

Will a high slope valve, when placed in the instrument, burst into spurious oscillation, thus giving rise to incorrect readings and possible damage

The "AVO" Valve Characteristic Meter incorporates a specially designed panel layout and wiring system (prov. patent) which virtually eliminates spurious oscillation.

Does the instrument contain valves which may need replacing from time

With the exception of a small protection diode, there are no internal valves to deteriorate or break down and cause misleading readings to be given. Thus, expensive periodical replacements are not required.

Will the instrument detect grid current and indicate its direction and

The "AVO" Valve Characteristic Meter will indicate the direction of flow of grid current and give its magnitude in microamps.

Does the instrument test diodes and rectifiers under load? The "AVO" Valve Characteristic Meter checks diodes and rectifiers under load conditions.

The "AVO" Valve Characteristic Meter measures inter-electrode insulation in megohms with valve cold or hot, also cathode/heater insulation with the valve hot, and indicates any breakdown below 10 megohms. It will carry out tests on small thyratrons, tuning indicators, etc. It is fitted with bases for most valves in current use and adaptors will be available to keep the instrument fully up-to-date should new bases come into use. A special form of polarised relay is incorporated to give protection against inadvertent overloads or valve failure.

Write for fully descriptive literature

with sufficient scope for YOUR requirements!

When purchasing a Valve Tester ask the following questions:-

Is it a simple Go/No Go instrument, or will it enable you to take measurements at any point on a characteristic curve?

The "AVO" Valve Characteristic Meter can be set up in a matter of seconds and used as a simple Go/No Go tester if required. It will, in addition, produce sufficient information to enable the valve's static characteristic curves to be plotted.

Does the instrument depend for its operation on pre-determined empirical data issued by its manufacturer?

The "AVO" Valve Characteristic Meter simulates nor-

mal working conditions for the valve under test and thus is capable of reproducing the valve manufacturer's data.

If you are called upon to select a pair of accurately matched valves, will the valve tester carry out the required checks, and maintain your reputation as an expert?

The "AVO" Valve Characteristic Meter enables the slope, and anode, screen, or grid current of a multi-electrode valve to be checked with any voltage between 0 and-100V on the control grid.

Before any information can be obtained about a valve, must the instru-ment be provided with a complex series of accessories which may become lost, mutilated, or are not available when an unusual or new type of valve has to be tested?

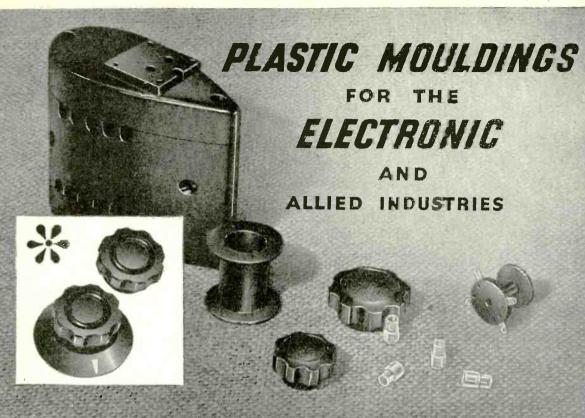
The "AVO" Valve Characteristic Meter is provided with two handbooks. The first gives detailed information on the technique of valve testing, full circuit diagrams and adequate operating instructions. The second is a quick reference Data Manual covering more than 3,000 British, American and Continental valves, and gives inter-service equivalents. The Valve Data Manual is issued for the convenience of the instrument user, but

even without it valves can, if necessary, be checked using data taken from the valve maker's data sheets.

Valve CHARACTERISTIC

THE AUTOMATIC COIL WINDER ELECTRICAL EQUIPMENT CO. LTD. WINDER HOUSE . DOUGLAS STREET Jelephone VICtorio 3404-9 LW.2 NOGNOJ

VC.5



- FULLY A.J.D. APPROVED FOR DEFENCE PROGRAMME REQUIREMENTS.
- AMPLE CAPACITY AVAILABLE FOR ALL COMPRESSION MOULDINGS, UP TO 250 TON PRESSES, AND SMALL PRECISION MOULDINGS IN THERMOPLASTICS.
- SPECIAL GRADE MOULDINGS IN MELANINE AND NYLON-FILLED PHENOL.
- PROMPT ATTENTION TO ALL ENQUIRIES.
- GOOD, RELIABLE DELIVERY, AND FIRST-RATE QUALITY IN PRODUCTION.
- A REPRESENTATIVE WILL CALL, IF DESIRED.



Introducing ...

PLEASE WRITE FOR FULL DETAILS

THE VISCOSE RANGE OF INSTRUMENT CONTROL KNOBS

SKIRTED AND UNSKIRTED, IN TWO SIZES, AT EXTREMELY KEEM PRICES

VISCOSE DEVELOPMENT COMPANY LIMITED WOLDHAM ROAD, STROMLEY, KENT. RAVENSBOURNE 2641

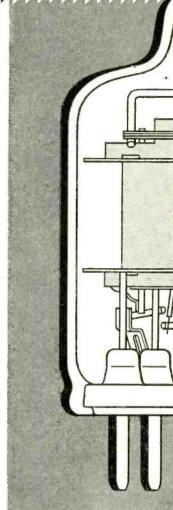


A NEW R.F. PENTODE WITH

- 1 Recommended Frequency Limit 400 Mc/s.
- 2 Mutual Conductance 5.1 mA/V
- 3 Filament Consumption 175 mA.

The Mullard R.F. Pentode, EF95, provides a better size to performance ratio than that previously obtainable from British valves of a similar class. It is constructed on the B7G miniature base and works efficiently at frequencies up to 400 Mc/s. Some of the more outstanding features of this valve include low input capacitance, low anode to grid capacitance, high mutual conductance and low heater consumption. These features, together with an operating voltage of 180 volts (120 volts under certain conditions), will particularly interest designers of compact communications equipment. In circuits involving a number of R.F. and I.F. stages, the EF95 may be used throughout, with a resultant marked saving in total heater consumption. Furthermore, the use of only one valve type in such applications enables maintenance problems to be reduced. The EF95 has similar electrical characteristics to the American 6AK5, and may be used as a direct replacement for it. Full technical information on this and other

types in the Mullard range of communication

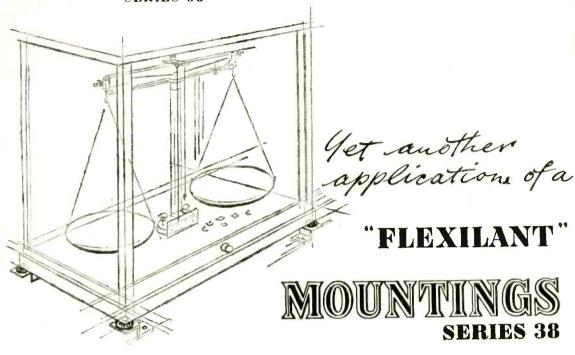


	TECHNICAL DATA				
HEATER	CHARACTERISTICS	LIMITING VALUES			
Vh - 6.3V	Va - 180 V	Va max 180 V			
Ih - 0.175 A	Vg2 - 120 V	pa max 1.7 W			
	Vg12.0 V	Vg2 max 140 V			
CAPACITANCES	Ia - 7.7 mA	pg2 max 0.5 W			
cin - 4.0 μμF	Ig2 - 2.4 mA	Ik max 18 mA			
Cout - 2.8 μμF	gm - 6.1 mA/V				
c _{a-g} l - 0.02 µµF	r _a - 690 KΩ	BASE B7G			

valves is available on request.

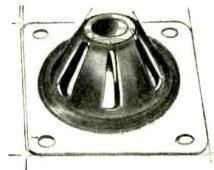






In this instance the Series 38 "Flexilant" Mounting protects a delicate instrument from vibration and shock. Other applications are manifold — from aircraft to power-station instrument panels: from ship's instruments to the protection of pyrometers in a steel works.

We produce a range of components that absorb vibration; eliminate noise; suppress shock. Our new catalogue lists all these for you.



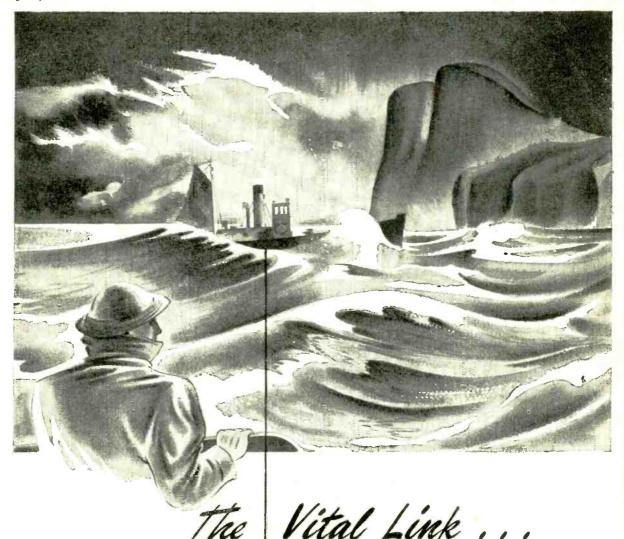
RURRER RONDERS LIMITED

IN ASSOCIATION WITH EMPIRE RUBBER COMPANY (Proprietors: H.G. MILES LTD.)

DUNSTABLE · · · REDFORDSHIRE

TELEPHONE: DUNSTABLE 533-536 14 LINES) TELEGRAMS: SPANDIT. DUNSTABLE





. with safety in the hazardous enterprise of the deep sea trawler is its radio and radar equipment upon which safe navigation depends. Thousands of soldered joints contribute to the efficient functioning of this delicate apparatus. One dry or H.R. joint could mean the breakdown of a circuit, the destruction of the vital link, a perilous voyage.



FAULTLESS FLUXING PRESERVES THE VITAL LINK

Dry or H.R. joints are impossible with Superspeed for the flux is always released in exactly the correct proportion. This faultless fluxing action is



achieved by the unique STELLATE core which gives six points of rapid solder collapse. At soldering temperature the activated rosin flux is released immediately for effective spreading and wetting. Superspeed is being used more and more in the production of radio and radar equipment where faultless joints are essential.

"WHITE FLASH" ACTIVATED ROSIN-CORED SOLDER

for general electrical, electronic and telecommunication work and all standard uses. A.I.D. and G.P.O. approved. Complies with M.O.S. Specification DTD 599. In all standard tinflead afloys 10-22 s.w.g. Also available in a range of coloured cores, indispensable for simple Intermediate and final Inspection and circuit or operator identification. Samplesof Superspeed and the comprehensive Superspeed booklet gladly sent on request. Technical advisers are available for free consultation.

Cored and solid solder rings and solid solder washers supplied to customers' specifications.

MANUFACTURED BY THE ENTHOVEN GROUP

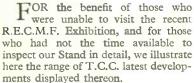
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present

THEIR LATEST DEVELOPMENTS

IN CONDENSERS...



These are indicative of the progress which is constantly being maintained, and which ensures that "T.C.C. Leadership in Condensers" is a tangible reality.

I. SMALL CAPACITY CLOSE TOLERANCE TUBULAR CERAMICS

For top end coupling in Band Pass Filters. Capacity range 0.5 pF to 5 pF at 500 v. D.C. Tolerances $\pm 20\%$ and $\pm 10\%$.

2. TANTALUM ELECTROLYTICS

The special neutral electrolyte prevents corrosive injury in the event of mechanical damage. These 8 μF condensers are for working voltages up to 120 °C. and for temperatures up to 120 °C.

3. "METALPACK" & "METALMITE" PAPER TUBULARS IMPREGNATED in "VISCONOL-X"

New impregnant improves reliability at 100°C. Full Ministry Type Approval (R.C.S.131 Cat.A.H2) has been granted.

4. "METALPACK" PAPER TUBULARS with CERAMIC END SEALS

New external construction gives complete protection against moisture in 100% humidity at 100°C.

5. H.V. TUBULAR CERAMICS

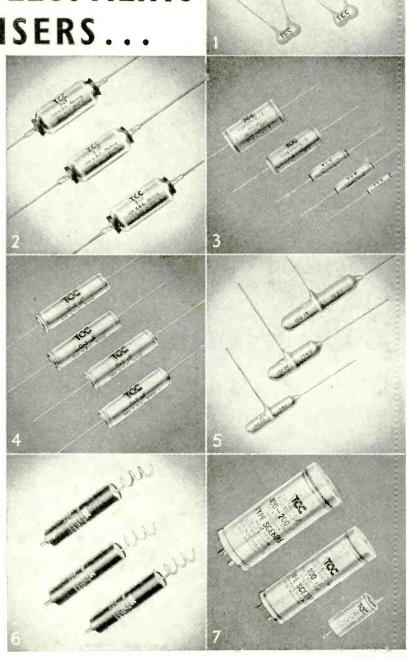
For Pulse Feeders in Radar equipment and Line Time bases in T.V. receivers. Ranges available for 1 kV. to 10 kV. D.C. working. Capacities from 10 to 620 pF.

6. HIGH VOLTAGE PAPER SMOOTHING CONDENSERS TYPE C.P. 561

For 25 kV. E.H.T. smoothing in large screen T.V. receivers. Absence of metal at "hot end" prevents corona losses.

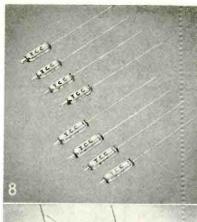
7. HIGH TEMPERATURE ELECTROLYTICS

Ability to work at 85°C. without voltage de-rating. Characteristics low leakage current and high ripple rating.



THE TELEGRAPH CONDENSER COMPANY LIMITED

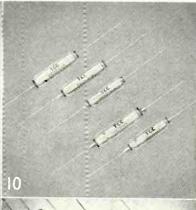
RADIO DIVISION: NORTH ACTON . LONDON . W.3 . Telephone: ACORN 0061 (9 lines)



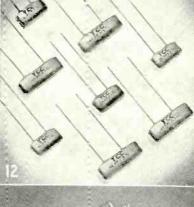
... as shown at the R.E.C.M.F. EXHIBITION IN LONDON.



7 CC (RE)











Obviously, there is no room in this announcement for full technical data on these various Condensers.

We shall be happy to supply complete details of any range in which you are particularly interested, or to advise you of the types most suited to your particular requirements.

8. SUB - MINIATURE ELECTROLYTICS for HEARING AIDS & TRANSISTORS

Smallest Electrolytic ever made. Two sizes available—6 μF for 3 v. D.C. working and 8 μF for 6 v. D.C. working.

9. Hi-K CERAMIC DISC

For T.V. de-coupling and spark suppression. Two sizes—10 mm. and 20 mm. diam. Capacity range .001 µF to .02 µF.

10. IMPROVED "PICOPACK" ELECTROLYTICS

Smaller sizes and higher ratings are now offered. Voltage range extended to 450 v. D.C. at 70°C. Entirely new range for 85°C. working.

II. METALLISED POLYSTYRENE CONDENSERS

Small size tubulars for Tuned Filters. Excellent electrical properties. Max. capacity is .5 μF for 350 v. D.C. wkg. at 70°C.

12. CLOSE CONTROLLED TEMPERATURE COEFFICIENT CERAMICS

For Temperature Compensation in Oscillator and I.F. circuits. "Plimoseal" finish improves stability. Available in 6 temperature Coefficients.

13. HIGH VOLTAGE ELECTROLYTICS

Type 928—8 μF. 800 v. D.C. working. 900 v. surge at 60°C. 700 v. D.C. working. 800 v. surge at 70°C. All-Aluminium Internal Construction: Chassis mounting, Fully tropical.

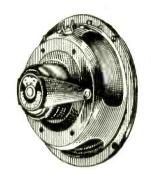
14. CLOSE ACCURACY PLASTIC FILM CONDENSERS

For Tuned Filters in Carrier Telephony equipment and Reference Standards. Exceptionally stable capacity, better than 0.1%. Tolerances $\pm \frac{1}{6}\%$.

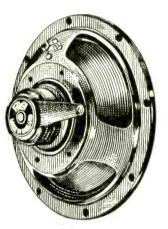
THE TELEGRAPH CONDENSER COMPANY LIMITED

RADIO DIVISION: NORTH ACTON . LONDON . W.3 . Telephone: ACORN 0061 (9 lines)

WE'PRESENT another advance in our new Series 800, Mark II Reproducers. Skilful design of the magnet system enables us to provide increased sensitivity in the three most popular sizes—5in., 6½in. and 7 x 4in. elliptical—with a negligible increase in overall depth.

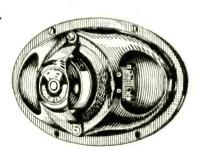


Designers of sets in which bulk, weight and cost are important factors are invited to ask for samples of the 10,000 Gauss versions of Types 850, 865 and 874. These will gladly be supplied, together with full technical information.





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Manufacturers
to the radio industry
since 1930



REPRODUCERS AND AMPLIFIERS LIMITED

WOLVERHAMPTON ENGLAND

Telephone: Wolverhampton 22241 (5 lines)

Telegrams: Audio, Wolverhampton



* A NEW, BETTER TV TUNER!



PERFORMANCE

GAIN

Power gain of the unit is 24dB. measured from the aerial input to the 1.F. output, the mixer anode load for measurement purposes being 1k/ohm shunted by 12pF. As a practical example, using a two valve transformer-coupled amplifier with a bandwidth of 2.75 Mc/s (including sound rejector circuits) an aerial input of 25 microvolts modulated 100% produces 2 volts p.p. across the diode load.

NOISE

Noise figure on all channels better than 10.5dB.

I.F. REJECTION

Better than 45dB. on all channels at any spot frequency in the I.F. channel.

IMAGE REJECTION

Better than 60dB, on all channels.

OSCILLATOR DRIFT

Measured on channel 5, with stable H.T. supply, for a period of two hours after a warming-up period of two minutes, ambient temperature increased from 18°C to 60°C, total drift 30Kc/s. Drift, with change in H.T. supply from 160 volts to 230 volts, less than 10Kc/s.

SWITCH RESETABILITY

Better than 5Kc/s on all channels.

POWER REQUIREMENTS

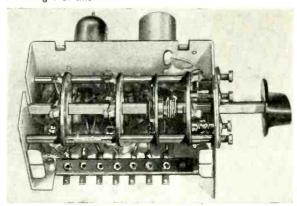
180V. 12.6V. at .3 amps. Heaters are series connected with both ends isolated from chassis.

Cyldon

5-Channel, Switched TELETUNER Type TV.5

INSTANT and POSITIVE SELECTION by single knob control of any one of the five B.B.C. Television channels is the job for which we designed this new "Cyldon" Switched Teletuner. It was the centre of great interest at the recent R.E.C.M.F. Exhibition, and we are pleased and proud to present these further details.

The "Cyldon" TV.5 Teletuner comprises a pentode R.F. amplifier stage and a double triode frequency changer, channel selection being accomplished by the switching of incremental inductances. More constant performance over the television band is thus obtained by avoiding the tracking difficulties inherent in the infinitely variable type of tuner. Ease of handling by the user and rapid conversion as alternative transmissions become available are further important advantages of this unit.



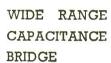
Underside view of "Cyldon" TV.5 Teletuner, with casing removed.

Another new "Cyldon" Teletuner ... Type TV.12, a 12-channel Tuner which performs the functions of RF amplifier and frequency changer of a television receiver. Write for booklet TV.1953 giving full details.

SYDNEY. S. BIRD

Contractors to Ministry of Supply Post Office. and other H.M. Government Depts

CAMBRIDGE ARTERIAL ROAD . ENFIELD . MIDDX. Enfield 2071-2





For the accurate measurement of in situ capacitance or resistance, all measurements being made in the form of a three terminal network.

Capacitance range — $0.002\,\mathrm{pF}$ to $100\mu\mathrm{F}$ in 18 ranges. Resistance range — 1α to $10,000\mathrm{M}\alpha$ in 18 ranges. Ranges increase in alternate decimal multiples of 3 and 10. Frequency 1592c/s ($\omega=10,000$). Accuracy $\pm1.0\%$ of full scale on all ranges.

Full technical details are available on request.



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A Company within the J. Arthur Rank Organisation

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SALES AND SERVICING AGENTS F. C. Robinson & Partners Ltd., 287 Deansgate, Manchester, 3 Hawnt & Co., Ltd., 59 Moor St. Birmingham, 4 Atkins, Robertson & Whiteford Ltd., 100 Torrisdale Street, Glasgow, S.2.



FROM THE OUTSIDE and READY FOR USE IN FIVE MINUTES!

The "AUTEX"

Here is revolution in car aerial design-a ONE hole fixing aerial that can be completely installed FROM THE OUTSIDE. No longer is it necessary to manoeuvre under the scuttle or dashboard and to work "by feel." Thanks to the use of a special split washer device, in conjunction with a positioning sleeve, the aerial is self-locating, and is firmly secured FROM THE OUTSIDE. It can be mounted vertically or horizontally (or at any angle in between) in any convenient position on the car-on either a flat or curved surface, such as the bonnet, scuttle, roof or mudguard.

And in position it is entirely free from rattle—due to the special packing glands which also ensure the smooth action of the telescopic rod. This aerial has that high-signal pick-up and electrical efficiency always associated with every Antiference Aerial.

NO ASSEMBLING—WIRED COMPLETE
FOR IMMEDIATE
INSTALLATION

model TCA/6236 with mounting assembly of sturdy die-cast metal; three section telescopic rod (extended 62 in., closed 24 in.) of high-grade brass. All exposed parts heavily chromium plated and with fully weatherproofed connections. Complete with 36 in. low-loss co-axial polythene insulated P.V.C. covered cable, fitted with standard co-axial plug.

MODEL TCA/6260 as above but with 60 in. cable.

LIST PRICE 37/6

Full details are given in leaflet No. NI/W, available on request.

ANTIFERENCE

ANTIFERENCE LIMITED, BICESTER ROAD, AYLESBURY, BUCKS.

FOR HIGH-FREQUENCY INSULATION



The Tuning Coil shown is supported by our "FREQUELEX" Ceramic Rods, and forms part of a 200 K.W. Radio Transmitter. This is only one of many applications where Rods made to close limits are required.

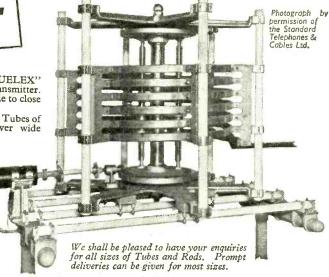
We specialise in the manufacture of Ceramic Rods and Tubes of various sections in several classes of materials over wide dimensional ranges.

The Principal Materials are :-

 Porcelain for general insulation.
 Frequelex for High Frequency insulation. 3. Permalex and Templex for Capacitors.

The degree of accuracy depends on the size of the Rod or Tube, but the standard degree of accuracy is outlined in the Inter Service Component Manufacturer's Council—Panel R Specification embodied in our Catalogue of Radio Frequency Ceramics, copy of which will be sent on request.

Large Rods up to 44" long and 14" square are used as supports for Tuning Coils, etc.



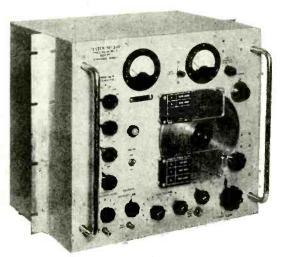


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BULLERS LIMITED, 6 Laurence Pountney Hill, E.C.4.

Phone: MANsion House 9971 (3 lines) Grams: Bullers, Cannon, London

BL4B



Power supplies: 200 — 250 Volt. 50 c/s

SELECTIVE TRANSMISSION

MEASURING SET

MODEL RP 3110

Designed and manufactured for G.P.O.

This is a precision instrument for measurements on multi-circuit coaxial cable carrier systems by means of a comparison with locally generated signals of known frequency and level.

Frequency coverage: 60 Kc/s-3 Mc/s in 7 ranges.

Calibration accuracy: below 0.2% or 2 Kc/s whichever is the greater.

Range of measurements:

through levels + 10 db to - 61-5 db or terminated levels + 10 db to - 81-5 db referred to ImW in 75 ohms

BRITISH COMMUNICATIONS CORPORATION LTD.

SECOND WAY, EXHIBITION GROUNDS, WEMBLEY, MIDDX.

Telephone: WEMBLEY 1212

Cables: BEECEECEE, WEMBLEY

DARITIES

CAPACITOR



MICA DIELECTRIC CAPACITORS

Eminently suitable for H.F. Transmitting and R.F. Heating Circuits.

Makers of the first, and of the largest Mica Capacitors in the World, Dubilier have maintained the lead in this important branch of Capacitor Eugineering. The example shown is a solid filled mica capacitor in a substantial porcelain

container. Screw threaded metal terminal bosses with large surface area contacts provide a convenient means of mounting.

These capacitors are designed for use as Grid and Anode stoppers, as By-Pass Capacitors in radio-frequency power circuits where a small radio-frequency component is superimposed upon a higher D.C. or low-frequency A.C. voltage, and in oscillatory circuit positions in low power radio-frequency transmitters and similar equipment.

Full details of these and other outstanding Capacitors are available upon application.

DUBILIERCAPACITORS

DUBILIER CONDENSER CO. (1925) LTD., DUCON WORKS, VICTORIA RD., N. ACTON, LONDON, W.3. Phone: Acorn 2241 (5 lines). Grams: Hivoltcon, Wesphone, London. Cables: Hivoltcon, London, Marconi International Code



SEA FISHING with INSTRUMENTS!

Sifam Instruments are fitted to the SIMRAD Echo Sounding electronic gear manufactured by Simonsen Radio A.S., Oslo. This highly sensitive apparatus is used by the Norwegian fishing fleet to locate shoals of fish.

When the fishermen have hauled their nets or seines, and secured a good catch, they call the fish wholesaler on their SIMRAD Radio Telephone, which is also fitted with a SIFAM Instrument.

The particular instrument used for this purpose is the SIFAM Type M.20. Details of this and other Sifam Instruments will be furnished on application.

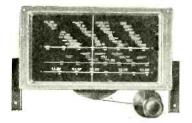
Write for Catalogue No. S.11.



SIFAM ELECTRICAL INSTRUMENT CO. LTD.

Phone: Torquay 4547/8. LEIGH COURT, TORQUAY, DEVON

EXACT EFFORTLESS TUNING



The S.L.8 Spin wheel drive gives easy control through a ratio 24-1. Fitted with constant velocity coupling, it eliminates strain on the Condenser, providing mechanical and electrical isolation from vibration and noise.

Complete with 3-band glass scale 9in. \times 4½in. Printed short, medium and long wavebands with station names. Scale length 7in. Supplied with florentine bronze escutcheon.

PRICE 27/6.

S.L.5, similar but fitted with reverse vernier drive, gives ratios of 18-1 search and 50-1 reverse vernier.

PRICE 26/6.

Replacement Scales calibrated to Copenhagen Plan now available for:

Airplane drive 2/3 retail
Squareplane Drive 2/6 retail

Full Vision Drive 2/9 retail S.L.8 or S.L.5 Drive 4/6 retail

PRECISION COMPONENTS BY

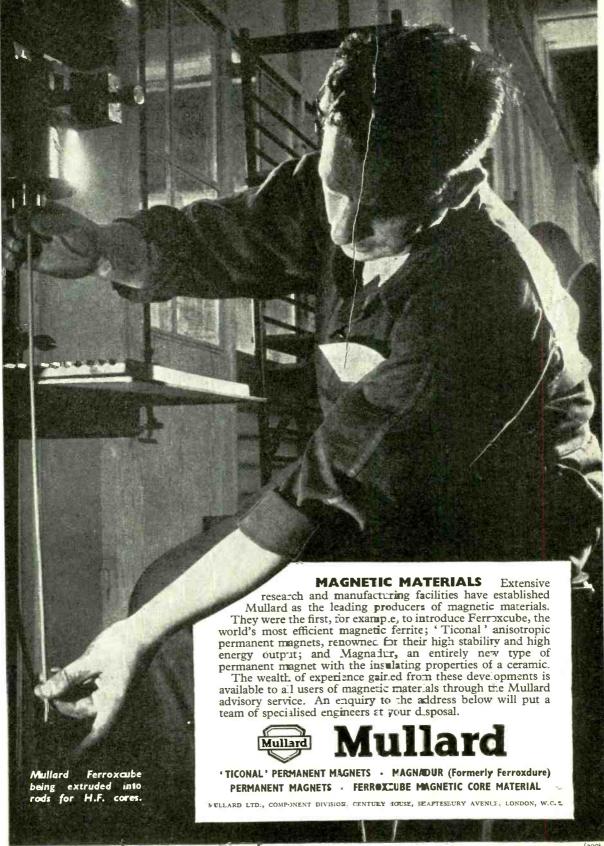


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- Constant Tape Speed-7.5 inches per second.
- Frequency Response-Essentially flat from 100-7500 c.p.s.
- High Quality Push/Pull Output.
- Recording Duration 30 minutes per reel.
- Dynamic Range approximately 40 decibels.
- Power Supply 200/250 A.C. 50 cycles—Consumption 80 watts.

Trade enquiries

invited

Now available in England—the book "Magnetic Recording" by Dr. S. J. Begun. A comprehensive treatise. Price 25/-, postage 9d. extra.

THERMIONIC PRODUCTS LTD.

Division S/M WW, HYTHE, SOUTHAMPTON, Phone: Hythe 3265 London Showrooms: Morris House, Jermyn Street, Haymarket, S.W.I. Phone: Whitehall 6422,

MODELS AVAILABLE **FROM**

£69-10-0

Sales and Service Centres: Birmingham -Manchester - Leeds - Newcastle and Glasgow



Wayne

VIDEO OSCILLATOR

TYPE 0222A

covers 10 Kc/s-10 Mc/s

Model 0222A is introduced to meet the demand for an oscillator reaching 10 Mc/s. It is an improved version of the 0222 which it supersedes All the outstanding features of the original model are retained, including low harmonic content and exceptional stability of frequency and amplitude.

SPECIFICATION

Frequency Range: 10 Kc/s-10 Mc/s in 6 ranges Frequency Stability: better than 1 in 103 in 1 hour

Frequency Accuracy:

+ 10 db to - 50 db on 1 Vp-p

Output Impedance:

75 ohms

Total Harmonic Content: less than 1%

Amplitude constant to within ± 1 db at any frequency setting

THE WAYNE KERR LABORATORIES LIMITED . NEW MALDEN . SURREY . MALDEN 2202

Output:

A Technical Handbook for Electronic Engineers

This Handbook contains the fullest information about all types of Ferranti Valves and Cathode Ray Tubes, giving for each type complete data such as physical details, base connections, ratings, operating conditions, with graphs, etc., where necessary.

The whole is a most valuable book of reference to the electronics engineer. It is in loose-leaf form, so that new data can readily be inserted.

Price 5'-

Additional data sheets will be sent to subscribers from time to time.



NEW



Designed to meet the demand for Egen reliability within the smallest possible compass, these exceptionally small carbon potentiometers (* diameter) retain all the desirable features of their standard-size counterparts. The special Egen carbon deposition process ensures a highly stable resistance element of extreme durability.



noise. Positively located soldering tags, silver plated for easy soldering. All steel parts rustproofed. Standard resistance values available, from 5000 ohms

Type 115 is identical to Type 105 except that a 2-pole Q.M.B. switch is incorporated.



to 2 megohms.







TYPE 105

PRE-SET RESISTORS A wire-wound pre-set resistor for panel or chassis mounting

Export enquiries welcomed



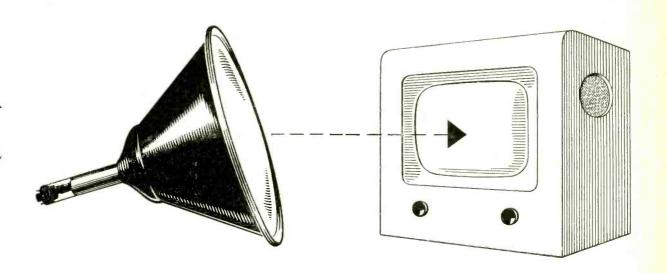
EGEN ELECTRIC LTD., CHARFLEET INDUSTRIAL ESTATE,
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ı	FULLY INTERLEAVED	
ı	SCREENED AND IMPREGNATED. ALL GUARANT ALL PRIMARIES ARE 200/250 v. Half Shrouded.	EED.
1	HSM63 (Midget). Ourput 250-0-250 v. 60 m/a , 6.3 v. at 3 amps.,	
1	5v. at 2 amps	18/-
1	2 amps	18/6
1	MS40. Windings as above. 4 v. at 4 amps., 4v. at 2 amps	18/6
1	Output HS2 250-0-250 v 80 m/a	21/-
	HS2, 250-0-250 v. 80 m/a. HS3, 350-0-350 v. 80 m/a. HS30, 300-0-300 v. 80 m/a HS2X, 250-0-250 v. 100 m/a. HS75, 275-0-275 v. 100 m/a	21/-
1	HS2X. 250-0-250 v. 100 m/a. HS75. 275-0-275 v. 100 m/a	23/ - 23/-
	HS30X. 300-0-300 v, 100 m/a. HS3X. 350-0-350 v, 100 m/a. Fully Shrouded	23/-
	FSM63 (Midget). Output 250-0-250 v. 60 m/a., 6.3 v. at 3 amps.	18/6
1	5 v. 2 amps. Output	10/9
1	FS2. 250-0-250 v. 80 m/a.	23/-
Į	FS30. 300-0-300 v. 80 m/a. FS3. 350-0-350 v. 80 m/a	23/ - 25/9
	FS30X. 300-0-300 v. 100 m/a. FS3X. 350-0-350 v. 100 m/a	25/9
Į	FS2. 250-0-250 v. 80 m/a. FS30. 300-0-300 v. 80 m/a. FS2X. 250-0-250 v. 100 m/a. FS3X. 350-0-350 v. 100 m/a. All the above have 6.3 4-0 v. at 4 amps., 5-4-0 at 2 amps. FS43. Output 425-0-425 v. 200 m/a., 6.3 v. 4 amps., C.T. 5 v. 4 amps. C.T. 5 v. 3 amps. Fully shrouded	
1	4 amps. C.T. 5. v 3 amps. Fully shrouded	51/-
	FS50. Output 450-0-450 v. 250 m/a., 6.3 v. 2 amps., C.T. 6.3. v.	75/-
	4 amps., C.T. 5 v. 3 amps. Fully shrouded. F30X. Output 300-0-300 v. 80 m/a., 6.3 v. 7 amps., 5 v. 2 amps., Framed. Flying leads	•
	Framed. Flying leads	31/9
	4 v. 3 amps., 0-2-6,3 v. 2 amps. Fully shrouded	71/6
ļ	Framed. Hying leads F35 X. Output 350-0-350 v. 250 m/a., 6.3 v. 6 amps., 4 v. 8 amps., 4 v. 3 amps., 0-2-6.3 v. 2 amps. Fully shrouded FS160 X. Output 350-0-350 v. 160 m/a., 6.3 v. 6 amps., 6.3 v. 3 amps., 5 v. 3 amps. Fully shrouded FS43 X. Output 425-0-425 v. 250 m/a., 6.3 v. 6 amps., 6.3 v.	47/6
	3 amps., 5 v. 3 amps. Fully shrouded	4//0
	6 amps., 5 v. 3 amps. Fully shrouded HS6. Output 250-0-250 v. 100 m/a, 6.3 v. 6 amps., C.T. 5 v. 3 amps. For receiver R1355. Half shrouded. HS150. Output 350-0-350 v. 150 m/a, 6.3 v. 3 amps., C.T. 5 v.	69/-
1	HS6. Output 250-0-250 v. 100 m/a., 6.3 v. 6 amps., C.1. 5 v.	29/3
1	HS150. Output 350-0-350 v. 150 m/a., 6.3 v. 3 amps., C.T. 5 v.	
1	3 amps. Half shrouded	30/9
	3 amps. Fully shrouded	32/6
	3 amps. Fully shrouded FS120. Ourput 350-0-350 v. 120 m/a., 6.3 v. 2 amps., C.T. 6.3. v.	33/-
	2. amps., C.T. 5 v. 3 amps. Fully shrouded	
1	3 amps. Fully shrouded	30/9 23/-
	FS150. 350-0-350 v. 150 m/a., 6.3 v. 4 amps., 5 v. 3 amps	34/9
	3 amps. Fully shrouded PRI/I. Output 230 v. at 30 m/a., 6.3 v. at 1.5/2 amps. FSI50. 350-0-350 v. 150 m/a., 6.3 v. 4 amps., 5 v. 3 amps FSI50X. Output 350-0-350 v. at 150 m/a., 6.3 v. at 2 amps., C.T. 6.3 v. at 2 amps., C.T. 5 v. at 3 amps. Fully shrouded	34/9
	The above have inputs of 200/250 v.	34/2
	FILAMENT TRANSFORMERS	
	All 200/250 v. Input	7/4
i	F4. 4 v. at 2 amps., 9/ F6. 6.3 v at 2 amps. F6X. 6.3 v. at 0.3 amps., 6/ F12X. 12 v. at 1 amp	7/6 8/-
į	FU6. 0-2-4-5-6.3 v. at 2 amps., 11/ F12. 12.6 v tapped 6.3 v.	10//
	at 3 amps.	18/6
ļ	F24. 24 v. tapped 12 v. at 3 amps. F29. 0-2-4-5-6.3 v. at 4 amps., 20/9. FUI2. 0-4-6.3 v. at	
	3 amps	19/6
	FU24. 0-12-24 v. at 1 amp. F5. 6.3 v. at 10 amps. or 5 v. at 10 amps. or 12.6 v. at 5 amps. or 10 v. at 5 amps.	
ł	or 10 v. at 5 amps. F6/4. Four windings at 6.3 v. tapped 5 v. at 5 amps. each, giving	37/9
١	by suitable series and parallel connections up to 6.3 v. at	
	20 amps	57/- 23/6
,	20 amps. F30. 30 v. at 4 amps., 40/ F31. 0.4-6.3 v. at 4 amps. F25. 25 v. at 4 amps., 40/ F26. Two windings 6.3 v. at	
į	l amp.	11/-
	1 amp. F.27. Two windings 12 v. at 1.5 amp. F.28. Two windings 5. v at 3 amps., 25/ F32. 10 v. at 5 amps. F33. 0.10.30-60-100 v. at 1 amp. F34. 0.4-9-15-24 v. at 3 amps., 31/6. F35. 6.3 v. at 6 amps F36. 0.9-30 v. at 3 amps., 30/ F37. 0.9-15 v. at 3 amps. F38. 0.9-15 v. at 1.5 amps., 24/ F39. 0.9-15 v. at 6 amps F40. 0.12-18-24 v. at 4 amps., 42/6. F41. 6.3 v. at 1.5 amps	30/-
	F33. 0-10-30-60-100 v, at 1 amp	45/- 25/-
	F36. 0-9-30 v. at 3 amps., 30/ F37. 0-9-15 v. at 6 amps	26/-
	F38. 0-9-15 v. at 1.5 amps., 24/ F39. 0-9-15 v. at 6 amps	32/6 8/6
	OUTPUT TRANSFORMERS	0/0
	MOPI. Ratios. 26, 46, 56, 66, 90, 120-1 50 m/a. max. current.	
	MOPI. Ratios, 26, 46, 56, 66, 90, 120-1 50 m/a. max. current, C.T. for Q.P.P. Class B, etc. Secondary 2/4 ohms. Top panel	
		19/9
	oP10. (0)15 watts output. 20 ratios on Full and Half primary OP30. 30 watts output, 20 ratios on Full and Half primary Williamson's O.P. Transformer to Author's specification 6 Chokes for Williamson's Amplifier. 30H. at 20 m/a	28/6
	Williamson's O.P. Transformer to Author's specification £	4/13/6
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	REDUCTION OF 1/6 IN THE £ ON ALL ITEMS	
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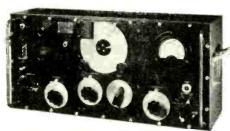
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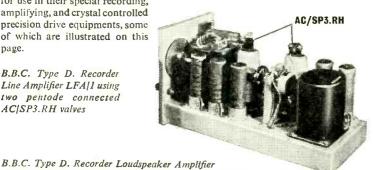
The Ediswan Mazda AC/SP3.RH is an indirectly heated Pentode with a special heater construction designed to reduce hum due to A.C. fields within the valve. Its high working slope makes it very suitable for use in audio frequency stages employing negative feed back.

The high-slope short grid-base characteristic renders it suitable also as an harmonic generator and as an oscillator in high stability crystal drive equipment. Provided precautions are taken to minimise hum due to external wiring the AC/SP3.RH may also be successfully employed in the early stages of amplifiers where the reduction of hum, noise and microphony is of primary importance.

Many of these valves have been supplied to the British Broadcasting Corporation

for use in their special recording, amplifying, and crystal controlled precision drive equipments, some of which are illustrated on this page.

B.B.C. Type D. Recorder Line Amplifier LFA/1 using two pentode connected AC|SP3.RH valves



LSM/7 using three pentode connected AC|SP3.RH valves



AC/SP3.RH

RATING Heater Voltage

BASE British 7 pin

Pin No. 1 Metallising

Pin No. 2 Anode

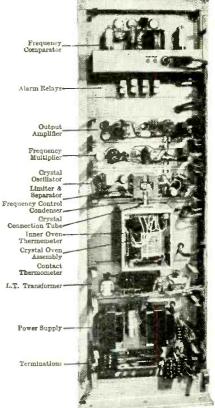
Pin No. 4 Heater

Heater Current (Amps) .

Maximum Anode Voltage Maximum Screen Voltage

Mutual Conductance (mA/V)

Pin No. 3 Suppressor Grid (G3)



B.B.C. Crystal Drive Equipment (Type CP-17E) using nine ACISP3.RH valves in the crystal maintaining amplifier, frequency divider, frequency multiplier and oven temperature relay.

Pin No. 5 Heater

Pin No. 6 Cathode

Pin No. 7 Screen (G2)

Top Cap Control Grid (G1)



	I TPICAL UPERA	IING	COMPLET	NM2	
	Anode Voltage (Va)	250	250	250	250
	Screen Voltage (Vg2)	80	100	160	200
	Grid Bias (Vgl)	1.2	5 1.7	2.75	3.5
	Anode Current (mA)	7.8	7.9	10.5	12.3
Screen Current (mA)		2.4	5 2.5	3.3	3.85
Mutual Conductance (mA/V)		7.0	7.0	7.45	7.6
	Anode AC Resistance (ra) (Meg ohms)	0.5	5 0.55	0.4	0.3
	Input Capacity (Hot) (μμF)	20	19.9	19.7	19.5

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40

1.0 250

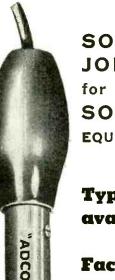
250

7.7

Standard model 3, bit (illustrated)

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CODE

1	10.071	0.D.	TYPE	NO.
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		fits on GD.071 CD.071 VD.071	Elbow plug adaptor	LD.071
		fits on GD.071 LD.071	Bulkhead (Junction) adaptor	VD.071
0	3	fits on GD.071 LD.071	Chassis receptacle	CD.071

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given by the

NATIONAL FEDERATION OF GRAMOPHONE SOCIETIES*

on

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the Mark I model, with a firmer, smoother middle
the Mark I model, with a firmer, smoother middle
register and lower fundamental resonance (nominally
register and lower fundamental resonance (nominally
register and lower fundamental resonance (nominally
register and lowes the speaker
35 c.p.s.). It was not possible to house the speaker
in the cabinet designed for the purpose by Messrs.
in the cabinet designed for the purpose by Messrs.
in the cabinet designed for the purpose by Messrs
in the cabinet designed from the back of the cone
virtually all the sound from the back of the cone
were hard, clear bass, very even response in the
middle and upper registers and low needle hiss of
middle and upper registers and low needle hiss of
middle and upper registers and low needle hiss of
middle and upper registers and low needle hiss of
middle and upper registers and low needle hiss of
middle and upper registers and low needle hiss of
middle and upper registers. It will handle up
every satisfaction to Societies. It will handle up
to 15 watts.
The main difference between the Models 101 and 102

every satisfaction to Societies. It will nevery satisfaction to Societies. It will nevery satisfaction to Societies. It will nevery satisfaction to Societies. It will never be to 10 and 102 to 15 watts.

The main difference between the Models 101 and 102 is the increased sensitivity and flux density of the is the increased sensitivity and flux density of the is the increased price by improved damping and increased price by improved damping and increased price. These are undoubtedly the best 8" units which we have so far tested, and the maker's claim for response have so far tested, and the maker's claim for response have so far tested, and the maker's claim for response have so far tested, and the maker's claim for response have so far tested, and the maker's claim for response have so far tested, and the maker's claim for response have so far tested, and the maker's claim for response with the few wider and in parallel with the Axiom 150 to secure wider 101 in parallel. In the latter case there was units in parallel. In the latter case there was units in parallel. In the latter case there was rather less weight in the extreme bass. rather less weight in the extreme bass. rather less weight in the extreme by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source so be secured by using an 8" and wide sound source so be secured by using an 8" and wide sound source so be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source can be secured by using an 8" and wide sound source con be secured by using an 8" and wide sound source con be secured by using an 8" and wide sound source con be



AXIOM ISO Mk. II £13. 11 5 (Incl. purchase tax)



£19.8.4 (incl. purchase tax)



£6, 12. I (incl. purchase tax)

AXIOM 102 £9, 18, 2 (incl. purchase tax)

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 Picture lipagity better than 5% 1 (Some commercial receivers are
- Picture linearity better than 5%! (Some commercial receivers are passed at 15%).
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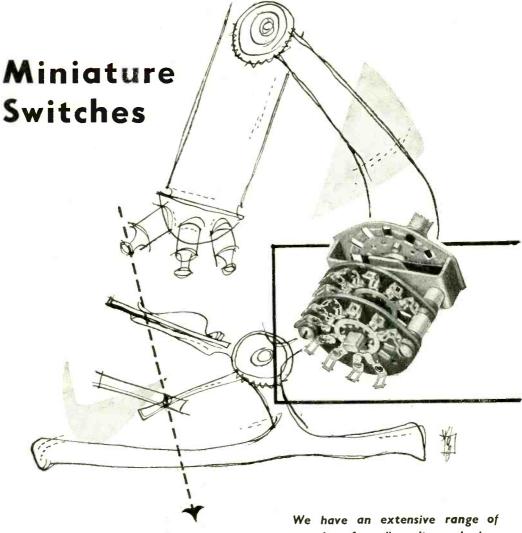
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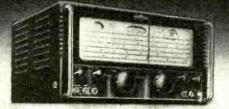


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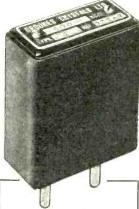
- Three very high grade motors designed and made for the job, by the Verdik engineers.
- Even better heads.
- Positive braking on all functions.
- Fast forward run and rewind in 50 secs. WITHOUT UNLACING TAPE.
- Very simple to use. Only two controls. One for rewind and one ON-OFF switch.

No Tape Table of this grade has ever been offered to the public at anything like the price and it is fully guaranteed.

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Type " 5 " Type "S"
Frequency range: 100 Kc/s to
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Quartz crystal plate of appropriate cut and dimensions to
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1/4 in. high, 1/4 in. wide, 1/4 in.
thick, with two 1/4 in. diameter
pins 1/4 in. apart. Frequency
tolerance 0.01% of nominal at
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applications. Frequency-temperature co-efficient better than

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For the measurement of the Q of a circuit, there are

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frequency range 50 kc/s to 50 Mc/s. In addition to direct Q readings,

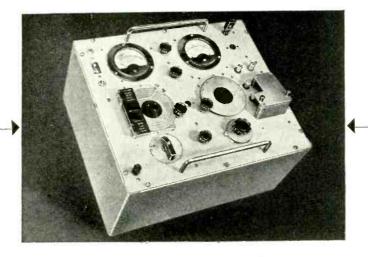
the TF 329G can be used for a considerable range of

indirect measurements carried out by the normal resonance methods.

These include inductance of coils, capacitance and phase defect of condensers,

the characteristics of transmission lines. Special jigs

are available for investigating dielectric losses.



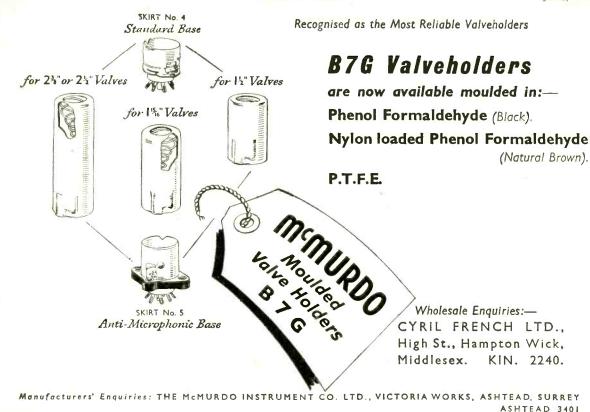
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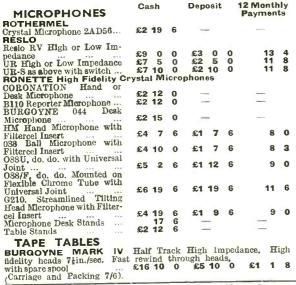
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We carry extensive stocks of all accessories and detail below a selection of these. Pay us a visit-it will be worth while, and you will be able to see and hear the remarkable Burgoyne Recorder, at only £33.12.0.



				Recor				6	
TAPE TABLES (cont)	Cash I			Dep	osit		12 Monthly Payments		
LANE MARK IV do. do TRUVOX 2 speed. Push Button Control. 3 Motor	£17	10	0	£6	10	0	£1		
Drive, Half Track, Low Impedance Heads (Carriage and Packing 10/-).	£23	2	0	£7	14	0	£1	9	0
CABINETS									
A suitable Cabinet for Transp Recorder, 21 in. x 13 in. x 12 i	portal n. £4	10	ecc 0	order, £1	as u	sed 0	in Bu	1g0)	ne 4
AMPLIFIERS	1.00					4.0		-1-4	
BURGOYNE 5 Valve Reco	£11	15	O O	£3	118	0	, com	16	5
COMPLETE RECOR	DER	lS							
BURGOYNE Dual Track Transportable Recorder	£33	12	0	£11	4	0	€2	2	9
(Carriage and Packing 21/-). GRUNDIG Reporter, 2-spd. (See illustration).	£84	0	0	£28	0	0	£5	7	0
GRUNDIG Console, 2-spd.	£99	15	0	£33	5	0	£6	7	0
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s. q. BROWN. Type A, adjustable Reed Movements. q. BROWN. Type F,	£4	5	0	£1	5	0		8	0
Featherweight General Pur-									
s. G. BROWN. Type K,	#1	15	0	_	_		_	_	
Moving Coil for High Fidelity		10	0	£1	10	0		10	0
	HE/	IDS						Cach	

The Grundia

TAPES		Cash		TAPES (cont)	C	ash		HEADS		Cash	
BURGOYNE 1,200ft, High		15		GEC 1,200ft. Medium Coer- civity	£1	10	0	ance, half track width, built in tape guides, fully enclosed,			
BURGOYNE 600ft. High Coercivity (Specially imported for high	£1	1	0	eivity AGFA 600ft. High Coercivity Tape Spools 1,200ft.	£1 £1	17 2 4	6	single hole fixing. Record Playback or Erase TAMSA high impedance, half	£1	17	6
emi 600ft. High or Low	£1	1	0	Tape Spools 600ft. B.S.R. Type FP.10 Clock or Anticlock-wise. 1,400 r.p.m.		3	6	track width, Record/Play- back, Playback or Erase Series 100	£2	7	6
EMI 1,200ft. High or Low Coercivity	£1	15	0	MOTORS				OSCILLATORS			
FERROGRAPH 1,200ft.	£2	5	0	4 pole 3in./03 Torque B.S.R. Type SR.1, 2,750	£1			BURGOYNE Oscillator Unit, complete with 6V6 Valve	£2	2	0
B.A.S.F. MAGNETO- PHON 1,200ft. High Coerc- ivity	€2	0	0	r.p.m. 2 pole 3in./03 Torque B.S.R. Type SR.2, 2,750 r.p.m. 2 pole 2in./03 Torque	£1			LANE Oscillator Unit, com- plete with 6V6 Valve	£3	10	0
SCOTCH BOY 600ft. Medium Coercivity	£1	1	0	COLLARO Clock or Anti- clockwise. (Inc. cooling fan),				for high impedance heads TAMSA Oscillator Coil for		8	6
Medium Coercivity 1,200ft.	£1	15	0	1,400 r.p.m. 4 pole 4in./03 Torque	£1	18	6	high impedance heads WEARITE 579 Oscillator or		10	
SOUND MIRROR 1,200ft. Paper Tape	£1	5	0	*Post and packing extra when	e not	shoe	vn.	Bias Transformer		7	6

TONE CONTROL UNIT MODEL A.7/8 THE NEW BURGOYNE AMPLIFIER AND

In response to widespread demand we have decided to introduce an entirely new Amplifier equipment, capable of a high standard of performance, at the extremely low figure of £9.19s.6d. complete. This low price is made possible by the increased production now available from our factory.

