneously from a "dual standard" aerial. The other two 625 -line equipments ordered are for stations at Mount Leinster, Co. Carlow, and Mullaghanish Mountain, Co. Cork. Proposed date for the commencement of 405 line programme transmissions from the television station at Kippure is December 31st. Test transmissions are being radiated in Channel 7 with horizontal polarization, between the hours of $11.30 \mathrm{a} . \mathrm{m}$. and 1 p.m., also from 3 p.m. to 5 p.m. and 6.30 p.m. to $7 \mathrm{p} . \mathrm{m}$.

## "Random Radiations"

THIS is the first issue since January 18th, 1935, in which "Diallist's" contribution "Random Radiations" has not appeared. As a result of ill health, and at his own request, he has felt obliged to relinquish the task of sustaining this regular feature.
As some readers may know, "Diallist" is the pen name of Major R. W. Hallows, M.A.(Cantab.), M.I.E.E., who, in addition to his regular contribution to Wireless World, has also frequently written under his own name. One of his special interests is batteries, and he was, for some 30 years, European consultant to the Burgess Battery Co. Inc.
Throughout the war Major Hallows, who is 76, was in the Royal Artillery and was for some time Chief Instructor, Radar, at the 6 th A.A. Group School. He is the author or joint author of a number of books, including "The Oscilloscope at Work," "Introduction to Valves" and "Radar Simply Explained."

## Pay TV Tests?

A PLEA to the Postmaster General for a licence to allow relay undertakings to conduct an experimental field test of Pay TV by wire was made by Barry King, chairman of the Council of the Relay Services Association, at the Association's annual luncheon on November 14th, at which Miss Mervyn Pike, Asst. P.M.G., was principal guest. Miss Pike had herself referred to the potentialities of Pay TV in her speech. The number of homes in this country served by wire television systems is now over 500,000 ; about $95 \%$ of all subscribers to television and sound relay systems in the U.K. are served by members of the Association.

## Instruments for Export

SOME 150 delegates, representing over 70 scientific instrument manufacturers and a number of Government research establishments, attended the tenth annual convention of the Scientific Instrument Manufacturers' Association at Eastbourne from November 15th-18th. The theme was "export." After the opening session, which was addressed by Sir Charles Fitton, past president of the Institute of Export, and representatives from the goverments of the U.S.A., Swederi and Australia, the delegates were free to attend the meetings of the three specialized panels (technical, marketing and economics) which ran concurrently.

The first session of the technical panel was addressed by G. W. A. Dummer, of the Royal Radar Establishment, on the subject of design for export. By way of introduction he mentioned that $6.3 \%$ of all equipment delivered to the R.R.E. under contract was outside tolerance or not working. Manufacturers may be interested to learn that the results of the R.R.E.'s specialized tests on a variety of apparatus are readily available.

Other sessions of the technical panel dealt with the "requirements of the overseas user," "problems of overseas manufacture " and "after sales service."
B.B.C. Portsmouth Exhibition.-The B.B.C. is staging a public exhibition at the Guildhall, Portsmouth, from November 29th to December 2nd, from 12 noon to 10 p.m. daily. B.R.E.M.A. are supporting the show and nineteen manufacturers will be exhibiting their radio and TV receivers. The B.B.C. is to relay TV and sound programmes direct from the Guildhall and the f.m. signal from Rowridge will also be provided for demonstrating radio.
I.T.A. Selkirk Station.-A temporary 200 ft mast at the Independent Television Authority's Selkirk station will come into operation at the beginning of December. A permanent 750 ft tower is being built which it is hoped will become operational not later than March 1962. The signal radiated from the temporary mast will be on Channel 13 , vertically polarized, and e.r.p. will be 4 kW , to be increased to 25 kW when the permanent mast is used.

Microwave Valves Conferences.-September 1963 has been chosen as the date for a Conference on the Design and Use of Microwave Valves and an associated scientific exhibition, which is being organized by the Electronics and Communications Section of the Institution of Electrical Engineers. It will be held at Savoy Place, London, W.C.2. The next in the series of international conventions on microwave valves is to be held at The Hague, Holland, from September 3rd-7th, 1962. The I.E.E. also announces that a Conference on Components in Microwave Circuits will take place in London in September 1962.

Radio \& Television Servicing.-The report on the servicing examinations held in May by the City and Guilds of London Institute and the Radio Trades Examination Board records that of the 2,068 candidates who sat the intermediate written exam. 1,108 (53.6\%) passed. The 1960 figures were 560 entrants, $336(60 \%)$ passes. Of the 717 who took the final examination in May 285 ( $29.8 \%$ ) got a first class and 367 ( $51.2 \%$ ) second class pass. This is the first year of the combined sound radio and television syllabus.

Radio Amateurs' Examination.-The Standard of papers submitted at the examination, conducted by the City and Guilds in May, "sliowed a welcome improvement over that of last year", says the report. A total of 1,251 entered and $866(69.2 \%)$ passed compared with 1,274 and $699(54.9 \%)$ in 1960.

The Physics of Semiconductors is the subject of an international conference, which is to be held at the University of Exeter from July 16th-20th, 1962. It is being organized under the auspices of the International Union of Pure and Applied Physics by the Institute of Physics and the Physical Society, 47 Belgrave Square, London, S.W.1. Provisional programmes and application forms may be obtained from the Administration Assistant at the aforementioned address.
The F.B.I. and its Japanese counterpart, Keidanren, are to make efforts "to realize at an early date a freer flow of trade between the two countries by progressively reducing and ultimately eliminating import restrictions and conducting orderly marketing, and to promote economic co-operation and technical links between the two countries by encouraging closer contact and fuller understanding between the industrialists of both countries." Following a visit by Sir Norman Kipping, Director-General, and J. R. M. Whitehorn, Deputy Overseas Director, the Federation has published a report entitled "A Look at Japan." Copies, price 10s, are available from the F.B.I., at 21 Tothill Street, London, S.W.I.

Domestic Receiver Design.-Papers of particular interest to those in the "entertainment radio and television industry" are being sought for the I.R.E. Chicago Spring Conference on Broadcast and Television Receivers, arranged for June 18th and 19th. Offers of papers, including a $50-100$-word summary, should be sent to Al Cotsworth, Zenith Radio Corporation, 6001 West Dickens Avenue, Chicago 39, Ill., as soon as possible.

Television in South Africa will not arrive for at least another five years owing to the heavy cost of installation, stated Dr. P. J. Meyer, chairman of the board of the South African Broadcasting Corporation, on his return from a two-month trip abroad to study radio and television techniques.

The B.B.C. has placed an order for ten Marconi $250-\mathrm{kW}$ short-wave transmitters which use vapourcooled triodes made by the English Electric Valve Company. The new transmitters form part of a re-equipment programme for the B.B.C.'s External Services transmitting stations; six will be installed at the Woofferton station, which is used to relay the Voice of America, and two each at Daventry and Rampisham, Dorset.
U.S.S.R. Academy of Sciences were hosts to Professor T. Kilburn and Dr. D. B. G. Edwards of the University of Manchester, when they travelled to Moscow recently to deliver a series of lectures on the Ferranti Atlas electronic digital computer. Ten lectures were given altogether, over a period of five days, to an audience of technologists and engineers at the Institute of Precise Mechanics and Computing Technique in Moscow. Discussions showed that the Russians have a different approach on the general philosophy of computer design. Their policy is to build separate machines for scientific and data processing applications, and they are putting a great deal of effort into the development of faster storage and other components.

Colour Television test transmissions on 405 lines from the Crystal Palace transmitter were restarted by the B.B.C. in October. They are conducted from 1600 to 1630 on Mondays to Fridays. A simplified explanation and also a detailed specification of the system employed are available from the Engineering Information Department, Broadcasting House, London, W.1. The detailed specification is given on Information Sheet 2202/2.
The Scottish Electrical Training Scheme, launched some six years ago to train executives for the member firms in Scotland, has made outstanding progress, reports J. S. Hastie, of Scottish Cables Ltd., current chairman of directors. He said the 119 graduates and students attending the recent fifth annual conference was the highest figure since the start of the scheme, and it was planned to encourage volunteers for higher advanced courses to qualify graduates for the top posts in the industry and a start would be made shortly on an advanced mathematics course to meet this need. S.E.T.S. also plans to train one overseas student each year, returning him to his own country to work, as a gessture to the electrical industry abroad.

Westinghouse Schools Training Course.-A further "Introduction to Industry" training course will be held by Westinghouse at their Chippenham Works during the week January 8 th-12th inclusive. This is for sixthform boys taking G.C.E. "A" level examinations in science subjects in 1963. Applications should be addressed to the Personnel Superintendent, Westinghouse Brake \& Signal Co. Ltd., Chippenham, Wilts., by December 1st.

Norwood Technical College, London, S.E.27, is introducing the first of two six-lecture evening courses on transistors on January 16th. The first course covers fundamentals and the second, beginning on February 27 th , applications. The fee for each course is 10 s .
Medium-wave DX.-A " set listening period" from 0100 to 0300 G.M.T. on December 2 nd has been arranged by the group of DX enthusiasts which issues the monthly duplicated news sheet "Medium-wave News". Reports of long-distance reception will be welcomed by K. Brownless, 7 The Avenue, Clifton, York, who edits the news sheet.

## What they say

Component Research.-"It is perhaps not widely known that the British Electronics Industry spends out of its own resources a greater percentage of its gross turnover [on reasearch and development], approximately, $12 \%$, than any other industry in the United Kingdom." -A.F. Bulgin, president of R.E.C.M.F., at the opening of the Stockholm component exhibition.

Problems for Pilkington.-" Never in the long history of committees and commissions have so many problems been compressed into so few words."-Miss Mervyn Pike, Assistant P.M.G., referring to the terms of reference of the Pilkington Committee at the Relay Services Association luncheon.

## Personalities

Sir Gordon Radley has succeeded Lord Nelson of Stafford as chairman of Marconi Instruments, Marconi Marine, and English Electric Valve Company and has also been appointed depuiy chairman of Marconi's W/T Company. Lord Nelson has also retired from the chairmanship of Marconi's W/T and is succeeded by his son the Hon. George Nelson. Other appointments tồ the Boards of the subsidiaries of the English Electric Company include:-F. N. Sutherland as depuiy chairman and Dr. E. Eastwood as a director of Marconi Instruments; P. L. de Laszlo as deputy chairman of E.E. Valve Co.; and D. P. Furneaux as managing director designate of Marconi Marine in succession to R. Ferguson who retires at the end of the year.
J. H. Westcott, B.Sc., D.I.C., Ph.D., M.I.E.E., who is 41, has had the title of Professor of Electrical Engineering in the University of London conferred on him in respect of his readership at Imperial College. Dr. Westcott, after post-graduate research on servomechanisms at the college and at the Massachusetts Institute of Technology, joined the Goyarnment scientific service in 1942 and was for some time at what is now R.R.E., Malvern. He was on the Control Commission for Germany in 1945/6. Dr. Westcott, who is chairman of Feedback Ltd., of Crowborough, Sussex, was responsible for the setting up of the control systems laboratory at Imperial College which he joined in 1950.
R. J. Hitcheock, M.A., A.M.I.E.E., consultant to Cable and Wireless where he was for some time engaged on radio-frequency allocations and radio propagation problems in general, has recently visited the Bell Laboratories in America to study the problems of satellite communications. Mr. Hitchcock, who has represented C. \& W. at many international conferences and is a member of several study groups of the C.C.I.R., has contributed articles to Wireless World on various aspects of international teiecommunications. He is a member of the committee set up by C. \& W. to consider "what part, if any, the company should take in the provision of satellite relays." The committee is presided. over by H. C. Baker, a director, and among the eight members is P. A. C. Morris, who is in charge of the company's radio propagation section.

John V. Dunworth, C.B.E., M.A., Ph.D., F.Inst.P., A.M.I.E.E., the new deputy director of the Nat.onal Physical Laboratory, was throughout the major part of the war working on the development of radar; first with the Admiralty and later with the Ministry of Supply at R.R.E. He succeeds Dr. G. G. Macfarlane, who, as announced recently, is going to Malvern as director of R.R.E. Dr. Dunworth, who is 44, graduated at Cambridge University in 1937 and did post-graduate research under Lord Rutherford. After the war he returned to Cambridge to take up his Fellowship at Trinity College and was appointed a demonstrator in physics in the Cavendish Laboratory. He joined, the Atomic Energy Research Establishment in 1946, and since 1959 has been deputy director of the Atomic Energy Establishment, Winfrith.
R. E. Fischbacher, B.Sc., A.M.I.E.E., has been appointed an assistant director of the British Scientific Instrument Research Association which he joined in 1957 as head of the Electronics Department. Educated at the Royal College of Science and Technology, Glasgow, and the University of Glasgow, Mr. Fischbacher served for 12 years in the Admiralty Signal and Radar Establishment as a member of the Royal Naval Scientific Service before joining the B.S.I.R.A.

Air Comdre. A. G. P. Brightmore; M.Brit.I.R.E., Director of Electronics Research and Development (Air) in the Ministry of Aviation, and Air Comdre. F. E. Tyndali, B.Sc., Director of Radio at the Air Ministry, have exchanged posts. Air Comdre. Brightmore, who is 53, has been in the Ministry of Aviation since 1958 having previously served for two years as chief signals officer of the 2nd Tactical Air Force. At one time he commanded No. 3 Radio School, R.A.F., at Compton Bassett, Wilts. Air Comdre. Tyndall, who is a member of the Post Office Frequency Advisory Committee, has been in the Air Ministry directorate of radio since April, 1959. He is 48.

Frank Poperwell, Assoc.Brit.I.R.E., who recently joined the Derritron group of companies as technical sales supervisor, has now been appointed general manager of Reslosound Lid. (a member of the group). Prior to joining the group a few months ago he was with the G.E.C. for 35 years where he was technical supervisor of the Sound Equipment Division. L. W. Murkham, founder of Reslosound recently sold his interest in the company to the Derritron group.
C. J. Salvage contributes to this issue a constructional article on a transistor communications receiver which he designed for use with a 6-band minia:urized transmitter. He is a keen s.s.b. amateur transmitter (his call is G3HRO) and in 1956, using his own s.s.b. equipment, participated in the first six-continent R/T link-up on 20 metres. The receiver described, and its associated transmitter, was awarded first prize at the National Mobile Rally at Woburn Abbey in September. Mr. Salvage is chairman of the Aquila Radio Club of the Inspection Branch of the Ministry of Aviation where he has been employed since 1940.
T. H. Whitaker, who has been with Cossor Radar \& Electronics since 1957, is going to New Zealand early next year to supervise the installation of eight meteorological radars, three of which will be on the islands of Fiji, Funafuti, and Rarotonga. He will also instruct staff of the N.Z. Civil Air Administration on the handling and servicing of the equipment. Mr. Whitaker, who is 32, was trained as a radar mechanic in the R.A.F.

T. H. Whitaker

W. P. Raffan
W. P, Raffan, B.Sc., A.Inst.P., has been appointed head of the newly formed Solid State Division of 20th Century Electronics. He was formerly with Rank Cintel where, during the past three years he has been engaged in the development of solid state devices.

Eric K. Cole, C.B.E., M.Brit.I.R.E., has resigned from the position of deputy chairman of British Electronic Industries Ltd. (the holding company formed on the merger of Pye and Ekco a year ago) and also from the chairmanship of E. K. Cole Ltd. and its subsidiaries, which include Ekco Electronics Ltd. and 20th Century Electronics Lid. Mr. Cole, who was elected an honorary member of the Brit.I.R.E. in 1959 "in recogn.tion of his services to the radio and electronics industry and profession," founded the company bearing his name in 1926 when he was 25 . He was appointed a Commander of the Order of the British Empire in 1958. The chairman of B.E.I. is C. O. Stanley, chairman and managing director of the Pye Group.
C. J. Maurer, B.Sc.(Eng.), A.M.I.E.E., of Romford, Essex, and W. T. Warnock, A.M.I.E.E., A.M.Brit.I.R.E., of Stone, Staffs., both Post Office engineers, have received the Insign:a Award in Technology from the City and Guilds of London Institute (C.G.I.A.). Mr. Maurer joined the Post Office Engineering Department in 1939, where he returned in 1946 after war service as a radar mechanic in the R.A.F. He is now an executive engineer and for the past six years has been working on the introduction of "international subscriber dialling". Mr. Warnock, who joined the Post Office in 1933, has been on the staff of the P.O. Central Engineering Training School at Stone since 1958, where he is now deputy principal.

## News from Industry

Associated Television has formed a new wholly owned subsidiary, Planned Holdings Ltd., to integrate the technical and marketing resources of all the firms in its Planned Group of companies. This new company will be responsible for the future development of the Group into the field of sound and music services. Mernber companies of the Planned Group are Planned Music Ltd. (Muzak background music system), Planned Communications Ltd. (line networks) and Planned Equipment Lid. (Audiomatic automatic audio-visual selling and communication system). J. B. C. Bennett, B.Sc. (Eng.), A.M.I.E.E., has joined the board of Planned Music Ltd. D. Humphriss and H. F. Mould, who were until recently in the Sound Equipment Section of the G.E.C., have joined the Planned Group of companies. Mr . Humphriss is regional liaison engineer and Mr. Mould public address engineer.
G.E.C. Telecommunications Group.-Two new operating companies, G.E.C. (Telecommunications) Ltd. and G.E.C. (Electronics) Ltd., have been formed by the General Electric Company to take over the activities of its Telecommunications Group. Co-ordination and direction of these companies will be undertaken by a newly formed holding company, G.E.C. (T. \& E.) Holdings Ltd. O. W. Humphreys has been appointed executive chairman of the holding company and chairman of the two new operating companies. W. A. C. Maskell is director of the holding company, C. Riley director and general manager of G.E.C. (Telecommunications) Ltd., and R. J. Clayton director and general manager of G.E.C. (Electronics) Ltd. Brigadier John Clemow has been appointed engineering director of the latter company. The headquarters of G.E.C. (Telecommunications) Ltd. will be at G.E.C. Telephone Works, Coventry, and of G.E.C. (Electronics) Ltd. at Union Works, Wembley.

Cossor Board Appointments.-As a result of the purchase of A. C. Cossor Ltd. by Raytheon Company, of Massachusetts, U.S.A., the following have been elected to the board of A. C. Cossor:--Charles F. Adams, chairman of the board of Raytheon; Richard E. Krafve, president of Raytheon; and Dr. Carlo L. Calosi, vice-president of Raytheon. Raytheon have already announced their intention of preserving the identity of the Cossor Group. Major-General Sir Miles Graham continues as chairman and James S . Clark as managing director.

English Electric in France.-A new company, La Compagnie Continental D'Equipements Electriques (C.E.E.) has been formed by the English Electric Company and the French firm, Les Exploitations Electriques et Industrielles, to manufacture electric and electronic control equipment for France and the Common Market countries.

Plessey-A.T.E.-Ericsson Merger.-Completion of the merger between the Plessey Co. Lid., Automatic Telephone \& Electric Co. Ltd., and Ericsson Telephones Ltd., has been effected, and it is announced that A. F. Roger, A.T.E. chairman, and Sir Harold A. Wernher, chairman of Ericcson, have been appointed to the Plessey board of directors.
Decca Record Company's group net profit for the year ended March 31 st is $£ 1,249,229$ as compared with $£ 1,260,729$ for the previous twelve months. Consolidated trading balance was higher at $£ 3.7 \mathrm{M}$ ( $£ 3.4 \mathrm{M}$ ), but exports, including $£ 1.4 \mathrm{M}(£ 2.3 \mathrm{M})$ to the U.S. and Canada, were lower at $£ 7.1 \mathrm{M}$ (£8.1M).
International Rectifier Corporation.-Consolidated sales and earnings for the year to June 30th show a sales increase of $11 \%$ over the previous twelve-month period, and a profit margin of $7.4 \%$ after taxes. The Corporation, with headquarters at El Segundo, California, U.S.A., has a $50 \%$ share in International Rectifier Co. (Great Britain) Ltd. with Metal Industries Ltd. having a similar interest.

Solartron Sold To Schlumberger.-Firth Cleveland have sold for just under $£ 2 \mathrm{M}$ their $56.7 \%$ holding in the Solartron Electronic Group to Schlumberger of Houston, Texas, who themselves were linked recently with the American Daystrom company. Firth Cleveland acquired their controlling interest in Solartron two years ago. Schlumberger has other interests in electronics and instrumentation both in the U.S.A. and Europe.


Console of the 34-channel sound mixer manufactured by Pye for the Elstree Studios of Associated Television. In addition to providing mixing facilities for studio microphones it also provides echo effects and talk-back facilities.
S.I.M.A. Delegation to Italy.-In 1960, only $8 \%$ of the scientific instruments imported into Italy came from the U.K. compared with $35 \%$ from west Germany and $21 \%$ from the U.S.A. In an effort to remedy this a delegation of the Scientific Instrument Manufacturers' Association of Great Britain visited main Italian cities recently to discuss marketing problems and to collect information on the instrument needs of Italian research programmes and industry.

Cambridge-C.G.S. is the title of a new company formed jointly by Cambridge Instrument Co. Ltd. and Istrumenti Di Misura, C.B.S. Located at Casoria, near Naples, the company will initially manufacture instruments based on Cambridge designs. English members on the board of Cambridge-C.G.S. are Dr. P. Dunsheath, H. C. Pritchard and W. E. Lamb.
T.C.C.--Sprague Exchange.-The Telegraph Condenser Company and the American Sprague Electric Company have recently agreed to a mutual exchange of technica! "know-how," whereby the two organizations will share their research and manufacturing experience. T.C.C. are the sole distributors in the U.K. for Sprague products.

Raytheon Company are to acquire all of the assets of Rheem Semiconductor Corp., a subsidiary of Rheem Manufacturing Company, at Mountain View, California.

Marconi Cameras For ITN.--Four Marconi Mark IV television cameras ordered by Independent Television News are now in use at the ITN headquarters in Television House, Kingsway. This is part of a general reequipment of ITN's facilities to enable them to carry out more ambitious programmes. The installation has beer designed by ITN's own engineering staff and will be their first use of $4 \frac{1}{2}$ in image orthicon cameras.

Hudson Electronic Devices Ltd., who specialize in the design and manufacture of v.h.f. radio-telephone equipment, have received an order from the Home Office, worth nearly $£ 30,000$, for 200 of their Type AM112 mobile $15-\mathrm{W}$ equipments to be used by the Police. This follows a similar order last year.
E.M.I. Electronics Ltd. have been awarded a $£ 30,000$ contract by the Independent Television Authority for the installation of a 450 ft tower and aerial array in Jersey, Channel Islands.
I. S. B. Transmitters.-Marconi's are to supply to the Admiralty a large number of $500-\mathrm{W}$ m.f./h.f. independent sideband communication transmitters of a new type, NT204, which embody contmuous tuning from $240 \mathrm{kc} / \mathrm{s}$ to $24 \mathrm{Mc} / \mathrm{s}$. Value of order is about $£ 90,000$.

Manchester Mincabs have been equipped with Storno-Southern f.m. transistor radio telephones. A $25-\mathrm{W}$ base station at Gorton feeds a standard centre-fed dipole aerial mounted on an 80 ft mast, and ranges of up to 30 miles are being obtained.

British Communications Corporation, a subsidiary of Radio \& Television Trust, has recently obtained a large contract for the supply of v.h.f. transmitter/receivers Type A. 40 to the British Army.

Pickering Cartridges.-Goldring Manufacturing Company, of Leytonstone, London, E.11, advise that they are now marketing certain items of the American Pickering range of audio equipment in this country. These include the Unipoise 198 integrated arm and cartridge and a selection of Pickering cartridges.

Walmore Electronics Ltd., of 11-15 Betterton Street, London, W.C.2, have been appointed by Siemens \& Halske A.G., west Germany, as U.K. representatives for their transmatting and special recciving valves.

Metal oxide film resistors developed in the U.S.A. by Corning Glass Works, are being manufactured in the U.K. by Jobling and marketed by Electrosil Ltd., of Colnbrook By-Pass, Slough, Bucks. The latter company was formed recently by Corning in association with James A. Jobling \& Co. Ltd.

Tape heads manufactured by Wolfgang Bogen G.m.b.H. of Berlin, previously available through Gopalco Ltd., are now obtainable from R. H. Cole (Overseas) Ltd., 2 Caxton Street, Westminster, London, S.W.1. (Tel. : Sullivan 7060), who have been appointed sole U.K. agents. Components made by Bogen include mono and stereo heads for domestic tape recorders, erase heads and a range of single and multiple heads for professional applications.

ETEL Sales Move.-Electronic Tubes Ltd. advise that the sales and technical information office of their Instrument Cathode-Ray Tube Division is now at 80 New Oxford Street, London, W.C. 1 (Tel.: Langham 0800).

New Telephone Numbers.-The Gresham Lion Group of Companies, Gresham House, Hanworth, Middx., advise their new number is Feltham 3655. (The telephone number of Gresham Transformers Ltd. continues as Feltham 6661.) Mullard Equipment Ltd., Crawley New Town, Sussex, have had their number changed to Crawley 28787.

Ampex Great Britain Ltd., which is responsible for the sales of Ampex equipment in the U.K., has moved to 72 Berkeley Avenue, Reading (Tel.: Reading 55341).

Dawe Instruments Ltd. have moved from Harlequin Avenue, Brenford, to Western Avenue, Acton, London, W. 3 (Tel.: Acorn 6751).

Lee Products (Gt. Britain) Ltd. have transferred from Longford Street, N.W.1, to new offices at 10-18 Clifton Street, London, E.C. 2 (Tel.: Bishopsgate 6711).

## overseas trade

1962 Near East International Fair is to be staged in Tel Aviv, Israel, from June 5 to July 5, when Western visitors will find the opening times a little strange. They are 4 p.m. to midnight except on Saturdays, when they will be sunset to midnight. Electrical, cooling, heating and radio and TV products will be exhibited in a wide range of merchandise. British participation is being organized by Industrial \& Trade Fairs Ltd., Commonwealth House, New Oxford Street, London, W.C.1.

Marconi's were responsible for equipping Ghana's new external broadcasting station, with its four $100-\mathrm{kW}$ transmitters capable of world coverage. Marconi's have also been awarded a contract by the Ghana Posts \& Telegraphs authorities for the supply and installation of a twin-path v.h.f. multichannel radio-telephone system to link the Volta river dam area with Accra, the capital. The carrier equipment will be provided by the Automatic Telephone \& Electric Company.
W. G. Pye Get Russian Order.-Following an enquiry received at the British Trade Fair in Moscow this year, an order for industrial pH measuring, recording and controlling equipment worth $£ 15,000$ has been obtained by W. G. Pye \& Co. Ltd. from the official U.S.S.R. buying agency, Mashpriborintorg.

Danmarks Radio, the Danish state broadcasting service, has placed an order with E.M.I. Electronics Lid. to supply four $4 \frac{1}{2}$ in image orthicon camera channels for use in the Copenhagen studios.

The Royal Malayan Navy has selected Decca True Motion marine radar for the six new fast patrol craft now on order from Vosper's.

# Transistor High-Fidelity Pre-Amplifier <br> By R. TOBEY, m.A. and J. DINSDALE, в.a. 

COMPREHENSIVE INPUT/EQUALIZING CIRCUITS, TONE CONTROLS AND FILTERS

I$N$ the following article details are given of the design of a pre-amplifier, incorporating all the usual facilities, for use with the transformerless transistor power amplifier described in last month's issue.

This pre-amplifier may also be used with sensitive vaive power amplifiers, such as the Mullard 510, when compactness, complete absence of hum and (with suitable transistors) improved signal-to-noise ratio, are required.

A two-stage circuit (Fig. 1) conforming fairly closely to standard valve practice, is used. The first stage provides equalization by frequency-selective negative feedback, and a wide variety of inputs may be catered for. The second stage is an adaptation of the well-known Baxandall tone control circuit, giving an ample range of control of both treble and bass by negative fcedback. High- and low-pass filtering is also provided, again by the use of negative feedback.

Input Equalizing Stage.-The basic circuit is shown in Fig. 2. Any equalization curve consisting of slopes not exceeding 6 dB per octave may be
produced by a suitable choice of components $\mathrm{R}_{1}, \mathrm{~K}_{F}, \mathrm{U}_{1}, \mathrm{C}_{2}$. A typical curve is shown in Fig. 3.

The value of $\mathrm{R}_{F}$ sets the current sensitivity of the stage, and $R_{1}$ sets the input impedance (equal to $R_{1}$ ) and hence the input voltage sensitivity. Where maximum input sensitivity is not required, the equalizing networks may be derived directly from those used in valve circuits, but using component values suitable for transistors. Fig. 4 and Table I giv: typical values for the most usual applications.

This approach, however, does not lead to the best exploitation of transistor characteristics, since the transistor is a current-operated device, and the lower the input impedance which can be used, the greater the sensitivity. When used with low-output magnetic pickups and tape heads, valve pre-amplifiers are arranged to have an input impedance which places the $L / R$ integration beyond the audio passband. For example, for a $500-\mathrm{mH}$ pickup, most manufacturers specify an input impedance of at least $68 \mathrm{k} \Omega$, giving attenuation starting around $20 \mathrm{kc} / \mathrm{s}$. Greater sensitivity can be produced from a transistor pre-amplifier by using a lower impedance,

Fig. 1. Complete preamplifier circuit.



Table 1
C mmponent Values for Pre-Amplifier (Figs. 1, 4, 8)

| Resistor | Value ( $k \Omega$ ) All Resistors are $\frac{1}{4} \mathrm{~W}, 5 \%$ | Capacitor | Value (F) and Working Voltage | inductance of the input source which gives part of the required equalization characteristic. <br> For example, the standard l.p. characteristic calls |
| :---: | :---: | :---: | :---: | :---: |
| R 1 | 3.9 | C 1 | 2,000p | by feeding a 500 mH -pickup into $6.8 \mathrm{k} \Omega$-resistor. |
| R 2 | 5.6 | C 2 | 5,000p | The bass emphasis required during the playback |
| R 3 | 47 | C 3 | ${ }_{0} 0.01 \mu$ | of tape may also be produced in this way. The |
| R 4 <br> R 5 | 47 100 | C 4 | ${ }^{0.01 \mu}$ | complete circuit diagram (Fig. 1), together with |
| $\begin{array}{lll}\mathrm{R} & 5 \\ \mathrm{R} & 6\end{array}$ | 100 1 | C 5 C 6 | $\begin{aligned} & 8,200 \mathrm{p} \\ & 10 \mu \mathrm{p} \\ & 12 \mathrm{~V} \mathrm{wkg} \end{aligned}$ | Table 1, give component values for the most widely |
| R 7 | 1 | C 7 | 2 $2 \mu 25 \mathrm{~V}$ wkg | used types of equalization, assuming in the case of |
| R 8 | 47 | C 8 | $100 \mu 6 \mathrm{~V} \text { wkg }$ | the magnetic pickup and tape head, an inductance |
| R 9 | 39 | C 9 | $0.1 \mu 5 \%$ | of $50 . \mathrm{mH}$, which is the value most commonly |
| R10 R11 | 33 180 | C10 | 0.1 $\mu$ 5\% | used. For other inductances the input resistance |
| R11 | 180 18 | C 11 C 12 | 0.01 $\mu$ 5\% | should be changed to keep the same L/R ratio. |
| R13 | 12 | C13 | 25/. 12 V \% wkg | The performance of the record equalizing networks is shown in Fig 5 |
| R14 | 22 | C14 | $2 \mu 25 \mathrm{~V}$ wkg | If it is desired to use the same equalizing networks |
| R15 | 2.7 | C15 | $100 \mu 6 \mathrm{~V}$ wkg | for non-inductive pickups (e.g., a crystal nickup) |
| R16 | 10 | C 16 C 17 | $1,000 \mathrm{p}$ $1,000 \mathrm{p}$ | the treble de-emphasis must be provided at the input. |
| R18 | 3.3 | C18 | 2,000p | In Fig. 1 this is done by $\mathrm{R}_{3}$ and $\mathrm{C}_{1}$. |
| R19 | 3.3 | C19 | 2,000p |  |
| R20 | 39 10 | C20 | 5,000p | Tone Controls.-The tone-control circuit gives a |
| R22 | 1 | C22 | $5 \mu 12 \mathrm{~V}$ wkg | gain set by the values of $\mathrm{R}_{22}$ and $\mathrm{R}_{2}$ |
| R23 | 2.2 | C23 | $50 \mu 25 \mathrm{~V}$ wkg |  |
| R24 | 1.5 | C24 | $50 \mu 25 \mathrm{~V}$ wkg | $\mathrm{C}_{25} \sim^{\text {R35 }}$ |
| R25 | 2.7 | C25 | 5,000p | +1- $\mathrm{Cl}_{26}$ |
| R26 | 2.7 | C26 | $\begin{aligned} & 1,500 \mathrm{p} \\ & 0.01 \mu \end{aligned}$ | Fig. 4. Aiter- |
| R28 | 6.8 | C28 | 1,000p | native low-sen- sitivity |
| R29 | 47 180 | C29 C 30 | $2,000 \mathrm{p}$ | sitivity input $S_{1 a}$ equalizing |
| R31 | 220 | C30 | $100 \mu 6 \mathrm{~V}$ wkg | stage. |
| R32 | 100 22 |  |  |  |
| R34 | 47 |  |  | $\mathrm{R}_{38}$ |
| R35 | 62 |  |  | -mu |
| R36 | 47 |  |  | $\mathrm{C}_{29} \quad \mathrm{R}_{39}$ |
| R37 | 33 |  |  | ${ }_{29} \quad$ 39 |
| R38 | 150 |  | Magneticla |  |
| R39 | 47 |  |  | $\mathrm{R}_{28}$ |
| R40 | 2.2 |  |  | - 28 |
| R42 | 1.8 |  | Stal | $R_{31} \mathrm{R}_{30}$ ! $\mathrm{m}^{\text {a }}$ |
| R43 | 1.5 |  |  | $\cdots{ }_{20}{ }^{1}{ }^{0} \mathrm{C}_{6}$ |
| R44 | 1.5 |  | xitiary |  |
| R45 | 3.9 |  |  | 516 |
| R46 | 0.33 |  | MICROPHONE, |  |
| RV1 | 50 lin |  |  | R/4 |
| RV2 | 25 lin 10 log |  | replay |  |
| RV4 | 5 lin |  |  | $\mathrm{R}_{34}$ |

a stage gain of about three being convenient. For a fuller description of the operation of this type of circuit the reader is referred to the original article (by P. J. Baxandall in the Oct. 1952 issue of Wireless World). The tone-control characteristics of the pre-amplifier are shown in Fig. 6. A different form of the treble characteristics, giving less severe control of the highest frequencies, is shown dotted, and these may be obtained by removing $\mathrm{C}_{11}$. Without $\mathrm{C}_{11}$, the "star" formed by $\mathrm{R}_{17}$, $\mathrm{R}_{18}, \mathrm{R}_{19}$ is equivalent at high frequencies to a "delta" "connected configuration of resistors which shunts each portion of the treble control, giving additional feedback and feed forward of current to the virtual-earth point (Vt 2 base). $\mathrm{C}_{11}$ earths the centre-point of the star at high frequencies and eliminates the shunting effect, hence allowing the treble control to operate as expected.

