When purchasing a Valve Tester ask the following questions:-

Is it a simple Go/No Go instrument, or will it enable you to take measurements at any point on a characteristic curve?
The "AVO" Valve Characteristic Meter can be set up in a matter of seconds and used as a simple Go/No Go tester if required. It will, in addition, produce sufficient information to enable the valve's static characteristic curves to be plotted.
Does the instrument depend for its opcration on pre-determined empirical data issued by its manufacturer?
The "AVO" Valve Characteristic Meter simulates normal working conditions for the valve under test and thus is capable of reproducing the valve manufacturer's data.

Will a high slope valve, wher placed in the instrument, hurst into spurious oscillation, thus giving rise to incorrect readings and possible damage to the valve?
The "AVO" Valve Characteristic Meter incorporates a specially designed panel layout and wiring system (prov. patent) which virtually eliminates spurious oscillation.
Does the instrument contain valves which may need replacing from time to time?
With the exception of a small protection diode, there are no internal valves to deteriorate or break down and cause misleading readings to be given. Thus, expensive periodical replacements are not required.
Will the instrument detect arid current and indicate its direction and magnitude?
The "AVO" Valve Characteristic Meter will indicate the direction of flow of gnd current and give its magnitude in microamps.
Does the Instrument test diolles and rectifiers under load? The "AVO" Valve Characteristic Meter checks diodes and rectifiers under load conditions.

The "AVO" Valve Characteristic Meter measures interelectrode insulation in megohms with valve cold or hot, also cathode/heater insulation with the valve hot, and indicates any breakdown below $10 \mathrm{~m}=\mathrm{gohms}$. It will carry out tests on small thyratrons, tuning indicators, etc. It is fitted with on small thyratrons, tuning indicators, etc. It is fitted with available to keep the instrument fully up-to-date should new bases come into use. A special form of polarised relay is incorporated to give protection against inadvertent over. loads or valve failure.

Write for fully descriptive literoture

THE AUTOMATIC COIL WINDER \& ELECTRICALEQUIPMENT CO. LTD. WINDER HOUSE. DOUGLAS STREET . LONDON S.W.I Celephore VICiorio $3104-9$
 If you are called upon to select a pair of accurately matched valves, will the valve tester carry out the required checks, and maintain your reputation as an expert
The "AVO" Valve Characteristic Meter enables the slope, and anode, screen, or grid current of a multielectrode valve to be checked with any voltage between 0 and- 100 V on the control grid.
Before any information can be obtained about a valve, must the instrument be provided with a complex serics of accessories which may become lost, mutilated, or are not available when an umusual or now type of ralve has to be tested?
The "AVO" Valve Characteristic Meter is provided with two handbooks. The first gives detailed information on the technique of valve testing, full circuit diagrams and adequate operating instructions. The second is a quick reference Data Manual covering more than 3,000 British, American and Continental valves, and gives inter-service equivalents. The Valve Data Manual is

## PLASTIC MOULDINGS

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A NEW R.F. PENTODE WITH

## 1 Recommended Frequency Limit $400 \mathrm{Mc} / \mathrm{s}$.

2 Mutual Conductance 5.1mA/V
3 Filament Consumption 175 mA ,
The Mullard R.F. Pentode, EF95, provides a better size to performance ratio than that previously obtainable from British valves of a similar class. It is constructed on the B7G miniature base and works efficiently at frequencies up to $400 \mathrm{Mc} / \mathrm{s}$. Some of the more outstanding features of this valve include low input capacitance, low anode to grid capacitance, high mutual conductance and low heater consumption. These features, together with an operating voltage of 180 volts ( 120 volts under certain conditions), will particularly interest designers of compact communications equipment. In circuits involving a number of R.F. and I.F. stages, the EF95 may be used throughout, with a resultant marked saving in total heater consumption. Furthermore, the use of only one valve type in such applications enables maintenance problems to be reduced. The EF95 has similar electrical characteristics to the American 6AK5, and may be used as a direct replacement for it.
Full technical information on this and other types in the Mullard range of communication valves is available on request.


TECHNICAL DATA

HEATER

| Vh | $-\quad 6.3 \mathrm{~V}$ |
| :--- | ---: |
| lh | -0.175 A |

## CAPACITANCES

Cin - $4.0 \mu \mu \mathrm{~F}$
Cout $=2.8 \mu \mu \mathrm{~F}$
$C_{a-g l}-0.02 \mu \mu \mathrm{~F}$

CHARACTERISTICS

| $\mathrm{Va}_{\text {a }}$ | - | 180 V |
| :---: | :---: | :---: |
| $V_{g 2}$ | - | 120 V |
| $\mathrm{VgI}^{1}$ | - | -2.0 V |
| La | - | 7.7 mA |
| $\mathrm{I}_{\mathrm{g} 2}$ | - | 2.4 mA |
| gm | - | 6.1 ma/V |
| ra | - | $690 \mathrm{~K} \Omega$ |

LIMITING VALUES
Va max. - 180 V
pa max. - 1.7 W
$\mathrm{V}_{\mathrm{g} 2}$ max. - 140 V
pg2 max. - 0.5 W
lk max. - 18 mA
BASE B7G

## Mullard

## APPLICATION 95

SERIES 38


IN this instance the Series $38^{\text {" }}$ Flexilant" Mounting protects a delicate instrument from vibration and shock. Other applications are manifold - from aircraft to power-station instrument panels: from ship's instruments to the protection of pyrometers in a steel works.

We produce a range of components that absorb vibration; climinate noise; suppress shock. Our new catalogue lists all these
 for you.

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IN ASSOCLATION WITH EMPIRE RUBBER COMPANY


. . . with safety in the hazardous enterprise of the deep sea trawler is its radio and radar equipment upon which safe navigation depends. Thousands of soldered joints contribute to the efficient functioning of this delicate apparatus. One dry or H.R. joint could mean the breakdown of a circuit, the destruction of the vital link, a perilous voyage.

## faUltless fluxing preseryes the vital link

Dry or H.R. joints are impossible with Superspeed for the flux is always released in exactly the correct proportion. This faultless fluxing action is
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for general electrical, electronic and telecommunication work and all standard uses. A.I.D. and G.P.O approved. Complies with M.O.S. Specification DTD 599. In all standard tin/lead alloys, 10-22 S.w.g. Also available in a range of coloured cores, indispensable for simple intermediate and final inspection and circuit or operator identificazion. Samplesor Superspeed and the compreheasive Superspeed bookles gladly sent on request. Technical adviser: are avallable for free consultation.

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##  <br> present THEIR LATEST DEVELOPMENTS IN CONDENSERS



FfOR the benefit of those who were unable to visit the recent R.E.C.M.F. Exhibition, and for those who had not the time available to inspect our Stand in detail, we illustrate here the range of T.C.C. latest developments displayed thereon.

These are indicative of the progress which is constantly being maintained, and which ensures that "T.C.C. Leadership in Condensers" is a tangible reality.
I. SMALl CAPACITY Close tolerance tubular ceramics
For top end coupling in Band Pass Filters. Capacity range 0.5 pF to 5 pF at 500 v.D.C. Tolerances $\pm 20 \%$ and $\pm 10 \%$.

## 2. TANTALUM ELECTROLYTICS

The special neutral electrolyte prevents corrosive injury in the event of mechanical damage. These $8 \mu \mathrm{~F}$ condensers are for working voltages up to 120 v D.C. and for temperatures up to $120^{\circ} \mathrm{C}$.
3. "METALPACK" \& "METALMITE" PAPER TUBULARS IMPREGNATED in "VISCONOL-X"

New impregnant improves reliability at $100^{\circ} \mathrm{C}$. Full Ministry Type Approval (R.C.S.I31 Cat.A.H2) has been granted.
4. "METALPACK" PAPER TUBULARS with CERAMIC END SEALS
New external construction gives complete protection against moisture in $100 \%$ humidity at $100^{\circ} \mathrm{C}$.
5. H.V. TUBULAR CERAMICS

For Pulse Feeders in Radar equipment and Line Time bases in T.V. receivers. Ranges available for 1 kV . to 10 kV . D.C. working. Capacities from 10 to 620 pF .
6. HIGH VOLTAGE PAPER SMOOTHING CONDENSERS TYPE C.P. 561
For 25 kV . E.H.T. smoothing in large screen T.V. receivers. Absence of metal at "hot end" prevents corona losses.

## 7. HIGH TEMPERATURE ELECTROLYTICS

Ability to work at $85^{\circ} \mathrm{C}$. without voltage de-rating. Characteristics low leakage current and high ripple rating.


## THE TELEGRAPH CONDENSERCOMPANYLIMITED

 RADIO DIVISION: NORTH ACTON•LONDON W. W. $\cdot$ Telephone: ACORN 0061 (9 lines)

Obviously, there is no room in this announcement for full technical data on these various Condensers.

We shall be happy to supply complete details of any range in which you are particularly interested, or to advise you of the types most suited to your particular requirements.

## 8. SUB . MINIATURE ELECTROLYTICS for

 HEARING AIDS \& TRANSISTORSSmallest Electrolytic ever made. Two sizes available- $6 \mu \mathrm{~F}$ for 3 v . D.C. working and $8 \mu \mathrm{~F}$ for 6 v. D.C. working.

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## 12. CLOSE CONTROLLED TEMPERATURE COEFFICIENT CERAMICS

For Temperature Compensation in Oscillator and I.F. circuits. "Plimosea!" finlsh improves stability. Available in 6 temperature Coefficients.

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Type $928-8 \mu$ F. $800 v$. D.C. working. 900 v . surge at $60^{\circ} \mathrm{C} .700 \mathrm{v}$. D.C. working. 800 v . surge at $70^{\circ} \mathrm{C}$. All-Aluminium Internal Construction: Chassis mounting. Fully tropical.

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INSTANT and POSITIVE SELECTION by single knob control of any one of the five B.B.C. Television channels is the job for which we designed this new "Cyldon" Switched Teletuner. It was the centre of great interest at the recent R.E.C.M.F. Exhibition, and we are pleased and proud to present these further details.
The "Cyidon" TV. 5 Teletuner comprises a pentode R.F. amplifier stage and a double triode frequency changer, channel selection being accomplished by the switching of incremental inductances. More constant performance over the television band is thus obtalned by avoiding the tracking difficulties inherent in the infinitely variable type of tuner. Ease of handling by the user and rapid conversion as alternative transmissions become available are further important advantages of this unit.


$$
\text { Underside view of "Cyldon" TV. } 5 \text { Teletuner, with casing removed. }
$$

Another new "Cyldon" Teletuner . . . Type TV.12, a 12-channel Tuner which performs the functions of RF amplifier and frequency changer of a television receiver. Write for booklet TV. 1953 giving full details.