The Amplifier is built as two units :-

1. THE TONE CONTROL AND PREAMPLIFIER section consists of a pentode and triode valve and is capable of fully loading the main Amplifier when used with the current high fidelity, low output type of pick-up. A wide range of bass and treble control is available; approximately 20 DB cut and lift at each end of the scale. A three position input switch is incorporated:—RADIO-78-33/45. Each position brings into use the correct compensation for the particular input, with special attention to the rising frequency characteristic of LP records.

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At one time we were leading Government Surplus Stockiess—a fact which will be to your advantage if you call at our Showrooms. We have left miscellaneous quantities of surplus electronic equipment, in very great variety and this wil. be offered at unheard of and unrepeatable Bargain Prices for a limited period. Do not fail to pay us a visit. A showroom is being altotted to the display of this material which can be inspected at your leisure.

2. THE MAIN AMPLIFIER consists of a 6J7 pentode feeding a 6V6 output valve. In view of the large signal obtained from the preamplifier, considerable overall negative feed-back is permissible and the quality achieved sets an entirely new standard for inexpensive

and the quality achieved sets an entirely new standard for mexpensive equipment.

The division of this 5 valve Amplifier into two units permits the small and comparatively light preamplifier unit to be mounted in an easily accessible position, i.e., on the top board of the cablnet, and an engraved indicator panel is included in order that a smart appearance may be achieved. The main Amplifier, which includes power pack, may then stand in the bottom of the cabinet, thus simplifying any installation problems to a considerable degree.

The complete equipment may be heard at our showroom and we suggest that you bring along a favourite record and judge it for yourself. You will hear the sort of reproduction associated normally with 25-30 guinea equipment, and we feel quite confident that you will be amazed at the fidelity and "punch" of such a modestly priced outfit.

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'Scotch Boy' fits all makes of tape recorders. It brings new clarity, new fidelity, an all-round improvement to your own recordings.

'Scotch Boy' is a medium coercivity, plasticbacked tape with a frequency range of 50 c/s to 10 kc/s at a tape speed of 7½" per second. It is available in six reel sizes from 300 ft. to 1,000 metres, to provide a wide range of playing times.

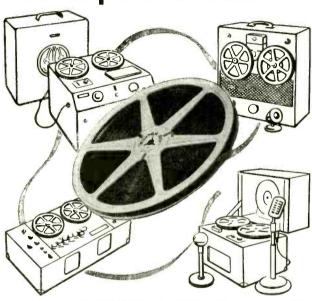
'Scotch Boy' is used by the B.B.C. and most other big recording and broadcasting corporations. Ask your dealer for 'Scotch Boy' and hear the difference it makes on your own machine.



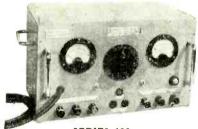
Product

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gets the best out of **ALL** makes of tape-recorder



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SERIES 100

DC Output, Stabilised, 200-350V 120mA, continuously variable.

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Bench Model as illustrated £58. Rack Mounting Model

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Available with negative bias supply at £63 and £64. Power Supply Units and other special electronic equipment made to customers' specifications.

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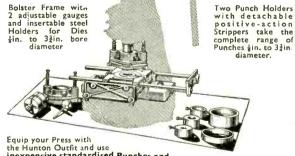
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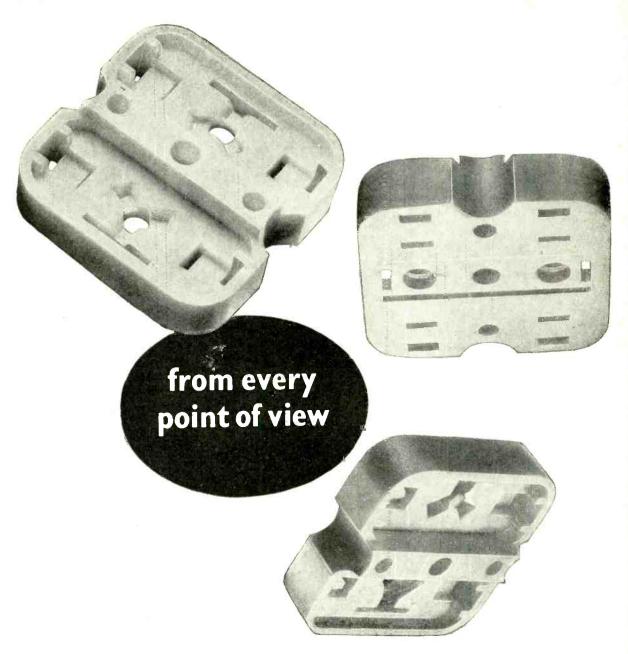
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BRIGHT SPOT-AND-HAIRLINE INDICATOR.

This instrument introduces a completely new conception of electrostatic voltmeter. It is compact,

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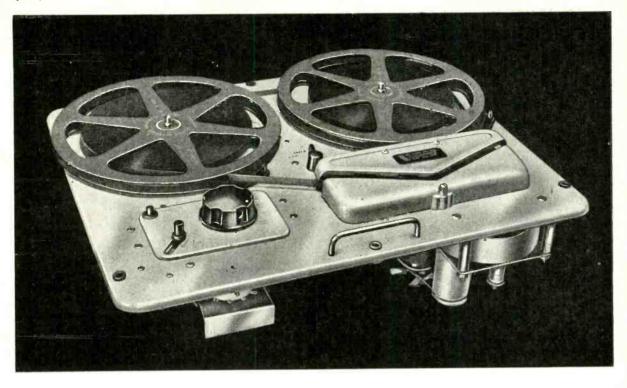
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MEDIUM Standard 4" plastic or paper based coated tape. TRACK WIDTH O.1"

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REWIND TIME (AND RAPID WIND-ON) Less than

ATTAINABLE FREQUENCY RESPONSE ± 3 DB 50-12,000 c.p.s. at $7\frac{1}{2}$ " per sec. 50-6000 c.p.s. at $3\frac{3}{4}$ " per sec.

(Tape to Spec. WW372/49) "WOW" AND FLUTTER Less than 0.2%.

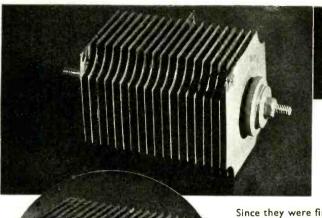
LONGTERM SPEED STABILITY Better than 0.5%.

POWER CONSUMPTION 57 watts.

DIMENSIONS 163" x 13" x 1" above deck and 6" max. below WEIGHT 18 lbs.

* "Tape-Deck" is registered Trade Mark No. 684413 granted in 1949. The Manual of the Tape Deck-price 2/6can be obtained from your local dealer or direct if difficulty is experienced. The Manual contains a technical description of the "Tape-Deck" and suggests a tried and proven circuit for its best usage.

LTD WRIGHT & WEAIRE



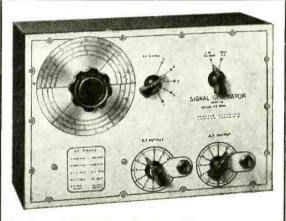
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SIGNAL GENERATOR TYPE 10. 100 Kc/s-100 Mc/s Price £7. 10. 0

The accuracy, reliability and comprehensive specification, are some of the reasons why the $\it TYPE$ 10 has achieved such outstanding success.

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100 Kc/s to 100 Mc/s Modulated or unmodulated carrier Direct
calibration Adjustable 400 c.p.s., AF signal Stable RF oscillator
Large, easily read scale AC mains operation.

New instruments now available include the HOMELAB CHECKTEST price 37/6d. and a range of accurately calibrated variable condensers, 100pf, 500pf, and 1000pf, price 42/- each.

100pf, 500pf, and 1000pf, price 42/- each.

Obtainable only direct from the manufacturers. Send for full technical details or call at address below.

Overseas enquiries invited.

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Dear Mr. Briggs,

Letter from America

Central Research Station,

The Super 8 (CS) AL arrived last week, and I have given week and I have given a small arrived last week, and I have given the last second will be the small and the last of th

and the W.10/CS.

Single speaker, the Super 12/CS/AL base against as ingle speaker, the performance against as most interest as another outstanding triple corner chamber aroused a most the outstanding triple corner chamber aroused to the triple corner chamber the corner than the outstanding triple corner chamber aroused to the triple corner chamber than the corner

Mr. Hrikes, and I have given the Bure of the super given to acknowledge its receipt.
The Super given before writing to acknowledge its receipt.
Athorough

1st April, 1953.

Letter from N. Rhodesia

West 110th Street. New York U.S.A 21st March, 1953.

Dear Mr. Briggs,

Dear Mr. Briggs,

Upon acquiring HiFi equipment recently I found the speaker I had thought suitable was far from it. While pondering housed in a 20 × 20 × 16in. cabinet on the floor close by my A Super 12/CS/AL Wharfedale. The salesman assured me it reflex about 6 cu. ft. I settled for it with no hesitation whatever. As we have been a scant 6 or 7 weeks from leaving your works to getting into my hands, which for some obscure reason pleased

gering into my names, which for some obscure reason present me greatly.

Scarcely a day has passed but this speaker has amazed me. In your book "Loudspeakers" (which I have read and re-read speaker sorts out the instruments. By saying this you do not speaker sorts out the instruments. By saying this you do not program source, is completely 3rd dimensional. To me it is pricked up on one's receiving set the instruments are set forth object of you as though you, the listener, were standing at the will gather from this that the Super 12in. gives me immense could do this. Incidentally, I am receiving on FM only. Once indication, in fact I would never have dreamed that a speaker in a while I have turned the volume fairly high. On Wash-Stripes conducted by, of all people, Toscamin. On such an occasion as this one thinks any neighbour who objects can go gloriously.

(Signed) L. I.

(Signed) L. J.

The share the outstanding feature. The constraint of the control o **WHARFEDALE SPEAKERS**

(Signed) C.A.W.

Super 5 Diameter 5in. Flux density 13,000 lines.

£6/13/3, inc. P.T.

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W15/CS

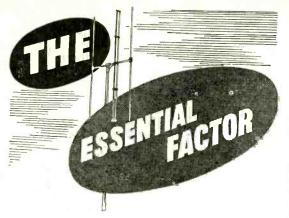
Diameter 15in. Flux density 13,500 lines.

£16.



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It is the aerial which provides the vital link between transmitted waves and the receiver. Its efficiency in terms of maximum forward gain, high front/back ratio, broad bandwidth, and accurate matching governs the picture strength, quality and freedom from interference. That is why it is wise to specify Aerialite aerials-designed and manufactured by an organisation with 21 years specialisation in this field. Some of the television aerials in the Aerialite comprehensive range are :-



The AERFRINGE Models are three element fringe types which have a folded dipole construction for extra broad bandwidth and high definition.

The Model 63A (Illustrated) has a forward gain of 8.0 dB which ensures excellent reception even in difficult and distant areas. Retail price: £13/5/- complete with 2in. x 10ft. light alloy mast, double chimney lashing brackets, etc.





The AERBEAM Model is a four element folded the AERBEATI Plode is a four element folded dipole aerial with an extra high forward gain of 11 dB and a very narrow beam. It is suitable for outer fringe areas and is available for channels 3, 4 and 5 on vertical polarisation and channels I and 5 on horizontal polarisation. Retail price: £13/5/- complete with 10ft. mast, double chimney lashing hrackets are lashing brackets, etc.





The DUBLEX range was first introduced at the 1952 National Radio Show and has proved its 1952 National Radio Show and has proved its value as an inexpensive yet high gain aerial with excellent interference rejection properties. The novel double folded element construction gives a forward gain of 6.0 dB with a max/min ratio of 25 dB. Retail price: 775 with 7ft, mast etc., £4/8/6. 77T with 10ft. x 2in. o.d. mast, double lashings £7/15/-. 77X array only £2/15/-. For horizontal polarisation retail prices are 10. For horizontal polarisation retail prices are 10 extra on above.



For Belfast and Newcastle Transmitters. The majority of Aerialite T/V aerials are suitable for horizontal polarisation and provide same high level of aerial efficiency. Please add the suffix HOR to the model number when ordering.



Specify and use Aerial te R.F. Cables for T/V Aerial Installations.

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"EXCEL" TAPE RECORDERS MAGNETIC

Used as a first class recorder for high fidelity work; also employed with EXCEL Synchroniser Unit for high quality synchronised sound with sub-standard film proiectors. Standard full track; also half track to order.

- WIDE FREQUENCY RESPONSE
- FREEDOM FROM " WOW " AND FLUTTER 101 in. DIAMETER FLYWHEEL
- SUPERIMPOSING
- NOISE SUPPRESSION
 TAPE CAPACITY: Standard 3250 ft. single sided spools and NAB 2400 ft. double sided spools.
- PORTABLE, WIDTH 142in. DEPTH 174in. HEIGHT 84in.

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COILPACKS. Now at new lower prices! A full range is available for Superhet and T.R.F. Mains or Battery. Size only 1½in. high x 3½in, wide x 2½in, Ideal for the reliable construction of new sets, also for conversion of the 21 RECEIVER, TR 1196, TYPE 18, WARTIME UTILITY and others. Aligned and tested, with 6th significant. with full circuirs, etc. Fully descriptive leaflets available.





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H.F. CHOKE Type Q.C.1.

Frequency coverage 150 kc/s. to 20 m/c. Iron-dust core and single-screw fixing. Prototype tested and ap-

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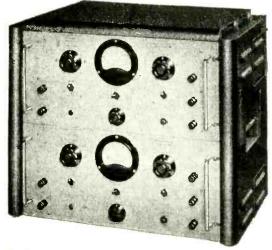
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Tape speeds 7½" and 15" per second, or 3¾" and 1¾" per second.

Synchronous drive motor.

Remote operation or foot control.

Automatic back spacing and reverse drive for dictation purposes.

Cassette tape loading.

Rack mounted assembly.

TAPE SPEEDS 7½" and 3¾" per second.

TRACKS 1" wide. Number of tracks 2.

PLAYING TIME 30 minutes at 7½" per second. 60 minutes at 3¾" per second.

Standard 7" and 5" plastic or metal.

SENSE OF From left to right with tape coating inwards.

REWIND TIME One minute for 1,200 ft. of tape (approx.).

R.F. erase head. Record/ playback head off-set for recording on upper track.

playback head off-set for recording on upper track. Provision on player unit for additional monitoring head for special applications.

TAPE OPERATION

SPOOLS

HEADS

Single control provides:— Record, Playback, Fast Forward, Cueing, Rewind.

ward, Cueing, Rewind.

To ensure additional safety against accidental erase, an additional record / playback switch is provided on the amplifier assembly. Power and brake operation is by means of a relay which will enable remote operation to be provided in special applications.

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At 7½" per second 60-10,000 C.P.S. plus or minus 3 db. At 3¾" per second 70-7,000 C.P.S. plus or minus 3 db.

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3 // C	,,	**	1/7	3 6 1 4 3 8 1 2 5 8 3 4 7 8 , , ,	, ,,	1/6	구 CH NP 로 RH SC	1/-
5 "	,,	,,	1/7	3"		1/7	I' CS CP	1/-
3"	,,	,,	1/9	1//		1/9	a" RH SC	1/2
7/	11	,	1/10	<u>\$</u> "		1/11	TATE OF THE SECOND TO SECOND THE	1/1
1 "	,,	**	1/11	3"	, ,,	2/-	<u>1</u> "	1/2
9 "	.,	. ,,	2/-	7"	SC	2/1	آج RH SC	1/2
9 "	,,	SC	1/11	Ĭ″,	, NP	2/3	₹" CS CP	1/4
5"	,,	NP	2/1	3 " C	S SC	1/4	3"	1/5
3"	,,	**	2/3	5 //	, NP	1/6	बै" RH SC	1/5
1"	,,	,,	2/6	1/2 1	, ,,	1/7	I" CS CP	1/7
1" ln	ist		1/9	16	1 19	1/8	I" CH ,,	1/9
32 "	29	NP	1/9	5"		1/9	1 7 // H/H	2/6
32 / C	S	9.6	2/-	3 " C 16 " 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1/10	17/ H/H	2/9

4BA		BRASS	STEEL	
₹" CH SC	2/-	¼" RH NP	1/10 ½" CS CP	1/2
¼″ ,, N	IP 2/1	1/2 21 22	2/3 3/8 ,, ,,	1/3
9 " 32" " "	2/1	3",,,,,	2/9 흫" RH ,,	1/4
16 22 22		7" "	$3/-\frac{1}{4}''$,, SC	1/2
1 11 11		¼″ CS ,,	$1/8 \frac{1}{2}''$,, ,,	1/4
7"	3/3	2" ", ",	$2/-\frac{1}{2}''$ CS CP	1/4
흫"Hex/H ,,	2/6	§ 11 11	2/3 3" RH SC	1/6
3"	3/6	3" B 22 21	1/10 7/ ,, CP	1/9

2BA	BRASS	STEEL	
· RH NP	2/10 &" CH NP		1/9
4" ,, ,,	$\frac{3}{4}$,, SC	3/- ½" LgeRH	2/-
3" "	3/3 1" ,, ,,		2/-
7 " 11 11	3/6 I콤" ,, NP	6/- I" CH	2/6
1" ,, ,,	5/- \frac{5''}{8} CS ,,	4/- 1\frac{1}{2}" RH CP	2/9
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8BA			BRASS		STEEL	
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1/2 ,,	9 9	2/6	表" RH NP	2/2	3 CS ,,	2/-
₫" CS	,,	1/8	9 //	2/6	ਜੁੱ CH "	2/2
를" CH	,,	2/3	3"	2/9	375" RH ,,	2/2
5" CS	,,	1/9	ਭੂ" Hex ,,	2/9	L' CH NP	2/3
3"	11	2/6	7"	2/10	¾″ RH CP	2/3
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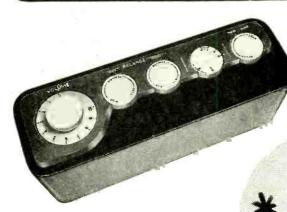




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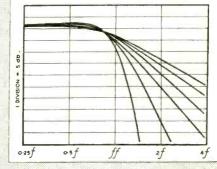
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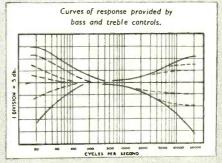
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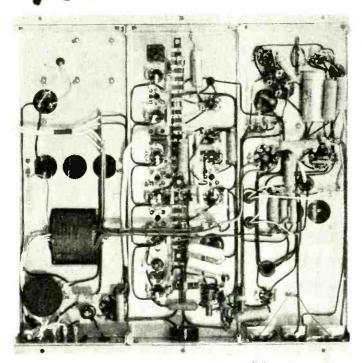
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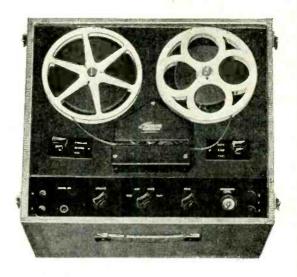
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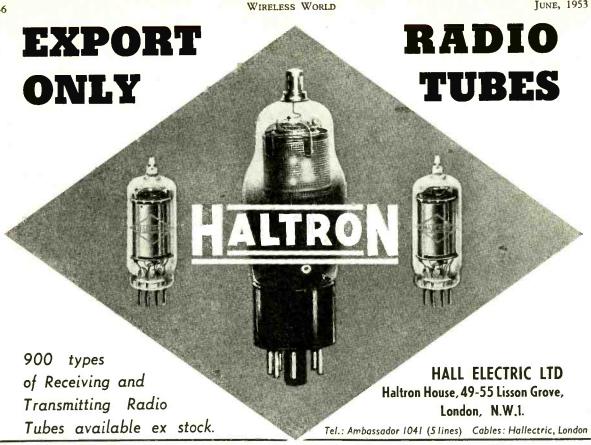
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60+100	350	400	450	41"	13"	L33	K178	18/6
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64+120	350	400	450	41/2	13"	L35	K503	19/6
						The same of the sa		

TYPES L.32 and L.33 EXTERNAL CLIP MOUNTING

Dimensions

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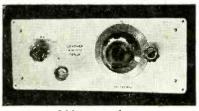
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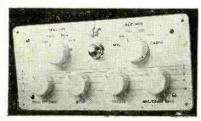
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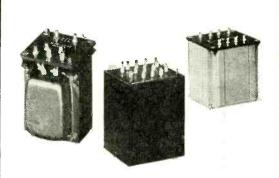
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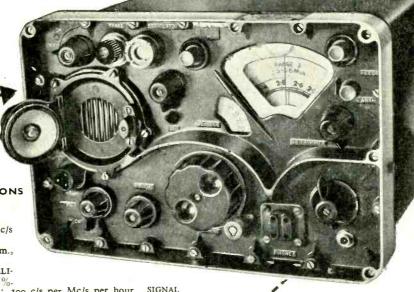
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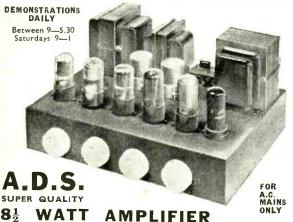
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SEND 1.6 FOR EASY TO FOLLOW POINT-TO-PC 3/9 Cabinet, Bakelite, in Walnut or Ivory or Wooden 1/6/20 | Nature of Ivory or Wooden 1/6/20 | Packing and Insurance | 17/6 | Packing and Insurance | 18/6 | SEND 1/6 FOR EASY TO FOLLOW POINT-TO-POINT DIAGRAMS AND CIRCUIT DIAGRAM which shows how YOU can build the Receiver Insustrated above YOU can build the Receiver Insustrated above YOU can build the Receiver Insustrated above 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1/6 | 1

APT4-Output, and APTI—Output, and Metal Rectifior. Waveband coverage is for the medium and long bands. Choice of 3 Cabinets: Bake lite in Walnut or Ivory, or Wooden (Walnut finish).

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short. CONTROLS: Tuning.

short. CONTROLS: Tuning.

on/off Gram. Position on Switch. Pick-up and Extension

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A.C. mains. DIMENSIONS: Length 14jim., height

11jim., width 6jim. Distance between controls, left to

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67,19.6

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LINE-UP: TP25, VP23,
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Position on Switch. Pick-up and Extension Speaker
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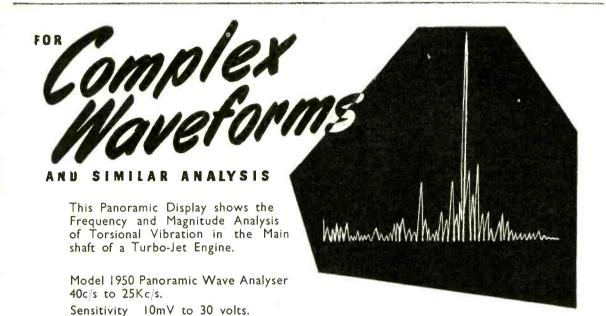
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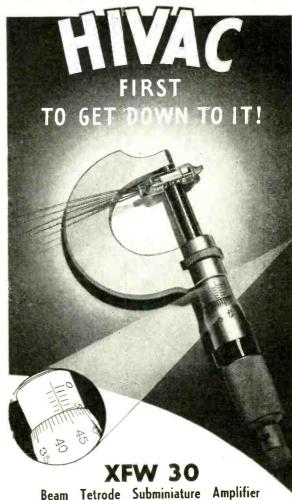


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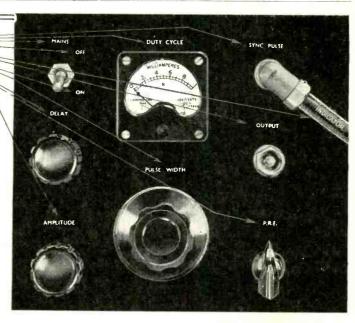
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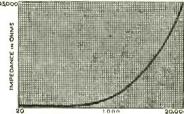
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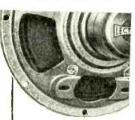
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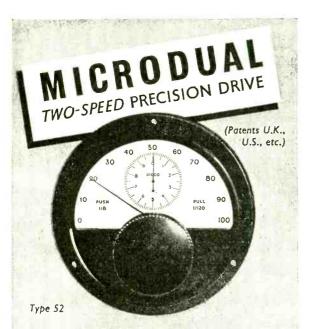
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43rd YEAR OF PUBLICATION

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La Lilentia de la cidona June 1953

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PUBLISHED MONTHLY (last Tuesday of preceding month) by ILIFFE & SONS LTD., Dorset House, Stanford Street, London, S.E.1. Telephone: Waterloo 3333 (60 lines). Telegrams: "Ethaworld, Sedist, London." Annual Subscription: Home and Overseas, £1 7s. 0d. U.S.A. \$4.50. Canada \$4.00. BRANCH OFFICES: Birmingham: King Edward House, New Street, 2. Coventry: 8-10, Corporation Street, Glasgow: 26B. Renfield Street, C.2. Manchester: 260, Deansgate, 3.

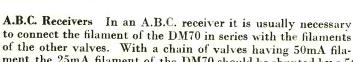


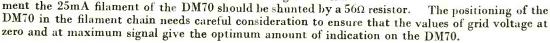
VALVES, TUBES & CIRCUITS

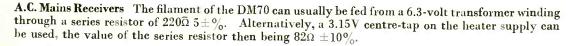
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APPLICATION IN VARIOUS TYPES OF RECEIVERS

Battery Receivers Those receivers provided with a 90-volt battery operate with an h.t. of about 85V after deducting the negative grid bias required for the output valve. In such a receiver a DM70 connected with pin 4 earthed has a cut-off voltage of -10V, which is adequate to indicate the strongest signal likely to be encountered. Similarly for a 67.5V battery, the h.t. is of the order of 60V giving a cut-off voltage of -7V when connected with pin 5 earthed.







It is not recommended that the filament of the DM70 be fed with a direct current from the cathode resistor of the output valve owing to the possibility of wide variations in this current resulting in reduced life of the indicator.

The recommended anode voltage for the DM70 in mains receivers is 60V, which can be obtained from the h.t. line by means of a series resistor. This results in a sliding anode voltage dependent upon the current of the valve and so extends the range of grid control to deal adequately with strong signals in a very sensitive receiver.

As the filament is supplied with an alternating voltage it is necessary to take precautions to prevent hum being introduced into the a.g.c. circuit from the grid of the DM70.

A.C./D.C. Receivers The filament of the DM70 shunted by a suitable resistor may be connected in series with the heaters of the other valves in an A.C./D.C. receiver provided a surge current limiting device is also included in the series circuit. For mains voltages above 160V the shunt resistor should be $180 \pm 10\%$ when included in a 100mA heater chain.



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MWV 230

Wireless World

JUNE 1953

VOL. LIX No. 6

Exhibitions

T would be ungracious—and indeed, foolish— to complain that too much limelight is thrown on our art. All the same, the very large number of exhibitions concerned with radio and electronics are something of an embarrassment to many people, including visitors and exhibitors as well. Although almost all the exhibitions with which we are concerned nowadays are in fact, if not in name, specialized, there is a good deal of overlapping between them. Manufacturers, naturally enough, want to show their products to the largest number of potential users, who, in their turn, want to see what is available to them. But is it possible to avoid the present duplication of effort and to reduce the expenditure of manhours and money by both exhibitors and visitors?

An exhibition organized by the Radio Communication and Electronic Association, with collaboration of the Ministry of Supply, was held recently at Farnborough for the benefit of delegates from the European Defence Community, N.A.T.O. and the British Commonwealth. It was supported by firms in the components and valve sections of the radio industry, and though outwardly of a military character, did in fact cover a much wider field. With some justification this was claimed to be "the most comprehensive display of electronic equipment held anywhere in the world." The pity of it is that this impressive show, which presented the "professional" side of the industry as it has never been presented before, was seen by a mere handful of visitors.

The success of the Farnborough show gives rise to the thought that, for purposes of exhibitions, all radio could be divided into two sections, which might very roughly be described as professional and domestic. The first category would include all products for communication, industrial, commercial and military applications. The domestic show would, of course, deal predominantly with broadcast receiving equipment, but might also cover electronic equipment intended to some extent at least for the general public, including perhaps "business radio." The advantage would be that annual exhibitions organized in this way would provide a focal point of the year

for developments in the main spheres of activity. Such a scheme might not entirely avoid the need for specialized exhibitions, but would at least allow them to be still more specialized, and thus obviate much of the wasteful overlapping that now occurs.

Television Conversion

A LETTER from a correspondent, printed elsewhere in this issue, expresses the view that the problems involved in designing converters for adapting existing television receivers for reception of the proposed alternative service are rather more difficult than is commonly believed. No doubt, certain types of set, operated in favourable conditions, could be fairly simply adapted, but it does seem most unlikely that a standardized design of converter, applicable to all sets in all conditions, could be produced at low cost.

The tunable receiver having channel selection under the control of the user will lend itself more readily to conversion to the new band, and so it is to be expected that this type of set will become increasingly popular when the start of the alternative service becomes imminent.

An allied problem that has not yet been touched upon at any length is that of aerials for two-band reception. That is one of the many matters connected with the proposed alternative television service that we hope to discuss in detail in the near future.

Local Conditions

THE task of the B.B.C. in providing an acceptable medium-wave signal for the whole country is not an enviable one, and becomes more difficult as time goes on. To an increasing extent, compromises are necessary. Critics of B.B.C. quality are inclined to overlook the fact that a transmitting technique that satisfies the listener who lives, figuratively speaking, on the doorstep of a station is quite unacceptable to those in the wilds. The only way out of this difficulty lies in the use of v.h.f.

Components and Techniques

Survey of the R.E.C.M.F. and Physical Society's Exhibitions

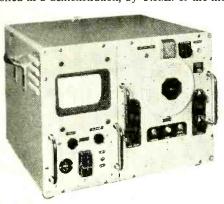
Since the above two exhibitions ran more or less concurrently in London this year and also overlapped to some extent in their types of exhibits, we have selected the most interesting items from both shows and combined them into this one report. No distinction is made between Physical Society exhibits and R.E.C.M.F. exhibits, but each section dealing with components is followed by a list of the exhibitors in that class.

RESEARCH AND MATERIALS

The problems of noise measurement in fractional-ohm resistors at temperatures of the order of 20 deg K (-253deg C) are formidable and offer an interesting challenge to the amplifier designer. These have been successfully solved in an amplifier designed by P. J. Baxandall at the Telecommunications Research Establishment. Two input transformers are used, the first operating at low temperature and stepping up to 300 in order that the leads to the refrigerant container shall be thin enough to avoid too much loss by heat conduction; the second transformer provides an impedance of $1\,\mathrm{M}\Omega$ at 4,000 c/s. In designing the first transformer it was found that at 20 deg K the permeability of Mumetal falls to a third of its normal value, but the shunt eddy-current losses are not appreciably effective. At the level of the noise to be measured microphony in the input transformers is a serious factor, and anti-vibration mounting is necessary. In order to reduce shot noise in the first stage, an ME1400 version of the EF37A was used under electrometer conditions with an anode current of $110 \,\mu\text{A}$ and grid current of $10^{-4}\mu\text{A}$. When used with a tuned circuit having a Q of 50 to 800 c/s, the noise factor was 2.7 db (a figure of 3 db was stipulated).

A compact selective amplifier for the analysis of fluctuation noise in germanium rectifiers has been developed by the Radio Research Station, Slough. The basis is the RC circuit due to Schneider (*Phil. Mag.* 1945, Vol. 36, p. 371) and five resonant frequencies are provided at 0.1, 0.04, 0.02, 0.01 and 0.005 c/s with an effective Q of 8.

The transparency to infra-red radiation of germanium is exploited in a demonstration, by T.R.E. of the modula-



G.E.C. wide-band panoramic v.h.f. receiver.

tion of a beam. The transmission of infra-red through the germanium is dependent on the number of current carriers present in the germanium and this can be varied by applying an audio signal to a contact fulfilling a similar function to the emitter in a transistor. It was shown that some plastics with high light transmission are relatively opaque at the frequency used, $1.5 \times 10^8 \, \text{Mc/s}$ (2 microns).

Selenium in its amorphous form is also transparent to radiation from the infra-red to centimetre wavelengths, and "optical" components such as prisms and lenses have been made by a simple casting technique by the Services Electronics Research Laboratory, Baldock.

An infra-red image converter tube has been applied by Prof. B. K. Johnson (Imperial College) to the microscopy of opaque specimens, and is being used in the examination of minerals for the identification of uniaxial and biaxial crystals.

The detection of impurities in air by the change in emission and surface potential of a prepared plate at normal temperatures was demonstrated by the Signals Research and Development Establishment (Christchurch) using a vibrating capacitor in association with a selective phase-sensitive amplifier-detector. Potential changes of the order of $10~\mu V$ can be measured.

Exploration of the wavelengths and field patterns associated with different oscillation modes in a magnetron is effected in apparatus designed by S.E.R.L., Baldock, by means of a rotating pick-up probe extending from the surface of the cathode. The anode is excited by a tunable oscillator and mode "contamination" is readily visible on a c.r.t. display. By changing the axial positions of the excitation and pick-up probes, longitudinal distributions of r.f. voltage can be explored.

Some results of research into the effects of irradiation of insulants by radioactive emanations has been disclosed by the Ministry of Supply. Cross linking in long-chain polymers, such as polyethylene, affects not only the mechanical and chemical properties such as elasticity, melting (transition) point and solubility, but also the power factor which is increased at 65 c/s and 1 Mc/s, but appears to be such anged at 2000 Mc/s.

which is incleased at 9,000 Mc/s. Although well past the "breadboard" stage a G.E.C. wide-band panoramic v.h.f. receiver developed by the Research Laboratories is conveniently included in this section, if only to show that there can be no hard dividing lines between research, development and production. It is of the double superheterodyne type and gives c.r.t. display of all signals in bands 10 Mc/s wide between 80 and 220 Mc/s. Sensitivity for twice peak noise level is 10 μ V, and limitations usually set to bandwidth by considerations of image rejection have been overcome by sweeping the second oscillator through the converted signal frequency

in the i.f. amplifier. Pulses on either side of zero beat for each signal are combined to give a single response in the display. Frequency markers are derived from a quartz crystal.

Materials

Some interesting developments are taking place in the field of magnetic materials which will upset many preconceived ideas on the subject. Having become more or less accustomed to the idea of ceramic (ferrite) permanent magnets such as Mullard "Magnadur," we must now accept soft iron permanent magnets. The prediction of Prof. Néel of the University of Grenoble, that pure iron should develop very high corcive force when the particle size is of the order of magnitude of a magnetic domain, has been experimentally confirmed and is found to be a maximum when the crystal size is between 0.1 and 0.01 micron. Above and below these limits the material exhibits its familiar "soft" characteristics. The problems of producing the right grade of power have been solved and G.E.C. in this country are now supplying 'Gecalloy Micropowder' magnets in a variety of shapes. The powder has strong cohesive properties and can be cold pressed at normal temperatures without a binder, though a binder is an advantage in some applications. Like the ferrites, micropowder magnets are light, easily moulded and have low eddy current losses, but they have the added advantage of mechanical softness and ease of working. Their properties can also be controlled and in particular the ratio of remanence to coercivity can be varied over a wide range. Energy content ranges from 0.5 to $1.7 \times 10^{\circ}$ gauss-ocrsteds according to the grade of the material and coercive forces up to 700 oersteds are available.

Among conventional magnetic alloys the introduction by Telegraphic Construction and Maintenance of a new series of high-saturation alloys with properties comparable with Permendur, but with better machining qualities was noted; and Swift Levick are now producing columnar crystal anisotropic permanent magnets in simple shapes on a quantity basis. Made under the trade name of "Columax" this alloy has an average energy content of 6.8×10^6 gauss-oersteds compared with 5×10^6 for Alcomax III.

London Electric Wire (Lewcos) are now producing instrument wires with p.t.f.e. coatings from 0.0005 to 0.0015in thickness with adequate adherence and abrasion resistance to withstand normal hazards of winding. Synthetic enamel coatings with greater abrasion resistance than

conventional oil-based enamels are now available, under the name "Diamel," on precision resistance wires made by Johnson, Matthey. A new range of wires introduced by B.I. Callenders and known as "Fifty Three" have a new strongly adherent and abrasion resistant enamel coating with mechanical and electrical properties intermediate between oil-base and vinyl acetal enamels. Nonstretching binding twines, treated with p.v.c., and designed to withstand tropical acceptance tests, are now available from Associated Techincal Manufacturers.

Although, for all practical purposes, modern activated rosin solder fluxes are non-corrosive, there is still prejudice against their use in some quarters, and ordinary rosin is used in spite of its slow and uncertain fluxing properties. Enthoven have discovered a method of increasing the activity of rosin-cored solder without the use of chemical additives and have marketed the product under the name of "Actol," with a characteristic stellate core, in all stan-

dard tin/lead alloys and gauges.

To increase still further the ratio of solder to flux in their three-cored solders "Multicore" have developed an improved activating agent "Pentacol" which will in future be incorporated in their Ersin fluxes which now form 2.2 instead of 3.4 per cent of the total weight. Fluxed solder in tape form is a new departure from Multicore. It can be wrapped round a pair of wires and makes an effective joint when heated by a match flame.

Aluminium soldering has always been regarded as

difficult, but a new process developed by the Sheffield Smelting Co., shows more than usual promise and can be carried out with ordinary torch flames at a temperature of 450 deg C. The joints will withstand the accepted

accelerated corrosion tests.

accelerated corrosion tests.

Makers*: Associated Technical Manufacturers (B, C, IM, IS, W);
Bakelite (IM); Geo. Bray (CE); B.I. Callenders (C, CO, IS, W);
British Moulded Plastics (IM); Bullers (CE); Clarke (CF, IM,
IS); Connollys (IM, W); De La Rue (IM); Duratube and Wire
(C, CO, IS, W); Enthoven (S); Fine Wires (W); Hellerman
(IM, IS); Henley's (CO, IM, W); London Electric Wire (CO,
W); Long & Hambley (IM, IS, RP); Magnetic and Electrical
Alloys (L, M); Marrison and Catherall (M); Micanite and
Insulators (CF, B, CO, IM, IS); Mullard (DC, M); Multicore
(S); Murex (M); Mycalex (IM); James Neill (M); Reliance Wire
(B, C, CO, IS, W); Rola-Celestion (D, L, M); Salford (DC, M);
Geo. L. Scott (L); S.T.C. (M); Steatite (CE); Suffex (B, CO,
IM, IS, W); Swift Levick (M); H. D. Symons (IM, IS); Taylor
Tunnicliff (CE); Telcon (C, DC, L, M W); Thermo Plastics
(CF, IM); Transradio (C, IS, W); United Insulator (CF, CE, IM);

* Abbreviations: B, braiding; C, cables: CE, ceramics: CF, coil

Abbreviations: B, braiding; C, cables; CE, ceramics; CF, coil formers, bobbins; CO, cords; DC, dust cores; IM, insulating materials; IS, insulating sleeving; L, laminations; M, magnets and magnetic alloys; RP, rubber products; S, solder; W, bare

or covered wires.

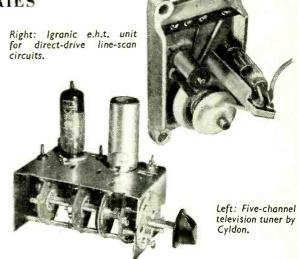
COMPONENTS AND ACCESSORIES

The fact that we now have five television channels all occupied is emphasized this year by the appearance of a five-channel tuner for receivers. Made by Cyldon it has an EF80 r.f. amplifier and an ECC81 frequency changer, and the channels are selected, not by a continuously variable control, but by switching in incremental inductances. The power gain of the unit is 24db and the i.f. output can be either in the band 9.5-14 Mc/s or the band 15.5-22 Mc/s according to the receiver manufacturer's requirements.

Another thing which is more of a sub-assembly than a component is the Igranic e.h.t. generator, for use with the new transformerless line scanning circuits. It contains an inductor for boosting the line flyback voltage, an EY51 e.h.t. rectifier and variable inductor for linearity control, the whole being mounted on a moulded base-plate. The

unit supplies an e.h.t. voltage of 13.5kV

For c.r.t. focusing, permanent magnets moulded from insulated metal powder are coming very much to the fore. Having the advantage of high resistivity, they can be placed close to deflector coils without affecting their performance. An example of their use is to be seen in the focus unit made by Elac, designed for wide-angle c.r.



tubes. This has two ring magnets mounted with their fields opposing, and focus is controlled by varying the spacing between them—the minimum field being when they are closest together. The unit centains two other rings, magnetized transversely, which can be adjusted to centre the picture.

The problem of mounting the variable inductors used for width and linearity control has been solved in one way by Egen Electric, who have combined them into a twin unit, and in another by Plessey, who have stowed them in the mounting bracket of their new line scan

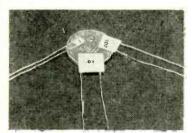
transformers.

Makers: Advance, British Moulded Plastics, Cyldon, Egen, Electro Acoustic Industries, Igranic. Long & Hambly. Magnetic & Elec-trical Alloys, Mullard, Plessey, Thermo-Plastics, Weymouth, Whiteley.

Capacitors

Metallized polystyrene film capacitors figure among the latest T.C.C. products. These are comparable in size to small paper types but have infinitely better characteristics. Capacitances up to $0.5\,\mu\mathrm{F}$ are available. Another plastic film capacitor, also made by this firm, has the exceptionally close tolerance of $\pm \frac{1}{8}$ per cent only and power factor of 0.0005.

The potentially high stability of silvered mica capacitors is not always possible to retain when stacked plates are used, but Johnson, Matthey have introduced a new manufacturing process in which the stack is bonded by



Left: Plessey " Casfilm" silvered ceramic capacitors.

Below: Two of the Parmeko Jupiter range of resin potted transformers.



Above: Zenith twin-brush Variac variable voltage transformer.



firing at a controlled temperature. Reduction in size is claimed as a by-product of this process.

Wider temperature ranges are a feature of some of the latest Hunt's capacitors; for example, their "Thermetic Midget" can be used without derating from -100 deg C to +120 deg C.

A new technique is exemplified by the Plessey "Casm" silvered ceramic film capacitors. The smallest, silvered ceramic film capacitors. measuring 0.2 in square only, provides a capacitance of

0.001 µF at 120 V d.c. working.

Some interesting miniature trimmers for television and v.h.f. applications have appeared this year. Cyldon has a chassis-mounting model with ceramic insulation of 0.5 to 3 pF or 3 to 9 pF, Wingrove & Rogers one of 0.5 to 3.5 pF with P.T.F.E. insulation and Mullard have a new version of their concentric air-dielectric trimmer with precision adjustment.

Makers*: Cyldon (T, V), Daly (E), Dubilier (C, E, M, P, T), Eric (C, T), Hunt (E, M, P), Jackson (T, V), Johnson, Matthey (M), London Electrical Mfg. (C. M), Mullard (T, V), Plessey (C, E, T, V), Stability (C, M). Static (P), Suffex (F), T.C.C. (C, E, F, M, P. T). T.M.C. (F, M. P), Walter (T), Wego (M, P), Welwyn (T), Wingrove & Rogers (T, V).

*Abbreviations: C=ceramic, E=clectrolytic, F=plastic film. M=mica, P=paper, T=trimmers, V=variable.

Resistors

To produce a standard resistance of 0,0001 ohm is in itself no mean achievement, but to guarantee its accuracy to 0.03 per cent demands such skill that few can emulate. Yet standards of this value, increasing in decade steps to 1,000 ohms, are now included in the Sullivan range of standard components. Salford have a new range of precision wirewound potentiometers intended primarily for use in desyn systems. They have tapped windings, single and double elements, twin wipers and provision for 360-deg rotation.

Miniaturization is extending into unusual fields; for example, Painton has introduced a range of miniature faders and attenuators of the type generally used in control consoles. Some are of the edgewise pattern and

occupy very little space.

A glimpse into future development was vouchsafed by some unusual fixed resistors shown by the Ministry of Supply. In one case a form of conducting glass is applied to glass plates and rods and then fired to fuse the whole together. In another, microscopic films of one of the precious metals is applied to glass plates and glass fibres. The former is etched to produce long paths and various values of resistance, while the fibres are wound on rods to provide a high resistance in a compact form. High stability is the aim in these designs.

Makers*: Doran (S), Dubilier (C, Hs, W), Egen (C), Erg (Hs, W), Electrothermal (Hs), Electronic Components (C, W), Erie (C, Hs, W), Morganite (C), N.S.F. (C, W), Painton (Hs, W), Plessey (C, W), Pye (W), Salford (W), Sullivan (S), Welwyn (C, Hs, W), Whiteley (C).

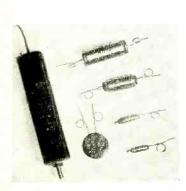
*Abbreviations: C=carbon, Hs=high stability, S=standards.

W=wistenandad

W = wirewound.

Transformers

The extension of the resin "potting" technique, as used for certain sub-miniature radio assemblies, to the





Left: Selection of T.C.C. latest type capacitors. Above: Elac focusing unit with device for picture centring. Right: Marconi 4-ft metal aerial lens for the 9-mm wavelength.



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construction of mains transformers may prove an important advance in the design of this class of component. It results in a considerable saving in size and weight of the article and also in the materials used for clamping the core and generally providing either an attractive or functional finish according to the use to which the component is put.

The potting resin not only provides a seamless protective case, but before setting it penetrates all parts of the core and windings and gives internal as well as external sealing. Transformers and chokes constructed in this way are extremely robust and will withstand a

considerable amount of rough handling.

Examples of the potting technique as applied to these components are the Jupiter range made by Parmeko and the Pentland series introduced recently by Ferranti.

To the Variac range of variable voltage transformers made by Zenith Electric has been added some new models in open and enclosed types fitted with twin brushes and providing two independently controlled output voltages.

Makers: Advance, Bulgin, Electro Acoustic, Ferranti, Goodmans Gresham, Igranic, Parmeko, Partridge, Plessey, Rola-Celestion, T.M.C., Weymouth, Whiteley, Woden, Wearite, Zenith.

Aerials

A few minor improvements and one or two new indoor television aerials seem to comprise this year's

contribution to broadcast aerial design.

Belling and Lee have modified the reflector (and director) fitting of their television aerials to simplify assembly and also impart greater strength. A clamping device is used which by means of a single screw simultaneously locks the elements and secures the fitting to the cross-arm.

A square-section cross-arm is Wolsey's contribution to the general betterment of aerials. It is claimed to secure the elements more positively, prevent displacement by high wind and also enables the aerial to be part assembled in the factory, thus simplifying the erection on the site.

Antiference have a new indoor television aerial called a "Loftex" for either vertical or horizontal mounting and based on the Antex (X-type) principle. This firm has introduced also a new type of car aerial with a swivelling split-ball base for scuttle mounting at any desired angle of slope. It is telescopic, extends to 62 in and closes to 24 in.

Aerial lenses for the 9-mm wavelength in metal and in plastic were used for an interesting demonstration staged by Marconi's to illustrate some of the characteristics of this type. They varied in size from 6 in to 4 ft in diameter. These lenses are now finding certain

applications in relay systems.

Makers*: Antiference (B, C, T), B.I. Callender's (B, C), Belling-Lee (B, C, T), Henley's (C), Marconi's (S), Reliance Wire (C), Suflex (C), Telcon (C), Transradio (C), Wolsey (C, T).

*Abbreviations: B=sound broadcast, including anti-interference. C=cables and feeders, S=special types, T=television.

Sub-assemblies

The printed circuit technique is used by Eire in a range of compact resistance-capacitance units covering such requirements as diode filters, triode and pentode RC couplings and various other combinations.

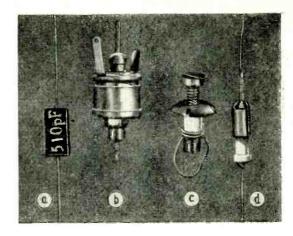
A considerable saving in assembly time can be effected by the use of these units. In one particular case six joints replace some 16 or so if separate components are

used.

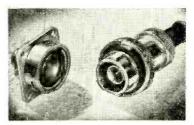
Interference suppressors form another convenient subassembly and as produced by Dubilier they comprise capacitors and chokes of one kind or another. A special range of television suppressors is now available for use on or in small domestic appliances such as electric sewing machine motors and hair dryers.

Chassis Fittings

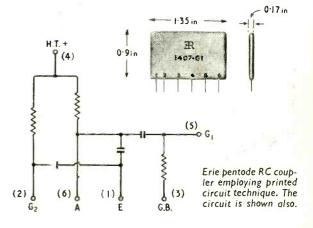
Careful insulation is the main feature of the latest valveholder from McMurdo. Intended for B9A e.h.t. rectifiers, it has a Nylon-loaded Bakelite socket moulded



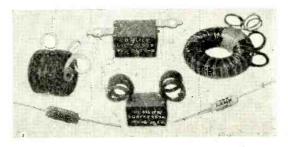
Some modern miniature trimmers; (b) Mullard air-dielectric with precision adjustment, (c) Cyldon television model, (d) Wingrove & Rogers with P.T.F.E., insulation compared in size with a Hunt's "Micromold" (a) measuring ½-in long.

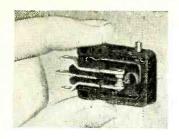


Left: Belling-Lee double-screened coaxial plug and socket.



Below: Dubilier television interference suppressors and some of the special chokes now available.

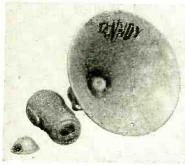




Left: Bulgin micro-switch with side cover-plate removed.

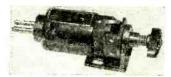


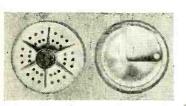




Left: Tannoy 100watt loudspeaker for airfields, harbours, etc.

Right: Coldring No. 200 magnetic pickup.

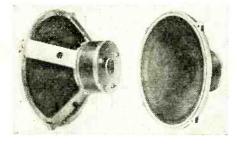


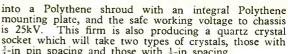


Left: Front and back plates of Acos Mic. 32 microphone capsule.

Right: Collaro "Studio" crystal

Below: Plessey 15-inch movingcoil loudspeaker.





³-in pin spacing and those with ½-in spacing. Belling-Lee have put on the market a very useful double-screened coaxial plug and socket. The contact assemblies are interchangeable in their housings to give either fixed-plug and free-socket or free-plug and fixed-socket, and the two parts are secured by a half-turn locking ring on the housing of the free part. Another improved connecting device is a moulded terminal strip, made by Carr Fastener, with screw terminals on the top face and small insulating barriers separating them. This is claimed to be more reliable than the usual strip containing metal inserts.

The range of cabinet components made by Widney-Dorlec now includes parts for miniature cabinets. These are made on a rather different principle from previous ones and are designed for spot welding. This firm also has a new telescopic mounting for draw-out chassis which locks in two places.

Makırs: A.B. Metal Products, Aerialite, Antiference, Belling-Lee, Berco, British Mechanical Productions, British Moulded Plastics, Bulg.n, Carr Fastener, Colvern, Cosmocord, Electronic Components, Electrothermal Engineering, G.K.N., Goldring, Hasset & Harper, Hellerman, Igranic, Imbof, Jackson Bros, Long & Harnoly, McMurdo. Pa nton, Ptessey, Reslosound. Simmonds Aerocessories, Steatite, Telcon, Thermo-Plastics, T.M.C., Transrad o. Tucker Eyelet. United Insulator Co. Walter, Weymouth, Whiteley, Widney-Dorlec, Wimbledon, Wingrove & Rogers, Wireless Telephone Co., Wolsey.