Filters.-The pre-amplifier can be designed to give a frequency response extending vell outside the audio band, but in practice this is often an embarrassment. Many wide-range pickups produce peaks of considerable amplitude at frequencies above the audio band, which can give rise to audible intermodulation effects; also the modern trend to stereo pickups with their high vertical output, and small speaker enclosures giving little loading of the extreme bass, may make high-pass (or rumble) filtering a necessity. The slope of attenuation of frequencies above and below the audio band given by the filters varies with the setting of the corresponding tone control (see Fig. 6), since both filtering and tone control are achieved by feedback around the same transistor. The maximum boost position of the tone control gives the greatest slope of the corresponding filter. This ensures maximum discrimination against frequencies outside the audio band, when they would otherwise prove most objectionable.

The low-pass filter shown in Fig. 1 is provided by $R_{25}$ and $C_{10}$ to $C_{21}$. Although two passive $R-C$ lags would have the same ultimate slope of 12 dB per octave, the circuit of Fig. 1 has a sharper rurnover. In theory this circuit would tend to peak below the turnover frequency, but in practice the finite output and input impedances of the transistor, in conjunction with the values used, prevent this happening.
The switch is normally in position 1, giving a turnover frequency of $20 \mathrm{kc} / \mathrm{s}$, while positions 2 and 3 (with turnovers at 10 and $6 \mathrm{kc} / \mathrm{s}$ respectively) may be used to deal with programme material such as worn shellac discs or a.m. radio.
A smooth roll-off of frequencies below $20 \mathrm{c} / \mathrm{s}$ is provided in the pre-amplifier, and below $40 \mathrm{c} / \mathrm{s}$ in the power amplifier described in last month's issue. In the pre-amplifier (Fig. 1), the d.c. base current for Vt 1 is supplied from the top end of the emitter by-pass capacitor of Vt 2, so that increasing negative feedback via $R_{14}$, results as the frequency is lowered. The input stage of the power amplifier is also arranged to give increasing feedback below $40 \mathrm{c} / \mathrm{s}$.

The overall characteristic of the filters is shown in Fig. 7.
Stereophonic Version.-The circuit diagram of part of one half of a stereophonic version of the pre-amplifier is given in Fig. 8. $\quad \mathrm{RV}_{4}$ is the channelbalance control, which forms part of the potentiometer $R_{22}, R_{23}$ in Fig. 1. Rotation of this control


Fig. 5. Response of record equalizing circuits of Fig. I (magnetic pickup input).


Fig. 6. Tone control characteristics with (full lines) and without (dotted lines) $C_{11}$. The low-pass filter was switched to $20 \mathrm{kc} / \mathrm{s}$.


One channel of the pre-amplifier viewed from the top (power amplifier and screen removed).
ncreases the gain of the tone-control stage of one channel, and decreases that of the other chann. 1 , hence correcting for any slight out-of-balancs in other pars of the equipment. A difference of $\pm 3 \mathrm{~dB}$ in gain between channels is catered for. Gross differences in channel sensi ivity, such as might by produced by using amplifiers and speakers of different types in the two channels, should be eliminated by an attenuator in the most sensitive channel.

In the prototype, switched tone controls and a single position low-pass filter were used, for the sake of compactness.

Transistors.-The transistors used in the preamplifier should have as high a gain as possible (greater than 80 at 1 mA ), to ensure close agreement between the theoretical and practical operation of the circuits. Suitable types for both Vt 1 and Vt 2 are the OC44, OC75, GET874, GET113 or XA102, but this list is merely a guide, and is by no means exhaustive. Two low-gain transistors as a "superalpha" pair might, however, be used instead of one high-gain transistor, with appropriate changes of


Fig. 7. Characteristics of high- and low-pass filters.


Fig. 8. Part of one half of stereophonic version of preamplifier.


Rear view of stereo pre-omplifier and power amplifier showing one pair of power output transistors.


Front panel of stero power amplifier and pre-amplifier.
biasing resistors. (For a discussion of the super-alpha pair see, for example, p. 388 of the article by $F$. Butler in our Aug. 1960 issue.)

The noise factor of the first transistor determines to a large extent the noise produced by the overall equipment. Though most transistors have proved satisfactory in this application, the occasional specimen may be found which is not, since large variations of noise factor exist between different transistors even of the same type. The signal-to-noise ratio is 70 dB with the tone controls level, or 60 dB with maximum treble boost.

Power Supply.-The pre-amplifier is designed to work off a nominal 12 -volt supply but it will tolerate supply variations between 9 and 15 volts. When the pre-amplifier is being used with a valve power amplifier, the negative voltage required by the pre-amplifier may be conveniently supplied by a dry battery, since the current drain of $2 \frac{1}{2} \mathrm{~mA}$ is small enough to ensure very long battery life.

When compared with a valve pre-amplifier, the transistor pre-amplifier has less capacity to tolerate over driving, since the voltage swing which can be accommodated within the circuit is limited by the lower supply voltage. The present design will not significantly distort signals corresponding to 20 dB above those needed to give full output from the power amplifier, which gives a reasonable margin of safety. However, inputs requiring a sensitivity much less than the design values (see Tables 2 and 3) should be attenuated at the input, rather than by having the volume control turned right down.
Layout.-The layout is not critical though normal commonsense precautions should be observed. When the power amplifier and pre-amplifier are mounted in close proximity, a screening plate must


Fig. 9. Earthing diagram of pre-amplifier and associated equipment.
be used to prevent coupling between the output of the power amplifier and the input of the preamplifier, which may be troublesome at high frequencies, especially when treble boost is applied. The low-pass filter also helps to prevent trouble from this source.

The photographs show one channel of the preamplifier, and two views of the completed prototype stereo version. This was built up on a chassis $\sin \times$ 3in $\times 7$ in. The pre-amplifiers were built up on fibre-board with terminal pins. By arranging the layout of components and wiring in such a way that no wires cross each other, it is very easy to transfer the layout to a printed circuit form of

TABLE 2
Input Data for Fig 1

| Switch <br> Position | Function | Sensitivity <br> $(\mathrm{mV} \mathrm{at} \mathrm{1} \mathrm{kc/s)}$ | Input <br> Impedance <br> $(\mathrm{k} \Omega)$ |
| :---: | :--- | :--- | :--- |
| 1 | Microgroove | Mag 5 <br> Xtal 100 | 6 <br> 100 |
| 2 | 78 r.p.m. | Mag 8 <br> Xtal 150 | 7.5 <br> 100 |
| 3 | Auxiliary | 150 | 100 |
| 4 | Microphone | 1.5 | 1 |
| 5 | Tape replay <br> $7 \frac{1}{2}$ in/sec | 2.5 | 1 |

TABI.E 3
Input Data for Fig. 4

| Switch <br> Position | Function | Sensitivity <br> (mV) | Input <br> Impedance <br> (k $\Omega)$ |
| :---: | :---: | :---: | :---: |
| 1 | Microgroove | Mag 25 <br> Xtal 100 | 47 <br> 100 |
|  | 78 r.p.m. | Mag 30 <br> Xtal 120 | 47 <br> 100 |
| 3 | Auxiliary | 100 | 100 |
| 4 | Microphone | 4 | 22 |
| 5 | Tape replay <br> $7 \frac{1}{2}$ in/sec | 30 | 47 |

assembly. The boards for the stereophonic version were made of opposite hands to facilitate connections to the controls.

The importance of correct earthing, owing to the high currents flowing in the output stage, was stressed in the previous article (Fig. 9).

In conclusion, this article shows that in domestic high-fidelity apparatus, transistors can give just as good results as valves.
(In the article on the transistor power ampli ier in last month's issue, in line 11 of the left-hand column of $\mathrm{p} .568 \mathrm{R}_{10}$ should read $\mathrm{R}_{9}$.)

## Characteristics of Whole Stereophonic System

Output power .. .. 10 watts per channel.
Frequency response. . .. $45 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{kc} / \mathrm{s}$ within 3 dB .
Total harmonic distortion .. $0.25 \%$ at 10 watts output.
Signal-to-noise ratio
(at 10W output)
Negative feedback in power
amplifier .. .

Power requirements" $\quad \cdots$ Version 1: 40 volts d.c. at

Controls .. .. .. Input Selector (Micro-

## Size

Weight
Maximum äbient
temperature

Version 1: 40 volts d.c. at
800 mA (max) or 150 mA (average) for 10 watts in 15 ohm speakers.
Version 2: 24 volts d.c. at 1.6 A (max) or 300 mA (average) for 10 watts in 3 ohm speakers and 24 volts d.c. at 500 mA (max) or 100 mA (average) for $3 \frac{1}{2}$ watts in 15 ohm speakers. phone, Radio, Tape, l.p., 78 r.p.m.), Treble, Bass, Filter, Volume, Balance. 70 dB (with controls level) 60 dB (with max. treble boost).

## 60 dB .

 $\times$ in $\times 7$ in. 31b $20 z$.$40^{\circ} \mathrm{C}$.

## "Guide to Broadcasting Stations"

NEW edition of the Wireless World book "Guide to Broadcasting Stations" lists 500 v.h.f. sound broadcasting stations and 250 TV stations in Europe with an e.r.p. of 5 kW and over. Completely revised this 13 th edition includes, as usual, details of all European longand medium-wave broadcasting stations and over 2,000 s.w. transmitters throughout the world which are listed both geographically and in order of frequency.

Tabies covering standard time, wavelength-frequency conversion and the international allocation of call signs, are included in the new Guide, which costs 3 s 6 d (by post 4s).

## "ALL-BAND" TRANSISTOR COMMUNICATIONS RECEIVER

Design Suitable for Mobile Use

THE introduction of transistors has opened a new field to the amateur constructor and now the " drift" types have made possible the construction cf an all-band all-transistor communications receiver. The set described here was designed primarily as a car radio and operates in the broadcast and six amateur bands. A b.f.o. is included for reception of s.s.b. and c.w. transmissions.

## Circuit

As can be seen from the circuit diagrams (Figs. 1, 2 and 3) the line up follows closely that of a conventional communications receiver using valves.
R.f., Mixer and Oscillator Stages.-The aerial circuit has seven coils, either tapped at a suitable position from earth or bearing a coupling winding to give an input impedance of approximately $50 \Omega$, as the receiver is designed to operate from a whip aerial. The broadcast-band coils $L_{1}, L_{8}$ and $L_{15}$ in the aerial, r.f. and oscillator sections are tuned by the $310-\mathrm{pF}$ three-gang capacitor $\mathrm{C}_{1}, \mathrm{C}_{2}$ and $\mathrm{C}_{3}$ giving a coverage of $1.5-0.7 \mathrm{Mc} / \mathrm{s}$. For the amateur bands 22-pF fixed capacitors $\mathrm{C}_{4}, \mathrm{C}_{10}$ and $\mathrm{C}_{11}$ are switched in series with the main $310-\mathrm{pF}$ tuning capacitors in order to provide the necessary bandspread. The capacitive dividing circuit $\mathrm{C}_{5}$ and $\mathrm{C}_{6}$ provides an impedance match to the base of V1 ( OC 171 ) the r.f. amplifier. $\mathrm{V} 1, \mathrm{~V} 2$ and V3 are supplied from the $6-\mathrm{V}$ Zener-diode (Mullard

OAZ203) stabilizing circuit via the $470-\Omega$ resistor $\mathrm{R}_{10}$, thus reducing the operating voltage to 4 . No useful purpose is served by raising the supply above this value which was found to be the optimum working point for all bands. High values for decoupling capacitors are necessary as all the circuits are of low impedance compared with the corresponding valve circuitry.
1.f. Amplifier.-The output from the mixer stage (V3), at a frequency of $470 \mathrm{kc} / \mathrm{s}$, passes to the i.f. amplifier (Fig. 2) which employs three stages. Two stages of amplification can provide sufficient gain if the d.c. supply is increased; but the extra stage was added in order to increase selectivity as the i.f. transformers have only one tuned winding, the secondary being untuned and providing an impedance step-down to match the base of the i.f. transi-



Above: Front view of tuner showing slider control for band switch below dial. Travel of switch "tab" is about two-and-a-half inches.

Left: Plan view of "tuner" unit. Chassis and compartments are 18 s.w.g. aluminium; at top of photograph are, left to right, aerial, r.f. and oscillator compartments each containing seven coils. I.f. transformers are bottom left with b.f.o. stage to right of tuning capacitor drum.
stors V4, V5 and V6. Transformer $\mathrm{T}_{4}$ has a secondary winding designed to match the detector diode (OA70) which supplies the a.g.c. to V5 and the demodulated signal for subsequent audio-frequency amplification. I.f. neutralizing feedback is provided by the R-C network connected to Pin 1 of each of the i.f. transformers $\left(\mathrm{C}_{23}\right.$ and $\mathrm{R}_{16}$ with $\mathrm{T}_{2}$ etc.).
First A.f. Stage.-The audio output from the $5 \mathrm{k} \Omega$ potentiometer $R V_{2}$, which forms the volume
control, is taken to the first a.f. amplifier. The receiver up to this point is all included in the main chassis; the loudspeaker, second and final push-pull a.f. stages are all mounted on a separate panel which is conveniently placed adjacent to the main "tuner " chassis.

Beat-frequency Oscillator.-A b.f.o. stage is included fos reception of s.s.b. and c.w. transmissions. Now a drawback of transistors, especially


Fig. f. R.f., mixer and local-oscillator stages. $\frac{1}{1}-W$ resistors are used.
Fig. 2. I.f., detector, b.f.o. and first a.f. stoges. Note that b.f.o. coupling to Pin 4 of $T_{1}$ first i.f. transformer, is by "stray" capocitance. $\frac{1}{8}-W$ resistors are used.



Fig. 3. Power amplifier unit.


Fig. 4. Arrangement of tuning drive cord and levers actuating band switch from slide on front panel.


Back of loudspeaker and power amplifier panel. Fuse for power supply is at extreme right. First a.f. stage collector resistor and coupling copacitor to driver transistor are connected to socket ot extreme left.
in oscillators, is that they are sensitive to supplyvoltage variations. This, however, can be used to advantage here and adjustment of the rheostat $\left(\mathrm{RV}_{3}\right.$, $10 \mathrm{k} \Omega$ ) in series with the supply to V7 can provide sufficient change of frequency for upper or lower sideband reception of s.s.b. signals or c.w. operation. $\mathrm{C}_{33}$ (a $10-\mathrm{pF}$ trimmer) allows fine pre-setting of b.f.o. frequency. The coupling from the b.f.o. to the i.f. amplifier is provided by a lead running from the " hot" end of $\mathrm{T}_{5}$ to a point near Pin 4 of the first i.f. tranformer $\mathrm{T}_{1}$.

## Construction \& Layout

As will be seen from the photographs the set was designed for fitting into a recess that is normally provided for a broadcast receiver in a car and, as this space is different in different cars, no exact dimensions have been given. The versatility of the receiver makes it very suitable for mobile operation.

The front view of the receiver shows the general lay-out of the front panel. The large knob on the left is the a.f. gain control $\mathrm{RV}_{2}$, with the on-off switch $\mathrm{S}_{5}$ incorporated, and the small knob near it is the r.f. gain control $R V_{1}$. The tuning control is the large knob on the right and a cord drive transfers the motion to the tuning capacitor. The small knob adjacent is for control of the b.f.o. ( $\mathrm{RV}_{3}$ ) and is ganged to the associated b.f.o. on-off switch $S_{4}$. The sliding band switch can be seen under the dial, which is lit by two low-consumption lamps (12V, 50.nA).

The plan photograph shows the two aerial sockets (top left) with the three screened compartments to the right for aerial, r.f. and oscillator coils. Holes for the adjustment of the cores of coils in the second row near the tuning capacitor are located between the coils at the rear of the compartment. The eight-pole seven-way switch used for band selection is operated by the sliding control whose motion is transferred to a right-angled crank fastened to the base of the compartment. In turn the crank transfers the motion to an arm on the rotating spindle of the band-change switch.

The switch itself is a nine-position type, two positions remaining unused, of three banks of three poles each. The small space available and the need for a very smooth mechanical action indicated that something rather different from the ordinary type of wavechange switch was wanted: thus a "Winkler" type switch made by Painton was used.

The small aerial trimming capacitor, shown on the left near the i.f. transformers, has now been replaced by the $10-k \Omega$ potentiometer $R V_{1}$ and provides r.f. gain control. This control was incorporated as it was found that cross modulation occurred when receiving a very strong signal. The b.f.o. coil $\mathrm{T}_{5}$ is to the right of the tuning capacitor and next to it is the trimmer $\mathrm{C}_{33}$.

The layout of the output panel and speaker is simple, with the amplifier ranged along a tagstrip. The socket for connection to the main tuning unit is to the left of this strip. V9, the driver transistor, and its associated transformer are on the left with the two push-pull output transistors (V10 and V11) 'and their output transformer to the right, feeding into the $3-\Omega$ loudspeaker. Negative feedback is
(Continued on page 629)
supplied from the secondary of this output transformer via the $56-\mathrm{k} \Omega$ resistor $\mathrm{R}_{43}$ to the base of V9. All resistors are of $\frac{1}{W}$ rating in this section.

## Performance

The set has a sensitivity of $1 \mu \mathrm{~V}$ on the lower frequency and on 10 and 15 metres this falls to $5 \mu \mathrm{~V}$. The power consumption is about 150 mA at 12 V for normal reception, increasing to 400 mA at full output. Even this current can be conserved when used with transmitter as the whole set is switched off in the transmit condition, rather than, as with a valve receiver, leaving the heaters running. A separate switch for the dial lamps would be worthwhile for dry-battery operation.

## Components Specifications

Coils.-All coils are wound on " Neosid " Type 358/8BA formers 0.3 in . dia., with Grade 900 cores.
(Neosid Ltd., Stonehills House, Welwyn Garden City, Herts.).

| Coil | Band |
| :---: | :---: |
| L1 | Broadcast |
| L2 | 160 metres |

Aerial

## Coil Band

 $180 \mu \mathrm{H}$, wave-wound (about $\frac{3}{16}$ in wide) with 40 s.w.g. d.s.c. wire: coupling coil 15 turns close-wound adjacent to main coil, 30 s.w.g. d.s.c. $90 \mu \mathrm{H}$, wave-wound (about $\frac{3}{10} \mathrm{in}$ wide), 40 s.w.g. d.s.c.: coupling coil 10 turns close-wound adjacent to main coil, 30 s.w.g. d.s.c.L3 80 metres 76 turns, close-wound, 38 s.w.g. enamelled (en.), tapped 7 turns from bottom.
L4 40 metres 28 turns, close-wound, 36 s.w.g. en., tapped 5 turns from bottom.
L5 20 metres
19 turns, close-wound, 30 s.w.g. en. tapped 5 turns from bottom.
12 turns, close-wound, 30 s.w.g. en., tapped 2 turns from bottom.
8 turns, close-wound, 30 s.w.g. en., tapped 1 turn from bottom.

## R.f. Amplifier

L8 Broadcast $200 \mu \mathrm{H}$, wave-wound (about $\frac{3}{16}$ in wide), 40 s.w.g. d.s.c.
L9 160 metres
L10 80 metres
L11 40 metres
$100 \mu \mathrm{H}$, wave-wound (about $\frac{3}{16}$ in wide), with 40 s.w.g. d.s.c.
80 turns, close-wound, 38 s.w.g. en.
L12 20 metres 21 turns, close-wound, 30 s.w.g. en.
L13 15 metres 21 turns, close-wound, 30 s.w.g. en. 14 turns, close-wound, 30 s.w.g. en.
L14 10 metres 10 turns, close-wound, $30 \mathrm{~s} . w . g$. en.

## Oscillator

L15 Broadcast
$120 \mu \mathrm{H}$, wave-wound (about $\frac{3}{16}$ in wide), 40 s.w.g. d.s.c.: coupling coil, 15 turns close-wound adjacent to main coil, 36 s.w.g. d.s.c.
L16 160 metres $80 \mu \mathrm{H}$, wave-wound (about $\frac{3}{16} \mathrm{in}$ wide), 40 s.w.g. d.s.c.: coupling coil closewound adjacent to the main coil, 36 s.w.g. d.s.c.
L17 80 metres 55 turns, close-wound, 38 s.w.g. en., tapped 8 turns from bottom.
L18 40 metres 28 turns, close-wound, 36 s.w.g. en., tapped 8 turns from bottom.
L19 20 metres 14 turns, close-wound, 30 s.w.g. en., tapped 5 turns from bottom.
L20 15 metres 8 turns, close-wound, 30 s.w.g. en., tapped 4 turns from bottom.
L21 10 metres 5 turns, close-wound, with 30 s.w.g. en., tapped 2 turns from bottom.
All coils are covered with polystyrene cement to secure turns.
I.f. Transformers. $-T_{1}, T_{2}, T_{3}$ and $T_{5}$ are identical and are "Weymouth" Type P50/2CC. The detector transformer $T_{4}$ is "Weymouth" Type P50/3CC. $\mathrm{C}_{18}$ to $\mathrm{C}_{22}$ inclusive are supplied as part of the transformer.
(Weymouth Radio Manufacturing Co. Ltd., Regent Factory, Weymouth, Dorset.).
Band Switch.-Painton "Winkler" Type AS/3P/9/33 three-pole wafers, nine-position, make-before-break, threebank with Type "A" spindle
(Painton \& Co. Ltd., Bembridge Drive, Kingsthorpe, Northampton.)
A.f. Transformers.-Details of these are given below; but if home design and construction is not contemplated Radiospares Type T/T1, ratio $1: 1$, is satisfactory for $T_{6}$ and Type T/T2, ratio $6.6: 1$, for $T_{7}$.
(Radiospares, Ltd., 4-8, Maple Street, London, W.1.)
$\mathrm{T}_{6}$ Turns ratio $2: 1+1$
Primary inductance 1 H
Primary resistance $20 \Omega$
Secondary resistance $10 \Omega$ (each half).
$\mathrm{T}_{7}$ Turns ratio $3.2+3.2: 1$
Primary inductance 50 H
Primary resistance $1.0 \Omega$ (each half).
Secondary resistance $0.2 \Omega$.

## Commercial Literature

Controller-Indicator is a mov.ng coil meter movement, with its pointer moving between two parallel plates, one plate being divided into sections. If the two plates are compressed, a circuit is made between one plate and whichever section of the other is under the pointer. Applications are alarms, recording and control, and many variations on the basic form are available. The equipment is part of the Canadian Bach-Simpson range of instruments. including testmeters, panel meters and engine-testing equipment, now marketed by Aveley Electric, Lid., South Ockendon, Essex.

Chopper Type D introduced by Ericsson is capable of handling signals down to $10 \mu \mathrm{~V}$. Minimum noise pick-up is achieved by terminating the coil and contact leads at opposite ends of the unit. Units are supplied to work at $40-60 \mathrm{c} / \mathrm{s}$, but can be adjusted to operate at any frequency up to $100 \mathrm{c} / \mathrm{s}$. The standard coil is for 6.3 V at a resistance of $500 \Omega$. Full details from Ericsson Telephones, Ltd., 22 Lincoln's Inn Fields, London, W.C.2.

Universal C/tan $\delta$ Bridge by Siemens and Halske offers measurement of capac:tance from 10 pF to $2000 \mu \mathrm{~F}$ at charging currents up to 1003 A (with shunts). Direct reading of capacitance and loss factor is provided and there is provision for recording readings of crest voltage, loss angle and $\Delta \mathrm{C} / \Delta$. Details from R. H. Cole (Overseas), Ltd., 2 Caxton Srreet, Westminster, London, S.W.1.

Phase-sensitive Voltmeter is described in a leaflet from Theta Instrument Corporation, 520 Victor Street, Saddle Brook, New Jersey. The instrument is panel-mounting and takes the form of a cyinder 5 -in long, 3 -in in diameter. Sensitivity 1 mV f.s.d., frequency response $60 \mathrm{c} / \mathrm{s}-20 \mathrm{kc} / \mathrm{s}$.

Position Control system-the EMICON B100-is described in a leaflet from E.M.I. E'ectronics Ltd., Industrial Division, Hayes, Middlesex. The system will control machines driven by electric or hydraulic motors, Ward Leonard controls or a.c. motors with clutches. Details are given of peripheral equipment for use with the system.

Components in the wide ranges made by Buigin are listed in a new 174-page catalogue (No. 202) from A. F. Bulgin and Co. Ltd., Bye Pass Road, Barking, Essex.

Integrator Series 5300 is the subject of a leaflet from Electromethods Ltd., Coxton Way, Stevenage, Herts. The integrator, driven by the company's low-inertia integrating motor, employs a lamp and photocell with a rotating shutter to produce pulses. Motors are available to work at voltages between 1.5 V and 24 V .

# Paralleling Transistors 

AUTOMATIC DRIVE CURRENT EQUALIZATION

By F. BUTLER, O.B.E., B.So., M.I.E.E., M.BrIt.I.R.E.

ALTHOUGH very high power transistors are now becoming available it is still quite common practice to use paralleled banks of smaller units in amplifiers and inverters designed to give a large power output. Parallel operation of small transistors has special advantages when the equipment is required to operate at high frequencies since the cut-off frequency of most high power units is unacceptably low. Matched pairs of power transistors can be supplied on demand by most manufacturers, but the provision of larger groups calls for special selection and this may delay delivery or result in increased costs. Replacements cannot be supplied to match earlier samples. When using unmatched transistors it is good practice to equalize the driving currents by the use of external resistance large enough to swamp the variations of input impedance of the individual units. The virtue of this technique is that it tends to linearize the driving currents as well as ensuring strict equality. Its drawback is that it is wasteful of driving power.

A recent paper has shown how transformers of novel and unusual construction may be used to supply nearly equal currents to a number of loads of different, variable or ill-defined impedance. The author describes two distinct types of transformer which are equally effective in securing the desired equality of drive currents. In the simpler type the leakage inductance is rather larger than in a normal transformer which tends to reduce the operating bandwidth and may be objectionable on other counts, e.g. transient response. The second form of construction employs multiple cores with both individual and common windings. Good characteristics are thus assured but at the expense of increased production costs.

In power engineering it is frequently required to operate rectifiers in parallel and to provide some automatic means of load sharing between them. The usual way of doing this is to make use of small centre-tapped reactors or auto-transformers and the idea is readily adaptable for use in transistor power amplifiers or inverters.
Load Sharing by Tapped Reactors.-Fig. 1 shows an alternator of e.m.f. E supplying power to the unequal load resistances $R_{1}$ and $R_{2}$ through a centre-tapped reactor. Each half-winding has an inductance $L$ with mutual inductance $M$ between the windings. In practice an iron core is used and the windings are so closely coupled that M is virtually equal to L .

The action is best understood by first considering the case of equal load resistances. From the symmetry of the circuit it is clear that the input current
to the reactor centre-tap will split so that each load resistor carries half the total current. The reactor core magnetization produced by current in one half-winding is exactly cancelled by that due to the oppositely directed current in the other halfwinding. The net core flux is zero and no voltage appears across the outer ends of the reactor windings. On the other hand, if the reactor currents are unbalanced due to the use of unequal load resistances, there is an incomplete cancellation of core flux and the residual flux changes result in the induction of an e.m.f. in the windings of such a polarity as to cause an increase in the current in the high impedance arm of the network.

It is not difficult to determine the exact ratio of the two currents (see Appendix). Using the notation in Fig. 1 it can be shown that :-
$i_{1} / i_{2}=\frac{\mathbf{R}_{2}+j \omega(\mathrm{~L}+\mathrm{M})}{\mathrm{R}_{1}+j \omega(\mathrm{~L}+\mathrm{M})}$
For close-coupled windings $L=M$ and :-
$i_{1} / i_{2}=\frac{\mathbf{R}_{2}+2 j \omega \mathbf{L}}{\mathbf{R}_{1}+2 j \omega \mathbf{L}}$
Provided the choke reactance is much larger than the load resistances it is clear that the current ratio is almost unity. In general, the two currents are out of phase but the phase difference is negligible in the case where the choke reactance is substantially larger than the load resistances.

It is instructive to look at the circuit of Fig. 1


Fig. I. Equal current division using centretapped reactor.

Fig. 2. Alternative treatment of Fig. 1.


Fig. 3. Extension of current-sharing principle.


Fig. 4. Inverter using parallel push-pull circuit.
from a slightly different point of view. This has been redrawn in Fig. 2 in which a circuit current $2 i$ is shown dividing equally at the reactor centre-tap. The current unbalance due to unequal load resistances is represented by a fictitious make-up current $i_{1}$ which adds to $i$ in the low impedance arm and subtracts from $i$ in the other. This of course calls for a reactor current $i_{1}$ flowing in the direction shown. The magnitude of this current $i_{1}$ depends on the choke reactance and on the net voltage between the outer choke terminals. In turn, this is the difference in the voltage drops across the two load resistors. If the choke is of high inductance it is clear that a large difference of voltage across the two resistances will be required to cause a significant current to flow. This is the unbalance current $i_{1}$.

A mathematical study of the arrangement of Fig. 2 leads to exactly the same conclusion as before and to the same expression for the current ratio $\left(i+i_{1}\right)$ ) $\left(i-i_{1}\right)$.

By making use of additional centre-tapped reactors it is possible to supply nearly equal load currents to $4,8,16$ or, in general, $2^{\text {n }}$ different load impedances. The principle is shown in Fig. 3. At each stage of division the actual current to be handled becomes smaller and smaller so that finer gauges of winding wire may be used as the working current becomes smaller.
Construction of Reactors.-In most applications the tapped reactors will only be required to equalize
the currents in moderately unbalanced loads. The working currents will seldom exceed one or two amperes and quite small magnetic cores are adequate. To provide maximum inductance with minimum physical size it is worth using cores of high grade magnetic material. Grain-oriented silicon-steel Ccores are suitable for high power $50 \mathrm{c} / \mathrm{s}$ equipment but for other applications it may be preferable to choose nickel alloy laminations of the HCR type.

As regards the windings, close magnetic coupling is best achieved by two-ply, bifilar winding, the two half-sections being connected series-aiding. To do this involves connecting the start of one winding to the finish of the other and regarding the junction as the centre-tap. The two free ends then become the outer terminals.
The wide variety of requirements makes it impossible to give useful winding specifications. In any event the design tolerances are very wide. As a rough guide it will be found that a few hundred turns of wire wound on a core with a cross-section about half an inch square will be adequate for most audio-frequency applications. For use in high frequency inverters it is sufficient to wind a few dozen turns of wire on a very small core, say about $\frac{1}{4}$ inch square section.
Practical Circuits.-Fig. 4 shows a typical d.c.a.c. inverter circuit using four transistors in parallel push-pull. Two centre-tapped reactors serve to equalize the base drive currents. For simplicity, the normal starting-bias circuits have been omitted, but any standard arrangement can be incorporated.

The output stage of a typical Class B audio amplifier is shown in Fig. 5. Here again, the tapped reactors ensure equal base currents in the paralleled transistors. Finally, a full-wave rectifier circuit is illustrated in Fig. 6.

In all three cases two separate equalizing reactors have been shown. In the rectifier circuit both reactor windings may be placed on a single common core with suitable inter-winding insulation. With minor reservations, this technique is permissible in audio


Fig. 5. High power class-B audio amplifier.


Fig. 6. Rectifier unit with current-equalizing reactors.
amplifier and inverter circuits. If a common core is used it may be found that current-sharing is imperfect near the cross-over point where the instantaneous driving currents are low. This disadvantage is not important, since the current division becomes more exact as the drive amplitude increases and the peak currents will be accurately equalized.
Conclusion.-The provision of small, simple and inexpensive reactors allows the use of unmatched transistors in paralleled groups. There is no degradation in the performance of equipment using them and few if any circuit modifications are called for. Such reactors are extensively used in high power rectifier circuits and are ideally suited for use with germanium or silicon rectifiers which can then be operated in paralleled groups without de-rating.