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Capacitance range -0.002 pF to $100 \mu \mathrm{~F}$ in 18 ranges.
Resistance range - 18 to $10,000 \mathrm{Mn}$ in 18 ranges.
Ranges increase in alternate decimal multiples of 3 and 10 .
Frequency 1592c/s $(\omega=10,000$ ).
Accuracy $\pm 1.0 \%$ of full scale on all ranges,

Full technical details are available on request.
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MODEL TCA/6236 with mounting assembly of sturdy die-cast metal; three section telescopic rod (extended 62 in. , closed 24 in .) of bighgradz brass. All exposed parts heavily chromium plated and with fully weatherproofed connections. Complete with 36 in . lcw-loss co-axial polythene insulated P.V.C. covered cable, fitted with standard co-axial plug.

List price $35^{\prime}$ -
MODEL TCA/6260 as above but with 60 in. cable.
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Full detoits ore given in leoflet No. NI/W, avolable on request.

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H ere is revolurion in car aerial design-a ONE hole fixing aerial that can be completely installed FROM THE OUTSIDE. No longer is it necessary to manocuvre under the scuttle or dashboard and to work "by feel." Thanks to the use of a special split washer device, in conjunction with a positioning sleeve, the aerial is self-locating, and is firmly secured FROM THE OUTSIDE. It can be mounted vertically or horizontally (or at any angle in between) in any convenient position on the car-on either a flat or curved surface, such as the bonnet, scuttle, roof or mudguard.

And in position it is entirely free from rattle - due to the special packing glands which also ensure the smooth action of the telescopic rod. This aerial has that highsignal pick-up and electrical efficiency always associated with every Antiference Aerial.

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## specify

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The Tuning Coil shown is supported by our "FREQUELEX" Ceramic Rods, and forms part of a 200 K.W. Radio Transmitter. This is only one of many applications where Rods made to close limits are required.
We specialise in the manufacture of Ceramic Rods and Tubes of various sections in several classes of materials over wide dimensional ranges.
The Principal Materials are :-

1. Porcelain for general insulation.
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Large Rods up to $44^{\prime \prime}$ long and I " " square are used as supports for Tuning Coils, etc.


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Designed and manufactured for G.P.O.
This is a precislon instrument for measurements on multi-circuit coaxial cable carrier systems by means of a comparison with locally generated signals of known frequency and level.

Frequency coverage : $60 \mathrm{Kc} / \mathrm{s}-3 \mathrm{Mc} / \mathrm{s}$ in 7 ranges.

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When the fishermen have hauled their nets or seines, and secured a good catch, they call the fish whole. saler on their SIMRAD Radio Telephone, which is also fitted with a SIFAM Instrument.

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Complete with 3-band glass scale 9in. $\times 4 \frac{1}{4} \mathrm{in}$. Printed short, medium and long wavebands with station names. Scale length 7in. Supplied with florentine bronze escutcheon.

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Replacement Scales calbrated to Copenhagen Plan now available for:
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Model 0222A is introduced to meet the demand for an oscillator reaching $10 \mathrm{Mc} / \mathrm{s}$. It is an improved version of the 0222 which it supersedes All the outstanding features of the original model are retained, including low harmonic content and exceptional stability of frequency and amplitude.

## SPECIFICATION

Frequency Range:
$10 \mathrm{Kc} / \mathrm{s}-10 \mathrm{Mc} / \mathrm{s}$ in 6 ranges
Frequency Stability: better than 1 in $10^{3}$ in 1 hour

Frequency Accuracy: Output:
$+10 \mathrm{db} 10-50 \mathrm{db}$ on $1 V p-p$

Output Impedance:
75 ohms
Total Harmonic Content:
less than 1\%

Amplitude constant to within $\pm \frac{1}{2} d b$ at any frequency setting

## A Technical for Electronic Engineers

This Handbook contains the fullest information about all types of Ferranti Valves and Cathode Ray Tubes, giving for each type complete data such as physical details, base connections, ratings, operating conditions, with graphs, etc., where necessary.
The whole is a most valuable book of reference to the electronics engineer. It is in loose-leaf form, so that new data can readily be inserted.

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 POTENTIOMETERSDesigned to meet the demand for Egen reliability within the smallest possible compass, these exceptionally small carbon potentiometers ( $\mathbf{z}^{\prime \prime}$ diameter) retain all the desirable features of their standard-size counterparts. The special Egen carbon deposition process ensures a highly stable

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## FULLY INTERLEAVED

SCREENED AND IMPREGNATED. ALL GUARANTEED.
ALL PRIMARIES ARE 200/250 v. Half Shrouded.
HSM63 (Midget). Ourput $250-0-250 \mathrm{v} .60 \mathrm{~m} / \mathrm{a} .6 .3 \mathrm{v}$. at 3 amps .
5v. at 2 amps. ..............................................................
HS63. Output 250-0-250 v. $60 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v}$. at 3 amps., 5 v . at
HS40. Windings as above. 4 v . at 4 amps., 4 v . at 2 amps......... Output
HS2. 250-0-250 v. $80 \mathrm{~m} / \mathrm{a}$
HS3. $350-0-350$ v. $80 \mathrm{~m} / \mathrm{a}$. HS $30.300-0-300 \mathrm{v} .80 \mathrm{~m} / \mathrm{a} \ldots \ldots$
HS2X. 250-0-250 v. $100 \mathrm{~m} / \mathrm{a}$. HS75. 275-0.275 v. $100 \mathrm{~m} / \mathrm{a} . \ldots . .$.
HS $30 \times .300-0-300 \mathrm{v}, 100 \mathrm{~m} / \mathrm{a}$. HS3X. $350-0-350 \mathrm{v} .100 \mathrm{~m} / \mathrm{a}$ Fully Shrouded
FSM63 (Midget). Output $250-0-250$ v. $60 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v}$. at 3 amps . 5 V .2 amps.
FS2. 250-0-250 v. $80 \mathrm{~m} / \mathrm{a}$.
FS30. $300-0-300$ v $80 \mathrm{~m} / \mathrm{a}$. FS3. $350-0-350$ ४. $80 \mathrm{~m} / \mathrm{a}$
FS2X. 250.0-250 v $100 \mathrm{~m} / \mathrm{a}$. FS75, 275-0-275 v. $100 \mathrm{~m} / \mathrm{a}$. FS $30 \times \quad 300-0.300$ ₹ $100 \mathrm{~m} / \mathrm{l}$ FS3X, 350-0-350 v. $100 \mathrm{~m} / \mathrm{a}$
All the above have $6.34-0 \mathrm{v}$, at $4 \mathrm{amps} .5 .4-0$ at 2 amps.
FS43. Output $425-0-425 \mathrm{v} .200 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .4 \mathrm{amps}$., C.T. 6.3 v
4 amps. C.T. 5. v 3 amps. Fully shrouded
FS50. Output $450-0-450$ v. $250 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .2$ amps., C.T. 6.3. v.
4 amps., C.T, 5 v. 3 amps. Fully shrouded
F30X. Output $300-0-300 \mathrm{v}, 80 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .7 \mathrm{amps} ., 5 \mathrm{v}, 2 \mathrm{amps}$.
Framed. Flying leads
F35X. Output $350-0.350$ v. $250 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .6 \mathrm{amps}$., 4 v .8 amps .
4 v .3 amps., $0-2-6.3 \mathrm{v} .2 \mathrm{amps}$. Fully shrouded
FSI60X. Output $350-0-350$ v. $160 \mathrm{~m} / \mathrm{a}, 6.3$ v .6 amps ., 6.3 v 3 amps., 5 v .3 amps. Fully shrouded
FS43X. Output $425-0.425$ v. $250 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .6 \mathrm{amps} ., 6.3 \mathrm{v}$ 6 amps., 5 v. 3 amps. Fully shrouded
HS6. Output $250-0-250$ v. $100 \mathrm{~m} / \mathrm{a}$, , $6.3 \mathrm{v} .6 \mathrm{amps} .$, C.T. 5 v 3 amps. For receiver R1355. Half shrouded.
HS150. Output $350-0-350$ v. $150 \mathrm{~m} / \mathrm{a}$., $6.3 \mathrm{v} .3 \mathrm{amps} .$, C.T. 5 v
3 amps. Half shrouded ….........................................
F36. Output $250-0-250$ v. $100 \mathrm{~m} / \mathrm{a} ., 6.3$ v. 6 amps., C.T. 5 v
3 amps. Fully shrouded $\ldots . .120 \mathrm{~m} / \mathrm{a} .6 .3 \mathrm{v} .2$ amps., C. T. 6.3 y v
FSI20. Ourput 350-0-3
2. amps. C.T. 5 v. 3 amps. Fully shrouded

FS256. Output $250-0-250$ v. $80 \mathrm{~m} / \mathrm{a} .63$ v at 6 amps ., 5 v . at
3 amps. Fully 5 hrouded
PRI/I. Output 230 v , at $30 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v}$. at $1.5 / 2 \mathrm{amps} . . . . . . . . . . . .$.
FSI $150^{\circ} .350-0.350 \mathrm{v}, 150 \mathrm{~m} / \mathrm{a} ., 6.3 \mathrm{v} .4$ amps., $5 \mathrm{v} .3 \mathrm{amps} . . . . . . .$.
FSI 50 X . Output $350-0-350 \mathrm{v}$. at $150 \mathrm{~m} / \mathrm{a}$, , 6.3 v . at 2 amps .,
C.T. 6.3 v . at 2 amps., C.T. 5 v . at 3 amps . Fully shrouded..

The above have inputs of $200 / 250 \mathrm{v}$.

## FILAMENT TRANSFORMERS

All 200/250 v. Input
F4. 4 v . at $2 \mathrm{amps}, 9 / \mathrm{m}$. F6. 6.3 v at 2 amps .
F6X. 6.3 v . at 0.3 amps., $6 / \%$. F 12 X. 12 v at 1 amp .
FU6. $0-2-4-5-6.3 \mathrm{v}$, at $2 \mathrm{amps} ., 11 / \mathrm{w}$. F12. 12.6 v tapped 6.3. at 3 amps .
F24. 24 v . tapped 12 v . at 3 amps.
F29. 0-2-4-5-6.3 v. at 4 amps., 20/9. FÜi2. 0-4-6.3 v. at
3 amps.
FU24. 0-12-24 v. at I amp. ..................................................
F5. 6.3 v . at 10 amps ., or 5 v . at 10 amps . or 12.6 v . at 5 amps . or 10 v . at 5 amps .
F6/4. Four windings at $6.3 \%$ tapped 5 v . at 5 amps. each, giving by suitable series and parallel connections up to 6.3 v . at 20 amps.
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F25. 25 v. at 4 amps ., $40 /$. F26. Two windings 6.3 v . at
F.27. Two windings 12 v . at 1.5 amp

F28. Two windings 5 v at 3 mps $25 /-\mathrm{F} 32 \mathrm{l} 10 \mathrm{v}$ at 5 mps
F.28. Two w 60100 . $v$ at

F33. $0-10-30-60-100 \mathrm{v}$. at I amp.
F34. 0-4-9-15-24 vo at 3 amps ., 31/6. F35. 6.3 v o at 6 amps .
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10 H . at $150 \mathrm{~m} / \mathrm{a}$.