Switches

There was nothing very outstanding in switches this year except that Bulgan have produced a new and smaller version of their well-known micro-switch. Broadly the mechanism is as before (see picture) but it has been made smaller by folding back on itself the spring leaf on which the operating stud presses. Also, the moulded Bakelite body has been made as a flat tablet only \$\frac{1}{2}\$ in thick. The switch can be operated with a pressure of less than an ounce and a movement as small as 5 hundredths of an inch, and will break a current of up to 3 amps.

Makers: A.B. Metal Products, Belling-Lee. Berco, British Mechanical Productions, Bulgin, Diamond H Switches, Electronic Components, Electrothermal Engineering, Erie, N.S.F., Painton, Plessey, T.M.C., Walter, Whiteley, Wearite.

Sound Reproduction

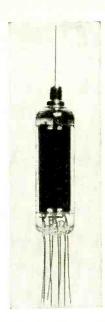
An interesting new p.a. loudspeaker has been developed by Tannoy for airfields, harbours, etc. The single driver unit is rated to handle 10 watts (120 watts peak) and is used in conjunction with a 200-c/s cut-off horn to give an electro-acoustic conversion efficiency of 50 per cent. The pressure unit is waterproof and incorporates a switched transformer for coupling to line impedances of 50, 100, 200 or 330 ohms; the coil impedance is 8 ohms.

Plessey have developed a conventional cone loudspeaker with a power-handling capacity of 25 watts. It is 15 inches in nominal diameter and has applications both as a p.a. unit and as a bass unit in high-quality loudspeaker combinations. Elliptical-type loudspeakers have now been added to the range of "Elac" units made by Electro-Acoustic Industries.

In the new "53" series of Collaro gramophone motors and record changers a new speed-change mechanism with a large-diameter, concentric-ground rubber idler has been designed with a cam mechanism to minimize wear when changing speed. A new crystal turnover pickup head, the "Studio," has been added to the existing Collaro range and incorporates a simple screw fixing for the replaceable cantilever stylus arms.

A turnover pickup working on the moving-iron magnetic principle, giving an output of 0.5V at 3.16 cm/sec lateral velocity has been marketed by Erwin Schaff (Goldring No. 200) The armature is coupled to the stylus by a rubber block in which the cantilever arm is a push fit.

Garrard are now in production with a new transcription-





Above: Mullard double tetrode for use at u.h.f.

Brimar reliable valve with Left: flying leads (equivalent to R18).

type 3-speed turntable (Model 301) in which speed fluctuations are less than 0.2 per cent.

A new crystal microphone of interesting design, the Acos (Cosmocord) Model 32, is of the diaphragm-driven type, and has a flat response up to 6,000 c/s. Cavity resonance and that a transfer and the state of the enclosed air, while the front the state of the enclosed air, while the front the enclosed air, while the front the state of the enclosed air, while the front the state of the enclosed air, while the front the state of the enclosed air, while the front the state of the enclosed air, while the front the enclosed air, while th

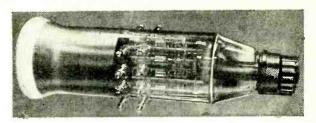
plate carries a buttressed lug which performs the dual function of providing rigidity and improving the polar response of the microphone.

Makers (Components)*: Birmingham Sound Reproducers (GM, GU, RC, PU); Collaro (GM, GU, RC, PU); Cosmocord (E, M, PU); Ediswan (RC); Electro Acoustic Industries (LS): Garrard (GM, GU, RC, PU); Goodmans (LS, M); Plessey (GM, GU, RC, LS, PU); Reslosound (LS, M); Rola-Celestion (D, LS); Goldring (PU); Tannoy (LS, M); Truvox (LS); Vitavox (LS, M); Whiteley (LS, M).

Abbreviations: D, diaphragms; E. earphones; GM, gramophone motors; GU, gramophone units; RC, record changers; LS, loud-speakers; M, microphones; PU, pickups.

Valves and Cathode Ray Tubes

Sub-miniature valves with indirectly-heated cathodes are quite a new thing in this country. Osram have produced two pentodes, a triode, a beam tetrode and a rectifier of this type, while Mullard have a triode which can be used at frequencies up to 500 Mc/s. In directly-heated, sub-ministures. Mullard are contributing directly-heated sub-miniatures, Mullard are contributing two new hearing-aid pentodes, the DF64 and DL64, designed for 15-V h.t. batteries and with the very low filament consumption of 10mA. Also very economical



Four-gun oscilloscope c.r. tube made by 20th Century Electronics.

to run are their new miniature valves for portable battery sets-the filament consumption being only 25mA. Another new miniature battery valve is the Brimar 1AC6 heptode 0.7mA and will operate up to 30 Mc/s. Brimar have also produced an e.h.t. rectifier, the R19, which has the high peak inverse voltage of 25kV, and is enclosed in a lead-glass bulb to prevent radiation of x-rays.

Production of reliable valves is continuing and this year a new range is available from Osram. The valves are mechanically-improved versions of existing Osram types and are known as the "Q" series. Brimar have extended their range of "Trustworthy" reliable valves with equivalents of the 6AM5, 6C4 and R18.

Two transistors of the point type are now available on the British market. These are the Osram GET1 and the S.T.C. LS737, both of which can be used to give a gain of about 20db. New germanium diodes are being made by S.T.C. and Mullard.

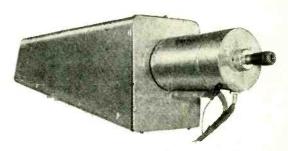
In cathode ray tubes much interest has been aroused by an oscilloscope tube containing four separate guns, made by 20th Century Electronics. It operates at 5kV on the final anode and the deflection sensitivity is just under ½mm per volt. Each gun has independent deflecting plates and the makers claim there is no interaction between them.

Another tube with more electrodes than usual is the Mullard 17-in rectangular television tube MW43-64. This is basically a tetrode, but has an extra electrode between the accelerator and the final anode for improving the uniformity of focus over the whole screen. Like the new Ediswan 15-in tetrode CRM153, this tube has a tinted glass face. Two more tetrodes are being made by Brimar, a 14-in rectangular tube C14FM and a 17-in rectangular tube C17FM.

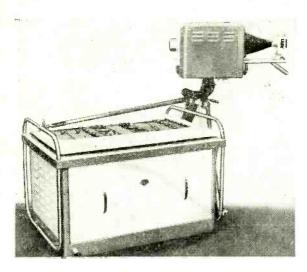
Remarkable for its extremely small size is the Ferranti KD10 voltage stabilizer, which stabilizes at 62 volts ± 0.15 volts with a running current of 1-1.2mA. It is made in a metal capsule measuring only $\frac{2}{5}$ in $\times \frac{3}{5}$ in $\times \frac{1}{4}$ in. Miniaturization is also the main feature of the new Westinghouse tubular e.h.t. rectifiers, Type 39. They are $\frac{3}{15}$ in in diameter, and with the selenium elements working at the high P.I.V. of 85 volts they are only 0.6in long per 1,000 volts. The current rating is 100 µA and the upper frequency limit 50 kc/s.

ELECTRONIC APPARATUS

The definition of "electronics" concerned with the extension of man's senses was well illustrated this year by three interesting aids to visual observation. One, produced by Philips, is an instrument for intensifying x-ray images so that the radiologist can see them immediately. It works on the image converter principle. The x-ray image is formed on a fluorescent screen and this is in contact with a photo-cathode, which emits a corresponding pattern of electrons. The electrons are accelerated by an electrode carrying a high positive potential and focused on to a second fluorescent screen very much smaller than the first. As a result of this acceleration and reduction



Philips instrument for intensifying x-ray images.



Mullard image converter equipment for high-speed photography.

in size the final image (which is viewed through an eyepiece) is about 1,000 times brighter than the original one.

The second instrument, made by Mullard, uses an image converter tube as an electronic shutter for highspeed photography—the point being that the electron beam in the tube can be interrupted electronically much faster than a light beam can be by a mechanical shutter. In this way exposures can be made as short as 1/20th of a microsecond! The exposure is actually made by applying a positive pulse to a control electrode in the tube, which normally has a negative bias to cut off the electron beam. This produces a brief image on the fluorescent screen which is recorded photographically. Deflector coils enable the instrument to make a line of successive images across the screen so that a cinematographic effect can be obtained.

The third electronic aid to observation is a flying-spot microscope, produced by Cinema-Television. This uses

a conventional flying-spot scanning system in conjunction with an optical microscope. The main feature of the instrument is that the image can be displayed on a number of c.r.t. monitors (magnified about 2,000 times) for demonstration purposes. Apart from this, the ability to alter contrast avoids the necessity for staining specimens, while the use of ultra-violet light for scanning gives greater resolving power than is possible with an ordinary microscope (because of the shorter wavelength).

Probably the most original instrument that has appeared recently is the electronic anemometer made by Isotope Developments. It measures wind velocities as low as 10ft per minute. Basically a radiation detector, it uses a wire-cage ionization chamber in which is fixed a small piece of radioactive material. The wind simply blows away the ions which are formed in

the chamber and the effect is registered on a meter in the detector. The servo or negative feedback principle

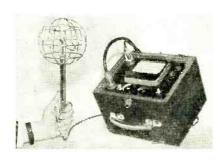
is to be seen in a good many electronic instruments nowadays. In several d.c. amplifiers of the mirror-galvanometer type, for example, a portion of the output is fed back to stabilize the action of the galvo. Then in two a.c. voltage regulators a change in input voltage is amplified and applied to a motor, which drives a variable transformer to correct the change. A new pen recorder works on a similar principle with

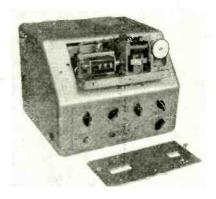
the fluctuations of the d.c. input, the movements of the correcting" motor being used to drive the pen.

Industrial Electronics

Applications of electronic techniques in industry depend primarily on the measurement of physical constants and the subsequent derivation of signals for automatic control. Sometimes one parameter is obtained in terms of another as in radioactive thickness gauges where the fundamental quantity indicated is mass per unit area of sheet material. In the Baldwin rolling mill extension gauge, thickness is derived in terms of change in length (velocity) of steel strip as it passes through the mill, and the method of measurement is novel. Magnetic recording heads print an alternating pattern of magnetization on the strip before and after rolling, the tracks being offset to avoid interference. Pick-up heads follow the recording heads and their outputs are combined in a differential phase-indicating meter. If the distance between heads before and after the rolls is equal, and if there is no reduction in thickness, the meter reads zero-fluctuations in roll speed are eliminated by driving the recording generator from one of the roll spindles. When there is a reduction in thickness a corresponding increase in wavelength takes place after rolling, and to bring the meter back to zero the "pre-rolling" recording head can be moved relative to its pick-up by a micrometer, which can be calibrated in percentage reduction of thickness. instrument will detect reductions of less than 0.1 per cent and can be applied to the production of thin steel strip running at speeds of the order of 1,000ft/sec.

B.T.H. have applied a high-speed multiple preselecting batch counter to the measurement of length, and have used it for cutting veneer wood to predetermined lengths. A perforated wheel is driven by the wood strip and interrupts a photo-cell light beam at intervals equivalent to 1/10th inch. Four Dekatron counters in cascade record the passage of the strip, and when the glow reaches the predetermined cathodes in all four tubes, the strip is stopped, cut and the counter reset. Up to ten different lengths can be selected by push-button and this enables the operator to avoid blemishes economically. In practice the measuring speed is limited to 12in/sec, though the counting speed would permit 200in/sec.







Top left: Electronic anemometer by Isotobe Developments. Above: Baldwin "Quantex" light quantity meter. Left: Pye direct - reading (counter) pH meter.

Liquid level meters depending on electronic methods are widely used, and in one recent model introduced by Fielden, a self-balancing capacitance bridge technique is used which provides positive indication and control to less than 1 per cent. The principle of the Fielden "Servograph" recorder has been applied by Stanton Instruments to the continuous measurement of weight in a "thermobalance" designed to record the change of weight with time in specimens heated in a small furnace to temperatures up to 1,000 deg. C.

The metering of light quantity is of importance in many

photographic and printing processes, and the Baldwin Quantex" light quantity meter is based on the charging of a capacitor by a current derived from a photoelectric cell. Preset relays give exposures in two ranges covering

1 sec to 1 hour.

Process timers are widely used and depend usually on the time-constant of an RC circuit. As a demonstration, Allied Electronics show equipment designed to life-test an electronic d.c. voltage stabilizer through a regime of vary-

ing load and supply voltage.

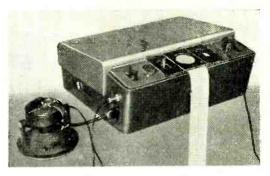
Two watch timers are available from Furzehill Laboratories. Type 774V gives a bright spot on a circular c.r.t. The time-base frequency can be varied over a small range to bring the spot to a stationary point, when the error can be read off a calibrated dial. An alternative display expands the watch pulse and provides useful information for the diagnosis of irregularities. In the Type 774E each watch beat is recorded on a strip of paper which records short-term irregularities as well as the average rate. Both instruments make provision for the testing of watches with all standard gear trains giving beats of 3½ to 6 per sec.

Developments in strain gauge technique include the production by Saunders Roe of foil elements by a process evolved by Technograph Printed Circuits, Ltd. Considerable simplification of the associated equipment results from the increased current-carrying capacity of these elements. Pressure gauges employing strain gauges are made by Langham Thompson for use in pipe lines and the technique is applied by C. N. Smyth to hypodermic

needles for use in medical research.

Ultrasonic flaw detection is now well established and developments are mainly in detail. The latest equipment made by Glass Developments, Ltd., includes barium titanate probes, steerable beam over angles from 90 to 55 deg to the surface, miniature probes for small specimens and a single probe transmitting-receiving technique. C. N. Smyth has introduced an inexpensive flaw detector, with separate or combined transmitting and receiving probes, which can be used as an accessory to a Cossor oscilloscope.

The machining of brittle materials by an ultrasonic technique has been developed by Mullard. A magneto-striction transducer operating at 22 kc/s is coupled by a tapered metal "velocity step-up transformer" to a cutting



Furzehill recording watch timer.

tip, which, when applied with suitable abrasive, rapidly penetrates glass and other difficult materials. motion is translatory rather than rotary, holes and depres-

sions of other than circular shape are easily formed.

Measurement of pH (hydrogen ion concentration) is important in many industries and a correspondingly wide variety of instruments is available, as exemplified by the small battery-operated portable (Model 30) and the industrial, hermetically-sealed instrument (Model 28) made by Electronic Instruments, for which a wide range of electrode systems is available. The W. G. Pye No. 11082 pH meter gives direct readings on a 4-figure counter with an accuracy of 0.01pH. A self-balancing potentiometer is driven by a servo motor which is also coupled to the counter. Automatic zero correction is carried out continuously while the instrument is idle, so that it is always available for immediate use.

In the "Humicon" humidity detector Standard Telephones make use of glass silk between two perforated plates as a moisture-sensitive impedance. The voltage drop across this is used to control a series of thyratrons which operate appropriate ventilation or heating devices

in, for example, a G.C.A. radar mobile van.

The measurement of moisture in coal dust presents difficulties due to variable conductivity from impurities, and the National Coal Board have found that these effects can be eliminated by measuring the effective dielectric constant at 30 Mc/s for which purpose a Fielden "Drimeter" has been adapted.

Dawe Instruments have developed a comprehensive warning system for inflammable gases in the ventilating systems of oil tankers. The principle involved is the rise in temperature and resistance of a catalytic platinum fila-A motor-driven commutator samples all the detectors in sequence and an alarm signal is given on the bridge indicator board by concentrations well below the explosive limit.

TEST AND MEASURING INSTRUMENTS

Under this heading are included instruments intended for laboratory use, for production testing, and for servicing. It is not possible to review any but new or substantially improved models, nor the numerous industrial instruments (many employing electronic techniques) such as material testers, that might conceivably

be employed in the radio industry.

The first impression on surveying the instruments exhibited this year might have been one of disappointment at not finding outstanding new types or techniques. Closer examination would have shown, however, that behind many of the apparently similar front panels a vast amount of real progress has been made. Anyone experienced in the use of instruments knows that small refinements may add up to a more significant total than some striking departure from previous practice.

Even the old-established moving-coil meter has not reached the limit of improvement, and this year there seems to be more evidence of this than usual. To obtain a high sensitivity and speed of response, Everett Edgcumbe use four high-flux magnets in the magnetic circuit, which is shaped so as to allow a 270-degree scale instead of the usual 120 degrees. In the Metrovick meters an exceptionally robust result is achieved by skilful use of die castings and mouldings. Ballistic characteristics are especially important in signal level indicators, and the new Pullin VU meter, which is a rectifier m.c. voltmeter, claims to reach 99 per cent of steady value in about 0.3 sec, with an overswing not more than 1.5 per cent. Another specialized m.c. instrument is the Pye fluxmetei, full-scale reading 700,000 "line-turns" (7 milliweber-turns), in the well-known "Scalamp" format; provision is included for rapidly restoring the deflection to zero. A portable silicon-crystal millivoltmeter developed by A.I.D. for testing signal-generator output calibration might well find wider applications on account of its frequency range of 1-300 Mc/s. An attenuator has been designed which extends its voltage range (0.05-0.15).

Among valve-aided meters the most noticeable trend is the use of pre-detector wide-band amplification to increase sensitivity, as in those by Dawe and Furzehill. The ranges of the latter (Type V.200) are now lmV-lkV full-scale, and the frequency coverage—10 c/s-6 Mc/s—is adequate for high-definition v.f. work. The Philips 6010 battery-powered millivoltmeter, for zero frequency, employs the modulation principle so as to amplify stably over twelve ranges, 0.1mV-300V, with input resistance 0.67-100 $\mathrm{M}\Omega$; with the addition of a probe containing a germanium rectifier it can be used for measuring voltages from 5-1,000 mV over the wide frequency range 2-800 Mc/s. Very high input resistance is now becoming common in z.f. valve voltmeters; an instrument shown by B.T.-H. is exceptional in having an input current of only 0.1 micromicroamp at frequencies from zero to 100 kc/s.

Measurement of very high voltages is a problem. The latest Ernest Turner electrostatic voltmeters up to 20 kV are protected against brush discharge by the use of fixed vanes of graphite-loaded Bakelite. At still higher voltages, safety is a major consideration. A capacitive potential divider by Hivolt uses a concentrated field around the periphery to protect the divider proper (arranged axially) from proximity effects; the indicator, connected by a long

cable, can be read at an amply safe distance. Capacitive dividers are also made by B.T.-H. for examining high-voltage pulses on a c.r. oscilloscope.

The facilities of wide-band amplification are perhaps even more valuable when the indicator is an oscilloscope. In this application, width of frequency band is usually appreciated as

U.h.f. absorption frequency meter, Type TF. 1026/I (Marconi Instruments).



speed of response. Amplifiers are obtainable separately from Nagard and Cossor, working from z.f. or thereabouts upwards, but for examining high-speed transients there are obvious advantages in having the amplifier built into the oscilloscope. Several new models are well adapted for this type of work, notably the Nagard DG.103 with double-beam tube, the Philips GM.5660 with frequency band 15 c/s-10 Mc/s and pulse rise time 40 mµs, and the Airmec 830 (30 c/s-20 Mc/s and 25 mµs respectively). The notable sharpness and brightness of the trace on the screen of the last-named oscilloscope is maintained even at the extreme speed of 30 cm per µsec. Philips also have a new oscilloscope which, although a general-purpose model, takes into account the importance of pulse technique in television. It is notable for including two identical amplifiers covering 0.3 c/s-1 Mc/s and exceptional synchronization facilities. There are several other new general-purpose oscilloscopes. Cossor 1052 also has two identical amplifiers and other improvements on the old 339, but does not include voltage-calibrated shifts like the 1049; a separate voltage calibrator (1433) is obtainable however. The Furzehill 1684D/2 continues and extends the association of this marque with direct-coupled amplification, the frequency range now being 0-4 Mc/s. The Industrial Electronics 2300, although a truly miniature 2½ in-tube instrument weighing only 64 pounds, includes features usually obtainable only in types many times its size—push-pull amplification from zero to 100 kc/s on both X and Y plates, and automatic synchronization.

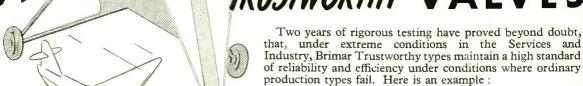
The Advance range of signal generators has been extended in the $15 \, \text{c/s-} 50 \, \text{kc/s}$ band by Type J, which differs from the H.1 in having a calibrated power output up to 1 watt at a constant $600 \, ^{\circ} \Omega$ impedance, rather than a voltage output. Two varieties are obtainable, with and without output meter. There is now a smaller version of the Dawe a.f. source. The previous Muirhead decade oscillator has been superseded by an improved model having remarkable frequency accuracy.

All of these employ RC tuning, which has displaced the beat method for a.f. purposes, but where a very wide frequency is required without switching the beat method still applies, as exemplified in the interesting Philips GM.2889 a.m.-f.m. oscillator, covering 5-225 Mc/s in one sweep. It is particularly suitable for measuring bandpass response of television and other receivers; f.m. at mains frequency can be obtained with deviation up to 10 Mc/s by means of a "loudspeaker" movement. For testing discriminator characteristics, 400 c/s f.m. is available up to 250 kc/s deviation. A separate 15-30 Mc/s oscillator is incorporated for introducing frequency marker "pips."

The Marconi Instruments TF948 signal generator covers 20-80 Mc/s in two ranges, the effective scale length being over 14 feet, and is provided with sine wave f.m. and sine and square wave a.m., internally at three audio frequencies. The specification is elaborate and includes crystal frequency checking and modulation depth and deviation measurement. Another new instrument from the same firm is the v.h.f. test set TF.982, comprising a signal generator for 60-184 Mc/s and four i.f. ranges, a crystal calibrator, a r.f. field detector, an a.f. output power meter, and a multi-range test meter. A range of frequency hitherto not at all well provided for—300-1,000 Mc/s—is covered by the Advance L.1 signal generator in two ranges, using a 6F4 valve in a conventional series-tuned oscillator circuit. Output is controlled over a 130db range by a piston waveguide attenuator, and modulation can be either sine or pulse.

Instruments for frequency measurement are not so prominent as they have been in times past, but there are three new Furzehill crystal frequency standards: one providing 150 watts at 50 ± 10^{-5} c/s, and two portable units for general frequency checking, of which Type G.410 is provided with push-button control for selecting standard frequency signals at multiples of 0.1, 1, 10, 100, 1,000 and 5,000 kc/s. A vastly more elaborate equipment is the Plessey frequency synthesizer, which now appears with motor-driven operation by which any multiple of 1 kc/s up to 100 Mc/s can be automatically selected. An unusual





In order to investigate the stresses of helicopter motor blades, a D.C. amplifier was installed in the motor head, transmitting signal levels to the control cabin below.

The excessive vibration rendered normal valves useless, and reduced the valve life to only a few minutes.

Substitution of Brimar "Trustworthy" type 6067 freed the D.C. Signals of all noise, and measurements were able to proceed.

In another case, an Aircraft Company required instrumentation to measure stresses on jet aircraft when approaching the speed of sound. This equipment consisted of sensitive amplifiers located in the aircraft. Normal valves were too noisy under these conditions to give reliable results, but modification, to employ Trustworthy valves, has since solved the problem. Further, the equipment has stood up for a considerable number of hours service under these arduous conditions.

These are but two of many examples which prove that extra-rugged, extra-reliable Trustworthy valves are so often the perfect solution to an otherwise insoluble problem.

3 TRUSTWORTHY types are immediately available for commercial use

6064 the Trustworthy version of CVI38 (6AM6/8D3) 6065 ,, , , CVI3I (9D6)

6058 ,, ,, CVI40 (6AL5)

BRITISH MADE

TRUSTWORTHY

BRIMAR

Standard Telephones and Cables Limited FOOTSCRAY, SIDCUP, KENI

Tracking 2000g at 10 grammes maximum stylus pressure



The listening public is inclined to take technical achievements for granted -to assume, for instance, that the increasingly exacting requirements of microgroove records can automatically be met by pick-up manufacturers. This is not the case. There is nothing automatic about it. The technical progress made by record manufacturers is, in effect, a challenge to pick-up manufacturers—a challenge which Cosmocord, whose slogan "Always well ahead" really does mean something, are always ready to take up.

Sometimes the record manufacturers set us a problem, to which the solution is "impossible" and therefore takes quite a time to provide.

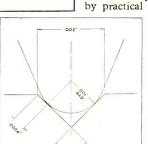
Such a problem is involved with regard pick-up tracing capabilities which now have to be of a substantially higher order than those for 78 r.p.m. records, and are likely

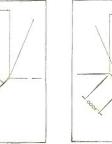
to become even more critical. Cosmocord, with the very helpful co-operation of the Decca Record Company, have recently made a detailed examination into the optimum tracking requirements that could arise in modern types of microgroove records. This was done in order to establish a basis for the design of pick-ups that would not only satisfy the requirements of all records at present available to the public, but if possible anticipate future developments within the limits as set out in the recently published British Standard Specification (B.S.1928: 1953).

THREE FACTORS

The three important factors that had to be considered by Cosmocord in designing such a pick-up were minimum groove width, maximum lateral displacement and maximum stylus tip acceleration.

The minimum groove width as laid down by the British Standard Specification is .002in. The conditions existing in a record giving up to 30 minutes playing time per 12in. side are well demonstrated in the accompanying scale drawings. For simplicity's sake, the groove angle has been shown as 90° and the radius at the bottom of the groove has been left out, as at .0003in. maximum it has no effect. Three pick-up





stylus radii are shown, the nominal .001in. radius (Fig. 1) and its upper and lower limits of .0012in. and .0008in. (Figs. 2 and 3 respectively) according to British Standard Specification. It can be seen that the .001in. radius has .0004in. wall above its point of contact, whilst the .0012in. radius has no more than .0002in. This does not take into account the pinch effect which can reduce the margin by .0002in. at 5,000 c/s.

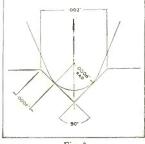
PRACTICAL CONSIDERATIONS

In order to arrive at maximum possible displacement, some assumptions have to be made that are dictated by practical considerations. Working on the basis of 200 grooves per inch the maximum

possible displacement (d) is .003in. At a frequency of 40 c/s. this displacement $corresponds \, approximately \, to \, a \, maximum$

velocity of 2 cm/sec. (v = $2\pi fd$). Accepting the recording characteristics of the Decca Long Playing test record No. LXT 2695 as typical for commercially produced long playing records, the maximum velocity and corresponding acceleration at 10,000 c/s. can be calculated. According to the record specification the recording pre-emphasis at 10,000 c/s. relative to 40 c/s. is + 24.4 dbs. and

this gives a velocity of 31.6 cm/sec. and a corresponding displacement of .0002in. $\left(e = \frac{v}{2\pi f}\right)$. It further follows that expressed in gravitational units the acceleration 10,000 c/s. may be as ef^2 high as 2000g (g =where e = displacement = .0002in. and f = 10,000 c/s.).



WHAT OF THE FUTURE?

The examination, as can be seen even from this simplified statement, has brought to light conditions that appear to be incredible at first sight. They are, however, far from being purely hypothetical and it may be only a question of time before they appear on commercially produced records. Even now there are a few odd records on the market which come very close to these limiting conditions.

It can be seen that the problem set by the record manufacturers in this matter was a formidable one. Cosmocord have answered it so completely with their Acos "Hi-g" series of pick-up cartridges that they already meet, here and now, any likely future development of gramophone records within the B.S. 1928: 1953 specification.



always well abead

Acos Crystal Devices are Protected by Patents and Patent Applications in Gt. Britain and Other Countries.

form of absorption frequency meter (TF.1026 series), illustrating an entirely different conception of frequency measurement, has been introduced by Marconi Instruments; each has a 2:1 frequency ratio, the whole series of five covering 125-4,000 Mc/s. The resonant system comprises a coaxial line closed at one end and tuned at

the other by a variable capacitance.

Nearly all new a.c. bridge designs, for all frequencies from power to v.h.f., are based on the use of transformer ratio arms for input or output or both. One of the chief advantages is that an admittance connected across part of a low-leakage transformer winding does not appreciably alter the ratio, as it would if connected across one of a pair of resistance ratio arms. As a result, the values of components can be measured in situ, notwithstanding that relatively low admittances exist between both terminals and earth. An example is the grid-to-anode capacitance of a screened valve, which is small absolutely and also relatively to the capacitances to cathode, etc. Wayne Kerr have for some time been exponents of this technique for high r.f., and now have several experimental models for a.f. In one, capacitances can be measured from 12,000 pF down to 0.0001 pF, at 10 kc/s. A 1-Mc/s transformer bridge devoted more particularly to interelectrode capacitances and conductances and therefore less wide in range has been produced by Electronic Tubes. It is worth noting that in both these bridges, as well as in other high performance modern equipment, the humble "magic eye" is adequate as the indicator. In another experimental Wayne Kerr bridge the Maxwell form is brought up to date with a transformer output, 10 kc/s source, and "magic eye," to such good effect that self and mutual inductance are measurable in ranges as low as 0.01 µH full-scale. But perhaps the most interesting of the series is a 1-kc/s bridge for four-terminal network measurements, in which full use is made of transformer arms to cover all four quadrants of the complex plane.

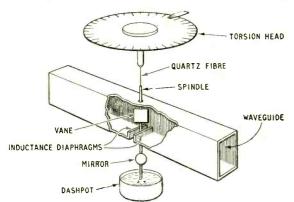
If one terminal of a bridge arm is joined to its screen, as in most of these obtainable separately, its use is thereby

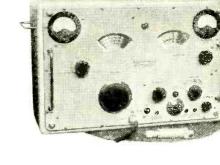
limited. For adaptability it is necessary to have two screens, the outer earthed and the inner joined to the arm; decade resistance boxes so arranged are produced by the Croydon Precision Instrument Company.

Apparatus for displaying valve characteristics on a c.r. tube screen now appears in a form adapted for germanium valves (transistors), by Marconi's W.T. Co. The development of equipment for testing the mechanical properties of valves has been stimulated by the requirement for valves to stand severe conditions, such as being shot from guns. The usual technique is to vibrate the valves by a modified loudspeaker drive and to examine them mechanically and electrically. In the set-up by Electronic Tubes the movements of the electrodes can be seen stroboscopically, and their resonance spectrum recorded photographically from electrical responses. The observing instrument in the Industrial Electronics vibrator equipment is the c.r.

panoramic wave analyzer by the same firm.

Measuring apparatus for frequencies over 2,000 Mc/s centres on the waveguide "test bench" assembled from a wide variety of waveguide sections and components. Most of the work is based on observance of standing-wave ratio and node positions, and some recent devices have the object of facilitating this. In the Decca automatic s.w.r. indicator four crystal detectors mounted in the waveguide and spaced at eighth-wave intervals are connected to a c.r. unit which provides a display in Smith chart form from which the frequency variation of a match can be seen at once. A cylindrical chart enabling displacements measured at one frequency to be seen by inspection for any other frequency in the waveband has been devised by Among the precision microwave instruthe Admiralty. ments offered by Elliott Bros. is a torque vane wattmeter for absolute measurements of power in the X band. The vane is suspended by a fine quartz fibre at 45 degrees in the waveguide, and the power passing along the guide is measured in terms of the mechanical torque exerted on This can hardly fail to remind one of the the vane. Raleigh disc absolute method of measuring sound intensity.

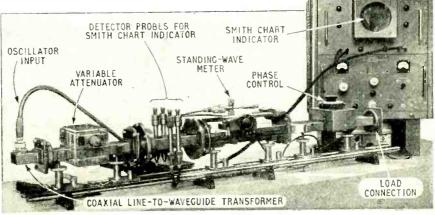




Above: Torque vane wattmeter, for absolute measurements of power in the X (3-cm) band (Elliott Bros.).

Above, right: U.h.f. (300-1,000 Mc/s) standard signal generator, Type L.1 (Advance Components).

Right: Microwave test bench, fitted with spaced detectors for automatic Smith chart display on the indicator seen on the right (Decca Radar).



5—Applications in Trigger Circuits

LARLIER articles in this series have dealt rather generally with the nature of the two common forms of transistor and with some of the more elementary linear circuit properties. Following the plan of the series, which is to hop from topic to topic in an effort to cover an enormous field sometime in the foreseeable future, we must now look at the applications of transistors to trigger or switching circuits. Here the future is wide open and, from some points of view, rather depressing. As an example of a transistor application here, I have two blocking oscillator circuits performing equivalent functions, one using a valve, power consumption 1 watt, and a transformer, as well as the few resistors and capacitors; the other uses a transistor, three resistors and one capacitor, and consumes only 50 mW. Apart from the difference in bulk and power consumption, the smaller unit should operate in the particular application for ever, while the valve must have its heater operating continuously, so we can expect to change valves at least once a year.

I say this is rather depressing, because it makes the fully automatic factory a much more immediate prospect. As Norbert Wiener has pointed out, we shall then have a community supported by slaves, a state of affairs which can be studied better in Gibbon than

in the works of the economists. This may happen quite quickly, and our only hope is to make sure that the first computing machine can be solving the economic problems faster than the industrial machines are creating them. I do not think we shall get much guidance from either the Georgics or from "Das Kapital." But make no mistake, within 10 years or so we shall see the development of two economies, transistorized and non-transistorized, and if we are to belong to the second class we might as well start planting cabbages now.

The trigger circuit is the key item of any digital device. It produces pulses, re-shapes pulses, accepts them, rejects them. In most existing computer systems a twin-triode circuit has been used, but now the single or double transistor circuits are sweeping the board. Let us consider the general properties of these trigger circuits.

The equations given earlier in parts 2 and 3 of this series showed that the impedances presented at the input or output terminals of a transistor-resistor circuit could be negative, provided that the current gain, α , of the transistor was greater than unity. At the present time we can take this to mean that a point transistor must be used. This negative resistance is the first requirement for obtaining the type of

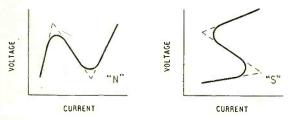
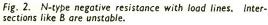
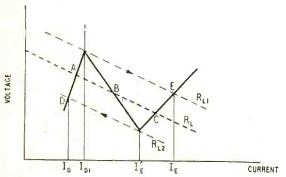


Fig. 1. Characteristics of the two main types of negative resistance.





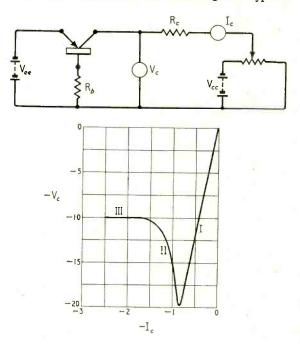
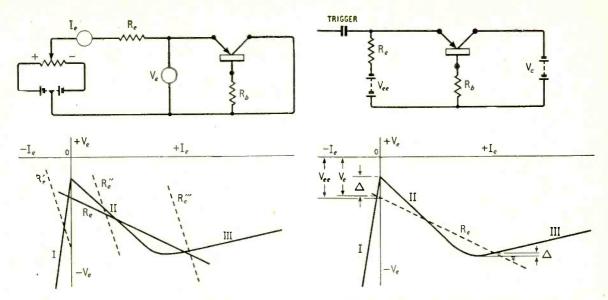


Fig. 3. Collector large-signal negative-resistance characteristic.



Left: Fig. 4. Idealized emitter large-signal negative-resistance characteristic. Right: Fig. 5. Bistable transistor circuit.

non-linear operation which is nowadays called a "switching function." A general investigation of these "switching functions" leads to the view that the most rational method of analysis is obtained by splitting the action into three regions: on, off, and transition. The classic example of such a system is the famous Duke of York, who had 10,000 men (when they were up, they were up...). All the important switching functions used in engineering contain some sort of energy storage which drives the circuit through the transition region. A very simple example is the ordinary press type of electric light switch. As you press the button you store energy in a spring until a triggering threshold is reached, when the spring drives the mechanism from one position to the other.

There are two types of negative-resistance characteristic, and it is necessary to be clear which type we are using in any particular circuit. The reason why there are two types is only understood when the full impedance diagram is plotted, because it depends on the way the impedance behaves at the extremes of high and low frequency. This is a topic for an article in itself. Here we can content ourselves with the voltage-current diagrams of what are called, for obvious reasons, the N and S types of negative resistance. Fig. 1 shows the simplified forms of these diagrams. The N type of negative resistance is stable when open-circuited, but is not stable when shortcircuited: the S type is short-circuit stable, but unstable when open-circuited. A rough picture of the difference between the two is obtained by considering some conventional oscillator circuits, in which the tuned circuit may be either resonant, if the negative resistance is short-circuit unstable, or anti-resonant, if the negative resistance is open-circuit unstable.

Let us consider what happens if we have an N-type negative resistance and we connect a positive load resistance R to the terminals. Since the N characteristic is the characteristic of an active network we must put a bias battery in the circuit, too. The load line can then be moved parallel to itself, and three possible positions are shown in Fig. 2. The middle position, marked R_L is the most interesting. It intersects the N at three

points, of which A and C correspond simply to two positive resistances in series and are thus stable. At B we have a loop consisting of a negative resistance in series with a numerically smaller positive resistance. This is unstable, and if the system is moved to B by some means it will snap (as fast as the reactances in the circuit will allow) to either A or C.

Now suppose that the system is stable at A and we alter the bias to move the load line up to $R_{\rm L1}$. The only stable point is E, and the current through the loop jumps smartly from $I_{\rm D1}$ to $I_{\rm E}$. Now we change the bias in the opposite direction, to bring the load line down to $R_{\rm L2}$. The current falls slightly to $I'_{\rm E}$ and then as the load line leaves the right-hand corner the current drops to $I_{\rm D}$ as the only stable point becomes D. This sort of snap action will be familiar to anyone who has ever used the Schmitt double-triode trigger circuit.

It does not require much imagination to see that a load line can be imposed on the S-type characteristic in Fig. 1 to give three-point intersection. All the discussion in the last paragraph can be rewritten with the word current replacing voltage and viceversa and it will then apply to the S-type characteristic. These two characteristics are, in fact, duals. The subject of duality has been explored by "Cathode Ray," and will be discussed in detail later.

Switching Circuits

Now, perhaps, we can turn our attention to transistor circuits. In Fig. 3 and 4, we have two very simple test circuits and the voltage-current characteristics obtained with them. In Fig. 3, the circuit is held under control by using a large value of $R_{\rm c}$ so that the tests can be carried out even in the negative resistance region II. The same stabilizing function for the emitter characteristic of Fig. 4 is performed by $R_{\rm c}$. Both these curves belong to the N-type, although region III has got flattened out a bit: but regions I and III are positive resistance regions, linked by the negative resistance region II.

Fig. 5 shows the simple transistor bistable circuit.

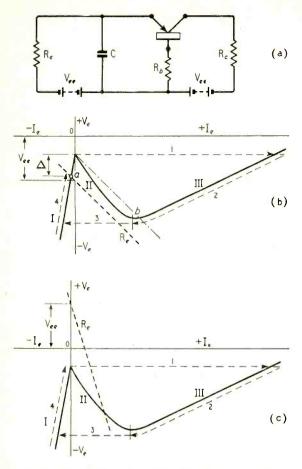


Fig. 6. Monostable and astable characteristics resulting from the addition of capacitor C.

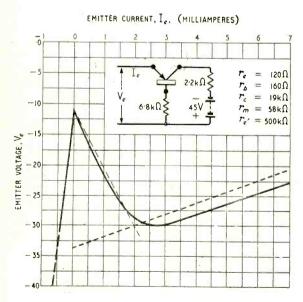


Fig. 7. Basic circuit values and calculated (dotted) and measured emitter negative resistance characteristics, for a Type 1698 point transistor.

If you compare the characteristic with that of Fig. 2, you will see that there are two stable positions, and the system can be triggered from one to the other by applying a pulse of the right polarity at the "trigger" input. This circuit is equivalent in properties to the resistance-coupled multivibrator using two triodes.

Having this idea of the multivibrator in our heads, let us see how we can introduce capacitors into the transistor circuit to convert it to either an oscillator or a "single-shot" multivibrator. A single capacitor has been introduced in the circuit shown at the top of Fig. 6. The extra resistance R_c is fairly small, and is introduced to provide a convenient way of getting a low impedance output from the circuit. In the case shown in Fig. 6(b), the controlling resistance R_e is low enough for the three-point intersection to be possible. The value of Vee is such that the circuit is normally stable at a. Suppose now we put in a trigger voltage \triangle . The load line is lifted up to the apex of the N-curve, and can then "see" the single stable point b. As soon as the system starts to re-set itself to b, however, the capacitor C presents a short-circuit to the emitter, and the operating point jumps along the line 1 to a high emitter current. When the intersection with the N-curve is reached, however, Re takes control again, and the capacitor starts to discharge along the path 2. By this time, however, the trigger pulse has ended, and when the discharge brings the emitter voltage to the trough, the working point jumps along the shortcircuit line 3 to meet region I again. Finally, the emitter voltage runs up along 4 to the point a, where the system waits for a new trigger.

With a higher value of R_e and positive bias applied to the emitter we have the conditions shown in Fig. 6(c). This arrangement is astable, as the only intersection is in region II. The circuit oscillates steadily round the path 1, 2, 3, 4.

Pulse Length and Spacing

Practical values for a circuit of this kind are shown in Fig. 7 for a 1698 point transistor. With the values given in the inset diagram and an emitter load resistance of 15,600 ohms returned to the earth line, frequencies of 2,000-10,000 pulses/second and pulse lengths of 20-2,000 microseconds can be obtained with capacitors in the region $0.01-0.5\mu F$. Both experimentally and theoretically it can be shown that pulse length and spacing are proportional to capacitance. Experimentally I have found that pulse repetition rate is fairly linear with emitter bias. The characteristic in Fig. 7 is not extended far enough to enable the peak emitter current to be determined, but a rough estimate is about 12 mA. The pulse available at the collector will be about 40 volts. When very short pulses at repetition rates of the order of 1,000 pulses/second are needed, the most satisfactory arrangement seems to be to use an emitter load resistance of the order of one megohm, and a correspondingly smaller capacitance. The 40-volt output pulse can then be obtained with collector current of about 1-2 mA, but for reliable operation a positive bias voltage on the emitter is needed to lift the intersection clear of the corner.

More elaborate circuits of this basic kind for bistable operation incorporate diodes in the base or emitter circuit. I hope we shall be able to consider these in more detail later, but for the moment we may note that one form of this arrangement converts the R_e line into a "dog leg," and provides a more certain three-point intersection condition. A very similar discussion will apply to the arrangements shown in Fig. 8. The N-type collector characteristic enables us to arrange for bistable, monostable or astable working. There is nothing of special interest here, unless it is the danger of excessive currents with the low emitter impedance.

The base connection is rather more interesting. The voltage-current plot shown in Fig. 9(a) on the following page is of the S-type and it can be seen that one condition for the three-point intersection load line is that the external base load resistance must be numerically larger than the negative input impedance. By inserting inductance in the base lead we get the instantaneous open-circuit effect, corresponding to the capacitance short-circuit, needed to give the snap action in monostable and astable action. The circuits and conditions are shown in Figs. 9(b) and 9(c), and in any practical circuit a resistance in the collector lead would be added to provide an output. The main disadvantage,

of course, is the rather limited range of time constants available

using inductances.

This treatment is obviously of great value in considering sinusoidal oscillators. If the capacitor in the emitter or collector astable circuit is replaced by a resonant circuit, the system will act as a sinusoidal generator, limited by overloading. Similarly, the inductance in the base circuit can be replaced by an anti-resonant circuit. The design problem is quite easy now. Looking at Fig. 7 we see that the emitter circuit resistance can be just over 9,000 ohms and the emitter bias -10 volts to give a barely astable condition with the other values as shown. The net negative resistance is then very small, so that oscillations will be limited without much overloading.

Refinements of the simple emitter circuit, the most commonly used form, are directed towards improving the pulse shape. With the simple capacitor circuit the collector current pulse has a drooping top caused by the run down path 2 (see Fig. 6). The capacitor can be replaced by an open-circuited delay network, of the ordinary pulse-forming type. This has two results: the pulse top becomes flat, and the pulse duration no longer depends on the time constant $(C \times \text{ emitter resistance})$, but is fixed by the line. Different samples of transistor give identical pulses. The second refinement is to use diodes in the monostable circuit, so that it takes the form shown in Fig. 10. This circuit is triggered by a negative pulse applied to the base. Once the trigger action starts, the diode CD2 cuts off the input terminal so that it has no further control over the action. As a

result, the output pulse is practically independent, both in width and amplitude, of the input trigger. The other diode, CD1, is provided to reduce the time constant of the capacitor discharge in section 4 of the path. This means that the circuit returns very quickly to its quiescent position after producing a pulse, and very high repetition rates are possible. This circuit is used in computers to reform the pulses after they have passed through the various gates. Obviously it could also be used as a repeater in a pulse code modulation system.

Another application of diodes is in stabilizing the position of the junction between regions I and II. In the characteristic shown in Fig. 7 this junction is at 11.5 volts. The value can be calculated, and is approximately $V_c R_b/(R_b + r_c)$, where V_c is the collector voltage, R_b the total base resistance and r_c the collector resistance. The weak point is r_c , which varies with temperature. Typical figures suggest that the junction

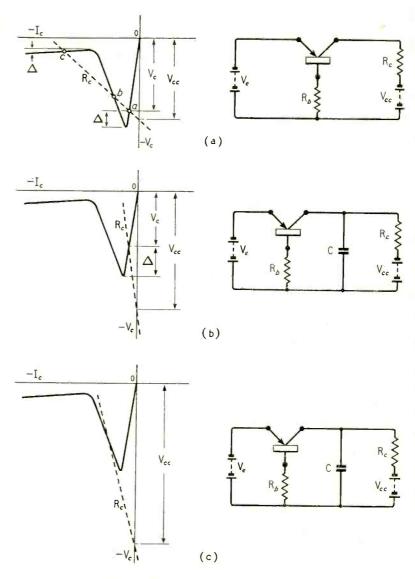


Fig. 8. Collector-connection switching circuits.

may move about 5 per cent, or, say, 0.5 volts. For circuits adjusted to maximum sensitivity this is rather important, especially if the transistor moves

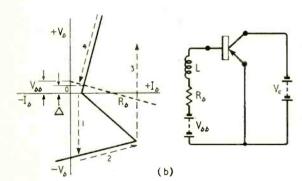
into the bistable condition and locks on.

I do not propose to discuss the actual circuits used to prevent this until some later date. A word of warning is perhaps the best conclusion: in using these circuits, always make sure that they will fail safe and that if an oscillator or monostable circuit does lock on it will not allow a destructive current to flow.

Inductive loads are especially dangerous in trigger circuit working because they slow down the passage through the region in which the transistor has a large dissipation.

Acknowledgment.—Figs 3 to 9 are based on Figs. 3, 4, 6, 7, 20, 9 and 11 respectively of "Transistors in Switching Circuits" by A. E. Anderson and Fig. 10 on Fig. 16(a) of "Transistor Trigger Circuits" by A. W. Lo. Both papers appeared in *Proc. I.R.E.*, Vol. 40, No. 11, Nov. 1952.

$\begin{array}{c|c} & +V_b \\ \hline V_{bb} & +I_b \\ \hline -I_b & \Delta \\ \hline \end{array}$ $\begin{array}{c|c} & +I_b \\ \hline \end{array}$ $\begin{array}{c|c} & \\ & \\ \end{array}$ $\begin{array}{c|c} & \\ \end{array}$



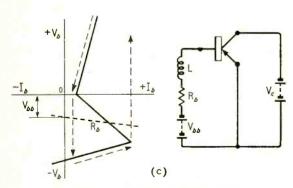


Fig. 9. Base connection switching circuits.

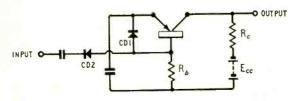


Fig. 10. Addition of diodes to stabilize pulse width and amplitude.

Manufacturers' Literature

Metal Rectifiers; a brochure giving dimensions and weights of selenium spindle-mounted stacks, with an explanation of the coding system used to identify them. From Standard Telephones and Cables, Rectifier Division, Warwick Road, Boreham Wood, Herts.

Solder, in wire, pellet and fluid form; a leaflet giving a summary of the products of Multicore Solders, Hemel Hempstead, Herts.

Television Receiver, type TUG36; console with a 17-in tube giving a picture $14 \text{in} \times 10\frac{1}{2} \text{in}$ and with five controls on the front panel, described in a leaflet from Bush Radio, Power Road, Chiswick, London, W.4

Radio-gramophone, H.M.V. model 1617A, with ten waveband ranges, three-speed record changer and 8-watt output from a 13½-in speaker. Circuit description and specification in a leaflet from the Gramophone Company, Blyth Road, Hayes, Middlesex.

Universal Television Servicing Unit ("Klempt" Type FW0200), comprising a versatile a.m./f.m. signal generator and oscilloscope. Technical specification leaflet from Otto Gruoner, Winterbach bei Stuttgart, Germany.

High-energy Permanent Magnets using "Columax," an improved grade of "Alcomax III," and claimed to have the highest magnetic energy per unit of volume yet achieved (8.63 × 10⁶ gauss-oersteds max.). Specification and curves in a leaflet from Swift Levick & Sons, Clarence Steel Works, Sheffield, 4.

Electro-mechanical Devices, including a.c. and d.c. relays, mercury relays, time-delay relays, solenoids, thermostats and low-inertia motors for instruments. Specifications and operating characteristics in a catalogue from Electro Methods, Caxton Way, Stevenage, Herts.

Anti-vibration Instrument Mountings, in stud form, made of rubber with projecting metal pins. A leaflet giving shapes and sizes available from Howard Clayton-Wright, Wellesbourne, Warwickshire.

Television Converters; alignment instructions for Type AC/4 units in a leaflet from Spencer-West, Quay Works, Great Yarmouth, Norfolk.

Surplus Equipment, Government and manufacturers', listed in a catalogue from Clydesdale Supply Co., 2, Bridge Street, Glasgow, C.5. Also a supplementary list of Components and Accessories.

Microwave Test Equipment, for waveguide sizes 10 and 11, including standing-wave meters, adjustable short circuits, matched loads, waveguide-to-coaxial line transformers, variable attenuators, waveguide bench rails and supports, and a Heiltube test oscillator. Loose-leaf book containing specifications from Decca Radar, 1-3, Brixton Road, London, S.W.9.

Toggle Switches and Signal Lamps, also a number of special-purpose switches, described in an illustrated catalogue with blue-print drawings from Arcolectric Switches, Central Avenue, West Molesey, Surrey.

"Permanent Magnets," a well-produced illustrated book of 58 pages covering the theory of magnetism, design of magnets, materials used, properties of various alloys (with curves and tables), effects of heat, shock and alternating fields, magnetizing and demagnetizing, testing, storage and handling; with a glossary of technical terms. From the Permanent Magnet Association, 301, Glossop Road, Sheffield, 10, price 10s.

Waveform Analyser; description and specification (with curves) of the Muirhead-Pametrada instrument and associated equipment, with notes on its use for vibration measurement and waveform analysis in various industries. An illustrated booklet from Muirhead & Co., Beckenham, Kent. Also a leaflet on their amplifier-maintained tuning forks for frequencies of 480-2,000c/s.

=THE "BELLING-LEE" PAGE=

Providing technical information, service and advice in relation to our products and the suppression of electrical interference.

Gold Plated Components

Considerable interest was aroused by the gold plated contacts on several of our components on view at the recent R.E.C.M.F. exhibi-

This finish came about as a result of stringent tests to which many components under develop-ment for the Ministry of Supply

and Admiralty are subjected.

These tests, particularly those of R.C.S.II, to which components of the H.I grading have to be submitted, include subjection to temperatures of 100°C dry heat, where hitherto the top temperature in many cases was only 70°C. addition, there are tests in which the components are exposed to exacting and prolonged conditions of damp heat.

To maintain a low contact resistance under the exhaustive tests described above, considerable attention had to be given to the contact surfaces. After intensive investigation it was found that a gold flash on an appropriate underfinish gave the required durability, together with low contact resistance.