## Reference

${ }^{1}$ H. G. Bassett, "Novel Transformer Suitable for the Parallel Opera'ion of Current Driven Devices," Radio and Electronic Components, March, 1961, p. 129.

## APPENDIX

From Fig. 1,

$$
\begin{aligned}
\mathrm{E} & =\left(\mathbf{R}_{1}+j \omega \mathrm{~L}\right) i_{3}-j \omega \mathrm{M} i_{2}, \\
& =\left(\mathrm{R}_{2}+j \omega \mathrm{~L}\right) i_{2}-j \omega \mathrm{M} i_{1},
\end{aligned}
$$

Hence:-

$$
\begin{aligned}
& \left\{\mathrm{R}_{1}+j \omega(\mathrm{~L}+M)\right\} i_{1}=\left\{\mathrm{R}_{2}+j \omega(\mathrm{~L}+\mathrm{M})\right\} i_{2} . \\
& \therefore \frac{i_{1}}{i_{2}}=\frac{\mathrm{R}_{2}+j \omega(\mathrm{~L}+\mathrm{M})}{\mathrm{R}_{1}+j \omega(\mathrm{~L}+\mathrm{M})} .
\end{aligned}
$$

For a reactor with close-coupled windings $\mathrm{L}=\mathrm{M}$ so that:-

$$
\begin{equation*}
\frac{i_{1}}{i_{2}}=\frac{\mathrm{R}_{2}+2 j \omega \mathrm{~L}}{\mathrm{R}_{3}+2 j \omega \overline{\mathrm{~L}}} . \tag{1}
\end{equation*}
$$

From Fig. 2, total choke inductance (end to end) is $\mathrm{L}+\mathrm{L}+2 \mathrm{M}$, with $\mathrm{L}=\mathrm{M}$. Thus, total inductance $=$ 4L.

$$
\begin{aligned}
& i_{1}=\frac{\mathrm{E}_{1}-\mathrm{E}_{2}}{4 j \omega \mathrm{~L}} \\
& \text { where } \mathrm{E}_{1}=\mathrm{R}_{1}\left(i+i_{1}\right) \\
& \qquad \mathrm{E}_{2}=\mathrm{R}_{2}\left(i-i_{1}\right) \\
& \text { Current ratio }=\frac{i+i_{1}}{i-i_{1}}=\frac{1+\frac{i_{1}}{i}}{1-\frac{i_{1}}{i}}
\end{aligned}
$$

$$
=\frac{R_{2}+2 j \omega \mathrm{~L}}{\mathrm{R}_{3}+2 j \omega \mathrm{~L}^{-}} \text {, as before. }
$$

The impedance seen by the source voltage E is
$\mathbf{Z}=\mathbf{E} /\left(i_{1}+i_{2}\right)$. Again taking $M=\mathrm{L}$,

$$
\begin{equation*}
\mathrm{Z}=\frac{\mathrm{R}_{1} \mathrm{R}_{2}+j \omega \mathrm{~L}\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)}{\mathrm{R}_{1}+\mathrm{R}_{2}+4 j \omega \mathrm{~L}} \tag{2}
\end{equation*}
$$

Some special cases are:-
(a) $L=O$ so that $Z=\frac{R_{1} R_{2}}{R_{1}+R_{2}}=\frac{R}{2}$ if $R_{1}=R_{2}=R$.

The load impedance is simply $R_{1}$ and $R_{2}$ in parallel.
(b) $\mathrm{L}=\infty, \mathrm{Z}=\frac{\mathrm{R}_{1}+\mathrm{R}_{2}}{4}$,
(c) $R_{1}=R_{2}, Z=R / 2$ and is independent of $L$.

SHORT-WAVE CONDITIONS


THE full-line curves indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during December.
Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.

**** FREQUENCY 8ELOW WHICH COMMUNICATION SHOULD BE POSSIBLE FOR $25 \%$ OF THE TOTAL TIME

-     - PREDICTED MEDIAN STANDARD MAXIMUM USABLE FREQUENCY

FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE
ON ALL UNDISTURBED DAYS

## HETMERS TO THE EDITOR

## The Editor does not necessarily endorse the opinions expressed by his correspondents

## Hybrid Amplifiers

THE accompanying circuit which appeared in the Hew-lett-Packard fournal for April, 1961, is interesting. This hybrid is used in the X and Y amplifiers of an oscilloscope to provide high gain with a bandwidth of $22 \mathrm{Mc} / \mathrm{s}$. The designers point out that the circuit is useful in a direct-coupled amplifier, since the difference in the steady voltage levels at the input and output is only 3 volts, compared with 60 volts for an all-valve circuit. As a result, the powei supply can be simplified, and heater-cathode potentials can be kept low.
My article on hybrid amplifiers was written in January, and since then the cost of transistors has dropped

considerably For example, the Texas Instruments 2G301, an r.f. transistor with a cut-off frequency of $6 \mathrm{Mc} / \mathrm{s}$ and a current gain of 60 , is listed at under five shillings. This is less than the price of a triode valve, so hybrid circuits should now be a more attractive economic proposition. The intrusion of transistors into mains television receivers reported in W.W.'s Radio Show Review seems to confirm this.
Croydon.
G. W. SHORT.

IN your October issue, G. W. Short has analysed two of the many connections possible with a valve-transistor combination. In my work, a requirement arose for a high-impedance amplifier with good linearity for measuring the voltage stored on a $0.1 \mu \mathrm{~F}$ capacitor, without discharging the capacitor unduly. The voltage range was $0-10 \mathrm{~V}$, and the amplifier was required to drive a $1000-\mathrm{ohm}$ load at up to 1 mA . A hybrid amplifier has proved ideal for this, using the common-anode plus com-mon-collector combination.
In a simple cathode-follower circuit, low grid current can be obtained by operating the valve at low anode voltage and low cathode current. This results in poor linearity, but this can be improved by operating the valve with a constant cathode current. A germanium junction diode, operating in its reverse current direction, is a suitable cathode load, and the circuit is completed by an emitter follower driving the output load.

The accompanying diagram shows the practical circuit. The only additions necessary to the basic circuit are zero setting arrangements and the use of components $\mathbf{R}_{1,}$ D2 and D3 to protect the transistor in the event of the input voltage exceeding about 12 V . Diodes D2 and D3 are operating on the reverse part of their characteristic and limit the valve anode current under abnormal operating conditions.
The linearity obtained with the circuit was $\pm 0.1 \%$ of

maximum input and the input current was less than $10^{-14}$ amps over the range $0-10 \mathrm{~V}$.

No attempt was made to compensate the circuit for temperature changes and the voltage drift referred to the input is therefore rather large. This has not proved troublesome for the $0-10 \mathrm{~V}$ range chosen.

The work described in this letter is published by permission of the Director, Central Electricity Research Laboratories.

Leatherhead.
A. E. T. NYE.

## Safety of Life at Sea

THE Ministry of Transport announced in August that as from 1st September, 1961, direction-finding facilities from British coast radio stations would be suspended. While these services offered by the coast stations have not been patronized to any appreciable extent, the ability of a wireless station to take the bearing of a transmission is a facility that should not readily be withdrawn.

That it is not the desired intention of the Post Office, who staff and operate the stations, to curtail this facility seems apparent from the reservation of a four-acre site for direction-finding aerials at the new Ilfracombe radio station and also from their action in resiting the aerials at Humber Radio within the past few years.

At a coast station the $\mathrm{M} / \mathrm{F}$ watch, on $500 \mathrm{kc} / \mathrm{s}$, is conducted by the Post Office for the Ministry of Transport, who pay for the service. This is considered to be a non-commercial activity. The direction-finding equipment consists, the present tense is used, of large triangular loop aerials erected at a site about half a mile away from the station. The loops are unscreened and are centrally supported from a wooden pole. The site for the direction-finder aerials has to be on suitable elevated ground well clear of buildings, trees, wire fences and overhead lines. Long term preservation of
the site is usually secured by the Post Office becoming the landowner of surrounding territory that then may be leased for agricultural use. At the operating position, which is manned by the operator listening on $500 \mathrm{kc} / \mathrm{s}$, there is a radiogoniometer and a receiver that can be switched at will to either the radiogoniometer or a receiving aerial. A.g.c. is automatically removed from the receiver when it is connected to the radiogoniometer. At frequent and regular periods throughout the day bearings are taken on other coast stations and by this means the operational efficiency of the system is checked.

The prime purpose of radio apparatus on board ship and of the coast radio stations is the safety of life at sea. In the past it has always been the automatic action of an operator at a coast station to take a bearing of a distress signal on $500 \mathrm{kc} / \mathrm{s}$; most often this information is unnecessary but occasionally it has prove $\perp$ of great value and assistance in guiding rescue craft to the location of the distress. Information of this kind is generally only required when weather conditions are foul and only one transmission is made from the vessel in distress. The Ministry of Transport notice, issued from St. Christopher House, states "... there is not sufficient demand for navigational purposes to justify the retention of the service, and the needs of ships in distress are met by cther methods." What these methods are is not stipulated.
What could they be? Bearings taken by other vessels? This is unlikely to happen if only one call is made from the station in distress because ships at sea do not normally keep watch on a D/F receiver and circumstances can arise, as was the case in the rescue operations subsequent to the foundering of the Princess Victoria in January 1953, when the search vessel is unable to take a reliable bearing owing to the extreme yawing of the vessel. Additionally, transmission of the distress message may occur when the ships' operators are not on watch, or the direction finder may be in the chartroom. Bearings provided by naval stations? These stations have not contributed directly in such operations in the past and it does seem unlikely that the $D / F$ facilities would be transferred to the Service at this stage. The use of other modern aids to navigation? If a ship runs aground it would appear that these aids had failed and that it is uncertain of its position. How, then, is assistance to be directed to it promptly?

It seems that the cost of maintenance of these installations, compared with the revenue for the particular service rendered, is considered to be out of proportion. Another factor of influence will be that, in recent years, other countries have abandoned this service; not, however, countries with strong maritime interests. That the facility is not required for navigational purposes is not disputed; but it should be retained for distress purposes and even extended.

The D/F system just abandoned worked in the band 410 to $500 \mathrm{kc} / \mathrm{s}$. This was, perhaps, its greatest disadvantage because the majority of ships using the coastal waters about the United Kingdom, fishing and home-trade vessels, are fitted with radiotelephone equipment that operates in the band 1,625 to $2,850 \mathrm{kc} / \mathrm{s}$. $\mathrm{D} / \mathrm{F}$ coverage in this band would be difficult to provide over the entire coastal area unless the facilities of the Coastguard Service were linked into the scheme. The segregation of marine communication into two bands without ready means of contact from one band to the other has, in the past, hampered rescue work; the most recent instance of this nature occurred after the collision involving the Crystal fewel in the English Channel. It is peculiar that a modern ocean-going vessel cannot communicate directly with a lifeboat or coastal vessel that is coming to its assistance. The Merchant Shipping (Radio) Rules, 1952, make no provision for circumstances like these. Would it be unfair to hint that there seems to be a lack of complete assessment of practical conditions?
If the measures taken by the Ministry are unable to prevent accidents taking place, at least all facilities
should be provided for rescue operations; and while it is not anticipated that they will in any way rescind their decision, the usefulness of permanent $\mathrm{D} / \mathrm{F}$ installations, capable of reception over a wide frequency range, should not be overlooked. Who could help the crew of an aircraft in a rubber dinghy in the North Sea at 0130 G.M.T.? German coast stations, Dutch coast stations and, we are told, " other methods," but not British coast stations.

South Shields.
A. T. FERGUSON.

## Hearing High Frequencies

MR. MAWSON'S conclusion (November issue), that the most acceptable type of radio receiver for the elderly is one which has plenty of built-in top cut, would indicate that at high frequencies not only does the absolute level of hearing threshold increase with age but that also the absolute level of the threshold of pain reduces with age.

This would account for the often observed phenomena that such persons are the first to reach for the top cut and/or filter conurols in reproduced music.

Many eminent elderly musicians, however, although ardent top-cut fans at home, make no complaint about the top from a live orchestra, even sitting in the middle of it. Can it be that with the experience of advancing years one becomes more discerning and thus less prepared to accept the imperfections which most transducers exhibit at high frequencies?

Huntingdon.

## P. J. WALKER.

## Telemetry

I WAS pained to read in your November issue of the abuse of the word "Telemeter." A magazine with as much influence as yours should realize that some confusion will arise from its use.

Unless action is taken, followers of the noble science of measurement at a distance will become identical in the public image with gas company inspectors, and will have to coin a new word to cover their activities. I leave suggestions to Mr. F. Grid. I can only think of "Slotelly" for them.
One group will have to change. We have got classical justificat:on and we got there first.

Cambridge.
S. H. SALTER.
[While we sympathize with our correspondent's point of view, we think that "abuse" is perhaps too strong a word. After all the coins are measured, and at a distance from the company's headquarters.-ED.]

## Degrees of Definition

THE suggestion in your November editorial, to use the word "Mark" in distinguishing different degrees of television, is astonishing.

Present day use of "Mark . . .", by individuals or commerc al firms, suggests adherence to a style which became familiar to many in war time, or alternatively a snobbish attempt to suggest that the items referred to have a large "official" backing.

In the early days of multiple production, mainly in the gun industry I believe, when designs were modified for improvements or economies, it was found convenient to put on a d stinguishing number, letter or other mark. When referring, in writing, to such distinctions, to avoid referring to "Gun II" or "Tank III," the reference became Gun or Tank "MARK II," sometimes abbrevated to "Mk. II." For consistency the word "Mark" or its abbreviation was then added on the articles themselves. Incidentally not all Armament and Government work makes use of the "Mark" system. I met it first as a curiosity of another branch when connected with Naval work in the early 1930's.

For a system to distinguish different standards of
television definition, I suggest "Definition I," etc., for it will always be necessary to note that definition is referred to and the word "Mark" is superfluous. Subsequently in a single artucle, abbreviation to " 1 ," " II," etc., would be reasonable. It is interesting for compar son to note that there seems no tendency to further abbreviate "Band I," etc., no matter how often repeated.
As the editorial also refers to "hair-splitting" about "service," it might not be wise for me to go on and list some of the ways in which "service" is used portmanteau fashion, like "thingamajig" to cover careless lack of discrimination.
Huwever, as an engineer I like to avoid quibbling which is liable to waste time, like redundant reference symbols.
London, N.W.6. W. G. EALY.

## Electronic Music

SINCE it is not possible in a short article to outline fully the artistic or manipulative techniques necessary to extract real value from electronic music, I append some references which readers will find useful. Mr.

Judd, in his article in September, did not give sufficieni credit to the father of musique concrète, Pierre Schaeffer, or his colleagues Olivier and Pierre Messian, whose musical knowledge enabled the art to be launched.
The same applies to the monumental work of Prof. W Meyer-Eppler and his colleagues Herbert Eimert, Frita Enkel and Karlheinz Stockhausen, at Cologne. The immense amount of research into musical notation, composition, and apparatus for electronic music research cannot be fully appreciated without reference to the literature cited below.
Radcliffe-on-Trent.
ALAN DOUGLAS.
Schaffer, P. "A la Recherche d'une Musique Concrète." Edition du Seuil, 1952.
Poullin, J. "Son et Espace." Editions Richard Masse, 1954.

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Moles, A. "Studium und Darstellung des Complexen Tones in der Musikalischen Akustik. Funk und Ton, 1953. Bernhart, J." Deux Applications de la Notion de Distortion Spatiale." L'Onde Elecirique, No. 304. July, 1952. Articles in the special number "Elektronische Musik," Vol. 6, No. 1/2, 1954, of Technesche Hausmitteilungen des Nordwestdeuische Rundfunks.

# TUNED COUPLED CIRCUITS 

USE OF MAXIMUM POWER TRANSFER THEOREM

By B. J. AUSTIN

THE theory of tuned coupled circuits is a straightforward example of elementary circuit analysis and is adequately treated as such in many text books. However, in view of the importance of such circuits, it seems worth while to review the situation in a way which focuses attention on the underlying physics, not on the algebraic manipulations.
The purpose of the article is not, then, to carry out a complete analysis of the circuit of Fig. 1. This would be unrewarding and without much interest. Instead, let us try to see just why tuned coupled circuits behave as they do. In particular, let us attempt to explain, from basic physical principles, the observation that the secondary current $\mathrm{I}_{2}$ can never be made to exceed $\mathrm{V} / 2 \mathrm{R}$, however larg: the coupling M may be. Familiarity with this fact may detract from its striking character, but could we, on a first acquaintance with the problem, merely write off such strange behaviour as accidental? Would we not contrast the docile increase of $I_{2}$ with $M$, up to the critical value $V / 2 R$, with its stubborn refusal to increase beyond this point, and begin to suspect the workings of a hidden law? Of course we would, and this article is intended to show how well-founded our suspicions would have been. Any of our readers who have read the subtitle will know that the law involved is one about maximum power transfer.
First of all, we must know what the Maximum Power Transfer theorem states. Imagine that we have a voltage generator V with internal resistance R. We connect, in turn, load resistances of various values and measure, in each case, the power which is dissipated in the load. The theorem then simply states that this power is greatest when the load resistance is equal to $R$, the internal resistance of
the generator. The reader will be able to show that the maximum power available for dissipation in the load is then $\mathrm{V}^{2} / 4 \mathrm{R}$, corresponding to a current of $\mathrm{V} / 2 \mathrm{R}$. The theorem applies to steady or alternating voltage generators and, if necessary, it could be extended to include generators having complex internal impedances. We will not require this extension.

The theorem is still valid when the load is separated from the generator by a tangle of L's and C's. Indeed, in this situation, it is more flexible since it is possible to " match " any value of load resistance to the generator by means of a suitable lossless coupling network. The network must be chosen so that the generator "sees" a load equal to $\mathbf{R}$, while the real load thinks that the generator has an internal resistance equal to itself. Fortunately, the second half follows from the first, so that we can forget about it. A well-known example of this technique is the matching of a loudspeaker coil


Fig. I. Basic tuned coupled circuit. The dotted box contains a network which couples a "load" to a "generator".


Fig. 2. Squared deviation from $\|(L C))^{\ddagger}$ plotted against $\| Z_{0^{2}}{ }^{2}$ (for high-Q circuits). Graph ( 0 ) is for small $M$, when $/ / Z_{0}{ }^{2}$ never reaches $/ / \mathbb{R}^{2}$ (undercoupling), (b) is when $\| Z_{0}{ }^{2}$ just reaches $1 / R^{2}$ (critical coupling) and (c) is for large $M$ (over coupling).
(resistance 15 ohms, say) to a power output valve (internal resistance 5000 ohms, say) by a transformer with a suitable turns ratio.

To see the application to tuned coupled circuits, let us view the circuit of Fig. 1 in an unusual way. Let us think of the resistance R in the primary as the internal resistance of the generator, and the secondary resistance as a load. Of course, this is an artificial dodge because the R's are inseparably bound up with the transformer, and, anyway, we are not using the tuned circuits merely to dissipate power in the secondary. These objections are not fundamental however, so we may lay them aside. Our problem is to find the condition for greatest secondary current, which amounts to finding the condition for maximum power dissipation in the "load". The properties of the coupling network are in this case frequency dependent, and we are seeking the frequencies at which a load R connected to the output terminals gives rise to a resistance $R$ at the input terminals. (The point here is that the resistance "seen" at the input must be the same as the internal resistance of the generator, i.e. also R.)

At first sight, this problem may seem quite impossible to solve, but actually it can be done. At least, it is always possible to find an impedance (called $Z_{o}$ ) which, when connected to the output terminals of a symmetrical four-terminal network, causes the input impedance to be $\mathrm{Z}_{o}$ as well. $\mathrm{Z}_{0}$ is called, among other things, the iterative impedance, and it is a concept much used in some branches of circuit theory (e.g. the theory of filters). We need not worry about this, but merely remark that our problem is to find the frequencies at which the iterative impedance of the coupling network is equal to $R$.

It can be shown (and this stock phrase hides quite a lot of algebra) that in our case $Z_{0}$ is given by:$1 / Z_{0}{ }^{2}=-[\omega C-1 / \omega(L+M)][\omega C-1 / \omega(L-M)]$ (1)
Hence, the frequencies at which the secondary
current is a maximum are the solutions of:$1 / R^{2}=1 / Z_{0}{ }^{2}=-[\omega C-1 / \omega(L+M)][\omega C-1 /$ $\omega(\mathrm{L}-\mathrm{M})]$
The reader may be tempted to feel that this is the end. After all, we have only to find what frequencies satisfy equation (2) for any given values of the parameters ( $M$ in particular), and we have the frequencies at which the load power is a maximum, and hence the secondary current is greatest. Disappointingly enough, we have not quite finished, since it is not always possible to satisfy equation (2). This is most easily seen by reference to Fig. 2. A word of explanation about this figure is in order here. The abscissa is plotted in terms of the squared frequency obviation from the centre frequency i.e. from $1 /(\mathrm{LC})^{\ddagger}$. Thus each point to the right of the origin represents two frequencies, one above and one below the centre frequency. Negative points have no meaning. When plotted against this variable for high $Q$ circuits, the graph of $1 / \mathrm{Z}_{0}{ }^{2}$ is practically a straight line in the region which concerns us.
For a given value of $M, 1 / Z_{0}{ }^{2}$ is greatest at the centre frequency (remember that negative values of the abscissa are not allowed). If the highest value attained is less than $1 / \mathbf{R}^{2}$, as will happen if we make $M$ sufficiently small, we will not be able to find a solution of equation (2). This is, of course, the situation known as "undercoupling". The secondary current has a single maximum at the centre frequency (i.e. where matching is most nearly achieved). The current is always less than $V / 2 \mathrm{R}$ since we can never have the theoretical maximum power transfer.
If we make $M$ large enough, we arrive at the situation called " overcoupling". We now have the line representing $1 / \mathrm{Z}_{0}{ }^{2}$ rising above $1 / \mathrm{R}^{2}$ at some real (positive) abscissa value. Hence we will have two solutions of equation (2) and thus two frequencies at which $I_{2}$ is a maximum. We can now see that the value of these maxima will be $V / 2 R$, for all values of $M$ greater than the critical value. Thus, the obstinate refusal of $I_{2}$ to exceed $V / 2 R$ can be seen to be a consequence of the maximum power transfer theorem.

At last we have reached the end of the road. It may seem that an undue amount of effort has been expended to arrive at rather meagre scraps of information, especially as the method cannot be extended to include the case of unequal primary and secondary resistances. We could, however, have worked out one more detail, namely the critical value of M , but this is left as an exercise for the reader.

## CLUB NEWS

Bexleyheath.-W. J. Green (G3FBA) will give a talk entitled "Bandspreading HRO Coils" at the meeting of the North Kent Radio Society (G3ENT) on December I4th at 8.0 at the Congregational Hall, Clock Tower, Bexleyheath, Kent.

Birmingham. - The subject for discussion at the December Ist meeting of the Slade Radio Society (G3JBN) is d.f. developments. Meetings are held on alternate Fridays at 7.45 at Church House, High Street, Erdington, Birmingham, 23.

Bradford.-" The development of time measurement" is the title of the talk to be given by W. Barton at the December 12 th meeting of the Bradford Radio Society. The club headquarters are at Cambridge House, 66, Little Horton Lane, Bradford, 5, where meetings are held at 7.30. Instruction for junior members is given at 7.0.

# The D.C. Feedback Pair 

## A USEFUL TRANSISTOR AMPLIFIER CIRCUIT

By G. W. SHORT

THE circuit shown in Fig. 1 has several virtues. Not the least is economy: it gives good temperature stability with fewer components than the conventional one (Fig. 2(b)). It is useful in low-level audio stages, and it lends itself to negative feedback arrangements.
It has been called the transistor d.c. feedback pair,


Fig. I. Transistor d.c. feedback pair.
because it contains two transistors in a d.c. feedback circuit. The operation is complicated. Interested readers can look up reference (2) which contains a full circuit analysis. But they are warned that the formulx are su complex that they mean very little to ordinary mortals.
A rough qualitative picture of what happens can be arrived at without any mathematics. Suppose that, as the result of a temperature change, there is a change in the base current of V1. The increment of base current is amplified by V1, which causes phase inversion as well. Part of the amplified increment is passed to V2, where it is further amplified, and finally a portion is fed back to Vl via $\mathrm{R}_{5}$. Since there is no phase reversal in V2, which is a common-collector circuit as far as this feedback is concerned, the overall feedback is negative.
What about the temperature drift of V2? Assuming that ambient temperature, not the heat of internal power dissipation, is the controlling factor, then both transistors will be subject to the same temperature fluctuations. Their collector-base leakage currents ( $I_{c b o}$ ) will drift in the same direction. Since there is phase inversion in V1, its amplified drift current appears at the base of V2 in opposite polarity to V2's own drift current. Thus some cancellation of V2's drift takes place. In practice, with two
similar transistors, the drift in V2 is overcompensated by V1. As the temperature increases, the collector current of V2 decreases.
The behaviour of a practical circuit is shown in Fig. 3. This compares the performance of the d.c. feedback pair with the more conventio nal arrangements of Fig. 2. The same transistor was used for V1 and for the two conventional arrangements, and the operating current at room temperature was arranged to be the same in each case. A water bath was used to control the temperature: the transistor envelopes were immersed for about three-quarters of their length.
Simplified Circuits:-The d.c. feedback pair can be simplified by connecting the emitter of V1 straight to "earth ", and increasing $R_{5}$. This has

(a)

(b)

Fig. 2. Conventional temperature-compensated circuits; (a) with shunt feedback, (b) with emitter resistor and base bias potentiometer.


Fig. 3. Variation of collector current with temperature. Curve A refers to the circuit of Fig. 2(a), Curve B to that of fig. 2(b), and Curve $C$ to the d.c. feedback pair of Fig. I.
the advantage of getting rid of $\mathrm{R}_{2}$ and $\mathrm{C}_{2}$. (It also increases the input impedance of V1 slightly, but this is hardly important, since $R_{5}$ can usually be made at least twice as big as the input impedance of the transistor V1 itself.)

Two simplified circuits are shown in Fig. 4. The first one (Fig. 4(a)) is applicable when the input is connected through a capacitor. The second (Fig. 4,b)) has too low an input resistance for this (in

(a)

(b)

Fig. 4. Simplified feedback-pair circuits.
vestigated by the writer, $\mathrm{R}_{4(\mathrm{~b})}$ was only about $30 \Omega$ ) but it can be used with transformer input-coupling, as indicated.

The temperature responses of these circuits are compared with that of full circuit in Fig. 5. The immediate conclusion is that the Fig. 4(a) type of circuit is no good: in this particular instance it is worse than the simple circuit of Fig. 2(a). In fact the trouble with this particular circuit was caused by an over-large $\mathrm{R}_{4}$, which in turn made necessary an over-large $\mathrm{K}_{5}$. For good stability, $\mathrm{R}_{5}$ should be as small as possible.

Measurements taken on the circuit of Fig. 6, in which $R_{5}$ is reduced to $4.7 \mathrm{k} \Omega$, are shown in Fig. 7, along with those of the full circuit for comparison. The simpler circuit gives quite a good performance. ( $\mathrm{R} 4_{(\mathrm{t})}$ was $37 \Omega$.)

In general, then, all the variants of the d.c. feedback pair can be made to provide good enough temperature stability for use in domestic equipment, at any rate in a temperate climate. We shall now review some specific applications of the circuit.

Low-Level Input Stages.-Transistor noise can be scrious in audio work. In order to minimize it, the transistor should be operated at a low current. In addition, the collector voltage ( $\mathrm{V}_{c e}$ ) should be kept small, though this is not so important as low current.

Tne temperature-stability curves show that the feedback-pair circuit is a good one for this application. The current in V1 is low and fairly constant, so that the transistor can be operated at a low voltage without the risk of "bottoming" at the higher temperatures. The OC71 is not conspicuously good from the point of view of noise. A special lownoise transistor such as the Mullard AC107 should give less noise, and also less temperature drift: its base leakage current is an order of magnitude less than that of the OC71. It would be reasonable to use an OC71 in the second stage, where noise and $\mathrm{I}_{c o}$ are less important.

Negative Feedback.-The d.c. feedback pair behaves also as an a.c. feedback circuit at frequencies at which the capacitor whic' decouples the emitter of V2 has an appreciable impedance. The effect of this feedback is twofold. It reduces the input impedance of the amplifier as a whole, and it increases the input impedance of V2. Both effects
can cause a reduction of gain as the frequency decreases. The magnitude of this "bottom cut" depends on the signal-source impedance and on the size of the collector load of V1. If the signal source has a very high impedance (constant-current drive) then the input current divides between the base of VI and the feedback resistor $\mathrm{R}_{5}$. Under these conditions the maximum amount of bottom cut is obtained. Note, however, that the process does not go on for ever. As the frequency is reduced, a stage is reacized at which the reactance of the V2 emitterdecoupling capacitor becomes so great compared with the emitter resistance ( $\mathrm{R}_{3}$ ) that the feedback is virtually independent of frequency. The response then levels out again.

If the amplifier is driven from a low-impedance source (constant-voltage drive) the overall feedback has no effect. There is still the local feedback, however. The input impedance of V2 increases as the frequency is reduced. If V2 were driven from a source with a very high impedance, its base current would be unaffected, and there would be no bottom cut. In fact, the source impedance is the collector load of the first stage in parallel with the output impedance of Vl , and it is unlikely to be very high compared with the input impedance of V2, The latter becomes approximately $\beta \mathrm{R}_{5}$ at very low frequencies.

As in all transistor circuits, the two effects can-


Fig. 5. Temperature performance of various feedback-pair circuits. Curve A refers to the circuit of Fig. 4(a), Curve B to Fig. $4(b)$, Curve $C$ to one like Fig. I, but with $R_{5}=10 \mathrm{k} \Omega$.
not be completely separated. The output impedance of Vl is influenced by the signal-source impedance, for instance. But in typical audio circuits the signal-source impedance has only a small effect on the output impedance of V2. One can then get an idea of the effect of the second type of feedback by taking frequency response using a constantvoltage source.

M easurements on a practical circuit showed a low-frequency fall-off of about 5 dB per octave with constant-voltage drive, and 8 dB per octave with constant-current drive. These values were obtained when the capacitance $\mathrm{C}_{3}$ was big enough to bypass the second emitter more or less completely above about $10 \mathrm{kc} / \mathrm{s}$. If, on the other hand, $\mathrm{C}_{3}$ is so small that it only begins to bypass the second emitter at frequencies near the upper cut-off frequency of a normal amplifier, a compensation effect occurs, and the frequency response is improved. In a particular instance, a $0.005 \mu \mathrm{~F}$ capacitor doubled the bandwidth of the amplifier compared to that when no


Fig. 6. Improved version of Fig. 4(a). By fixing $R_{5}$ and adjusting $R_{4}$ to obtain the right operating conditions the resistance in the base circuit of VI is kept fairly low.


Fig. 7. Temperature performance of Fig. 6 (curve A) compared with full feedback-pair circuit with $R_{5}=10 \mathrm{k} \Omega$.
capacitor was used, the gain remaining almost the same.
Tape Recorder Equalization.-Readers may remember an article in the December, 1958, issue in which P. F. Ridler ${ }^{3}$ showed that the circuit of Fig. 8 produced playback equalization for a tape recorder. In this case the inductance was that of the playback head, which was 500 mH .


Fig. 8. Ridler's tape-recorder playback equalization circuit.
In tape-recording, two effects occur which modify the frequency response-a bass cut and a top cut. The bass cut arises simply because, as the frequency is reduced, the rate-of-change of flux at the playbıck head is reduced. The result is a bass cut of $6 \mathrm{~dB} /$ octave. The top cut arises from more than one cause.

It the response of the recording amplifier is flat, and the recording current is constant, then, because of the low-frequency effect, the voltage induced in the playback head by the moving tape is proportional to the frequency. The lower the frequency, the lower the voltage, other things bsing equal. If, as is usual, the playback head is worked into a high-resistance load, so that it acts as a voltage generator, l.f. boost is necessary somewhere in the system.

If, however, the playback head is connected to a load with such a low resistance that it can be consıdered a short circuit, the output current does not tall off as the frequency is reduced. It remains constant. The reason is simple. The voltage induced in the head falls with frequency, as before. But the impedance of the head also falls, since the head is an inductor. These two effects cancel one another, and the output current is not a function of trequency.

Taus, in principle, the need for l.f. equalization can be avoided. The system fails if there is an appreciable amount of resistance in the circuit, either in the winding of the playback head or in the load. While a common-emitter transistor has a lowish input resistance (say $1 \mathrm{k} \Omega$ ), this is by no means a short-circuit. The l.f. current response is 3 dB down when the total resistance is equal to the reactance of the head. Assuming a 1 H head, then for a loss of no more than 3 dB at $30 \mathrm{c} / \mathrm{s}$ the total resistance of winding and load must not exceed about $200 \Omega$. While the winding resistance of the head may be less than 200 s , the input resistance of a common-emitter transistor is much greater. One must either use a common-base transistor, or artificially reduce the input resistance of a commonemitter circuit. Since the feedback pair does this for us if we omit $\mathrm{C}_{3}$, and since r e jative feedback brings other advantages, it is reasonable to use the feedback pair in equalization (i:cuits.