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Many of these valves have been supplied to the British Broadcasting Corporation for use in their special recording, amplifying, and crystal controlled precision drive equipments, some of which are illustrated on this page.
B.B.C. Type D. Recorder Line Amplifier LFA|1 using two pentode connected ACISP3.RH valves
B.B.C. Type D. Recorder Loudspeaker Amplifier LSM17 using three pentode connected ACISP3.RH valves


AC/SP3.RH

| Anode Voltage (Va) | 250 | 250 | 250 | 250 |
| :---: | :---: | :---: | :---: | :---: |
| Screen Voltage (Vg2) | 80 | 100 | 160 | 200 |
| Grid Bias (Vgl) | 1.25 | 1.7 | 2.75 | 3.5 |
| Anode Current (mA) | 7.8 | 7.9 | 10.5 | 12.3 |
| Screen Current (mA) | 2.45 | 2.5 | 3.3 | 3.85 |
| Mutual Conductance (mA/V) | 7.0 | 7.0 | 7.45 | 7.6 |
| Anode AC Resistance (ra) | 0.55 | 0.55 | 0.4 | 0.3 |
| Input Capacity (Hot) ( $\mu \mu \mathrm{F}$ ) | 20 | 19.9 | 19.7 | 19.5 |

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MODEL 150 MARK II $12^{\prime \prime}$ TWIN CONE
$1018^{\prime \prime}$ SINGLE CONE
$1028^{\circ}$ SINGLE CONE
BY THE COURTESY of Messrs. Goodmans Industries Ltd. we have recently had the opp tests. improvement on these speakers in, is a very definite smother middle The 1 model, with a firmer, smoothe (nominally the Mark 10 wer fundamental resonase the speaker register and It was not possible to house by Messrs. $35 \mathrm{c} \cdot \mathrm{p} . \mathrm{S}$. cabinet designed for the purpose Goodmans, but mounted in a labyrin back of the cone Goodmans, birtually the sound from the of this reproducer virtually alling characteristics very even response in the were hard. clear bass, very even respoedle hiss of were hard and upper registers and middle andonable quality. Responit which should give This is an excellent to Societies. It will handle up every satisfaction to 15 watts.
The main difference between the rlux density of the is the increased sensitivity andurally.
latter. These quallt and increased price ${ }^{\text {m }}$ units we by improved dampingly the best 8 units whic response These are undested, and the maker soch for was fully have so far te. from 40 to 15,000 c.p. withintiated. They showed no signs or when fed with peak inputs uptained running the Axiom Excellent results were obtained 150 to secure wider 101 in parallel with the Axiom sound, and also running two 8 distribution of sound, andatter case there was units in parallel. In the extreme bass. rather less weight in the extht and air in the treble A very pleasing offect of lightanda by using an 8 and wide sound source canflecting into a corner in unit on a small baffle refinet-mounted 8 or 12 parallel with another cab should have a 2 mfd the speaker. The (NOT electrolytic) in series voice coil. For their size and price the performance oity. Axioms 101 and 102 is outstanding-in quality. Axioms 101 and


 El9.8. 4 (incl. purchase tax)

66. 12. I (inel. purchase tax) AXIOM 102
69. 18.2 (incl. purchase tax)

- We acknowledge with thanks the permissian to reproduce the above report which is on extract from the lanuary issue of the Society's private journal All these models are stocked by the leading dealers, but in case of difficulty please order direct from us. We invite you to write for further details of any unit. Remember we can give you outlined dimensioned drawings of reflex chambers for all Speakers mentioned.
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"WOW" AND FLUTTER Less than $0.2 \%$.
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Tommy Bars
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For cutting smaller holes neatly and quickly with one blow of a light hammer

Prou.
Pad.

| Type | Hole Size tin. | $\begin{gathered} \text { Price } \\ 6 / 6 \end{gathered}$ |
| :---: | :---: | :---: |
| 2 | 䨞in. | 7/6 |
| 3 | $\frac{1}{2} \mathrm{in}$. | 8/9 |
| types | cutters ar | of hard |
| and 3 | for use | steel |

steel and are for use on steel up to
$18 \mathrm{s.w.g}$. Brass and Dural up to $16 \mathrm{~s} . \mathrm{w} . g$. $18 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. Brass and Dural up to $16 \mathrm{~s} . \mathrm{w} . g$.
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Constanta High Stability Resistors
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Tape speeds $7 \frac{t^{\prime \prime}}{}$ and 15" per second, or $33^{\prime \prime}$ and $1 \mathrm{l}^{\prime \prime}$ per second.
$\bullet$
Synchronous drive motor.

## -

Remote operation or foot control. -
Automatic back spacing and reverse drive for dictation purposes.
-
Cassette tape loading. -
Rack mounted assembly.

TAPE SPEEDS $7 \frac{1}{2}$ " and $3 \frac{3}{3}^{\prime \prime}$ per second.
TRACKS
PLAYING TIME PER TRACK

SPOOLS

SENSE OF
SPOOLING
REWIND TIME
HEADS

TAPE
OPERATION

1" wide. Number of tracks 2 30 minutes at $7 \mathrm{~J}^{*}$ per second. 60 minutes at $34^{\circ}$ per second.

$$
\text { Standard } 7^{\circ} \text { and } 5^{\circ} \text { plastic or }
$$ metal.

From left to right with tape coating inwards.
One minute for $1,200 \mathrm{ft}$. of tape (approx.).
R.F. erase head. Record/ playback head off-set for recording on upper track. Provision on player unit for additional monitoring head for spectial applications.

Single control provides:Record, Playback, Fast Forward, Cueing, Rewind.
To ensure additional safety against accidental erase, an against accidental erase, an additional record playback
switch is provided on the amplifier assembly. Power and amplifier assembly. Power and brake operation is by means of
a relay which will enable rea relay which will enable re-
mote operation to be provided mote operation to be pr
in special applications.

## DIMENSIONS

WEIGHT

## FREQUENCY RESPONSE

DISTORTION

SIGNAL/NOISE

## RATIO

INPUTS

OUTPUTS (1) $2 \frac{1}{2}$ ohms at 3 watts to in-

WOW AND
FLUTTER
MAINS SUPPLY less than $\cdot 2 \%$.
$200 / 250$ v. 50 cycles 230 V.A Other voltages and frequencies supplied to special order.
At 71." per second $60-10,000$
C.P.S. plus or minus 3 db . At $32^{\circ}$ per second $70-7.000$ C.P.S. plus or minus 3 db .

Less than $2 \frac{1}{2} \%$ total harmonic disrortion at normal operaring level.

Approximately 50 db . using standard high output tape.
(1) Up to 50 ohms low level -110 db . microphone input.
(2) High Z up to 100 K at Iv . unbalanced (radio inpur). rernal loudspeaker.
(2) 15 ohms at 3 watts for external speaker.

Total wow and flutter content
$16^{\circ}$ wide $\times 11^{\circ}$ high $\times 18^{\circ}$ deep approx.
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| BRASS |  | TEEL |  |
| :---: | :---: | :---: | :---: |
| NP | 1/10 | ${ }^{\prime \prime}{ }^{\prime \prime}$ CS CP | $1 / 2$ |
| $\frac{1}{2}{ }^{\prime \prime}$, , , | 2/3 |  | 1/3 |
| $\frac{3}{4}$ " , , , | 2/9 | $\frac{3^{\prime \prime}}{}{ }^{\prime \prime} \mathrm{RH}$ | 1/4 |
| $\frac{7}{8 \prime \prime}{ }^{\prime \prime}{ }^{\prime \prime}$ | 3/- | SC | 1/2 |
| $\frac{11}{\prime \prime}$ CS ", | 1/8 |  | 1/4 |
|  | 2- | $\frac{1}{2}^{\prime \prime}$ CS CP | 1/4 |
| 㝘" ${ }^{\prime \prime}$, | 2/3 | RH SC | 1/6 |
| $\frac{3}{8 \prime \prime}$ ", , | 1/10 | $\frac{7}{8}{ }^{\prime \prime}$, ${ }^{\text {c }}$ | /9 |

## 2BA

|  | H |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
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|  | " | " |  |  |
| $\frac{7}{1}$ |  | , |  |  |
|  |  |  |  | 5 |

BRASS

| CH NP | 4/6 | $\frac{1_{4}^{\prime \prime}}{4} \mathrm{H}$ HSC | 1/9 |
| :---: | :---: | :---: | :---: |
| SC | 3- | $\frac{1}{2}{ }^{\prime \prime}$ LgeRH | 2- |
| 1" .. ., | 5/- | $\frac{3}{4}{ }^{\prime \prime}$ RH SC | 2 |
| NP | 6/- | $\mathrm{I}^{\prime \prime} \mathrm{CH}$ | 216 |
| CS | 4/- | $1 \frac{1}{1}{ }^{\prime \prime}$ RH CP | $2 / 9$ |
| SC | 4/9 | [" CS | 2 |

## 8BA

| $\frac{3}{10^{\prime \prime}} \mathrm{CHNP}$ |  | 2- | 8/" CH SC | 2- | CH CP | 2- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $2 / 6$ | $\frac{5}{10}^{10}$ RH NP | $2 / 2$ | $\frac{3}{16}{ }^{\prime \prime} \mathrm{CS}$ | 2- |
| $\frac{1^{\prime \prime}}{4} \mathrm{CS}$ | ," | 1/8 | $\frac{9}{16}$ | 216 | ${ }^{\frac{3}{16}}{ }^{\prime \prime} \mathrm{CH}$ | $2 / 2$ |
| $\frac{5}{16}{ }^{\prime \prime} \mathrm{CH}$ | " | 2/3 | ${ }^{\frac{3}{4}}$ | $2 \cdot 9$ | $3^{7}{ }^{\prime \prime}{ }^{\prime \prime} \mathrm{RH}$ | 2/2 |
| $\frac{5}{16}{ }^{6}$ CS | , | 1/9 | ${ }^{\frac{3}{81}}{ }^{\prime \prime}$ Hex | $2 / 9$ | ${ }_{\frac{1}{4}} / \mathrm{CH}$ NP | $2 / 3$ |
| $\frac{7^{\prime \prime}}{}{ }^{\prime \prime}$ | , | 216 | $\frac{7}{16}{ }^{\prime \prime}$ | $2 / 10$ | $\frac{3}{8 \prime \prime}$ RH CP | 2/3 |

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seep it up.
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16.3 .53

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32. Collaro 3 -speed Mixer $7^{\prime \prime}, 10^{\prime \prime}, 12^{\prime \prime}$.
33. B.S.R. Monarch $7^{\prime \prime}, 10^{\prime \prime}, 12^{\prime \prime}$.
34. Trixette A358 3-speed Garrard.
35. Decca Decalian 2-speed S/p.

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34. Decca XMS with two Heads.
35. Decca Hi-Fi Mag. Pickup Head
36. Connoisseur Pickup.
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38. Connoisseur Pickup Transformer
39. Leak Ruby Standard or L.P.
40. Leak Diamond Std. or L.P.
41. Leak Pickup Transformer.
42. Acos G.P. 19.
43. Acos G.P. 20.
44. Acos L.P. and Std. Heads.
45. Acos Pickup Arm.
46. Decca Pickup Arm.
47. Collaro Pickup Arm.
48. Chancery Crystal Pickup.