It will be obvious that once the process had been introduced, its benefits would be applied wherever desirable.

It may be asked why not keep to silver? Silver discolours badly as silver sulphide has an awful appearance, and makes it very difficult for soldering.

Birds on the Aerial

When speaking to an audience in a district where horizontal aerials are necessary, one question certain to be asked is,



happens if a row of seagulls decide to perch on the elements?" Webfooted birds don't perch in the accepted meaning of the term. They will sit in rows on the comparatively rounded apex of a roof, or on the flat "bun finial" of a flag pole, but they cannot grasp a

half-inch rod or tube. Starlings might, but they only weigh a few ounces. We have seen rooks that have developed a technique of grasping the top of an "H" aerial, and sitting apparently in comfort, but even a rook has little weight. Birds are built for lightness, even their bones are hollow and contain

Suppression of Household Appliances

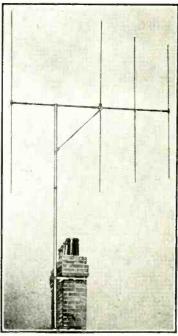
A few days ago we were testing out a new flex lead suppressor on a number of appliances, hair-dryers of various makes, fans, sewing machine motors, etc. The tests were carried out at home. When tried with T.V. on an outdoor aerial, suppression was quite good, making all the difference between intolerable nuisance and entertainment value. On an indoor aerial in the same room as the receiver however, interference was still troublesome. That is why, as we have so often written before, the authorities will have scant sympathy for a complaining viewer who has not done his best for himself by the erection of an aerial suitable for his location.

A Lightning Tip

A few peals of thunder at Easter reminds us to issue the annual soother regarding lightning. The chance of a strike on your house is very remote, and the presence of an aerial does not increase the If anything, it is bound to reduce the chance, as the presence of the aerial connected to a receiver is constantly discharging that little pocket of air in the immediate vicinity, thereby reducing the voltage gradient.

We can pass on a useful tip for those who feel they should do something to satisfy a qualm. Theoretically, the top element should be connected to the centre conductor of a co-axial feeder and the lower to the screen. We doubt if the average user would notice the difference, therefore reverse the arrangement and take the upper element to the screen, and before it enters the house, remove the P.V.C. outer covering exposing the screen, twist round it a length of heavy copper wire and take to a good earth by the most direct route. Care should be taken to waterproof the join with adhesive tape, otherwise water might syphon into the house via the screening mesh.

"Non-Directional" "Multirod"
We had a report from a useful source, that a "Multirod," carefully installed, was apparently "all round looking." The case was sufficiently interesting to warrant sending the mobile research laboratory to examine the situation. We found that the answer was due to the fact that the site was surrounded by hills, there was



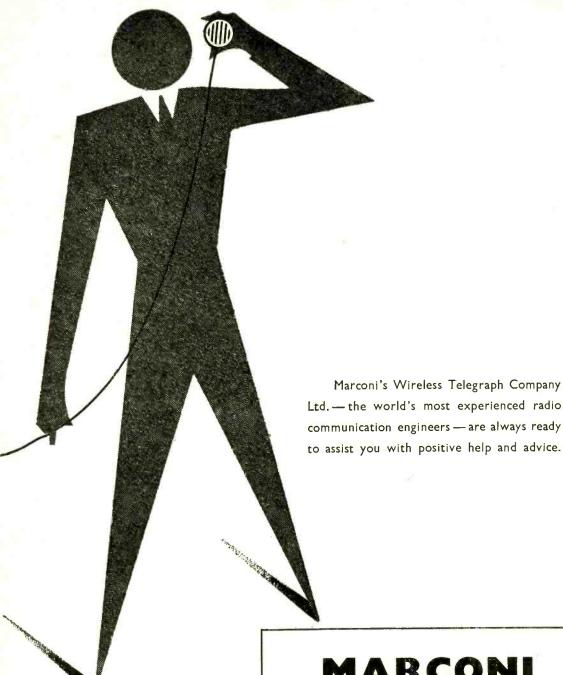
Belling-Lee" " Multirod" ment array.

apparently no direct signal, all that the aerial received was reflections and diffusions from the high ground.

Aluminium Corrosion

Most forms of corrosion are very serious to the engineer, and we would prefer to think that there was no such thing associated with our aerials. We ask users to paint aerials on erection and at intervals, but we know that few are so treated. The form that aluminium alloy corrosion takes, is that parts tend to "grow" together, with a reduction of electrical resistance.

Written 27th April, 1953



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Diagnosis of Distortion

R. WIGAN* B.Sc.(Eng.), A.M.I.E.E.

The "Difference Diagram" and Its Interpretation

T the outset it should be emphasized that this article is not concerned with the measurement of distortion; it deals with a method of diagnosis aimed at recognizing, locating and removing the source of any distortion which is found.

The diagnosis is made by examining an oscilloscope trace which represents all the defects of the apparatus which is being tested. By comparing the outline of this picture with certain standard shapes, examples of which are given here, the various sources of distortion can be recognized. For example, typical overload conditions can be recognized at a glance (Figs. 10 and 11). In other photographs the distortion conditions have been artificially exaggerated to bring out the characteristic features.

The technique adopted to generate these pictures can be summarized briefly as follows:-

A pure sine wave signal is applied to the test object (an amplifier, for example) and also to the X-plates (horizontal axis) of an oscilloscope.

The distorted output signal is applied to the Y-plates after passing through a network which subtracts the pure fundamental wave and leaves only the distortion terms, together with any hum, hum-modulation or circuit "noise." Before being applied to the Y-plates this "difference" signal is amplified, generally 30 to 100 times.

When the phase of the X-signal is suitably adjusted the trace shown on the oscilloscope closes into a curved line which is a representation of the transfer

characteristic of the circuit tested with all its defects enormously magnified (see Figs. 1 and 2). Because this display is produced by a subtraction process the term "difference diagram" has been chosen for it.

The technique has the special merit that transient or slowly changing distortion conditions can be observed. Moreover, although it is not put forward as a measuring technique, it is possible to read off from the difference diagram the magnitude of the primary distortion terms with useful accuracy, a procedure which is necessary when correlation with standard harmonic analyses is required.

Since distortion components as small as 0.1 per cent can be recognized under good conditions, this method of diagnosis is applicable to amplifiers, oscillators, and the like, which have to meet even the most stringent performance specifications.

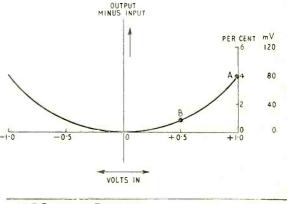
The equipment required is relatively simple and can be assembled from apparatus generally available

in an audio-frequency laboratory.

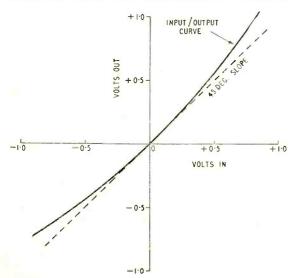
Details of Apparatus. To understand the difference diagram, consider first the typical input/output transfer characteristic of a single-valve amplifier shown in Fig. 1. The curve for an ideal amplifier is represented by the dotted line with a slope of 45 degrees, and the difference (i.e., vertical intercept) between these two curves represents the departure of the system from the ideal conditions. In Fig. 2 this difference is shown, plotted in the form which has been called the difference diagram.

Left: Fig. 1. Ideal (dotted) and actual transfer characteristic of an amplifier.

Below: Fig. 2. "Difference diagram" corresponding to Fig. 1.



* B.B.C. Research Departmen...



The block schematic of the apparatus to produce this diagram electronically is shown in Fig. 3. The two upper branches carry out, at (9), the subtraction process illustrated in Figs. 1 and 2. The fourth branch is used only when a large distortion term has to be cancelled to prevent confusion of the fine detail.

The circuits shown are arranged for a test frequency of 1,000c/s. The filter (8) in Fig. 3 is necessary only if the phase shifter (7) contains valves which may introduce distortion. The ganged attenuators (4) and (6) are used to alter the input level to the test object (5) without changing the output level delivered by (6).

If it is desired to cancel any selected component in the difference signal, the oscillator (15), which can be set to multiples of 1,000c/s, is locked to the input signal by a "spike" generated by clipping and differentiation at (14). Element (12) is used to adjust the phase of the harmonic frequency generated by (15) relative to the phase of the test signal.

The arrangement shown in Fig. 3 is used when both the pure input signal and the distorted output signal from the test object are available, but if this is not so, and only the output can be obtained, the

arrangement of Fig. 4 is employed.

Since the signal equivalent to the missing input signal is necessary for the "subtraction" process, a filter (8) is employed to abstract a pure sine wave from the output signal. Tests of this kind are called here 2-terminal tests, to distinguish them from the 4-terminal test made when both input and output terminals can be used.

Typical Diagrams. Essentially the difference diagram is a Lissajous figure, the configuration of which will change with the setting of the phase control of the X-amplifier. In some circumstances it follows the shape of the transfer characteristics and it may also be used, with caution, to estimate the harmonic content. To introduce the reader to the kind of information which a difference diagram yields the following examples have been chosen: Fig. 5(a) is the difference diagram generated by a single-valve output stage. The input/output curve of such a stage is similar to Fig. 1, so the diagram of Fig. 5(a)

resembles Fig. 2. When the input voltage is increased the diagram changes to Fig. 5(b) The downward "spike" on the right is due to grid-current which sets in fairly sharply and reduces the output voltage. (The reason for the curve being looped is dealt with in the Appendix.)

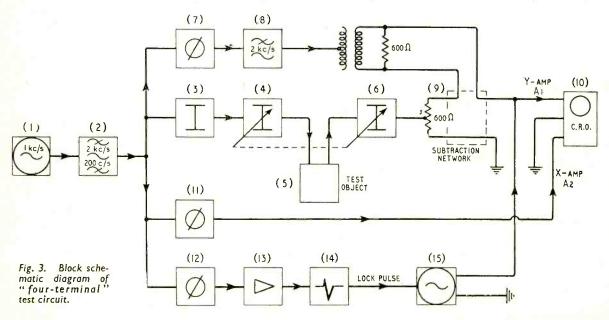
The input/output curve of a push-pull stage is like Fig. 1 in the upper part, but in the lower part lies below the dotted line. As a result the difference diagram (see Fig. 6) droops downwards on the left-

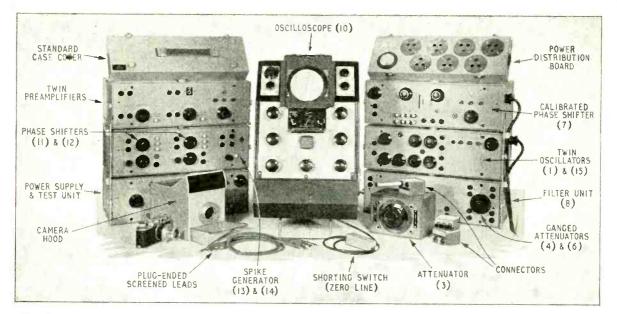
hand side and tips up on the right.

The distortion component present in Figs. 2 and 5(a) is almost pure second harmonic, shown by the two positive maxima in the difference signal. Fig. 6, however, shows nearly pure third harmonic because there are three positive maxima in the trace on the tube; one on the extreme right, one as the fundamental approaches negative maximum, and one as it returns to the centre again. In this photograph the "go" and "return" traces are, of course, superimposed. The vertical width of the diagram is due to hum in the amplifier. In spite of this the upper and lower edges retain their characteristic S-shape.

The flattened parabola of Fig. 7 indicates a heavily driven triode stage and contains both second and third harmonics. It consists of a parabola (characteristic of second harmonic) to which has been added an S-shaped curve which steepens one end and flattens the other. The relative proportions of the two components can be deduced from this. Here again, in spite of a very large proportion of hum, the upper and lower edges of the diagram retain the shape characteristic of the non-linearity of the system. To get this photograph the earlier stages of the amplifier were heavily driven while the gain control at the input to the final stage was turned down.

Fig. 8 shows the presence of hum-modulation in a push-pull output stage in which there was a strong 100-c/s ripple in the h.t. supply. The test-frequency was set to be exactly ten times the ripple frequency so that ten individual stationary traces could be seen, each corresponding to a different h.t. voltage. Each trace, Fig. 8(a), is a distorted S-shape and oscillates 100 times per second about the centre point of the





Portable test equipment and accessories. Numbering corresponds to that used in Figs. 3 and 4. The twin pre-amplifiers on the left are used to provide either high-level test signals (up to 20 dbm) or to act as a buffer between the output from the test object and the input to the test gear. All units are housed in the standard ventilated boxes used by the B.B.C. Research Dept. for portable test apparatus.

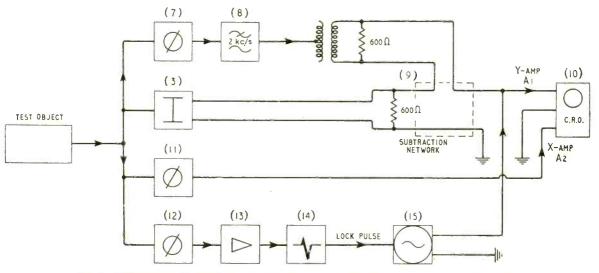


Fig. 4. "Two-terminal" circuit for use when the input to the apparatus under test is inaccessible.

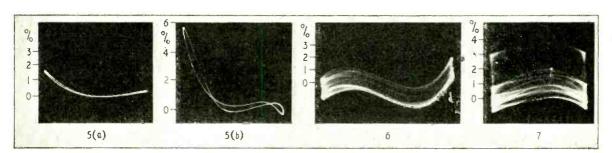


Fig. 5. Single-valve output stage working (a) just below and (b) just above the overload point. Fig. 6. Hum and third harmonic in a push-pull output stage. Fig. 7. Hum at greater level than second and third harmonics (§ingle-valve output stage).

diagram. When the driver stage was balanced the second harmonic term disappeared, yielding Fig. 8(b). Finally the third harmonic was removed by "injection" (see Appendix). The resulting diagram, Fig. 8(c), has nearly straight edges which shows that higher distortion terms were negligible, evidence that the system was operating well within its capacity.

The previous example illustrates very well how effective a picture of the distortion can be, for the amplifier in question had earlier been tested with a wave analyser. The 100-c/s modulation had not then been noted, whereas the diagram showed at a glance that the modulation term was several times larger than the

second or third harmonic.

Figs. 9(a), (b) and (c) show gross distortion in an amplifier of the electro-mechanical type in which a moving-iron loudspeaker movement drives a pair of push-pull carbon buttons. There are some novel features. Fig. 9(a) shows the stepwise response of the carbon granules. Fig. 9(b) shows a double line at bottom centre due to an alternative transient condition. Figs. 9(c) and (d) show an unsuspected phenomenon, the reversal of the phase of the distortion terms when the d.c. voltage fed to the carbon button was increased slowly through a critical value. The distortion, Fig. 9(c), momentarily disappeared and reappeared in reversed phase, as shown in Fig. 9(d). It will be noted that the "go" and "return" traces are different, owing to friction or other forces between the carbon granules.

The remaining diagrams were obtained with the circuit of Fig. 4. Figs. 10 and 11 show the "spike" characteristic of a system driven beyond its designed limits. Figs. 12(a) and (b) show very clearly the sharp origin distortion produced by a diode. The loop in Fig. 12(b) generally appears when severe overload is

associated with a large transient phase shift.

The distortion illustrated in Figs. 11 and 12 is the result of two processes, and neither diagram alone gives any clue to the true cause. Both the recording and the playback equipment combine to produce Fig. 11, and transmitter and receiver combine to produce Figs. 12(a) and (b). From a series of diagrams representing different carrier levels and degrees of modulation it is, however, possible to separate the influence of the receiver from that of the transmitter, but it is difficult to find an equivalent method of dealing with recording distortion.

Fig. 11 is a good example of a difference diagram containing "noise" which has blurred the edges of the trace. Variation of the speed of the turntable caused slight oscillations of this diagram about its centre point. This has slightly lengthened the extremes of the trace and confused details which could

be clearly distinguished when the diagram was directly viewed on the tube face.

Scale of the Diagram. The Y co-ordinate (i.e., the height) of any difference diagram will depend directly upon the gain chosen for the Y-amplifier of the oscilloscope. This gain must be known and included in any photograph of the diagram either for record purposes or to allow one picture to be compared with another. If the procedure set out below is followed the photograph is like Fig. 12(b). The necessary information is given by the scale.

The percentages represent the deviation from linearity of the transfer characteristic; the scale must be used with caution, however, for it can be applied directly only to the extremities of the diagram (e.g., the point A in Fig. 2). At that point the percentage scale reads 4 per cent while the input voltage is 2.0 V peak-to-peak. It follows that the 4 per cent ordinate corresponds to 80 mV. That is to say that if the conventional transfer characteristic were drawn, the instantaneous output voltage would exceed the instantaneous input voltage by 80 mV where the latter was +1.0 volt. Observe, however, that the corresponding ordinate at -1.0 volt input indicates that at this point on the diagram the output voltage will be less than the input voltage by 80 mV. This follows from the simultaneous change of sign of input and output voltage as the left-hand side of the diagram is entered.

This apparent anomaly should be carefully noted, and in practice a test always has to be made to establish whether positive or negative ordinates on the tube face represent gains or losses. A simple test is to apply a biased-off diode to the test-circuit; where the signal voltage exceeds the bias a sharp kink or spike appears in the diagram. The direction of this spike indicates the loss ordinate.

Suppose now that the diagram of Fig. 2 were used to predict what the distortion would be if the signal input were reduced from 2 volts to 1 volt peak-to-peak. The diagram of Fig. 2 would then terminate at B. The mV scale shows that the error voltages would be 20 mV; i.e., 2 per cent of the input signal. The percentage scale reads 1 per cent.

At first sight it appears that this kind of difficulty could be avoided by scaling each diagram in mV instead of percentages. This, however, would involve a new scale for every photograph, which would be

impracticable.

On the other hand, if a percentage scale is used, three scales will serve for all purposes. In practice the percentage scale is determined as follows:—

(a) The cancellation circuit (7), (8) in Figs. 3 or 4

Fig. 8. Push-pull output stage with 100-c/s ripple in h.t. supply. (a) modulation with second and third harmonics. (b) driver stage balanced to remove second harmonic. (c) both second and third harmonics removed.

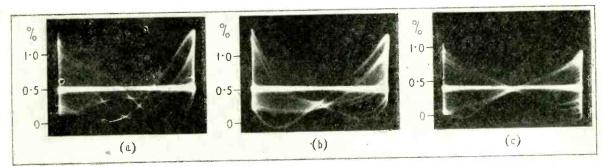
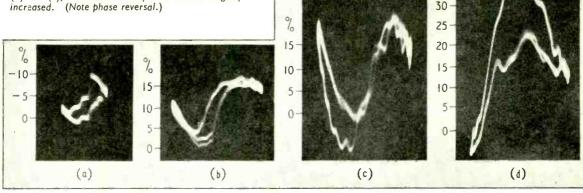


Fig. 9. (a), (b), (c) Distortion in electro-mechanical amplifier at successively increasing input levels. (d) as (c), but with microphone current slightly increased. (Note phase reversal.)



is interrupted, the X-signal removed, and the gain of the Y-amplifier adjusted to bring the resulting vertical line to a chosen height on the oscilloscope graticule. Let this height be D units.

(b) Having restored the cancellation circuit (7), (8) and the X-signal, the gain of the Y-amplifier is increased by a known amount (usually not more than 30 times) so as to make the details of the diagram clearly visible. Let the gain increase by N times.

(c) The percentage scale to be associated with this diagram must have an interval of DN/100 between

the 1 per cent marks on the scale.

It is convenient to arrange that the Y-amplifier (A1) has several fixed steps of gain which are exactly known (say N=10, 30, 100), and to prepare in advance the corresponding percentage scales, which can be fixed to the face of the tube and photographed together with the diagram.

Simplifications. The somewhat elaborate networks of Figs. 3 and 4 can be simplified if no more than a general impression of the distortion is required. If changes of régime are considered unimportant, and only the larger distortion terms are of interest, the ganged attenuators and the "slave" oscillator chain

(12) to (15) may be omitted.

Bridge-type circuits are a common feature of apparatus designed to measure total harmonic distortion, but although they provide an output which contains only the distortion terms, they cannot be used to generate a difference diagram, because the various distortion products are "dispersed," i.e., shifted in relative phase, by passing through the bridge network.

The essential components of a 2-terminal circuit are the phase-shifter and filter, (7) and (8). A 4-terminal circuit requires, in addition, a bandpass or possibly a low-pass filter at (2). The performance of these filters need not be superlative, for many commercial oscillators generate no more than 1 per cent or 2 per cent of second or third harmonics, which can be reduced to 0.1 or 0.2 per cent by 20db attenuation at (2). If a valve stage, which may generate distortion, is incorporated in (7), filter (8) should have a slightly better performance.

Photographing the Diagram. For the illustrations a Cossor oscilloscope, Type 1035, with a green tube,

Type 89D, was used.

The photographs were obtained with a Leica II camera on Kodak 35mm orthochromatic film R55, with an exposure of 1½sec at F/6.3. The brightness of the trace was adjusted for each exposure by the following procedure. The trace was dimmed until only just visible in its weakest part while being traversed to and fro by the X-shift control. The brightness control was then advanced by a fixed amount predetermined by trial exposures.

This procedure makes allowance for the influence of mains-voltage variations upon the brilliance of the spot, and also for the large variations in writing speed which are caused by changes of test frequency or

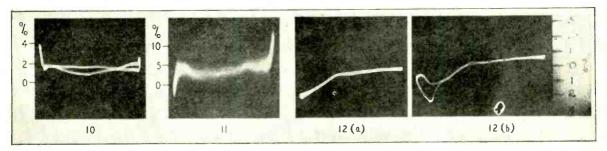
size and degree of detail of the diagram.

The percentage scale will appear in the photograph if it has been attached to the face of the tube and

is given local illumination.

Conclusion. It is not easy to bring out in a short survey the full merits of this technique; the informa-

Fig. 10. Oscillator running into grid current. Fig. 11. Disc recording grossly over-modulated. Fig. 12. Radio receiver with "delayed" a.v.c.; modulation (a) just below and (b) just above 100 per cent.



tion given should, however, be sufficient to guide those who wish to explore its possibilities. The method has been in use in the Research Department of the B.B.C. in the course of the last 2-3 years, its development being part of a general investigation into distortion in a.f. systems.

The illustrations in this article are taken from a stock of several hundreds collected over this period. It should be noted that, in order to simplify discussion, the most elementary examples have been chosen, whereas in practice much more complex forms may occur. Fig. 9 has therefore been included to demonstrate the application of this new technique to

a more complex problem.

For the investigation of distortion in recording systems the difference diagram has unique value, for unless the speed of the medium (disc or tape) is practically constant only the simplest of the conventional distortion measuring systems can be applied in such work. It is justifiable in such cases to attempt to deduce the harmonic content from a geometrical analysis of the diagram, should a numerical expression of the distortion be required. In general, the diagram serves its most useful purpose in bringing to light the nature of the distortion and its relationship to hum and circuit noise. The history of Fig. 8 is a striking example of this.

It is not unreasonable to suppose that there is a relationship between the shape of the diagram and the aural assessment of the resulting distortion. Indications of such relationship have been found, but

cannot be discussed here.

APPENDIX

Operational Procedure. The circuits of Figs. 3 and 4 are used for 4-terminal and 2-terminal tests respectively. Their operation will be described for a 1,000 c/s test tone. For tests at any other frequency the filters must be changed. The figures marked against the filters refer to the attenuation peaks adjacent to the cut-off points.

In setting up the difference diagram of an amplifier the first operation is to put 20 db at (4) and zero at (6) (see Fig. 3). Add attenuation at (3) to bring the overall attenuation from (3)-(6) to about overload point. (7) and slightly adjust (3) until the difference signal contains no fundamental tone. This will be shown by minimum vertical deflection of the oscilloscope trace. Turn up the gain of the X-amplifier of the oscilloscope to get a nearly horizontal line.

Now transfer attenuation from (4) to (6) thus driving (5) harder. The Y-deflection will grow and a loop will form. Adjust (11) until this loop closes to a line. When the input to (5) is small this line will resemble Fig. 2 if the output stage is a single valve. As the input increases a difference diagram like Fig. 5(a) will appear. The centre should be tangential to the X-axis of the tube. If not, adjust (3) very slightly to tilt the diagram correctly. If a loop appears as in Fig. 5(b) first adjust (7) and then (11) to remove it. The final curve is a representative difference diagram.

The phase shifter (7) should be designed to shift the phase without changing the amplitude of the 1,000-c/s signal, otherwise any adjustment will cause the diagram to tilt about its centre point and this has then to be corrected by readjusting (3).

The 2-terminal network is adjusted in much the same

way, except that (3) is adjusted initially to equal the

loss in (7) and (8).

In some amplifiers a change of operating regime occurs as the drive increases. This is shown up by a 4-terminal test but not by a 2-terminal test. The gain at 1,000 c/s alters and the diagram tilts about its centre point. The change in gain can be measured by introducing a slight

compensating loss in the (7) (8) chain to restore the diagram to its original position.

The most difficult adjustment is the setting of phase shifter (11). If there are "overload spikes" as in Figs. 10 and 11 there is no difficulty, for it is clear that these must be located at the extremities of the X-axis. Sometimes artificial "spikes" have to be introduced (by a biased-off diode or rectifier) before the correct setting of (11) can be found.

When, as in Figs. 9(c) and (d), the "go" and "return" traces are different and have to be displayed separately for examination, the diagram is opened into a loop by

a slight readjustment of (7).

If oscillator (15) uses a 2-valve zero-phase-shift RC circuit, it can be locked by injecting the "spike" from (14) into the common anode lead. No frequency calibration is needed, since the harmonic number can be read from the trace which appears when the output of (15) is made large enough. The magnitude of the spike signal must be adjustable so that it locks the oscillator without introducing visible distortion.

Cancellation of the unwanted distortion term can be observed on headphones connected temporarily to the output of the Y-amplifier of the oscilloscope. Phaseshifter (12) can be of a simple type in which the output voltage is not strictly independent of the phase adjust-ment, for the size of the locking "spike" will not seriously

affect the output of the oscillator (15).

EARL'S COURT

Preliminary List of Exhibitors

AS a result of the recent ballot for space at the 20th National Radio Show to be held at Earl's Court from September 1st to the 12th, the Radio Industry Council has issued a preliminary list of exhibitors. In addition to the 80 manufacturers, traders and journals, etc., listed below, four banks, British Railways, the Electrical Trades Union, and the Association of Radio Battery Manufacturers have also taken space.

turers nave also taken space.

Aerialite, Ambassador, Antiference, Argosy, Automatic Coil Winder.

B.B.C., Baird, Balcombe, Belling & Lee, Bernards, Boosey & Hawkes,
Bowmaker, Brown Brothers, Bulgin, Bush.

C.W.S., Cole, Collaro, Cosmocord, Cossor.

Decca, Dubilier, Dynatron.

Econasign, Edison Swan, English Electric, Ever Ready, Electrical

& Radio Trading.

Ferguson, Ferranti.

G.E.C., Garrard, Goodmans, Gramophone Co.

Hobday, Hunt.

Invicta.

Invicta.

J.B. Manufacturing.
Keith Prowse, Kerry's, Kolster-Brandes.
Linguaphone, Lugton.
McMichael, Marconiphone, Masteradio, Mullard, Multicore, Murphy.
Peto Scott, Philico, Philips, Pilot, Plessey, Portogram, Practical
Wireless, Pye.
R.G.D., Regentone, Reproducers, Roberts, Rola-Celestion.
S.T.C., Simon Sound Service, Sobell, Stella.
T.C.C., Taylor Electrical Instruments, Telerection, Thompson,
Diamond & Butcher, Truvox.

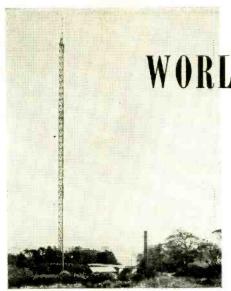
Diamond A Tultra.

Ultra.
Valradio, Vidor.
Westinghouse, Whiteley, Wireless World and Wireless Engineer,
Wireless Trader, Wolsey, Wright & Weaire.

public from September 2nd, include considerable space for displays of radio and electronic equipment to be provided by the Services and manufacturers. It is also planned to have an educational and training exhibit on the lines of that introduced last year. Technical training colleges will be represented by Norwood T.C. and the Borough Polytechnic and industrial training establishments by E.M.I. Institutes and Marconi College. The B.B.C. Engineering Training Department will be participating and the universities will also be represented.

Many of the exhibitors will be equipping demonstra-tion rooms and there will be the usual Television Avenue in which manufacturers have the opportunity of demon-

strating their receivers.



New TV Stations

THE temporary low-power mobile stations at Glencairn (Belfast) and Pontop Pike (Newcastle) were brought into regular service by the B.B.C. on May 1st. Pontop Pike is linked with the main radio network, but Glencairn relies on its direct reception of the Kirk o' Shotts transmitter for rebroadcasting. Initially, the Newcastle station used a temporary aerial, but the main radiator, which will eventually be employed by the permanent medium-power transmitter, is now in use.

Both stations use horizontal polarization and their sound and vision carriers are slightly offset from those of the main high-power transmitters using the same channel to reduce interference. Glencairn, shown with its Marconi aerial in the above photograph, operates in Channel 1 (41.5 and 45 Mc/s), and Pontop Pike in Channel 5 (63.25 and

66.75 Mc/s).

The low-power booster station near Brighton started a regular service on May 9th. It uses vertical polarization, operates in Channel 3 (53.25 and 56.75 Mc/s) and relies on its direct reception of Alexandra Palace for rebroadcasting.
As in the case of the other two low-power stations, Brighton's carriers are slightly offset.

MSF Schedules

STANDARD FREQUENCY transmissions from the Rugby station MSF are now being radiated continuously for 24 hours a day. In accordance with the Atlantic City Convention (1947), the carrier frequencies will be 2.5, 5, 10, 15 and 20 Mc/s, but only three of these will be used simultaneously. Initially the transmissions are being radiated on 2.5, 5 and 10 Mc/s with a power of 0.5 kW.

These frequencies are not the most suitable for reception within the United Kingdom and it has, therefore, been decided to continue the transmissions on 60 kc/s for a short period each day. A power of 10 kW will be used for this transmission which will be radiated from 1429 to

1530 G.M.T.

The carriers will be modulated in accordance with the following cycle (repeated each quarter of an hour): 0-5 mins, 1,000 c/s tone; 5-10 mins, 1 c/s pulses (59th pulse in each minute being omitted); 10-14 mins, unmodulated; and 14-15 mins, speech announcement. The carrier and modulating frequencies are derived from the same 100kc/s standard and are maintained to within ± two parts n 10⁸ of their nominal values.

Results of N.P.L. measurements of these transmissions

are given each month in our sister journal Wireless

Engineer.

WORLD OF WIRELESS

Mobile Television Transmitters . Standard Frequencies • New Amateur Band

Coronation Radio

BIGGEST-EVER radio hook-up has been planned by the B.B.C. for the Coronation Day broadcasts. In addition to the television arrangements (which include the relay to Europe detailed on pages 274 and 275) and those for home listeners, the entire transmitting equipment of the External Services of the Corporation will be employed. This includes thirty-six high-power and two medium-Ans includes thirty-six high-power and two medium-power short-wave transmitters in this country, six in Malaya, two in Canada and two in Ceylon as well as m.w. transmitters in this country, Germany and Austria. The B.B.C. has also been asked to provide land lines for a large number of overseas broadcasting authorities, while many other countries are retropositing the

while many other countries are retransmitting the received programme. It is estimated that in all some 1,000 stations throughout the world will be broadcasting some part of the day's proceedings. Eighty-four microphone positions for commentaries in 44 foreign languages

have been provided by the B.B.C.

Amateur 2-Mc/s Band

SINCE MAY 1st amateurs in the U.K. have not been permitted to use the band 1715-1800 kc/s, but instead have been granted the 200-kc/s band above 1800 kc/s. This change was necessitated by the enforcement of part of the Atlantic City allocation table and the Geneva fre-

quency plan covering that band.

It will be recalled that in the Atlantic City Radio Regulations there was no 2-Mc/s allocation in Region I (Europe and Africa) for amateurs. A footnote to the frequency allocation table, however, reads "In the band 1715-2000 kc/s, Austria, Ireland, the Netherlands, Northern Rhodesia, Southern Rhodesia, Switzerland, the Union of South Africa and the United Kingdom may assign up to 200 kc/s for the amateur service provided that the mean power of any amateur station does not exceed 10 watts and that no harmful interference is caused to the authorized services of other countries.

The Radio Society of Great Britain in giving details of the change lists the maritime stations (see p. 214 of our last issue) in the band which are likely to be particularly vulnerable to interference.

"Trader Year Book"

THE "Wireless and Electrical Trader Year Book, 1953," to give it its full title, is a veritable mine of information—technical, legal and general—for the radio and electrical trader. This 24th edition includes thumbnail specifications of current broadcast and television receivers, i.f. values of broadcast receivers marketed between 1947 and 1951, valve base connections and mains voltages in the principal towns in Great Britain. It also includes in its 264 pages directories of trade organizations, manufacturers, wholesalers and proprietary names. It is published by the Trader Publishing Co., Dorset House, Stamford Street, London, S.E.1, price 10s 6d.

Modern Navigational Aids

AN EXHIBITION "Navigation Today" has been arranged from now until September at the Science Museum, South Kensington, to show the basic principles of navigation and the changes which have taken place in navigational methods under the impact of high-speed flying and the developments of radio and radar.

There are demonstrations of such radio aids as Consol, Gee, Decca Navigator, v.h.f. omni-range, ground controlled approach and, of course, radar. The latter includes an interesting supersonic simulator by Kelvin and Hughes of the Thames approaches in which model craft in motion on water are reproduced on a standard p.p.i. display.

Firms contributing to the exhibition include S. G. Brown, Cossor, Decca, G.E.C., Kelvin and Hughes, Kolster-Brandes, Marconi, Siemens, Sperry and Ultra.

PERSONALITIES

Wing Commander R. Stanford-Tuck, D.S.O., D.F.C., who joined Marconi's W.T. Co. in 1949, and earlier this year was appointed sales manager of the Aeronautical Division, has been released by the company to join the Aircraft Division of the English Electric Co. Marconi's is a member of the group of which English Electric is the parent company.

H. R. L. Lamont, Ph.D., M.A., B.Sc., A.M.I.E.E., has recently joined the scientific staff of the European Technical Representative of the Radio Corporation of America whose office is in London. Dr. Lamont, who is well known for his book on waveguides, will be principally concerned with technical liaison. Until his present appointment he was senior lecturer in electronics at the Royal Technical College, Glasgow, and was formerly at the G.E.C. Research Laboratories, Wembley.

C. L. G. Fairfield, M.A., M.I.E.E., A.M.I.Mech.E., who has joined the Telegraph Construction and Maintenance Co., Ltd., as manager of the overseas division, had been with Mullard, Ltd., since 1947, latterly as manager of the valve division. He has been a director of Mullard Equipment, Ltd., for the past two years, and was a Mullard representative on the board of Telcon Telecommunications, Ltd.



Wilfred Sampson, B.A., A.M.I.E.E., has been appointed commercial manager of Teleon Telecommunications, Ltd. (owned iointly by Mullard, Ltd., and the Telegraph Construction and Maintenance Co., Ltd.). A graduate of Queen's, Cambridge, Mr. Sampson joined the transmission systems division of Standard Telephones and Cables, Ltd., in 1929, where he gained wide experience in the field of telecommunications both in this country and abroad, particularly in South Africa.

J. Foster Veevers, M.I.E.E., has resigned his recent appointment as general manager of the Swindon factory of the Plessey Company to become managing director of Peto Scott Electrical Instruments, Ltd. Before joining Plessey's he was for many years manager of the Stockport factory of Salford Electrical Instruments, Ltd.

Until his recent appointment as senior liaison engineer of the Components Division of the Plessey Co., E. Morgan, B.Sc., A.M.I.E.E., had been in the Engineering Division of the B.B.C. since 1950. He had held the positions of superintendent engineer (transmitters) and assistant head of the Valve Section. Before joining the Corporation he was a member of the technical sales staff in the Osram Valve Department of the General Electric Co.

OUR AUTHORS

Ralph W. Hallows, who has been a frequent contributor to Wireless World for the past 21 years, writes in this issue on the efficiency of the dry cell and suggests ways in which its design and construction might be improved. He has been European Consultant to the Burgess Battery Co. Inc. since 1925. During the war he was a major in the Royal Artillery and became chief instructor (radar) at the 6th A.A. Group School. Major Hallows, who was an open exhibitioner at Magdalene College and an honours M.A. (Cantab.), is author of a number of books including "Radar Simply Explained" which has been translated into six European languages.

E. R. Wigan, who writes in this issue on the diagnosis of distortion, spent some 14 years in industry (graduating from d.c. and 50 c/s on the test beds of the G.E.C., Witton, in 1924 to audio and carrier frequencies in the laboratories of Siemens Bros., Woolwich, before joining the Signals Research and Development Establishment, Ministry of Supply, in 1938. At S.R.D.E. he was primarily concerned with the design of acoustic and a.f. field equipment and the associated test gear. Since 1949 Mr. Wigan has been in the B.B.C. Research Department, Kingswood Warren, Surrey, dealing with problems associated with distortion.

Eric Griffiths, contributor of the article on the design and construction of portable equipment in our last issue, is in the Lines Department of the B.B.C. Since joining the Corporation in 1941 he has worked at both transmitter and studio centres, and was for some time an instructor in the Engineering Training Department. Before joining the B.B.C. he was in the Research Laboratory of Callender's Cables (1936-39) and with the Ministry of Supply (1939-41).

OBITUARY

It is with regret that we record the sudden death of **Simon Orde**, manager of the B.B.C. Engineering Information Department, on April 23rd at the age of 59. Mr. Orde joined the Corporation in 1942 as a censor and in 1943 transferred to the Engineering Division.

We record with regret that Charles Walter Eve, a former director of Standard Telephones and Cables, Ltd., and a director of Kolster-Brandes, Ltd., died on April 19th aged 66. He joined S.T.C. in 1906 and retired in 1947. Mr. Eve was closely associated with the formation of the Radio Industry Council, the Radio Communication and Electronic Engineering Association and the Telecommunication Engineering and Manufacturing Association, and was at one time vice-chairman of the British Radio Valve Manufacturers' Association.

IN BRIEF

Broadcast Receiving Licences totalled 12,892,231, including 2,142,452 for television sets and 183,996 for car radio at the end of March. The month's increase in television licences totalled 69,472.

Stand-by Equipment has now been installed at the Sutton Coldfield television station and the switching arrangements permit it to be used with either the main or stand-by aerials. The powers are vision 5 kW, sound 2 kW. The last of the main stations to be equipped with stand-by gear is Alexandra Palace, where similar Marconi transmitters are now being installed.

Radio Exports.—Of the £2.2M worth of radio equipment exported in March, £855,084 was for capital goods—transmitting gear, etc. According to Customs and Excise figures, components and test gear accounted for £454,580, domestic receivers £442,072, sound reproducing equipment £253,128, and valves £216,531.

Plastics Exhibition.—Among the 90 exhibitors at the British Plastics Exhibition, which will be held at Olympia from June 8th to 18th (10 a.m. to 6 p.m. daily) are the following radio and electronic manufacturers:—E. K. Cole, G.E.C., Radio Heaters, Redion and T.C.M. Admission to the exhibition costs 2s 6d, but free tickets for the convention which runs concurrently with the show are available from British Plastics (the organizers), Dorset House, Stamford Street, London, S.E.1.

Instruments.—The second British Instrument Industries Exhibition opens in the National Hall at Olympia on June 30th for 12 days. The Scientific Instrument Manufacturers' Association is among the five supporting organizations. The exhibition will be open daily, except Sunday, from 10 to 6.30.

Canadian Trade Fair.—Eight British publishers are combining to present a display of 55 technical, trade and specialized journals at the sixth Canadian International Trade Fair, to be held in Toronto from June 1st to 12th. Our own publishers will be exhibiting 24 journals including Wireless World and Wireless Engineer. Among the British companies participating in the fair is the G.E.C., who will be exhibiting the BRT400E communication receiver and v.h.f. gear.

Communications in the widest sense will be featured at the German Communication and Transport Exhibition which opens in the 670,000-sq yd Munich Exhibition Park on June 20th. The exhibition, which will remain open until October 11th, will include sections devoted to broadcasting, radio-telegraphy and telephony and navigation.

German Radio Show, which was to have been held last August and has twice been postponed, will open in Dusseldorf on August 29th for nine days.

A.P.A.E. Officers.—At the annual general meeting of the Association of Public Address Engineers, L. W. Murkham was re-elected president. The vice-presidents are A. V. Sharp, J. F. Doust, C. Clarabut (who is also chairman of the Council), A. H. Middleton and Alex J. Walker, who is also honorary general secretary. The Council consists of G. F. Baker, A. B. Hulme, W. O. Mannerings, A. E. Buchan, F. Hedges, A. E. Ward, R. Jackson and S. W. Lewis (trade members), and R. E. Owen, J. F. Doust, F. Poperwell, S. Norley, A. V. Sharp, S. Kelly, C. T. Wright and P. Whiteley (manufacturing members).

"Solid-State Electronics," which is at the foundation of such practical applications as germanium diodes, transitors and other semi-conducting devices, will be dealt with by Dr. Karl K. Darrow of Bell Telephone Laboratories, in a series of four lectures at King's College, Strand, London, W.C.2, at 5.30 on June 22nd, 23rd, 25th and 26th. Although the lectures are addressed to students of London University, admission is free to others interested in the subject.

Transistor circuitry and applications will be dealt with by G. C. Sziklai of the R.C.A. Research Laboratories, Princeton, U.S.A., at a meeting at the Royal Society of Arts, John Adam Street, London, W.C.2, at 5.30 on July 1st. Dr. R. L. Smith-Rose will be in the chair. Tickets are available from the R.C.A. European Technical Representative, The Tower, Brook Green Road, London, W.6.

Electro-Acoustics.—A series of 10 lectures covering the nature, generation, propagation, measurement, recording and reproduction of sound has been planned by the Department of Radio and Musical Instrument Technology at the Northern Polytechnic, Holloway, London, N.7. The lectures by E. H. Jones, B.Sc., A.M.Brit.I.R.E., will be given on Tuesdays and Thursdays, commencing on June 4th. The fee is two guineas.

Fringe-area Reception.—A series of papers on this subject will be given at the summer meeting of the Television Society, which will be held at Bedford on June 27th.

Photographing TV Pictures.—Readers interested in the photographing of television pictures from the cathode-ray tube may like to know that in the Coronation number of Amateur Photographer (May 27th) there is an article dealing with the subject.

"Designing a Tape Recorder."—In the complete circuit diagram (Fig. 7, p.231, May issue) the cathode resistor R_{26} of V_o should be 470 ohms and in Fig. 4 (p. 165, April issue) C_{27} should be 0.5nF.



SIR NOEL ASHBRIDGE. The Radio Industry Council is to present him with this portrait by Frank O. Salisbury. Sir Noel was recently elected an honorary member of the Brit.I.R.E. "in recognition of his services to the radio engineering profession of Great Britain and as a tribute to his outstanding work in developing the technical services of the B.B.C."

LITERATURE

Engineering Education.—A booklet setting out the full-time and part-time courses in technical education available at colleges and institutes in London and the Home Counties has been issued by the Regional Advisory Council for Higher Technological Education. It includes a list of courses in radio and television servicing, in telecommunications for the C. & G. certificates and in electrical engineering for the Higher National certificate. It is available from Tavistock House South, Tavistock Square, London, W.C.1, price 1s.

Metric Edition of the British Standard for enamelled round copper wire (oleo-resinous enamel) has recently been published as B.S.1961:1953. It differs from the 1951 edition of B.S.156 only in that all quantities are expressed in metric units. Copies may be obtained from the British Standards Institution, 24, Victoria Street, London, S.W.1, price 4s.

Technical Papers issued by all departments of the Department of Scientific and Industrial Research, including the National Physical Laboratory and the Radio Research Station, are listed in the 31-page catalogue "Government Publications, Sectional List No. 3 D.S.I.R.", revised to March 1st. It is obtainable free from H.M. Stationery Office, York House, Kingsway, London, W.C.2.

Scientific Literature published by and for the Institute of Physics is listed in a catalogue which is obtainable gratis from the Institute, 47, Belgrave Square, London, S.W.1. A summary is given of some 30 books, monographs and pamphlets including "Physics as a Career" by N. Clarke, which deals with the fields of work open to physicists and the training necessary.

BUSINESS NOTES

Emitron Television, Ltd., are to supply two flying-spot film channels for the new television station being built by the Italian broadcasting organization (Radio Audizioni Italiano) at Turin. They will operate on 625 lines and are fitted with magnetic heads for reproduction of sound tape recordings. Either married or single picture and sound films can be used.

Mullard is to transfer the manufacture of cathode-ray tubes from its factory at Mitcham, London, to a new Government-financed factory of approximately 250,000 sq ft to be built in the North-East Lancashire Development Area. The vacated space at the Mitcham factory will be utilized for the production of other electronic devices.

B.I. Callender's Cables, Ltd., have formed a new company in Australia to co-ordinate the activities of agents in the Commonwealth and to establish a technical service organization. The registered office of British Insulated Callender's Cables (Australia), Pty., Ltd., is 84/88, William Street, Melbourne, C.I., Victoria, Australia. B.I.C.c. has also formed a Canadian company. It has acquired the business of Phillips Electrical Works, Ltd., of Montreal and Ontario, which will now be known as Phillips Electrical Company (1953), Ltd.

Modern Acoustics, Ltd., of Manor Way, Boreham Wood, Herts, (Tel.: Elstree 3636), has been formed to manufacture "Lectrona" loudspeakers which were previously produced and marketed by Acoustic Products, Ltd. E. L. Edwards, late of Edstone, Ltd., is managing director of the new company.

Mattis Industries, Ltd., of 4, John Adam Street, London, W.C.2, (Tel.: Trafalgar 5502), inform us that they have been appointed sales representatives for London and the Home Counties for the "Milaflex" range of insulating silks, tapes and cloths manufactured by Miller & Ferguson, Ltd., of Glasgow.

Decca's Glasgow office, which deals with both radar and navigation business, is now at 67, Blythswood Street, Glasgow, C.2, (Tel.: City 6457/8). The manager is R. E. G. Simmons.

London Docks servicing depot of Rees Mace Marine, Ltd., is now at Yabsley Street, Poplar, E.14, (Tel.: East 4216). It is under the management of R. Aveyard.

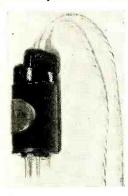
Exporting Computers.—The second electronic digital computer to be produced by Ferranti, Ltd., for export has been ordered by the Royal Dutch/Shell Group for installation in their research establishment in Amsterdam.

B.T.H. has received an order from the European Headquarters Command of the U.S. Army for \$4M worth of mobile fire-control radar equipment for supply to N.A.T.O. countries.

Marconi Marine radio and navigational equipment is being supplied by Marconi's associates Deutsche Betriebsgesellschaft für Drahtlose Telegrafie M.B.H., for four motor vessels being built at Rendsburg on the Kiel Canal.

TRANSISTOR AMPLIFIER

PROBABLY the first piece of commercial apparatus on the British market to make use of a transistor is a small pocket amplifier for boosting the outputs of hearing-aids.



Designed by Multitone, it is intended for hearing-aid users who get adequate output from close-range sounds but not enough from sounds at a distance. The G.E.C. Type GET1 point transistor used gives a power gain of about 15 db, and it has to be used with a high-impedance earpiece which is supplied with the instrument. The cylindrical housing has a plug at one end to fit into a standard hearing-aid battery $(22\frac{1}{2} \text{ V} \text{ or } 15 \text{ V})$, and two sockets at the other for the input and output plugs and cords. Multitone have also

produced a hearing-aid with a transistor output stage, the main object being to reduce l.t. consumption.

No More "Reliable" Valves

VALVE manufacturers in this country deplore the use of the term "reliable valves" because it implies that all other valves are not reliable. Their trade association, the B.V.A., now announces that it intends to describe these valves as "Special Quality" in future. A "Special Quality" valve is defined as "a valve which has certain design and manufacturing features making it suitable for use under conditions different from or in excess of those experienced in normal radio or television receivers and when operated under stated or agreed electrical or mechanical conditions it has an acceptable statistically determined expectation of life."

This definition covers several classes of valves, for example, those which will withstand severe mechanical shock but do not necessarily have long lives; those which have particularly long lives or high electrical stability but not so much ability to withstand shock; and those giving normal lives under moderate conditions of shock and vibration. Thus the term "Special Quality" has quite a wide meaning, and does not really distinguish the particular class of valves hitherto known as "reliable" from valves with other special qualities such as long life or stability.

Books Received

Television Picture Faults. By John Cura and Leonard Stanley. Contains 150 photographs of television pictures illustrating various faults together with explanations of their cause. These explanations are printed in contrasting types for readers with and without technical knowledge. The faults mainly comprise those resulting from incorrect adjustment of the controls, but various forms of interference are also illustrated. Pp. 68. Television Times, Ltd., 39a, Bartholomew Close, London, E.C.1. Price 3s 6d.

Radio Engineering (Second Edition). By E. K. Sandeman, Ph.D., A.C.G.I., M.I.E.E. Method of approach is fundamental and general, though specifically related to practical ends. The book grew from an instruction manual written primarily for maintenance engineers at B.B.C. stations. Pp. 613+xxi; Figs. 204. Chapman and Hall, 37, Essex St., London, W.C.2. Price 55s.

Télévision Dépannage. By A. V. J. Martin. A practical book on the installation, adjustment, fault-tracing and

repair of television receivers. Pp. 176; Figs. 197. Société des Editions Radio, 9, Rue Jacob, Paris, 6. Price 600 francs.

Modulators and Frequency-changers. By D. G. Tucker, D.Sc. An analytical and largely mathematical approach to the subject as applicable to amplitude-modulated radio and line systems. The book is intended for design and maintenance engineers. Pp. 218+xiv; Figs. 115. Macdonald and Company, 16, Maddox St., London, W.1. Price 28s.

The Living Brain. By W. Grey Walter, M.A., Sc.D. (Cantab). Basically a book about research into the mechanics of the brain by means of electro-encephalography (and intended for general reading), but contains technical information on EEG apparatus developed by the author with appendices describing his electronic analogues of physiological mechanisms. Pp. 216+xii; Figs. 23. Gerald Duckworth & Co., 3, Henrietta Street, Covent Garden, London, W.C.2. Price 15s.

"Radio Designer's Handbook"

MANY thousands of copies of earlier editions of "Radio Designer's Handbook" have been sold throughout the world. The fourth edition of this popular work, just issued by our Publishers (price 42s; by post 43s 6d) is more than four times as large as its predecessors. The book deals in detail with basic principles and the practical design of all types of modern radio receivers, audio amplifiers and record-reproducing equipment. It is the work of 10 authors and 23 collaborating engineers, under the editorship of F. Langford-Smith.

CLUB NEWS

Birmingham.—The June programme of the Slade Radio Society includes two direction-finding contests. On the 12th there is to be an evening contest and on the 13th-14th the second event for the Harcourt Trophy. There will be a technical discussion evening on the 26th at 7.45 at Church House, Erdington. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

Coventry Amateur Radio Society's "night on the air" has been suspended for the summer months, but meetings continue to be held on alternate Mondays at the Y.W.C.A., Queens Road, at 7.30. On June 8th G2BVW will talk about 70-centimetre operation. There will be a v.h.f. field-day on Sunday, June 21st. Sec.: K. G. Lines (G3FOH), 142, Shorn-cliffe Road, Coventry.

Hastings and District Amateur Radio Club, of which L. H. Thomas, M.B.E. (G6QB), assistant editor of Short Wave Magazine, is president, is participating in the Hobbies Exhibition to be held in the town during Carnival Week, July 4th-11th. Membership of the club, which during the summer meets only once a month, is now over 30. Sec.: W. E. Thompson, 8, Coventry Road, St. Leonards-on-Sea.