The mechanism by which the equalization works is then as follows. The input resistance of V1 is unaffected by the feedback. What the feedback


Fig. 9. Test circuit for playback equalization.
does is to make $\mathrm{R}_{5}$ look smaller to the signal source, so that the input current mostly flows through $\mathrm{R}_{5}$. If the amount of feedback is the same at all frequencies, the ratio in which the input current is shared by V1 and $\mathrm{R}_{5}$ remains constant. (By reducing the feedback at high frequencies, one can produce top lift. With reduced feedback, $\mathrm{R}_{5}$ looks more like its real value, and V1 gets more current from the source.)
The Mullard OC71 transistors used by the writer had a higher current gain than the transistors used by Ridler (about 50, compared with 30 ). In addition, the supply voltage available was less than Ridler's ( 8.4 V compar ${ }^{\text {d }}$ with 12 V ). Tnese factors prevented the use of an exact copy of Ridler's circuit. The one actually used is shown in Fig. 9. No test tape was available, so instead of using a tape rccorder to gencrate an input voltage proportional to frequercy, the effct was simulated $\mathrm{by}^{2}$ the method suggested by Murray. ${ }^{1}$ This is to force a constant signal current through a small inductance ( $L_{1}$ in Fig. 9). At low frequencies, $R_{s}$ was $10 \mathrm{k} \Omega$, and above about $1 \mathrm{kc} / \mathrm{s}$ it was $30 \mathrm{k} \Omega$. In each case the condition $\mathrm{R}_{8} \gg \omega \mathrm{~L}_{1}$, which is necessary if the current is to approach constancy, is satisfied, since $L_{1}$ is only 8 mH . (It might be mentioned that hum pick-up by $L_{1}$ and $L_{2}$ was somewhat troublesome at first, but was eliminated by carefully orienting the two chokes.)
Measurements were made using two different components for $L_{2}$. One was a choke of 800 mH , with a zero-frequency resistance of $70 \Omega$, and the other was an actual tape head of 200 mH inductance with a resistance of $100 \Omega$. The results are shown in Figs. 10 and 11. To begin with, the frequency response of the amplifier itself was measured;
i.e., without any chokes at all. This is shown by the curve in Fig. 10 labelled $L_{1}=L_{2}=O, C_{3}=0$. In theory, exact l.f. equalization is obtained using the full circuit with $\mathrm{C}_{3}=0$, and this is borne out by the measurement. Note, however, that when the tape head has an appreciable resistance compared with its reactance, the system fails at really low frequencies (Fig. 11, ${ }^{2} 00 \mathrm{mH}, 0_{\mu} \mathrm{F}$ ).

Referring again to Fig. 10, it can be seen that, by including $\mathrm{C}_{3}$, and so reducing negative feedback at high frequencies, a rising response is obtained. This is used by Ridler to compensate the h.f. losses of the head. With his particular circuit, he found a distinct peak at the h.f. end. Such a peak is beginning to appear in the Fig. 10 curves. If the gain of the amplifier is muct higher, it can oscillate at the peak frequency. Ridler's remedy for the peak of inserting a low resistance in series with $\mathrm{C}_{3}$ stops this and gives the designer additional control over the h.f. response.

Tne effect of changing $\mathrm{C}_{3}$ is to shift the response curves bodily. The slope remains nearly the same (about 6 dB per octave). This suggests that, simply by switching in different capacitors, one might change the equalization to suit different tape speeds. The amount of equalization is sufficient to compensate


Fig. 10. Response of test circuit with simulated high-impedance playback head $\left(800 \mathrm{mH}\right.$ ). The capacitance values refer to $C_{3}$.


Fig. 11. Response of test circuit with low inductance head ( $200 \mathrm{mH}, 100 \Omega \mathrm{~d} . \mathrm{c}$. resistance). The dotted curve shows how the I.f. response was restored by connecting $2 k \Omega$ in series with $0.5 \mu F$ across the collector load of the first transistor.


Fig. 12. Effect of $C_{1}$ on the low-frequency response of the test circuit, using the low-impedance tape head.
the l.f. tape loss completely. No pre-emphasis of low frequencies should be required when recording. If, as is probable, the same amplifier has to $b=$ used for recording and playback, one might wish to take advantage of the full gain for recording purposes. All one needs do to get it is to switch a large capacitor across the sccond emitter resistor-say $100 \mu \mathrm{~F}$. 'This will remove negative feedback at all significant frequencies. On the other hand, one might not need the full gain. The opportunity then presents itself of using some his $\boldsymbol{h}$-frequency pre-emphasis by leaving a small capacitor across the second emitrer resistor. By suitable choice of values it should be possible to use the same capacitor during recording and playback and end up with a flat overall response.

The bass loss due to the head winding-resistance can be compensated, at the expense of gain, by connecting a series RC network across $\mathrm{R}_{1}$. The effect of $2 \mathrm{k} \Omega$ and $0.5 \mu \mathrm{~F}$ is shown by the dotted curve in Fig. 11. With $\mathrm{C}_{3}=0$, the shape of the h.f. response was unaffected, but with $\mathrm{C}_{3}=0.1 \mu \mathrm{~F}$ the h.f. lift at $10 \mathrm{kc} / \mathrm{s}$ was reduced by about 4 dB . Partial l.f. compensation can be obtained by selecting a value for $\mathrm{C}_{1}$ which resonates with $\mathrm{L}_{2}$ near the l.f. end of the response curve. The effect is shown in Fig. 12. As the resonant frequency is reduced, the circuit $Q$ falls, and there is no peak in the response.
High-Impedance Input.-If the feedback loop is broken, the impedance looking into the break is high. This can $b:$ useful if one has a high-impedance signal source which must not be loaded appreciably by the amplifier. One then connects the signal source in place of $R_{5}$.

The input impedance can be measured by means of the circuit of Fig. 13. In this, there is no d.c. feedback, because to measure the impedance it is necessary to alter R, and this would upset the static conditions if $R$ were carrying the base current of V1. With $\mathrm{R}=0$, apply an input signal big enough to produce a sizeable meter reading. Then adjust R so that this reading is halved. R is now the same as the input impedance. It can easily be a few hundred kilohms. An a.c. feedback pair along the lines of Fig. 13, but preferably with proper temperature stabilization of V1, may be useful when the signal source is a crystal pickup or crystal microphone. It is, of course, arguable that it may be just as good to use a straightforward amplifier without a.c. feedback and connect the crystal device to the input in the ordinary way, but with a series resistance big enough to provide an adequate load. For all the writer knows, this arrangement may be satisfactory. There is, however, one apparent virtue in doing it the other way. If the signal source is in the feedback path, the amount of feedback is controlled by the
source impedance. As the latter decreases, the frequency response improves. Th s appears to work out the right way for crystal transducers, since their impedance falls as the frequency is raised.

Some evidence is provided by the following test results. The circuit used was like Fig. 9, but without the inductors, $\mathrm{R}_{5}$, or $\mathrm{C}_{3}$. V1 was biased by a resistor from base to the collcctor supply, and set up with $\mathrm{V}_{c e}=1 \mathrm{~V}$. The input was applied between the emittcr of V 2 and the free end of $\mathrm{C}_{1}$. The input resistance was over $500 \mathrm{k} \Omega$. When the input signal was applied from a low-impedance source in series with 1000 pF (this simulates a crystal device) the output was 3 dB down at $250 \mathrm{c} / \mathrm{s}$ and $16 \mathrm{kc} / \mathrm{s}$.
Conclusion.-Now that the writer has shown, to his own satisfaction, at least, that the d.c. feedback pair is a useful circuit, he will attempt to parry the inevitable question. If a feedback pair is good, why not a feedback triple, or quadruple? Let me say right away that circuits with d.c. feedback over three stages exist (Fig. 14). Readers can look up details in Reference 4. But there are a couple of snags. One


Fig. 13. Circuit for measuring imput impedance, looking into the feedback loop.


Fig. 14. D.C. Feedback Triple. In one variant, all the emitters are returned to earth directly.
is that, with germanium transistors, the temperature drift may be so great that the third transistor bottoms as the tcmperature rises. The point is that, with three stages, the drift of the first transistor gets amplified rather a lot before it reaches the third transistor, and may overload it. It's all right with
silicon, but hardly with germanium transistors. Before readers who are familiar with Reference 4 rush to get pen and paper to write me rude letters, let me say that two of the germanium transistors in the threetransistor direct-coupled hearing aid described in it are not cperated on the linear part of the $\mathrm{V}_{c}-\mathrm{I}_{c}$ characteristics, bat below the knee.

The other snag is that negative feedback over three stages isn't always practicable. If audio transistors are used, internal phase shifts may turn the amplifier into an oscillator if one attempts to apply a substantial amount of feedback. However, this objection is less valid if transistors with cut-off
frequencies in the r.f. region are used, as for example in the amplifier described by R. C. Bowes in the July issue.

## References

${ }^{1}$ J. S. Murray, "Transistors Bias Stabilization," Electronic and Radio Engineer, May, 1957.
${ }^{2}$ S. D. Berry, "Transistor Amplifiers for Sound Broadcasting," B.B.C. Engineering Monograph No. 26, Aug., 1959.

3 P. F. Ridler, "Transistors Tape Pre-amplifier," Wirsless World, Dec., 1958 (correspondence, March, 1959).

4 "Mullard Reference Manual of Transistor Circuits," pp. 165-6 and pp. 268-270.

## BOOKS RECEIVED

Audio Biographies, by G. A. Briggs. With the collaboration of 64 of his contemporaries and frends the author has penetrated the façade of "hi fi" and explored the background, the upbring.ng and the motives which drive and sustain those who practise the art of sound record.ng and reproduction, either as professionals or amateurs. Quite apart from the human interest and the entertaining wit of the author/editor there is a wealth of technical information which should be invaluable to present and future historians. Pp. 343; Fig. 113. Wharfedale Wireless Works Lid., Idle, Bradford. Frice 19s 6d.

Printed Circuits, by J. M. C. Dukes. The book provides the background knowledge necessary for the engineer to undertake the electrical and mechanical design of printed-circuit assemblies at all frequencies up to the microwave region. A useful chapter contains design information for printed inductors, capacitors and resistors, and the bibliography is extensive. Pp. 228; Figs. 91. Macdonald and Co. (Publishers), Lid., 16, Maddox Street, London, W.1. Price 40s.

Two-Way Radio, by Allan Lytel. A comprehensive, practical book on the theory and installation of voicemodulated radio-communication systems. The two main types of modulation, f.m. and a.m., are compared, and the later methods of amplitude-modulation such as single-sideband working are described. Information is given on power supplies, test cquipment and servicing, and a chapter on selective-calling is included. Pp. 291; Figs. 277. McGraw-Hill Publishing Company, Ltd., McGraw-Hill House, 95, Farringdon Strect, London, E.C.4. Price 74s.

Brimar Valve and Teletube Manual No. 9 is the latest in the series of manuals published by the Brimar Commercial Division of Thorn-AEI. Valves and Tubes, Ltd., Rochester. Kent (formerly Brimar Division of S.T.C.). Costing 6s, the new edition incorporates data on many new devices (including bonded-faceplate television c.r.ts) and has a tabular section listing characteristics of obsolere and obsolescent valves. Circuits included in this edition encompass a.f. amplifiers from 1.5 to 75 W output, a crystal-controlled f.m. receiver and an R-C a.f. oscillator.

The Advance Science Master's Handbook, compiled by Ivan L. Muter. Intended to help the science teacher concerned with electricity and electron.cs. The first part of the book contains reference material and basic theory, while the second section is a set of nearly fifty experiments and demonstrations ranging from elementary a.c. theory to pulse circuits. Experiments to illustrate the nature of sound and wave motion are also included. Pp. 124; il'ustrated. Advance Components Ltd., Roebuck Road, Hannault, Ilford, Essex. Free to science teachers; otherwise available at 12 s 6 d .

Dictionary of Electronics, by Harley Carter. A crossindexed, illustrated dictionary. Appendices contain lists of graphical symbols, colour codes and other tabulated data. Pp. 337; illustrated. George Newnes, Ltd., Tower House, Southampton Street, Strand, London, W.C.2. Price 35 s .

Elsevier's Telecommunication Dictionary, compiled by A. Visser. Nearly ten thousand words and expressions are arranged in alphabetical order, using English as the base, with translations in five languages set out underneath. Following the main table, alphabetical lists of the terms in each language are given, and each term is linked to the main table by a refererice number. The languages given are German, Spanish, French, Italian and Dutch. Pp. 1011. D. Van Nostrand Company, Ltd., 358, Kensington High Street, London, W.14. Price £7 7s.

The Mobile Manual For Radio Amateurs. Selected articles on mobile radio equipment, taken from past issues of "QST"" Articles on s.s.b. equipment are included, and there is a complete section on portable and emergency units. Pp. 282. Profusely illustrated. American Radio Relay League, Inc., West Hartford 7, Connecticut, U.S.A. Price $\$ 2$ (in U.S.A.), $\$ 3$ (elsewhere).

Communications (Progress of Science Series), by Charles A. Marshall. Alfords the younger reader an overall view, in non-technical language, of the field of telecommunications, including radar and television. A chapter on careers is included. Pp. 64; Figs. 19; plates 28. Phenix House, Lid., 38, William IV Street, Charing Cross, London, W.C.2. Price 9s 6d.

Sensitometric Control in Film Making, by L. J. Wheeler. Describes the system of sensitometry used to control the continuous processing of films used in B.B.C. Television news programmes. Pp. 22; Figs. 14. A B.B.C. Engineering Monograph. B.B.C. Publications, 35, Marylebone High Strect, London, W.l. Price 5s.

Shortwave Propagation, by Stanley Leinwoll. Directed at both the amateur and the engineer, the book presents the basic principles of propagation on short waves, with chapters on circuit analysis and the preparation of m.u.f. curves. Mathematics are avoided wherever possible. Pp. 151; Figs. 75. John F. Rider (Publisher) Inc. Available from Chapman and Hall, 37, Essex Sireet, London, W.C.2. Price 36s.

Sound Recording Works Like This, by Clement Brown. An introduction to the subject for the layman, which describes in an unsclfconscious way the working of all rypes of equipment, both domestic and professional. Pp. 62; Figs. 60. Phœnix House, 10-13, Bedford Street, Strand, London, W.C.2. Price 9s 6d.

# Radio-Frequency Measurements 

2.-LISSAJOUS FIGURES AND COUNTING TECHNIQUES

By R. BROWN

THE low difference frequency which is the output from some of the comparison systems has to be measured. A quick check through some of the standard textbooks reveals an almost bewildering number of ways in which such a measurement can be made. Many of the techniques described, however, seem now to be of only historical interest, and there seems to be only one or two of these methods of measurement in current use.

## Lissajous Figures

By far the most common method is the one based on the use of Lissajous figures. This is an extremely accurate method, and it is one which calls for no other test equipment than the oscilloscope and a low frequency oscillator. It is a comparison method, the basic set up of which is shown in Fig. 9a.

The frequency to be measured $\left(f_{2}\right)$ is fed to the " $Y$ " plates of the oscilloscope, the " $X$ " plates of which are fed from a reference oscillator ( $f_{1}$ ). A figure will be traced on the oscilloscope, and the shape of this figure will depend upon the ratio of the frequency of $f_{1}$ to $f_{2}$.

The simplest case is where $f_{1}=f_{z}$, and the shape the figure will take can be found with the aid of Fig. 9b. Here $f_{1}$ is represented by the equation

$$
\begin{equation*}
\mathbf{X}=A \sin \theta \tag{7}
\end{equation*}
$$

and $f_{2}$ is represented by the equation

$$
\begin{equation*}
\mathbf{Y}=\mathbf{B} \sin (\theta+\alpha) \tag{8}
\end{equation*}
$$

where $\alpha$ is the phase difference between $f_{1}$ and $f_{2}$.
The two vectors in Fig. 9b, being of the same frequency will rotate at the same speed, and the figure is constructed by marking off the projection of the rotating vector $B$ on the vertical axis-this represents $Y$ in equation (8)-and marking off the projection of the rotating vector $A$ on the horizontal axis-this represents $\mathbf{X}$ in equation (7).

The shape will vary with the phase difference $\alpha$. In Fig. 9b this is $45^{\circ}$ : when the two signals are in phase the ellipse of 9 b closes to a straight line, broadening out again to an ellipse, and then to a full circle as the phase angle increases through $45^{\circ}$ to $90^{\circ}$. This is shown in Fig. 10a.

The procedure when measuring the frequency of $f_{2}$ is simply to adjust the frequency of the reference oscillator ( $f_{1}$ ), until a stationary figure is obtained on the oscilloscope screen. $f_{1}$ and $f_{2}$ are then equal, and their frequency can be read off the reference oscillator tuning dial. This should be known with sufficient accuracy, for most commercial oscillators are accurate to within about $1 \%$, and if the frequency being used is, say, $100 \mathrm{c} / \mathrm{s}$ the error will only be one cycle, and this is one cycle error in the measurement of the high frequency signal. So if the high fre-
 figure.
quency signal were say, $10 \mathrm{Mc} / \mathrm{s}$ this one cycle would amount to one part in $10^{7}$.

Where the two frequencies $f_{1}$ and $f_{2}$ are fixed, and differ by only a fraction of a cycle, as is usually the case when checking fixed frequency oscillators against a standard oscillator for example, a stationary pattern will not be obtained. The phase angle between the two frequencies will slowly change, the rate of change depending upon their frequency difference. The figure on the oscilloscope screen will thus be of the form shown in Fig. 10, but it will change from a straight line, to an ellipse, then a circle and so on as the phase difference changes. If Fig. 9b is redrawn with vector $Y$ say, rotating slightly faster than vector X and the results repeated as the phase difference increases from $0^{\circ}$ to $360^{\circ}$ it will be seen that the rate of rotation of the figure is equal to the frequency difference between $f_{1}$ and $f_{2}$. Frequency difference of as small as a cycle every few minutes can be measured in this way. It is not necessary to use an oscilloscope to time these slow rotations of the Lissajous figures; some quite simple device such as a magic eye tuning indicator can be used.

So far we have only considered the case where $f_{1}$


Fig. 10a, b, c. Some standard Lissajous figures.
is equal to, or very nearly equal to $\mathrm{f}_{2}$. It is often more convenient, however, to have $f_{1}$ a sub-multiple, or a multiple of $f_{2}$. Stationary figures will be obtained when the ratio of $f_{1}$ to $f_{2}$ is $2: 1,1: 2,3: 1$, $1: 3$ etc. Examples of some of these figures are shown in Fig. 10b and 10c. They are all constructed in a similar manner to which Fig. 9b was constructed. Frequency ratios of four, five, six and higher can also be displayed; the figure becomes very complex with high ratios, however, and a ratio of six is about the highest that can be easily distinguished.

From Fig. 9b these intersections can only occur when $Y=+B$, i.e. from (10) when

$$
\begin{equation*}
\sin (p \theta+\alpha)=1 \tag{11}
\end{equation*}
$$

i.e. when $\mathrm{p} \theta+\alpha=\pi / 2,3 \pi / 2$ etc.

Now the figure has a period of $2 \pi$. That is, the figure will be traced out once as $\theta$ goes through $360^{\circ}$ (one revolution of the vector X ). When $\mathrm{p}=1$ there will be only one value of $\mathrm{p} \theta+\alpha$ lying between $0^{\circ}$ and $360^{\circ}$, and so the curve will intersect with the line $+B$ only once. When $\mathrm{p}=2$ there will be two values of $\mathrm{p} \theta+\alpha$ lying between $0^{\circ}$ and $360^{\circ}$, and the curve intersects with the line $+B$ when $\theta=\frac{\pi}{4}-\frac{\alpha}{4}$ and when $\theta=\frac{5 \pi}{4}-\frac{\alpha_{2}}{4}$ In the same way when $p=3$ there will be three values of $\mathrm{p} \theta+\alpha$ lying between $0^{\circ}$ and $360^{\circ}$, and the curve will intersect with the line $+B$ when $\theta=\frac{\pi}{6}-\frac{\alpha,}{6}$ when $\theta=\frac{5 \pi}{6}-\frac{\alpha}{6}$ and when $\theta=\frac{9 \pi}{6}-\frac{\alpha}{6}$ And so on for high values of $p$.
As has been said the highest frequency ratio $p$ that can be easily distinguished, at least by people who don't spend the whole of their lives looking at Lissajous figures, is about six to one. One way of viewing high frequency ratios is by connecting the lowest frequency to both the ' X ' and ' Y ' plates, and the higher frequency to the grid or cathode of the cathode ray tube so that it intensity modulates the beam. The lower frequency signal is connected to the tube via a resistance-capacitance phase shifting network as shown in Fig. 11a. The ' X ' and ' Y ' plates will thus have connected to them signals of the same frequency, but which have a large phase difference, approaching $90^{\circ}$. Hence an ellipse, which is very nearly a circle, will be displayed on the oscilloscope. The time taken to

Fig. Il (a). Determining frequency ratios up to $50: 1$.
(b) Determinotion of frequency ratios greater than $50 \%$.


An important rule for determining the ratio of $f_{2}$ to $f_{1}$ can be found from these figures. Examining the three left-hand figures of each frequency ratio, that is the figures in which the go and return traces are separate, it can be seen that the number of times the curve intersects with the line $+B$ is the same as the frequency ratio. That this must be so may be seen from the following:-
Let $f_{1}$ be represented by

$$
\begin{equation*}
X=A \sin \theta \tag{9}
\end{equation*}
$$

as before, and let $f_{2}$ be represented by
$\mathrm{Y}=\mathrm{B} \sin (\mathrm{p} \theta+\alpha)$


Fig. 12. Digital frequency meter-the counter displays frequency directly.
display the figures once will, as before, be the period of one cycle of the low frequency. The high frequency signal, which is being used to intensitymodulate the tube will shut off the beam on the peaks of the positive or negative half cycle (depending upon how it is connected). The result will be to produce a figure of the form shown in Fig. 11b, a broken circle. Since the circle is being displayed once for every cycle of the low frequency the number of blank spots must be equal to the ratio between the two frequencies.
As with Lissajous figures a stationary figure will only be obtained when one frequency is an exact multiple of the other. When the frequency is close to, but not an exact multiple the pattern will rotate slowly. Using this method frequency ratios of up to $50: 1$ can be determined. Much higher ratios can be determined by using a second oscillator, whose frequency need not be accurately known, and a second oscilloscope. This is shown in Fig. 11c.
A number of other similar comparison techniques use an oscilloscope, ${ }^{18}$ and stroboscopes are also used to measure low frequencies.

## Counter-type Frequency Meters

Frequency measuring techniques based on' counters are being increasingly used. Where the accuracy required lies between about one part in $10^{4}$ and one part in $10^{8}$ the use of counters is becoming almost universal. This is largely because of the extreme simplicity of operation of the counter-type frequency meter.
A simple arrangement is shown in Fig. 12. The signal to be measured is connected to the input of the counter via a gate. When the measurement is to be made a trigger pulse is used to open the gate. The counter starts to count the individual cycles of the signal being measured; after one second a second trigger pulse closes the gate, and the counter stops counting. There will thus be displayed on the counter the number of cycles in one second of the signal being measured-that is its frequency. This count is usually repeated automatically. One small snag with this arrangement is that while the count is being made no information is presented to the operator, and conversely when the count is being displayed no information can enter the counter. This can be avoided if the counting and display sections are separate and if a memory device is included. ${ }^{19}$ The memory system holds a count and displays it continuously while the new count is being accumulated. At the end of each counting
interval the new count is transferred to the display in a very brief time- $100 \mu \mathrm{~s}$ in a commercial instrument. Thus the frequency is displayed practically continuously and the counter is collecting information on the frequency also almost continuously.
The trigger pulses, since they determine the width of the gate, must occur at accurately known intervals of time. A $100 \mathrm{kc} / \mathrm{s}$ crystal oscillator is usually the basic standard for determining this, the one per second trigger pulses being obtained by successive division of the $100 \mathrm{kc} / \mathrm{s}$ signal.

The highest frequency that can be measured is limited by the speed of the counter. In commercial instruments it is usually one megacycle or ten megacycles. ${ }^{20,}{ }^{21}$

Any frequency within the range of the counter can, however, be measured simply by connecting it to the input of the counter, no adjustments being required.
To measure frequencies above the top limit of the counter, heterodyne techniques can be used. A suitable arrangement is shown in Fig. 13. The


Fig. 13. Measuring frequencies above the upper limit of the counter by means of o heterodyne unit.
local oscillator can be locked, at $10 \mathrm{Mc} / \mathrm{s}$ intervals in the case of a $10 \mathrm{Mc} / \mathrm{s}$ counter, to the harmonics of the crystal oscillator. If the frequency to be measured was, say, $26 \mathrm{Mc} / \mathrm{s}$, the local oscillator would be tuned to $20 \mathrm{Mc} / \mathrm{s}$ and locked to one of the crystal harmonics. The local oscillator output is then mixed with the signal in the mixer, and the difference frequency, $26 \mathrm{Mc} / \mathrm{s}-20 \mathrm{Mc} / \mathrm{s}=6 \mathrm{Mc} / \mathrm{s}$, is passed on to the counter and displayed.

With this sort of arrangement the signal frequency is given by the sum of the local oscillator frequency, and the frequency displayed on the counter. Some adjustment is now necessary when making measurements, but once the local oscillator has been set up any frequency over a $10 \mathrm{Mc} / \mathrm{s}$ band can be measured without any further adjustment.

This type of frequency meter suffers from two types of error. There is first of all the effects of an error in the standard $100 \mathrm{kc} / \mathrm{s}$ frequency which produces errors in the gate period. When using a heterodyne system, however, the local oscillator frequency will also be in error, and this error will add to the error in the gate period. If the $100 \mathrm{kc} / \mathrm{s}$ signal was for example slightly high, the gate period would be shorter than it should be. The local oscillator frequency would then be higher than it should be, causing the difference frequency to be low. The error in the standard frequency would thus result in low difference frequency and a short gate period. It is shown in the appendix, however,


Fig. 14. A frequency measuring receiver. Either the loudspeaker or the C.R.O. can be used.
ROM STANDARD
OSCILLATOR
that the total error can never be greater than the error in the local standard.

The second source of error, and this is peculiar to counters, is what is called gate error. There is no direct relationship between the signal being measured and the trigger pulses that open the gate; the point in time when the trigger pulses arrive can be at any point on the signal waveform. Whether or not the first cycle is counted will depend upon what point on the waveform the gate opens, and an error of $\pm 1$ digit is possible.

This error is the same, one digit, whatever the length of the gate period, so its effect can be consider-
ably reduced by lengthening the gate period. A ten second gate can be used, for instance, and if the frequency being measured was, say, $10 \mathrm{Mc} / \mathrm{s}$, then $10^{8}$ cycles would be counted in the gate period and the gate error of one digit would then be equivalent to only 1 in $10^{8}$. The displayed count must then be divided by ten, of course, and this does rather increase the possibility of errors due to misreading.

Counters with much higher counting rates seem to be just around the corner, and counter-type frequency measuring systems using computer techniques have also been described. ${ }^{22}$

## Frequency Measuring Receivers

Errors due to misreading are always a possibility with frequency measuring systems, particularly the more sophisticated ones. Where readings have to be taken over a long period this can become a serious problem, and special care has to be taken with the design of the operating controls and read-out sections.

A technique which while covering a wide frequency range is almost free of misreading errors is the frequency measuring receiver. A simple type is shown in Fig. 14. The receiver, a conventional one, is tuned accurately to the signal to be measured. The heterodyne oscillator is then tuned until it is set to a frequency corresponding to the nearest whole number of kilocycles below the frequency to be measured, the accuracy of the oscillator setting being checked against the harmonics from the $1 \mathrm{kc} / \mathrm{s}$ multivibrator.

The heterodyne note produced in the receiver output will thus be below $1 \mathrm{kc} / \mathrm{s}$. The output from
(Continued on page 647)

## APPENDIX

That the total error can never be proportionately greater than the error in the local standard when using a counter in a heterodyne set-up can be seen in the following way. Any error in the local standard will cause the frequency of the local oscillator to

be in error and the gate interval to be in error. Suppose this error is a small fraction e, and the nominal local oscillator frequency is fo, then the possible limits of the local oscillator frequency will be

$$
\begin{equation*}
\mathrm{f}_{0}^{\prime}=\mathrm{f}_{\mathrm{o}}(1 \pm \mathrm{e}) \tag{1}
\end{equation*}
$$

The difference frequency $f_{d}$ between the local oscillator frequency and the signal frequency $f_{0}$ will, therefore, be somewhere between the limits

$$
\begin{equation*}
f_{d}=f_{b}-f_{0}(1 \pm e) \tag{2}
\end{equation*}
$$

Next consider the effect of the error in the local standard on the gate interval. If $f_{g}$ is the nominal gate frequency then the actual gate frequency will vary between the limits
$\mathrm{f}_{\mathrm{b}}^{\prime}=\mathrm{f}_{\mathrm{g}}(1 \pm \mathrm{e})$
But the gate time interval $t_{g}{ }^{\prime}$ is given by $1 / \mathrm{f}_{\mathrm{g}}{ }^{\prime}$.
Hence

$$
\begin{equation*}
\mathrm{t}_{\mathrm{g}}{ }^{\prime}=\frac{1}{\mathrm{f}_{\mathrm{g}}(1 \pm \mathrm{e})} \tag{4}
\end{equation*}
$$

For a frequency $f_{d}$ counted for a time interval $t_{b}$ the counter display will be N where N is given by $\mathrm{f}_{\mathrm{d}} \times \mathrm{t}_{\mathrm{g}}$, and the actual indicated count will vary between the limits

$$
\begin{equation*}
N=f_{\mathrm{t}} t_{\mathrm{s}}(1 \mathrm{e}) \tag{5}
\end{equation*}
$$

The indicated frequency $\mathrm{N} / \mathrm{t}_{\mathrm{s}}$ will thus vary between the limits

$$
\begin{equation*}
f=N / t_{p}=f_{d}(1 \mp e) \tag{6}
\end{equation*}
$$

The actual indicated value of the signal frequency $f_{s}$ can now be found by adding the nominal value of the local oscillator frequency to this, or $f_{s}=f_{o}{ }^{\prime}+f_{d}(1 \mp e)$
Substituting for $f_{d}$ in equation (2) we get

$$
\begin{aligned}
\mathrm{f}_{\mathrm{s}} & =\mathrm{f}_{\mathrm{o}}+\left[\mathrm{f}_{\mathrm{s}}-\mathrm{f}_{\mathrm{o}}(1 \pm \mathrm{e})\right] \quad(1 \mp \mathrm{Fe}) \\
& =\mathrm{f}_{\mathrm{s}} \mp e \mathrm{f}_{\mathrm{s}}+\mathrm{e}^{2 f_{\mathrm{o}}}
\end{aligned}
$$

If we ignore the second order terms, which we can do since e is normally a very small fraction, then the limits of error in the measurement are given by Fef $_{\text {s }}$.
an audio oscillator is then mixed with the heterodyne note, and the audio oscillator tuned until it zero beats with the heterodyne note. The reading of the audio oscillator tuning plus the reading of the heterodyne oscillator tuning then gives the signal frequency. ${ }^{23}$

A counter can be included in the receiver to further increase the simplicity of operation, and one such arrangement is shown in Fig. 15. A receiver covering the desired range in 1 $\mathrm{Mc} / \mathrm{s}$ bands is used. If the frequency to be measured was, say, $6.3 \mathrm{Mc} / \mathrm{s}$, the receiver would be switcked to the 6 $\mathrm{Mc} / \mathrm{s}$ band, and tuned to $6.3 \mathrm{Mc} / \mathrm{s}$. The range switch will have caused the first local oscillator to be locked to the 50 th harmonic of the standard, that is to $5 \mathrm{Mc} / \mathrm{s}$. The signal is mixed with this to give a difference frequency of $1.3 \mathrm{Mc} / \mathrm{s}$. The output from a variable frequency oscillator, covering $900 \mathrm{kc} / \mathrm{s}$ to $1.9 \mathrm{Mc} / \mathrm{s}$, is mixed with this, and the oscillator tuning is set to give an accurate difference frequency of $100 \mathrm{kc} / \mathrm{s}$. This tuning is checked by comparing the $100 \mathrm{kc} / \mathrm{s}$ difference frequency with the standard $100 \mathrm{kc} / \mathrm{s}$ using Lissajous figures. The variable oscillator output at 1.2 $\mathrm{Mc} / \mathrm{s}$ is now mixed with the 9 th harmonic of the 100 $\mathrm{kc} / \mathrm{s}$ standard to produce a $300 \mathrm{kc} / \mathrm{s}$ difference frequency which is displayed on the counter. The frequency of the signal is thus given by the frequency range in use, $6 \mathrm{Mc} / \mathrm{s}$, and the counter reading, $300 \mathrm{kc} / \mathrm{s}$, as $6.3 \mathrm{Mc} / \mathrm{s}$.

Practical counter type frequency measuring receivers are usually more complicated than this; but despite the high inherent accuracy of such a system frequency measurement is no more difficult


Fig. 15. A frequency measuring receiver using a ccunter.
than tuning the receiver to the signal to be measured. Quite an improvement on some of the earlier high accuracy systems where a training period of anything from three to six months was usually required.

## References

18. F. R. Stansel, "An Interpolation Method for Setting Laboratory Oscillators", Bell Laboratories Record, 1940, Vol. 19, p. 98.
19. "A Frequency Counter with a Memory and with Built-in Reliability", The General Radio Experimenter, Vol. 35, No. 5, p. 3, May 1961.
20. D. W. Bissett, " $10 \mathrm{Mc} / \mathrm{s}$ Electronic Counter Type TF $1345^{\prime \prime}$, Marconi Instrumentation, Vol. 7, No. 5, p. 133, 1960.
21. A. S. Bagley, "A $10 \mathrm{Mc} / \mathrm{s}$ Scaler for Nucleat Counting and Frequency Measurements", HewlettPackard 7., Vol. 2, p. 1, October, 1950.
22. J. Stevenson, "Digital Rate Synthesis for Frequency Measurement and Control", Proc. I.R.E.: December 1959.
23. J. Treeby Dickenson, "International Monitoring" Wireless World, Vol. 59, p. 422, Sept. 1953.