5‥ Decca Crystal Pickup.

## * LOUDSPEAKERS

52. Goodman's Axiom $1018^{*}$ 53. Goodmans Audiom 60. 54. Goodmans Axiom 150 Mk. II.
53. Tannoy Duo Concentric $15^{\prime \prime}$.
54. Tannoy Duo Concencric $12^{\prime \prime}$
55. Decca Corner Speaker.
56. Wharfedale Super 5/CS/AL.
57. Wharfedale Super B/CS/AL.
58. Wharfedale OMMI Direc. 3-unit. Wharfedale $10^{\prime \prime}$ Golden Wharfedale $10^{\prime \prime}$ CSB. Wharfedale W/12/CS. Wharfedale WI2/CS/AL Whariedale WIS/CS. WB Stentorian $12^{\prime \prime}$ unit. Rola G. 12 units. Classic " Concert " 2-unit. Acoustical Corner Ribbon. Vitavox "Klipschorne"
59. Classic Hi-Fi Cabinet for Quad/Leak Amp.
60. Vaigt. unit only.
61. Voigt. Corner Horn (White).

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76. Wearite Type $B$ Tape Deck.
77. Bradmatic Desk 6RP Heads.
78. Sound Mirror Type A.
79. Truvox Type A.
80. Lane Type 1
81. Qualtape Type 1.
82. Excel. Pro Tape Desk.
83. MSS Type PM RI Recorder
84. Ferrograph Type A.
85. Vortexion Recorder with Wearite Deck. Deck.
84A. Vortexion with Truvox Desk..
86. CIR Portable Recorder
87. Sound Mirror Portable.
88. Sound Mirror Table Model.
89. Simon Model 2B.
90. Simon Model IA.
91. Wirek Magnograph.

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Bradmatic Amplifiers.
3. Scophony Baird Mk. 2
94. Grundig Model A.

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> 96. Bradmatic Plate Coil.
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> 99. Bradmatic Mumetal Screens.
> 100. Bradmatic Tape Guides.
> 101. Bradmatic 5RP Heads
> 102. Bradmatic 6RP Heads.
> 104. Sound Mirror Tape, per ree
> 105. Sound Mirror Tape, per reel
> 106. G.E.C. Tape, per reel
> 107. Scotch Boy Tape, per reel.
> 108. Collaro Tape/Rec. Motors*
> 108. Collaro Tape Rec.
> 109. Spare Spools.
> 110. Acos Microphone.
> 11. Rothermel Mike.
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43rd YEAR OF PUBLICATION

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JUNE 1953

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A.B.C. Receivers In an A.B.C. receiver it is usually necessary to connect the filament of the DM70 in series with the filaments of the other valves. With a chain of valves having 50 mA filament the 25 mA filament of the DM70 should he shunted by a $56 \Omega$ resistor. The positioning of the DM70 in the filament chain needs careful consideration to ensure that the values of grid voltage at zero and at maximum signal give the optimum amount of indication on the DM70.
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It is not recommended that the filament of the DM70 be fed with a direct current from the cathode resistor of the output valve owing to the possibility of wide variations in this current resulting in reduced life of the indicator.

The recommended anode voltage for the DM70 in mains receivers is 60 V , which can be obtained from the h.t. line by means of a series resistor. This results in a sliding anode voltage dependent upon the current of the valve and so extends the range of grid control to deal adequately with strong
signals in a very sensitive receiver. signals in a very sensitive receiver.

As the filament is supplied with an alternating voltage it is necessary to take precautions to prevent hum being introduced into the a.g.c. circuit from the grid of the DMF0.
A.C.D.C. Receivers The filament of the DM70 shunted by a suitable resistor may be connected in series with the heaters of the other valves in an A.C./D.C. receiver provided a surge current limiting device is also included in the series circuit. For mains voltages above 160 V the shunt resistor should be $18 \Omega \pm 10 \%$ when included in a 100 mA heater chain.


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# JIirdoloss World 

## Exhibicions

T would be ungracious-and indeed, foolish- to complain that too much limelight is thrown on our art. All the same, the very large number of exhibitions concerned with radio and electronics are something of an embarrassment to many people, including visitors and exhibitors as well. Although almost all the exhibitions with which we are concerned nowadays are in fact, if not in name, specialized, there is a good deal of overlapping between them. Manufacturers, naturally enough, want to show their products to the largest number of potential users, who, in their turn, want to see what is available to them. But is it possible to avoid the present duplication of effort and to reduce the expenditure of manhours and money by both exhibitors and visitors?
An exhibition organized by the Radio Communication and Electronic Association, with collaboration of the Ministry of Supply, was held recently at Farnborough for the benefit of delegates from the European Defence Community, N.A.T.O. and the British Commonwealth. It was supported by firms in the components and valve sections of the radio industry, and though outwardly of a military character, did in fact cover a much wider field. With some justification this was claimed to be " the most comprehensive display of electronic equipment held anywhere in the world." The pity of it is that this impressive show, which presented the "professional" side of the industry as it has never been presented before, was seen by a mere handful of visitors.
The success of the Farnborough show gives rise to the thought that, for purposes of exhibitions, all radio could be divided into two sections, which might very roughly be described as professional and domestic. The first category would include all products for communication, industrial, commercial and military applications. The domestic show would, of course, deal predominantly with broadcast receiving equipment, but might also cover electronic equipment intended to some extent at least for the general public, including perhaps "business radio." The advantage would be that annual exhibitions organized in this way would provide a focal point of the year
for developments in the main spheres of activity. Such a scheme might not entirely avoid the need for specialized exhibitions, but would at least allow them to be still more specialized, and thus obviate much of the wasteful overlapping that now occurs.

## Tolevision Contersion

A LETTER from a correspondent, printed eisewhere in this issue, expresses the view that the problems involved in designing converters for adapting existing television receivers for reception of the proposed alternative service are rather more difficult than is commonly believed. No doubt, certain types of set, operated in favourable conditions, could be fairly simply adapted, but it does seem most unlikely that a standardized design of converter, applicable to all sets in all conditions, could be produced at low cost.

The tunable receiver having channel selection under the control of the user will lend itself more readily to conversion to the new band, and so it is to be expected that this type of set will become increasingly popular when the start of the alternative service becomes imminent.

An allied problem that has not yet been touched upon at any length is that of aerials for two-band reception. That is one of the many matters connected with the proposed alternative television service that we hope to discuss in detail in the near future.

## Local Conditions:

THE task of the B.B.C. in providing an acceptable medium-wave signal for the whole country is not an enviable one, and becomes more difficult as time goes on. To an increasing extent, compromises are necessary. Critics of B.B.C. quality are inclined to overlook the fact that a transmitting technique that satisfies the listener who lives, figuratively speaking, on the doorstep of a station is quite unacceptable to those in the wilds. The only way out of this difficulty lies in the use of v.h.f.

Survey of the R.E.C.M.F. and Physical Society's Exhibitions


#### Abstract

Since the above two exhibitions ran more or less concurrently in London this year and also overlapped to some extent in their types of exhibits, we have selected the most interesting items from both shows and combined them into this one report. No distinction is made between Physical Society exhibits and R.E.C.M.F. exhibits, but each section dealing with components is followed by a list of the exhibitors in that class.


## RESEARCH AND MATERIALS

The problems of noise measurement in fractional-ohm resistors at temperatures of the order of 20 deg K ( -253 $\operatorname{deg} \mathrm{C}$ ) are formidable and offer an interesting challenge to the amplifier designer. These have been successfully solved in an amplifier designed by P. J. Baxandall at the Telecommunications Research Establishment. Two input transformers are used, the first operating at low temperature and stepping up to 300 in order that the leads to the refrigerant container shall be thin enough to avoid too much loss by heat conduction; the second transformer provides an impedance of $1 \mathrm{M} \Omega$ at $4,000 \mathrm{c} / \mathrm{s}$. In designing the first transformer it was found that at 20 deg K the permeability of Mumetal falls to a third of its normal value, but the shunt eddy-current losses are not appreciably effective. At the level of the noise to be measured microphony in the input transformers is a serious factor, and anti-vibration mounting is necessary. In order to reduce shot noise in the first stage, an ME1400 version of the EF37A was used under electrometer conditions with an anode current of $110 \mu \mathrm{~A}$ and grid current of $10^{-4} \mu \mathrm{~A}$. When used with a tuned circuit having a $Q$ of 50 to $800 \mathrm{c} / \mathrm{s}$, the noise factor was 2.7 db (a figure of 3 db was stipulated).

A compact selective amplifier for the analysis of fluctuation noise in germanium rectifiers has been developed by the Radio Research Station, Slough. The basis is the RC circuit due to Schneider (Phil. Mag. 1945, Vol. 36, p. 371) and five resonant frequencies are provided at $0.1,0.04,0.02,0.01$ and $0.005 \mathrm{c} / \mathrm{s}$ with an effective $Q$ of 8 .

The transparency to infra-red radiation of germanium is exploited in a demonstration, by T.R.E. of the modula-

G.E.C. wide-band panoramic v.h.f. receiver.
tion of a beam. The transmission of infra-red through the germanium is dependent on the number of current carriers present in the germanium and this can be varied by applying an audio signal to a contact fulfilling a similar function to the emitter in a transistor. It was shown that some plastics with high light transmission are relatively opaque at the frequency used, $1.5 \times 10^{8} \mathrm{Mc} / \mathrm{s}$ ( 2 microns).
Selenium in its amorphous form is also transparent to radiation from the infra-red to centimetre wavelengths, and "optical" components such as prisms and lenses have been made by a simple casting technique by the Services Electronics Research Laboratory, Baldock.

An infra-red image converter tube has been applied by Prof. B. K. Johnson (Imperial College) to the microscopy of opaque specimens, and is being used in the examination of minerals for the identification of uniaxial and biaxial crystals.
The detection of impurities in air by the change in emission and surface potential of a prepared plate at normal temperatures was demonstrated by the Signals Research and Development Establishment (Christchurch) using a vibrating capacitor in association with a selective phase-sensitive amplifier-detector. Potential changes of the order of $10 \mu \mathrm{~V}$ can be measured.
Exploration of the wavelengths and field patterns associated with different oscillation modes in a magnetron is effected in apparatus designed by S.E.R.L., Baldock, by means of a rotating pick-up probe extending from the surface of the cathode. The anode is excited by a tunable oscillator and mode "contamination" is readily visible on a c.r.t. display. By changing the axial positions of the excitation and pick-up probes, longitudinal distributions of r.f. voitage can be explored.

Some results of research into the effects of irradiation of insulants by radioactive emanations has been disclosed by the Ministry of Supply. Cross linking in long-chain polymers, such as polyethylene, affects not only the mechanical and chemical properties such as elasticity, melting (transition) point and solubility, but also the power factor which is increased at $65 \mathrm{c} / \mathrm{s}$ and $1 \mathrm{Mc} / \mathrm{s}$, but appears to be unchanged at $9,000 \mathrm{Mc} / \mathrm{s}$.