Manchester.—The South Manchester Radio Club (G3FVA) meets on alternate Fridays at 7.30 at Ladybarn House, Mauldeth Road, Fallowfield, Manchester, 14, and is planning a course of instruction for the Radio Amateur Examination. Sec.: M. Barnsley (G3HZM), 17, Cross Street, Bradford, Manchester, 11.

Reading.—Meetings of the Reading Radio Society, of which W. A. Smallcombe, B.Sc., was recently elected president, are held on the second and last Saturdays of each month at 7.0 at the Abbey Gateway, Reading. The programme for the coming session includes lectures, debates and demonstrations. Sec.: L. A. Hensford (G2BHS), 30, Boston Avenue, Reading.

Southend.—At the meeting of the Southend and District Radio Society on June 12th S. W. F. Asquith, A.M.I.E.E., will talk on frequency measurement. The winners of the recently awarded Pocock and Hudson Cups for home-built gear—J. Wallace and D. Whitworth, respectively—will demonstrate their equipment at the meeting on June 26th. Meetings are held on alternate Fridays at 7.30 in the Queen's Road Annexe of the Municipal College, Victoria Circus. Temp. Sec.: J. H. Barrance, M.B.E. (G3BUJ), 49, Swanage Road, Southend-on-Sea.

LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

Two-band Television Reception

WHEN alternative television programmes are provided, whether by the B.B.C. or by sponsoring or by both, it is plain that the new stations must operate on frequencies higher than the present 40-70 Mc/s band. New television sets will be designed to cover the new band as well as the old and must obviously include some station-selection

The problems of design are technically straightforward ones, but what about the several million existing sets? Has anyone yet thought seriously about the problem of making them suitable? The usual glib answer is that cheap, mass-produced converters will be produced which will enable the frequency of the new station to be changed to that for which the receiver is designed.

That is a satisfactory solution provided that the converter does what it is supposed to do, but will it? It seems to me that there are a great many technical snags.

It so happens that most existing television sets are not readily tunable from one channel to another and some cannot be changed at all without a major operation. In order that normal reception of the station in the 40-70 Mc/s band may be retained, therefore, the receiver must be left tuned to this station and the converter must operate to change the frequency of a signal in the higher band to this lower frequency. There is then a possi-bility of interference due to the direct pick-up of signals from the 40-70 Mc/s station by the early circuits of the receiver. For the avoidance of interference a disparity of some 50 db between the two signals is required. In some areas and with some receivers this may be easily obtainable, but when the receiver is used near a 40-70 Mc/s station and remote from one of the new ones, the interference may well be intolerable. This is especially likely to be so with some of the earlier receivers which were not very well screened.

The solution would seem to lie in having the television set permanently tuned to a channel other than the local one-say to Sutton Coldfield in the London area-and to include in the converter provision for changing the frequency of the local 40-70 Mc/s station to this chosen channel. The converter then becomes necessary for all reception. This will increase its cost and the changing of the tuning of the set itself may be an expensive matter with some sets, although negligible with others.

In addition to this, where the television set is a superheterodyne, as most now are, the set plus converter will be a double superheterodyne having two oscillators. The almost limitless possibilities of self-generated interference by beats between their harmonics are well known and it seems likely that satisfactory operation would be largely a matter of chance and would depend on the precise frequencies of the signal, the input of the set (1st i.f.), the i.f. of the set (2nd i.f.) and upon whether the oscillator of the television receiver is above or below the signal. The converter oscillator will have to be always below the signal to prevent inversion of the sound and vision channels.

The development and rapid growth of competitive television services will depend very much on the finding of satisfactory solutions to all these problems. London, N.14. W. T. O

W. T. COCKING.

Broadcast Transmitter Distortion

THE letters of Ian Leslie in your April issue and A. Yates in your May issue both deal with the overall performance of the broadcasting chain, and a few notes on B.B.C. practice may be of value.

There is, of course, no such thing as completely dis-

tortionless transmission, and the problem facing any authority engaged in broadcasting is to what extent shall distortion be permitted. If no restriction of volume range is used between microphone and transmitter, and the modulation is adjusted to such a level that 100 per cent modulation is never reached, then distortion may be very slight, but the average level of modulation will be extremely low, and listeners will rightly complain of excessive background noise due to interference and receiver noise in the quiet passages. For these reasons it is the practice in this and every other country to adjust levels manually so as to bring up the quiet passages and to keep down somewhat the level of the loud passages. This is done at the originating point in the programme chain. Sharp transients will, however, always occur, probably of such short duration as to be unobserved at the manual control position, and in any case so short as to make it impossible to take any human steps to limit their amplitude. In order to deal with this situation automatic means of amplitude limitation are incorporated at the transmitter input. These ensure that such transients cannot cause the transmitter to be modulated more than 100 per cent. Admittedly while so doing a certain amount of distortion is necessarily introduced by a very short period of time, but this distortion is very much less than that which would be heard by listeners if the transmitter were modulated more than 100 per cent. In that case the carrier amplitude would be reduced to zero for short periods of time and a very noticeable distortion radiated. Also, of course, heavy over-modula-tion can be very dangerous for the transmitting equipment.

The extent to which the average programme level is raised, and the extent to which limitation is used, is, of course, very much dependent on judgment of the degree to which distortion is acceptable, and on a balance being made between the amount of such distortion and the improvement in signal-to-noise ratio for the general listener. This improvement in signal-to-noise ratio is particularly important at times like the present, when on certain wavelengths there is appreciable interference from continental broadcasting stations.

The B.B.C. has arrived at its present standards after very careful listening tests, and believes that in the existing circumstances these represent the best compromise

between distortion and interference.

Within the restricted band of frequencies available for medium-wave broadcasting there seems to be no prospect whatsoever of any appreciable reduction in interference from stations in other parts of Europe, and in fact a probability that this may increase. To increase the power of the medium-wave stations is not permitted by the Copenhagen Plan, and in any case to increase by an adequate amount would in most cases be impracticable. The hope for future improvements in transmitting conditions lies therefore in the development of a v.h.f. broadcasting service. The B.B.C. has published the results of its experimental transmissions from Wrotham, and the development of a regular service is now under consideration by the Advisory Committee set up by the Post-master General under the terms of the Government White Paper on Broadcasting.

Mr. Yates is in error in stating that we rarely give live transmissions. Of the programmes radiated after 6 p.m. in the week ending May 2nd, recorded programmes represented 25 per cent of the Home Service, 40 per cent of the Light Programme, and 62 per cent of the Third Programme. In any case, for the vast majority of recorded programmes the quality of reproduction is indistinguishable from that of a live programme. continued introduction of new recording and reproducing equipment should in time eliminate all unsatis-

factory recorded items.

The quality of transmissions over the land lines from the studio to the various transmitters is subject to continual careful check. Only very occasionally does the quality of transmission deteriorate, and in such cases it is rectified at the earliest possible moment.

Consideration has been given to the use of the sound channels of the television service for the transmission of a sound programme, but the continued development of the television service and the fact that the equipment is in use for television purposes at times when the greater part of the public would wish to listen precludes such

use.

The conclusion drawn by Mr. Yates that the general average of performance has deteriorated in the last twenty years is, I think, not justified, as the improvements in the design of the equipment in the transmitting chain over the last twenty years have been very appreciable, while every care in the operation and maintenance of the equipment continues to be taken.

London, W.1. F. C. McLEAN. Deputy Chief Engineer, B.B.C.

I WAS interested to see A. Yates' letter, supporting my plea for better B.B.C. transmission quality, in your May

As regards the use of recordings, I wrote to the Director of the Third Programme last autumn deploring the trend towards the development of a "transcribed service" and pointing out that, apart from questions of optimum signal quality, those shortcomings which identify the medium used—rumble, regular clicks due to a scratch, the change in quality as between the end of one disc and the start of the next-produce a mental image of the revolving turntable and destroy the illusion of reality, that psychological factor so important in a live service.

In reply I was informed that the extensive use of recordings is both necessary and expedient in a comprehensive service. Further, I was invited to Broadcasting House and shown that on direct playback (pickup tracking the groove freshly made by the cutter, with monitor switched instantaneously to input line or replay amplifier at will) the reproduced signal is almost indistinguishable from the input signal and total background noise imperceptible. I was told, and it was evident, that deterioration in the signal finally radiated is due to deterioration in the equipment of the playback channels, and in the recorded discs, due to careless handling by staff other than that of the recording department. There can be no that of the recording department. excuse for this.

That improvement is possible in landline quality is indicated by the fact that excellent quality is in fact obtained from landline relays-sometimes. It is doubtful whether the use of television transmitters for sound services would serve any useful purpose in view of the fact that they would only be available at odd, "off-peak" hours. As regards the development of a comprehensive f.m. service, clearly the B.B.C.'s hands are tied by the financial powers-that-be.

Regarding automatic volume compression, the B.B.C.'s Parthian shot was a suggestion that I should see the matter in perspective; that "there is nothing more annoying than a strong carrier with low average modulation." I strongly disagree. Average level means nothing; minimum level matters but can be maintained by manual Various measures can be undertaken by the listener to improve signal pick-up and/or mitigate interference of all types, but nothing can be done to correct a signal that contains non-linearity distortion. aspects of the interference problem are out of the B.B.C.'s control, but radiated signal quality is entirely their responsibility; in this at least let them set their house in order.

London, N.10,

IAN LESLIE.

Flywheel Sync

THE observation made in the opening paragraph of K. G. Beauchamp's letter in the April issue on the fly-wheel synchronizing circuit, described by B. T. Gilling in your March issue, we consider to be incorrect when it is stated without reservation that neutralization of impulsive interference is effected across the common load resistance of the diodes. This is true during the sync period; i.e., when the fly-back has been initiated and point B (B. T. Gilling's Fig. 2) is neutral, but prior to the sync pulse the circuit does not appear to be immune to noise. For example, during the period between the middle and end of the scan, point B is negative and thus noise spikes appearing 180 degrees out of phase at V2(a) and V2 (b), anode and cathode respectively, will result in the greater conduction by V2 (a), and hence a positive signal voltage developed across the common load.

The operation of the d.c. amplifier, as shown in Fig. 5, is obscure, since the valve is without cathode bias and will be driven by positive excursions during the sync period into grid current which can find no d.c. path to

cathode.

We support your correspondent in identifying the circuit as a phase discriminator, and it is to be hoped that the discriminator as used in frequency modulation applications, which for so long has assumed a similar identity, will be regarded more correctly as a frequency discriminator. W. J. CROSSLEY, S. L. FIFE.

English Electric Company, Liverpool.

Lamp Interference

THE problem of lamp interference, raised by K. Robinson in your May issue, is quite well known, though it does seem extraordinary that a lamp with a continuous filament can give trouble.

Whilst the complete mechanism is, so far as I know, not fully understood, it is quite normal for vacuum lamps to act as quite powerful energy generators, and interference from them can cover a range of at least 4-mile.

The functioning of a lamp as a r.f. generator, and the frequency, depends on instantaneous voltage, and thus when a.c. is used the interference only occurs on certain parts of the voltage cycle, and the frequency also varies, this accounting for "herringbone" and similar effects.

Luckily, this phenomenon is restricted to vacuum lamps normally of 25 watts or more, and these lamps are only used in special installations, such as traffic signs and "keep left" bollards, and are not on sale to the general public. The "gasfilled" lamp is quite innocent. Enfield, Middx.

A. P. HALE.

"Designing a Tape Recorder"

REFERRING to the above article in your April issue, I should like to make two further suggestions for a level monitor. Both incorporate the refinement, particularly desirable in home-built equipment, of monitoring bias oscillator and audio output voltages simultaneously.

The first uses the two meters from an aircraft direction indicator (see Wireless World article of September, 1951, and remember the warning about beta radiation-January, Each meter is put in a bridge rectifier circuit which is fed through a high resistance from either the erase oscillator or the anode of the audio output valve. Because of the high sensitivity of these meters, there is no trouble

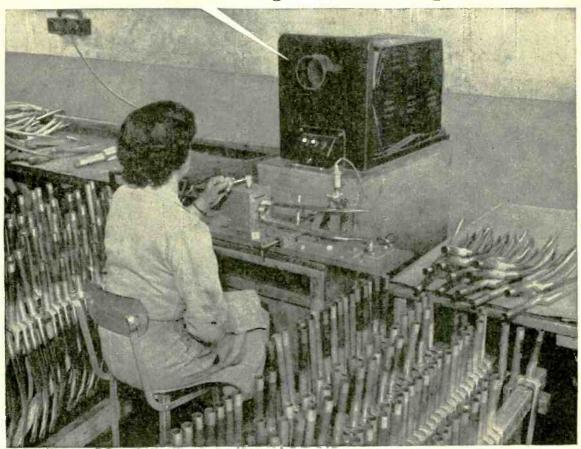
concerning the load they will put on the two outputs.

The second method is very suitable if a 500-volt h.t. line is available. A ICP1 type cathode ray tube is used as the indicating device, the oscillator volts being fed across one set of plates whilst the audio output is fed across the other. This gives a rectangular fluorescent area the width of which is proportional to oscillator output and the depth to audio output.

W. D. CUSSINS. Cussins and Light, Ltd.

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The B.S.A. Cycle Factory in Birmingham uses the Cossor Model 1035 Oscillograph for a vital production test.

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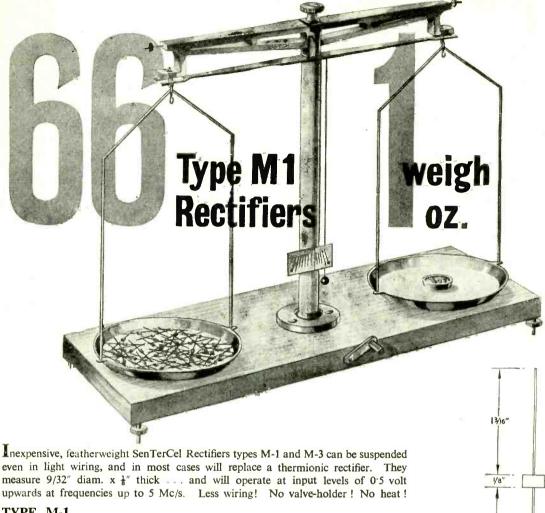
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Average characteristics :

Self Capacitance	200		22 pF
Forward resistance at 5 V D.C.			10 k Ω
Reverse resistance at 5 V D.C.		1	000 M Ω
Maximum peak inverse voltage			68 V
Minimum A.C. input			0.5 V

TYPE M-3

Has similar characteristics and application with a maximum frequency of 100 kc/s.

Average characteristics:

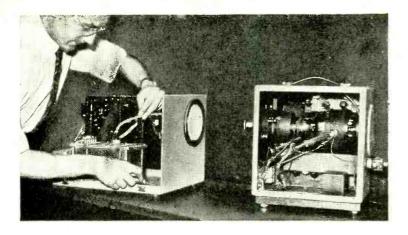
Self Capacitance			 65pF
Forward resistance at 5 V D.C.		****	 1.2 k Ω
Reverse resistance at 5 V D.C.			 45 M Ω
Maximum peak inverse voltage			 68 V
Minimum A.C. input	* * * *		 0.5 V



Standard Telephones and Cables Limited

Registered Office: Connaught House, Aldwych, London, W.C.2

RECTIFIER DIVISION: Warwick Road, Boreham Wood, Hertfordshire Telephone: Elstree 2401 Telegrams: SenTerCel, Borehamwood



Television Standards Converter

Mobile Equipment in Holland for the Coronation Relay

READERS will see from our route map of the Coronation relay to Europe (following page) that the British 405-line signals are converted to the continental 625-line standard at Breda in Holland. The converter equipment, designed by the Philips Research Laboratories at Eindhoven, is basically the same as that used by the B.B.C. at Cassel last year for changing from French to British standards-a c.r.t. monitor displays the incoming picture and this is viewed by a camera working on the new standards. The situation is rather different at Breda, however, in that the pictures are going in the opposite direc-tion and are being converted from a low number of lines to a higher number of lines. Moreover, the equipment is a good deal smaller than the B.B.C.'s, and is actually installed in a trailer—which also contains a reserve converter (in case of breakdowns) and a quantity of monitoring and test gear. This trailer is stationed outside a church known as the Grote Kerk in Breda, and from it cables run up the side of the building to the centimetre-wave transmitting and receiving equipments which are mounted on the steeple.

The smallness of the converter has been achieved mainly by the use of a c.r. tube with a screen diameter of only 5in to display the incoming picture. Normally, with a screen of this diameter, the definition would not be very good because of the relatively large size of the spot; but the tube is actually a flying-spot scanner with a very small spot and has a definition of 1,000 lines. The camera has an image iconoscope pick-up tube, and this is fitted with a mask at the edge of its viewing window to provide a black reference for the 625-line signal.

As in previous converter equipments, the monitor c.r. tube uses a long-persistence screen as a means of light storage. Without this, the camera pick-up tube would tend to act as a simple photo-cell and would respond to the instantaneous variations of intensity of the light spot. Thus it would produce a spurious waveform corresponding to the 405-line vision signal, and this would beat with the normal 625-line signal to give a completely meaningless output. With the long-persistence screen, however, a large component of unmodulated light is introduced, so that the intensity variations of the spot are made negligible in comparison and have little or no effect on the pick-up tube.

At the same time, of course, the persistence must not be made long enough to preserve one picture into the next picture period, otherwise blurring would occur with moving images. Actually the decay characteristic of the phosphor is such that the brightness of a point on the screen falls to about at the of its original value by the end of one frame period.

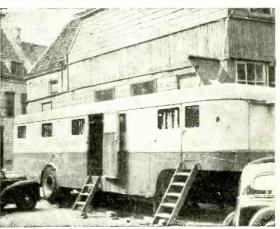
Another important point is that the scanning beam of the camera is arranged to "read" the picture at a moreor-less constant time interval behind the "writing" spot of the c.r. tube. (This is possible because, although the line periods of the two systems are different, the frame periods are the same.) If this were not done there would be a phase drift between the two scanning systems, and sometimes the camera would be "reading" the picture while it was still bright from the spot and sometimes while it was fading out a long way behind the spot, and the result would be that the outgoing picture would fluctuate in brightness. The two scanning systems are actually locked together by synchronizing the camera waveform generators with the frame sync pulses of the incoming 405-line signal.

Since the conversion is from a low number of lines to a higher number, it has been necessary to "fill in the gaps" in the 405-line picture by spot-wobbling. Without this device, the scanning lines of the camera would sometimes coincide with those of the 405-line picture and sometimes fall between them, and an interference pattern would appear on the outgoing picture.

would appear on the outgoing picture.

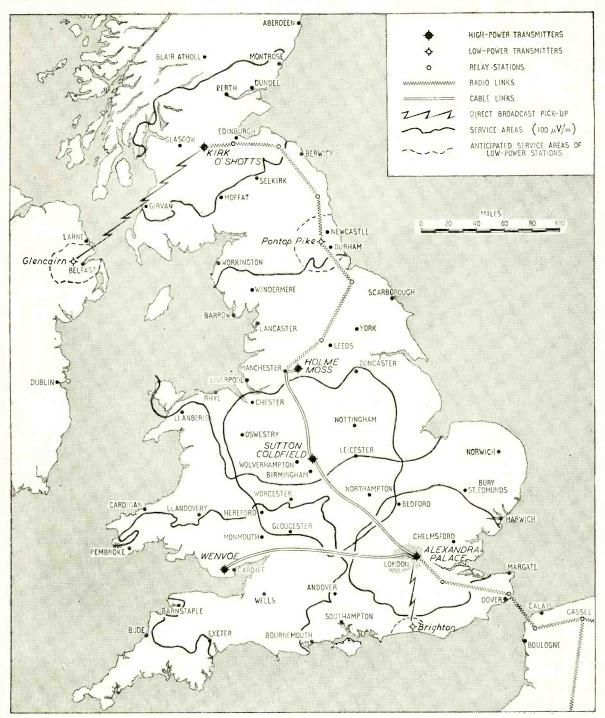
Recently Wireless World had an opportunity of seeing the converted pictures at Amsterdam, after they had been transmitted from Lopik, and we were agreeably surprised by their quality. Inevitably there was some degradation, but not enough to worry the average viewer, and we have seen worse on receivers in this country.

The converter equipment, with the monitor unit on the left and the camera on the right, is shown above, and below is the trailer in which the equipment is installed.



International Television:

Radio and



With the recent opening of the temporary, mobile, low-power television stations at Glencairn (Belfast) and Pontop Pike (Newcastle) and the booster station near Brighton, approximately 80% of the population are now within the B.B.C. television service area, indicated on this mab by the $100\mu V$ m contours. The estimated coverage of the Glencairn transmitter, which relies on its direct reception of Kirk o'Shotts, is Belfast and its immediate surroundings. Using the permanent aerial, Pontop Pike serves an area within a radius of approximately 20 miles of the transmitter. The Brighton booster station, which re-transmits the Alexandra Palace transmission, is intended to serve the town and district.

Cable 2,000-mile Network for the Coronation Transmissions

THE international exchange of television programmes has been brought a stage nearer by the unqualified success of the recent tests conducted on the Continent, preparatory to the re-radiation of the B.B.C. Coronation day transmissions by stations in France, Holland and Western Germany. On these two pages we reproduce sketch maps of the British Isles and northern Europe showing the 2,000-mile radio and cable network which will convey the B.B.C. television transmissions on June 2nd to viewers in four countries. On the opposite page is shown the complete chain of British television stations, the methods of linking and the service areas of each of the five high-power and three low-power transmitters now in use.

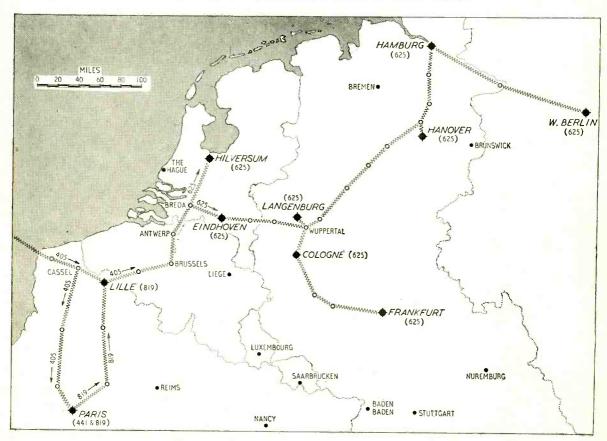
For the continental relay the vision signal will be transmitted from London to France by relay stations provided by Standard Telephones & Cables, Ltd. It will be picked up at a point near Cap Blanc Nez, Calais, and re-transmitted to Cassel. It will be seen from the map that the 405-line signal is carried by the French P.T.T. and Radio-diffusion et Télévision Françaises south from Cassel to Paris for conversion to 441 and 819 lines for re-transmission by Paris and Lille. The 405-line signal is also carried east from Cassel to Lille where it is conveyed over a chain of centimetre-wave links across Belgium, which has not yet a television service. It is, however, planned to monitor the transmission in Brussels where a

limited number of people will see the 405-line picture probably on large-screen equipment.

The key point for the 625-line transmissions by the Dutch and West German stations is Breda, where, as described on page 273, the Philips organization has set up a conversion unit. The 625-line signal will be taken by direct links to Hilversum and Eindhoven and via four centimetre-wave relays to Wuppertal to be fed into the permanent network recently inaugurated by the Nordwestdeutsche Runfunk to link the five N.W.D.R. television stations. The longest hop in this chain of relay stations is that linking the Berlin transmitter with the last station in Western Germany—a distance of nearly 100 miles. The frequency used for this hop is 196.25 Mc/s. In addition to the five N.W.D.R. stations the Frankfurt transmitter in the American Zone and possibly the Weinbiet station near Baden Baden (French Zone) will be radiating the 625-line transmission.

The complementary sound transmissions will be carried by cable to the Continent, where broadcasting organizations will have the choice of two of the following three circuits: 1, background sound free from any commentary; 2, English commentary; and 3, French commentary. It will, therefore, be possible for Dutch and German commentators to hear the English or French commentary which they can then translate for superimposition on the background sound.

Centimetre-wave links covering some 1,200 miles form the chain for the re-transmission of the B.B.C.'s Coronation day broadcasts by Continental television stations. Against each transmitter is indicated the standard employed.



Improving the Dry Cell

Making Better Use of the Raw Materials

By R. W. HALLOWS, M.A.(Cantab), M.I.E.E.

HEN zinc was plentiful and little accounted, a run-down dry battery, whose cell-cans might still contain from two-thirds to four-fifths of their original weight of the metal, could be thrown light-heartedly into the dustbin. To-day, there is a world shortage of zinc, and it is a matter of some importance that it should not be used wastefully. The dry Leclanché cell, which has proved itself to be the most convenient, the least messy and the most foolproof source of what the late Dr. C. F. Burgess aptly termed portable power, is nowadays one of the major callers on the world's zinc supplies, for the number of such cells in use at any moment runs into astronomical figures. Apart from the fact that most of the world's homes are now within range of some source of broadcast entertainment, and that the majority are still without mains supplies of electricity, portable wireless receivers of various kinds enjoy wide popularity; much of any army's wireless equipment must be battery-operated; hearing-aid appliances, developed from the a.f. side of the wireless receiver, are being used in larger and larger numbers. If one thinks, too, of the flashlamps, the cycle lamps and other small electrical appliances used now by millions of people in all parts of the world, it is quickly realized that the term astronomical is no exaggeration when applied to the number of dry cells in use the world over at any time.

The purpose of the present article is to investigate the efficiency, or otherwise, of the dry cell as we know it and to suggest ways in which its design, composition and construction might be improved. A second article will deal with the possibilities of using relatively cheap power from the supply mains to bring dry cells after discharge back to something like their original condi-

As almost everyone knows, the Leclanché cell "generates a current of electricity by consuming zinc as a fuel." Or, to put it a little less unscientifically, such a cell maintains a flow of electrons through an external closed circuit by converting into electrical

energy the chemical energy involved in the recombination of ammonuim-chloride and zinc into zincchloride, ammonia and hydrogen. As the textbooks have it,

$$2NH_4C1 + Zn = ZnC1_2 + 2NH_3 + H_2$$
.

That is a considerable over-simplification, for every manufacturer has his own pet electrolyte, which may contain calcium, lithium, magnesium, zinc and possibly other metals in the form of chlorides. This, however, is not the place to discuss such a complex matter, and we may accept for working purposes that the primary reaction is on these lines.

Depolarizing Process

The word "primary" is used because the cell is really a two-part affair. Part 1 consists of the electrolyte and the zinc, between which (on open circuit) there is a potential difference of about 1.1 volt. This portion is very efficient, in so far as it does not suffer from polarization: it gets rid of its surplus hydrogen in the form of positive ions. In Part II we have a p.d. of $0.4\,\mathrm{V}$ between the carbon and manganese-dioxide element and the electrolyte; hence the overall open circuit p.d. between the terminals of the cell is about $1.1\,\mathrm{V} + 0.4\,\mathrm{V} = 1.5\,\mathrm{V}$. But in this second part of the cell we run into considerable trouble when the external circuit is closed.

Each positive hydrogen ion, on reaching the carbon element, exerts an attraction which causes one electron to leave the negative pole, to travel through the external circuit and to turn the positive ion in question into a neutral hydrogen atom. Were nothing done about it, the carbon would soon be surrounded by a blanket of inert hydrogen molecules. Part II of the cell would be clogged and the action of Part I would also be brought to a standstill, for it would no longer be able to discard its surplus hydrogen ions.

Many textbooks lightly show the action of the man-

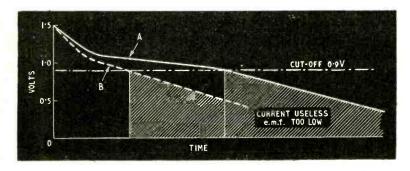


Fig. 1. Curve A shows typical end voltages during intermittent discharge of high-grade cells under ideal conditions of load, temperature and rest periods. A considerable proportion of the ampere-hours potentially available from the zinc in the can is useless, since the e.m.f. is too low. B is the discharge curve of moderately good cells under similar conditions.

ganese-dioxide depolarizer usually employed as: $2H + 2MnO_9 = Mn_9O_9 + H_9O$

If that were a complete statement of the case polarization would be eliminated; or, in any event, complete depolarization, with a return to its original e.m.f., would occur in a cell "rested" for a short time. That this does not happen is common knowledge. The reactions involved are far more complicated. It would be nearer the truth to write: "In time, a certain amount of the hydrogen molecules become dissociated into ions and some of these react with some of the manganese dioxide to form another oxide of manganese and water. Other slow and complex reactions are involved, and this process of depolarization is never sufficiently rapid to keep pace with the clogging that takes place during discharge, or complete enough to restore the original load e.m.f., no matter how long the cell is rested."

Now let us see how effectively the zinc is used. My experiments were made with cells of the $1\frac{1}{4} \times 2\frac{1}{4}$ -inch size. Each maker has his own designation for these. The Ever Ready "U2" will be familiar to most readers and will be used as a general term, though cells of a number of different makes, British and American, were subjected to the series of tests on which the present articles are based. The cans of such cells vary somewhat in weight from make to make; nor is it always easy to determine the exact weight of zinc, for seamed cans contain a certain amount of solder. Some cans are thicker than others and there are slight variations in dimensions. On the whole, though, we shall not be far out if we put the average weight of zinc in cans of this size at 19 grams.

There is no difficulty about discovering the number of ampere-hours of current which 19 grams of zinc would furnish, could it be used with complete efficiency. An ampere is a flow of one coulomb a second, and a coulomb consists of 6.3×10^{18} electrons. Zinc is bivalent; each atom passing into the electrolyte is a doubly positive ion, Zn++. This means that for every zinc atom removed from the can two electrons are available at the negative terminal of the cell. To maintain a current of one ampere, then, 3.15×10^{18} atoms must leave the can every second. The atomic weight of zinc is 65.38 (O=16), and from Avogadro's Number we know that 65.38 grams of zinc contain 6.0234 \times 10²³ atoms. Hence the weight of 3.15 \times 10¹⁸ zinc atoms is 0.000338 gram; and that is the electrochemical equivalent of zinc. Multiplying by 60 \times 60, we have, in round figures, 1.2 grams of zinc per ampere-hour.

In other words, the current obtainable if 19 grams of zinc were used a hundred per cent efficiently, would be 15.8 Ah. Discharged under ideal conditions of load, temperature and time allowed for recuperation, average cells of "U2" size give 3-4 Ah, and those of the highest quality from 5.5 to a little over 6 Ah. In other words, cells in common use may turn only from 19 to 24 per cent of their zinc to good account, while for the very best the figure does not exceed 40 per cent.

Many factors contribute to this low efficiency. One of the most important of these is that most apparatus intended to be operated by dry cells is designed to work satisfactorily down to, but not below, an e.m.f. of 0.9V per cell. Curve A of Fig. 1 shows typical lumped end voltages (that is, the average e.m.f.s at the end of each day's run) of a group of first-rate cells, discharged under the ideal conditions mentioned. It will be seen that much of the current potentially avail-

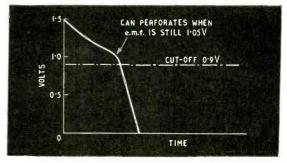


Fig. 2. Discharge curve showing the effects of perforation of the can at a moment when the e.m.f. is still 1.05V.

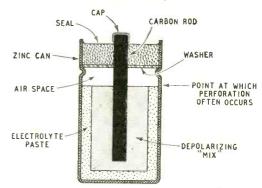


Fig. 3. Construction of modern dry cell. It will be seen that no sac is used. Perforation often occurs in line with the top of the electrolyte paste.

able from the zinc is useless, since the e.m.f. has fallen below cut-off as a result of progressive polarization. The first requirement, then, if cells of high quality are to be made more efficient, is to speed up the depolarizing process and to make it more thorough. Possible means to this end will be considered later. Curve B of Fig. 1 shows the curve for moderately good cells, discharged under similar conditions.

Though their overall performance is poor, the cells are classed as moderately good because they do not show one shocking and all-too-common fault; perforation of the can when the e.m.f. is still above (sometimes well above) cut-off. Fig. 2 indicates what happens in such cases. The e.m.f. begins to fluctuate and then falls almost like the proverbial stone. The electrolyte paste oozes from the hole in the can and may do serious damage. Perforation of one or more cans is in my experience one of the commonest causes of the breakdown of h.t. batteries. I have many times known it occur in batteries which had till then been giving readings of from 0.95V to 1.15V per cell. A curious point is that the cans perforated are nearly always near the middle of the battery; that is, in an 80-cell (120-volt) battery untimely perforation is most liable to occur between the 20th and 60th cells from the negative end.

Causes of Perforation

Premature perforation is in most instances due to poor design or construction. Fig. 3 (which may come as a surprise to any who have not examined the inside of a dry cell for some time) shows how most of these cells are made to-day. There is no sac, the depolarizing "mix" being in direct contact with the

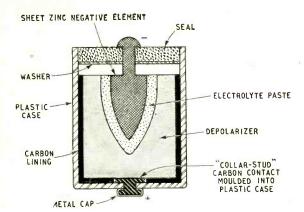


Fig. 4. Suggested "inside-out" cell. Only a small part of the zinc used is now unemployed. By designing the cell so that the carbon forms a lining to the plastic container, the depolarizer is given a much larger surface area on which to act.

paste electrolyte. As Fig. 3 indicates, a position at which the first signs of perforation very often occur is in the part of the can on a level with the top of the electrolyte. When a cell which has failed in this way is opened one frequently finds evidence of a considerable amount of "creeping" of salts from the electrolyte in the vicinity of the puncture. Small differences in the concentrations of such salts may give rise to undesirable local action.

Creeping does not occur to any marked extent inside really good dry cells. It may be due to one of two causes, or to both together. The first of these is the use of too strong a concentration of sal-ammoniac in the electrolyte; the second is failure to make the seal perfectly air-tight. These two causes are probably inter-connected. When a cell is not air-tight, evaporation takes place from the electrolyte, with the result that the ratio of sal-ammoniac to water increases. Another cause of the perforation of cans before cut-off e.m.f. is reached, is the use of zinc of too light a gauge.

There is another important reason why a considerable amount of the zinc in the can is not available for the production of current. A glance at Fig. 3 will show that all that part of the can which surrounds the air-space, the washer and the seal is out of the running: it is merely acting as part of a container and has no electrical role. Again, there is very little electro-chemical action at or near the bottom of the can; and here again zinc as zinc is mainly wasted.

New Design of Cell

Could not the dry cell be entirely redesigned on lines more in keeping with the present availability of raw materials? I think I am right in saying that, when the first dry cells were made, suitable carbon was most readily obtainable in the form of rods or plates. Zinc being then plentiful and cheap, the line of least resistance led to the familiar design of the dry cell. Great changes have occurred in the sixty-odd years that have passed since these cells began to come into anything like general use—changes, that is, in everything except their general make-up. High-density carbon, for example, is now readily shaped—or deposited—in any required way.

It is some time now since it occurred to me that a good many advantages might accrue, were the dry cell turned, so to speak, inside out. I have not the facilities for making up the dry cell illustrated in Fig. 4—or, for that matter, any kind of dry cell. But experiments made with wet Leclanché cells using carbon elements of large area have given very promising results. The main purpose of these has been (a) to put the zinc element where the greatest possible proportion of it plays a useful part; (b) to provide the depolarizer with the largest possible surface of carbon on which to act; (c) to make the greatest use of cheap and easily obtainable materials; (d) to evolve a cell which cannot play havoc by perforating; and (e) to produce a cell of exactly the same dimensions as the zinc-cased cell and fitting into any apparatus designed to be operated by it.

Fig. 4 illustrates more or less diagrammatically the suggested new look for the dry cell. The case is of plastic and into the bottom is moulded a "collar-stud" carbon (or metal) contact, with a metal cap on its external end. Immediately inside the case is a thin carbon lining; it need not be more than a few hundredths of an inch in thickness, for in the cell

the carbon is chemically inert.

The zinc element is hollow and made of sheet metal, possibly perforated. Or again, it may be a finned diecasting. Its exact shape and mass must be the subject of experiments. The zinc is "pasted" with electrolyte in the ordinary way. The parts between the electrolyte and the button forming the negative contact are protected from chemical and electro-chemical action by a plastic coating.

. . . And its Advantages

A cell made on the proposed lines cannot perforate; by far the greater part of the zinc is usefully employed; polarization must be much slower and depolarization quicker and more complete owing to the far larger area of carbon over which the hydrogen ions are distributed and on which the depolarizer is free to act. The surface area of the carbon walls is actually more than four times greater than that provided by the rod element now used. It will be seen that the proposed cell appears to be also inside-out, or perhaps one should say upside-down, as regards the polarity of its terminals. That protruding from the seal is the negative, while the cap at the bottom is the positive. This, however, is not a matter of importance, so long as the terminals are plainly marked + and -.

Though the idea of designing a dry cell on the lines described was original, in so far as it was based on my own line of thinking and on nothing that I had read, seen or heard, I cannot claim to be first in the field in trying to make the dry cell more efficient by turning it inside-out. Somebody always seems to have thought a little sooner than oneself of any new con-

ception that occurs!

Explaining my scheme recently to an American friend, I learnt that an "inside-out" dry cell had made its appearance in the United States. I have not been able to acquire American cells of this type, or to find out anything more about them. Whether or not they bear any resemblance to the design suggested in Fig. 4 I do not know. What I venture to hope is that this article may stimulate British designers of dry cells to break away from tradition and to give us (and the all-important export market) something far more efficient and more economical than the familiar dry cells of to-day.

VORTEXION TAPE RECORDER

FEATURES WORTH NOTING

- ★ Extremely low distortion and background noise, with a frequency response of 50 c/s.-10 Kc/s., plus or minus 1.5 db. A meter is fitted for the measurement of signal level and bias level.
- ★ Sufficient power is available for recording on disc, either direct or from the tape, without additional amplifiers.
- \bigstar The 15 to 30 ohms microphone balanced line input is fully loaded with 20 microvolts.
- Input 1, which requires 35 millivolts on .5 megohm, is suitable for crystal P.U.s, microphones or radio inputs.
- ★ A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of the play back signal.
- ★ The power output is 3.5 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.
- ★ Facilities are provided for using the amplifier alone and using power output or headphones while recording or to drive additional amplifiers.
- ★ Total power consumption is approximately 50 watts.
- ★ The hum and noise level which was already very low has been still further reduced.



The amplifier, speaker and case, with detachable lid, measures $8\frac{1}{4}$ in. x $22\frac{1}{2}$ in. x $15\frac{3}{4}$ in. and weighs 31 lb.

PRICE, complete with WEARITE TAPE DECK£84 0 0

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TYPE CP20A AMPLIFIER

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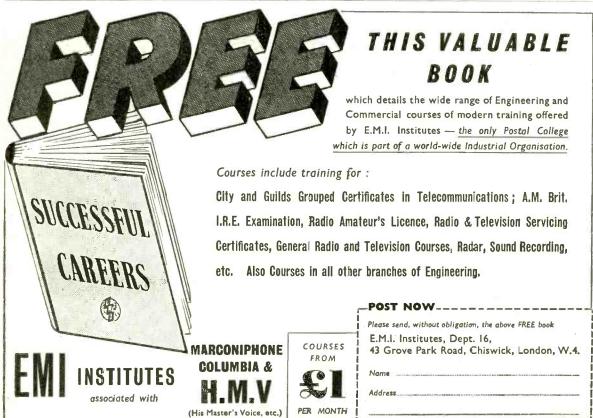
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Wireless World Television Receiver

Part 2.—Time-Base Circuits

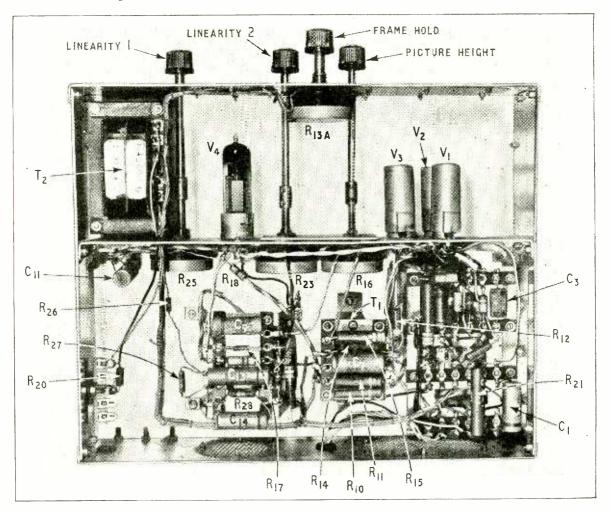
N the original Wireless World Television Receiver the frame and line time-bases were built on two separate chassis and the sync-separator circuits were included with the frame time-base. A similar arrangement is adopted for these new time-bases and the sync-separator is included with them.

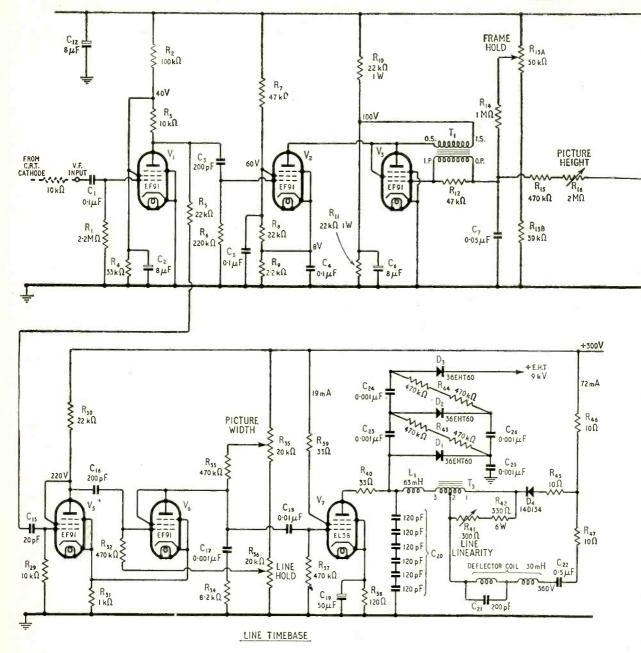
The circuit diagram is shown in Fig. 1. V_1 is the sync-separator and is fed with the combined sync and picture signal from the cathode of the tube. It is actually fed through a $10-k\Omega$ ½-W resistor suspended

in the lead from the tube cathode to the sync-input connector on the time-base. This resistor is shown dotted in the diagrams to indicate that it is external to the chassis. In the original time-bases, C_1 was so mounted and can be still if desired, but it is normally convenient to include it in the chassis. It must be so mounted that it has a low stray capacitance to earth.

D.C. restoration is effected in the grid circuit in the usual way and the separated negative-going sync pulses appear in the anode circuit. They are applied

Internal view of the frame time-base unit with some of the chief components indicated. The sync-separator components are on the extreme right.





through a differentiator and attenuator R_5 , C_{15} , R_{29} , to V_5 of the line saw-tooth generator. They are also applied through a semi-differentiator C_3 , R_6 , to the limiter V_2 which produces sharp output pulses from the trailing edges of the frame pulses. These are negative-going and are applied to the anode of the frame saw-tooth generator V_3 .

This generator is a blocking oscillator using a transformer T_1 . This transformer is identical with the one used in the original receiver. The saw-tooth appears across C_7 . Instead of using a variable charging resistance for the Hold control, the charging resistance R_{14} is now fixed and is taken to a variable

voltage point provided by $R_{13\Delta}$. The main reason for this is that a lower value variable component can be used and therefore one which can be wire-wound.

The saw-tooth voltage across C_7 is fed to the grid of V_4 , the frame output valve, through R_{15} and R_{16} , the latter of which is variable as a Height control. The deflector coil is transformer-coupled to the valve by T_2 and the 150- Ω resistance R_{20} across the deflector coil is for the purpose of reducing the line-frequency voltages set up in the deflector coil by unavoidable coupling to the line deflector coil.

Since it is not possible to make the inductance of the transformer anything like high enough to avoid

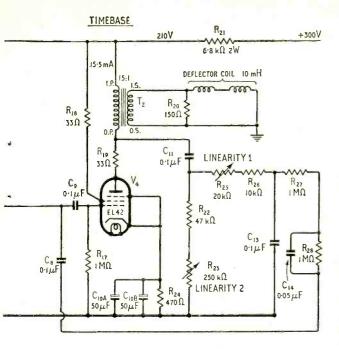


Fig. 1. Complete circuit diagram of the new time-bases. The resistor shown dotted is mounted in the wiring between the tube cathode and the input to the sync separator. C_{21} is mounted on the deflector-coil assembly. R_{45} , R_{46} and R_{47} have no circuit function but are included merely so that the current waveforms can be checked easily with an oscilloscope.

severe waveform distortion, very heavy correction is needed to obtain linearity. This is obtained by a feedback circuit of the Blumlein type. There are in all four circuits introducing distortion of the same form; the initial charging circuit R_{11} , C_7 , the coupling R_{17} , C_9 , the cathode-bias circuit R_{24} , C_{10} , and the transformer coupling. The transformer is the major source of distortion and the bias circuit the next in importance.

The correction circuit comprises C_{11} with R_{22} and R_{23} , the latter being variable as a linearity control. It is the main such control and affects the linearity generally over the picture. The next elements R_{25} and R_{26} with C_{13} affect the linearity at the extreme top of the picture only. In practice, R_{25} opens or closes the top half-inch of the picture. The remaining components R_{27} , R_{28} , C_{14} and C_{8} , are unusual ones, but were found experimentally to improve the linearity at the extreme bottom of the picture.

The linearity is affected by valve curvature, and so the settings of the linearity controls are slightly affected by the Height control. The dependence is small, however, and causes no practical inconvenience. In initial setting up the Height control should be adjusted for a picture of about three-quarters normal height and the two linearity controls roughly adjusted. Height should then be increased until the picture is just a little smaller than the mask and the linearity controls finally adjusted. Linearity 1 can easily be adjusted at any time for uniform line spacing at the top of the picture. Linearity 2 should be adjusted on Test Card C if possible. Height can then be increased to the proper value

A very hard frame lock is usually obtained, with the result that over a large part of its range a variation of Hold only affects the picture Height. Usually it is sufficient to set Hold at about the middle of the hold range and leave it there.

In the line time-base the saw-tooth generator is a cathode-coupled multivibrator V_5 , V_6 . The charging capacitance is C_{17} and the charging resistance is R_{33} . The applied voltage is varied by R_{35} as a width control. This varies the amplitude of the generated saw-tooth and hence the drive on the output valve V_7 .

The valve V_6 is normally held beyond cut-off by the charge on C_{16} , thus enabling C_{17} to charge. V_5 is conductive. A negative-going sync pulse on the grid of V_5 reduces its anode current and causes a rise of voltage on its anode which is passed to V_6 by C_{16} . This makes V_6 conductive and its anode current is drawn from C_{17} to discharge it. Grid current also flows to charge C_{16} . These currents flow through R_{31} and raise the cathode potential of both valves, which still further reduces the current in V_5 . The action is regenerative. When C_{17} is discharged, the current in V_6 drops and so the cathode potential falls and the current in V_5 rises. The action is again regenerative and V_6 is cut off. It is held cut off by the charge on C_{16} until the next sync pulse comes along or until C_{16} has discharged sufficiently to let V_6 conduct again. The grid-return potential of V_6 is adjustable by R_{30} as a hold control.

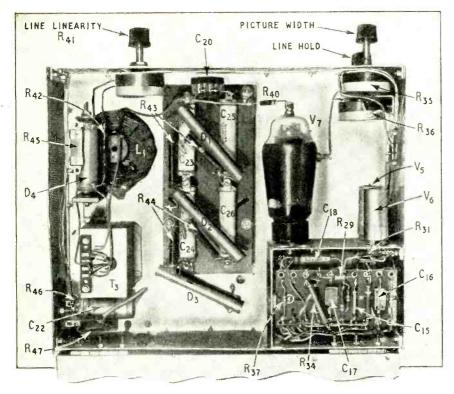
A resistance R_{34} is included in series with C_{17} in order to produce a large negative-going pulse on flyback. This is necessary in order to cut off the output valve rapidly and hold it cut off during flyback. The value of this resistance has an appreciable effect on the e.h.t. voltage produced and some effect on the linearity at the start of the scan.

No coupling transformer is used between the valve and the deflector coil and the circuit is one using a resonant flyback with an energy-recovery diode. Because of losses, the natural overshoot is less than 100%, and to obtain h.t. boost either a step-down transformer must be used or energy must be fed into the deflector-coil circuit during flyback so that the overshoot does become 100%. This energy is derived from a second circuit comprising L_1 and stray capacitances which is coupled to the deflector coil by C_{20} .

For a detailed explanation reference should be made to a previous article, but, briefly, L_1 and the deflector coil form two tuned circuits with their self- and stray-capacitances and they are coupled together by C_{20} , which acts as a "top-end" coupling capacitance. When V_7 is cut off during flyback, energy is stored in the magnetic fields of both coils. In the case of the deflector coil, it is required that the energy in its field be turned into electric form in the capacitance and then back again into magnetic form ready for the next scan. A loss of energy inevitably occurs, and this is made good by a transference of energy from L_1 through C_{20} .

The capacitance needed for this coupling is formed partly by the anode-cathode capacitance of V_7 and partly by a 20-pF capacitor C_{20} . This capacitor actually comprises six 120-pF capacitors in series, each of 750-V rating, in order to obtain the required voltage rating of 4 kV total.

A metal rectifier is used as a diode for energy recovery and avoids any difficulty over heater supply. It recovers about 50–60 V at the mean anode current of V_7 and this appears across C_{22} . With the 300-V h.t.



The line time-base unit. The e.h.t. voltage-tripler components are mounted near the centre on a sub-panel of Paxolin: slots are cut around the fixing holes to lengthen the leakage paths.

line the anode supply for the output stage is thus 350-360 V.

Linearity is controlled by the variable resistor R_{44} , which varies the magnitude of a control voltage injected by T_3 in series with the diode and derived from the anode current of V_7 . This transformer is a simple scramble-wound component which needs no special insulation in itself and is, therefore, easy to make. As a whole it needs insulating for up to 2 kV from the chassis, because the peak voltage of the deflector coil appears on it. Magnetostriction in the core produces a whistle and the two are remedied together by enclosing it in sponge rubber to provide both electrical and acoustical insulation.

The resistors R_{15} , R_{16} and R_{47} have no circuit function. They are included merely to enable the current waveforms to be checked with an oscilloscope. If an oscilloscope is not used they need not be included. If they are employed they should be wire-wound resistors of 1% accuracy so that they can be used for actual measurement purposes. The mean anode current can be measured, for instance, by measuring the voltage drop across R_{15} or R_{46} . The reading in volts multiplied by 100 gives the current in milliamperes.

 \dot{E} .h.t. is obtained through a voltage-tripler rectifier system from the peak voltage which appears on flyback across L_1 and the deflector coil. The tripler gives a multiplication of about 2.5 times and produces some 8.5 kV from the 3.4-kV peak. The magnitude of the e.h.t. voltage is governed by the rate of cut-off of the output valve and by the value of C_{20} . Increasing

the first by increasing R_{34} , and/or reducing C_{20} , will increase e.h.t. and, under some conditions, up to 11 kV has been obtained with full picture width. Generally speaking, if C_{20} is reduced, R_{34} must be increased to maintain linearity.

It is not recommended that these changes should be made, for the picture width becomes rather bare at voltages much over 9 kV and the full width may not always be obtainable. Also, difficulty from corona is

likely

Under the normal conditions of the circuit diagram, ample width is available with very good linearity and a complete absence of fold-over or visible ringing, and the adjustments are not critical. Normally the linearity control R41 should be set at about halfway and Width increased until the picture nearly fills the mask. Hold should be adjusted for a good lock, which will narrow the picture considerably. Then turn up Width again and re-adjust Hold. Adjust linearity on Test Card C.

It is not a critical control. When $R_{\rm H}$ is too small the picture tends to be gradually compressed towards the right. As $R_{\rm H}$ is increased the linearity is improved and, if it is too high, it may expand towards the right. Adjust Width to the proper value and lastly, Hold.

A large range of width is available without losing synchronization but, after adjusting it, Hold should be readjusted because, even if synchronizing has not been lost, it may be nearly lost, and a slight change of

mains voltage may send it over.