## HORN RADIATOR

ON a 1,000 -acre site near Rumford, Maine, U.S.A., Bell Telephone Laboratories is installing what is said to be the world's largest horn aerial as part of a new experimental space communications station. The 250 -ton steel and aluminium structure will be a rotating aerial- 177 ft long, 94 ft high, and will be protected from the weather by an inflated spherical cover, or radome, 210 ft wide, - 161 ft high.

The huge horn will rotate on two concentric circular tracks on the ground. It will also "roll" about its horizontal axis so that it can follow a satellite from low to high angles of elevation.

Carried around on the structure with the horn will be two "houses" for equipment including a travellingwave maser.

The radome will be supported by air pressure of one tenth of a pound per square inch greater than the outside atmospheric pressure. It will be anchored to the top of a 14 -foot wall that will encircle the base of the aerial. Double doors provide an "air lock" to avoid losing pressure.

> Cut-away drowing of the Bell horn radiator inside its radome. Eventually five such structures may be built on the Rumford site.


## MANUFACIURETRS' PRODUCLSS

## NEW ELECTRONIC EQUIPMENT AND ACCESSORIES

## Capacitance-Type Moisture Meter

SIMPLICITY of operation is afforded by the single knob control of the "Varsity" moisture meter, in which the capacitance method of measurement is employed at a frequency of $100 \mathrm{Mc} / \mathrm{s}$. Readings are obtained by noting the combined readings of a 10 -turn calibrated control and a moving coil meter. The meter reading can be converted to moisture content by means of a graph or a transparent scale placed over the meter. The


Show "Varsity" moisture meter. Material sample is placed in $2,000 \mathrm{~cm}^{3}$ container on top of the instrument.
instrument is fully stabilized for mains variations of $190 \mathrm{~V}-260 \mathrm{~V}$. Details are obtainable from Shaw Moisture Meters Ltd., Rawson Road, Westgate, Bradford.

## Direct Writing Recorder

A SINGLE-CHANNEL recorder, the R.1, with a choice of two writing systems, is announced by Devices Ltd. Either a hot stylus on heat-sensitive paper using rectilinear co-ordinates, or an ink pen on curvilinear coordinates may be used, and any of six paper speeds can be selected. The sensitivity is $0.5 \mathrm{~V} / \mathrm{cm}$ or with preamplifier $0.5 \mathrm{mV} / \mathrm{cm}$, giving a linear excursion of 5 cm .


Devices R.I. recorder, with hot stylus unit in use. This may quickly be interchanged with an ink pen system.

A differential feedback amplifier is employed, and the frequency response of the complete instrument is 0-65 $\mathrm{c} / \mathrm{s}(-3 \mathrm{~dB})$. Full details of the instrument, which uses transistors throughout, may be obtained from Devices Sales Ltd., 13-15 Broadwater Road, Welwyn Garden City, Herts.

## Polar Recording Turntable

IN conjunction with level recorder Type 2305, the Brüel and Kjaer turntable Type 3921 enables directional measurements to be made on aerials, microphones, loudspeakers, etc., and the results automatically recorded on polar co-ordinate graph paper. The item under test may be either bolted to the table by means of the threaded holes provided, or may be mounted centrally in the chuck. The specimen can be provided


Brüel and Kjaer polar recórding turntable.
with power or signals via a slip-ring arrangement below the table. Full details are obtainable from B. and K. Laboratories, Ltd., 4 Tilney Street, Park Lane, London, W.1.

## Adjustable Delay Line

VARIABLE magnetostrictive delay lines with delays between $2 \mu \mathrm{sec}$ and $20 \mu \mathrm{sec}$ are announced by Sealectro. The unit is contained in a hermetically sealed steel case, and adjusiment of the delay is by means of a single screw. The maximum pulse repetition rate is $500 \mathrm{kc} / \mathrm{s}$, with a pulse width of $1 \mu \mathrm{sec}$. Input and output impe-

Sealectro Deltime Type 157 varioble delay line. Adjustment screw is ot left-hond end.

dances are 400 ohms and insertion loss is 45 dB . A complete description can be obtained from Sealectro Corporation, Hersham Factory Estate, Walton-onThames, Surrey.

## Inexpensive Oscilloscope

ALTHOUGH marketed at the very low price of $£ 36$, the Model 381 general-purpose oscilloscope is capable of a high performance. The Y-amplifier has a band-


Dartronic Model 381 oscilloscope.
width of $0-9 \mathrm{Mc} / \mathrm{s}$, a rise time of 40 nsec . and a sensitivity of 100 mV r.m.s. $/ \mathrm{cm}$. Input impedance is 1 M and 20 pF . The timebase speed is from $0.55 \mu \mathrm{sec} /$ cm to $0.15 \mathrm{sec} / \mathrm{cm}$ and the waveform is made available at the front panel. Accessibility for servicing is assured by the sensible construction; the top, bottom and side panels are removable, and most of the circuitry is mounted on two vertical panels. The instrument is made by Dartronic Ltd., 3, 5 and 7 Windmill Lane, London, E. 15 .

## Sensitive Millivoltmeter

ALTERNATING voltages from $300 \mu \mathrm{~V}$ in the range $100 \mathrm{c} / \mathrm{s}$ to $900 \mathrm{Mc} / \mathrm{s}$ may be measured by means of the Airmec Type 301. Measurement of direct voltages may be made in the range $100 \mu \mathrm{~V}$ to 10 V .


Airmec millivoltmeter Type 301.
The amplifier is direct-coupled throughout, stability being achieved by the use of chopper. A semiconductor rectifying probe allows the use of a simplified attenuator
which needs no frequency-compensation. The input impedance is $5 \mathrm{M} \Omega$ on d.v. ranges and when measuring alternating voltage varies from $120 \mathrm{k} \Omega+2 \mathrm{pf}$ at $100 \mathrm{kc} / \mathrm{s}$ to $3 \mathrm{k} \Omega+2 \mathrm{pf}$ at $200 \mathrm{Mc} / \mathrm{s}$ and above. Fluctuation of reading with $\pm 10 \%$ mains variation is less than $\pm 1.5 \%$ on all ranges. Full details are obtainable from Airmec Ltd., High Wycombe, Bucks.

## Wobbulator Attachment

TO extend the coverage of currently-available sweepfrequency generators to the Bands IV and V region, Grundig have introduced their VS-2 u.h.f. converter. The output of the existing generator is set to $55 \mathrm{Mc} / \mathrm{s}$ and applied to the converter, where it is mixed with


Grundig VS-2 u.h.f. converter for wobbulators.
the output of a u.h.f. oscillator. The resultant signal covers the range $460-795 \mathrm{Mc} / \mathrm{s}$ and the level is -13 dB on the output of the sweep frequency generator. Input and output impedances are $60 \Omega$ unbalanced. The converter costs $£ 30$, and is available from the British distributors, Wolsey Electronics, Ltd., Cray Avenue, St. Mary Cray, Orpington, Kent.

## Cable Identifier

DESIGNED for application without tools, the Helagrip is a flexible p.v.c. sleeve supplied in sizes to fit cables of $\frac{1}{8}$-in to $\frac{7}{16}-$ in dia. The indented edge of the sleeve prevents adjacent pieces twisting relative to each other, and the special section prevents sliding. The sleeving is supplied partially cut in lengths of identical coding (A-Z, 0-9).
Further details may be obtained from Hellermann, Ltd., Gatwick Road, Crawley, Sussex.
"Helagrip " cable identifier.


## DECEMBER MEETINGS

Tickers are required for some meetings; readers are advised, therefore, to communicate with the secretary of the society concerned.

## LONDON

4th. I.E.E.-Discussion on " Backward waves in waveguides" opened by Dr. P. J. B. Clarricoats, R. A. Waldron and G. H. B Thompson at 5.30 at Savoy Place, W.C. 2.
6th. Brit.I.R.E.-Discussion on " Possible uses of computers in medical diagnosis" opened by Dr. A. D. Booth at 6.0 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C. 1 .

8th. Institute of Physics and Physical Society.-"Electron microscopy in Japan " by T. Mulvey and Dr. M. Whelan at 2.30 at 47 Belgrave Square, S. W. 1 .

8th. Television Society.-" Remote control operation of television cameras" by H. C. Nickels at 7.0 at the Cinematograph Exhibitors' Association, 164 Shaftesbury Avenue, W.C. 2.

11th. I.E.E. Graduate and Student Section. -"The professional engineer and an expanding industry" by G. S. C. Lucas at 6.45 at Savoy Place, W.C.2. 12th. I.E.E.-"Diversity reception and automatic phase reception" by L. Lewin at 5.30 at Savoy Place, W.C. 2.

12 th. Institute of Physics and Physical Society.-"Integrated electronics" by Dr. W. J. Granville at 5.30 at 47 Belgrave Square, S.W.1.
14th. Brit.I.R.E.-Symposium on "Constant luminance colour television" including papers by I. J. P. James and W. A. Karwowski, W. N. Sproson, A. V. Lord, K. Hacking and G. F. Newell at 6.0 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C. 1 .

14th. Radar \& Electronics Association. -" Loudspeaker enclosures" by J. Gough and Prof. F. Landgrebe at 7.0 at the Royal Society of Arts, John Adam Street, W.C.2.

15th. Television Society.-"The "Nev-Eye' vidicon camera" by N. S. Rutherford at 7.0 at the Cinematograph Exhibitors' Association, 164 Shaftesbury Avenue, W.C.2.

15th. B.S.R.A.-" Problems in telephone transmission" by D. L. Richards at 7.15 at the Royal Society of Arts, John Adam Street, W.C.2.

18th. I.E.E.-" Large microwave steerable aerials for communication with artificial earth satellites and space probes" by F. J. D. Taylor at 5.30 at Savoy Place, W.C. 2.
20th. I.E.E.-" Satellite instrumentation" by Dr. R. L. F. Boyd at 5.30 at Savoy Place, W.C. 2.

## ARBORFIELD

11th. I.E.E. Graduate \& Student Sec-tion.-"Design of service equipment" by B. W. Norman at 7.0 at the Unit Cinema, 3 (Tels.) Training Bn., R.E.M.E.

## BIRMINGHAM

4th. I.E.E.-"The banana-tube display system-a new approach to the display of colour-television pictures "by Dr. P. Schagen at 6.30 at the College of Technology. (Joint meeting with the Institution of Post Office Electrical Engineers.)

8th. Society of Instrument Technology. " Instruments in clinical chemistry" by N Crawford and "Electronics in surgery" by R. Lightwood at 7.0 at the College of Technology, Aston Street.

12th. Institute of Physics and Physical Society. - "The observation of radio stars" by Dr. P. F. Scott at 6.30 at the Midland Institute.

14th. Brit.I.R.E.-" The R.R.E. radiotelescope interferometer" by H. Gent at 6.15 at the Electrical Engineering Department, The University.

## "WIRELESS WORLD" PUBLICATIONS



## BRADFORD

5th. I.E.E.-" The potentialities of artificial earth satellites for radiocommunication" by W. J. Bray at 6.30 at the Institute of Technology.

## BRISTOL

14th. Society of Instrument Tech-nology.-"The atomic clock" by Dr. L. Essen at 7.30 at the Department of Physics, the University.

20th. Brit.I.R.E.-Annual general meeting of the South-Western Section followed by "Transistors in transmitters and communications receivers" by D. C. Carey at 6.0 at the School of Management Studies, Unity Street.

## CAMBRIDGE

12th. I.E.E.--" The banana-tube display system-a new approach to the display of colour television pictures" by Dr. P. Schagen at 8.0 at the Cavendish Laboratory, Free School Lane.

## CARDIFF

6th. Brit.I.R.E.-" Microwave valves" by R. W. White at 6.30 at the Welsh College of Advanced Technology.

## CHELTENHAM

1st. Brit.I.R.E.-" Electronic telephone exchanges" by J. F. Hesketh at 7.0 at the North Gloucestershire Technical College.

## EDINBURGH

5th. I.E.E.-" Precision Measurement" by G. H. Rayner and A. Felton at 7.0 at the Carlton Hotel.

13th. Bri.I.R.E.-" Jodrell Bank" by J. B. Wilson at 7.0 at the Department of Natural Philosophy, The University, Drummond Street.

## FARNBOROUGH

7th. I.E.E. Graduate and Student Section.-"The synthesis of speech for communication purposes" by H. L. Chesters at 6.30 at the Technical College.

## FAWLEY

1st. Society of Instrument Techno-logy.-"Applications of transistors and diodes" by D. Osborne at 5.45 in Room 4a, Administration Building, Esso Petroleum Co.

## GLASGOW

4th. I.E.E.-" Precision measurement" by G. H. Rayner and A. Felton at 6.0 at the Royal College of Science and Technology.

14th. Brit.I.R.E.-" Jodrell Bank" by J. B. Wilson at 7.0 at the Institution of Engineers and Shipbuilders, 39 Elmbank Crescent.

## GRANGEMOUTH

21st. Society of Instrument Tech-nology.-"Instrumentation of space vehicles" by Dr. A. E. Roy at 7.0 at the Leapark Hotel, Bo'ness Road.

## LEICESTER

6th. Brit.I.R.E.-"Transistors in computets and control equipment" by $P$. James at 6.45 at the University.

12th. I.E.E.-"Altitude control of earth satellites" by B. Stewart at 6.30 at the Lecture Theatre, E.M.G.B. Showrooms, Charles Street.

## LINCOLN

7th. I.E.E.-Discussion on "Semiconductors for light-current engineering" opened by L. Rushforth at 7.30 at the E.M.E.B. Showrooms, 191 High Street.

## LIVERPOOL

4th. I.E.E.-" Simulation of intelligence" by Prof. D. M. MacKay at 6.30 at the Royal Institution.

13th. Brit.I.R.E.-"Nuclear power station instrumentation " by $M$. W. Jervis at 7.30 at the Walker Art Gallery.
14th. Society of Instrument Technology. -"The versatility of the electronic potentiometer" by F. W. J. Howard at 7.0 at the Merseyside and North Wales Electricity Board Industrial Centre, Paradise Street.

18th. I.E.E. -" Education of an electrical engineer" by Prof. M. R. Gavin and "The place of formal study in the post-graduate training of an electrical engineer" at 6.30 at the Royal Institution.

## MAIDSTONE

 postal mail services" by G. P. Copping at 7.0 at the "Wig and Gown."

## MANCHESTER

6th. I.E.E.- " Generation and amplification in the millimetre wave field" by W. E. Willshaw at 6.25 at the Engineers' Club, Albert Square.
7th. Brit.I.R.E.-"Radar for civil aviation purposes " by K. F. Slater at 7.0 at the Reynolds Hall, College of Technology.

## NEWCASTLE-UPON-TYNE

4th. I.E.E.- " Planning and installation of the sound broadcasting headquarters for the B.B.C.'s Overseas and European Services" by F. Axon and O. H. Barron at 6.15 at the Rutherford College of Technology, Northumberland Road.

13th. Brit.I.R.E.-" Masers and parametric amplifiers" by Dr. T. H. Wilmhurst at 6.0 at the Institute of Mining and Mechanical Engineers, Neville Hall, Westgate Road.

18th. I.E.E.-" Heaviside-his life and work" by Prof. R. L. Russell at 6.15 at the Rutherford College of Technology, Northumberland Road.

## PORTSMOUTH

13th. I.E.E.-Discussion on "Silicon controlled rectifiers" opened by R. J. Alexander, J. P. Birchenough and R. Thompson at 6.30 at the C.E.G.B. Offices, 111 High Street.

## SHEFFIELD

13th. I.E.E.-"Millimetre waves" by Dr. J. Allison at 6.30 at the University.

## SOUTHAMPTON

12th. I.E.E.-Discussion on " High speed measuring techniques in the nano-second region" opened by B. H. Venning and D. Grollet at 6.30 at the University.

## WEYMOUTH

1st. I.E.E.-"The banana tube" by Dr. P. Schagen at 6.30 at the South Dorset Technical College.

## WOLVERHAMPTON

6th. Brit.I.R.E.-Symposium on "New electronic techniques in nondestructive testing" at 10.0 at the Wolverhampton and Staffordshire College of Technology.

LIST NO. D. 830

This unique Multi-Legend Indicator has been developed to meet the needs of modern electronic control, measuring and monitoring equipment, where the conventional singnal or warning lamp ife ufien insufficient to portray the sometimes complex operational sequences as they occur. The design enables a display of letters, numbers, words, etc., to be "written up" as the corresponding operations or processes take place. Legends are individually illuminated by 5 mm . tubular L.E.S. (B.S.98/E5) lamps (not supplied) and are normally invisible until "lit." The legending is carried out to customers' requirements and the adjoining illustrations give a few examples of the wide range of applications. The flanged, easy to fit unit is moulded in highly polished black thermo-setting Bakelite, with a contrasting chromium bezel.
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## UNBIASED

## By "FREE GRID"

## In Old Bohemia

AMERICANS often claim to be far ahead of us Europeans-and in particular of us Limeys-in the various activities of life, and in many cases they are, of course, quite justified in their claims. For instance, in some of their big cities, their buildings and their crime statistics are much higher than anything we can boast of.

However, it is mostly in matters of annlied science that the Americans claim to be so turahead of us, and here again they are fully justifed. What European state, for instance, can boast of having had, since 1890 , an electric chair for the administration of what they call "electrocution" but which we old-fashioned grammarians prefer to call "electrocussion"? I believe that American doctors are as out of date as we are when they speak of "concussion," rather than of "concution."
But there is one instance of applied science where the U.S.A. is twenty years behind Europe, as Mr. Kenneth Greenberg, writing to me from the city of sudden and violent death, has made quite clear by sending me a cutting from the October 1957 issue of the American journal Popular Mechanics.

This cutting has an illustration of an American ambulance fitted with a radio transmitter which turns all traffic lights red for a few seconds to give it a clear passage as it speeds on its way.

Mr. Greenberg quite rightly sends this cutting to me to refute the statement I made in the September issue of $W . W$. that the idea had never been put into use. But my statement was all wrong, and it is all the


[^2]more blameworthy in that I had forgotten that in the issue of Dec. 2nd, 1937-nigh on a quarter of a century ago-I myself reported in these columns that I had seen this idea in use in a European city. I can only hang my debowlered head in shame at forgetting my own words, and thus misleading my readers.
I did not mention the name of the city but unless my memory has let me down again it was in the city of Good King Wenceslas that I saw this sight.
7f onv of vou are so ignorant that you don't know the ramit of the land over which Good King Wenceslas ruled, and the name of his capital city-still unchanged today-in which he did his looking out on St. Stephen's Day, I do not consider it my duty to enlighten you. Ask any of the children who sing carols on your doorstep this Christmas.

## Diary Data and Dates

I AM very gratified to see in the "W.W. Diary" for 1962 that the pages in which we record our daily doings have been kept as free from printed matter as possible. Thus the Editor has kept his hagiographical information to a min:mum, only including saints' days and other ecclesiastical information where they coincide with quarter days and halfquarter days.
In the non-diary pages I was a little surprised to see that the terminating sigma (s) had been omitted from the Greek alphabet, but I suppose the reason is that it has no symbolic significance. I suppose, too, that a similar reason, namely lack of usefulness, causes the omission on the page of abbreviations of r.d.f., to denote what we now call radar. I think it is a pity that this was ever allowed to be superseded by the American name of "radar," but it is too late to alter it now.

I was very pleased to see the page of some historic wireless dates. I notice that the adjective "some" is used in the title, but even so I wonder why some dates were omitted. The omission which dismayed me most was the date when the cavity magnetron was invented.*

It is made quite clear in the Diary that G.M.T. is used throughout but I think it is carrying accuracy a bit too far when the time of the Titanic

[^3]disaster is reduced to G.M.T. from local meridian time, thus causing what I regard as the wrong date of 15th April, 1912, to be given for the event which I, and all others who personally remember the disaster have always regarded as occurring on 14th April. It occurred at 11.40 p.m. local meridian time on Sunday, 14th April, but as the ship's longitude was $50^{\circ} 14^{\prime} W$ it would be just after 3 a.m. G.M.T. on 15th April.

## Forty Years On

ALTHOUGH it is only three months since the British National Radio Show closed its doors, preliminary plans for the 1962 show are already being discussed. I think, therefore, I had better remind the organizers that next autumn we shall be celebrating not only the fortieth anniversary of the first radio show, held in the old Horticultural Hall in 1922, but also the fortieth anniversary of the beginning of broadcasting itself; at any rate of regular broadcasting in this country from 2 LO .

I hope these anniversaries will be celebrated in some way at the show next August but we don't want merely a static museum showing a few sets that were on sale in 1922. Of course a museum section could form a part of the exhibition; there is, at any rate, plenty of room for it in the vast open spaces of which I complained in 1960 and which were again in evidence at the last show.

In order to celebrate these two anniversaries I think it would be a good idea for the B.B.C. to combine with receiver manufacturers to bring home to people how excellent is the quality of 1962 compared with that of 1922, not only on the technical side but on the entertainment side also. I am not trying to decry the pioneers of 1922, but, of necessity, they were venturing into a new field of entertainment altogether, and their efforts were naturally somewhat amateurish compared with today's polished standards.

Could not the B.B.C. arrange to give a programme or two of the type we used to get in 1922. I wonder if there are any recordings available. If such programmes were fed through 1922 sets, present day listeners-including youngsters of 40 -would know what we had to put up with in those far off days.

## Senescent Senescience

I MUST accept with becoming grace the rebuke administered to me by Mr. K. W. Mawson of the Royal Eye \& Ear Hospital, Bradford (Nov. issue), concerning remedial measures necessary to combat the hearing defects of the ageing. It is quite clear to me that I have advanced further along the road of senescence than I had supposed, without a corresponding increase in my senescience.

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| $\begin{aligned} & \text { ZD } 518 \\ & \text { CD } 518 \end{aligned}$ | 18 | 10 |
| $\begin{aligned} & \text { ZD } 522 \\ & \text { CD } 522 \end{aligned}$ | 22 | 10 |
| $\begin{aligned} & \text { ZD } 527 \\ & \text { CD } 527 \end{aligned}$ | 27 | 10 |
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| THICKNESS | $: 0.156^{\prime \prime}$ max. | $0.156^{\prime \prime}$ max. |
| WORKING VOLTS $: 3$ d.c. | 3 d.c. |  |


$\begin{array}{llllllll}\text { R } & \text { E } & \text { S } & \text { I } & \text { S } & \text { T } & \text { O } & \text { R } \\ \text { L } & \text { I } & \text { M } & \text { I } & \text { T } & \text { E } & \text { D }\end{array}$

In line with the Erie policy of anticipating the component requirements of the future, the Erie Transcap capacitor is now added to our everincreasing range of components for use with transistors.
Designed specifically as a small, reliable, high capacitance,. low voltage, coupling, and by-pass capacitor, the Erie developed Transcap is manufactured entirely at our Great Yormouth factory.
Styles 811T and 831T shown here in their actual physical sizes are only forerunners of the wide range in differing values and voltages which will ultimately emerge.

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| 2" | (5.1 CM) | Type | 2SM |
| :---: | :---: | :---: | :---: |
| $2 \frac{1}{4}^{\prime \prime}$ | (5.7 CM) | " | 2SS |
| 3" | (7.6 CM) | " | 3SL |
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The four main outputs of the generator are (1) a prepulse of fixed amplitude and width. (2) A single or double main pulse of variable width and amplitude. (3) A single or double negative going sawnooth (sweep) pulse coinciding with the main pulse. (4) A single or double cable pulse derived from the main pulse.
APPLICATIONS of this instrument can be made in many ficlds of research and measurement. Ils comprehensive specification makes it particularly suitable for use in radio navigation, radar, television, electronics, nucleonics, computors, telemetering and physiological research. Other uses will be apparent and the more common applications are listed in a comprehensive leaflet available on written request.

## BRIEF SPECIFICATION

PERIOD: Continuously variable from 0.9 usec to 1.05 sec corresponding with a frequency range $0.95 \mathrm{c} / \mathrm{s}$ to $1.1 \mathrm{Mc} / \mathrm{s}$. Accuracy is within $\pm 5 \%$.

PRE-PULSE: Fixed amplitude 8 V peak in $75 \Omega$ positive going. Fixed width $60 \mathrm{~m} \mu \mathrm{sec}$.

DELAX: The time between the peak of the pre-pulse and the advent of the main pulse is variable from $0.9 \mu \mathrm{sec}$ to 105 msec . Accuracy is within $\pm 5 \%$.

MAIN OUTPUT PULSE: Continuously variable in width from $0.09 \mu \mathrm{sec}$ to 105 msec with a calibration accuracy of $\pm 5 \%$. The amplitude and impedance is controlled by a four position switch and a fine control giving a $4: 1$ attenuation of each maximum as follows

| AMPLITUDE | IMPEDANCE | RISE TIME |
| :---: | :---: | :---: |
| $5 \mathrm{~V} \max$ | $75 \Omega$ | $<10 \mathrm{~m} \mu \mathrm{sec}$ |
| $10 \mathrm{~V} \max$ | $150 \Omega$ | $7.25 \mathrm{~m} \mu \mathrm{sec}$ |
| $25 \mathrm{~V} \max$ | $600 \Omega$ | $740 \mathrm{~m} \mu \mathrm{sec}$ |
| $50 \mathrm{~V} \max$ | $1000 \Omega$ | $550 \mathrm{~m} \mu \mathrm{sec}$ |

POLARITY of the output pulse can be positive or negative going with respect to earth as required. Accuracy of calibration is within $=2 \%$ on all ranges except the 50 V range where it is within $\pm 5 \%$.

THESWEEP waveform is, a direct coupled negative going sawtooth with the same width and delay as the main pulse. The amplitude of this waveform is 15 V peak at maximum width. Linearity is maintained to within $\leq 2 \%$. Output impedance approximately $300 \Omega$.
CABLE PULSE is obtained from a short circuited pure line. Two narrow output pulses are obtained, one positive and one negative going, coincident with the leading and trailing edges of the main pulse. The width of both pulses is 25 nusec. The maximum amplitude is 3 V peak in $75 \Omega$ and rise time 8 musec .
DOUBLE PULSE operation can be obtained by a setting on the fromt panel. Two pulses are produced, the first coincident with the pre-pulse and the second delayed on it by a selected amount.


SYNC/TRIGGER The generator can be synchronised or triggered by almost any externally applied waveform. The minimum amplitude levels for a sinc wave being: $\$$ YNC operation 0.5 V peak to peak $2 \mathrm{Mc} / \mathrm{s}$ max., and trigGer operation 1.0 V peak to peak $2 \mathrm{Mc} / \mathrm{s}$ max. SINGLE SHOT operation obtained by a push-button switch POWER SUPPLY . , $110-120 \mathrm{~V}$ and $200-250 \mathrm{~V}$ a.c. in 10 V steps 40 to $60 \mathrm{c} / \mathrm{s}$
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- Complete suppression of re-trace
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- New D.C. Coupled Flyback Blanking System.

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Wide Range Calibrated Time Base
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Versatile Triggering Circuit gives two modes of triggering:
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[^4]

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## ABRIDGED DATA

4LP31 single gun dual trace tube.


* (The green medium persistence phosphor used by E.T.L. has now been designated P31. If is exactly the same as the E.T.L. phosphor prevlously called P1.)
Capacitances



## Typical Operating Conditions

| $\mathrm{V}_{\mathrm{a} 1} \ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 1.5 kV |
| :--- | :---: | :---: | :---: | :---: | :---: | ---: |
| $\mathrm{V}_{\mathrm{a} 2}$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 320 to 420 V |  |
| $\mathrm{~V}_{\mathrm{a} 3}$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 1.5 kV |
| $\mathrm{V}_{\mathrm{a} 4}$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | 3.0 kV |
| $\mathrm{Vg}_{g}$ (for cut-off) | $\ldots$ | $\ldots$ | $\ldots$ | -40 to -95 V |  |  |
| Sx | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $27 \mathrm{~V} / \mathrm{cm}$ |
| $\mathrm{Sy}^{\prime}$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $27 \mathrm{~V} / \mathrm{cm}$ |
| Sy $^{\prime \prime}$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $27 \mathrm{~V} / \mathrm{cm}$ |

## ETEL

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-1 dB at $0.1 \mathrm{Mc} / \mathrm{s}$
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Measuring range
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## ARTICLES

## IN THE DECEMBER ISSUE INCLUDE:

## FERRITE CORES AS LOGICAL ELEMENTS

In this article the properties of ferrite cores are explained and some of the ways in which they can be arranged to provide logical functions are then described. The operation of a typical core logical circuit is analysed and the implications of the analysis in design is discussed.

## SILICON P-N-P-N SWITCH—2

The newly-developed four-layer semiconductor device which is known as a p-n-p-n switch can be used in many interesting ways to perform a number of functions. This article primarily deals with the practical applications of the p-n-p-n switch. It gives a number of circuits using this new device and briefly describes the operation of each circuit.

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Pholo 185 A


Photo 150 A


Photo 120 A

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## SONTRANIC LIMITED

## No. 4 IN THE SERIES

## Technical Information for the Transistor Circuit Designer

## Thermal Runaway

The maximum temperature at which a circuit will operate is not always determined by the maxımum power rating of the transistor but by its thermal stability in the circuit. The thermal stability of the circeit depends partly on the stability factor which was discussed in an earlier note in this series.
What, then, does the circuit designer want to know?
(1) Given the maximum ambient temperature and power dissipation, he will want to know
the stability factor.
(2) Given a maximum ambient temperature, he will want to know the power he can dissipate
for a given stability factor.
(3) Given the dissipation and stability factor, he will want to know the maximum ambient temperature for safe operation.
For case (1) when the junction temperature (i.e, the ambient temperature and dissipation) and the value of $I_{C B O}$ at that temperature are known, the expression for the stability factor is relatively simple:-

$$
\begin{equation*}
S<\frac{1}{V \theta K I_{C B O}} \tag{1}
\end{equation*}
$$

where $S$ is the stability factor (defined in No. 3 of this series).
$V$ is the voltage
$\theta$ is the thermal resistance of the transistor (in a heat sink if used)
$K$ is a constant $=\frac{\log _{e} 2}{T_{D}}$
where $T_{D}$ is the temperature change to double or halve $I_{C B O}$. $K$ is typically of the order of 0.07 to 0.09 for germanium)
$I_{C B O}$ is the value of the leakage current at the appropriate junction temperature $T_{f}$,
and $T_{J}=T_{a m b}+P_{D} \theta$
where $P_{D}$ is the total device dissipation.
For case (2) the maximum allowable power disslpation is:

$$
\begin{equation*}
P_{D}<\frac{1}{\theta}\left(T_{R}-T_{a m b}+\frac{2.3}{K} \log _{10} \frac{1}{K S V_{C} \theta I_{C B O}}\right) \tag{2}
\end{equation*}
$$

For case (3) the maximum permissible ambient temperature is:

$$
\begin{equation*}
T_{a m b}<\left(T_{R}-P_{D} \theta+\frac{2 \cdot 3}{K} \log _{10} \frac{1}{K S V_{C} \theta I_{C B O}}\right) \tag{3}
\end{equation*}
$$

where $T_{R}$ is some reference temperature (usually $25^{\circ} \mathrm{C}$ ) at which the value of $I_{C B O}$ used in (2) and (3) above is known.
It is clear that the thermal stability can be improved by having a lower value of supply voltage and a more effective heat sink. In estimating the thermal stability, one should always consider the case of those transistors which have the highest values of $I_{C B O}$.
Of course, the above is subject to individual temperature, power and voltage ratings, given in the data sheet, not being exceeded.

| $\begin{gathered} \text { STC } \\ \text { TRANSISTOR TYPE } \end{gathered}$ | $\begin{aligned} & \text { TK } \\ & \text { 20C } \end{aligned}$ | $\begin{aligned} & \text { TK } \\ & 23 C \end{aligned}$ | $\begin{gathered} \mathrm{TK} \\ 25 \mathrm{C} \end{gathered}$ | $\begin{aligned} & 7 K \\ & 28 C \end{aligned}$ | $\begin{aligned} & \text { TK } \\ & 30 \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { TK } \\ & 31 C \end{aligned}$ | $\begin{aligned} & \text { TK } \\ & 40 \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { TK } \\ & 41 C \end{aligned}$ | $\begin{aligned} & \mathrm{TK} \\ & 42 \mathrm{C} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Max. I } \subset 80 \\ & \text { at } 25^{\circ} \mathrm{C}(\mu \mathrm{~A}) \end{aligned}$ | 5 | 5 | 5 | $5 \dagger$ | 5 | 5 | 5 | 6 | 6 |
| $\begin{aligned} & \text { Max. I } \mathrm{CBO} \\ & \text { at } 60^{\circ} \mathrm{C}(\mu \mathrm{~A}) \end{aligned}$ | $30 \dagger$ | $50 \dagger$ | $30 \dagger$ | $30 \dagger$ | $30 \dagger$ | $30+$ | $50 \dagger$ | $50 \dagger$ | $50 \dagger$ |
| $K$ | 0.05* | 0.087 | 0.05 | 0.05 * | 0.05* | 0.05* | 0.087 | 0.087 | 0.087 |

*Note that the value of $K$ for a typical transistor is higher than that for a limit transistor and is about 0.077 .