Although well past the "breadboard" stage a G.E.C. wide-band panoramic v.h.f. receiver developed by the Research Laboratories is conveniently included in this section, if only to show that there can be no hard dividing lines between research, development and production. It is of the double superheterodyne type and gives c.r.t. display of all signals in bands $10 \mathrm{Mc} / \mathrm{s}$ wide between 80 and $220 \mathrm{Mc} / \mathrm{s}$. Sensitivity for twice peak noise level is $10 \mu \mathrm{~V}$, and limitations rusually set to bandwidth by considerations of image rejection have been overcome by sweeping the second oscillator through the converted signal Irequency
in the i.f. amplifier. Pulses on either side of zero beat for each signal are combined to give a single response in the display. Frequency markers are derived from a quartz crystal.

## Materials

Some interesting developments are taking place in the ficld of magnetic materials which will upset many preconceived ideas on the subject. Having become more or less accustomed to the idea of ceramic (ferrite) permanent magnets such as Mullard "Magnadur," we must now accept soft iron permanent magnets. The prediction of Prof. Néel of the University of Grenoble, that pure iron should develop very high coercive force when the particle size is of the order of magnitude of a magnetic domain, has been experimentally confirmed and is found to be a maximum when the crystal size is between 0.1 and 0.01 micron. Above and below these limits the material exhibits its familiar "soft" characteristics. The problems of producing the right grade of power have been solved and G.E.C. in this country are now supplying "Gecalloy Micropowder" magnets in a variety of shapes. The powder has strong cohesive properties and can be cold pressed at normal temperatures without a binder, though a binder is an advantage in some applications. Like the ferrites, micropowder magnets are light, easily moulded and have low eddy current losses, but they have the added advantage of mechanical softness and ease of working. Their properties can also be controlled and in particular the ratio of remanence to coercivity can be varied over a wide range. Energy content ranges from 0.5 to $1.7 \times 10^{\circ}$ gauss-ocrsteds according to the grade of the material and coercive forces up to 700 oersteds are available.

Among conventional magnetic alloys the introduction by Telegraphic Construction and Maintenance of a new series of high-saturation alloys with properties comparable with Permendur, but with better machining qualities was noted; and Swift Levick are now producing columnar crystal anisotropic permanent magnets in simple shapes on a quantity basis. Made under the trade name of "Columax" this alloy has an average energy content of $6.8 \times 10^{6}$ gauss-ocrsteds compared with $5 \times 10^{6}$ for Alcomax III.

London Electric Wire (Lewcos) are now producing instrument wires with p.t.f.e. coatings from 0.0005 to 0.0015 in thickness with adequate adherence and abrasion resistance to withstand normal hazards of winding. Synthetic enamel coatings with greater abrasion resistance than
conventronal oil-based enamels are now available, under the name "Diamel," on precision resistance wires made by Johnson, Matthey. A new range of wires introduced by B.I. Callenders and known as "Fifty Three" have a new strongly adherent and abrasion resistant enamel coating with mechanical and electrical properties intermediate between oil-base and vinyl acetal enamels. Nonstretching binding twines, treated with p.v.c., and designed to withstand tropical acceptance tests, are now available from Associated Techincal Manufacturers.

Although, for all practical purposes, modern activated rosin solder fluxes are non-corrosive, there is still prejudice against their use in some quarters, and ordinary rosin is used in spite of its slow and uncertain fluxing properties. Enthoven have discovered a method of increasing the activity of rosin-cored solder without the use of chemical additives and have marketed the product under the name of "Actol," with a characteristic stellate core, in all standard tin/lead alloys and gauges.

To increase still further the ratio of solder to flux in their three-cored solders "Multicore" have developed an improved activating agent "Pentacol" which will in future be incorporated in their Ersin fluxes which now form 2.2 instead of 3.4 per cent of the total weight. Fluxed solder in tape form is a new departure from Multicore. It can be wrapped round a pair of wires and makes an effective joint when heated by a match flame.

Aluminium soldering has always been regarded as difficult, but a new process developed by the Sheffield Smelting Co., shows more than usual promise and can be carried out with ordinary torch flames at a temperature of 450 deg C . The joints will withstand the accepted accelerated corrosion tests.
Makers*: Associated Technical Manufacturers (B, C, IM, IS, W"); Bakelite (IM); Geo. Bray (CE); B.I. Callenders (C, CO, IS, W); British Moulded Plastics (IM); Bullers ( CE ); Clarke ( CF , ${ }^{\text {MM }}$, British Moulded Plastics (IM); Bullers (CE); Clarke (CF, WM, (C, CO. IS, W); Enthoven (S); Fine Wires (W); Hellerman (IM, IS); Henley's (CO, IM, W); London Electric Wire (CO, W); Long \& Hambley (IM, IS, RP); Magnetic and Electrical Alloys (L, M); Marrison and' Catherall (M); Micanite and Insulators (CF, B, CO, IM, IS); Mullard (DC, M); Multicore (S); Murex (M); Mycalex (IM); James Neill (M); Reliance Wire (B, C, CO, IS, W); Rola-Celestion (D, L, M); Salford (DC, M); Geo. L. Scott (L); S.T.C. (M); Steatite (CE); Suflex (B, CO, IM, IS, W); Swift Levick (M); H. D. Symons (IM, IS); Taylor Tunnicliff (CE); Telcon (C, DC, L, M W); Thermo Plastics (CF, IM); Transradio (C. IS, W); United Insulator (CF, CE, IM); Vactite Wire (W).

* Abbreviations: B, braiding; C, cables; CE, ceramics; CF, coil formers, bobbins; CO, cords; DC, dust cores; IM, insulating materials; IS, insulating slecving; L, laminations; $M$, magnets and magnetic alloys; RP, rubber products; S , solder; W , bare or covered wires.


## COMPONENTS AND ACCESSORIES

The fact that we now have five television channels all occupied is emphasized this year by the appearance of a five-channel tuner for receivers. Made by Cyldon it has an EF80 r.f. amplifier and an ECC81 frequency changer, and the channels are selected, not by a continuously variable control, but by switching in incremental inductances. The power gain of the unit is 24 db and the i.f. output can be either in the band $9.5-14 \mathrm{Mc} / \mathrm{s}$ or the band $15.5-22 \mathrm{Mc} / \mathrm{s}$ according to the receiver manufacturer's requirements.

Another thing which is more of a sub-assembly than a component is the Igranic e.h.t. generator, for use with the new transformerless line scanning circuits. It contains an inductor for boosting the line flyback voltage, an EY51 e.h.t. rectifier and variable inductor for linearity control, the whole being mounted on a moulded base-plate. The unit supplies an e.h.t. voltage of 13.5 kV .

For c.r.t. focusing, permanent magnets moulded from insulated metal powder are coming very much to the fore. Having the advantage of high resistivity, they can be placed close to deflector coils without affecting their performance. An example of their use is to be seen in the focus unit made by Elac, designed for wide-angle c.r.

Right: Igranic e.h.t. unit for direct-drive line-scan

tubes. This has two ring magnets mounted with their fields opposing, and focus is controlled by varying the spacing between them-the minimum field being when they are closest together. The unit centains two other rings, magnetized transversely, which can be adjusted to centre the picture.

The problem of mounting the variable inductors used for width and linearity control has been solved in one way by Egen Electric, who have combined them into a twin unit, and in another by Plessey, who have stowed them in the mounting bracket of their new line scan transformers.
Makers : Advance, British Moulded Plastics, Cyldon, Egen, Electro Acoustic Industries, Igranic. Long \& Hambly. Magnetic \& Electrical Alloys, Mullard, Plesses, Thermo-Plastics, Weymouth, Whiteley.

## Capacitors

Metallized polystyrene film capacitors figure among the latest T.C.C. products. These are comparable in size to small paper types but have infinitely better characteristics. Capacitances up to $0.5 \mu \mathrm{~F}$ are available. Another plastic film capacitor, also made by this firm, has the exceptionally close tolerance of $\pm \frac{1}{8}$ per cent only and power factor of 0.0005 .

The potertially high stability of silvered mica capacitors is not always possible to retain when stacked plates are used, but Johnson, Matthey have introduced a new manufacturing process in which the stack is bonded by


Left: Plessey " Casfilm" silvered ceramic capacitors.

Below: Two of the Parmeko jupiter range of resin potted transformers.


Above: Zenith twin-brush Variac variable voltage transformer.
firing at a controlled temperature. Reduction in size is claimed as a by-product of this process.
Wider temperature ranges are a feature of some of the latest Hunt's capacitors; for example, their "Thermetic Midget" can be used without derating from -100 deg C to +120 deg C .
A new technique is exemplified by the Plessey "Casfilm" silvered ceramic film capacitors. The smallest, measuring 0.2 in square only, provides a capacitance of $0.001 \mu \mathrm{~F}$ at 120 V d.c. working.
Some interesting miniature trimmers for television and v.h.f. applications have appeared this year. Cyldon has a chassis-mounting model with ceramic insulation of 0.5 to 3 pF or 3 to 9 pF , Wingrove \& Rogers one of 0.5 to 3.5 pF with P.T.F.E. insulation and Mullard have a new version of their concentric air-dielectric trimmer with precision adjustment.
Makers*: Cyldon (T, V), Daly (E), Dubilicr (C, E, M, P, T), Erie (C, T), Hunt ( $\mathrm{E}, \mathrm{M}$, P ), Jackson ( $\mathrm{T}, \mathrm{V}$ ), Johnson. Matthe ( M ), London Electrical Mitg. (C. M), Mullard (T, V), Plessey (C, E
 M, P. T). T.M.C. (F, M. P) Walter (T), Wego (M, P), Welwyn ( T ), Wingrove \& Rogers ( $\mathrm{T}, \mathrm{V}$ ).
*Abbreviations: $\quad C=$ ceramic,$\quad E=$ electrolytic $\quad F=$ plastic film. $\mathrm{M}=$ mica, $\mathrm{P}=$ paper, $\mathrm{T}=$ trimmers, $\mathrm{V}=$ variable.

## Resistors

To produce a standard resistance of 0.0001 ohm is in itself no mean achicvement, but to guarantec its accuracy to 0.03 per cent demands such skill that few can emulate. Yet standards of this value, increasing in decade steps to 1,000 ohms, are now included in the Sullivan range of standard components. Salford have a new range of precision wirewound poientiometers intended primarily for use in desyn systems. They have tapped windings, single and double elements, twin wipers and provision for $360-\mathrm{deg}$ rotation.