Some adjustment to C_{21} may be required. If this component is omitted, a series of grey and white bars will appear over the left-hand side of the picture. They are produced by ringing in the deflector coil itself and are quite independent of the time-base. They can only be avoided, in the absence of heavy coil losses, by equalizing the capacitances on the two coils of the line assembly. Ideally, C_{21} would be an adjustable component and would be adjusted to the critical value at which the bars disappear from the picture. In practice a suitable component is difficult to obtain, for it must be stable and withstand 1-kV peak. An approximate balance using a fixed capacitor has been adopted, therefore, with the result that the bars may not be completely absent.

The balance is normally good enough if the bars are just visible on a blank raster, for they are then unnoticeable on a picture. Precise adjustment of C₂₁ will make them disappear even on a blank raster, but sufficient precision for this is hard to obtain without

using an adjustable component.

This capacitor is not mounted in the chassis but

directly on the deflector-coil assembly and across the "uncarthy" coil of the line pair. If the deflector-coil connections as a whole have to be reversed, C_{21} must be changed over to the other coil.

Adjustment of C_{21} is best carried out on a blank raster, which need not be synchronized. Without it, a series of vertical grey and white bars on the left-hand side of the picture will be seen gradually decreasing in intensity towards the right and ceasing about the middle. As C_{21} is increased in value up to the optimum they decrease in intensity, but reappear again when it is too large.

In practice, if the bars are more than just detectable with a blank raster and a 200-pF capacitor, one should try different values for C_{21} . The first step is obviously to try an extra 20–30 pF capacitor in shunt with it, and to note whether this increases or reduces them.

If it reduces them try a bit more, but if it increases them reduce the main capacitor to 150 pF and then start adding more capacitance.

The precise value for the complete elimination of the bars is quite critical. However, a value which renders them undetectable on anything but a blank raster is far from critical, and no difficulty should be experienced in finding one. If, by any mischance, the proper value cannot be found, it is a good plan to replace C₂₁ temporarily by a variable air capacitor of 500 pF or so. This can be smoothly adjusted while watching the picture, and if a sharp balance point cannot be found, something is wrong somewhere.

Before turning to the constructional side it may be as well to say something about what parts of the original time-bases can be retained in making a change to the new one. The original sync-separator V1 and V2 can be retained unaltered with the original circuit values; but R5, C15 and R₂₉ of Fig. 1 must be included and have their new values. It may be found desirable in this case to reduce R₂₉ to 4.7 kΩ, for the original sync separator gives a larger output than the new one.

In the frame time-base the EF37 can be retained for V_3 and the EL33 for V_4 , but using all the new circuit values of Fig. 1. In the line time-base the EL38 is the only thing that can be retained. Although this has not been tried, it is probable

that the EF50 can be used in place of the EF91 without change of values. A 6SN7 double-triode has been employed successfully in place of $V_{\rm 5}$ and $V_{\rm 6}$ without changing component values.

The use of an 807 in place of the EL38 has not been tried and can hardly be recommended. It has a screen dissipation rating of 3 W only, compared with the 6 W of the EL38, and its rating is therefore exceeded in this circuit. Apart from this, it would probably work satisfactorily but it might well have a short life.

The time-bases give ample scan for a tube operating at 8–9 kV, and this is an adequate voltage for a 12-in tube. Many will consider it enough for larger tubes, although the trend is to operate such tubes at higher voltages. The use of higher voltages is not recommended to the inexperienced, however, on account of the difficulty of avoiding corona troubles. These are

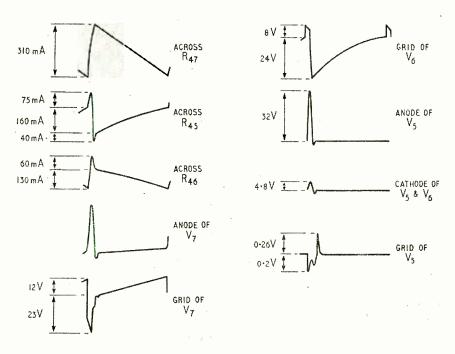
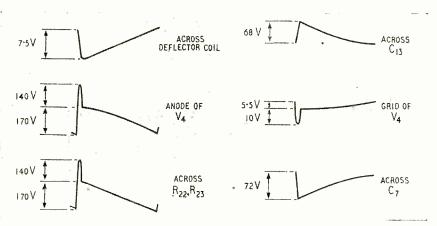


Fig. 2. Waveforms at important points in the line time-base. The current waveforms were measured as voltages across $10-\Omega$ resistors.

Fig. 3. Waveforms in the frame time-base. A $10-M\Omega$ resistor was connected to the oscilloscope cable to reduce small superimposed line-frequency voltages.



small for voltages below 8 kV, but become very considerable above 10 kV. In the region 9-10 kV corona can be troublesome, but is not unduly so. To minimize these troubles the voltage is limited to 9 kV in the present design and, allowing for the inevitable variations, may be 8 kV in some models.

It may be remarked in passing that a major effect of slight corona, which may be otherwise unsuspected, is poor line synchronizing. The discharge produces pulses which fire the time-base erratically. The visible effect is a ragged edge to the picture.

The waveforms in various parts of the circuit are shown in Figs. 2 and 3 for the line and frame time-bases respectively. These were all taken using the "Television Oscilloscope"." In the case of the frame time-base, most were taken using a $10\text{-M}\Omega$ resistor as a probe to minimize the effect of the oscilloscope on the time-base. In conjunction with the capacitance of the cable, this acts as a filter and removes the small content of line pulses which appear on some of the waveforms. If such a filter is not used, several of the frame waveforms will not appear as traces with clean lines but rather as fuzzy outlines.

In the line time-base the oscilloscope was connected across R_{45} , R_{46} and R_{47} , so that its case was live to h.t. If this is not done, the small ripple on the h.t. line appears also on the trace to distort it. Since this makes the case of the oscilloscope live, care must be taken in handling it.

 [&]quot;Television Oscilloscope", by W. Tusting, Wireless World, June and July 1952.

	LIST (OF PARTS	
Resistors			
R ₁	$2.2M\Omega$	₿W	Erie
R_2	100kΩ	₹W	Erie
R ₃ , R ₂₆ , R ₂₉	$10k\Omega$	į̃W	Erie
R ₄	$33k\Omega$	1 W 1 W	Erie
R ₅ , R ₈ , R ₃₀	$22k\Omega$	į̈́W	Erie
R ₆	$220k\Omega$	i W	Erie
R_7, R_{12}, R_{22}	$47k\Omega$	$\frac{1}{2}$ W	Erie
R ₉	$2.2k\Omega$	$\frac{1}{2}\mathbf{W}$	Erie
R_{10}, R_{11}	$22k\Omega$	1 W	Erie
R _{13A}	$50k\Omega$	potentiometer,	Reliance
		wire-wound,	Type T.W./1
		linear, 5W	
R _{13B}	$39k\Omega$	1W	Erie
$R_{14}, R_{17}, R_{27}, R_{28}$	$1M\Omega$	$\frac{1}{2}$ W	Erie
R ₁₅ , R ₃₂ , R ₃₃ , R ₃₇	$470k\Omega$	$\frac{1}{2}W$	Erie
R ₁₆	$2M\Omega$	variable, linear	Reliance
			Type S.G./1
$R_{18}, R_{19}, R_{39}, R_{40}$	33Ω	½W	Erie
R ₂₀	150Ω	$\frac{1}{2}$ W	Erie
R ₂₁	6.8 k Ω	2W	Erie
R ₂₃	$250k\Omega$	variable, log-	Reliance
		law	Type S.G./1
R ₂₄	470Ω	$\frac{1}{2}$ W	Erie
R_{25}, R_{35}, R_{36}	$20k\Omega$	variable, wire-	
		wound, linear,	Type T.W./1
		5W	
R ₃₁	lkΩ	$\frac{1}{2}\mathbf{W}$	Erie
R ₃₄	$8.2k\Omega$	$\frac{1}{2}\mathbf{W}$	Erie
R ₃₈	120Ω	2W	Erie
R ₄₁	300Ω	variable, wire-	Reliance
		wound, linear,	Type T.W./1
_	2226	5W	1377 1
R ₄₂	330Ω	6W	Welwyn
R_{43} , R_{44} each $2 \times$	470 k Ω	1W	Erie

Capacitors		
$C_1, C_4, C_5, C_8, C_9,$	$0.1 \mu F$,	tubular paper, 350 V, Dubilier
C_{11}, C_{13}		Type 460
C2, C6, C12	$8\mu \mathbf{F}$,	electrolytic, 500 V, Dubilier
<u>.</u>		Drilitic BR850

C ₃ , C ₁₆	200pF, silvered mica, 350 V, Dubilier Type 635
C ₇ , C ₁₄	0.05μF, tubular paper, 350 V, Ďubilier
C_{10A}, C_{10B}, C_{19}	Type 450 50μF, electrolytic, 50 V, Dubilier Drilitic BR505
C ₁₅	20pF, ceramic, Dubilier Type CTD316
C ₁₇	0.001 μF, moulded mica, 350 V, Dubilier Type 635
C ₁₈	0.01μF, tubular paper, 350 V, Dubilier Type 460
C ₂₀ 6 ×	
C_{21}	200pF, mica (see text), Dubilier Type 680
C_{22}	0.5μF, tubular paper, Dubilier Type 4706B
$C_{23}, C_{24}, C_{25}, C_{26}$	0.001 µF, 10 kV, Dubilier Type 411
Valves	
V_1, V_2, V_3, V_5, V_6 V_4 V_7	EF91 Mullard EL42 Mullard EL38 Mullard
D_1 , D_2 , D_3 D_4	Westinghouse 36 EHT60 Westinghouse 14 D134

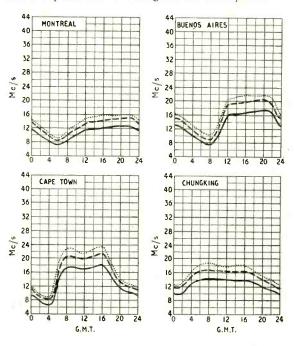
Short-wave Conditions

(to be concluded)

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Radio Waves

How the Magnetic and Electric Fields Support Each Other

URING the war, when thousands of people had to be trained in the shortest possible time to look after radar equipment, it surprised everybody, I think, how in a few months any reasonably intelligent lad, starting right from scratch, seemed to be quite at home among unprecedentedly complicated circuitry. Some of them, not noticeably bright in other respects, could quite readily reproduce diagrams of such circuits from memory. We, who were called upon to do our spot of instructing, sometimes wondered what we could have been doing during our years of study! But when questions were asked that required the application of basic principles to a new situation some of the most outstanding memorizers failed the most

dismally. It was not that they couldn't recite all the necessary principles from memory. The difficulty was-and is-first to know which to pull out of the bag, and secondly, how to use it. A, who relies entirely on memory and practical experience can go far

astray when he comes up against something unfamiliar; B, who works things out from principles may be hopelessly slow at routine stuff but can find his own way

Exactly what happens between radio sender and receiver doesn't concern most of us very deeply most of the time; we are taken up with what happens before and after, and may not have to dig out our basic principles often enough to prevent them from getting rusty. So a little practice here and now may be all to the good.

Two months ago, you may remember, I mentioned that radio waves-electromagnetic waves, to be precise —consist of equal electric and magnetic fields. People sometimes ask, "Which part produces the signal in the receiving aerial; the magnetic, the electric, or both?" If the receiving aerial were close enough to the source to be affected by induction fields, this would be quite a sensible question, because the induction fields are those parts of the total electric and magnetic fields that depend directly on the source, so it is possible for them to be mainly electric or mainly magnetic, depending on whether the source is energized mainly by voltage or current. That is why G. Bramslev was able to show (in the Nov. 1952 issue) how to use a frame aerial to discriminate against noise interference from sources producing mainly electric fields. When no clear distinction is made between induction fields, tied to their mother's apron strings, and radiation or wave-motion fields, making their own independent way through the world, it is not surprising that there are confused ideas about wave reception, such as a belief that an open-wire aerial responds to the electric part of a radiated wave and a frame aerial to the magnetic part, so that one can choose whichever one wants. Actually, asking which part of the wave causes the signal in either kind of aerial is rather like asking whether things blown over by the wind are affected by the movement or the pressure of the wind. Without movement there would be no one-way pressure, and without pressure there would be no movement. The two are inseparable, so you can please yourself which you say is the cause.

If you still feel puzzled about this, even after the difference between induction and radiation has been made clear, I am not surprised. It does seem contradictory. Fact One is that an open-wire aerial responds to an induction electric field and a frame aerial or coil to an induction magnetic field, but not vice versa.

Fact Two is that there is no

difference between induction and radiation fields themselves but only in the way they are organized. And yet one is asked to believe that with radiation fields the type of aerial cannot be used to distinguish between the electric

and magnetic parts, and that this is not simply because the electric and magnetic fields happen to be present in equal proportions. The only possible explanation must lie in the difference in organization between

RAY"

"CATHODE

induction and radiation fields.

That is quite so, but to see it one needs to fall back on first principles. And it is just as well to remember that these principles are not mere armchair theory but are the results of actual experiments. One of the greatest of all experimenters was Faraday. He it was who discovered how to generate electricity by magnetism. (The generation of magnetism by electricity had already been discovered.) He found there were two ways of generating an e.m.f. in a coil of wire. One was to push a magnet in or pull it out. He found the e.m.f. lasted only while the magnet was moving relative to the coil. Of course the same result was obtainable with a fixed magnet and moving coil. The principle of the thing was summed up by saying that whenever any part of a circuit is cut by the flux of a magnetic field the circuit receives an e.m.f. proportional to the rate of cutting. If you were to get a large magnet and a small piece of wire as in Fig. 1, and move the magnet at right angles to the wire (i.e., towards or away from you in (a), and to left or right in (b)) the magnetic field extending between the poles of the magnet would cut across the wire and generate in it an e.m.f. The rate of cutting, and hence the e.m.f., would obviously be proportional to (i) the strength of the field, or flux density, (ii) the speed of movement, and (iii) the length of the wire.

The other epoch-making experiment of Faraday was to generate an e.m.f. in a coil without any movement, by varying the strength of the magnet. He did this, of course, by using a coil of wire as the magnet, switching the current on and off. Again, the e.m.f. lasted only while the magnetism was varying. This result was generalized by saying that if the amount of magnetic flux linked with any circuit is varied the circuit will receive an e.m.f. proportional to the rate of variation.

On the first experiment is based the generation of nearly all the world's electricity supplies, and on the second the transformers needed to make those supplies economically available; so no wonder Faraday is the

" patron saint" of electrical engineers.

As sometimes taught, the flux-cutting idea (Fig. 1) is given as the basic principle, and the flux-varying idea is brought into line with it by supposing that when a current is switched on the resulting flux springs out from it and cuts across any close-up circuits, and when it is switched off it returns inwards and cuts them again in the opposite direction. This mental picture is none too clear when it is called upon to explain the e.m.f. of self-inductance. How does the flux springing out from a wire cut that wire itself? And this is not the only dubious aspect of the flux-cutting idea. The "experiment" purporting to demonstrate it (Fig. 1) is quite phoney. Unlike those of Faraday, it is not an experiment that can be per-

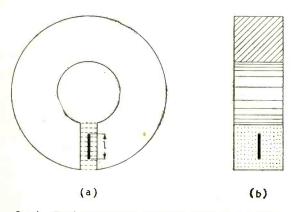


Fig. 1. The basic principle of how electricity is generated in a power station is often expressed something like this, by saying that if a magnetic field is moved across a length of circuit I an e.m.f. is generated in it, proportional to I and to the rate at which the field is moved across. Here the field is shown as due to a permanent magnet, moved towards or away in (a) and to right or left in (b), which is a cross-section of (a).

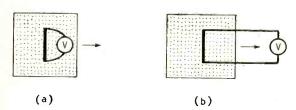


Fig. 2. When an attempt is made to verify Fig. 1, it is necessary to take account of the voltmeter leads. Moving the magnet causes no reading in (a); the arrangement shown in (b) is successful, but the action can at least equally well be explained as change of magnetic field passing through the whole circuit.

formed. To demonstrate the existence of the e.m.f. it is necessary to connect a voltmeter between the ends of the wire; then what about the voltmeter leads? If they are kept within the field as in Fig. 2(a) they too are cut by the flux so they receive an e.m.f. which (assuming the field is uniform) exactly counterbalances the e.m.f. in the wire and one is none the wiser. If the leads are taken horizontally as in Fig. 2(b) so that they are not cut, the e.m.f. now shown by the voltmeter can be explained equally well by the fact that moving the magnet in the direction of the arrow increases the flux linking the circuit. The absence of result in Fig. 2 can likewise be explained on the same basis; the assumption that the field is uniform means that moving the magnet does not alter the flux linked with the circuit. So both of Faraday's methods of inducing an e.m.f. can be visualized and calculated as flux-linkage variation, without any need to bring in the rather shaky and experimentally undemonstrable flux-cutting picture.

Example of Flux Linkage

Just to consolidate the matter, let us take a simple example; say the Fig. 2(b) situation, making the assumption that the flux density is uniform between the pole-pieces and zero elsewhere—no "edge effect." Wire, flux, and motion are all mutually at right angles. Field calculations are easiest if one uses the m.k.s. system of units, as most modern books do. voltage generated is equal to the rate of flux cutting or linkage if that is in webers per second (1 weber = 108 "lines"). Suppose the flux density (B) is 1.2 webers per sq metre (12 kilogauss in the old units), the wire is 0.02 metre long, and the magnet is moved at 0.5 metre per sec. Then the cross-section area of flux passing through the circuit increases at the rate of $0.5 \times 0.02 = 0.01$ sq metre per sec, so the rate of flux linkage, and hence the induced voltage, is $0.01 \times$ 1.2 = 0.012. If the process is pictured as flux cutting the original vertical wire, the figures are of course the same, but the result (0.012) must not be taken as the measurable voltage until one has made sure that no other parts of the circuit are being cut by any flux. Because of this the flux-linkage way of looking at it is both safer and (in less absurdly simple examples) may be easier.

So far we have supposed this moving magnetic field to be produced by a permanent magnet. But of course it could be an electromagnet. Fig. 3(a) shows a single-turn coil of wire carrying d.c. Its magnetic field is at right angles to the paper, and with an anticlockwise current as shown it is towards us, as suggested by the dots. Next (b) imagine the loop to be whisked rapidly to the right. The effect of this is that paths such as those shown dotted experience an e.m.f. tending to drive current in the directions shown. But because no circuits are provided there, it is only a tendency. One can say that within the area covered by the loop at any instant there is an upward e.m.f.

Electric-Field Current

At this stage a little digression may be necessary to recall what happens when an e.m.f. is applied across a space. This is done in Fig. 4 by connecting a battery to a pair of parallel plates. The e.m.f. of the battery sets up a potential difference between

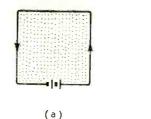
the plates, which is another way of saying that there is an electric field between them, indicated conventionally by the lines in Fig. 4. This field is reckoned in volts per metre. But before it can exist the battery must have driven a current from the lower to the upper plate in order to charge it positively. (Actually what happens, of course, is that electrons are driven downwards on to the lower plate to charge it negatively, but that is just another way of saying the same thing.) To anybody who thinks in terms of circuits and current electricity rather than charges and static electricity, this charging current is something of an anomaly. How can a current flow in a circuit that is not complete? Maxwell, the genius who brought his mathematics to bear on Faraday's experimental results and predicted electromagnetic waves, argued that what happened in the space occupied by the field was equivalent to a current; it flowed only so long as the field strength was varying, so could not continue indefinitely in the same direction, and to distinguish it from conduction or circuit current he called it displacement current. It is like the limited movement in a fixed block of rubber while pressure is being increased across it. So we think of the temporary current that flows upward through the battery in Fig. 4 when it is connected as being continued back to the start by a downward displacement current in the space between the plates.

To fit this Fig. 4 picture into Fig. 3 it is necessary to imagine that the battery fills the whole of the space covered by the loop, because it is all occupied by upward e.m.f. So the downward displacement current must all flow outside the loop area. Finally, since the e.m.f. is not produced by a battery at all but by a moving magnetic field, the upward current too must be a displacement current. Since space at the top of the loop is positively charged, an upward displacement current must have just occurred in order to make it so; in fact, at the extreme right-hand side of the loop the space is actually in the process of becoming positive at the top, and so a displacement current must still be occurring here. Note that it is in the same direction as the magnetizing current produced by the loop battery. At the left-hand side the positive charge must disperse as the edge of the loop passes by, so here there is a downward displacement current again in the same direction as the magnetizing current.

Now any current causes a magnetic field; no questions are asked as to whether it is a conduction current or a displacement current. So when the loop is moved there is no need to supply quite so much current from the battery; the difference is made good by the displacement current caused by the motion. The faster the loop is moved the greater the electric field developed by a given magnetic field and the greater the displacement current. If the loop were moved fast enough, could it be dispensed with altogether, the moving magnetic field being sustained entirely by displacement currents?

That is the question that Maxwell answered and expressed in the celebrated Maxwell equations. These don't mean a thing to anybody who is not rather unusually bright at mathematics, so I shall try to arrive at the answer by an easier route, even if it may not altogether satisfy the stricter mathematicians.

What we know already is that the electric field (denoted by ϵ) is equal to the voltage per metre p.d. set up by the movement of the magnetic field. (If an



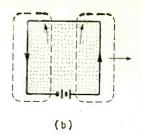
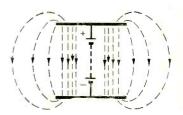


Fig. 3. If a simple loop electromagnet as shown, producing a magnetic field pointing towards the reader, is moved to the right it causes an upward e.m.f.

Fig. 4. In order to set up a potential difference between two plates it is first necessary for a temporary charging current to flow, and this is supposed to be continued as a displacement current along the directions of the electric field, shown here.



air capacitor with plates 1 mm apart is charged to 50V, the electric field in the space between is 50,000 V/m.) And we know that the voltage is equal to the rate at which the flux is changing in the space concerned. The flux (Φ) is equal to the flux density (B) multiplied by the area of its cross-section. And B is equal to the magnetic field strength (H) multiplied by the permeability (μ) . And in m.k.s. units H is equal to the ampere-turns per metre of field length. We can greatly simplify the putting of all this together if we make our chunk of space a one-metre cube. original magnetizing loop would appear in Fig. 3 as a one-metre square, but this would be an edge-on view of a turn made of strip one metre wide. Suppose that at the instant considered it exactly contains our stationary cube of space. And let the current round the loop be I amps. Then H is equal to I, and B (and therefore Φ in this case) is equal to μI . The rate at which Φ is changing in this space depends on the speed with which the loop is moved across the space. By the time it has been shifted one metre the whole of the flux Φ has been taken away, so if the speed is v metres per second the rate of change of Φ is $v\Phi$, and we know this is equal to €. So the final upshot is $\epsilon = v \mu I$

Doing Without the Loop

Now to render the magnetizing loop entirely unnecessary, I has to be the displacement current generated by the charging of the space. A current is the rate at which electric charges are being moved. If a charge amounting to one coulomb is transferred at a steady rate in one second the current is one amp. The amount needed to charge C farads to V volts is CV coulombs. Our chunk of space can be regarded as a capacitor with plates one metre in area spaced one metre apart. Its capacitance in m.k.s. units is equal to the permittivity (κ) of space. The movement of the magnetic field at v m/s causes it to be charged to ϵ volts v times per second, so the rate at

which charging takes place (which is I) is $\kappa \epsilon v$ coulombs per second. So now we know that $I = \kappa \epsilon v$. But our previous result told us that $l = \epsilon / v \mu$. So putting these together we get

$$\kappa \epsilon v = rac{\epsilon}{v \mu}$$
 $\therefore \kappa v = rac{1}{v \mu}$
and $v^2 = rac{1}{\mu \kappa}$
so $v = rac{1}{\sqrt{\mu \kappa}}$

For reasons that are too involved to explain in passing, the m.k.s. electrical units are based on the μ of empty space—air is practically the same—being equal to $4\pi/10^7$. Measured in the same units, κ is found to be almost exactly $1/(36\pi \times 10^9)$, so

$$v = \sqrt{\frac{10^7}{4\pi} \times 36\pi \times 10^9}$$
$$= \sqrt{(9 \times 10^{16})}$$

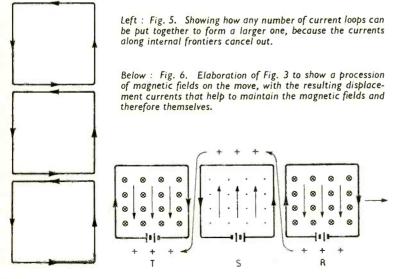
= 300,000,000 metres per second approximately*.

That is the speed at which fields have to move through space in order to be self-supporting. This apparently formidable requirement is in fact quite easily met, for any change in the magnitude of any current or voltage anywhere starts the process and launches an electromagnetic wave. But as we have seen in recent issues, it is only when the originating circuit is large and the rate of change rapid that the resulting wave is likely to be substantial.

If we did the above calculation more thoroughly, using a chunk of any dimensions, these would cancel out, giving the same result. I suggest you try it, just to convince yourself. Maxwell, being the bright boy he was, arrived at it by strict mathematical processes, before anybody knew definitely that electromagnetic waves were possible. It was Hertz who came along later and proved Maxwell right by demonstrating such waves produced by electrical means.

In case anyone thinks I have been trying to pull a

^{*} The latest estimate is 299,792,000



fast one by quietly forgetting about the current in the top and bottom of the magnetizing loop that was necessary to produce the magnetic field, I would hasten on to Fig. 5, which shows what happens when 1-metre "bricks" are put together as a start towards unrestricted open space. The currents in adjacent parts cancel out, so the dimensions of the bricks don't matter at all.

Another thing: the result does not depend on using m.k.s. units. Any system of units, recognized or unrecognized, will do, provided it is a system.

Procession of Fields

Before finally knocking away the visible scaffolding that has helped us to build a picture of electromagnetic radiation, let us multiply it a little as in Fig. 6, showing three links in a whole chain of loops all moving to the right, with currents alternately clockwise and anticlock. The middle one, S, is just our old Fig. 3 friend, now escorted fore and aft by R and T. Between R and S the space which a moment ago, while R was passing, was positive below is becoming positive above, so an upward displacement current is necessary. Between S and T it must clearly be downward. Now accelerate the procession to the speed at which battery magnetization is unnecessary, and what remains is a sequence of moving fields, alternately positive and negative; each bunch of magnetic field pointing towards us being accompanied by an upward-pointing electric field, and followed by an away-pointing magnetic field accompanied by a downward electric field. Since there is now no apparatus to maintain either field, each relies entirely on the other for its existence. It is the perfect marriage; they cannot be parted even by death.

So there is really not very much point in arguing about which partner causes the signal in a receiving aerial. Radiation can only exist as a combination—an electromagnetic wave. The logical view is that the electric field is primarily responsible, because that is what the free electrons in the aerial respond to. But since the radiated electric field is generated by the magnetic field the same answer is obtained if one supposed the e.m.f. in the aerial to be generated by

the magnetic field as in ordinary Faraday induction. In practice the strength of a radio wave is usually given in terms of its electric field, in microvolts per metre, because this gives the aerial e.m.f. directly.

Fig. 6, you remember, was a sample of what we imagined to be a long chain of "links." A pair of them, say S and R, makes up one complete wave, with positive and negative half-cycles. So wavelength is represented by twice the width of one link.

All the way through we have, for simplicity, been assuming that the fields are uniform over a whole link, loop, chunk, or brick. So Fig. 6 represents square waves. In practice one is more often concerned with sinusoidal patterns of field strength, and the calculations are usually made on that basis, which does not alter the main conclusions.

WIRELESS WORLD, JUNE 1953

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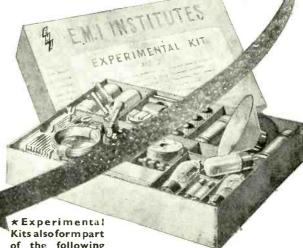
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Voltmeter Loading

Use of Potentiometer Method

T is very well known that the measurement of voltage in high-resistance circuits is liable to be inaccurate because of the load imposed by the voltmeter. It is surprising, therefore, that more use is not made of a method which is described in all text-books of electricity—the potentiometer method.

A voltmeter requires some power to operate it and this power is normally supplied by the circuit under test. If this circuit is of high resistance it cannot supply the necessary power without a drop in voltage. In the potentiometer method, a separate source of power is used to operate the voltmeter and the circuit under test has to supply no power at all. It is, therefore, quite unaffected by the connection of the measur-

ing circuit.

The arrangement is shown in Fig. 1, where M_1 is any ordinary voltmeter. The associated apparatus comprises a second meter M_2 , which is preferably a centre-zero galvanometer, a potentiometer R and a battery V of voltage greater than that to be measured. The circuit under test is represented by a box with two terminals AB. The measuring circuit is connected to AB, R is adjusted so that M_2 indicates zero and the

voltage is read from the voltmeter M1.

If R is adjusted so that there is no current in M_2 , then AB neither supplies current to nor draws current from the measuring circuit. The voltage between A and B is thus the same as if the measuring circuit were not connected. If there is no current in M_2 the voltage across M_2 must be zero and so the voltage between C and D must be the same as that between A and B. The voltmeter M_1 , however, indicates the voltage between C and D; therefore, it gives a true indication of the voltage between A and B. The power for operating the voltmeter is drawn entirely from the battery V.

In practice, it is not very convenient to have to use a separate power supply in this way. In most radio apparatus, however, the voltages appearing at high-resistance points are derived by voltage-dropping from a common higher-voltage supply of relatively low resistance. Screen-grids, for example, are fed from the main h.t. line through dropping resistors or potential dividers. In most cases, therefore, the main h.t. line of the apparatus can be used for the voltmeter supply and the battery of Fig. 1 becomes unnecessary.

The basic circuit of Fig. 1 can be simplified by the omission of the battery but in other ways it requires some elaboration. It is necessary to have something to protect the meter M_1 in case R is a long way from the proper adjustment when the circuit is connected. Let the voltage under test be V_{AB} with a source resistance R_{AB} . If the slider of R is at the bottom, the current in M_2 will be $V_{AB}/(R_{AB} + R_m)$, while if it is at the top it will be $(V_{AB} - V)/(R_{AB} + R_m)$, where R_m is the resistance of the meter.

 R_m is the resistance of the meter. It is necessary to make R_m large enough so that under these extreme conditions the current will not exceed the full-scale value of M_2 . The worst conditions

are when V_{AB} is much less than V or nearly equal to V and, for complete safety under all conditions, it is desirable to have V/R_m no greater than the full-scale current of M_2 . In effect, this means that M_2 must be a voltmeter having V within its range.

The resistance of M_2 will then be high and this will make the meter an insensitive indicator of the balance condition and it will be difficult to determine the proper setting of R. To overcome this, the resistance

can be short-circuited by a switch as balance is approached.

A second defect of the arrangement of Fig. 1 is that a potentiometer of ordinary quality does not give a fine enough control of voltage, particularly at low-voltage settings. It is often desirable to supplement it by a variable resistance. The circuit then takes the form shown in Fig. 2. R_1 and R_2 should be of about the same value and $20 \text{ k}\Omega$ is suitable in most cases. With a 300-V h.t. supply they will draw up to 15 mA and the power will be up to 4.5 W, so components of at least 6-W rating should be used. If M_2 is a centre-zero instrument reading 1 mA f.s.d., R_m should be $300 \text{ k}\Omega$ to avoid any possibility of overloading it.

In use, terminals 1 and 3 are connected to positive and negative h.t. of the apparatus under test and 2 is joined to the point at which it is desired to measure the voltage. With R_1 about mid-way on its travel, R_2 is adjusted for zero reading on M_2 (if this comes at the top of R_2 , R_1 is reduced). Then S_1 is closed and R_2 (and R_1 if necessary) is re-adjusted more precisely.

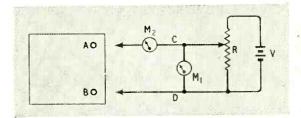
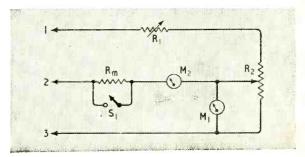


Fig. 1. Basic potentiometer circuit for voltage measurement.

Fig. 2. Practical circuit. M_2 is a centre-zero milliammeter.



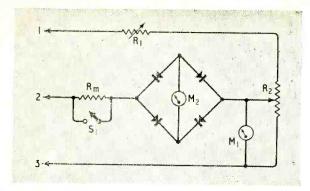


Fig. 3. Circuit for use with a left-hand zero meter for M_2 . The metal rectifiers ensure that the meter deflects one way only irrespective of the direction of the current.

When a centre-zero meter is not available, the ordinary left-hand zero type can be used in conjunction with a bridge-type metal rectifier of the kind used in a.c. instruments, as shown in Fig. 3. This makes the meter reading independent of polarity and so the adjustment for zero current becomes one for minimum deflection of the pointer. The sensitivity obtainable is not quite so great because the resistance of the rectifier elements increases as the balance point is approached, but the adjustment of R is easier to carry out for a minimum reading than for zero.

It is, of course, possible to elaborate the scheme. By introducing switching, for instance, one meter can be used for both purposes. The voltmeter M_1 , for instance, is only a milliammeter with series resistors. The meter itself can, therefore, be switched to do duty for M_2 if its voltage-range resistors are left in place to keep the proper load on $R_{\rm sc}$

NEW BOOKS

Television Receiver Design: Monograph 1; I.F. Stages. By A. G. W. Uitjens. Pp. 177 + xii; Figs. 123. Philips Technical Library: distributors; Cleaver Hume Press, Ltd., 42a, South Audley St., London, W.1. Price 21s.

THE Philips organization (Holland) have already published English translations of a series of books on broadcast receivers by members of their staff, and they are now embarking on a similar series on television receivers. This, the first, deals with the i.f. stages; the translation is, on the whole quite satisfactory; printer's errors are few and, except in one instance, of minor importance. At the end is a list of symbols, some of which will be unfamiliar to the English reader. It is a pity that the opportunity was not taken to bring all the symbols into line with English usage, as this would greatly enhance the value of the book to a student reader. There are seven chapters on single and coupled tuned i.f. circuits with staggered tuning; gain-bandwidth, distortion, noise and valve interelectrode feedback problems are thoroughly explored. The text is illustrated by numerical examples and the last chapter details a particular design of staggered tuning with five single circuits as well as indicates the response to a modulation envelope step function; a circuit diagram of the complete amplifier would have been helpful. effect of trap circuits protecting from adjacent channels is considered, and reasons are given for the choice of the circuit to which they are connected. To preserve continuity proofs of many expressions used in the text are relegated to appendices. In Appendix 1, the attenuation and phrase responses of a single tuned circuit are derived,

and input, output and transfer impedances, and admittance locus diagrams are developed for dissimilar as well as similar tuned circuits coupled by mutual inductance. Constant reference must be made to the list of symbols if the derivations are to be followed. In section 1g it is not immediately clear that the primary is the coupling circuit and the secondary an absorber circuit when discussing trap circuits in terms of tuned coupled circuits. A diagram including values, such as Fig. 74 with suitable captions, would have made this clear. Appendix 2 develops the expression for determining the response of staggered tuned circuits as used in Chapter 2 where the principle of "flat" staggered tuning is clearly set out.

In television receiver design it is important to know how the pulse shapes of the input signal are modified in their passage through the i.f. stages, and Appendix 3 shows how the modifications can be determined from the attenuation and phase response characteristics. A misprint makes Appendix 4 on noise factor calculations difficult to follow; Fig. 31 should read Fig. 56. Appendix 5 develops expressions used in Chapter 6, where feedback effects due to valves are considered. Table 1 provides information on the characteristics (gain-bandwidth, etc.) of Philips valves suitable for use in wideband amplifier stages. The remaining three tables are concerned with factors of importance in staggered tuned circuits. There is no index.

The inexperienced designer will find much of value in this book but the expert will discover little that he does not already know.

K. R. S.

Sound Reproduction (Third Edition) by G. A. Briggs. Pp. 368; Figs. 315. Wharfedale Wireless Works, Bradford Road, Idle, Bradford, Yorks. Price 17s 6d.

WRITTEN professedly in non-technical language and addressed primarily to the layman, this book contains, nevertheless, much material of interest to the knowledgeable enthusiast, and the terms non-technical and semitechnical, often used by the author, should be liberally interpreted. The field covered is wide—literally all aspects of sound reproduction not dealt with in greater detail in the author's other books on "Loudspeakers" and "Amplifiers"—and this third edition has been brought up to date by extensive revision of the original text and by the addition of eight new chapters.

Mr. Briggs has been fortunate in his collaborators and the chapter on vented (reflex) cabinets by R. E. Cooke is probably the best exposition of the underlying principles so far published. This is backed by tables giving specific recommendations for cabinet dimensions to suit typical sizes of loudspeaker and cone resonances. R. L. West and S. Kelly contribute new material on the design of pickups, and the practical aspects of successful magnetic tape recording are ably dealt with by C. H. Banks and L. J. Bradley. The chapter on cross-over networks is detailed and contains much useful coil-winding data, together with some concrete facts about phase shifts near the cross-over frequency—hitherto a somewhat nebulous bogy.

Mr. Briggs is an indefatigable experimenter and he has photographed countless cathode-ray oscillograms to verify the axiomatic as well as to illuminate the controversial in his search for better quality of reproduction. His conclusions are generally sound, but occasionally hasty as when he states (p. 37) that there is no "vibration" at the mouth of a quarter-wave pipe. A "velocity" instead of a "pressure" microphone would have given quite a different picture. There is also some confusion of thought on the role of density, Young's modulus and viscosity sic of materials involved in the production and transmission of sounds. Weight rather than density (p. 102) is the criterion for confining low-frequency sounds, and a high Young's modulus is not a necessity for producing high frequencies as his "odd man out" example of hand clapping (p. 183) secms to prove.

Whether one is learning from or disagreeing with the author—and no one interested in sound reproduction can fail to do both—there is little fear of falling asleep while reading this book.

F. L. D.

Proposed Television **Stations**

Plans for British Two-programme Service

N July 1st the Stockholm Plans for broadcasting in bands 41-68, 87.5-100 and 174-216 Mc/s, which were signed on June 30th last year, officially come into force. So far as this country (which was among the 21 signatories) is concerned, the signature is effective only for Band I. The British delegation would not commit this country to the plans for Bands II and III until it had been finally decided by the Government whether a.m. or f.m. was to be used for the sound service in Band II and also precisely how Band III was to be used. The Atlantic City Convention (1947), which allocated frequencies en bloc to the various services, contains a footnote permitting the U.K. to use Band III for other than broadcasting; actually for point-to-point communication (174-200 Mc/s) and air navigational aids (200-216 Mc/s).

Provision is made in the Stockholm Plans for 40 television stations in this country—12 in Band I (including the existing and projected 10 stations) and 28 in Band III. In view of the recent statement by Sir Ian Jacob, director-general of the B.B.C., that the Corporation hopes to erect 10 low-power stations when the present scheme is completed we give below a list power stations when the present scheme is completed, we give below a list of the 30 additional British stations provided for in the Stockholm Plans.

It must, of course, be pointed out that this list, which provides for a dual service for the whole country, was drawn up before any decision had been reached regarding sponsored television.

Vision	Sound	Station	E.R.P.	* (kW)	Polariz-
(Mc/s)	(Mc/s)	Station	Vision	Sound	ation
	ND I	Isle of Man	25	6	Н
61.75	58.25	Channel Islands	5	1.25	Ĥ
BAN 179.75	D III 176.25	Channel Islands London Pontop Pike	5 200 50	1.25 50 12	V V H
184.75	181.25	Aberdeen Holme Moss South Devon	50 200 50	12 50 12	H V H
189.75	186.25	Kirk o' Shotts Norfolk North Wales	200 50 50	50 12 12	V V H
19 4.7 5	191.25	Northern Ireland South East Kent Sutton Coldfield West Cornwall	50 50 200 50	12 12 50 12	H V V V
199.75	196.25	Cumberland Wenvoe	50 200	12 50	H V
204.75	201.25	Isle of Man Isle of Wight Londonderry North Scotland West Wales	50 50 50 50 50	12 12 12 12 12	V V H V H
209.75	206.25	Cumberland South East Kent West Wales	50 5 50	12 1.25 12	H V H
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^{*} Effective radiated power.

H. Horizontal.

V, Vertical.

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RANDOM RADIATIONS

By "DIALLIST"

The Components Show

THAT SUCH NUMBERS of visitors should have made special journeys to the Components Show from twentyone countries is an outsize feather in the cap of the R.E.C.M.F. This year there were more of them than ever. How important the exhibition has become in the eyes of the world may be gathered from the fact that not a few technical journals in other countries didn't just send reporters: their editors came themselves. Two whom I was delighted to meet (and who expressed unbounded admiration for what they had seen) were the editor of Audio Engineering from America and the editor of Toute la Radio from France. There were buyers, manufacturers, journalists. and others from all over the Empire, and from many countries in Western Europe, Asia, America and Africa. It is indeed a tribute to British components that so many people should find it well worth while to make long journeys to attend this small, private, three-day exhibition. The R.E.C.M.F. has been wise in adopting and adhering to the world's strictest and most rigid standards in materials, design and workmanship. Quality pays-and goes on paying.

Striving for Inefficiency

So POWERFUL are the a.m. and f.m. signals that I receive from the 20-kW Wrotham transmitter at a range of 50 miles with a pukka dipole mounted on a chimney stack, that I've been trying out aerials of lower and lower electrical efficiency with a view to discovering how far one can go before any marked falling off occurs. The arrangement I'm using at the moment cost 1s 8d, including the feeder. It consists of four yards of PVC-covered flex, the last 21ft of which were untwisted and straightened out, the single wires being stapled to right and left along a picture rail 8ft above the floor of a ground-floor room. Signal strength is still so ample that I shall have to work out something a good deal less effective before the answer is found. Metre-wave broadcasting when it comes (and may that be soon!) looks like having very great advantages over medium- and long-wave transmission. Among these, if f.m. is

selected, are: (1) coverage of the same service area with about a quarter of the transmitter output power; (2) excellent reception (except in fringe areas) with the simplest and cheapest of indoor aerials; (3) far greater freedom from background hiss and impulsive interference; and (4) much better quality.

A Nice Point

SETTLE A COUPLE of wireless enthusiasts into comfortable armchairs of an evening and it won't be long before they start an argument on one of the finer points of their pet subject. Man has probably been an argumentative animal ever since he found out how to use speech to convey his thoughts and ideas to others. Our discussions and debates to-day carry on his age-old attempt to arrive at the truth about this or that. On a recent chilly evening a friend and I got on to the subject of valves as we basked in the warmth of a welcome fire. He's a bit of an authority on matters wireless; but I had to take him up when he described the thermionic valve as basically a voltage amplifier. His thesis was that voltage changes applied to the grid give rise to similar but much larger changes at the anode when a load is provided. By choosing the kind of anode load suitable for the work in

hand you can pass these voltages on to another valve; or, you can use them as e.m.f.'s to drive current through a power-operated device such as a loudspeaker. I hold that the valve is essentially a power amplifier. There must be some resistance in the grid circuit and you can't get away from the fact that V2/R= W, however small the figures may be. An amplified copy of these small applied powers appears in the anode circuit and you can use it as suits your purpose by selecting the right kind of anode load. I firmly believe that that is the best way of picturing the working of an amplifying valve. What are your views?

Room for Improvement

Sorry Though I am to have to say it, there cannot be much doubt that too many of the h.t. batteries available nowadays are pretty poor things. I am thinking particularly of those made up of 4in × 21in cells, for they are by far the most widely used; but my criticisms apply equally to those with larger and smaller cells. If you care to work it out from the electrochemical equivalent of zinc, you'll find that a $\frac{3}{4}$ in $\times 2\frac{1}{8}$ in can, weighing about 12 grams, has, in theory, a possible current output of 10Ah. Of course, you cannot expect to get anything like that from it since the cell is usually discarded when the e.m.f. has fallen from 1.5V to 0.9V. Still, with a load of 8-10 mA you should iustifiably hope for a good bit more than the 0.7Ah to 1.1Ah that is all that I've been able to obtain of late from h.t. batteries with cells of this

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size. Again and again the overall e.m.f. of a battery has become unsteady after far too short a period of intermittent use. Once that happens, the set becomes increasingly noisy for an hour or two, and then packs up altogether. Test the battery with a high-resistance voltmeter and you'll find only tiny fractions of their stated e.m.f.s between certain tappingsusually near the middle. I have conducted post-mortems on scores of such batteries and have found in each case one or more perforated cells. Cell-perforation after a short period of intermittent use under a moderate load is something which, in my opinion, should not occur in a well-designed and well-made dry battery.

Full Speed Ahead

TOWARDS THE END OF MARCH an American friend asked me in one of his letters whether the imminence of the Coronation was producing record sales of television receivers. I replied that sales weren't too bad, except in Scotland, where comparatively few sets were being sold. "Possibly," I added, "the hardheaded Scots are holding their hands in the hope that the Budget will bring a reduction in purchase tax. If so, they are likely to be disappointed." My prediction could not have been more erroneous and I'm very glad of that. The reduced tax will mean bigger sales everywhere and, therefore, more money for research and development. It isn't always realized that television has had a hard battle to fight in this country. Our television service, the first in the world, was just getting nicely into its stride when the outbreak of war closed it down in the autumn of 1939. The TV research men were mobilized as the "backroom boys" of radar and had, so to speak, to beat their viewing screens into p.p.i. displays. Then when the war was over shortages of men, money and materials prevented the rapid development of our national television system. The heavy purchase tax imposed on receiving sets led inevitably to restricted sales and meant that with us television had to amble, instead of galloping, into its rightful position as the best of all sources of domestic With the lowering entertainment. of the tax, this Coronation year may well see a boom in television comparable with that which occurred in the early nineteen-twenties "sound" radio.

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Forestalling the Future?

WHEN our descendants celebrate the Queen's Golden Jubilee fortynine years hence, the newspapers will doubtless publish many articles dealing with various aspects of life in England during the early years of her reign. Our descendants are bound to be struck forcibly by the amazingly primitive and comfortless



Primitive and comfortless.

condition in which we were content to live having regard to the degree of scientific knowledge attained

of scientific knowledge attained.

I think that one of the things at which the people of the year 2002 will marvel most will be that we early Elizabethans of 1952 could make an atom bomb but failed to use the resources of radio to enable us to maintain communications with the rest of the world when journeying by land. The provision of radio-telephonic facilities on trains and other public vehicles, although technically possible is, I suppose, banned by bureaucrats. This is, however, equally true of private cars, for the P.M.G. has never bothered to equipeach telephone exchange with v.h.f. radio apparatus so that car owners, who installed the necessary equipment, could be linked with the national telephone system while travelling.

It is, however, a strange thing that if you own a boat and take your pleasure in it anywhere in the Thames Estuary the P.M.G. does provide a specially equipped telephone exchange for you so that you are as much "on the phone" as if you were at home. Recently I was visiting a friend who, like others of his kind, enjoys himself by spending his weekends on a small but well-equipped sailing craft.

I congratulated him on being "on the phone" in this special manner and said I wondered that he and others like him were not tempted, when temporarily abandoning ship on Monday mornings, to transfer the radio gear to their cars.

No reply was made to my observation but I did receive from my friend rather a queer look which might have been meant for silent reproof at my harbouring such subversive ideas; on the contrary, it might have been meant for withering contempt at my lack of sophistication. I just don't know. I merely record the facts and leave you to draw your own conclusions.

Silent TV

I WAS greatly interested in "Diallist's" prediction in the May issue that sets of the future may be provided with a three-position switch: sound and vision; vision only; sound only. But I certainly do not agree with him that more often than not the switch will be turned to the "sound-only" position. On the contrary, I think that if such a switch be provided it will almost invariably be turned to "vision only," and eventually the B.B.C. will radiate only silent TV.

I am led to this conclusion by the fact that owing to the development of a fault (which I have not yet found time to trace) in the "sound" side of my television set I have

lately been looking at silent TV. As a result I have become quite expert at lip reading. I can, in fact, follow the dialogue by this means far more easily than I could when I had to rely on my ears, as the sound was so often rendered unintelligible by the ceaseless chatter of Mrs. Free Grid and her fellow females discussing the shortcomings of their respective husbands.

their respective husbands.

Even when I have the house to myself the peace and enjoyment of watching this silent TV has to be experienced to be believed. It does mean, of course, that I have to give the programme full concentration if it is to be intelligible, but this is as it should be. I have no more patience with people who use sound broadcasting as a sort of soporific background to their

other activities than I have with those who go to the cinema and divide their attention between the screen and their own amateurish imitations of the amatory activities displayed on it. In common fairness, however, I must add that there is some excuse for their use of the cinema as an osculatorium as the proprietors fail to provide what used to be known in the U.S.A. as "necking niches" for those who don't want to see the film.

Inter-departmental Quiz

ANYTHING that smacks of the Totalitarian Police State is anathema to me. I must, therefore, register a very strong protest at the P.M.G.'s attempt to get the myrmidons of the Ministry of Transport to act as his Gestapo.

The current form which we all have to fill up when we want to renew our car licence asks bluntly "Is the vehicle fitted with a radio set?" If the answer is "Yes" we have to answer a further question which asks us if the set is separately licensed. These questions are, in my opinion, wholly irrelevant to the licensing of

I presume that if the wretched motorist answers "No" to the question which asks him if the set is licensed, the information will be passed on to the P.M.G. Supposing the motorist declines to answer this question on the grounds that no man is compelled to answer a question which might incriminate him, I wonder if the authorities would refuse to issue him a Road Fund licence? I wonder, too, whether the police have instructions and the necessary authority to ask about the licensing of any set they may see



Decibelless dialogue.

installed in the car when taking particulars for some misdemenour?

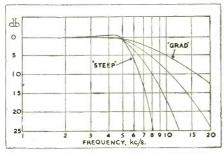
This sort of inter-departmental quiz is probably reciprocal and there is a danger that before long, when buying a radio licence at the local Post Office we may be asked if we have a clean driving licence. When applying for a marriage licence the bridegroom may, one day, be asked offensive questions about his income—at present the prerogative of the intended bride's father.