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Like the ears of a wary fox, the Grampian DP4 microphone is sensitive to an extremely wide range of sounds. With its uniform frequency response from 50 to $15,000 \mathrm{c} / \mathrm{s}$, the reliable. medium-priced DP4 will greatly improve the standard of your recordings.

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# Wireless World 

ELECTRONICS, RADIO, TELEVISION

## DECEMBER1961

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## - Vortexion quality equipment

Will deliver 120 watts continuous signal and over 200 watts peak Audio. It is completely stable with any type or load and may be used to drive motors or other devices to over 120 watts at irequencies from 20,000 down to 30 cps in standard form or other frequencies to order. The distortion is less than $0.2 \%$ and the noise level -95 dB . A floating series parallel output is provided for $100-120 \mathrm{~V}$. or $200-250 \mathrm{~V}$. and this cool running amplifier occupies $12 \frac{1}{4}$ inches of standard rack space by 11 inches deep. Weight 60 lb .

## $30 / 50$ WATT AMPLIFIER

Glves 30 watts continuous signal and 50 watts peak Audio. With voice coil leedback distortion is under 0.1\% and when arranged for tertiary leedback and 100 volt line it is under $0.15 \%$. The hum and noise is better than -85 dB referred to 30 watt.
It is available in our standard steel case with Baxendale tone controls and up to 4 mixed inputs, which may be balanced line 30 ohm microphones. or equalised P.U.s to choice.

120/200 WATT AMPLIFIER


## ELECTRONIC MIXER/AMPLIFIER

This high fidelity 10/15 watt Ultra Linear Amplifier has a built-in mixer and Baxendale tone controls. The standard model has 4 inputs, two lor balanced 30 ohm microphones, one lor pick-up C.C.I.R. compensated and one for tape or radio input. Alternative or additional inputs are available to special order. A leed direct out from the mixer is standard and output impedances of 4-8-16 ohms or 100 volt line are to choice. All inputs and outputs are at the rear and it has been designed for cool continuous operation either on $19 \times 7 \mathrm{in}$. rack panel form or in standard ventilated steel case.
Size $18 \times 7 \frac{1}{2} \times 9 \frac{1}{2} \mathrm{in}$, deep.
Price of standard model $£ 49$.

The 12-way electronic mixer has facilities for mixing 12 balanced line microphones. Each of the 12 lines has its own potted mumetal shielded microphone transiormer and input valve, each control is hermetically sealed. Muting switches are normally fitted on each channel and the unit is fed Irom its own mumetal shielded mains transformer and metal rectifier.

Also 3-way mixers and Peak Programme Meters. 4 -way mixers and $2 \times 5$-way stereo mixers with outputs for echo chambers, etc. Details on request.

## 12-WAY ELECTRONIC MIXER



Full details and prices of the above on request


Don't let gravel choke your Ravel. Don't let fluff fur up your Faith. Keep Britten tidy ! Your records are valuable. Dust and grit are attracted to them by 'static'. If you allow impurities to settle, the stylus must grind them into the groove, damaging the sensitive sound track (and the stylus, too). This greatly reduces the life of your records (and of the stylus, too). By the time you can hear loss of quality, irreparable harm has been done. Prevent damage before it happens. Slip on an Acos Changer Dust Bug - and let it sweep away dirt before the stylus gets there.

The Acos Changer Dust Bug easily clips onto practically every changer arm. Spring action automatically compensates for its weight, and no tracking adjustment is required. A durable Nylon brush cleans the groove, and a plush pad applies anti-static fluid before the stylus, collecting the dirt after. The Acos Dust Bug costs only $17 / 6$ plus $6 / 5$ P.T.

It pays for itself over and over again by giving very much greater record life, and five times longer stylus life.


## "BELLING-LEE" NOTES

## No. 35 of a Series

## Some mechanical aspects of design: Part 8

Standards of sealing are defined in terms of the maximum rate of leakage which will occur in a given time under a stated pressure differential. A typical specification, which applies to Services' Type Approved components (R.C.S. 262) requires that the leakage of gas shall not exceed 1 c.c. per hour under apressure differential of 201 b . per square inch. Notice that this is the total leakage permissible, irrespective of the area of the seal. Thus the maximum leakage per unit area is lower on a large seal than on a small one, but this does not necessarily mean that a small seal is easier to effect, for tolerances become more critical as sizes are reduced.

In the case of hermetic seals, where the rates of leakage are very small indeed, a unit of measurement called the "lusec" is employed. This word has been coined as an abbreviation of litre, micron per second, the letter " $u$ " sometimes being used for the Greek " m " $(\mu)$ which denotes " micro." The lusec is defined as the flow of as much gas into a vessel of 1 litre size as would produce a rate of pressure increase of 1 micron ( .001 mm .) of mercury per second at $0^{\circ} \mathrm{C}$. The pressure differential responsible for the leakage must be stated, of course. The lusec corresponds to a flow of approximately 5 c.c. per hour, but the leakage of quite an ordinary hermetic seal under a pressure differential of one atmosphere is better than $10^{-6}$ lusec, while a good seal measures less than $10^{-10}$ lusec, which is 1 c.c. in approximately 250,000 years !

Seals in the former category, i.e. non-hermetic, find applicat.ons in equipment which has to undergo a relatively short period of stress, e.g. equipment taken up to high altitudes (low pressure) in aircraft. The breakdown voltage of a component which measures 3 kV at sea level may fall to as little as 500 V . under the reduced pressure at $68,000 \mathrm{ft}$., which could be disastrous. Also, since the performance of such seals is considerably higher as regards resistance to passage of moisture (owing to the larger size of the water molecules) they form an effective barrier to ingress by capillary action and by "breathing " which occurs in unsealed equipment as the external pressure rises and falls or as the internal pressure varies due to thermal changes.

Such seals are usually demountable, which means that they are assembled on the job, although they may contain built-in elements. Thus, a typical sealed panel fuseholder, such as L.1382, employs a seal at the panel which is assembled in mounting, but the body contact which is moulded in, is permanently sealed in the process. Incidentially, this requires a special technique because the adhesion of a phenolic moulding material to a metal insert cannot be guaranteed to be gas tight. Demountable seals of this type, in which mechanical pressures are relatively low, employ a resilient sealing medium, such as rubber, situated in an accurately dimensioned cavity. In the case of the fuseholder, L.1382, there is an annular groove of rectangular section in the rear face of the front flange, in which a sealing ring is placed. This ring, in the free state, stands proud of the groove, and makes contact with the panel over a circle. As the fuseholder is tightened on the panel, the ring is mainly distorted, since rubber has only a limited degree of compression, and the area of contact is thereby increased considerably. The sealing ring may be of square or circular cross section, but the latter is generally found to be more effective.

Hermetic seals, which are employed where long-term stability is required, e.g. in valves, transistors and other components where the internal environment must be maintained, and impurities excluded, are formed by fusion, or chemical bonding. Hermetic sealing between metals may be achieved by soldering, brazing, welding, etc., and in the case of glass-metal seals, which are used extensively when electrical insulation is required, an oxide layer of carefully controlled thickness is formed on the metal surface and the glass is melted and bonds to it.

The testing of seals to ensure their literal compliance with specification is a tedious business, even in the case of the lower requirements of demountable seals; it is obviously impracticable as a production routine. While it may not be permissible to accelerate the tests by increasing the pressure differential without risk of breaking down the seal, perhaps resulting in permament damage, the time scale may legitimately be shortened if a smaller quantity of gas than 1 c.c. can be accurately measured.

## Advertisement of

bel.Ling \& LEE I.TD.
Great Cambridge Rd., Enfield, Middx.


Miniature


Economy of space-reduction in weight-even greater versatilitythese are the three major advantages of "Belling-Lee" Miniature Unitors over the standard pattern from which they were developed. All this has been achieved without any loss of performance. For example, the 12 pole Miniature Unitor effects a saving in space of over $70 \%$, and a reduction in weight of nearly $50 \%$, yet has the same working voltage ( 400 V . peak) and current rating ( 5 amp ), except that all poles are rated equally. One 8-pole type, however, includes four rated at Io amp. All units have a common face area and are therefore physically interchangeable. Die-cast mounting shrouds are available for one, two or three units.

Most "Belling-Lee'" products are
covered by patents or registered designs, or applications.

Fadiotelephones by ATE—a vital service for isolated communities


## Breaking the cold silence



The outposts of the ever expanding world of today are often to be found in remote, isolated areas. For these communities-lumber camps, trading posts, or even a holiday hotel in a beautiful snow-bound wilderness such as this, modern means of communication are essential. By means of the ATE Type 800 equipment the latest in the ATE single channel VHF rural radio-telephonerange--such remotecommunities can now be linked direct to the nearest telephone exchange and provided with full telephone facilities; Type 800 is specially equipped with full signalling and control equipment for this purpose.
Exhaustive testing under actual climatic extremes has fully proved its outstanding practicability and efficiency.

Extended frequency coverage over VHF and UHF bands.

New compact cabinet-type construction with slide-in chassis for easy access and maintenance.

Plug-in test meter facilities.
High or low power versions to suit propagation conditions.

Will work in to any type of telephone exchange with improved outband tone signalling facilities.

Modern design conforming to British Post Office, Canadian Department of Transport and Crown Agents' Specifications.


## NEW TELEVISION VIDEO

## MAZDA 6F28

The 6 F 28 is a screened high slope frame grid beam tetrode for use in television video output stages. High peak current is available, enabling adequate video drive to be provided for the cathode ray tube with anode loads down to 4700 ohms; this low value of load eases the problem of HF video compensation. This type has identical characteristics to the tetrode in the 30FL12 triode-tetrode combination.

$$
\begin{array}{lllll}
\text { Heater Voltage (volts) } & \text {.. } & \ldots & \text { Vh }_{\text {n }} & 6.3 \\
\text { Heater Current (amps) } & \text {. } & \ldots & \mathrm{I}_{\mathrm{h}} & 0.3
\end{array}
$$

## TENTATIVE RATINGS AND DATA


*Measured with respect to the higher potential heater pin.
Inter-Electrode Capacitances $\dagger(\mathrm{pF})$

$\dagger$ Measured in fully shielded socket without can.

## CHARACTERISTICS

| Anode Voltage (volts) | . | $\mathrm{V}_{\mathrm{a}}$ | 180 |  |
| :--- | :--- | :--- | :--- | :---: |
| Screen Grid Voltage (volts) | $\ldots$ | $\mathrm{V}_{\mathrm{g} 2}$ | 180 |  |
| Anode Current (mA) | $\ldots$ | .. | $\mathrm{I}_{\mathrm{a}}$ | 10 |
| Mutual Conductance (mA/V) | .. | $\mathrm{g}_{\mathrm{m}}$ | 12.5 |  |

## TYPICAL OPERATION AS VIDEO AMPLIFIER

Allowance must be made in circuit design, not only for component variation, but also for valve spread and deterioration during life. Values of peak anode current, for an average valve when new and at the assumed end of life point for any valve, are as follows:-


Mounting Position: Unrestricted
Base: B9A (Noval)

## Connections



## MAXIMUM DIMENSIONS (mm)

| Overall Length | .. | .. | .. | 56 |
| :--- | :--- | :--- | :--- | :--- |
| Seated Height | .. | .. | .. | 49 |
| Diameter .. | .. | .. | .. | 22.2 |



Tentative Characieristic Curves of Mazda Valve 1 уре 6 г $\mathbf{c 8}$



## NEW

## MAZDA

30FL13.
The 30FL13 consists of a high slope tetrode with frame grid construction and a general purpose triode for use in television sync. separator circuits. The short grid base and high slope of the tetrode enable good pulse limiting to be obtained with the anode load resistance directly connected to the HT line and a fairly high screen voltage.

The triode has identical characteristics to the 6/30L2.

| Heater current (amps) | . | . | $I_{\mathrm{b}}$ | 0.3 |
| :--- | :--- | :--- | :--- | ---: |
| Heater voltage (volts) | . | . | $\mathrm{V}_{\mathrm{b}}$ | 10.0 |

TENTATIVE RATINGS AND DATA

| aximum Design Centre | ngs | $\begin{gathered} \text { Triode } \\ 1.5 \end{gathered}$ | Tetrode |
| :---: | :---: | :---: | :---: |
| Anode Dissipation (watts) | $\mathrm{p}_{3}($ max $)$ |  | 1.5 |
| Screen Grid Dissipation (watts) | $\mathrm{p}_{\mathrm{g}}($ max $)$ |  | 0.5 |
| Anode Voltage (volts) | $\mathrm{Va}_{\text {(max }}$ ) | 250 | 250 |
| Screen Grid Voltage (volts) | $\mathrm{V}_{\mathrm{g} 2}($ max $)$ |  | 250 |
| Heater to Cathode |  |  |  |
|  |  |  |  |

Inter-Electrode Capacitances $\dagger(\mathrm{pF})$

|  |  | Triode | Tetrode |
| :---: | :---: | :---: | :---: |
| Input | $c_{\text {in }}$ | 2.3 |  |
| Output | cuat | 2.0 | 2.6 |
| Control Grid to Anode | $\mathrm{Cg}_{\mathrm{g}-\mathrm{a}}$ | 2.4 | . 04 |
| Grid Triode to Grid 1 Tetrode | $\mathbf{C s t - g l}^{\text {g }}$ |  |  |
| Anode Triode to Anode Tetrode | $\mathrm{C}_{\text {a } 4-\mathrm{aq}}$ |  |  |
| Grid Triode to Anode Tetrode | $\mathrm{c}_{\mathrm{gt}}$-aq |  |  |
| Anode Triode to Grid 1 Tetrode | $\mathrm{Cat}_{\text {at-g1 }}$ |  |  |

## TETRODE CHARACTERISTICS

$\qquad$ Screen Grid Voltage (volts) Control Grid Voltage (volts) Anode Current (mA) ..

| $\mathrm{V}_{\mathrm{b}}$ |  |
| :--- | :--- |
| $\mathrm{R}_{\mathrm{g}}$ |  |
| $\mathrm{V}_{\mathrm{g} 2}$ | -0.6 |
| $\mathrm{~V}_{\mathrm{g} 1}$ | 4 |
| $\mathrm{I}_{\mathrm{a}}$ | 4 |

## TRIODE CHARACTERISTICS

| Anode Voltage (volts) | $\ldots$ | $\mathrm{V}_{\mathrm{s}}$ | 150 |
| :--- | :--- | :--- | :--- |
| Anode Current $(\mathrm{mA})$ | $\therefore$ | $\therefore$ | $\mathrm{I}_{\mathrm{a}}$ |
| Mutual Conductance | $(\mathrm{mA} / \mathrm{V})$ | $\mathrm{g}_{\mathrm{m}}$ | 10 |
| Amplification Factor | $\ldots$ | .. | $\mu$ |

Mounting position: Unrestricted.
Base: B9A (Noval).
Connections:

Maximum Dimensions (mm)
Overall Length .. .. .. .. 56
Seated Height .. .. .. .. 49
Diameter .. .. .. .. .. 22.2

MAZDA COMMERCIAL DIVISION Thorn-AEI Radio Valves \& Tubes Ltd.
$155^{\circ}$ Charing Cross Road, London W.C. 2 Telephone: GERrard 9797.

SYNC SEPARATOR


## Tentative Characteristic Curves of Mazda Valve Type 30 FL13




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Bedford and
Pershore

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Model55SW 'Unidyne'

Model 545
'Unldyne III'


## TRANSMITTING

## VALVES



The tables below give data relating to some of the Transmitting Valves manufactured by the English Electric Valve Company. The full list of these valves, complete specifications and characteristics can be obtained on application to the Company.
'ENGLISH ELECTRIC'

| E.E.V. <br> Type | Equivalent Types | Service Type | Filament |  | Frequency $\mathrm{Mc} / \mathrm{s}$ § | Anode voltage max. (kV) | Anode dissipation max. (kW) | Type of cooling |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Voltage (V) | Current (A) |  |  |  |  |
| 5867 | 5867, TY3-250 | CVI350 | 5.0 | 14.0 | 100/150 | 3.0 | 0.25 | Natural <br> to $30 \mathrm{Mc} / \mathrm{s}$ |
| 833A | TY4-350, 833A | CV635 | 10.0 | 10.0 | 30 | $\left\{\begin{array}{l}3.0 \\ 4.0\end{array}\right.$ | 0.3 | Natural |
|  |  | CV635 |  |  |  | $\{4.0$ | 0.4 | Forced air |
| $\ddagger 5762$ | TY6-5000A, ACT30 | CV2383 | 12.6 | 29.0 | 30/220 | 6.2 | $3 \cdot 0$ | Forced air |
| BR 161 | - | CV2322 | 9.0 | 175.0 | 30/50 | 12.0 | 15.0 | Forced air |
| BR 189 | - | CV5218 | 9.0 | $240 \cdot 0$ | 5/50 | 15.0 | 27.0 | Forced air |
| BR 1122 | - | - | 6.0 | 115.0 | 5/110 | 12.0 | 10.0 | Forced air |
| BW 161 | - | - | 9.0 | 175.0 | 30/50 | 12.0 | $30 \cdot 0$ | Water |
| BW 189 | - | - | 9.0 | 240.0 | 5/50 | 15.0 | 35.0 | Water |
| BY 189 | - | - | 9.0 | $240 \cdot 0$ | 5/50 | 15.0 | $35 \cdot 0$ | Vapour |
| CR 192 | 6166 | - | 5.0 | 175.0 | 30/220 | 6.0 | 10.0 | Forced air |
| 6181 | 6181, CRIIO1 | - | 120.0 | 1.6 | 900 | 2.0 | 2.0 | Forced air |

$\ddagger$ Previously BR 191 B
§ The lower value indicates the operating frequency at full rating. Operation at the higher value is possible with suitable derating.

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" This occasion proved a mosi strinjent test as we were listening to a stereo recording of a very recent orchestral and operatic performance we had enjoyed either as audience or performer. By way of experiment other pairs of speakers were switched in, but the very smooth response of the Leak speakers won the day."

Quoted from the Test Report by Ralph West, B.Sc., M.Brit.I.R.E. The full report appeared in "Hi-Fi News," August, 1961.

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Quoted from the article "Frankly Speaking," by John Berridge, "Hi-Fi News," August, 1961.


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Name
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21. Tuning condensers for thems 1 and $3,9 / 6$. 22. Tuning condeusers for items 2 and 4, 10/6.
22. Printed circuit for items 1 and $3,6 / 6$.
23. Printed oircuit for items 2 and $4,7 / 6$
24. 21 in . speaker, 3 ohm, $19 / 6 ; 80$ ohm
25. 
26. 3in. peaker, $3 \mathrm{ohm}, 18 / 6 ; 80 \mathrm{ohm}, 18 / 6$.
27. Sin. speaker, 3 ohm, 18/6; 35 ohm
Hi flux, $18 / 6 ; 3 \hat{o h m}$ Buper Hi flur, 22/6. $18 / 6$; 35 ohm super
21
28. Elliptical speaker, $7 \times 4,3$ ohm, 19/6; $35 \mathrm{ohm}, 19 / 6$.
29. Battery connectors, large, $1 /$ - pair;

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Low Loss Erase Heads for $\frac{1}{4}$ in, $\frac{1}{2}$ in. and lin. Tape are also available. Considerable reductions in erase power made possible. Send for full details of all types.


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FREQUENCY MEASUREMENTS from d.c. up to at least $1 \mathrm{Mc} / \mathrm{s}$.
time measurements for any time between $3 \mu \mathrm{sec}$, and 2777 hours.
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L.T. TRANSFORMERS. All primaries sapped 200/250 volts. $3.5,9$ or 17 voles 1 amp., $9 / 9$ dirto 2 amp ., $14 / 3$; ditro, 4 amp ., $16 / 6$. 9 or 17 volt 6 amp., $26 /=3,4,5,6,8,10,12,15,18,20$, 24 or 30 voles 2 amp ., $18 / 6$. Ditto, $4 \mathrm{amp} ., 27 / 6$. Please add postage.

## AMERICAN ARB RECEIVERS

Frequency coverage on 4 bands $195 \mathrm{kc} / \mathrm{s}$ to $9.05 \mathrm{mc} / \mathrm{s}$. Precision vernier drive. Valve line-up: 12SA7, 4-12SF7, 12A6 and 991 Operation 24 voles D.C. Supplied fully tested and checked, $\{6 / 19 / 6$ each. Carriage $7 / 6$. ITHM 14 AMP. SLIDER RHEOSTATS, 15/6 each. P/P $2 / 6$.

## PHOTO VOLTAGE AMPLIFIERS

These special units contain a 1 microamp. Tinsley mirror galvanometer, ewin selenium Tinsley mirror galvanometer, twin selenium
photo cell. 12 v . lamp, lamp housing and photo cell. 12 v . lamp, lamp housing and
focusing unit. Brand new; boxed, $£ 9 / 19 / 6$ each. Carriage 7/6.
AR.88D SPARES. Complete wavechange witch assembly with screens, new, boxed, $17 / 6$ each. P/P 2/6. Ist L.F. transformers, new, boxed, 3/6 each. P/P 9d.

## SPEAKER BARGAINS

All brand new and guaranteed



$\left\{\begin{array}{c}\text { IDEAL } \\ \text { PRESENTS } \\ \text { FOR ANY } \\ \text { OCCASION } \\ \star \quad * \\ \text { Send } 1 /=\text { stamp } \\ \text { for full details } \\ \text { of our new } \\ \text { ranges }\end{array}\right\}$

## 3-TRANSISTOR AND DIODE PERSONAL POCKET RADIO



Quality Output on
Personal Earphone. A Personal Earphone. A simple to build local station with personal
earphone output. Bultin Ferrite Aerial and Battery lasting 9 months. Size $4 \times 3 \times 1$ Itin.
ALL PARTS 37/6
750 mW 4-TRANSISTOR

## PUSH-PULL AMPLIFIER

(over I watt peak outpur).

* Uses OC7I/OC8ID.

2-OC81.
$\pm \pm 3 \mathrm{~dB} 70 \mathrm{c} / \mathrm{s}$ to 12


*ircuit
BUILT \& $69 / 6 \quad \begin{aligned} & \text { P.P. } 1 / 6 \text { OR } \\ & \text { COMPLETE KIT } \\ & \text { TESTED }\end{aligned} 62 / 6$ P.P.
I/6 Ideal for Record Player, Intercomm., Baby Alarm, for Tuners, etc

Alarm, for Tuners, etc
$\star 3$ ohm output, fully guaranteed, 9 vols operated. Descriptive leaflet with uses FREE on request.

## BABY SITTER ALL TRAN. SISTOR BABYOR BANAL INVALID ALARM

Battery operated, push-pull, 400 mW output. Low impedance microphone enables unit to be used up to 203 yards. Output on quality speaker.
$\star$ GUARANTEED for 6 MONTHS

- Microph SAFE.
* Microphone is placed within loft. of baby: twin flex is taken to amplifier unit and placed in any room required. COMPLETELY BUILT AND TESTED.
* Used All Night, $£ 5 / 10 /=$. P.P. 2/6. Every Night, Battery Life 3 to 4 months. ALSO TELEPHONE AMPLIFIER FOR OFFICE OR HOME. $\mathbf{1 5 . 1 0 . 0 .}$ P.P. $2 / 6$.
TRANSISTOR PORTABLE TAPE


12 gns.
FULLY GUARANTEED. $\begin{aligned} & \text { tape, batteries and } \\ & \text { personal phone. }\end{aligned}$

## "TRANSFIVE" PORTABLE

MEDIUM AND LONG WAVE PORTABLE RADIO


Size $8 \frac{1}{2} \times 6 \frac{1}{2} \times 3 \frac{1}{2} \mathrm{in}$.

- 325 mW PushPull Output on Sin. Speaker.
- Fully illustrated Plans.
- Easy to Build Printed Circuit. - Carded Components.
- 5 Mullard Tran-

AFTER SALES SERVICE and FULLY GUARANTEED

## 

Full coverage on Medium and Long wavebands. Excellent quality with full station separation. Car aerial socket.
Building Plans and Prices Free on Request,
The "CONTESSA" COMBINED PORTABLE AND CAR RADIO
$10 \times 7 \frac{1}{2} \times 3 \frac{1}{1}$ in.
UNBEATABLE FOR PERFORMANCEAND APPEARANCE
DESCRIPTIVE LEAFLET ON REQUEST.
Employs the latest techniques. Double tuned IF's, AVC and first-grade components are standard features. Excellent tone, sensitivity and selecTotal Cost
of All Parts of All Parts
$\left\{10.19 .6^{P} . \mathrm{P}\right.$. All Parts sold All Parts sold
separately. 425 mW PUSH-PULI OUTPUT

* 425 mW PUSH-PULL OUTPUT. * $6^{\text {"TOP-GRADE " EDISWAN TRANSISTORS }}$ * NEW TYPE PRINTED CIRCUIT WITH ALL NEW TYPE PRINTED CIRCUIT WITH ALL
COMPONENTS MARKED. COMPONENTS MARKED.
* FULL MEDIUM AND LONG WAVE TUNING * HIGH "Q" INTERNAL FERRITE AERIAL * CAR RADIO ADAPTATION AND AVC. * SLOW MOTION FINGERTIP TUNING WITH STATION NAMES CLEARLY MARKED.
HI-FI' QUALITY SPEAKER.
* aTTRACTIVE REXINE COVERED CABINET, REDIWHITE OR BLUE/WHITE.
FULLY ILLUSTRATED BUILDING INSTRUC. TIONS $3 / 6$, FREE WITH COMPLETE SET OF PARTS.


## HENRY ${ }^{\circ}$ S RAIDID LTD.

5 HARROW ROAD, EDGWARE ROAD, PADDINGTON, LONDON, W. 2
Opposite Edgware Road Tube Stn. PADdington 1008/9. OPEN MON, vo SAT. 9-6. THURS. I o'clock.
"RANGER-3"
NO EXTERNAL
AERIAL OR EARTH 3-TRANSISTOR and 2 DIODES PERSONAL POCKET RADIO with 5 stages giving clear reception on medium Size $4 \frac{3}{1} \times 3 \times 1 \frac{1}{4} i n$. wave, amateur top band and shipping. Only first grade components used throughout. As described in March R.C.
ALL COMPONENTS

## 79/6 P.P. I/6 NO EXTRAS TO BUY

Everything Supplied


Size $4 \frac{3}{1} \times 3 \times 1 \frac{1}{4} \mathrm{in}$.
$\star$ Easy to follow instructions with pictorial layout.

* Reception of Radio Luxembourg guarFree Instructions and Free Instructions and
Price List on request. Easy to build.


## * AFTER SALES SERVICE-Guaranteed.

## TRANSISTOR FM TUNER

Fully tunable corporating Transistors and Printed Circuit Pre-assembled units. 2-OCI71 and 3-
OCI70 Selected Transistors.
Fully Tunable 85 to $108 \mathrm{Mc} / \mathrm{s}$.
$10.7 \mathrm{Mc} / \mathrm{s}$. I.F. A new design for $\mathrm{Hi}-\mathrm{Fi}$ to feed quality valve or transistor amplifiers.
 R.F. amp. Josc. mixer sta Details on request. able separacely.

I WATT TRANSISTOR AMPLIFIER - EMI 4-transistor Amplifier with speaker, tone and volume conerols. Ready assembled for use with crystal pick-ups. $7 \frac{1}{2}$ to 9 volt operated. $89 / 6$. P.P. I/6.
BATTERY RECORD PLAYER
6-7 $\frac{1}{2}$ vole Garrard Turntable with crystal pickup. for above amplifier. 79/6. P.P. $1 / 6$.


## TRANSISTOR INTERCOMM

$\star$ Two-way In kercomm. with clear reproduction. Incorporates unique buz-
zing system. 2 zing system. 2 speakers,volume control. Cabinet sizes about $3 \frac{3}{4} x$
$1 \frac{1}{2} \times 3 \frac{1}{2}$ in. Ready
to use.

* Printed Cir-
cuit Amplifier.


SUPPLIED IN PRESENTATION BOX WITH BATTERY AND GOFT. WIRE. 10 gIIS.
FOR HOME OR OFFICE.


FIDELITY POCKET RADIO "CORONET"
MEDIUM AND LONG WAVE


\section*{- Attractive cabinet. - Size $4 \frac{7}{x}$ 2 | 2 |
| :--- |
| $\times 1 \frac{1}{3} i n$ | Earphonel

Record socket. <br> 12 Months Guarantee}
£9.19.6 P.P. 2/With Battery RITISH DESIGN AND CONSTRUCTION PERSONAL EARPHONE FOR CORONET $12 / 6$ EXTRA.


## MERCURY BATTERIES

$1.3 \mathrm{~V}, 2200 \mathrm{~mA} / \mathrm{H}$, i $\times$ lin. dia., $2 / 6 ; 1.3$ V. $5000 \mathrm{~mA} / \mathrm{H} .2 \times 1 \mathrm{in}$. dia., $2 / 6 ; 1.3 \mathrm{~V}$. $500 \mathrm{~mA} . / \mathrm{H}$, f xin. dia., $1 / 3 ; 1.3 \mathrm{~V}$. $14000 \mathrm{~mA} / \mathrm{H}, 2 \frac{1}{4} \times 1 \frac{1}{4} \mathrm{in}$. dia., $5 /-$


- 7-TRANSISTOR

MEDIUM AND LONG WAVE LUXURY POCKET RADIO

Supplied in presentation box complete with leather case, carry straps, 16 g gS .
personal earphone, battery, etc.

ELECTRONIC DESIGNS VALVE VOLTMETER
FULLY GUARANTEED

D.C. ELECTRONIC VOLTMETER

6 Ranges. $0-3-10-30-100-300$ and 1,000 volts. Input res.: 11 -meg, constant on all ranges. Sensitivity: $3,666,666$ ohms per volt on 3 v . scale.
A.C. VOLTMETER

5 Ranges: $0-10-30-100 \cdot 300-1,000$ volts. Sensitivity: 1,000 ohms per volt.
ELECTRONIC OHMMETER
6 Ranges, from 0.1 ohms to 1,000 megohms. Movement. 200 microamperes. D.C. accuracy $\pm 2 \%$.

COMPLETE WITH INSTRUCTION BOOK AND TEST PRODS, BRAND NEW.
Input $110-250$ volts A.C.

£12.10.0 p.p. 3/6.



## CRYSTAL MICROPHONES

ACOS 39-1. Stick Mierophone with screened cable and stand (list 5 gns .), 39/6. P.P. $1 / 6$.

ACOS 40. Deck Microphone with sereened cable and built-in stand (list 50/-) 19/6. P.P. $1 / 6$.
ACOS 45. Hand Microphone with screened lead, very sensitive, 29/6. P.P.1/6.

MODEL IOOC STICK MICROPHONE
Supplied complete with detachable desk stand, neck cord, 7 ft , screened cable, built-in muting switch. 39/6. P.P. 1/6. * BRAND NEW FULLY GUARANTEED. *

PRACTICAL TRANSISTOR CIRCUITS

3/6 Contains easy follow plans of 40 all transistor units, including light operated switches, amplifiers, transmitters, receivers, test oscillators, signal tracers, conerol, etc. All parts available sepa* rately.
$* 600$ ohm PERSO. NAL EARPHONE with jack plug and socker. 10/6. P.P. 1/-.

POCKET IRON
$\pm$ Pocket Soldering Iron, 220/250 v. A.C. 1 D.C. 30 watts, complete with mains plug, case, etc. Handle unscrews to cover element, enabling iron to be carried in pocket. 18/6. P.P. I/-.

I Kohm DYNAMIC MICROPHONE Hand held or desk stand, complete with screened able. Ex cellent response.

5 HARROW ROAD, EDGWARE ROAD, PADDINGTON, LONDON, W. 2
Opposite Edgware Road Tube Stn. PADdingion 1008/9.
OPEN MON. 10 SAT. 9-6. THURS. 1 o'clock

STEREO AMPLIFIER

## BARGAIN OFFER <br> - 2 watts per channel

- Full tone, balance and volume controls.
- Complete with sockers. dials, etc. $97 / 6 \begin{aligned} & \text { P.P. } \\ & 2 / 6 .\end{aligned}$ Suitable Speakers, $10 \times 6$ in., 49/6 pair. UAI4 Stereo Deck, $£ 8 / 19 / 6$. P.P. $3 / 6$. READY BUILT \& TESTED.
PORTABLE LOUD HAILER * Pistol grip action. Special shape horn. Built-in batteries and detachable microteries and detachable miero-
phone. Made of ligheweight materials. Weight 4 lbs. materials. Weight

CRYSTAL MIC INSERTS * ACOS 43-2 $2 \frac{1}{4} \mathrm{in}$. round, A ACOS 43-2
12/6. P.P. $6 d$.
$\star$ ACOS $i \frac{1}{2}$ in. round, $7 / 6$. - A.P. 6d.

大 $\frac{3}{4} \mathrm{in}$. square, $3 / 6$. P.P. 6d.
LOUD IMPEDANCE
HEADPHONES, 6/-. P.P.
$1 / 3$.

## H.

## RECORD PLAYER AMPLIFIER

- 2-watt output

Ready built with Valves Ready built with Valves
and $8 \times 5$ Speaker, Tone and Volume controls. Printed circuit.

$$
75 /=\text { P.P. } 2 /=
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Ideal for Portable Record Player.
Changer, $\begin{gathered}\text { 4-speed } \\ \text { ideal for }\end{gathered} \begin{aligned} & \text { Record } \\ & \text { above. }\end{aligned}$ £ $6 / 19 / 6$. P.P. $3 / 6$.