Miniaturization is extending into unusual fields; for example, Painton has introduced a range of miniature faders and attenuators of the type generally used in control consoles. Some are of the edgewise pattern and occupy very little space.
A glimpse into future development was vouchsafed by some unusual fixed resistors shown by the Ministry of Supply. In one case a form of conducting glass is applied to glass plates and rods and then fired to fuse the whole together. In another, microscopic films of one of the precious metals is applied to glass plates and glass fibres. The former is etched to produce long paths and various values of resistance, while the fibres are wound on rods to provide a high resistance in a compact form. High stability is the aim in these designs.
Makers*: Doran (S), Dubilier (C, Hs, W), Egen (C), Erg (Hs, W), Electrothermal (Hs), Electronic Components (C, W), Erie (C, Hs, W), Morganite (C), N.S.F. (C. W), Painton (Hs, W), Plessey (C. W), Pye (W), Salford (W), Sullivan (S), Welwyn (C, Hs, W), Whiteley (C).
*Abbreviaitions:
W $=$ wirewound.
$\mathrm{C}=$ carbon, $\mathrm{Hs}=$ high stability, $\mathrm{S}=$ standards,

## Transformers

The extension of the resin "potting" technique, as used for certain sub-miniature radio assemblies, to the

construction of mains transformers may prove an important advance in the design of this class of component. It results in a considerable saving in size and weight of the article and also in the materials used for clamping the core and generally providing either an attractive or functional finish according to the use to which the component is put.

The potting resin not only provides a seamless protective case, but before setting it penetrates all parts of the core and windings and gives internal as well as external sealing. Transformers and chokes constructed in this way are extremely robust and will withstand a considerable amount of rough handling.

Examples of the potting technique as applied to these components are the Jupiter range made by Parmeko and the Pentland series introduced recently by Ferranti.

To the Variac range of variable voltage transformers made by Zenith Electric has bcen added some new models in open and enclosed types fitted with twin brushes and providing two independently controlled output voltages.
Makers: Advance, Bulgin, Electro Acoustic. Ferranti, Goodmans Gresham, Igranic, Parmeko, Partridge, Plessey, Rola-Celestion,
T.M.C., Weymouth, Whiteley, Woden, Wearite, Zenith

## Aerials

A few minor improvements and one or two new indoor television aerials scem to comprise this year's contribution to broadcast aerial design.
Belling and Lee have modified the reflector (and director) fitting of their television aerials to simplify assembly and also impart greater strength. A clamping device is used which by means of a single screw simultancously locks the elements and secures the firting to the cross-arm.
A square-section cross-arm is Wolsey's contribution to the general betterment of aerials. It is claimed to secure the elements more positively, prevent displacement by high wind and also enables the aerial to be part assembled in the factory, thus simplifying the erection on the site.

Antiference have a new indoor television aerial called a "Loftex" for either vertical or horizontal mounting and based on the Antex (X-type) principle. This firm has introduced also a new type of car aerial with a swivelling split-ball base for scuttle mounting at any desired angle of slope. It is telescopic, extends to 62 in and closes to 24 in .

Aerial lenses for the $9-\mathrm{mm}$ wavelength in metal and in plastic were used for an interesting demonstration staged by Marconi's to illustrate some of the characteristics of this type. They varied in size from 6 in to 4 ft in diameter. These lenses are now finding certain applications in relay systems.
Makers ${ }^{\star}$ : Antiference ( $\mathrm{B}, \mathrm{C}, \mathrm{T}$ ), B.I. Callender's (B, C), BellingLee (B, C, T), Heniey's (C), Marconi's (S), Reliance Wire (C), Suflex (C), Telcon (C), Transradio (C), Wolsey (C, T).
*Abbreviations: $\mathrm{B}=$ sound broadcast, including anti-interference. $\mathrm{C}=$ cables and feeders, $\mathrm{S}=$ special types, $\mathrm{T}=$ television.

## Sub-assemblies

The printed circuit technique is used by Eire in a range of compact resistance-capacitance units covering such requirements as diode filters, triode and pentode RC couplings and various other combinations.

A considerable saving in assembly time can be effected by the use of these units. In one particular case six joints replace some 16 or so if separate components are used.

Interference suppressors form another convenient subassembly and as produced by Dubilier they comprise capacitors and chokes of one kind or another. A special range of television suppressors is now available for use on or in small domestic appliances such as electric sewing machine motors and hair dryers.

## Chassis Fittings

Careful insulation is the main feature of the latest valveholder from McMurdo. Intended for B9A e.h.t. rectifiers, it has a Nylon-loaded Bakelite socket moulded


Some modern miniature trimmers; (b) Mullard air-dielectric with precision adjustment, (c) Cyldon television model, (d) Wingrove \& Rogers with P.T.F.E., insulation compared in size with a Hunt's " Micromold " (a) measuring $\frac{1}{2}$-in long.


Left: Belling-Lee double-screened coaxial plug and socket.


Below: Dubilier television interference suppressors and some of the special chokes now available.



Left: Tannoy 100watt loudspeaker for airfields, harbours, etc.

Right: roldring No. 200 magnetic pickup.


Left: Front and back plates of Acos Mic. 32 microphone capsule.

Right: Collaro "Studio" crystal pickup.

Below: Plessey 15 -irich mavirgcoil loudspeaker.


## Sound Reproduction

An interesting new p.a. loudspeaker has been developed by Tannoy for arrields, haroours, etc. The single driver unit is rated to handle 10 watts ( 120 watts peak) and is used in conjunction with a $200-\mathrm{c} / \mathrm{s}$ cut-off horn to give an electro-acoustic conversion efficiency of 50 per cent. The pressure unit is waterprooi and incorporates a switched transformer for coupling to line impedances of $50,100,200$ or 330 ohms; the coil impedance is 8 ohms.

Plessey have developed a convintionai cone loudspeaker with a power-handling capacity of 25 watts. It is 15 inches in nominal diameter and has applications both as a p.a. unit and as a bass unit in high-quality loudspeaker combinations. Elliptical-type loudspeakers have now been added to the range of "Elac" units made by ElectroAcoustic Industries.

In the new " 53 " series of Collaro gramophone motors and record changers a new speed-change mechanism with a large-diameter, concentric-ground rubber idler has been designed with ar cam mechanism to minimize wear when changing speed. A new crystal turnover pickup head, the "Studio," has been added to the existing Collaro range and incorporates a simple screw fixing for the replaceable cant:lever stylus arms.

A turnover pickup working on the moving-iron magnetic princ.ple, giving an output of 0.5 V at $3.16 \mathrm{~cm} / \mathrm{sec}$ lateral veloity has been marketed by Erwin Scharf (Goldring No. 200) The armature is coupled to the stylus by a rubber block in which the cantilever arm is a push fit.

Garrard are now in production with a new transcription-

type 3 -speed turntable (Model 301) in which speed fluctuations are less than 0.2 per cent.
A new crystal microphone of interesting design, the Acos (Cosmocord) Model 32, is of the diaphragm-driven type, and has a flat response up to $6,000 \mathrm{c} / \mathrm{s}$. Cavity resonance is controlled by a specially shaped back plate which reduces volume and compliance of the enclosed air, while the front plate carries a buttressed lug which performs the dual function of providing rigidity and improving the polar response of the microphone.
Makers (Components)*: Birmingham Sound Reproducers (GM, GU, RC, PU); Collaro (GM, GU, RC, PU); Cosmocord (E, M PU); Ediswan (RC); Electro Acoustic Industries (LS); Garrard (GM, GU, RC, PU); Goodmans (LS, M); Plessey (GM, GU RC, LS, PU); Reslosound (LS, M); Rola-Celestion (D, LS); Goldring (PU); Tannoy (LS, M); Truvox (LS); Vitavox (LS, M); Whiteley (LS, M).

* Abbreviations: D, diaphragms; E. earphones; GM, gramophone motors; GU, gramophone units; RC, record changers; LS, loudmpeakers; $M$, microphones; $P U$, pickups.


## Valves and Cathode Ray Tubes

Sub-miniature valves with indirectly-heated cathodes are quite a new thing in this country. Osram have produced two pentodes, a triode, a beam tetrode and a rectifier of this type, while Mullard have a triode which can be used at frequencies up to $500 \mathrm{Mc} / \mathrm{s}$. In directly-heated sub-miniatures, Mullard are contributing two new hearing-aid pentodes, the DF64 and DL64, designed for $15-\mathrm{V}$ h.t. batteries and with the very low filament consumption of 10 mA . Also very economical


Four-gun oscilloscope c.r. tube made by 20th Century Electronics.
to run are their new miniature valves for portable battery sets-the filament consumption being only 25 mA . Another new miniature battery valve is the Brimar 1AC6 heptode frequency changer, which has an h.t. consumption of only 0.7 mA and will operate up to $30 \mathrm{Mc} / \mathrm{s}$. Brimar have also produced an c.h.t. rectifier, the R19, which has the high peak inverse voltage of 25 kV , and is enclosed in a lead-glass bulb to prevent radiation of x-rays.

Production of reliable valves is continuing and this year a new range is available from Osram. The valves are mechanically-improved versions of existing Osram types and are known as the " $Q$ " series. Brimar have extended their range of "Trustworthy" reliable valves with equivalents of the 6AM5, 6C4 and R18.

Two transistors of the point type are now available on the British market. These are the Osram GET1 and the S.T.C. LS737, both of which can be used to give a gain of about 20db. New germanium diodes are being made by S.T.C. and Mullard.

In cathode ray tubes much interest has been aroused by an oscilloscope tube containing four separate guns, made by 20 th Century Electronics. It operates at 5 kV on the final anode and the deflection sensitivity is just under $\frac{1}{2} \mathrm{~mm}$ per volt. Each gun has independent deflecting plates and the makers claim there is no interaction between them.

Another tube with more electrodes than usual is the Mullard 17-in rectangular television tube MW43-64. This is basically a tetrode, but has an extra electrode between the accelerator and the final anode for improving the uniformity of focus over the whole screen. Like the new Ediswan 15-in tetrode CRM153, this tube has a tinted glass face. Two more tetrodes are being made by Brimar, a 14 -in rectangular tube C 14 FM and a 17 -in rectangular tube C17FM.

Remarkable for its extremely small size is the Ferranti KD10 voltage stabilizer, which stabilizes at 62 volts $\pm 0.15$ volts with a running current of $1-1.2 \mathrm{~mA}$. It is made in a metal capsule measuring only $\frac{7}{8} \mathrm{in} \times \frac{3}{16}$ in $\times \frac{1}{4} \mathrm{in}$. Miniaturization is also the main feature of the new Westinghouse tubular e.h.t. rectifiers, Type 39. They are $\frac{3}{6}$ in in diameter, and with the selenium elements working at the high P.I.V. of 85 volts they are only 0.6 in long per 1,000 volts. The current rating is $100 \mu \mathrm{~A}$ and the upper frequency limit $50 \mathrm{kc} / \mathrm{s}$.

## ELECTRONIC APPARATUS

The definition of "electronics" concerned with the extension of man's senses was well illustrated this year by three interesting ads to visual observation. One, produced by Philips, is an instrument for intensifying x-ray images so that the radiologist can see them immediately. It works on the image converter principle. The x-ray image is formed on a fluorescent screen and this is in contact with a photo-cathode, which emits a corresponding pattern of electrons. The electrons are accelerated by an electrode carrying a high positive potential and focused on to a second fluorescent screen very much smaller than the first. As a result of this acceleration and reduction


Philips instrument for intensifying $x$-ray images.


Mullard image converter equipment for high-speed photography.
in size the final image (which is viewed through an eyepiece) is about 1,000 times brighter than the original one.