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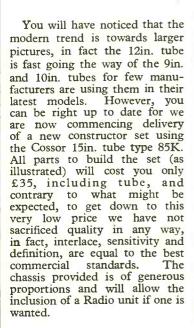
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1A4 1A5G	6F8 6F13	13D1	150A 150B	C2 C9	ECH42 ECL80	KL32 KL35	OM9 O202	SP61 SP210	U70 U71
1A6	6F14	13SPA 13VPA	185BT	C10	EC5	KTW61M	-	SP220	U74 U76
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1B4E	6H6	15	202MPG 202STH	C30B	EFM1	KTW73	PD220 PD3521	SP2220 SS210	U78 U81
1B5	6H7	15A2	202VPB	C36A	EF5	KTW74	PENB4	SS220PA	U82
1C1 1C5	6J5 6J7	15D1	202VP 210DDT	C36C C50B	EF6 EF8	KTW81M KTZ41	PENDD1360	SU25 SU61	U101 U142
107	618	15D2 15E	210HF	C50N	EF12	KTZ63	PENDD2530 PENDD4020	SU2150A	U14 5
1D6 1D5	6K5	17	210LF		EF13 EF22	KT4 KT8	PEN4VA	SW1	U281
1D3 1D7	6K6 6K7	18	210PG 210VPT	DAC1	EF36	KT24	PEN4DD	S3DD S8	U403 U404
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106	6L18 6L19	20LPT	220VPB 225du	DDT16	EF92 EK2	KT61 KT63	PEN383	mpg14	VPT4
1H4	6M1	21 A	230PEN	DD13 DD14	EK3	KT66	PEN428 PEN453DD	TBC14 TBL14	VP2B
1H20 1J6	6N7 6P25	22N41	240QP 290L4	DD40	EK32 EK91	KT71 KT72	PL33	TB9920	VP4 VP4A
1LA6E	6Q7	24 24A	244V	DD41 DD101	EL2	KT74	PL38 PL82	TCH24 TDD2A	VP4C
1LA4 1L4	6R7 6SA7	24E	301	DD207	EL32	KT76	PL83	TDD13C	VP13 VP13A
1P10	6SG7	25A8	302 307A	DD620	EL33 EL35	KT81 K23B	PM2A	TDD25 TE564	VP13B
1P11	68H7	25B5 25L6	329	DD818 DD2530	EL38	K30G	PM2B PM2HL	TF44	VP13C
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185	6SN7	26	408BU	DE3 DE5A	EL50	K40N	PM4 PM4DX	TH4A TH4B	VP20
1T4 1T5	6SQ7	27	410HF	DE5B	EL82	K50M	PM12	TH13C	VP23 VP28
1V	6S87 6S7	28D7	415PO 415XP	DF51	EL3 EM1	K50N K52	PM 12M	TH21C	VP41
2A6	6 T 7	30 31	424	DF91 DF92	EM4	K80A	PM14 PM20	TH30 TH29	VP41E
2A7	6U5 8U7	32E	425XP 442BU	DF495	EM35 EY91	K183 K535	PM22A	TH30C	VP133 VP1320
2A8	6W5	33	607G	DH2	EZ35	12000	PM25	TH233 TM1	VW48
2D2 2D4A	6Z¥5	34	625	DH63 DH76	EZ40	LD210	PM202 PPL4	TM14	V9 V914
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3V4 3Y4	7D5	39/44 41 MDG	1927	DL33 DL35	~~·	L13 L21DD	PP4118 PT/DD35DA	TSP4 TT4	W77 W81M
014	7D8 7H7	4bMH	1928	DL63	HD13 HD14	L38	PT10	TT4	W101M
4D1	7K7	41MHL 41MLF	2102 6153T	DL74 DL93	HD24	L63 L77	PT24A PT24/DAL	TT4A TX21	W142 W143
4DI 4THA	7Q7	41MP	9004	DL93 DL94	HL/DD1320	L410	PT230	T2	W 145
4TPB	7R7 7S7	41MRC 41MTA		DL145	HL4 HL13	L610	PV06-25	T20	W147
5		41MTL	AC/HL AC/HP5	DN41 DN 143	HL13C	ME17	PV230 PX230	T31 T32	W148
5U4	8 8A1	42	AC/P	DP495	HL21DD HL23	ME41 ME91	PY30		*****
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5¥4	8D3 9D2	42 A	AC/VHPZ	DW2	HL41DD HL42DD	MDH4	P8	UAF42 UBC41	X7 X17
5Z3		42E 42MPT	AC/044 AC2/HL	DW3 DW8	HL45DD	MHL13 MH4	P41 P140N	UBF80	X22 X24
6AB7	10C1 10D1	43IU	AC6/PEN	DO20	HL133DD	MH41	P215	UB41 UCH21	X63
6AC7	10D2	43	ASL125	D024	HL1320 HPB13	MH206 MH1118	P220	UCH42	X64
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6C5 6C6	12J7	77	B.2	EBF11	H21	N18	SD20	U18/20	ZD17
6C8	12K8	80		EBF32	H39	N37	8G410	U21	Z14
6C9 6C10	12Q7 12SA7	81 83	CBLL	EBF80	H63	N43	SP2	U22	Z21 Z22
6D1	12SF5	84	CBL31 CCH2	EBL21 EB4	H141D H607	N77 N145	SP2D SP4	U24	Z26
6D2	12507	101 104V	CCH2 CCH35	EB4 EB34	J249	N145 N150	SP4B.SP13	U25 U33	Z66
6D3 6D6	12SH7 12SJ7	104V 112A	CL4	EB41	KBC32	N152	SP13	U35	Z77 Z152

ELECTRONIC PRECISION EQUIPMENT LTD



- I5in. up to the minute Television for only £35, including Cossor Tube.
- H.P. Terms if required, i.e., send only £11/14/- deposit (carriage and insurance £1 extra).
- Working models demonstrated at both our Fleet Street or Ruislip branches.



The whole has been so arranged as to be particularly suitable for our popular Coronation Console cabinet, but there is no reason whatever why it cannot be fitted into any well made T.V. cabinet.

Technical features:

- A. Superhet circuit fed by a R.F. amplifier.
- B. Particularly carefully dimensioned Video stage.
- C. Diode damped interlace net-
- D. Line and frame blocking oscillators.
- E. Fly back EHT.
- F. Optional voltage doubler for aluminisation effect.

DATA. Full constructional data price 7/6, post free, are available on approval (if you decide not to make the set and return the data within 7 days 7/-will be refunded).

DEMONSTRATION. A made up chassis can be seen at Fleet Street, or Ruislip, and if you arrange to call during BBC transmission times, we will gladly demonstrate the excellent interlace and other qualities of which we are particularly proud.

HOW TO ORDER. All parts are available and total cost is £35, which includes 15in. tube, 20 valves, prepared metal chassis, in fact everything needed except cabinet and mask. Order form and parts list are included with the 7/6 data. H.P. Terms: £11.14.0 deposit then 12 monthly repayments of £2.7.0.

- OPPORTUNITY FOR ADVANCED CONSTRUCTORS

We continually need designs for novel radio and television test sets, servicing instruments, tuning units, pattern generators, etc., particularly those which can be made cheaply from Government surplus and other low priced valves and parts.

If you have made up any such equipment and would care to send us details we will willingly pay a fair price for the right to reproduce the data and/or equipment for our customers.

BOOKS & PUBLICATIONS



SERVICE DATA 100 service sheets, covering British receivers which have been sold in 100 service sheets, covering British receivers which have been sold in big quantities, and which every service engineer is ultimately bound to meet. The following makes are included: Aerodyne, Alba, Bush, Cossor, Ekco, Ever-Ready, Ferguson, Ferranti, G.E.C., H.M.V., Kolster Brandes, Lissen, McMichael, Marconi, Mullard, Murphy, Philco, Philos, Pye, Ultra. Undoubtedly a mine of information invaluable to all who earn their living from radio servicing. Price £1 for the complete folder.

Our folder No. 2 consists of 100 data sheets covering most of the popular American T.R.F. and superhet receivers "all dry" etc., which have been imported into this Country. Names include Sparton, Emmerson Admiral, Crossley, R.C.A. Victor etc. Each sheet gives circuit diagrams and component values alignment procedure, etc., etc. Price for the folder of 100 sheets is £1. Post free.

Post free.

FREE T.V. SERVICE SHEETS

The supplement to a new publication "Television Faults" contains complete circuit diagrams, component values, technical descriptions etc., of 6 popular T.V. receivers as follows:
Baird Everyman, T.29; Murphy, V.120C; English Electric, 1150M; Philips projection model 704A and 1800; Marconi, VT.53DA; Ultra V.711.
The book itself in the introductory chapter tabulates over 60 common faults from complete failures to such troubles as shadows in the corner. Against each fault symptom is given probable causes and a reference to the part of the book where more detailed information can be found. Following the quick fault finding guide are 10 chapters, each giving typical circuits and data indicating the actual components likely to be at fault. The book is invaluable to novice and experienced T.V. serviceman components likely to be at fault. The book is invaluable to novice and experienced T.V. serviceman alike because it contains a wealth of practical experience and priced at only 5/- it will undoubtedly save its cost the first time you have to refer to it. Order now to ensure getting the free supplement.

THE ELPREQER

This describes a completely effective but most inexpensive Signal Tracer that can be built in one hour at a total cost of 12/6. Price 1/6.

A VIBRATOR UNIT FOR 2 VOLT BATTERY RECEIVERS

Describes how an inexpensive unit, which will save its cost many times over, can be built and operated. Price 2/6. With Blueprint.

A VIBRATOR UNIT FOR 1.4 VOLT BATTERY RECEIVERS
Shows how to make a unit which will permit you to dispense with expensive dry batteries. You can work your little set from a 2 volt accumulator which can be re-charged. Price 2/6 with blueprint.

ELECTRONIC PRECISION EQUIPMENT LTD

FOR OUTSTANDING PERFORMANCE

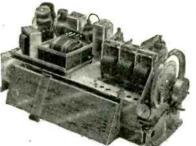
Six Wavebands Model B. Six Wavebands, 11-15 metres continuous in 5 ranges (4 Bandspread) and M.W. 185-550 metres. Six position Tone Switch (3 Radio -3 Gram). Price £15/15/-, plus 7/6 carr. and insurance, or H.P. terms £5/9/= deposit. Model B3. Three waveband, Long, Medium, Short, Gram switching on wave change switch. 3 position Tone. Price £12/12/-, plus 7/6 carr. and insurance, or H.P. terms £4/6/- deposit. Both chassis 11½in. × 7in. × Both chassis 11½in. × 7in. × Model B.



Both chassis 111in. × 7in. × 8in. high. Latest type valves: 6BE6, 6BA6, 6AT7, 6BW6, 6X4. A.C. mains operated, flywheel tuning, negative feedback over entire audio section, engraved knobs, fully guaranteed.

BUILT TO HIGHEST PERFORMANCE STANDARD AND SPECIFICATION

7 VALVE 5 WAVEBAND RADIO CHASSIS



GIVE AWAY PRICE

> only 47/deposit.

Less valves and power pack.

A famous set by a famous manufacturer. Undoubtedly a serious listener's receiver. Among many special features are an H.F. stage and tuning indicator. Tunes up to 11 metre band. Price complete with valves but less speaker, £14/19/6. H.P. terms £5/10/- deposit and 12 monthly payments of £1/10/-. We have a few left, less valves and power pack, otherwise in good condition; they definitely have never been used. Price £6/19/6, or £2/7/- deposit and 11 monthly payments of 10/9, plus 15/- carriage.



AMPLIFIER

(For A.C./D.C. working)

This is on an aluminium chassis, The layout is neat and simple and provision is made and in fact holes are drilled so that

fact holes are drilled so that tuning condenser and coil pack may be easily fitted if same are required. Alternatively this vacant space can be used for mounting a control panel to which various points of the circuit can be brought to plugs, thus making a signal tracer which is invaluable for radio and T.V. servicing. It uses one of the latest valve line-ups, as follows: 1487 Triode Hexode, 7B7 I.F. Amplifier, 7C6 D.D.T., 35A5 output, 35Z3 Rectifier. The I.F.s are present at 465 ke/s., but are variable over a fairly wide range. Price £6/10/- complete with valves and 8in. speaker. H.P. is 63/- deposit.

R1155 COMMUNICATION RECEIVER FOR ONLY £2/14/-DEPOSIT



This set, as most will know, is con-sidered to be one of the finest communications receivers available to-day. The frequency range is 75 kc/s to 18 Mc/s. It is complete with 10 valves and is fitted in a black metal

in a black metal case. Made for the R.A.F., so obviously a robust receiver which will give years of service. Slightly used but completely overhauled and guaranteed in perfect working order. PRICE £7/19/6 or will be sent against a deposit of £2/14/-, balance of 12 monthly payments of 11/6. If you cannot call to collect please include an additional 10/- to cover cost of transit and carriage. This partly returnable to you if and when you return the transit case.

MAINS POWER PACK FOR R.1155
With Pentode output stage. Plugs into socket on receiver so no internal modifications are required. Price £5/10/- complete with 5in. speaker ready to work, carriage 3/6.

BOOKS & PUBLICATIONS



"DEMOBBED VALVES."
Gives the commercial equivalents of many thousands of service valves, and conversely gives the service equivalent of many thousands of commercial type valves, an invaluable publication recently revised. Price 2/3.

"AN ELECTRONIC TIMER."
Shows how to build a device for controlling timed operations. The timer can be set to any timing up to 3 minutes. Price 2/3, "THE ELECTRONIC SWITCH."
Shows how to make a device for switching without mechanical contact. Price 2/3, "THE IMPULSE RELAY." Explains the working of an ingenious relay, and gives several circuits including radio control. Price 1/9. "THE OCCASIONAL T.R.F."
Shows how to build a T.R.F. Receiver for medium and long wave reception, of looks and quality output comparable with sets priced between £10 and £14. This costs less than £6 to build including cabinet. Price 1/6. "VALVE EQUIVALENTS."
These are the best equivalents charts available today. Also the booklet can be used for keeping records of valve stocks. Price 2/6. VISUAL ALIGNMENT " AN ELECTRONIC TIMER." ing records of valve stocks. Price 2/6. VISUAL ALIGNMENT SIGNAL GENERATOR. Reprint from "Radio Constructor" describes a very useful combined signal generator and oscilloscope.

RADIO HEARING AIDER
The world for a deaf person must be particularly blank and monotonous, and a hearing aid which will function as a radio when not needed for hearing should help considerably. Constructional data and technical notes dealing with this are available. Price 2/6. Only standard parts are incorporated therefore the constructor ated therefore the constructor will have no difficulty in making this up.

LF. ALIGNMENT PEAKS
This book gives the I.F. frequencies of more than 4,700 receivers including British, American and Continental types. Every popular British set is covered, and in addition hints on finding the frequencies of unknown British sets are also given. Sale price 3/9.

EX-GOVT. CIRCUITS
These give circuit diagrams and details of Ex-Government receivers and equipment. In practically all cases the information has been extracted from

	Linain	TAOLE
official pu	ducations.	
AR.88D	Ind.62	R.1355
A.1134	Ind.6K	R.F.24
A.1368	Ind.62A	R.F.25
A.3611	R.76	R.F.26
AN/APA1	R.78	R.F.27
A.S.B.3	R.103	R28/
BC.221	R.107	ARC5
BC.312	R.109	SCR269A
BC342	R.208	SCR522
BC.348	R.1082	T.1154
BC.453	R.1116	TR.1196
BC.454	R.1116/A	TR.18
BC.455	R.1124/25	
BC.624	R.1147	All 1/6
BC.625A	R.1132/	each or
BC.433G	1481	assorted
BC.1206	R.1155	dozen @
I.F.F.	R.1224A	12/
	,	

TOOLS, ETC. "Q-MAX" CHASSIS CUTTERS.

The simplest and quickest tool

The simplest and quickest tool for cutting holes in aluminium or steel chassis. Comprises die and punch operated by Allen key. A separate die and punch is required for each size.

hole (B7G, etc.) 11/6
hole (B8A, etc.) 12/6 Same key fits these three, price hole 11 hole (Octal base) ...
11 hole (English bases) ...
12 hole 16/6 16/6 18" hole 11" hole (EF50, etc.) 13" hole 18/6

2 3/32" hole 21" hole 1" x 1" square hole.... Same key fits these nine, price

METAL DIVIDERS.



Really well made for Government workshops. Ideal for marking out on metal chassis. Price 3/6.

HARMONIC GENERATOR

A harmonic generator is well worth making up, because it oscillates with a wave form having harmonics extending right into the radio frequencies. To trim a straight set therefore it is only necessary to inject its output into the aerial and adjust trimmers for maximum audio output, similarly with a superhet a great saving of time can be effected.

We will supply this as a kit of parts, with constructional details price 15/- for battery, and 30/- for mains operation; data available separately, price 1/6.

SPRING LOADED TERMINAL BLOCK Fully insula

ted so is ideal for mains. terminal point

fitted on bench of workshop or laboratory. Also suitable for temporary hook ups when testing components, etc., will save its cost the first week of use. Price 3/6.



SPRAY GUN
Hand operated, ideal to put a good finish on a completed chassis, and for respraying valves etc. (completes the perfect job). Price 15/6 complete with instructions, plus 9d. postage.



BUILD AN OUTPUT METER Switch, Transformer, meter and rectifier to build a dual range O.P. Meter with instructions. £1/15/-.

ELECTRONIC PRECISION EQUIPMENT LTD. LOW PRICED TEST GEAR, ETC.

T.V. SIGNAL AND PATTERN GENERATOR Cost of all components, valves, etc., only 29/6.

0

Although this generator can be built and used by any beginner it is at the same time a most useful instrument for the more advanced worker.

worker.

It can be tuned to the vision channel and will produce a pattern on the face of the C.R. tube.

Alternatively if tuned to the sound channel it will produce an audible signal in the loudspeaker.

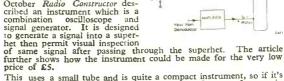
Thus its owner will become in-dependent of B.B.C. transmissions and can fault-find or test at any time. It operates entirely from A.C. mains and is quite suitable for use with superhet or straight receivers

receivers. A complete kit of parts (in fact everything except the cabinet) with full constructional and operational data will be supplied for 29/6, plus 2/6 post and insurance, alternatively data is available separately, price 2/6 (credited if you buy the kit later).

Cabinets as per the illustrated prototype are available price 17/6

VISUAL ALIGNMENT SIGNAL GENERATOR.

An interesting article in the October Radio Constructor described an instrument which is a



This uses a small tube and is quite a compact instrument, so if it's only use is that of checking the band pass on the I.F. transformers, in a high fidelity receiver, its construction is justified. It can, of course, be used for a variety of different jobs other than the alignment of I.F.'s, in fact, it is a good servicing 'scope.

We can supply a complete kit of parts for £5 containing valves, tube and all components except shassis and case. A re-print of the article from the Radio Constructor is available price 9d. The power pack not shown on the block diagram is, nevertheless, included in the kit.

CONTINUOUSLY VARIABLE MAINS TRANSFORMER

As described in the "Wireless World," August 1951 issue, this has a primary tapped at 81 v. and four secondaries of 1 v., 3 v., 9 v. and 27 v. respectively.

By suitable selection of windings, voltage in steps of 1 v. up to 40 v. can be obtained with isolation from the mains at 100 watt rating, e.g., 20 amps at 5 v. and 21 amps at 40 v. By adding the primary the voltage can be varied in steps of 1 v. up to 280 v. This is undoubtedly an essential piece of equipment in all experimental laboratories. Price £3/10/- each.

TRIMMER TOOL KIT.



WELD TYPE WIRE JOINTER

This jointer melts the wires and causes the metal of each to run together, thus making a strong and permanent weld. It obviously is not intended to replace the soldering iron but nevertheless is ideal for making joints that have, for instance, to withstand heat, vibration, chemical action, etc. In many cases also this method is faster than soldering and there can be a considerable saving of current. Price 9/6. Or complete with enclosed mains transformer 29/6.

SUNDRIES

SPINDLE EXTENDERS & COUPLINGS

Small type. Solid Brass with two Grub Screw, 7d. each.
Flexible Type. These ordinary Insulated. These have additional spindle moulded permanently and tend the control spindle.

they extend the control spindle by 1-1½". 1/6 each.
Bellows Coupling. These are ideal for slug tuning as they extend as well as bend. 1/9 each.

CLEAR CEMENT. Almost instantaneous drying for coil winding and all repairs, 1/6 per tube.

28-

HARD-WARE. Service man's 3 gross sorted nuts

1111111 bolts and washers, all useful sizes. Price 6/6. We en-deavour to main-tain stocks of wood screws, steel and brass round head prass round nead and counter sunk. Parker Kalon self cutting screws, washers and stud-ding. Send us your orders and enquir-

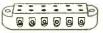


RUBBER GROMMETS.

½", ½", ½", 1d. each. ½", 1", 1½", 1½d. each. Serviceman's packet of 24 assorted sizes, 2/-.

CROCODILE CLIPS

Small instrument, of Car Battery type, 9d. 6d. Large



TERMINAL BLOCKS

Heavy duty type, 5 way 4in. long × 1in. wide × 1½in. high. 30 amp. rating. Price 1/6. Heavy Duty type, 6 way porcelain 15 amp. rating. Price 1/6. Heavy Duty type, 5 way porcelain 15 amp. rating. Price 1/3. Heavy Duty type, 3 way porcelain 15 amp. rating. Price 9d.

OCTOPUS CLIPS



An ideal clip for fixing anything to a rod or pole, this is self adjusting from 1 in. to 4 in. Price 1/- each

MILLIBAR BARO-METER, 7/6 The heart of a barometer bellows metal which will ex-



pand and contract with the varying air pressure. The aircraft altimeter works on the same principle, a series of gears and lever amplifying the expansion and contraction of the bellows and so works the pointer. We can offer the ex-R.A.F. Sensitive Altimeter slightly faulty but containing the essential bellows, gears, wheels, etc., from which a good barometer can be made. Price only 7/6, plus 1/-post. pand and conpost

- ELECTRONIC PRECISION EQUIPMENT LTD -

ELECTRICAL BARGAINS ELECTRICAL BARGAINS In addition to our large range of radio accessories we also carry a good stock of electrical wiring accessories; details of a few of these can be found below:—

******	COLL	- I	O CLIAN	
T.R.S				ASS
1/.044	Twin	flat		 9d.
3/.029	Twir	flat		 1/-
3/.029	Twin	with	earth	 1/3
3/.020				 1/6
3/.036				1/4
3/.036				1/7
3/.0363	3 core	flat		 2/-
7/.029	Twin	flat		 1/6
7/.029	Twin	with	earth	 1/11
7/.036	Twin	flat		 2/9
7/.036	Twin	with	earth:	 3/3
7/.064	Twin	flat		 4/9
TELL				

LEAD COVERED CABLES 250 v. CLASS

3/.029 3 core									,	2	3
3/.036 3 core										2	8
										3	3
3/.036 twin					,					2	_
										2/	9
7/.064 twin				٠	٠	*	٠			5/	-
		_	_		-	_			 		

WAR EMERGENCY TYPE CABLES 250 v. CLASS These are P.V.C. or rubber in-sulated, laid flat then braided with cotton and compounded :

7/.029	3-cor	e flat						2/-
7/.044	twin:	flat				٠.		2/-
7/.064	twin :	Hat						3/3

MULTICORED FLEXIBLES All are suitable for mains work as the separate conductors are very well insulated, then they covered overall either with hard rubber, plastic or waterproof braiding:

10 core										2/6
7 core							٠		,	2/-
5 core										1/-



5 AMP SURFACE SWITCHES HICRAFT. OblongBrown Plastic 1-way 1/3 each. Oblong White Plastic 1-way,

	ach.
Oblong Brown 2-way	 1/6
Oblong White 2-way	 1/6 ,,
Round Brown 1-way	 1/3 ,,
Round White 1-way	 1/3 ,,
Round Brown 2-way	 1/6 ,,
Dound White 2 were	116

SPECIAL THIS MONTH

Customers ordering quantities of bakelite accessories can take discounts as follows: 1 dozen of one item 25%. gross mixed or one item 33 3 %.

SOCKETS HICRAFT

Flush type for skirtings, 5 amp. 3-pin shuttered, 3-pin 1/3 each; ditto with switch, 2/3 ditto each.

in dozens.





CEILING HICRAFT

With cordand acorn. Brown or White, 1-way, 3/9 each; 2-way, each.

LAMP HOLDERS
Bakelite, 1/- each or 10/6 doz.
Bakelite skirted Batten holder, 1/6 or 15/- doz.

Bakelite type threaded for §in. with HO skirt, 1/6.

10 per cent. discount if bought

BARGAIN FOR CONSTRUCTORS



Special this month is the Portable Special this month is the Portable illustrated alongside. We offer a bakelite cabinet with carrying handle, metal chassis, battery housing and two waveband dial, all for 27/6, plus 5/- carr. and insurance. This cabinet and set of parts is ideal for making up either an all dry battery receiver for holidays, picnics, etc., or a battery mains set for everyday use. Constructional details of two suitable circuits using 1.5 v. valves 1R5, etc., will be given free with cabinet assembly, or is available separately price 1/6 post free.

SPECIAL RADIOGRAM OFFER

To those who want an auto radiogram at a low price, we offer the cabinet illustrated alongside complete with Collaro three speed record changer with dual purpose crystal pick up, at a special bargain price of £17/16/8, plus 12/6 carriage and insurance or H.P. terms £6/7/- deposit.

3 colour scale, scale pan, chassis, pulley, driving head, springs, etc., etc., to suit the radiogram and two radio cabinets are available as a parcel at 15/-, plus 1/6 post.

Cabinet separately £7/10/- (or £2/10/- deposit), plus 10/- carriage and insurance.



A Superhet Chassis to fit these two cabinets is now available. L.M. and S. waves, 3 colour scale, A.V.C. Tone control etc., complete with 8in. P.M. Speaker. Price £9/19/6 or H.P. £3/7/- deposit. Carriage 7/6 extra.

TABLE MODEL RADIO

This very nice-looking cabinet will take the same scale and chassis as the radiogram above, and we are able to offer this at the bargain price of 37/6, plus 3/6 post and insurance.

THE REGINA

T.V. Console Cabinet, undrilled, but cut for 12in. tube, with adjustable platform. This cabinet looks really superior and is ideal for all popular sets-Viewmaster, Tele-King, etc. Price £7/17/6. Carriage 10/- extra. Price £7/17/6.



The table model illustrated is available in fair quantity at £3/17/6, plus 7/6 carriage and insurance, which price includes the armour plate glass and surround.

Mechanical details for this Table Model are available as a parcel: Punched and prepared metal chassis, punched outrigger valve plate with spacers, 12in. Tube Clamping ring, tube rear support brackets, etc. Price 25/-, plus 2/6 post.

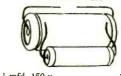


"MIDGETRONIC" Radio Cabinet

This pleasing small cabinet is in bakelite and is supplied complete with dial ring, pointer as illustrated but less knobs, also included is metal chassis and hardboard back. Price 15/-, plus 2/6 postage and packing.

To ensure receiving prompt reply, please enclose stamped addressed envelope, when writing for additional details.

ELECTROLYTIC CONDENSERS



	1 mfd. 150 v	1/-
	1 mfd. 250 v	1/-
	1 mfd. 450 v.	1/3
	2 mfd, 350 v.	1/3
	2 mfd. 450 v.	1/6
	4 mfd. 350 v.	1/8
	4 mfd. 450 v.	1/10
	4 mfd. 450 v. 8 mfd. 150 v.	1/10
	8 mfd. 350 v.	1/6
		2/-
	8 mfd. 450 v.	2/6
	8 mfd. 500 v	3/3
	8 mfd. 500 v. centre-screw	
	fixing	1/6
	8 mfd, 600 v. centre-screw	-1-
	fixing	1/9
	fixing 16 mfd. 350 v.	2/9
	16 mfd. 450 v.	
		3/6
	16 mfd. 500 v.	4/9
	32 mfd. 150 v.	2 3
	32 mfd. 250 v	2/3
	32 mfd. 350 v	2/9
	32 mfd, 350 v. 8 mfd. × 8 mfd. 350 v	3/-
l	8 mfd. × 8 mfd. 450 v.	3/9
ļ	8 mfd. × 8 mfd. 500 v.	3/9
١	8 mfd. × 8 mfd. 500 v 8 mfd. × 16 mfd. 450 v	4/9
	8 mfd. × 16 mfd. 500 v	6/-
	16 mfd. × 16 mfd. 450 v.	6/-
	16 mfd × 16 mfd 500	7/-
	16 mfd. × 16 mfd. 500 v. 20 mfd. × 20 mfd. 200 v.	4/-
	24 mfd × 24 mfd 200 -	
	24 mfd, × 24 mfd, 200 v. 25 mfd, × 25 mfd, 200 v. 32 mfd, × 32 mfd, 150 v.	4/6
	25 mid. × 25 mid. 200 v.	4/9
	32 mid. × 32 mid. 150 v.	4/9
	$32 \text{ mfd.} \times 32 \text{ mfd.} 450 \text{ v.}$	6/9
	100 mfd. × 100 mfd. 150 v.	5/6
	10 mfd, 25 v.	1/
	12 mfd. 50 v	1/4
	20 mfd. 50 v	1/6
	25 mfd. 25 v	1/6
	25 mfd. 50 v	2/-
	50 mfd. 12 v	9d.
	50 mfd. 50 v	2/3
	250 mfd 12 v	2/3
	250 mfd. 12 v.	2/3
	250 mfd. 25 v.	2/6
	8 mfd. × 8 mfd. × 8 mfd.	
	450 v	3/9



.0005 2-GANG CONDENSER Ceramic insulation with "no back lash" gear drive. Drive easily removed if required, when con-denser becomes a standard type with long spindle. Price 8/6 cach.



Two socket engraved L.S., 6d. each. Bin. C16B.

Two socket engraved A.E., 6d. each. Bin. C18A. Two socket engraved P.U., 6d. each. Bin. C19B.

Two socket engraved Dipole 6d. each. Bin. C19B.

Two socket plain, 5d. each. Bin. C18B.

Three socket engraved DIP and E, 9d. each. Bin. C16D.

Three socket engraved A1, A2 and E, 9d. each. Bin. C19D. Four socket engraved A.E. Pick-up, 9d. each, Bin. C19E.

Four socket engraved P.U. Ext. L.S., 9d. each. Bin. C16E. Five socket plain, 9d. each. Bin. C16C.

RADIO HEARING AIDER

The world for a deaf person must be particularly blank and mono-tonous, and a hearing aid which tonous, and a hearing aid which will function as a radio when not needed for hearing should help considerably. Due to Purchase Tax no kit of parts for this will be made available, but constructional data and technical notes dealing with this are available, price 2/6. Only standard parts are incorporated, therefore the constructor will have no difficulty in making this up. in making this up.

HIGH VOLTAGE VALVE HOLDERS



For four or five pin valves. Price 2/9 each.

2%in. TUBE MOUNTING

metal This comprises moulded rubber tube mounting, front escutcheon, 4 screws and Perspex window with engraved cursor lines, 5/- complete.

V.C.R. 139

Tube base with mu-metal screen,

MU-METAL SHIELD

For 6in. tube V.C.R.97, etc., 10/- per pair.

6in. TUBE MOUNTING

Shock proof rubber mounted and adjustable, i.e., tube may be turned, with tube holder, 4/6 each.

HIGH VOLTAGE

Insulated spindle couplers, 1/6



AUTO-MATIC D.C. STARTER

For remote ontrol D.C. motor between 1 and 3 kw., adjust-ment for 100 v. or 230 v. Unused and in

Unused and in first-class condition, complete with metal and wired glass cover. Price on request.

6KV. EHT FOR 35/-

6KV. R.F. EHT FOR 35/-6KV, R.F. EHT kit, comprises 2 valves, mains transformer, con-densers, coil formers and wiring instructions. Price 35/- com-plete. Data available separately, price 2/6 plete. In price 2/6.

SPECIAL LOW PRICES

AMPLIFIER UNIT A 1134A

This is a 2-stage intercom and Tx pre-amplifier with transformers, etc. Easily modified as gram etc. Easily modified as gram amplifier or dictaphone, etc. Complete with 2 2 v. valves, OPP and Triode. Price only 9/6, plus 1/6 post and packing. Circuit diagram, free with unit, or separately, 1/6.

MORSE OSCILLATOR UNIT

Variable note and variable output, fitted with jack for external modulation, 2 v. valves. Price 8/6, plus 2/post and packing.

STOP PRESS

Weymouth miniature Coil Packs at half price. Long, Medium and Short wavebands with gram position. Size, 3½in. ×3in. ×1½in., single hole fixing.

Limited quantity, price 22/6, plus 1/6 post.
12 for £12, post free.

ELECTRONIC PRECISION EQUIPMENT LTD

RADIO DIALS AND SCALES



Note.—Type A. Pointer moves from side to side. Type

moves up and down.

Type C. Pointer
rotates rotates centrally.

Type D. Pointer rotates in semi-circle

rotates in semi-circle from bottom centre.

Minimum dial openings are quoted to help you if you the dial could be cut down.

Post and position at

Post and packing charges. Owing to the fragile nature of these dials, 2/- extra must be included to cover post and packing.

Quantity Prices. Where 12 or more of one type are required discount is 25 per cent.; 144 or more, 33\frac{1}{2} per cent. (there are no carriage charges on quantity orders).

GLASS DIALS

Туре	Gl Si Wide	ass ze High	Min. Dial Opening	Wavebands	Colours	Price	List No.
A	in. 12	in. 6½	in. in. 8½×4½	M., S1, S2, S3, S4.	4	3/6	C73A
BBACABBADBDBAABBACBACCC	6 443 384 6 6 9 6 7 6 7 8 9 4 7 1 5 4 5 7 5 5	7113357777575754874704566	51 × 61 2 1 × 2 3 7 × 4 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	M., \$1 & \$2 L., M. & \$5 L., M.	3 3 3 3 2 3 2 3 1 3 2 3 3 3 3 3 3 3 3 3	3/6 3/6 3/6 1/6 4/6 2/6 3/6 2/6 3/6 3/6 3/6 3/6 3/6 3/6 3/6 2/6 3/6 3/6 2/6 3/6 3/6 3/6 3/6 3/6 3/6 3/6 3/6 3/6 3	C74A C77A C81A C81A C83A C84A C85A C90A C91A C92A C92A C95A C96A C96A C97A C96A C97A C101A C101A C102A

Metal, Fibre and Card Dials

A	10½	3 !	8 ×2	M., S1, S2, S3 & S4.	Metal	2/6	C75A
C	4 3 7		3 ×3 21×23		Fibre Card	1/6 9d.	C82A C86A
Ď	5 1	5	4 × 21	L., M. & S.	Card	9d.	C87A

EXCEPTIONAL I.F. TRANSFORMERS

Ferro enclosed and cored, 465KC adjustable, very high Q and gain. Ideal for car radios, personnel sets, etc. Dimensions: 12in. high x lin. dia. Price 8/6 per pair.

THIS MONTH'S SNIP

Owing to a fortunate bulk purchase we are able to offer .1 500 v. Tubular Condensers at 7/6 per dozen. These are not Government surplus but are recent manufacture of one of our most famous condenser firms and have been stored in air-tight tins.

COLLARO AUTO-CHANGER

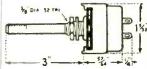


Last year we purchased a large quantity of the Collaro Auto record changers type RC/511, 3 speed, suitable for all types of records with the latest crystal pick-up, but these have been selling very rapidly, and it may well be that unless you buy one this month you will not be able to again, at this special price. We urge you, therefore to order right away, the price is 11 gns., plus 7/6 carriage and insurance.



ELECTRONIC TIMER

With this instrument processes which operate over a specified time can be controlled automatispecified to control exposures, etc. The instrument can be set to any length of time from a fraction of length of time from a fraction of a second up to three minutes, and it can be made to switch the appliance on or off. Circuit diagram and instructions, 2/3. Complete kit of parts, including valves, mains transformer, power pack, sensitive relay, potentiometer and metal case, 69/6.

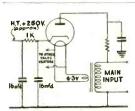


VOLUME CONTROLS

We carry a full range of standard-We carry a full range of standard-size volume controls from 2K to 2 meg. Prices are: less switch, 3/-; Single pole switch, 4/-; double pole switch, 5/-. We can also supply midget-type controls, less switch, 4/-; single pole switch, 5/9; double pole switch, 6/6. Each of these midget con-trols has a serial number and carries a 12-month guarantee by the makers; they are made on the new moulded track principle and really do perform well.

SHORT WAVE TUNING HEART

Coil Pack, 2 gang condenser, IF transformers and calibrated scale for frequency coverage of 13-37 metres, 37-100 metres and 200-500 metres. Price 39/6 complete with circuit diagram.



A POWER PACK FOR Efficient power supply, O.K. for receiver, amplifier, Efficient power supply, O.K. for operating a receiver, amplifier, instrument or other device requiring up to 60 mA. at approx. 250 v. Parcel consists of filament transformer, rectifying valve, smoothing resistor and 16×16 mfd. 350 v. electrolytic condenser. Note the filament transformer will supply enough current to operate 3 or 4 other 6.3 valves.

M.E.M. SWITCH **FUSES**

10 amp. all Porcelain 250 v., 6/- each. 15 amp. Ironclad, 10/6 each, plus 1/6 post. 30 amp. Ironclad, 16/6 each, plus 2/6

post.





CEILING FAN

This model, made by Revo, incorporates a series-wound totally enclosed ball bearing motor of robust construction and noiseless robust construction and noiseless operation. The fan has a blade diameter of 36in, and is supplied with 20in, suspension tube and ceiling canopy. All finished white cellulose enamel. The voltage working is 230-250 v. D.C. Revo catalogue number D12288. Price £7/107.

TWO ITEMS FOR V.C.R.97 USERS

(1) RF. E.H.T. UNIT

take the place of the mains E.H.T. transformer, has following advantages:

(a) Is more reliable.(b) Is cheaper.

(c) Can be repaired.
Complete kit comprises 2 valves, smoothing condenser, filament transformer and all necessary parts. Price 20/-, plus 1/6 post. Constructional and operational data free with kit or available separately, price 2/6.

(2) INTERNAL MAGNIFIER

The kit comprises a veneered and polished wooden surround, special mask, oil filled enlarger and four chrome-head fixing screws.

Has these advantages:—

(a) It gives the impression of being a standard 9in. tube.

(b) Saves the cost of a 6in. mask.

(c) Protects magnifier from accidental damage.

(d) Is equally suitable for use with a 9in, tube. Price of kit 39/6, plus 2/6 post and insurance.

PYREX AERIAL INSULATORS



Ideal for aerial connections through cabin walls or through panels. Consists panels. Consists of glass dome with threaded rod and terminal ends, and metal fixing flange Price 2/each.

STAND OFF **INSULATOR**

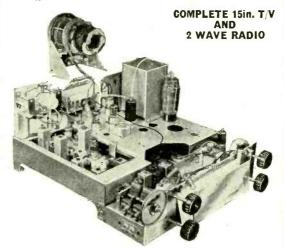
Vitreous porcelain. Price 1/- each or 10/- doz.



ELECTRONIC PRECISION EQUIPMENT LTD.

READY MADE T.V.

Combined 15in. Television and 2-wave Radio chassis. Brand New-Ready to work—Fully guaranteed. Complete with Tube, Mask, knobs and speaker, Adjustable to any channel. Price £55, carriage and ins. £2.



TECHNICAL DESCRIPTION

TELEVISION. This is an A.C. chassis of Superhet Design employing 14 valves, viz.: 7 6F1 Mazda, 1 CP25 Mazda, 2 6D2 Mazda, 1 6L18 Mazda, 1 EY51 Mullard, 1 EL38 Mullard, 1 6SN7 Brimar. Tube is Cossor 85K.

Special features: Focus, PM with pre-set centring and tilting facilities, and continuously adjustable focus control, accessible to the

user.

Picture Tone Control: 3-position Gradation Control which adjusts the level of vision interference suppression.

Aerial Attenuation: A screen Aerial Attenuator Box is provided on the chassis for use in the vicinity of transmitters.

Sensitivity: 50 micro volts for peak white on the screen giving extremely good results in fringe areas.

Picture Centring: 2 slider controls accessible from the back enable the picture to be moved horizontally or vertically to the centre of

RADIO. This is a 4-valve A.C./D.C. chassis employing superhet principle. A two wave band tunable dial for the long and medium

-VIEW MASTER OWNERS

You probably know that a 15in, tube gives approximately three times ar many square inches of actual picture as does a 9in, tube. You mry not know, however, that without any modification at all your View Master will scan the 15in. Cossor type 85K which we offer for cash or on H.P. If you would like to go over to the big 15in.picture, the easy way is to send for "View Master Big Picture Parcel" as follows:

Parcel "as follows:

1. 15in tube, type 85K.

2. Moulded rubber mask.

3. Tube clamping ring.

4. Spei ial ion trap.

We offer the above six items at less than what a new 9in. or 12in. tube alone would cost, namely, £14/10/- cash with order or £5 deposit and balance over 12 months, carriage 12/6. Limited quantity only at this price due to fortunate purchase of set manufacture's surplus C.R.T. stocks, so order by return.

LONG & MEDIUM WAVE OCCASIONAL RADIO Yours for £2 . 1 . 6 (Deposit)

You will find that the building of our all-mains radio receivers is simplicity itself, and the more you make the less time each takes, everything down to the last nut and bolt is supplied,



last nut and bolt is supplied, and everything fits together in a professional manner. When finished the receiver looks and plays as well as those being offered in radio shops at anything between £10 and £14. The one illustrated above we call the "Occasional," in a choice of colours, Ivory or Walnut and the T.R.F. costs £61/16 to make, H.P. nerms being £2/1/6 deposit and 10 monthly payments of 10/6.



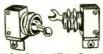
ENAMELLED WIRE

(On wooden reels)					
s.w.G.	2 oz. Reel	4 oz. Reel			
16	1/3	1/10			
18	1/3	2/-			
20	1/4	2/2			
22	1/5	2/4			
24	1/6	2/6			
26	1/7	2/8			
27	1/8	2/9			
28	1/8	2/10			
30	1/9	3/-			
31	1/10	3/1			
32	1/10	3/2			
33	1/11	3/3			
34	1/11	3/4			
36	2/-	3/6			
38	2/2	3/10			
40	2/4	4/2			

TINNED	COPPER	WIRE
S.W.G.	2 oz. Reel	4 oz. Reel
16	1/3	1/10
18	1/5	2/-
20	1/4	2/2
22	1/5	2/5

DOUBLE SILK COVERED WIRE

S.W.G.	2 oz. Reel	4 oz. Reel
16	1/3	1/10
18	1/3	1/11
19	1/5	2/3
20	1/6	2/6
22	1/8	2/10
23	1/9	3/-
24	1/9	3/-
26	1/11	3/4
27	2/-	3/6
28	2/1	3/8
29	2/2	3/10
30	2/3	4/-
31	2/4	4/2
32	2/6	4/6
33	2/9	5/-
34	2/10	5/2
35	3/-	5/6
36	3/2	5/10
38	3/6	6/6
39	3/9	-
40	4/-	7/6
41	2/3	_
42	2/6	-



TOGGLE SWITCHES

Metal body standard size, made by a leading maker. Available with round dolly or with special V cut dolly. State which type when ordering. Price while when ordering. stocks last only 2/3.

GERMANIUM DIODES Wire Ended

Several alternative types available

Types Equivalents Price Red CG4 GEX55, WG7A 10/-Green CG5, GEX45, WG7B, GEX33, WG4A

Orange CG6, GEX45, WG5A 7/6 7/6

Green/ Orange For super detectors Yellow For Crystal Re-5/6 ceivers 4/6 For General Experi-

mental purposes . . 2/3
Parcel containing one each of the above, price 30/-.

EX-GOVT. VALVES





CV922 CV1000 CV1018 CV1020 CV1023 CV2579

CV2539 CV2579 CV1025 CV1029 CV2679 CV2710 CV1031 CV1032

CV656

CV659 CV665

CV668

CV686 CV702 CV704 CV755 CV773

CV779 CV781

CV849 CV849 CV852

CV1199 CV1284 CV1300 CV1306 CV1310

CV1311 CV1366 CV1367 CV1368

CV1368 CV1449 CV1481 CV1504 CV1508 CV1573 CV1653 CV1755 CV1913 CV2530

ELECTRONIC PRECISION EQUIPMENT LTD. VALVE HOLDERS, ETC.



	-
6:4	-
1	
O	of 17 17

A DE

Type		Paxolin	Amph- enol	Cera- mic
		sd	sd	sd
	British 4-pin	6		9
	British 5-pin	6	-	9
	British 7-pin	6	1	9
	British 9-pin	9	1 -	_
	UX 4-pin	6		1 6
	UX 5-pin	6 6 7	_	9
	UX 6-pin		_	_
	UX 7-pin	8		t —
	Large UX7	1 -		1 0
	Diode B3G	6	8	_
	B7G	6	8	10
	B8G Loctal	9	1 1 —	_
	B8A	1 3 1 3	1 6	_
	B9A (Noval)	1 3	<u>-</u>	_
	B9G	1 0	1 0	_
	B12A (Duo-			
	decel)	1 3		-
	Int. Octal	6	9	1 6
	Mazda Octal	6	9	1 —
	8-pin side			
	contact	-	2 6	_
	Jumbo 4-pin	l -		3 6
	4-pin Hivac	9		<u> </u>
	5-pin Hivac	9	_	1
	5-contact			
	Acorn			1 6

VALVE SCREENING CANS

Suitable for standard size	S	d
valves consists of three		
parts, bottom plate, main		
body and spring top	1	3
B7G fixing base and top		
screen with spring	1	6
Screen for octal G.T. Valves		6





VALVE RETAINERS

Spring type for I	EF50		3
Threaded type for General type f	or all val	ves,	6
consists of a two springs	siik cord	and	3





)	Туре	Plain	Scr'ned	Insu- lated
	British lin.	s d	s d	s d
	top	11/2	9	1 6
	lin. type	1 1/2	9	1 6
	Screw to clip modern equiv	6		

To ensure receiving prompt reply, please enclose stamped addressed envelope, when writing for

EX-GOVT. VALVES American TYPES



2B26	807	8011
2C34	813	DET12
4C27	830B	DET19
3D6	832	RK20A
616	860	RK28A
35T	866	RKR72
54 Gam-	866A	RL5
matron	923	RL7
259A	954	RL18
714AB	1616	RX235
717A	1625	TZ0520
723AB	1629	VT90
801	4064B	VT114
803	4074B	VTX3
805	4328A	WE3A



EXPERI-MENTERS VALVE SNIP CV1147, High Current Thyratron, fila-ment 5 v. at 5 amp., peak plate voltage 1,000 v. peak plate current 12 amp. A limited quantity of these are available at 20/- each.

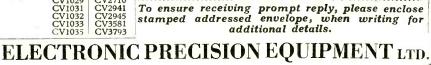
THERMAL DELAY SWITCH Hermetically sealed with 4-pin base, the operating voltage is 6 v. with a delay of 1 minute. Price 12/6 TUNGAR VALVE RECTIFIERS

Replacement for Replacement for many home and industrial chargers: 1 amp. type 68502.
Price 9/6.
3½ amp. type 68507.
Price 12/6.

MERCURY VAPOUR RECTIFIERS

CV2946 max current 1.8 max. 1,000 v. Price 6/6. VU29. max current 2.5 amps., max. 2.5 amps., max. 2,000 v. Price 9/6. BD10, max. current 25 amps. max. 25 1,000 Price £6/10/-.





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First Grade Quality - British and American Make - No Dollar Expenditure Involved

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MORE ROOM FOR YOU

MORE ROOM FOR US TO SHOW YOU

TELE-RADIO (1943) LTD.

For brilliant, high-fidelity sound recording the GRUNDIG 2-speed tape recorder

PUSH button controls and magic-eye tuning give you complete mastery over the Grundig's superb recording and reproducing qualities. The 1,200 feet of tape give you ONE HOUR of high-fidelity music recording and play back, High speed rewind mechanism enables you to reproduce from (or record on) any part of the tape in a few seconds. The same tape can be used repeatedly, each new recording automatically erasing the previous one, or recordings can be kept indefinitely. Sound frequency range: 7½in. per second, 50-10,000 c/s. 3¾in. per second, 50-6,000 c/s.

- ★ Condenser microphone as sensitive as the human ear.
- ★ Mixer unit—to mix up to 4 different recordings at once.
- * Remote controls—hand or foot operated.
- ★ Two-way telephone recorder—without alteration to G.P.O. handset.
- * As compact and portable as a suitcase.



Terms available.

THE



including condenser mike. L.P.

700L TWO-SPEED TAPE RECORDER

Not only a revelation but a revolution in tape recording!

GRUNDIG (GT. BRITAIN) LIMITED, KIDBROOKE PARK ROAD, LONDON, S.E.3.



GM6005 — a sensitive mains operated valve voltmeter for the measurement of voltages in the range 20 c/s to 1 Mc/s

- Features :-
- 1. 0-10 mV—0-300 V F.S.D. in 10 ranges.
- 2. Covers the frequency range 20 c/s to I Mc/s
- 3. Overall accuracy error < 5%

4. Input impedance 10 mV to 1 V at 20 Kcs = 1.5 M.ohm, < 15 pf 3 V to 300 V at 20 Kcs=1.9 M.ohm, < 6 pf

Specially recommended for A.F. work and vibration investigations.

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'phone: TEMple Bar 7587.

Immediate delivery from stock.

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Export enquiries welcom	ied.		
TAPE RECORD	ERS		
New Table, Twin Track New Portable, Twin	£69	01	0
Track	£74	10	0
SCOPHONY-BAIRD New Model Mk. 2	£68	5	0
SIMPHONIC New Model IA	€83	0	0
GRUNDIG 2 - Track 2-speed press-button			
control	£84	0	0
WIREK Portable Battery Model	£55	0	0
RECORDING T	APE	:	
GRUNDIG L.G.H., 1,200ft	£2		0
GRUNDIG L.G.H., 1,200ft SOUNDMIRROR	£2	0	Ĭ
GRUNDIG L.G.H., I,200ft SOUNDMIRROR Paper Tape, I,200ft	£2	0	0
GRUNDIG L.G.H., 1,200ft SOUNDMIRROR Paper Tape, 1,200ft FERROVOICE	£2	0 5 2	0 6
GRUNDIG L.G.H., 1,200ft. SOUNDMIRROR Paper Tape, 1,200ft FERROVOICE Spare Spools	£1 £1	0 5 2 4	6
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft FERROVOICE Spare Spools E.M.I. H.60, I,200ft	£2 £1 £1	0 5 2 4 15	0 6 6 0
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools	£2 £1 £1 £1	0 5 2 4 15	0 6 6 0 0
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft FERROVOICE Spare Spools E.M.I. H.60, I,200ft E.M.I. H.60, 600ft E.M.I. H.65, 600ft	£2 £1 £1 £1 £1	0 5 2 4 15 1	0 6 6 0
GRUNDIG L.G.H., 1,200ft. SOUNDMIRROR Paper Tape, 1,200ft FERROVOICE Spare Spools E.M.I. H.60, 1,200ft E.M.I. H.60, 600ft E.M.I. H.65 1,200ft E.M.I. H.65 1,200ft	£2 £1 £1 £1	0 5 2 4 15 1	0 6 6 0 0 0
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools	£2 £1 £1 £1 £1 £1 £2	0 5 2 4 15 1 15 8	0 6 6 0 0 0 0
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools. E.M.I. H.60, I,200ft. E.M.I. H.65, 600ft. E.M.I. H.65 I,200ft. E.M.I. H.50 I,200ft. SCOTCH BOY I,200ft.	£2 £1 £1 £1 £1	0 5 2 4 15 1	0 6 6 0 0 0 0
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools. E.M.I. H.60, I,200ft. E.M.I. H.60, 600ft. E.M.I. H.65 (200ft. E.M.I. H.50 I,200ft. SCOTCH BOY I,200ft. 600ft. Spare Spools, I,200ft.	£2 £1 £1 £1 £1 £1 £2	0 5 2 4 15 1 15 8	0 6 6 0 0 0 0 0 0 3
GRUNDIG LG.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools	£1 £1 £1 £1 £1 £2	0 5 2 4 15 1 15 8	066600000000000000000000000000000000000
GRUNDIG L.G.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools	£2 £1 £1 £1 £1 £1 £2	0 5 2 4 15 1 15 8	0 6 6 0 0 0 0 0 0 3
GRUNDIG LG.H., I,200ft. SOUNDMIRROR Paper Tape, I,200ft. FERROVOICE Spare Spools	£2 £1 £1 £1 £1 £2 £1	0 5 2 4 15 1 15 8 15 1 4 3 0	066600000000000000000000000000000000000

-	RECORD REPRODU		IG	
1	B.S.R.	•		
	3-spd. (Crystal T/O. hds.)	£9	4	11
	3-spd. (with 2 GP20 hds.)	£10	8	8
	3-spd. (with 2 Decca	£12	17	8
	3-spd. Auto-mixer			3
	GARRARD			
	R.C.80, less Head	£15	3	3
	R.C.75A, less Head			0
	S.201.B Variable 3-spd.			
	Transcription		14	8
	CONNOISSEUR			
	3-spd. Deck	£21	16	3
	GOODMANS			
	Axiom 150 Mk. 2			
	Audiom 60			-
	Axiom 101			1
	Axiom 102	£9	81	ı
	WHARFEDALE			
	W.12.CS	£13	3	3
	Golden 10 C.S.B		6	7
	Super 5 and 8 CS/AL			0
	Bronze Ioin			9
	Bronze 8in		4	0
	W.B. Crossover Unit	£I	- 6	- 6

RECORD REPRODUCING		TEST GEAR	V
EQUIPMENT		AVO	
B.S.R.	1	Model 8 £23 10 0	!
3-spd. (Crystal T/O.		Model 7 (latest) £19 10 0	
hds.)£9 4	11	Uniminor	A
3-spd. (with 2 GP20		Wide Band Sig./Gen. £30 0 0	~
hds.)£10 8	8	Valve Characteristic	
3-spd. (with 2 Decca		Meter £60 0 0	
hds.)£12 17	8	D.C. Minor £5 5 0	
3-spd. Auto-mixer £16 10	3	10kV. Multiplier for	
	-	Model 8	S
GARRARD		Carrying Cases for	
R.C.80, less Head £15 3	3	Models 7, 8 and 40 £3 0 0.	L
R.C.75A, less Head £13 10	0	ADVANCE H.I (Sig./Gen.)	
S.201.B Variable 3-spd.		H.1 (Sig./Gen.) £25 0 0 E.2 (Sig./Gen.) £28 0 0	1
		J.I. New Model £35 12 0	
Transcription £22 14	8	COSSOR	
CONNOISSEUR		Double Beam 1035 £93 10 0	
3-spd. Deck £21 16	3	Double Beam 1047£132 0 0	
	_	TAYLOR	
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Axiom 150 Mk. 2 £13 11	5	GEAR IN STOCK AND AVAIL-	
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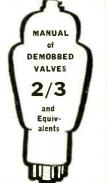
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G.E.C. VHF RECEIVERS complete with 10 valves. Ex-Govt. As used by police. Used but guaranteed in excellent condition. Used but guaranteed in excellent condition. Valves comprise ZA2's, 954's or EF50's in HF and 1st Det. stages. Det 19 in local oscillator, KTW63's in three IF stages, D63 Det and AVC, LF H63, Output KT63, Noise suppressor D63, Power requirements 6v 3a, 270v 80ma, 78.5-82 Mc/s. Intermediate frequency adjustable 8.3-9.8 Mc/s. Oscillator Crystal controlled (No crystal included). Sensitivity 3 microvolts for 50mw audio output. Input impedance 72 ohms. Housed in Grey enamel steel case with lid 10 x 8 x/in.