TELEPHONE ADAPTOR
$\star$ Ideal for recording telephone conversations. Supplied with sereened cable. Fitted rubber sucker. 14/-. P.P. 9d.

MINIATURE PANEL METERS (D.C.) 0/50 microamp. ...... 39/6 0/500 microamp. ... $32 / 6$ O/l milliamp. ............ 27/6 Vu meter ................ 42/6 | Vu meter ${ }^{\text {S ".............. }}$ meter ........... | 32/6 |
| :--- | :--- | :--- |

IRANSTSLORS
WEND
We Stock a Transistor FROM
and components for $3 / 6$
Every Purpose.
ENQUIRIES WELCOMED
ISt GRADE-FULLY GUARANTEED

SEND I/- STAMP FOR COMPLETE LISTS AND NEW CATALOGUE


## SANGAMO WESTON DUAL RANGE VOLTMETER. 5 \& 100 volt D.C. 3 in . scale, F.S.D. I mA. Brand new in carrying case with Test Prods and Leads. Price 27/6. P. \& P. 3/-.

AIRCRAFT CINE CAMERA G45B Mk. III. Fully modified, fitted with $1 / 3.5$ triple anastigmat lens, takes fitted with 24 v . fitted with 24 v .
motor, 16 exposures original packing, $£ 4 / 10 / \mathrm{m}$. per sec. Brand new, LABORATORY PRECISION VOLTMETER. Brand new in Brand new calished teak case. Moving Iron instruMoving lron instrument reading
or A.C. $0-160$ volt or A.C. mirror scale.

on Bin. miter | on Bin. mirror scale. |
| :--- |
| Accuracy $2 \% ~$ |
| $4 / 19 / 6$ | each. P. \& P. $3 / 6$.

BRAND NEW FREQUENCY METERS manufactured by Nalder \& Thompson Ltd. Calibrated 45 cycles to 55 cycles per second. 6in. dial. Panel mounting type. In original manufacturers' boxes. PRICE $£ 10 / 15 /$ each. Postage 3/6.

CLASS D WAVE METER. Latest release of these famous Heterodyne wave meters with directly calibrated illuminated dial, most suitable for amateur transmitters, covers two ranges $1.9-8.0 \mathrm{Mc} / \mathrm{s}$. and $4.0-1.0 \mathrm{Mc} / \mathrm{s}$. Complete with reference crystals for zero settings, two valves, $2 \times 6$ volt vibrators, MAKER'S instruction book and matched set of head. phones for monitoring. Designed for 6-volt D.C. operation, can easily be modified for mains and suitable transformer supplied for 7/6. In spotion condition as tested by R.E.M.E. In transit case. Price 5 gns, each, plus 6/6 carriage.

Magnetic Counters, very latest High Speed type, ex P.O., guaranteed per. fect, type No. 100B, coil 2,300 ohms, for 48 volt D.C. operation (will work on 36 volt), overall size $4 \times 1 \times$ lin. Price 15/- each, P. \& P. $1 / 6$.


GEARED MOTORS, 200/250 Volt A.C Input, single phase, 6.6 r.p.m., reversible torque $35 \mathrm{lbs} / \mathrm{inch}$. Stepped shaft $\frac{1}{2}$ and $\frac{3}{7}$. A compact and extremely powerful motor with double gearbox which can be adjusted for horizontal or vertical drive. Brand new in maker's carton. British made to B.S.S. 170 . Price $66 / 5 /$ each, plus 4/- each P. \& P.


HEAVY DUTY L.T. TRMER. TRANSconservatively rated
for continuous duty. New in manufac: turer's cases. Input 110.260 volt multitapped. 50 cycies, single phase. Out. put 28-29-30-31 volts at 21 ampere. Price 66/15/-. Carriage PLATE TRANSFORMER of very best U.S.A. make, brand new, original manufacturer's cases. Input tapped at 190/210/230/ 250v Output 2250-0.2250, centre tapped 400 mA . Nett weight 76 lb ., size $13 \mathrm{in}, \times$ gin. $\times 6$ in. -Price E6/:0;- each, plus carr. 10/-


MIDGET ROTARY TRANSFORMERS. $2 \dagger$ in. dia. $\times 4 \frac{1}{3}$ in. Input 365 volt. Output 300 Brand new. $10 / 6$ each. P. \& P. $2 /$-.

AUTO TRANSFORMERS. Step up, step down. 110-200-220-240 V. Fully shrouded New. 300 watt type $£ 2 / 2 /-$ each. P. \& P. $2 / 6$. 500 watt type $£ 3 / 3 /-$ each. P. \& P. 3/9. 1,000 watt type $84 / 4 /$ - each. P. \& P. $6 / 6$.
BRAND NEW SELENIUM FULL WAVE BRIDGE RECTIFIERS, in manufacturer's original packing. D.C. output 36 volt 10 amp . made up of $12 \times 110 \mathrm{~mm}$. dia. plates. These fitted in cooling funnel. (Removable.) Size $11 \frac{1}{2} \mathrm{in} . x 8 \mathrm{in}, x 4 \frac{3}{4} \mathrm{in}$. Price $45 /-$ P. \& P. $4 /$. S.T.C. BRIDGE RECTIFIER. New, perfect. 8 plates each 115 mm . Maximum A.C. input 36 v. D.C. output 5 ampere, 24 volt. Price 20/-. P. \& P. 3/-
R O T A R Y SWITCH REGU. LATOR. 25 ohms. very conservatively rated at 4 amp. will handle 8 amp Overall size $7 \times 8 \times$ 6in. Price 15/-. P. \& P. $2 / 6$.


BUILD AN EFFICIENT STROBE UNIT, the ideal instrument for workshop lab. or factory. This wonderful device enables you to "freeze"; motion and examine moving parts as if stationary. We supply a simple circuit diagram and all electrical parts including the NSP2 Strobe tube which will enable you to easily and quickly tube which will enable you to easily and quickiy construct a unit for an infinite variety of speeds,
from flash in several seconds to several from I flash in several seconds to several
thousands per second. New modified circuits thousands per second. New modified c
bring price down to $37 / 6$ plus $3 /-\mathrm{P}$ \& .

CRYSTAL CALIBRATOR. No. 10. A
 crystal controlled instrument in the instrument in the same category as the famous B.C. 221. Directly calibrated, does not require cross reference or
charts - functions charts - functions crystal fows: (I) A crystal controlled
oscillator which provides fixed frequency signals of 500 KC and all harmonics of 500 KC to beyond 10 Meg. and up to 30 Meg .
(2) A variable oscillator from 250 KC to 500 KC , this enables all intermediate frequencies between $250 \mathrm{Kc} / \mathrm{s}$, and 30 Meg . to be produced and modulated.
Supplied complete with 3 spare valves, all leads and instruction book in carrying haversack. The complete outfit is brand new-repeat NEW. Price $£ 4 / 10 / \%$. Carr. $3 / 6$.

NEW GALVASolid brass, 3 in. dial, in polished degree scale 35 mA either side. 100 ohm coil. Price $12 / 6$ each. P. \& P.


TANNOY P.A. LOUDSPEAKER. For outdoor use, metal exponential horn with 20 in. square flare. Overall length 30 in . Speech coil 15 ohms. Guaranteed in working order and good condition. Price ET/IO/. Carr. 10/-

BRAND NEW SOUND POWER OPERATEDEXADMIRALTY HEAD such sets connected up will provide perfect intercom., no batteries required. Will operate up to $\frac{1}{2}$ mile. Original manufacturer's boxes. Price $17 / 6$ each, plus P. \& P. 3/*; or 32/6 per pair P. \& P. 4/-.


## A.C.|D.C. OUTPUT UNIT

FIRST IN THE FIELD AT A PRICE THAT DEFIES ALL COMPETITION. This unique power unit will give variable outputs of $0-260 \mathrm{~V}$. A.C. or 0.230 V . D.C. at 8 ampere, from normal $230 \mathrm{~V}, 50$ cycles A.C. input. A voltmeter is fitted so that an indication of output voltage A.C. or D.C. is always available. Robustly constructed sheet metal case well ventilated for continuous operation, complete with safety fuse, neon indicator and meter. A modern instrument for up to date development and research. Size $17 \mathrm{in} . \times 12 \mathrm{in} . \times 7 \mathrm{in}$. Weight 36 lb . Brand new, freshly manufactured. Price $£ 34 / 10 / 0$. Carriage 20/-

## MAINS POWER MAINS POWER SUPPLY UNITS.

 Potted and sealed transformer and choke by famous maker. Mourited on metal chassis $6 \frac{1}{2} \times$ $7 \frac{1}{2} \mathrm{in}$., complete with $5 Z 4$ rectifier valve and full smoothing.

Input tapped 220-230-240 volts.
Output: 300 V . D.C. at 100 mA . 6.3 V . A.C. at 4.5 amp .

Rectifier supply 5 V. A.C. at 3 amp. Very conservatively rated. Price $47 / 6$ plus P. \& P. $81-$. MULLARD TRANSISTORS. OCI70, 70 to $100 \mathrm{Mc} / \mathrm{s}$., $13 / 6$ each. OCI71, 100 to $200 \mathrm{Mc} / \mathrm{s}$., 14/6:
Set of six $1 \times$ OC44; $2 \times$ OC45; I $\times$ OC8ID; $2 \times 0 \mathrm{OC81}$. Six for $39 / 6$.


14-day clockwork TIME SWITCH Contacts $2 \frac{1}{2}$ amp., 230 vole, 24 hour phase, $\frac{1}{\text { h }}$ hour divisions, allow setting for one make and one break to be made every 24 hours, complete with key. Used but guaranteed perfect. Price $27 / 6$ each. P. \& P. $2 / 6$.

14-day elockwork TIME SWITCH as above but fitted with 5 amp . contacts and enclosed in an aluminium weather proof case. Price 35/-. P. \& P. 2/6.
Similar TIME SWITCH, I amp, contacts, loose not cased. Price 22/6. P. \& P. 2/-.


EX P.O. MAGNETIC COUNTER. 3 ohm type for 6 V. D.C. operation. 4 figures to 9,999 . Price $8 / 6$. P. \& $P$. $1 / 6$.
20-WAY STRIP. Containing standard Post Office telephone Jack Sockets, overall size \|I $x$ $3\} \times \frac{1}{4}$ in. New. Price 15/- each. P. \& P. $1 / 6$.
NEW BALANCED ARMATURE HEADPHONES. TYPE DLR5. Guaranteed perfect. Price $12 / 6$ each. P. \& P. 2/-.
PHOTO MULTIPLIER, type 93IA, for Alfa counting. film scanning, spectography, etc., new, inclusive of 11 pin valve holder. Price E2/7/6. P. \& P. 1/-.
NSP2-CV2296 STROBOTRON FLASHTUBE made by Ferranti, brand new, on 1.0. base. Price 15/-. P. \& P. I/-.

MOVING COIL HEADPHONES, 150 ohm impedance. Padded, rubber backed chamois impedance. Parmuffs. Superb reproduction. Complete with earmufts. Superb reproductio
Jack Plug. 21/6. P. \& P. I/6.
CARPENTER'S TYPE POLARISED RELAYS. $2 \times$ 9,500 turns at 1,685 ohms. Price 22/6 each. P. \& P. 1/-
Bases for Carpenter relays ex new equipment, $3 / 6$ each.
HIGH SPEED RELAY. Siemens. Two bobbins 1,000 ohms each. New, $10 / 6$ each.
 HIGH SPEED RELAY. Siemens. Two
coils 145 ohms each. New $10 / 6$ each. P. \& P. 1/-.
VACUUM SEALED 3,100 OHMS RELAYS. Single pole changeover contacts in platinum. Pult in at 1.25 M .A. ( 4.25 volt). Price $18 / 6$ each. P. \& P. I/-.
G.E.C. SEALED RELAYS TYPE M1095. 24 volt 670 ohms. 2 make 2 break. Unused. 24 volt 670 ohms. 2 make
Price $12 /-$ each. P. \& P. $1 /-$.
G.E.C SEALED RELAYS TYPE M1494. 24 volt 670 ohms coil. I pole C.O. Brand new. Price 10/-. P. \& P. I/-.
NEW P.O. RELAYS TYPE 3000, 2,000 ohms coil. 4 make 4 break, $12 / 6$ each. P. \& P. I/-. MINIATURE MOVING COIL DIFFERENTIAL RELAY. Two colls 350 ohms each.
 Operating current minimum 140 microamp., nominal 400
microamp.,maximum 8 milliamp. One pole two way, or
centre stable. Two way contact current 100 mA ., at 50 V . A.C. or D.C. Size $1 \frac{1}{6} \times \frac{1}{4} \times \frac{3}{8} \frac{3}{2}$. Price $22 / 6$ each.

MINIATURE MOVING COIL DIFFERENTIAL RELAY exactly as above but totally sealed in metal case. New Price $27 / 6$ each.
MINIATURE RELAYS 250 ohms. Two makes. For operation on $4.5-9$ vole. Ideal for transistor circuits. Weight just over I oz. transistor circuits
Price $12 / 6$ each.
SIEMENS H.S. RELAY. Very latest type. sealed. H96E. 1,700 ohms plus 1,700 ohms, single C/O contacts. Brand new with fixing clip. In maker's cartons. Price $16 / 6$ each, plus $1 /-\mathrm{P}$ \& P .
SOLENOID OPERATED MAGNETIC RELAY. Type 5CW/3945, 4 pole changeover. 10 A contacts 24 v. operation. Brand new 13/6. P. \& P. 2/-.
W.W. RHEOSTAT. New. 3.5 K or 5 K . 25 watts. Price 7/6. P. \& P. 1/6.
CONSTANT SPEED, PRECISION MADE, BATTERY DRIV. EN D.C. GOVERNED MOTOR (Elliott Bros.). Commutator/brush incorporating loading ballast resistor 2,470 r.p.m. $\pm 2 \%$ at 21 volt. Loss on 8.5 volt only $4 \%$. Size 1 sin. dia. $\times 2$ 粦in. long. Spindle .77in. long $x .15575$ in dia. Weight 4 or. New. Price 25/-, plus 1/P. \& P. Ideal for portable tape recorders.
A.C. VARIABLE

TRANSFORMER brand new. im ported, highest quality electrical engj-
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Very attractive two-tone grey Vynide covered cabinet with black and gold printed escutcheon plate, cream and gold knobs, handle and cabinet fittings. * Weight-complete with long-life $7 \frac{1}{2}$-volt battery- $4 \frac{1}{2} 16$, Mullard high-grade transistors throughout. $\star$ High-Flux 7 in. $\times 4 i n$. Elliptical Speaker. $\star$ Slow motion tuning. * Co-axial socket at rear for direct connection to Car Radio Aerial. A Improved reception by use of five-section plated telescopic aerial disappearing into Cabinet when closed, 34in. above Cabinet:
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8in. $x 4$ in, $x$ cream knobs are included in graved cream knobs are included in the price of the complete kit with all necessary practical and theoretical diagrams at $£ 4 / 5 /-$ only, plus 2/6 p. \& p. or instruction Book fully illustrated for $1 /$ - post free. This amplifier can be supplied assembled, rested and ready for use at $65 / 5 /$ plus p. \& $p$.

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volume on/off, and simple 4 station volume on/off, and simple 4 station
rocary selection switch. Set to Light, rocary selection switch. Set to Light,
Home and Third programme, also Home and Third programme, also Light programme on long waves. Frame aerial included, also 5in. quality speaker mounted on chassis. Overall measurement $9 \mathrm{in} . \times 6 \frac{1}{2} i n . \times$ $5 \frac{1}{2}$ in. high. Only $4 / 17 / 6$ plus 5/p. \& $p$.

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Valve line-up: $6 K 8 \mathrm{G}, 6 \mathrm{~K} 7 \mathrm{G}, 6 \mathrm{Q}, \mathrm{C}$, $6 F 6 G, 6 \times 5 G$ and 6 vole 4 pin nonsynchronous vibrator. 8in. P.M. Speaker, 4 watts output. P.U. socket. Exc. L.S. socket, etc. Tone control. Fitted in polished wood cabinet. size $21 \frac{1}{4} \mathrm{in} . \times 10 \frac{1}{2} \mathrm{in}, \times 10 \frac{1}{3} \mathrm{in}$. These cabinets are slightly soiled owing to storage, but each is guaranteed unused, in serviceable condition, tested prior to despatch. Price $£ 5 / 19 / 6$ only plus P. \& P. $7 / 6$, plus $28 / 6$ for A.C. Mains Conversion Components if required. OUTSTANDING BUY!
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Dial engraved on attractive brown and gold front panel size $16 \frac{1}{2} \mathrm{in} . \times 9 \mathrm{in}$. which forms escutcheon for easy fixing. LIMITED QU P P HP at e8 ailable.

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LATEST COLLARO STUDIO TAPE TRANSCR.PTOR, Latest ype incorporating Record, Interlock, Lever, Button, 3 motors, 3 speeds, IT $\frac{7}{8}, 3 \frac{3}{3}, 7 \frac{1}{2}$ i.p.s., takes 7 in . spools. Push-butcon controls. El2/19/6 plus $5 /-$ P. \& P. Usual H.P. facilities.

## NEW! TAPE RECORDER AM

 PLIFIER TYPE 83II-V. Sub assembled - anyone can build! Printed Circuit, all components mounted and dip soldered. Already tested. Each lead cut to length. All that is required to complete the cape recorder is for a few component. iree ends of the leads soldered to terminals which are clearly marked. Everything supplied, all you need Moner. Yalve line-up, EFb6 ECCb3 $2 \times 4144$ EZ81 and EM84 magic eye. Monitoring facilities, output socket for leeding to high quality amplifier, can be used as "straighe " amplifier for record eproduction. EQUALISING ON TWO SPEEDS. OUTSTANDING VALUE AT $\mathrm{f} 11 / 11 /$ plus $2 / 6$ P. \& P. including all necessary instructions ATTRACTIVE TWO-TONE PORTABLE CARRYING CASE. Suitable for above amplifier and Collaro Studio deck. Fitted with 9in. x Sin. High Flux P.M. speaker for high quality reproduction. Inclusive price E5/5/-. Plus 5/- P. \& P.
The above 3 items purchased at one time, SUPPLIED CARRIAGE PAID N.B. Any microphone listed hereunder is suitable for use with this recorder.

CRYSTAL MICROPHONE. Sensitive Miniature Lapel-type. Complete with clip and screened lead. Brand new, 17/6. Plus 6d. P. \& P. (as illustrated).
MIC 45-1. Acos latest flat pistol-grip crystal microphone. Attractive black and gold finish. OUR PRICE 29/6 plus 1/- P. \& P. ACOS MiC-39-1. Crystal stick microphone. List price 6 gns. Our price $39 / 6$ plus $1 / 6$ P. \& P. MIC 40. General-purpose crystal microphone with desk stand. Our price $22 / 6$ only plus $1 / 6$ P. \& P. 100 C . Imported crystal, attractive streamlined polished metal case, incorporates muting switch. OUR PRICE $39 / 6$ plus $1 /-\mathrm{P}$. \& P. (stand $8 / 6$ extra).

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SUPERMAGNETIC RECORDING TAPE SPECIAL!!! amous American Ferrodynamics "BRAND FIVE" An enthusiast's " must." Brand new (NOT SUB-STANDARD) High grado Acetate Base. 5 in .600 ft . $16 /-, 5 \mathrm{in}$. 900 年. 18/6, $5 \frac{3}{4} \mathrm{in} .1,200 \mathrm{ft}$. $23 / 6$ 7 in . $1,200 \mathrm{ft}$. $25 / \mathrm{L}, 7 \mathrm{in}$. $1,800 \mathrm{fc}$. 35/-. Extra quality Mylar Dupont, 3 in , 300 ft . $13 /-\quad 5 \mathrm{in}$. $1,200 \mathrm{ft} .37 / 6$, 7in. $1,800 \mathrm{ft}$. 44/-, 7in. 2,400ft. 60/. Each on plastic spool. All Post free. Jrade enquiries invized PLASTIC TAPE SPOOLS. Best quality. $3 \mathrm{in}, 1 / 6,5 \mathrm{in} .2 /-, 5 \frac{1}{2} \mathrm{in} .2 / 3$, 7in. 2/6. PLASTIC SPOOL CONTAINERS for spool sizes 5 in . $1 / 6,5$ in 2/-, 7in. 2/3. Any single item plus 6d. P. \& P. Orders over \&1, post free, LANGUAGE COURSES ON TAPE!
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The following Japanese recorders are available for Callers only:-
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No. 38 AFV WALKIE-TALKIE wonderful offer. This famous trana receiver unit, with relas operated SEND/ RECBIVE switch covering $7.4 \cdot 9 \mathrm{Mc} / \mathrm{B}$ band, range approx. 5 miles. Good con dition, ONLY 22/6, plus 2/0 P. \& P. per unit (less accersories). Quantity export
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ANOTHER PORTABLE CABINET BARGAIN: EX leading manufacturer's battery portable attache type case. Attractive two-tone grey rexine finish. Size closed $13 \frac{1}{4} \mathrm{in}$. $\times 9 \frac{\mathrm{in}}{\mathrm{in}} \times \mathbf{x} \frac{\mathrm{3}}{\mathrm{h}} \mathrm{in}$. Complete with fittings and handle. Including Medium and Long Wave frame aerial which fits in lid. On/off switch on lid stay. Limited quantity only at bargain price of $19 / 6$ plus $2 /-$ P. \& P. Brand new.

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The well-known Brayhead TRANS TRONIC "SUPER $60^{\prime \prime}$ RADIO KIT
A complete construction kit to make your own transistorised make your own transistorised Transmitter and Receiver. No
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EXTENSION SPEAKER CABINET8 As illustrated; new design
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 20,000 OHMS PER VOLT!!MODEL 200 H . Volt-ohm-Milliammeter RANGES:
A.C. VOLTAGE: $10,50,100,500$ and 1,000 volts ( 10,000 ohms per volt).
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CAPACITANCE: 10 pf. to $.001 \mathrm{mfd} ., .001 \mathrm{mfd}$. to 1 mid.
DECIBELS: -20 to +22 db .
A fully guaranteed pocket size meter, knife edge pointer, top quality, supplied complete Actual size $4 \frac{1}{2} \times 3 \frac{3}{4} \times$ lin. $\begin{aligned} & \text { with test prods and full } \\ & \text { operating instructions at } \\ & \mathbf{E} .19 .6 \\ & \text { Post free }\end{aligned}$ JUST ARRIVED ! ! Model TE10. Identical in appearance and size with rotory type switch but 10,000 ohms per volt.
Ranges: D.C. Voltages: 0-6-30-120-600-1,200 volts ( 10,000 ohms per volt). A.C. voltage: $0-6-30-120-600-1,200$ volts ( 10,000 ohms per volt) D.C. current: $0-120$ microamp., $0-3-300 \mathrm{~mA}$. Resistance: $0-30 \mathrm{~K}, 0-3$ Meg. ( 150 ohms and 15 K at centre scale). Capacitance; 50 pf to 0.01 mfd , 0.001 mfd to 0.15 mfd . Decibels: 5.19 .6

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A quality 4 valve $A C / D C$ superhet chassis made by a world famous manufacturer. Long and Medium wave coverage. Fitted with a cord and drum reduction tuning drive and attractive illuminated glass dial (size $6 \frac{1}{2} \times 2 \frac{1}{2}$ in.). Controls: Volume on/off, tuning and wave change. The receiver is self-powered, employing a mains dropper and a valve rectifier. Chassis dimensions $6+\times 9 \times 5 \frac{1}{2} \mathrm{in}$, high. Supplied complete with a good quality 5 -inch loudspeaker, valves (UCH42, UAF42, UL41, UY41), AC/DC mains input lead, ivory knobs, etc
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DON'T HESITATE, ORDER NOW! This unbeatable bargain is bound to sell out quickly at only $£ 4 / 19 / 6$ plus $6 / 6$ post and packing.

# 4 STATION PRESET CHASSIS <br> with Speaker <br> <br> ONLY $£ 4.17 .6$ 

 <br> <br> ONLY $£ 4.17 .6$}

Plus 6/6 Post \& Packing
A compact, 4 station preset mains transportable receiver for operation from ACIDC mains. Two simple controls, volume on/ off and 4 position station selector. The latter is set to Light Programme (Long Wave), Third Programme, Home Service and Light Programme (Medium Wave) but may of course be adjusted co alternative selections if required. A frame aerial with throwout extension is supplied, making this receiver ideal as a general purpose trans-
 portable set for the home.
supply is provided from AC/DC mains input by a mains dropper and a supply is provided from AC/DC mains input by a mains dropper and a
valve rectifler. The good tonal qualities are assisted by the provision of a valve rectifler. The good tonal qualities are assisted by the provision of a
quality 5 in . speaker, which is ready-mounted on the chassis (this is easily quality 5 in . speaker, which is ready-mounted on the chassis (this is easily
detachable if alternative positioning is required). Valve line up: UCH42, detachable if alternative positioning is required). Valve line up: UCH42,
UAF42, UL41, UY41. This chassis (size $9 \times 6 \frac{1}{2} \times 5 \frac{1}{2} i n$, high) is supplied complete with valves, knobs, mains lead, aerial, etc. It is beautifully made by a famous maker, and is a first-class buy at the rock bottom price of only $£ 4 / 17 / 6$. plus $6 / 6$ post and packing.
A.M. RADIOGRAM CHASSIS


A chassis of distinction by a famous maker. Covering Long, Med, and Short Waves, plus gram posicion, this chassis (size $15 \frac{1}{2} \times 7 \times 6 \frac{1}{2}$ in, high), incorporates the latest circuitry, using fully delayed A.V.C. and negative feedback. Controls: Tone, Vol. On/Offi, W/Change (L.M.S, and Gram), Tuning, Tapped input $200-250$ v. A.C. only. An attractive brown and gold flluminated dial with matching knobs, make this one of the most handsome, in addition to being one of the best performing ehassis yet offered. Complete with valves (ECH81, EF89, EBC81, EL84, EZ81), knobs, output transformer, leads, etc. OUR PRICE 9.19 .6 plus $4 / 6$ post \& packing.

E.M.I. 4-speed Player and P.U.
Heavy $8 \frac{3}{2}$ in, metal turntable. Low flutter performance 200/250V. shaded motor with tap at 80V. for amplifier valve filament if required. Turnover LP/78 head, Price $89 / 6$ plus $4 / 6$ P. \& P.
CONDENSER RESISTOR PARCEL 50 mixed P.F. Condensers and 50 mlxed Resistors An assortment of useful values. All popular sizesall new-a must for the serviceman and constructor.
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## 6 TRANSISTOR KIT

Less cabinet \& speaker
Special offer. Limited quantity only of new ex-manufacturers parts to make a 6-transistor 2 waveband superhet chassis. Ideal for portable or table radio. All parts including transistors, ferrite aerial, printed circuit, etc., but EX CLUDING speaker and cabinet. Few only £4/19/6 plus 2/6 P. \& P. Simple instructions 1/6 (free with kit).
A FEW ONLY £4.19.6
P. \&

SUPER STEREO KIT MK. II A kit of ready-built units only requiring interconnection. Comprising two midget $3 W$ a mplifiers push button switch, transformer, control unit (bass, treble and vol.), power pack, two speakers, indicator light, valves (ECL82, EZ80 range), and comprehensive instruetions.
Plus $6 / 6 \mathrm{P} . \& \mathrm{P}$.
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## THE WORLD FAMOUS E.M.I.

 ANGEL TRANSCRIPTION P.U. (Model I7A)

A Pick-up for the connoisseur originally priced at $\quad 17 / 10 /$-. The last remaining few offered at E5/15/- plus P. \& P. 5/-.

TRANSISTOR AMPLIFIER KIT A complete kit of parts to build a compact 4transistor amplifier, with volume control and drilled panel. Two GT3 driver transistors, transformer coupled. I watt output from matched pair GTI5. Supplied with output transformer and $2 \frac{1}{2}$ in. 3 ohm speaker. Ideal for $\quad$ plus $4 / 6$ P. P. $59 / 6$

## record player, ete.

## SUPERHET CHASSIS

-less Valves \& Cabinet
Modern ACIDC chassis with printed circuit and ferrite rod aerial. Although not completely built, the main components are mounted. $L$. \& M. wave coverage. 4 valves (UBF89, UC்L83, UCH8I, UY85). Everything supplied except valves and cabinet. With speaker and
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OC71 …........ 8/- GET102 ............... $7 / 6$


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Please add 6d, postage for eact transistor. SWITCHED ATTENUATOR
Audio to V.H.F. in four steps of $20 \mathrm{~dB} \pm 0.02$


## 

## ENTHUSIASTS 14 WATT AMPLIFIER KIT

A kit designed to meet the exacting requirements of the audio enthusiast, yet remain within the price range of the average constructor. A stylishly finished monaural amplifier with an output of 14 watts from 2 EL84s in push-pull. Superb reproduction of both music and speech (frequency response $\pm 3 \mathrm{db} . \mathrm{c} / \mathrm{s} .-60 \mathrm{Kc} / \mathrm{s}$, with negligible hum). Separate inputs for mike and gram allow records and announcements to follow each other, and make this amplifier idzal for small halls, youth clubs, etc. Fully shrouded ultra linear output transformer (to match $3-15 \Omega$ speaker), and fully shrouded mains transformer (these alone are worth over $\mathrm{E} / / 10 /-$ ). Volume control, and separate bass and treble controls are provided, giving good lift and cut. Valve line up: 2 EL84s, ECC83, EF86, and EZ80 rectifier. All parts down to the lase nut and bolt, including valves, heavy gauge metal chassis finished in glossy hammer green enamel (mains and output eransformers finished to match)
P. \& P. $6 / 6$ (simple instruction booklet
$1 / 6$. Free with Kit )

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F.M./V.H.F. RECEIVER KIT
19.6
AT LAST-A COMPLETE F.M RECEIVER IN KIT FORM! Specially designed wtih the home constructor in mind, this kit enables the construction of completely self-contained V.H.F receiver at fraction of the norma cost of comparable equipment This is basically a quality selfpowered F.M. tuner plus 2 separate audio amplifier stages with output transformer and speaker.

* F.M. Tuning Head by famous maker.
* Guaranteed Non-dritt.
$\star$ Permeability Tuning.
* Frequency coverage $88-100$ Mc/s.
* OABI Balanced Diode Outpue
$\star$ Two I.F. Scages and Diseriminator.
* Self powered using a good quality mains eransformer and valve rectifier
* Valves used ECC85, two EF80's, ECL82 and EZ80 (rectifier).
$\star$ Fully drilled chassis.
$\star$ Good quality speaker
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* Aetractive maroon and gold glass dial.
* Two ourput stages (using ECL82).
* Everything supplied, down to the last nut and bolt.
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* All parts sold separately OUR PRICE 56.19 .6 Plus \& $4 / 6$


A 20 A 29 gn . record player) has a printed circuit, and has an internal fully smoothed power supply (input A.C.I.C. mains) using a mains dropper and contact cooled rectifer. Asiying panes (SLUpplied UFR9) and linear output transformer give crisp reproduction from all records at 4 wates.
Our price for the complete kit of parts (including valves) Plus $6 / 6$ P. \& P.
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59/6

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A very fortunate purchase allows us to
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A first-class 2 -waveband transistor su. perhet in kit form. $\star$ Printed circuit board (size 8f $\times$ 2<in.).

* 3 pre-aligned IF eransformers.
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* Output transfor
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TYPE 46 TRANSCEIVERS. The best bargain for many years. These fine Walkie Talkies are now available in new condition, complete with all accessories at a give-away price. Three-channel crystal controlled T/X and R/X, supplied complete with one pair crystals, coil box, rod aerial, leads, and plugs, valves, balanced armature head-
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POT CORES. $\}$ in. diam., 3 in. thick, adjustable slugs. $1 / 6$ each. CRYSTAL DIODES. Germainium general purpose, 6d. OA81 EQUW, 9d. Printed circuit board, fitted with 10 OA.81's and several other compenents. Price 2/6. Type (2) as above but fitted with 10 OA71's, price $2 / 6$.
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4 METER MOBLLE TX-RX. A few only B. 44 Mk . II radio ${ }_{\text {telephones. }}$ Coverage $60-95 \mathrm{mc} / \mathrm{s}$. $\mathrm{T} / \mathrm{X}$ and $\mathrm{R} / \mathbf{X}$ single channel, telephones. Coverage $60-95$ mc/s. Crystal controlled. $\mathrm{R} / \mathrm{X}$ is double superhet. T/X output 3 watts. crystal controlled. $R / X$ is double superhet.
Built in 12 volt power supply, draws 3 A . on receive, 4.5 a . on transmit. Built in 12 volt power supply, draws 3 A . on receive, 4.5 a a on transmit.
Provision for loud hailer operation ( 3 watts). Built in loudspeaker. Size $14 \times 7 \times 13 \mathrm{in}$. Complete with all plugs, technical manual, Size $14 \times 7 \times 13$ in. Complete with all plugs, technical manual, service manual, moving coil mike Unused, but may have minor
faults due to long storage. All spares availabie. Price £4/4/-. faults duse to $\mathrm{R} / \mathbf{X}$ crystal in 4 meter band (surplus) $5 /-$. T/X crystal (new) $37 / 6$.
B. 44 MK.I. An earlier version of the above, but an excellent basis for conversion to a fixed station. Output is nominally 4 watts but both final and modulator are QQZ04/15 doube beam tetrodes capable of 14.5 w . output at highest frequency. Specification is othet wise similat to the Mk. II, A built in 12 v . power supply is fitted on a separate chasis. Substitution of the power supply by a 400 v . mains separate chasis. Substitution of the power supply by a toviv. mains power pack plus the necessary circuit alterations will provide a base
station capable of over 30 watts input. Price (complete TX/RX) station capable of over 30 Watts input. Price (complete TX/RX)
with accessories as with Mk. II, $£ 5 / 15 /$ or less case and power supply with accessories as with Mk. I1, £S/15/- or less case and power supply (new) $37 / 6$.