The second instrument, made by Mullard, uses an image converter tube as an electronic shutter for highspeed photography-the point being that the electron beam in the tube can be interrupted electronically much faster than a light beam can be by a mechanical shutter. In this way exposures can be made as short as $1 / 20$ th of a microsecond! The exposure is actually made by applying a positive pulse to a control electrode in the tube, which normally has a negative bias to cut off the electron beam. This produces a brief image on the fluorescent screen which is recorded photographically. Deflector coils enable the instrument to make a line of successive images across the screen so that a cinematographic effect can be obtained.

The third electronic aid to obscrvation is a flying-spot microscope, produced by Cinema-Television. This uses a conventional flying-spot scanning system in conjunction with an optical microscope. The main feature of the instrument is that the image can be displayed on a number of c.r.t. monitors (magnified about 2,000 times) for demonstration purposes. Apart from this, the ability to alter contrast avoids the necessity for staining specimens, while the use of ultra-violet light for scanning gives greater resolving power than is possible with an ordinary microscope (because of the shorter wavelength).

Probably the most original instrument that has appeared recently is the electronic anemometer made by Isotope Developments. It measures wind velocities as low as loft per minute. Basically a radiation detector, it uses a wire-cage ionization chamber in which is fixed a small piece of radioactive material. The wind simply blows away the ions which are formed in the chamber and the effect is registered on a meter in the detector.

The servo or negative feedback principle is to be seen in a good many electronic instruments nowadays. In several d.c. amplifiers of the mirror-galvanometer type, for example, a portion of the output is fed back to stabilize the action of the galvo. Then in two a.c. voltage regulators a change in input voltage is amplified and applied to a motor, which drives a variable transformer to correct the change. A new pen recorder works on a similar principle with
the fluctuations of the d.c. input, the movements of the "correcting" motor being used to drive the pen.

## Industrial Electronics

Applications of electronic techniques in industry depend primarily oil the measurement of physical constants and the subsequent derivation of signals for automatic control. Sometimes one parameter is obtained in terms of another as in radioactive thickness gauges where the fundamental quantity indicated is mass per unit area of sheet material. In the Baldwin rolling mill exterision gauge, thickness is derived in terms of change in length (velocity) of steel strip as it passes through the mill, and the method of measurement is novel. Magnetic recording heads print an alternating pattern of magnetization on the strip before and after rolling, the tracks being offset to avoid interference. Pick-up heads follow the recording heads and their outputs are combined in a differential phase-indicating meter. If the distance between heads before and after the rolls is equal, and if there is no reduction in thickness, the meter reads zero-fluctuations in roll speed are eliminated by driving the recording generator from one of the roll spindles. When there is a reduction in thirkness a corresponding increase in wavelength takes place after rolling, and to bring the meter back to zero the "pre-rolling" recording head can be moved relative to its pick-up by a micrometer, which can be calibrated in percentage reduction of thickness. The instrument will detect reductions of less than 0.1 per cent and can be applied to the production of thin steel strip running at speeds of the order of $1,000 \mathrm{ft} / \mathrm{sec}$.
B.T.H. have applied a high-speed multiple preselecting batch counter to the measurement of length, and have used it for cutting veneer wood to predetermined lengths. A perforated wheel is driven by the wood strip and interrupts a photo-cell light beam at intervals equivalent to $1 / 10$ th inch. Four Dekatron counters in cascade record the passage of the strip, and when the glow reaches the predetermined cathodes in all four tubes, the strip is stopped, cut and the counter reset. Up to ten different lengths can be selected by push-button and this enables the operator to avoid blemishes economically. In practice the measuring speed is limited to $12 \mathrm{in} / \mathrm{sec}$, though the counting speed would permit $200 \mathrm{in} / \mathrm{sec}$.


Top left: Electronic anemometer by lsotope Developments. Above: Baldwin "Quantex" light quantity meter. Left : Pye direct-reading (counter) pH meter.

Liquid level meters depending on electronic methods are widely uscd, and in one recent model introduced by Fielden, a self-balancing capacitance bridge technique is used which provides positive indication and control to less than 1 per cent. The principle of the Fielden "Servograph" recorder has been applied by Stanton Instruments to the continuous measurement of weight in a "thermobalance" designed to record the change of weight with time in specimens heated in a small furnace to temperatures up to 1,000 deg. C.

The metering of light quantity is of importance in many photographic and printing processes, and the Baldwin "Quantex" light quantity meter is based on the charging of a capacitor by a current derived from a photoelectric cell. Preset relays give exposures in two ranges covering 1 sec to 1 hour

Process timers are widely used and depend usually on the time-constant of an RC circuit. As a demonstration, Allicd Electronics show equipment designed to life-test an electronic d.c. voltage stabilizer through a regime of varying load and supply voltage.

Two watch timers are available from Furzehill Laboratories. Type 774 V gives a bright spot on a circular c.r.t. trace. The time-base frequency can be varied over a small range to bring the spot to a stationary point, when the error can be read off a calibrated dial. An alternative display expands the watch pulse and provides useful information for the diagnosis of irregularities. In the Type 774E each watch beat is recorded on a strip of paper which records short-term irregularities as well as the average rate. Both instruments make provision for the testing of watches with all standard gear trains giving beats of $3 \frac{2}{2}$ to 6 per sec .

Developments in strain gauge technique include the production by Saunders Roe of foil elements by a process evolved by Technograph Printed Circuits, Ltd. Considerable simplification of the associated equipment results from the increased current-carrying capacity of these elements. Pressure gauges employing strain gauges are made by Langham Thompson for use in pipe lines and the technique is applied by C. N. Smyth to hypodermic needles for use in medical research.

Ultrasonic flaw detection is now well established and developments are mainly in detail. The latest equipment made by Glass Developments, Ltd., includes barium titanate probes, steerable beam over angles from 90 to 55 deg to the surface, miniature probes for small specimens and a single probe transmitting-receiving technique. C. N. Smyth has introduced an inexpensive flaw detector, with separate or combined transmitting and receiving probes, which can be used as an accessory 10 a Cossor oscilloscope.

The machining of brittle matcrials by an ultrasonic technique has been developed by Mullard. A magnetostriction transducer operating at $22 \mathrm{kc} / \mathrm{s}$ is coupled by a tapered metal "velocity step-up transformer" to a cutting


Furzehill recording watch timer.
tip, which, when applied with suitable abrasive, rapidly penetrates glass and other difficult materials. As the motion is translatory rather than rotary, holes and depressions of other than circular shape are easily formed.
Measurement of pH (hydrogen ion concentration) is important in many industries and a correspondingly wide variety of instruments is available, as exemplified by the small battery-operated portable (Model 30) and the industrial, hermetically-sealed instrument (Model 28) made by Electronic Instruments, for which a wide range of electrode systems is available. The W. G. Pyc No. 11082 pH meter gives direct readings on a 4 -figure counter with an accuracy of 0.01 pH . A self-balancing potentiometer is driven by a servo motor which is also coupled to the counter. Automatic zero correction is carried out continuously while the instrument is idle, so that it is always available for immediate use.

In the "Humicon" humidity detector Standard Telephones make use of glass silk between two perforated plates as a moisture-sensitive impedance. The voltage drop across this is used to control a series of thyratrons which operate appropriate ventilation or heating devices in, for example, a G.C.A. radar mobile van.

The measurement of moisture in coal dust presents difficulties due to variable conductivity from impurities, and the National Coal Board have found that these effects can be climinated by measuring the effective dielectric constant at $30 \mathrm{Mc} / \mathrm{s}$ for which purpose a Fielden "Drimeter" has been adapted.

Dawe Instruments have developed a comprehensive warning systerr. for inflammable gases in the ventilating systems of oil tankers. The principle involved is the rise in temperature and resistance of a catalytic platinum filament. A motor-driven commutator sampies all the detectors in sequence and an alarm signal is given on the bridge indicator board by concentrations well below the explosive limit.

## TEST AND MEASURING INSTRUMENTS

Under this heading are included instruments intended for laboratory use, for production testing, and for servicing. It is not possible to review any but new or substantially improved models, nor the numerous industrial instruments (many employing electronic techniques) such as material testers, that might conceivably be employed in the radio industry.

The first impression on surveying the instruments exhibited this year might have been one of disappointment at not finding outstanding new types or techniques. Closer examination; would have shown, however, that behind many of the apparently similar front pancls a vast amount of real progress has been made. Anyone experienced in the use of instruments knows that small refinements may add up to a more significant total than some striking departure from previous practice.

Even the old-established moving-coil meter has not reached the limit of improvement, and this year there seems to be more evidence of this than usual. To obtain a high sensitivity and speed of response, Everett Edgcumbe use four high-flux magnets in the magnetic circuit, which is shaped so as to allow a 270 -degree scale instead of the usual 120 degrees. In the Metrovick meters an exceptionally robust result is achieved by skilful use of die castings and mouldings. Ballistic characteristics are especially important in signal level indicators, and the new Pullin VU meter, which is a rectifier m.c. voltmeter, claims to reach 99 per cent of steady value in about 0.3 sec , with an overswing not more than 1.5 per cent. Another specialized m.c. instrument is the Pye fluxmeter, full-scale reading 700,000 "line-turns" ( 7 milliweber-turns), in the well-known "Scalamp" for-
mat; provision is included for rapidly restoring the deflection to zero. A portable silicon-crystal millivoltmeter developed by A.I.D. for testing signal-generator output calibration might well find wider applications on account of its frequency range of $1-300 \mathrm{Mc} / \mathrm{s}$. An attenuator has been designed which extends its voltage range ( $0.05-0.15$ ).

Among valve-aided meters the most noticeable trend is the use of pre-detector wide-band amplification to increase sensitivity, as in those by Dawe and Furzehill. The ranges of the latter (Type V.200) are now $1 \mathrm{mV}-1 \mathrm{kV}$ full-scale, and the frequency coverage- $10 \mathrm{c} / \mathrm{s}-6 \mathrm{Mc} / \mathrm{s}$-is adequate for high-definition v.f. work. The Philips 6010 batterypowered millivoltmeter, for zero frequency, employs the modulation principle so as to amplify stably over twelve ranges, $0.1 \mathrm{mV}-300 \mathrm{~V}$, with input resistance $0.67-100 \mathrm{M} \Omega$; with the addition of a probe containing a germanium rectifier it can be used for measuring voltages from $5-1,000 \mathrm{mV}$ over the wide frequency range $2-800 \mathrm{Mc} / \mathrm{s}$. Very high input resistance is now becoming common in z.f. valve voltmeters; an instrument shown by B.T.-H. is exceptional in having an input current of only 0.1 micromicroamp at frequencies from zero to $100 \mathrm{kc} / \mathrm{s}$.

Measurement of very high voltages is a problem. The latest Ernest Turner electrostatic voltmeters up to 20 kV are protected against brush discharge by the use of fixed vanes of graphite-loaded Bakelite. At still higher voltages, safety is a major consideration. A capacitive potential divider by Hivolt uses a concentrated field around the periphery to protect the divider proper (arranged axially) from proximity effects; the indicator, connected by a long cable, can be read at an amply safe distance. Capacitive dividers are also made by B.T.-H. for examining high-voltage pulses on a c.r. oscilloscope.