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A MIDGET 4-STATION "PRE-SET" RECEIVER A complete Kit to build a 4-station "Pre-set" Superhet Receiver for A.C. mains Superhet

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A Midget 4-valve Superhet Portable Set covering medium and long wave-bands.

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THE "Wireless World " 3-Valve Set

A Midget 3. vaive T.B.F. Receiver for operation on A.C. mains, covering long and medium wavebands We are able to supply all of the components to build this set, as designed and specified in the Feb. 1950 issue, including the drilled chassis. Vaives and moving coil the drilled chassis. Vaives and moving coil complete chassis, less dial and drive assembly, 25.75. Ditto including dial and drive assembly, 25.75. To construct the complete set, including dial and drive assembly, 25.75. To construct the complete set, including dial and drive assembly, 25.75. To construct the complete set, including dial and drive assembly, 25.75. Ditto including dial and drive assembly, 25.75. Ditto including dial and drive assembly and cubinet. \$773.6. Overall time continued to the complete set, including dial and drive assembly and cubinet. \$713.6. Overall size of cabinet is 71in. × 31in.x 11tin. A reprint of the designer's article, giving circuit and assembly instructions (this is available separately for 94.0 together with a practical component Layout is included with each of above assembles.

"PERSONAL SET" BATTERY ELIMINATOR

A complete Kit of parts to build Midget
"Alldry" Battery Eliminator, giving
approx. 69 volts and 1.4 volts.
This eliminator is for use on A.C. This eliminator is for use on A.C. mains and is suitable for any 4-valve Superhet Receiver requiring H.T. and L.T. voltage as above, or approx. to 69 volts.

The Kit is quite easily and quickly assembled and is housed in a light aluminium case size 4½in. x 1½in. x 3½in. Price of complete Kit with easy-to-follow assembly instructions, 42/6.

In addition we can offer a similar COMMETE KIT to provide approx. 99 volts and

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THE "MINI-TWIN" 1-VALVE BATTERY SET

A design of a simple 1-valve 2-stage Battery Receiver, giving excellent results on medium and long wavebands and having exceptionally low battery consumption.



TWO BATTERY PORTABLES

(a) THE "MINI TWO-THREE"

An "Aldry" Battery Portable of midget size, 6 jin. ×
4 jin. × 3 jin., designed to cover medium waveband 190-559
metres, with use of abort trailer aerial.
The simple design of this Ecceiver is so arranged that either
a 3-valve set or a 3-valve (atterwards easily converted to
the 3-valve) can be made.
Consists of a T.R.F. circuit using a regenerative detector
with H.F. stage and a high gain output pentode. Valve
line up IT4—TT4—DL94.
The 2-valve set can be completely built for \$4/3/6 (less

line up IT4—IT4—ID44.

The 2-valve set can be completely built for \$4/3/6 (less case), and the 3-valve for \$5/3/- (less case). Each price includes valves, speaker and drilled classis.

Send 1/9 for the assembly instructions: they leading simple and complete practical component layouts and diagrams, which enable the most inexperienced constructor to successfully build either to to concessfully build either

set. All components are available for separate sale, a price list being supplied with assembly instructions.



(b) THE "MINI-FOUR"

A 4-valve Battery Supernet Receiver designed to receive 4 pre-set stations, three cm medium waveband and one on long wave to suit local conditions. Each station is obtained on the set by the turn of a rotary switch. No tuning is

necessary.

11 so f nudget size, being only 4\forall in. \times 6\forall in. \times 4\forall in. \times the completely built and in very easily assembled from diagrams

supplied.

Cost of all components to build this set, in accordance with the design, including a drilled and cut chassis and panel and new valves, is £9/10/- (or less valves for £6/7/6). Attractive carrying case finished in blue leatherette, 16/9. Complete constructional data with a blue print, which shows the precious uteriors data was blue practical component layout and wiring diagram, together with an individual component price list, is available separately, 1/6. Our battery eliminators (illustrated above) available in kit form are sultable for use with this set.

THE FAMOUS "SHAFTESBURY" RIBBON MIKE

Incorporating internal line transformer having transformation ratio from ribbon impedance up to 500-600 ohms... reduced from 10 gns. to £6. A special line to grid, 500-600 ohms transformer, also available for

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For accurately giving 465 Kc. and 1.6 Mc. I.E. channels and associate circuits. Battery operated, small and completely self-contained, 59/6 (plus battery 1/8).

THE "WIRELESS WORLD" MIDGET A.C. MAINS 2-VALVE RECEIVER

We can supply all the components to build this set, including valves and moving coil speaker, for £3/10/-, including designers' complete building instructions including designers' complete building these are available separately for 9d.).

THE VIEWMASTER TELEVISOR

We have had vary considerable experience in assisting customers to build this T/V and can supply a SPECI-FIED COMPONENTS EX-STOCK. The assembly instructions showing practical layouts and price list are available for 7/8 for London, Sutton Coldfield, Holme Moss, Kirk-o'-Shotts and Wenvoe. Complete television of the contraction of the c price list is contained in our general STOCK LIST at 9d., including Haynes, etc., components.

THE DENCO ULTRA MIDGET SUPERHET COIL TURRETS WITH A ROTARY TURRET ACTION

Type CT9 consists of a four station "pre-set" unit from which any three stations on medium waveband and one on long wave can be received by a turn of the turnet switch.

ong wave can be received by a cart of an earlier switch Type CT10, is a 3 waveband coil pack incorporating a fourth switch position for Gram. Complete coverage Is, long wave-band 700-2,000 metras, medium waveband 190-570 and short wave 15-50 metras. Frice \$2.18/-. A complete receiver circuit and all necessary data is included with each turret. These can be supplied separately for 8d.

HOME CONSTRUCTORS RECEIVER FOR £12.0.0

A design of a 5 Valve Superhet Receiver, employing an R.F. Stage for 6 or 12 Volt supply. Send 2 8 for the complete set of Assembly Instructions, CIRCUITS, LAYOUTS, and POINT TO-POINT WIRING DIAGRAMS, together with a complete component Price List.

THIS IS NOT AN EX GOVT, RECEIVER, IT IS A NEW DESIGN EMPLOYING NEW COMPONENTS.

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Interchangeable (G.P.19) head for L.P. records, £2.
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For Standard or L.P. Records, £3/5/9.

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All kits incorporate metal rectifiers and are for use on A.C. mains 220-250 volts. All kits include an easily followed wiring diagram. All prices include a TAPPED RESISTOR and a five-position SELECTOR SWITCH For 6 or 12 volt batterles at max. 1 amp., £1/18/9 (excluding Resistor and Switch, £1/3/6).

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Send 9d. for our STOCK LIST it shows hundreds of RADIO AND TELEVISION COMPONENTS aud many KITS OF PARTS for both Sets and Battery Chargers. When ordering please include approx, cost of Post and Packing.

TWO COMPLETELY ASSEMBLED "ALL-WAVE" SUPERHET CHASSIS

(a) MODEL B.3. A 5-valve 3-waveband superhet Receiver.
(b) MODEL B. A 5-valve 6-waveband (4 bandspread) Superhet Receiver.
(b) MODEL B. A 5-valve 6-waveband (4 bandspread) Superhet Receiver.
Both Receivers are for operation on A.5. mains 100/200 volts and 200/250 volts, and employ the very latest miniature valves. They are designed to the most modern specification, great steenion having been given to the quality of reproduction which give accellent, clarity of speech and music on both gram and radio, making them the ideal replacement chassis for that "old Radiogram," etc.

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A GENUINE SPECIAL OFFER!

PLESSEY 3-SPEED AUTO CHANGE UNITS

Brand New in maker's Cartons, complete with mounting instructions.



with the very latest equipment. We will supply the 3 waveband chassis on the left with the Plessey auto changer on the right, complete with 10° speaker for £25 (£28/7/6 with the 6 waveband chassis). This is less than half the price of comparable commercial three speed auto radiograms. Brist specifications: Model B.3.—Valve line up, 6BE6, 6BA6, 6AT6, 6BW6, 6X.4—waveband coverage, short 16-50, medium 187-5-50, long 900-2,000 meters. Controls: (1) volume with on/eff; (2) tuning (flywheel-type); (3) wavechange and gram; (4) tone (3-position switch operative on gram



These units will auto change on all three speeds, 7in., 10in. and 12in.

They play MIXED 10in, and 12in, records,

They have separate sapphires for L.P. and 78 r.p.m., which are moved into position by a simple switch.

Minimum baseboard size required 16in, x 12in, with height above 5in. and height below baseboard 2in.

A bulk purchase enables us to offer these BRAND NEW UNITS at this exceptional price.

Please add 7/6 packand ing. carriage insurance.

A Complete Kit of Parts to build a 3-4 WATT HIGH GAIN AMPLIFIER



This amplifier will give 3 watts output for the small input voltage of only 75 millivolts, and is therefore suitable for use with any type of pick-up from the crystal type to the miniature HIF Magnetic type.

A tone control is incorporated and the quality produced is excellent. The overall size of chassis is 2in. x 5in. x 7in. and valve line up 25 % 5-bst7-2516.

Price of complete kit, including drilled chassis and valves, 24(2)9, ptu 64in. P.M. (which fits on chassis), 16/n, or 8in. F.M. 18/9.

Price of fully assembled chassis ready for use, £5/5/-(plus cost of speaker).

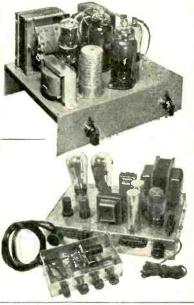
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embly instructions and components price list

!! AMPLIFIERS !! TWO COMPLETE KITS OF PARTS

TWO COMPLETE KITS OF PARTS
A 6-8 wait QUALITY "PUSH-PULL" AMPLIFIER
designed for A.C. mains 200 to 250 volts, incorporating a
simple arrangement to enable either a magnetic-crystal
or lightwelght pick-up to be used, and is suitable for use
with Standard or long-playing records. A tone control is
designed to match 2 to 16 ohm speakers.
The overall size of the assembled chassis is 10in. x 8in. x
7\(\frac{1}{2}\)in high, and full practical diagrams are supplied. Price,
including drilled chassis and valves, of complete kit,
28(17/6. Frice of assembled chassis, supplied ready for
use, 28(12/6. Full descriptive leaflets are available
separately for 1/-,

A 12-wait High FIDELITY "FUSH-PULL" AMPLIFIER designed for A.C. mains 200 to 250 volts, employs 6 valves plus rectifier, with negative feedback, and comprises a main amplifier chassis and a remote controlled Preamplifier and Tone Control Unit, incorporating four controls—bass, treble, main volume or mixing control, and a radio, gram, microphone, selector switch. This control unit measures only 7 x4 × 2in. The measured frequency range of the amplifier with this unit shows an excellent response from 14,000 cycles down to 20 cycles, the bass and treble controls allowing independent control of gain at both ends of the frequency range from zero to a gain of 50. It can be seen, therefore, that ample correction is provided to suit any type of pick-up with any type of recording. Input voltage for maximum output is 70 mV., 6.3 volts at 2 amps and 30 mA H.T. is provided for tuning unit, etc. Price of complete kis, including drilled chassis and valves, £12. Complete specification and layout, 2/3. We can also supply completely assembled and ready for TRIS AMPLIFIER COMPARES WELL WITH THE WILLIAMSON AND SIMILAR DESIGNS AT A FRACTION OF THE COST.



A 5-VALVE "ALL-WAVE" SUPERHET RECEIVER

rur use on A.C. Mains 200 to 250 votes. This small attractive Receiver, embodying modern circuit technique, is designed to cover Short, Medium and Long wavebands, and incorporates the following outstanding features: For use on A.C. Mains 200 to 250 volts.

A superhet circuit designed for high efficiency on all three wavebands.

A 54hi. P.M. Speaker accurately matched for good quality reproduction.

The latest range of new 6-vott B.V.A. ministure valves. Bull-in frame aerial with provision for external serial for distant stations.

A white plastic cabinet of very attractive appearance everall size 7½ia. × 5½m. × 5½m.

THE RECEIVER AN LILUSTRATED CAN BE BUILT FOB APPROX. £10/10/~.

d 2/6 for the fully descriptive stage by stage assembly wiring diagrams, with which complete price details given.



STERN RADIO Ltd. 109 & 115, FLEET STREET, E.C.4

Tel.: CENTRAL 5812-3-4

A DUAL CHANNEL PRE-AMPLIFIER and TONE CONTROL UNIT

This comprehensive PRE-AMPLIFIER and TONE CONTROL UNIT provides a full control of bass and treble in conjunction with a main Volume/Mixer Control.



It can be used with any amplifier and with any pick-up, the range of frequency control provided by the unit affording ample compensation for all types of pick-up and all natures of recordings, i.e., English, American and long playing, without the control of the state of the sta

CRYSTAL DIODES. Germanium Vacuum sealed glass type with wire ends, 2/8 each or 30/- per dozen. (P) Germanium Vacuum

WHANDA WIRE AND CABLE STRIPPERS, to take all size flexes and cables up to fin. diameter, with 3 alternative heads and triple screw adjustment. These are brand new and boxed, and the original price was 15/- each. Our Price 4/3 each or 48/- per doz. (P)

CARBON RESISTORS. $\frac{1}{4}-\frac{1}{2}$ watt, 3d. each. Virtually all standard values in stock. Nearest value supplied, unless otherwise stated. (PorG)

SILVER MICA OR CERAMIC CONDENSERS (pfs). 2, 4, 10, 15, 27, 30, 50, 75, 100, 160, 200, 220, 300, 330, 350, 500, 1,000, 2,000, 4,500, 4,700. All at 5d. each, or 4/- per doz.

WAX TUBULAR CONDENSERS. . 1 mfd. 350 v. 4d. each or 3/- per doz. (G)

MOULDED MICA CONDENSERS. .01 mfd. 500 v., 6d. each or 5/- per doz. (G)

EHT CONDENSERS. .001 mfd., 5kV. A.C. Test, 1/6 each or 15/- per doz. .02 mfd., 5kV. D.C. working, 1/6 each or 15/- per doz. (G)

SPEAKER FRET. Expanded Metal, finished Silver 6 x 6, 1/3; 9x9, 2/6; 12 x 12, 3/9; 18 x 18, 8/6. (P) SPEAKER FRET. Expanded metal, finished gold 6×6 , 1/6; 12×12 , 4/-. (P)

SPEAKER FABRIC. Fawn or brown, 12 x 12, 2/-; 18 x 18, 4/6. (P)

HEADPHONES. 4,000 ohms, per pair, 11/-.

METAL RECTIFIERS. RMI, 125 v. @ 80 mA, 3/11. RM2, 125 v. @ 100 mA, 4/3. RM4, 250 v. @ 250 mA, 17/-. 14D/972, 250 v. @ 25 mA, 6/6. 12 v. ½ A, 6/-. 6 v. I A., 4/6. 12 v. 2 A., 12/6. 12 v. 2½ A., 16/6. 12 v. 4 A., 21/-. (P)

SWITCH SOCKETS. Flush mounting 250 volt, 3 pin, 5 amp., bakelite. Price 3/6. (M)

LINE CORD. 3-way, 0.3 amp., 60 ohms per foot, 1/9 per yard. (P)
ELECTROLYTIC CONDENSERS.

are current production, not surplus stocks. 32 mfd., 450 volts, 250 mA ripple, can., 4/6; 8 mfd., 450 v., 1/9; 8 + 8 mfd., 450 v., 3/3; 8 + 16 mfd., 450 v., 4/-; 8 + 32 mfd., 450 v., 4/6; 16 + 16 mfd., 450 v., 5/-; 32 + 32 mfd., 450 v., 4/6; 25 mfd., 25 v., 1/9; 50 mfd., 12 v., 1/9. (P)

MAINS DROPPERS. Standard 0.2 and 0.3 amp. Price 3/9 each. (P)

AERIAL AND OSCILLATOR COILS. For medium and short waves. Price 5/- per set of 4 coils. (M)

HEATER TRANSFORMERS. 230 v. input, 6.3 v., 1.5 amp. output, 5/6 each. (P)

MOULDED BAKELITE ESCUTCHEONS. in. x 2%in. with opening 6%in. x 1%in., 1/- each. (M)

GENERAL PURPOSE TRIODES. Type 7193, 6.3 v. heater. Similar to 615G. Price 2/6 each. (G) ROTARY TOGGLE SWITCHES. 4-pole bunching. Price 1/6 each. (G)

OUTPUT TRANSFORMERS. Standard pen tode matching to 2/4 ohms. Price 4/6 each. (M) L.F. CHOKES. 10 Henry, 70 mA. Price 4/9

ENGRAVING TOOL. For 200-240 v. A.C. mains. Suitable for use on metals or plastics. Price 10/- each. (P)

COAXIAL CABLE. COAXIAL CABLE. Stranded centre conductor, ‡in. diameter, 80 ohms, 9d. per yard. (P)

TAPE RECORDER OSCILLATOR COILS. 6.3 mH, 45 kc/s, for high impedance heads only. Price 6/9 each. (P)

TELEVISION MAGNIFYING LENSES. 6in clear, 19/6; 9in. clear or filter, 50/-; 12in., clear or filter, 70/-. Please state which and add 5/- for carriage and packing. (P)

DIAL BULBS. 6-8 v. 0.3 amp., M.E.S. fitting Price 3 for 1/9. (P)

PAPER CONDENSERS 0.01 mfd., 500 v., 6d; 0.01 mfd., 750 v., 6d.; 0.25 mfd., 500 v., 6d.; 1 mfd. 400 v., 6d.; 1 mfd. 500 v., 9d.; 1 mfd. 600 v., 1/-; 1 mfd. 800 v., 1/3 (all G); 3 μfd., 750 v., 1/9. (U)

OIL FILLED CONDENSERS. Imfd. 600 v., 3/-.

AERIAL FILTER UNIT. No. 112. 10P/13089

ALADDIN in. COIL FORMERS. Ex-Govt.; wound. No slugs or cores. 2,- per doz. Iron dus cores for above 3/6 doz. (G)

ADMIRALTY TRANSFORMERS. 36 vA. 500/1,000 c. Pri. 0-80-180 v. Sec. 0-900-2,400 v. Can be used in reverse on 50 c., 3/9. (G)

DIMMER SWITCHES. 5C/725. Wire-wound, approx. 300 ohms, with off position. 1/3 each: (G) ELECTRON COPPER AERIALS. 50ft., 2/-; 100ft., 3/9. (PZ)

MAINSP-MT.

3-A.
0-30 v., tapped to give 3 v., 4 v., 5 v , 6 v.,
8 v., 9 v., 10 v., 12 v., 15 v., 18 v., 20 v.
24 v., 30 v., all at 2 amp.
4 v., 4 amp.; 10 v. 4 amp.; 20 v. 3 amp., for

battery chargers. MT5. Auto; 0-10-120-200-230-250 v., at 100 watt.

P.O. TYPE 3-WAY TELEPHONE PLUGS. Ex-equipment, Price 6d, each, (U)

MINIATURE LIGHT WEIGHT RELAYS. 270 ohm, 18 v. Single pole on-off. Ex-American equipment. Price 2/9 each. (U)

COMMERCIAL POTENTIOMETERS. usual values. Less switch, 2/3; with single p switch, 3/6; with double pole switch, 4/-. (P)

switch, 3/6; with double pole switch, 4/-. (P)

VALVE HOLDERS. B3G, pax, 4d.; Do., with spring retainers, 1/-; B5, pax, 4d.; B5, bakelite, 6d.; B5, baseboard, 6d.; B7, pax, 6d.; B7, amphenol 1/-; B7G, amphenol, 6d.; B1.. Octal, amphenol, 6d.; B8A, amphenol, 9d.; B8G (loctal), amphenol, 6d.; B9, pax, 6d.; B9A, amph. 9d.; B9G, pax, 6d.; B9G, ceramic or siliconised polystyrene, 6d.; B12A, pax, 9d.; UX5, pax, 6d.; UX5, amphenol, 9d.; UX5, pax, 6d.; UX5, ceramic, 1/-; UX6, pax, 4d.; UX7, pax, 4d.; UX7, medium (for 1625, RK34, etc.) ceramic, 1/-. (P)

NEON LAMPS. 85 volt striking, S.B.C. centre contact base. Price 2/6. (G)

SLEEVING. Approx. 2 mm. Price 1/6 per doz. yard lengths. (M)

CARTRIDGE FUSES, All usual values in lain., 5d. each. Other sizes 6d. each. (P)

SWITCHBOARD METERS. 6½in.: 0-5 v. A.C./D.C. full scale. Price 30/-. (G)

HIGH FREQUENCY PENTODES. Type 6SH7, high slope, octal based. 6.3 v. heaters. Price 6/-. (G)

GARLAND TAPE RECORDER OSCIL-LATOR UNITS. With valve, for use with high impedance heads only. Price 35/-. (PZ)

DECALS. 500 kin. high white transfer letters and words for marking electronic equipment. Price 4/9 per book. The new Decals book for the amateur now available. 29 words per page, 4 pages radio and audio, 4 pages T/V and Scope, 2 pages misc. incl. Tx. and Tape Recording. 3/6 per book. (PZ)

INSTRUMENT WIRES. Enamelled, silk and cotton covered, available in upwards of 2 oz. reels. Send S.A.E. for list of lowest prices. (P)

ROTARY TRANSFORMERS. Type 31, input 18 v. 12 A.; output 7.2 v. 13 A. and 225 v. 0.11 A. Price 22/6. (U)

VOLTAGE STABILISERS. Type VS110 (S130). With loose bases but otherwise sound. Price 3/6. (U)

GOODMANS OUTPUT TRANSFORMERS. 10 watts push-pull to match into 10,000 ohm., with two 3.75 ohm, secondaries for 3 or 15 ohm, speaker. Price 14/9. (P)

SMALL PAPER CONDENSERS. in tubular metal cases with wire ends. 0.25 mfd., 250 v., ½in. diam. x ¾in., 1/- each (M); 1 mfd. 150 v., ¾in. diam. x 1½in., 1/3 each (M); 2 mfd. 250 v., ¾in. diam. x 2½in., in Neoprene sleeve, 1/9 each (M)

TYANA SOLDER GUNS. Weight 30 oz., for v. A.C. mains only; consumption s. The low voltage bit can be easily bent 100 watts. to reach into corners and is insulated from the earthed case. Price 3 guineas. (PY)

CONNECTION BLOCKS. 3-way on porcelain base, 6d. each. (P)

WINDSOR SAPPHIRE NEEDLES. Available in the following three patterns: trailer type for magnetic or heavyweight pick-up; straight type for crystal pick-up; midget type for lightweight or high fidelity pick-up. Price 2/9 each. (P)

MIDGET 2-GANG CONDENSERS. American manufacture, 500 pF., 7/6 each. (M)

VARIABLE RESISTORS. 50 ohm, I amp., with calibrated very fine worm drive. Price 7/6. (U)

BELLING AND LEE PLUGS AND SOCKETS. 5 way, 2/-, 7 way, 2/3 complete. (G) JONES PLUGS AND SOCKETS. 6 way, 1/9; 8 way 2/- complete. (G)

E.H.T. PLUGS AND SOCKETS. 1/- complete.

PYE 3 COAXIAL PLUGS AND SOCKETS. I/- per pair, complete. (G)

4-WAY MOULDED PLUGS AND SOCKETS 2/6 per pair. (G) ZINC PLATED CHASSIS. 13½ x 6 x 2½in.

drilled for five valves, 2/6. (M)

DUMMY AERIAL LOADS. Tapped at 20, 10 and 5 ohms, 100 watts. British 5-pin base. Callers only, 1/6 each. (G)

PLASTIC SPEAKER CABINETS. Louvred for 5in, speaker, Callers only. Price 10/- each. (P) IGNITION SWITCHES. Low voltage, hi current, in bakelite case. Price 9d. each. (G)

S.W. TUNING CONDENSERS. with fixing feet. Price 2/3 each. (G) 160 pF,

CATHODE-RAY TUBES. Type 5CP1. green screen, electrostatic focussing and deflec-tion. Callers only. Price 17/6 each. (G)

FLEX CONNECTORS. 24 x 1/2 in., for 250 v., I/- complete. (G)

TWO GANG TUNING CONDENSERS. 0.0005 mfd., with fixing feet. Price 7/9 each. (P) THYRATRONS. Type NGTI (CVII4I), 4 volt heater. Price 5/6 each. (G)

TRIMMERS. 50 + 50 pF, 100 + 100 pF, 100 + 500 pF, 500 + 500 pF, eeramic mica, 9d. each; 250 pF, 1,000 pF, 9d. each; 50 pF, 75 pF, airspaced pre-set, 1/3 each; 75 pF, air-spaced, 2in. spindle, 2/-each. (G)

DENSERS. We have still a few thousand of these left, but as we can no longer offer our original

WENDERS. YVE nave still a few thousand of these left, but as we can no longer offer our original comprehensive range, we are clearing the balance, in the values shown hereunder, at 1/- each, or 9/- per dozen. Accuracy in all cases is plus or minus point five (0.5) per cent. Ruby mica and copper foil or silver. (a) 0.017970μF. (b) 0.027400μF, (d) 0.040710μF. (e) 0.055820μF, (g) 0.087460μF, (h) 0.108435μF. (G) ENGRAVED KNOBS. 1½in. diameter, fluted in Walnut or Ivory, with the following markings: Volume, Vol-On-Off. Treble, Bass, Tone, Tuning, Wavechange. S-M-L-Gram, On-Off, Brilliance, Price 1/6 each. Plain knobs to match, 1/3 each. (PZ)

VALVE TYPE 954. 6.3 volt Acorn pentodes. Brand new Westinghouse, boxed in 25's. Special offer per box of 25, 30/-. Supplied separately at 2/- each. (G)
CONNECTION BLOCKS. Moulded plastic with brass inserts. 3-way, 10d.; 4-way, 1/-. (P)

IDENTIFICATION CODE

G = Government unused; U = Ex-equipment, used: P = Current production, unused; M = Manufacturers surplus, unused; X, Y, Z = Varying trade discounts available. Particulars on request by bona-fide traders.

Post and packing extra on all items (minimum parcel post 1/-). Post orders to our Deptford address. Kindly print name and address. Early address. Kindly print name and addre closing Thursday, open all day Saturday.

GARLAND UETB RECORD PLAYBACK AMPLIFIER. A revised version of our popular amplifier designed to suit Truvox Tape Desk or Lane Tape Table. New features include higher gain, magic eye record level indicator, and smaller size for incorporation in portables. Oscillator and power supplies included. Standard valves throughout. Formica control panel. Supplied complete with 8in. P. M. loudspeaker. Price £13/2/6 plus 7/6 carriage, etc. Trade supplied. (PX)

UNDRILLED CHASSIS. In 20 s.w.g., bright mild steel: Four-sided size 13in. \times 7in. \times $2\frac{1}{2}$ in., 5/- each; two-sided with two straps, 12in. \times 4in. \times $2\frac{1}{2}$ in., price 3/- each. Two-sided with two straps, is each. Add one-third to above

prices if chassis required in aluminium. (P)

CUT 4000 in

ELECTROLYTIC CONDENSER OFFER. Tubular cardboard cased, with wire ends, 8 mfd., 4/5 v. wkg., 525 v. surge, 2l- each. (P) **RECTANGULAR KNOBS.** Size $l\frac{1}{4}$ in. $x = \frac{3}{4}$ in., with gold indicating spot; to fit standard $\frac{1}{4}$ in. spindles. Price **6d.** each. (G)

BOOKS FOR RADIO ENGINEERS Mullard Valve and Service Reference Manual Mullard Amateurs Guide to Valve Selection Osram Valve Manual, Part I

Brimar Radio Valve and Teletube Manual...

Wireless World Radio Valve Data, 3rd edition Radio Valve Guide. By W. J. May The Williamson Amplifier Manual, latest 5/edition
Wireless World High Quality Amplifier 3/6 Manual
T.V. Fault Finding Viewmaster Envelope (state transmitter for 7/6 which required).....

Tele-King Envelope 6/The Oscilloscope Book 5/Magnetic Recording (Quartermaine) 4/6
(Add 3d, to price in all cases for postage.)
TYANA SOLDERING IRONS. Lightweight, 40 watt irons with easily interchangeable elements and 3/16in. diameter bits. Voltage ranges, 6v, 100/110 v, 200/220 v. and 230/250 v. Price 16/9. "The iron that makes soldering a pleasure"

(PY)
WIRE WOUND RESISTORS. Open, cement coated or vitreous enamelled. 4 watt, 50, 90, Price 1/- each. 6 watt, 30, 145, 270 10 k., 15 k. Price 1/6 each. 10-15 watt, 5, 90, 100, 120, 170, 175, 200, 400, 700, 950, 1 k., 3.5 k., 4.5 k., 4.7 k., 11 k., 15 k., 25 k., 1/9 each. 15 watt, 650 ohm. Price 2/- (Mor G)
CERAMIC SWITCHES. Single pole, eightway, 3/6 each. (G)
VARLEY MAINS TRANSFORMERS. Primary 10, 0.200, 202, 204 velt. Secondary 300-0.300 volt

10-0-200-220-240 volts. Secondary 300-0-300 volt at 150 mA., 5 volt at 3 amps., 6.3 volt at 4 amps., 6.3 volt at 1 amp. Open type construction. Price 45/-. (P)

TOROIDAL CERAMIC POTENTIOMETERS. $260~\Omega$ 50 w., 6/6. | 17k. | 100 watt, 8/6 . (G)

METERS. 260 Ω 50 w., 6/6. 17k. 100 watt, 8/6. (G)
MAGNETIC TAPE. Scotch Boy MCI-III:
1,200ft., 35/-; 600ft., 21/-; 300ft., 12/3. Spare7in.
spools, 4/3. Ferrovoice, the new kraft-based medium coercivity tape: 1,200ft., 22/6. Spare 7in. spools, 4/6. (P)
BRIMISTORS. Non-linear resistors to protect valves from current surges: CZ1, 0.3A, 3/6; CZ2, 0.3A, 2/6; CZ3, 0.2A, 1/6; CZ4, 1.25 A, 5/-; CZ6, 0.45A, 3/6. (P)
MOULDED BROWN BAKELITE
CABINETS. Suitable for fitting Decca 3-speed gram. motor, amplifier or loudspeaker. Outside dimensions (closed) 15½in. x 10in. x 5½in.; thickness of walf., 1/16in. Price, 22/6, to callers only. (M)
AMPLION TESTMETER. 10 ranges A.C. and D.C. up to 500 v. Resistance up to 200,000 ohms, 1,800 ohms per volt A.C. and D.C. Price £5.

HIGH WATTAGE WIRE WOUND RESIS TORS. Capped end type, porcelain covered, at the following prices: 20 watt, 1/-; 40 watt, 1/3; 80 watt, 1/6; 100 watt, 1/9; 200 watt, 2/6; 3 ohm, semi-variable, 20 watt; 4 ohm, 40 watt: 13.852+1.352+8.352 ohm, 40 watt; 80 ohm, 40 watt; 350 ohm, 40 watt; 730 ohm, 200 watt; 5 k, 40 watt; 7.5 k, 40 watt; 12 k + 2 k, 80 watt; 20 k, 80 watt; 50 k. 100 watt 75 k, 40 watt; 100 k, 200 watt. Packing and carriage extra on all of these resistors. (G & M) TWIN SCREENED CABLE. Suitable to carrying currents of up to 5 Amps. Cotton covered, 9d, per yard. (M) HIGH WATTAGE WIRE WOUND RESISper yard. (M)
RUBBER TUBING. External diameter, 0.25in

internal diameter, 0.1 in. Price 2d. per yard. (G)
WALNUT VENEERED CABINETS. Size
12 in. x 7 in. x 5 in. Suitable for housing a T.R.F.
receiver or inter-com, Complete with back,
chassis, dial and clips. Price, to callers only, 22 (6)

LARGE DIAMETER SLEEVING. Transparent plastic, in diameter, 6d. per yard length. (M) Henry, wound on Aladdin 3in. coil former (niron dust core). Price, 2/6 per half-dozen. (G)

ELECTRO-MAGNETIC CONTACTORS. Energised at 9-14 volt, ½ Amp; maximum switched.

PAXOLIN PANELS, 3½in, x 1½in, x 3/32in, 1/- per doz., 5/- per 100. 2½in, x 2in, x 1/16in, 1/3 per doz., 6/- per 100. Many thousands available. (M)

able. (M)
CABINETS in handsome two-tone Walnut veneer to house 6½in. extension speaker. Price 16/6 each. (P)
VALVE OFFER. Type 1625. These are the 12 volt heater equivalent of the 807. Price complete with Ceramic holder 5/9 each. (G)



POTENTIOMETERS. 20k, 10w, 10% by famous maker, 1½ in, spindle, price 3/6. (G) RADAR REFLECTORS. Type MX138/-A. These consist of 6—2ft. x ½ in. dural tubes covered with fine wire mesh. The whole assembly can be used as an omni-directional aerial, and the mesh has many horticultural applications. Price 3/9 each.

BRENETTE MICROPHONES. We are sole distributors in Great Britain and Ireland of these new cell microphones. The following range is now available. Type DT. Directional in black and chromed case. Price £4/13/6. Type 9ND. Multidirectional ball type in black and chrome. Price £2/6/6. Type 11A. Wide frequency response, in brown and chrome. Price £6/17/-. Type 13U. Highly sensitive with wide frequency response, in black and chrome. Price £7/17/6. (PZ)

BRENETTE MICROPHONE STANDS. Desk

BRENETTE MICROPHONE STANDS. Desk type with flexible member to ease adjustment. These stands will suit all British and Continental microphone stands. Price 16/6 each. (PZ) CONDENSER OFFER. 25 mfd. 25 v. ear mounting. Price complete with ear, 1/- each or 10/- per dozen. .1 mfd. Condensers 350 v. screw mounting 1/- each, 9/- per dozen. (G)
AMPLIFIER ACII. Incorporating own power supplies ensuring that the chassis is completely isolated from the mains. Maximum output 3 watts; response 3 db. down at 30 c/s and 30,000 c/s. Distortion at 2 watts output and 1,000 c/s, .08%. Top cut tone control is fitted. Price 46/2/6, plus 5/- carriage. (PX)
ELECTRIC MOTORS. For use on 24 v. D.C. supply, 7/6 each. (G)

supply, 7/6 each. (G)
HIGH QUALITY LOUDS PEAKERS. Wharfe-

HIGH QUALITY LOUDSPEAKERS. Wharfedale Bronze 10in., £4/12/8. Wharfedale Golden 10in., £7/13/3. Wharfedale Golden 10in. C.S.B., £8/6/7. Goodmans Audiom 60, 12in., £11/10/3. Goodmans Axiom Mk. III, 12in., £13/12/4. All above prices include new P.T. (P) EX-GOVT. AND SURPLUS POTENTIOMETERS. Still available as in April copy of "Wireless World" with the exception of S0 ohm and 500 ohm. (G) ROTARY WAFER SWITCHES. 3-way, 3-pole, 3-bank, 2/3 each. 4-way, 2-pole, 4-bank, 2/6 each. (G)

TAMSA TYPE 100 TAPE RECORDING
HEADS. Housed in chromium placed TAMSA TYPE 100 TAPE RECORDING HEADS. Housed in chromium plated brass case on adjustable mounting. Record/playback heads have 1-thou. gaps and erase heads have 2.5 thou. gaps. These heads are of high impedance. Price 45/- each. (PZ)
PAXOLIN COIL FORMERS. These are of

rectangular cross section and are suitable for mains transformer bobbins. $2\frac{1}{6}$ in. \times $2\frac{1}{6}$ in. \times $3\frac{1}{2}$ in. long, I/- each. 25 in. x 13 in. x 12 in. long, I/3 each.

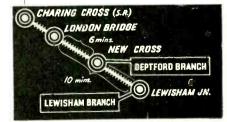
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Alexandra Palace, Sutton Coldfield, Sutton Col-Holme Moss,



SPECIAL C.R.T. OFFER. Brand new and unused 12in. ion trap cathode ray tubes. 6.3 volt heater, 7-9 Kv. E.H.T. 35 mm. neck. Black and white picture.

Screen has very slight blemishes £11/19/6. Perfect £12/19/6. Carriage and insurance 15/- per tube extra.

10,000 VALVES IN STOCK. B.V.A., Special Purpose, Transmitting, etc. A few specials: Raytheon sub miniature CK510AX, pentode, 3/11. 954, 956, VU120, 32, 57, E1148. All at 2/6 each. RK34, 2/-; MS/PEN 3/6; VU111, 3/6. Sylvania (red) EF50, 12/6.

CRYSTAL DIODES
Germanium 2/3d. each, post free.

ION TRAPS. All types available. PRICE 5/- each. State type number of c.r.t SPECIAL OFFER. (For MW31-16), 3/- each.

MANUFACTURERS SUR-PLUS T.V. COMPONENTS. Frame blocking oscillator transformer, Plessey.... 10/6 transformer, Plessey.... Multi ratio frame output transformer
Scanning coils. High impedance frame, low line.
By Plessey.
P.M. Focus units. For transformer 10/6 P.M. Focus units. For any type c.r. tube with 35 mm. neck, with vernier. Scanning coils. Low im-pedance frame, low line. With aluminium shroud. 25/-

ALL DRY PORTABLE CHASSIS. Superhet. Medium and short wave bands. I each ; 174, 185, 1R5, 384, 465 Kc/s. I.F. Fully assembled and wired. Ready to fit into a cabinet. HT. 90 volts. L.T. 1.4 volts. Size of chassis: 9in. wide, 5in. deep, 2in. high, 6in. overall height. LASKY'S PRICE. With valves, 85/-. Less valves, 52/6. Less valves, 52/6. Carriage 5/- extra.

THE TELE-KING

SUPERHET TELEVISION RECEIVER

Using the new 16-inch cathode ray tubes and wide angle components for the home

Complete instructions, Wiring diagrams and 32-page descriptive booklet.

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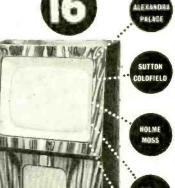
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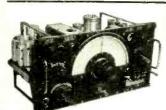
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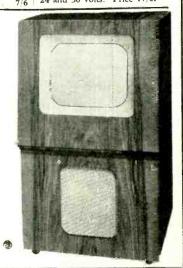
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3 in Plessey, with Trans.	15/-
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WELWYN	WIRE-WOUND SLID RESISTORS	ER
	PANEL FOR T/V SETS.	3. 1
	500 Ω , 2-10K	5/-
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100 Ω , 500 Ω , 2K, 10K and 30K

METRO-VIC (METROSIL) PENCIL TYPE E.H.T. REGULATOR up to 10 k.v. particularly suitable for regulating E.H.T. Ply-Back.

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L.T. RECTIFIER	łS	
		4
	ghouse	12
12 v. 4 amp. S.T.C.		1 12
12 v. 8 amp. S.T.C.	€	1 12

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This unit is complete with 6 valves, 2 EF36, 2 EF36, 1 EK32, 1 EBC33 and 465 kc/s l.F.T.s. In new condition. Circuit and conversion data supplied. 39/8.

S.T.C. RECTIFIERS E.H.T.		
K3/25, 650 v. 1 mA.	4	7
K3/40, 1,000 v. 1 mA.		0
K3/100, 8,500 v. 1 mA.		8
K3/200, 10,000 v. 1 mA.	£1 6	0

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H.T. RECTIFIERS			
S.T.C. 125 v. 60 mA.	4	6	
S.T.C. 125 v. 100 mA	5	0	
S.T.C. 125 v. 125 mA		0	
S.T.C. 250 v. 250 mA	18	0	
WESTINGHOUSE 14D/972			
250 v. 25 mA.	6	6	
S.T.C.M.1/3 Noise Limiter	6	Ö	
G.E.C. METER RECTIFIER, 1 mA	11	в	

RECEIVER R1355. As specified for "Inexpensive Television." Complete with 8 valves VR65 and 1 such SULG, VU120, VR02. Only 55/-, carriage 7/6. Brand new in original packing case. R724. 25/-; iR725, 25/-; iR725, 25/-; iR725, 25/-; iR725, 25/-;

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VCR97. Guaranteed full T/V Picture (carr. 2/-)	£2	0	0
VCR517. Guaranteed Full T/V Picture (carr. 2/-)	£2	0	0
Mu Metal Screens for above 6in. Enlarger Lens for above		10	6
VCR139A (ACR10). For T/V or Scope, brand new and boxed (carr. 1/6)		15	0
3BP1. For T/V or Scope (carr. 1/6)	£1	5	0

VR91 (EF50). original boxes	Brand new	Red Sylvanian,	10/-
British types, br	rand new an	new units, 6/	8/6
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Raytheon CK51	OAX Sub-	Miniature Valves,	brand

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INDICATOR UNIT TYPE 182A.
unit contains VCR517 Cathode Ray 6in. tube, complete with Mu-metal screen, 3 EF50. 4 SP61 and 1 5UJG valves, 9 wire-wound volume controls and quantity of resistors and condensers. Suitable either basis of television (full picture guaranteed) or filloscope. Offered BRAND NEW (less relay) in original packing case at 79/6. Plus 7/6 carr.

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SMOOTHING CHOKES 250 mA. 7-10 H. 200 ohms. Fully shrouded. 16,9 250 mA. 3 H. 50 ohms. 11,9 150 mA., 6-10 H. 100 ohms. 11,9 100 mA., 10 H. 100 ohms. 7,6 100 mA., 5 H. 150 ohms. 5,6 80 mA., 10 H. 350 ohms. 5,6 60 mA., 10 H. 400 ohms. 4,1 50 mA., 50 H. 1,000 ohms. 9,1 ELIMINATOR TRANSFORMERS Primaries 200-250 v. 50 c/s., 120 v. 40 mA. 90 v. 10 mA., 9-0-9 v. 250 mA. 10/6 120 v. 40 mA., 6 v. 1.5 a. 14/9 120 v. 40 mA., 5-0-5 v. 1.5 a. 15/9 120 v. 40 mA., 5-0-3 v. 1.5 a. 15/9 OUTPUT TRANSFORMERS 3/6 Midget Battery Pentode 66: 1 for 3S4, etc. 3/6 Small Pentode, $5,000\Omega$ to 3Ω 3/9 Small Pentode, $5,000\Omega$ to 3Ω 4/9 Standard Pentode, $5,000\Omega$ to 3Ω 4/9 Standard Pentode, 0,000 to 0.00 4/9 Standard Pentode, 0,000 to 0.00 4/9 Standard Pentode, 0.000 to 0.00 4/9 Multi-ratio 40 mA. 0.00 1, 45: 1, 60: 1, 90: 1, Class B Push-Pull. 5/6 Push-Pull 8 watts 6V6 to 0.00 15/9 Push-Pull 10-12 Watts 6V6 to 0.00 15/9 Push-Pull 10-12 Watts 6V6 to 0.00 15/9 Push-Pull 10-12 Watts by to 332 of 132... Push-Pull 10-12 Watts to match 6V6 to 3-5-8 or 15Ω Push-Pull 115-18 Watts to match 6L6, etc., to 3Ω or 15Ω Speaker Push-Pull 20 Watts, high-quality sectionally wound, 6L6, KT66, etc., to 3 or 15Ω.....

MICROPHONE TRANSFORMERS

22/9

COMMUNICATIONS RECEIVER R1155. The famous ex-Bomber Command Receiver known the world over to be supreme in its class. Covers 5 wave ranges 18.5-7.5 Mc/s, 7.5-3.0 Mc/s, 1,500-600 kc/s, 500-200 kc/s, 200-75 kc/s, and is easily and simply adapted for normal mains use, full details being supplied. Aerial tested before despatch. These are BRAND NEW AND UNUSED IN MAKER'S ORIGINAL TRANSIT CASES, ONLY £111/19/6. A few used receivers, also tested working before despatch, are available at £7 19.6. A few of the R1155N model can also be supplied. This is the latest version which covers the Trawler Bands, and in addition is fitted with ultra slow motion tuning. Used, but tested working before despatch, ONLY £11/19/6. A factory made Power Pack, Output Stage and Speaker, contained in a black crackled cabinet to match the receiver, can be supplied at ONLY £51/19-. Operates receiver immediately. DEDUCT 10/- 1F PURCHASING RECEIVER AND POWER PACK TOGETHER.

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PACK TOGETHER.
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RECEIVERS R1355, as specified for "Inexpensive Television."
Camplete with 8 valves SP61, and 1 each 5U4G and VU 120 or
VU 111. Used, good condition, ONLY 29/6 (carriage etc. 5:6).
RF UNITS TYPE 26 AND 27 for use with the above receiver.
The very popular variable tuning units, which use 2 valves EF54
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27 covers 85-65 Mc/ Mc/s, (3.5-5 metres).
RRAND NEW IN MAKER'S CARTONS. CNLY 59/6 each.
VIBRATOR UNITS. 2 volt type, American made, delivers
67 volts at 4.7 mA, 130 volts at 20 mA, and 1.4 v. L.T. Easily adapted
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ONLY 50/- (postage 2/-).

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6 volt type, made by The National Co. of America for use with HRO Communication Receivers, supplying 165 volts at 85 mA, fully smoothed D.C. Complete with vibrator and 6X5 rectifier in black crackle cabinet, size 7in. x 7½in. x 6in. Slightly used.

ONLY 39'6.

INDICATOR UNIT TYPE 62A. Contains VCR97 tube with mu metal screen, 12 valves EF50, 4 of SP61, 3 of EA50, and 2 of EB34. Built on a two deck chassis containing hundreds of condensers and resistors, potentiometers, etc. In BRAND NEW CONDITION IN MAKER'S TRANSIT CASES. ONLY £7/10/— (carriage 9/6)

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This 6 stage strip measures 18 in. x 5 in. x 5 in., and contains 6 valves working as per details in "Practical Television" October issue. This 6 stage strip measures 18in. x 5in. x 5in., and contains 6 valves VR 65, 1 VR 92 and 1 of VR 96 or VR 53. Mod. data supplied. ONLY 45 - (postage, etc., 2/6). Or less Valves 19,6 (post 2 6). 208 AMPLIFIER. Ideal for conversion into a high gain TV preamp. Complete with 2 valves EF 50. ONLY 15/- (postage, etc., 1/6). CERAMIC 2 WAY 3 BANK SWITCHES, 7/6 each. CHOKES. 10 H. 60 mA, 3/9; 30 H. 100 mA, 12/6; 5 H. 200 mA, 6/- (postage 1 - per choke). TRANSFORMERS. Manufactured to our specification and fully guaranteed. Upright mounties fully supposed account.

 Manufactured to our specification and Upright mounting, fully shrouded normal fully guaranteed. fully guaranteed. Opright mounting, nany shroused normal primaries. 425-0-425 v. 200 mA, 6.3 v. 4 a., 6.3 v. 4 a., 5 v. 3 a., 5 v. 3 a., 50/-. 350-0-350 v. 160 mA, 6.3 v. 6 a., 6.3 v. 3 a., 32 6. 250-0-250 v. 100 mA. 6.3 v. 6 a., 5 v. 3 a., 32 6. Please add 2'-per transformer postage. TRANSFORMERS, FILAMENT. 6.3 v. 2 a., 7/6; 6.3 v. 3 a., 10 f. (Perzene 1'-).

10 6. (Postage 1-2).

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EHT 7,000 v. 5 mA, 4 v. 1 a., 82/6. Please add 2/- per transformer

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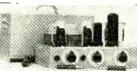
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correctly drilled, heavy angle base.

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	WILII	1622
	trans.	trans.
3in.		10/-
24in.		15/6
3lin.		13/6
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coil, 1,600 ohms O.P. trans.
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T.R.F. coils 5/6. 3 obsolete Ex-Govt. valves, 3 v/holders, and circuit of an A.C. mains 3-valve plus rec. T.R.F. which can be built for approx. £4, 8/6. Heater trans. 6/-. Volume control with switch 3/6. Wave-change switch 2/-. 32+32 mfd. 4/6. Bias condenser 1/-. Resistor kit 2/-. Condenser kit 4/-.

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PARCEL, comprising chassis 12½ x 8 x 2in., cad.
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AS ABOVE, but complete with 16+16 mfd. 350 wkg. and semi-shrouded drop thro' 250-0-250 60 m/a., 6 v. 3 amp. Pri. 200-250. 28/6. P. & P. 3/-.



MODERNISE YOUR OLD CAB-INET BY FITTING THE WAL-NUTBAKELITE ESCUTCHEON as illustrated. Size $15x8\frac{3}{4}$ in., complete with 3 wave-band scale size $5\frac{1}{4}$ x $4\frac{3}{4}$ in. 5/-. P. & P. 1/6.

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16 x 8 mfd., 500 wkg. 3/9
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150 mA. 3/6. 250 mA. 4 henry,
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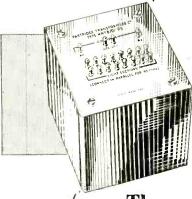
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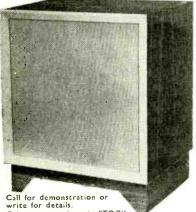
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FOR SALE AND WANTED ADVERTISEMENT FORM TURN TO PAGE NO. 114.

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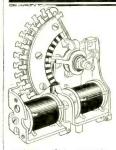
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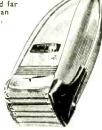
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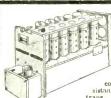
POWER-SERVOS, AP 55938 motor torque transmitters. £8.

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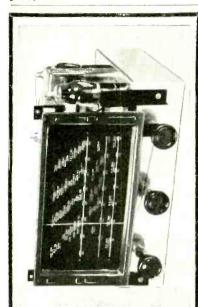
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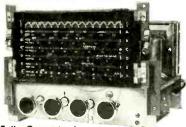
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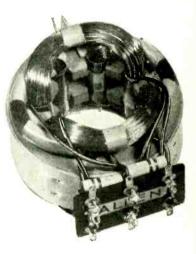
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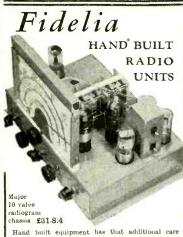
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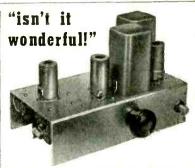
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NSPECTION supervisors required by a large engineering company situated in the London area, applicants should have held a similar position and have previous experience of radar and/or radio equipment: a knowledge of pulse circuitry essential; modern factory and good staff conditions; please write, in confidence quoting reference W/IP, giving full details of experience to—Box 7014.

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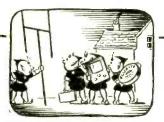
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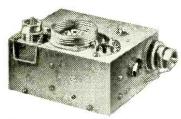
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[9908]

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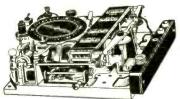
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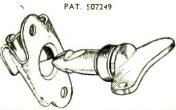
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