R/X UNIT TYPE R.114. An excellent basis for a 2 metet converte (See February S.W. mag.). Complete with valves and Jones plug and socket. Price $15 /$-, post paid. Extras if required, 7580 crystal 5/0. I.F. trans, as specified (unconverted) $2 / 6$.
MARCONI CR.150. In almosi new condition. Less power supply. $£ 21$.
TOP BAND CRYSTALS. For grinding to $1.8-2 \mathrm{mc} / \mathrm{s}$. we offer super quality extremely active $1,700 \mathrm{kc} / \mathrm{s}$. crystals at 4 for $10 /$ - including one (3-pin) socket.
H.F. CRYSTALS. Miniature, glass encapsulated, wire ended crystals. Six types each containing two quartz plates separated by $50 \mathrm{kc} / \mathrm{s}$ each. of six crystals are also scparated by $50 \mathrm{kc} / \mathrm{s}$. Lowest frequency is 19,887.5, highest 20,437.5. Ideal for "i rubber" crystal VFO., etc. Price $3 / 6$ each or $15 /$ - for set of 6
CRYSTAL BARGAIN PACKAGE. We have large stocks of $10 \times$ crystals surplus to our requirements. We offer 40 different crystals between 2 and $8.5 \mathrm{mc} / \mathrm{s}$, at $£ 1$. For customers ordering more than £1 worth we will still supply completely different frequencies.
RECEIVER TYPE R1475. The well known " 88 " set. R.F. stage, two I.F. stages, BFO, extensive bandspiead over $2-20 \mathrm{mc} / \mathrm{s}$. $600 \mathrm{k} / \mathrm{cs}$. (I.F. frequency) crystal calibrator. In excellent condition but untested. Price £7. Mains power pack £2. Several also available in poor condition (for callers only) fium $£ 3$.
$1,550 \mathrm{KC} / \mathrm{S}$ I.F. TRANSFORMERS. Size $1 \frac{1}{1} \times 1 \frac{1}{2} \times 2 \frac{1}{2} \mathrm{in}$. Price 2/6 each.
SMOOTHING CHOKES. $75 \mathrm{H}_{\text {, }} 25 \mathrm{~m} / \mathrm{a}$, , 1,500 ohms. $5 / \mathrm{m}$ 150 MICROAMP METERS. Edgewise (horizontal) scale type Mirror scale type (1) 7in. scale calibrated, -150 to- 200 deg. C Price $£ 3,10 /$-. Type (2) 10 in . scale calibrated, -130 to -200 deg . C. Price £4/15/-.
A.C. VOLTMETERS. Weston flush mounting $4 i n$. scale rectifier type. $0-100$ volis, $50-2,500 \mathrm{C}$. Price 30/-.
MAGNETIC AMPLIFIERS. Brand new units by Elliot. Price 35/-. Write for details.
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G.E.C. VTVM. 1.5-150 v. A.C./D.C. 8in. mirror scale with probe. 29/9/-
MARCONI VTVM. Type TF 2488/1. $1.5-150 \mathrm{v}$. Price $£ 14$. INSULATION TEST SETS. Contain a 5 kv . power supply. Metered. Price $£ 4$.
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MOVING IRON VOLT METERS. 4in. scale 0-300 V. 50 c . Flush mounting. Price 15/-.
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$7 \mathrm{MC} / \mathrm{S}$. CRYSTALS. 10 XJ fitting. Every $1 \mathrm{k} / \mathrm{c}$ from $7000 \mathrm{k} / \mathrm{c}$. to 7010 inclusive. Price $5 /=$ each.
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Type ( 2530 ). $250-0-250$ v. $60 \mathrm{~m} / \mathrm{a} .6 .3$ v. 3 a. 5 v. 2.5 a. 6.3 v. 2 a Price $17 / 6$.
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BATTERY CHARGERS. Will charge two 12 v . batteries at 6 amps in stecl case fitted with volt and amp meters. Variable output (coarse in stecl case fitted with vo
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HI-FI 10 WATt AMPLIFIERS BRAND NEW CARTONEO MODEL. A P \& Push-pull output. Push-pull output. Latest high emciency mivearard valves. Separate bass and treble controls. Hg mensitivity. Output for 3 obm or 15 obra loudspeaker. Guaranteed, tested and in perfect working order. For $200-250$ A.C. mains.

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Design of a bugh quaity Radio Tuner Unit (specially suitable for use with any of nor Ampliaers). A Triode Heptode F/o'hanger is used. Pentode I.F. and double Diode Second
Datector delayed A.V.C. Is arranged so that A.V.C. dis. Datector delayed A.V.C. is arranged so chat A.V.C. dis-
tortion is avolded. The $w$. Ch. Sw. Incorporates Gramposition Controls are Tuning, W. Ch. and Vol Output will load most Ampliflers requiring 500 mV . Input depending on Ae lecation. Only 250 v. 15 inA. H.T, and L.T. of 6.3 v . I amp. required from amplifler. Size of unit approx. g.6.7in. high. Bend 8.A.E. for Hustrated leaflet. Total buililing cosst of $24 / 15 /$
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## R.S.C. BATTERY TO MAINS CONVERSION UNITS

 piotels replaces butheries supply 1.4 . and 90 r. where A.C. mains $200-250$.
50 o/s is available. Snitable lor all battery portabic recelvers requiring 1.4 v . $50 \mathrm{o} / \mathrm{s}$ is available. Suitable tor all battery portabic receivers requiring 1.4 v .
and 90 v. Thls includes latest low consumption types. Complete kit with and 90 \%. Thls includes latest low co.
diagram $39 / 9$ or ready for use $40 / 9$.
Type RM2. Slze $8 \times 54 \times 2$ tin. Supplies 120 v , 90 v , and $60 \mathrm{v} ., 40 \mathrm{~mA}$, and 2 ₹. 0.4 a. to 1 amp., tully smothed. THEREBY COMPLETELY REPLACING BOTE E.T. BATTERIES AND L.T. 2 v. ACCUMOLATORS when connected to A.C. mains supply $2001-2500$. $50 \mathrm{~d} / \mathrm{s}$. 8UITABLE FOR ALL BATTEEY RECEIV
Complete kit with diagrams and Instructions. $49 / 9$ or ready for use 59/6.
POWER PAGE KITS. Only $19 / 11$. Fully smoothed H.T. output of 250 v . Bn taA and L.T. $u$ upply of 6.3 v. 1.5 amp. Consisting of Double Wound Maing
Pransformer $230 / 2 \overline{0} 0$ v. 50 o.p.s. A.O. primary. Seleniurn Rectifler. Smouich-


## R.S.C. A12 STEREO AMPLIFIER KIT

 GNS. Carr. 8/6
## WTTE TWEN Biln. SPEAKERS

 home onntrols Preset balance control. Outputs for matched 2
R.S.C. STEREO/TEN HIGH QUALITY AMPLIFIER KIT


Valves EZ81, ECC
83, ECC83, EL84 ELs4. separate bass and treble con.
trols giving ", cut
 output on quath
onnnnel. $\begin{gathered}\text { Can } \\ \text { be } \\ \text { besed as straight } \\ 10\end{gathered}$ used as straight 10
watt amplifer. Controls Stereo/Monaural switch ganged gace. Outputs for 3 ohm speakers, Point-to point wiring diagrams and instructions. Il lustration full wring details and priced parts list, 1/9. Assembled and tested $59 / 6$ extra.

8 ans.
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ACOS HGP 59 Hi-Fi Crystal Cartridges. (Turnover type With sapphire stylus). Standard replacement for Garrard nd Collaro, Only 19/9. B.s.B. Ful-zil 19/9. Acos

## R.S.C. MINIATURE 3 WATT GRAM AMPLIFIER KIT

All parts to construct a very compact, highly sensltive ampilfer suitable for any type of single or autochange
player. Size $12 \times 2 \mathrm{~F} \times 2$ tin. Cbassis is isolated mains transplayer. Size $12 \times 21 \times 2 \mathrm{Lin}$. Cbassis is isolated mains trans-
ormer. For $200-250$ V. A.C. maing. Output for $2-3$ ohis opeaker. Volume and tone
$39 / 9$

## SELENIUM RECTIFIERS

| L.T. Types | H.T. Types E.W. |
| :---: | :---: |
| $2 / 6 \mathrm{v}$. If an H.W... 1/9 | 120 v. 40 mA..... 3/ |
| 6/12 v. 1 a. H.W... 2/9 | $250 \mathrm{v}^{\text {c }} 50 \mathrm{~mA} \ldots \ldots .3 / 11$ |
| Following F.W. (Bridge) | 250 v. $60 \mathrm{~mA} \ldots . .4 / 11$ |
| 6/12 v. 1 a....... 3/11 | 250 v. $80 \mathrm{maA} . . . .6 / 11$ |
| 6/12 \%. 2 a........ 6/11 | 250 จ. 250 mA . . . $12 / 9$ |
| 6/12 v. 3 a......... 9/9 | Contaet Cooled |
| 6/13 v. 4 a........ . $12 / 3$ | 200 v. $80 \mathrm{maA} . . . .{ }^{\text {6 }}$ 6/11 |
| 6/12 จ. ธ а........ 14/6 | 250 จ. 50 mA . F.W. |
| 6/12 v. 6 a $\ldots$....... $15 / 8$ | (Bridge) ........ $8 / 11$ |
| 6/12 $\mathrm{v}^{6 / 12} 10$ ล...... $25 / 9$ | 250 จ. $75 \mathrm{~mA} . \mathrm{F} . \mathrm{W}$. |
| $6 / 12$ v. 15 a......35/9 | (Bridge) ....... $10 / 11$ |

designed for and is specially are well up to standard. Pointote-polnt wiring diagram instruotions and parta list $1 / 9$. Thals receiver can be bult in brown or oream bakalite or veneered walnut.

VARLEY 2 Y. 14 A.ET ACCUMULATORS. New

JASON F.M. TUNER
Type FMTL. All parts in-
cluding Dial, Escutcheon
Punched Chassis \& Valves,
Power supply required
Power supply required
180 v .25 mA and 6.3 v
180 V .25 mA and 6.3 V.
$1.5 \mathrm{a} . \ldots . . . . . . . . . . . .66 / 19 / 6$
EX GOVT.
SMJOTHING CHOKES
60 mA .10 h .400 ohms $3 / 11$
80 mA .20 h .900 ohms $5 / 11$
10. HAA. 5 h .100 ohms $3 / 11$
100 nA .10 h .100 ohms $6 / 9$
250 mA .10 h 100

120 mA .12 h .100 10/11
$1200 \mathrm{mA}$..12 h .100 ohms $9 / 9$
$200 \mathrm{~mA} .5-10 \mathrm{~h} .100$ ohms
250 mA .5 h .50 ohms $11 / 9$

## Battery <br> Battery

 HEAVY DUTY KIT6/12
v. variable charge rate up to 6 anps. Consisting of Madns Srans., F.W. (Bridge), Selenium Rectifier, meter. Variable Charge Selector. Fuses, fuse-holders, panels, plugs and circuit. Only 59/6. Post 4/6.
charger
TRANSFORMER 200-230-250 v. 50 200-230-250 v. $50 \mathrm{c} / \mathrm{s}$ $\begin{array}{lllll}0-9-15 & \text { v. } & 1 \nmid & \text { a....... } 12 / 9 \\ 0-9-15 & \text { v. } & 24 & \text { a..... } & 15 / 9\end{array}$ $\begin{array}{lll}0-9-15 & \text { v. } 24 \\ 0-9-15 & \text { v. } & 3\end{array}$ $0-9-15$
$0-9-15$
v. 5 a. $0-9.15$ v. 8 a.
$12 / 9$
$15 / 9$
$16 / 9$ $15 / 9$
$16 / 9$
$19 / 9$ $16 / 9$
$19 / 9$
$13 / 9$ $19 / 9$
$23 / 9$ 28/9

## MICRO-AMMETERS

0-50 milero-amp. Diameter 217. spproz. Seaied 0-100.
Flush mounting, 29/6.

## EX GOVT. MAINS TRANSFORMERS

 Input $200-350$ v. 50 c.p.s. 250 v. 60 ma. 6.3 v. \& a.
Primary 200-250 v. Sec. 12 v . 20 a . (Carr. 7/8.). Primary $200-240$ v. 8 ec. 3,500 v. 5 mA .2 v. 2 a 50 watts, $0-110 / 120-230 / 250 \quad$ v.
D.C. SUPLY KTTS. Sultablo or alectric trains. Consist
of malns trans. 200-250 v .50 o.p.s. 12 v. 1 amp. selenium roct. (F.W. Brdige); 2 fuseholders, 2 fuses, cbange direction switch, variable speed regulator, partially drilled steel case
and circuit. Very limited number, and circuit. Very limited number, 33/9.

## HEAVY DUTY EX GOVT.

 SELENIUM RECTIFIERSWith large square aluminium coolnz ithe, 12

## ASSEMBLED

 CHARGER6 v. or 12 v. 2 amps. Fitted Ammeter and selector plug and selector plug
for 6 v or 12 . for 6 v . or 12 . case, finished attractive liammer blue. Ready for use with mains Double Fused Oniy
Carr. Carr. 3/9. 49/9 6/12 v. 3 amp. with rate selector and ammeter. $59 / 9$.
$50 \mathrm{c} / \mathrm{s} . \mathrm{A} / \mathrm{C}$. Mains

## ASSEMBLED 6 v . or 12 v .



Fitted Ammeter and variable charge selector Also selector plug for 6 v . or 12 v . charging. Double or 12 v. Charging. Double fused. Well-ventilated steel case with blue
hammer finish. Ready $\begin{array}{ll}\text { hammer finish. } \\ \text { for use with } & 69 / 9\end{array}$ for use with

69/9 mains and
output leads $\begin{array}{ll}\text { output leads. Carr. } 5 / \text {. } \\ \text { Or Deposit } & 13 / 3 \text { and }\end{array}$ 5 monthly payments of $13 / 3$.
As above, but for 6 amp. charging 5 GNS. Carr. 5/-. Or Deposit 16/- and 5 monthly payments of $16 /=$.

VALVES: Full range at really competitive prices. EX GOVT, CASES
Well ventilated, black crackle finished, undrilled cover. Size $14 \times 10$ : 81 In , high. IDEAL FOR BATTERY CHAR-
GER OR LNGTRUMENT CASE. COVER COULD BE USED FOR AMPLIFIER. Only 9/9, plus 2/9 post. RELAYS. Carpenter Type Polariged, $2 \times 9,500$ turns at
1,685 ohms. $13 / 9$ M niature type G.E.C. 670 M 1092 1,680 ohms. $13 / 9$. MInature type G.E.C. 670 M 1092
sealed wire ends 4 c/overs platinum, 12/9.

## R.S.C. A10 ULTRA LINEAR HIGH FIDELITY 12-14 WATT 30 WATT AMPLIFIER AMPLIFIER TYPE A11

 inputs such as "mlke" and
 RADIO FPEDER UNIT. ONLY 11 orne Or Factory built using latest ELa4 output vaives and with 12 Carr. 10/-118MS. monthary gurantee, 14 GNS. TERMS ON ASSEMBLED UNIT8. Protective Cover 19/9. Type 807 output valves are used with High Quality Sectionally feedback of 20 D. 13 . In maln loop. CERTEFED PERFORMANCE FIGURES ARE EQUAL TO MOST EXPENSIVE UNITS AVALLABLE. Frequency response $\pm 3 \mathrm{D} . \mathrm{B} .30-20.000 \mathrm{c} / \mathrm{s}$. Tone Controls $\pm 12$ D. 8 , at 50 c/s. $\pm 12$ D.B. to $-6 \mathrm{D.B}$. at $12,000 \mathrm{c} / \mathrm{s}$. hum and
noise $70 \mathrm{D} . \mathrm{B}$. down. Good quality reliable components used. Chassis finish blue hamnoise 70 D.B. down. Good quality reliable components used. Chassis antsh For A.C. mains $200-2 \overline{2} 0$ F. $50 \mathrm{c} / \mathrm{s}$. Outputs for 3 and 15 ohm apeakers. EQUALLE SUITABLE
FOR TIEE CONNOISSEUR OR FOR LARGE BALLS, CLUBS OR OUTSIDE FUNCTIONS, IDEAL FOR USE WITH MUSIOAL INSIRUMENTS, SUCH AS STRING BASS, ELECTRONIC ORGAN, GUITAR, to FOR DANCE BANDS, GARRISON THEATRES, Efo, etc. We ean supply Microphones, Sjeakers, etc., at keen cash prices or on terms with a aplihers. EXPORT ENQUIRIES INVITED.

FULL RANGE OF LINEAR HIGH FLDELITY AMPLIFIERS ALWAYS IN STOCK GL3A MINIATURE 3 WATT GRAM AMPLIFIERS
For $200-250$ v. 50 c.p.s. A.C. mains, Overall size only $118 \times 2 \mathrm{k} \times 2$ tin. Fitted Vol, and Tone changer unlt. Output for $2 \cdot 3$ obm speaker. Guaranteed 12 months. Only $59 / 6$.
R.S.C. A5 4-5 WATT HIGH GAIN AMPLIFIER

A highly sensitive 4 -valve guality amplifer for the bome, small club, etc. Only 50 mallivolts input is required for full output so that it is suitable for use with the latest high fidelity pick-up heads in addition to all other types of pick-ups and practically all makes geparate Bass and Treble controls are provided. .Besc give fol hom phytag record
equalisation. Hum-level is negligible being 71 . equaisation. Hum-level is negligible being
down. 15 D.B. of negative feedback is used. H.T. of 300 v .26 mA . and L.T. of 6.3 v . 1.5 a. Is available for the supply of a Radlo Feeder Unit or Tape Deck pre-amplifier. For A.C. mains input of 200-250
$50 \mathrm{c} / \mathrm{A}$. Output for $2-3$ ohm speaker. Chassis is not allve. Kit is complete in every detail and Includes fully punched chassis (with baseplate) with the blue hammer finish and point-w-point wiriag diagrams
 riage. Or Deposit 22/- and five monthly piyments of $22 /$ - for assembled unit. P.M. SPEAKERS, $2-3$ ohms 2$\} / \mathrm{m}$ Perdio $21 / 9$. 5 in . Coodmans $17 / 9.7 \times 4 \mathrm{in}$. R.A.
 with bigh Alux magnet 25/9. $10 \mathrm{in}$. R.A. $28 / 9$. $10 \times 6 \mathrm{in}$. Eliptical Goodmans $29 / 9$.
12 in . R.A. 29/11. 12in. R.A. 3 or 15 ohms, 10 watts, 12.000 lines $59 / 6$. TWEETERS. 4 in . Plessey, 3 ohms 18/9. R.A. 15 ohmb $25 / 9$.
R.S.C. TRANSFORMERS MAINS TRANSFORMERS. Frimaries 200-250-250
FULLY 8REOUDED. UPRIGHT MOUNTING
 TOP SHROUDED DROP-THROUGH TYPE 2600260 v. $70 \mathrm{~mA} ., 6.3$ v. $2 \mathrm{a} ., 5 \mathrm{v} .2 \mathrm{a}$
250
0250 v. 100 mA .6 .3 v. 3.6 a. $2500-250 \mathrm{v} .100 \mathrm{~mA} ., 6.3 \forall .2 \mathrm{~h}_{\mathrm{p}, 1} 6.3 \mathrm{v} .1 \mathrm{a}$
 $300-0-300$ v. $100 \mathrm{~mA} ., 6.3$ v. 4 a., $5 \mathrm{v}, 3 \mathrm{a}$ $300-0-300$ ₹ $130 \mathrm{mAA}, 6.3 \mathrm{v}$. a., c.t. 6.3 叉. 1 a

 MIDGET CLAMPED TYPE. Primariea 200-250
 FILAMENT TRANSFORMERS


AUTO (Step Up/Step Down) TRANSFORMERS $50 \cdot 80$ watts $110-120$ v. /230-250 \%. 150 watts $110-120$ v. $1200-350$ ₹.

## LINEAR PRE-AMP/TREMOLO UNIT

suitable for use with any Guitar Ampllfer. Controls
Volume, Frequency, Amplitude and swithes. Falves: Volume, Frequency, Amplitude and switches, Dalves: Reallo or Gram. Power required onty 5 ans

## OTPUT TRANSFORMERS

Midget Battery Pemers Midget Battery Pentode Small Pentode 5,0000 to 30
Standard Pentode $5,000 \Omega$ to $3 \Omega^{\circ}$
Standard Pentode $8,000 \Omega$ to $3 \Omega$ Standard Pentode $8,000 \Omega$ to $3 \Omega$
Multi Ratio, Single or P/P 3 or 150 Push pull 8 watte ELSAS to 30 Push pull 8 watte ELS43 10 iso Push pull 10-12 watts 8V6 to $3 \Omega$ or 150 Push puil 10-12 watts to match 6V6 to Push pull Ultra Linear for Mullard 510 Push pult $15-18$ watts, sectionally wound, 6 L 6 . KT 66, etc for 3 or 150
q

$$
\text { wound, 6L } 6 \text {, }
$$

$$
\begin{aligned}
& \text { Puah puil } 20 \text { watt high-quality sectionally woun } \\
& 6 \mathrm{~L} 6, \mathrm{KT} 66, \text { etc., or } 4 \text { or } 15 \Omega \text { fully sbrouded }
\end{aligned}
$$

MICEOPHONE TRANSFORMERS
120:1 High quality, elamped

$$
\begin{aligned}
& 120: 1 \text { High quality, clamped .......... } \\
& \text { 120: \&igh quality Mu metal screened } \\
& \text { 8MOOTHING OHOKES }
\end{aligned}
$$

8MOOTHING CHOKES
$50 \mathrm{~mA} ., 5 \mathrm{H} ., 100 \Omega 11 / 9$ $\begin{array}{cc}150 \mathrm{~mA} .7-10 \mathrm{~F}, \\ 100 \mathrm{~mA} ., 10 \mathrm{H} ., 200 \Omega & 11 / 9 \\ 8 / 9\end{array}$ $0 \mathrm{~mA}, 10$ H., $200 \Omega \quad 8 / 8 \quad 1$ amp. $0.5 \Omega$ L.T. cype $8 / 6$ LINEAR TAPE PRE-AMPLIFIER Type LP/1. Switched negative feedback equalisation. Positions for Record 1 in., 3 iin. 7 inin. and Playback. EM84. Recording level Tape Transcripior and high fidelity ampllfer but suilable alinost any Tape Deck. Gavs. Send B.A.E. for leaflet. LINEAR L45 MINIATURE $4 / 5 \mathrm{~W}$, QUALITY AM PLIFIER suitable for use with any record playing unit and mobl microphones. Negative reedback 12 D. . bans and treble controls. For A.C. mains input of 200-250 v. 50 e.p.s. Output for $2 / 3$ ohm speaker. Three miniature inulard valves.
 of 22l-: Beca 8.A.E. for leatet.

PUSH-PULL
ULTRA LINEAR
OUTPUT
"BUILT-IN"
TONE CONTROL
PRE-AMP
STAGES

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[^8]

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\text { AUTU, 1KANs. OUU W., } 0,10,200,230,250 \text { ₹. }
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 Preciaion engincered. Size only lăin. dia. $\times$ tin. ACOS MUKE 40 25j-.......TSL. STICK MUKE 35/MORE TRANSF. 50: $1,3 / 9$ ea,. $100: 1$ Potled $10 / 6$. LOUDSPEAKERS P.M. 3 OHMS. $24 \operatorname{in}$. $3 \operatorname{in} ., 41 \mathrm{in}$. $19 / 6$ Sin. 17/6. 8in. $x$ bin, Goodmans 21/-. $7 \mathrm{in} . \times 41 \mathrm{n}$ 19/6. 64in. Rola 18/6. 8in. Bola 21/6. 10in. R. Plesse 18in. Plessey 30/- 121n. Plessey 15 ohms 45/-. Stentorian
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| Size | Type |
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| $21 . \mathrm{in}$. | MC/FR |
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| $21 . \mathrm{in}$. | MC/FR |
| 2in. | MC/FR |
| $2{ }^{\text {\% }}$ in | $\mathrm{MC} / \mathrm{FR}$ |
| 2 2in. | $\mathrm{MC/FR}$ |
| $2 \frac{1}{2}$ in. | MC/FR |
| $21 . \mathrm{in}$. | $\mathrm{MC} / \mathrm{FR}$ |
| 2 in . | MC/FR |
| $2 \frac{1}{12}$ | $\mathrm{MC} / \mathrm{FR}$ |
| 21 in. | MC/FR |
| 2 in . | $\mathrm{MC} / \mathrm{FR}$ |
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15 AMP. BATTERY CHARGER (Westinghouse Type B.C.3) will charge three lead acid cells at 15 amps Input $200 / 250$ volts, 50 cycles A.C. Charging current is regulated by four-position switch and variable resistance for fine control. Fitted with $0 / 20$ ammeter, rotary on/off switch and rewirable fuses. This first-class instrument at the bargain price of $£ 15$, carriage $15 /-$ RECTIFIER UNIT RA-63-B Input $105 / 125$ Volts A.C. Output 12 volts 5 amp. D.C. In neat crackle finish case with circuit breaker, reverse current relay, with 3 -way switch, "Trickle charge," "Off," "High Charge." This Brand New American unit is offered at only $85 / 10 / 0$, carriage $5 /-$. Can be Brand New American unit is offered at only $85 / 10 / 0$, car
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Large size as illustrated, 2-6 volts D.C., or $75-120$ volts D.C. 15/-

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$1 \times 1 \times 3 \frac{1}{2}$ in. operating from $100-120$ volts D.C. Coil resistance 2,300 ohms. Ten counts per sec. Type 100 B 35/- each, post $2 /$ -

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With less than $1 \%$ total harmonic distortion and a hum level -80 dB . The frequency response is level from 10 cps to 40 $\mathrm{K} / \mathrm{cps}$ and full power of 20 watts is delivered from 20 cps to 20 $\mathrm{K} / \mathrm{cps}$. Printed circuit design, 5 valves ECC82, 2-EF80, $2-$ EL. 34 with metal rectifiers. The pre-am-
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A pocket size individual circuit tester. Complete with test leads. Ranges: D.C Volts: 0-2.5-10-50-250.500-5.000 y A.C. Voles
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Size: $5 \frac{1}{2} \times 1 \frac{1}{2} \times 3 \frac{1}{2}$ in.
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S.T.C. SELENIUM METAL RECTIFIERS F/B
FOR BATTERY CHARGERS, ETC.
6 or 12 v. 1 a. $51-; 12$ v. 2 a. $7 / 6$;
 $\begin{array}{llllllllll}12 & \text { v. } & \text { a. } & 20 /=i & 12 & \text { v. } & 10 & \text { a. } & 35 / \% ; \\ 24 & \text { v. } & 1 & \text { a. } & 10 \% & 24 & \text { v. } & 2 & \text { a. } & 15 / \ldots ; \\ 24 & \text { v. } & \text { a. } & 25 /-: & 24 & \text { v. } & 4 & \text { a } & 30 /=;\end{array}$

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with built-in transformer
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Length 7 lin . Head dia. Itin. Supplied with neck band, lead and supplied with neck Terrific performance!
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TELESCOPIC FIOOR STAND base, chromium stand with screw top. Extends to approx. Git. Suitable No

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"I 2 in . P.M. HEAVY DUTY." 15 ohms, 15 watts, $30-14,000$ c.p.s OUR PRICE \&4110!
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12 VOLT D.C. AMPLIFIER (Parme'ro). As new, 15 watt push pull output Mike and gram. inputs tapoed output transiormer, E $9 / 19 / 6$ Carr. 10/6. (Hand microphone for above 30 - extra.) 50. WATT EX-GOVT. AMPLIFIER. Type III with 4KT66's in paralleled push-pull. Standard 200-250 v. A.C. input. Outpus imped. 600 ohms line. High imp. gram . and mike input. Bass boost
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4 -speed plays 10 records 12 in ., 10 in . or 7 in . at 16, 33 , 45 or $78 \mathrm{r} . \mathrm{p} . \mathrm{m}$. Intermixes 7 in ., 10in. and 12 in , re ords hrown. Dimensianse 1211 a . $x$ 10pin. 8pace required nhove baseboard 4 lin., below baseboard 2 2in. Fitted
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 sokes. Frame o.p. Pranntormer 600 pr. 18 KV . smoothing condenser. Can be used
 As above. but for 625 lines $29^{\prime} 6^{\text {Plos }} 4 / 6 \mathrm{P} .8 \mathrm{P}$. FOCUS MAGNET suitable for the above (state tube), 10 -. 3/-P. \& . P. P. £2.10 ${ }_{4 / 6 \mathrm{p}}^{\text {Plus }}$

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2in moving coil meter, scale calibrared in A.C./D.C. volts, ohms and milliamps. Voltage range A.C./D.C. 0 $\begin{array}{lll}50, & 0-100, & 0-250, \\ \text { Milliamps } 0-10,0-100 \text {. Ohms }\end{array}$ Milliamps $0-10.0-100$. Ohms
range $0-10,000$. Front panel, ranges witch, wire wound pot (for ohms zero setting). toggle switch, resistor and rectifier. 19/6. P. \& P, 2/-. Wiring diagram $1 /-$, FREE with kit.

[^9]
## 5-TRANSISTOR POCKET RADIO

## completely portable. no

 aERIAL OR EARTH REQUIRED Size $47 \times 3 / \times 1$ lin. Output $200 \mathrm{~m} / \mathrm{w}$. 5 first quality transistors. Pushpull ourpur.Fitted 2 tin. high-flux moving coil speaker.
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Coverage: $120 \mathrm{Kc} / \mathrm{s}-230 \mathrm{Kc} / \mathrm{s} . \quad 300 \mathrm{Kc} / \mathrm{s}$. $\begin{array}{llllll}\text { Coverage: } 120 & \mathrm{Kc} / \mathrm{s}-230 & \mathrm{Kc} / \mathrm{s} . & 300 & \mathrm{Kc} / \mathrm{s} . \\ 900 \mathrm{Kc} / \mathrm{s} ., & 900 \mathrm{Kc} / \mathrm{s}-2.75 \mathrm{Mc/s.} & 2.75 & \mathrm{Mc} / \mathrm{s} .\end{array}$ $8.5 \mathrm{Mc} / \mathrm{s},+8 \mathrm{Mc} / \mathrm{s}-25 \mathrm{Mc} / \mathrm{s}$, , If Mc/s.-56 Mc/a., $24 \mathrm{Mc} / \mathrm{s}$, , $84 \mathrm{Mc} / \mathrm{s}$. Metal, casse 10 in . $\times 61 \mathrm{in}$. $x 4 \mathrm{~Hz}$. Size of scale 64 in . $\times 3 \frac{1 \mathrm{in} \text {. } 2 \text { valves }}{}$ and rectifer. A.C. mains 230-250 F . Internal miodulation of 400 c.p.s. to a depth of 30 per cent. modulated or unmodulated R.F.
Output continuously varlable. 100 millivolts C.W. and mod. switch varlable A.F. output and moving enfl output meter. Grey hatomer falth case and white panel.

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Or 25/0 deposit. P. \& P. $5 / 6$ and 6 monthly payments of 21/6.
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Covering $100 \mathrm{Kc} / \mathrm{s}-100 \mathrm{Mc} / \mathrm{s}$, on fundamentals and $100 \mathrm{Mc} / \mathrm{s}$ to $200 \mathrm{Mc} / \mathrm{s}$. on harmonics. Metal case loitr. X olia. x otin. grey hams-
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$350-0-350,70 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .1 \mathrm{amp.}$,6.3 v .2 amp., $10 / 6,250-0-250,70 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} ., 2 \mathrm{amp}$, 10/6. Postiage and packing on the above $3 / 6$.
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 EZ81 ... 7/-3Q5GT 9/6 12Q7GT 6/6 $\begin{array}{lllllll}\text { FC13 } \ldots . . & 5 & -3 S 4 & \ldots & 7 / 6 & 12 S K 7 & 6 /- \\ \text { FW4 } 4 / 500 & 3 V 4 & \ldots & 8 /- & 125 L 7 & \ldots & 8 /-\end{array}$ \begin{tabular}{lllll|l}
\& $10 /-4 D 1$ \& $\cdots$ \& $3 /-$ \& $12 S N G T$ \& $10 /-$ <br>
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 $\begin{array}{llllllll} & 10 /-5 Y 3 G & \ldots & 8 /- & 25 L 6 G T & 10 / \\ \text { KT2 } & 5 / & 5 Y 4 G T & 7 / 6 & 25 Z 4 & \ldots & 9 / 6\end{array}$ $\begin{array}{lllllll}\text { KT33C… } & 8 / 6 & 5 Z 4 G & 9 /-25 Z 4 & \cdots & 9 / 6\end{array}$ KT61 ...13/6 6A7 KTIO1 101-6A8G KTW6I 6/6 6AK5 

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[^11]
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