The facilities of wide-band amplification are perhaps even more valuable when the indicator is an oscilloscope. In this application, width of frequency band is usually appreciated as


Field potential divider and remote indicator unit comprising $20-100 \mathrm{kV}$ voltmeter (Hivolt).

speed of response. Amplifiers are obtainable separately from Nagard and Cossor, working from z.f. or thereabouts upwards, but for examining high-speed transients there are obvious advantages in having the amplifier built into the oscilloscope. Several new models are well adapted for this type of work, notably the Nagard DG. 103 with double-beam tube, the Philips GM. 5660 with frequency band $15 \mathrm{c} / \mathrm{s}-10 \mathrm{Mc} / \mathrm{s}$ and pulse rise time $40 \mathrm{~m} \mu \mathrm{~s}$, and the Airmec $830(30 \mathrm{c} / \mathrm{s}-20 \mathrm{Mc} / \mathrm{s}$ and $25 \mathrm{~m} \mu \mathrm{~s}$ respectively). The notable sharpness and brightness of the trace on the screen of the last-named oscilloscope is maintained even at the extreme speed of 30 cm per $\mu \mathrm{sec}$. Philips also have a new oscilloscope which, although a general-purpose model, takes into account the importance of pulse technique in television. It is notable for including two identical amplifiers covering $0.3 \mathrm{c} / \mathrm{s}-$ $1 \mathrm{Mc} / \mathrm{s}$ and exceptional synchronization facilities. There are several other new general-purpose oscilloscopes. The Cossor 1052 also has two identical amplifiers and other improvements on the old 339, but does not include volt-age-calibrated shifts like the 1049; a separate voltage calibrator (1433) is obtainable however. The Furzehill 1684D/2 continues and extends the association of this marque with direct-coupled amplification, the frequency range now being $0-4 \mathrm{Mc} / \mathrm{s}$. The Industrial Electronics 2300, although a truly miniature $2 \frac{1}{2}$ in-tube instrument weighing only $6 \frac{1}{4}$ pounds, includes features usually obtainable only in types many times its size-push-pull amplification from zero to $100 \mathrm{kc} / \mathrm{s}$ on both X and Y plates, and automatic synchronization.

The Advance range of signal generators has been extended in the $15 \mathrm{c} / \mathrm{s}-50 \mathrm{kc} / \mathrm{s}$ band by Type J, which differs from the H. 1 in having a calibrated power output up to $l$ watt at a constant $600 \Omega$ impedance, rather than a voltage output. Two varieties are obtainable, with and without output meter. There is now a smaller version of the Dawe a.f. source. The previous Muirhead decade oscillator has been superseded by an improved model having remarkable frequency accuracy.

All of these employ RC tuning, which has displaced the beat method for a.f. purposes, but where a very wide frequency is required without switching the beat method still applies, as exemplified in the interesting Philips GM. $2889 \mathrm{a} . \mathrm{m} .-\mathrm{f} . \mathrm{m}$. oscillator, covering $5-225 \mathrm{Mc} / \mathrm{s}$ in one sweep. It is particularly suitable for measuring bandpass response of television and other receivers; f.m. at mains frequency can be obtained with deviation up to $10 \mathrm{Mc} / \mathrm{s}$ by means of a "loudspeaker" movement. For testing discriminator characteristics, $400 \mathrm{c} / \mathrm{s}$ f.m. is available up to $250 \mathrm{kc} / \mathrm{s}$ deviation. A separate $15-30 \mathrm{Mc} / \mathrm{s}$ oscillator is incorporated for introducing frequency marker "pips."

The Marconi Instruments TF948 signal generator covers $20-80 \mathrm{Mc} / \mathrm{s}$ in two ranges, the effective scale length being over 14 feet, and is provided with sine wave f.m. and sine and square wave a.m., internally at three audio frequencies. The specification is elaborate and includes crystal frequency checking and modulation depth and deviation measurement. Another new instrument from the same firm is the v.h.f. test set TF.982, comprising a signal generator for $60-184 \mathrm{Mc} / \mathrm{s}$ and four i.f. ranges, a crystal calibrator, a r.f. field detector, an a.f. output power meter, and a multi-range test meter. A range of frequency hitherto not at all well provided for- $300-1,000 \mathrm{Mc} / \mathrm{s}$-is covered by the Advance L. 1 signal generator in two ranges, using a 6F4 valve in a conventional series-tuned oscillator circuit. Output is controlled over a 130 db range by a piston waveguide attenuator, and modulation can be either sine or pulse.

Instruments for frequency measurement are not so prominent as they have been in times past, but there are three new Furzehill crystal frequency standards: one providing 150 watts at $50 \pm 10^{-5} \mathrm{c} / \mathrm{s}$, and two portable units for general frequency checking, of which Type G. 410 is provided with push-button control for selecting standard frequency signals at multiples of $0.1,1,10,100,1,000$ and $5,000 \mathrm{kc} / \mathrm{s}$. A vastly more elaborate equipment is the Plessey frequency synthesizer, which now appears with motor-driven operation by which any multiple of $1 \mathrm{kc} / \mathrm{s} u p$ to $100 \mathrm{Mc} / \mathrm{s}$ can be automatically selected. An unusual


## TRUSTWORTHY VALVES

Two years of rigorous testing have proved beyond doubt, that, under extreme conditions in the Services and Industry, Brimar Trustworthy types maintain a high standard of reliability and efficiency under conditions where ordinary production types fail. Here is an example :

In order to investigate the stresses of helicopter motor blades, a D.C. amplifier was installed in the motor head, transmitting signal levels to the control cabin below.

The excessive vibration rendered normal valves useless, and reduced the valve life to only a few minutes.
Substitution of Brimar "Trustworthy" type 6067 freed the D.C. Signals of all noise, and measurements were able to proceed.

In another case, an Aircraft Company required instrumentation to measure stresses on jet aircraft when approaching the speed of sound. This equipment consisted of sensitive amplifiers located in the aircraft. Normal valves were too noisy under these conditions to give reliable results, but modification, to employ Trustworthy valves, has since solved the problem. Further, the equipment has stood up for a considerable number of hours service under these arduous conditions.

These are but two of many examples which prove that extra-rugged, extra-reliable Trustworthy valves are so often the perfect solution to an otherwise insoluble problem.

## 3 TRUSTWORTHY types are immediately available for commercial use

| 6064 theTrustworthy <br> 6065 <br> 6058$\quad "$ |
| :--- |

# Tracking 2000 g at <br> 10 grammes maximum stylus pressure 


stylus radii are shown, the nominal .001 in . radius (Fig. 1) and its upper and lower limits of .0012 in . and .0008in. (Figs. 2 and 3 respectively) according to British Standard Specification. It can be seen that the .001 in. radius has .0004 in . wall above its point of contact, whilst the .0012 in . radius has no more than .0002 in . This does not take into account the pinch effect which can reduce the margin by .0002 in . at $5,000 \mathrm{c} / \mathrm{s}$.

## PRACTICAL CONSIDERATIONS

In order to arrive at maximum possible displacement, some assumptions have to be made that are dictated by practical considerations. Working on the basis of 200 grooves per inch the maximum possible displacement (d) is .003 in . At a frequency of $40 \mathrm{c} / \mathrm{s}$. this displacement corresponds approximately to a maximum velocity of $2 \mathrm{~cm} / \mathrm{sec}$. (v $=2 \pi \mathrm{fd}$ ). Accepting the recording characteristics of the Decca Long Playing test record No. LXT 2695 as typical for commercially produced long playing records, the maximum velocity and corresponding acceleration at $10,000 \mathrm{c} / \mathrm{s}$. can be calculated. According to the record specification the recording pre-emphasis at $10,000 \mathrm{c} / \mathrm{s}$. relative to $40 \mathrm{c} / \mathrm{s}$. is +24.4 dbs . and this gives a velocity of $31.6 \mathrm{~cm} / \mathrm{sec}$. and a corresponding displacement of .0002in. ( $\mathrm{e}=\frac{\mathrm{v}}{2 \pi \mathrm{f}}$ ). It further follows that expressed in gravitational units the acceleration at $10,000 \mathrm{c} / \mathrm{s}$. may be as high as $2000 \mathrm{~g}\left(\mathrm{~g}=\frac{\mathrm{ef}^{2}}{10}\right.$, where $\mathrm{e}=$ displacement $=.0002$ in. and $\mathrm{f}=10,000 \mathrm{c} / \mathrm{s}$.).
Fig. 3

## WHAT OF THE FUTURE?

The examination, as can be seen even from this simplified statement, has brought to light conditions that appear to be incredible at first sight. They are, however, far from being purely hypothetical and it may be only a question of time before they appear on commercially produced records. Even now there are a few odd records on the market which come very close to these limiting conditions.

It can be seen that the problem set by the record manufacturers in this matter was a formidable one. Cosmocord have answered it so completely with their Acos "Hi-g" series of pick-up cartridges that they already meet, here and now, any likely future development of gramophone records within the B.S. 1928 : 1953 specification.
 .0003in. maximum it has no effect. Three pick-up playing time per 12 a record giving up to 30 minutes accompanying scale drawings. For simplicity's sake, the groove angle has been shown as $90^{\circ}$ and the radius at the bottom of the groove has been left out, as at Acos Crustal Devices are Protected by Patents and Patent Apphications in Git. Britain and Other Countries.
form of absorption frequency meter (TF. 1026 series), illustrating an entirely different conception of frequency measurement, has been introduced by Marconi Instruments; each has a $2: 1$ frequency ratio, the whole series of five covering $125-4,000 \mathrm{Mc} / \mathrm{s}$. The resonant system comprises a coaxial line closed at one end and tuned at the other by a variable capacitance.

Nearly all new a.c. bridge designs, for all frequencies from power to v.h.f., are based on the use of transformer ratio arms for input or output or both. One of the chief advantages is that an admittance connected across part of a low-leakage transformer winding does not appreciably alter the ratio, as it would if connected across one of a pair of resistance ratio arms. As a result, the values of components can be measured in situ, notwithstanding that relatively low admittances exist between both terminals and earth. An example is the grid-to-anode capacivance of a screened valve, which is small absolutely and also relatively to the capacitances to cathode, etc. Wayne Kerr have for some time been exponents of this technique for high r.f., and now have several experimental models for a.f. In one, capacitances can be measured from $12,000 \mathrm{pF}$ down to 0.0001 pF , at $10 \mathrm{kc} / \mathrm{s}$. A $1-\mathrm{Mc} / \mathrm{s}$ transforme $i$ bridge devoted more particularly to interelectrode capacitances and conductances and therefore less wide in range has been produced by Electronic Tubes. It is worth noting that in both these bridges, as well as in other high-performance modern equipment, the humble "magic eye" is adequate as the indicator. In another experimental Wayne Kerr bridge the Maxwell form is brought up to date with a transformer output, $10 \mathrm{kc} / \mathrm{s}$ source. and "magic eye," to such good effect that self and mutual inductance are measurable in ranges as low as $0.01 \mu \mathrm{H}$ full-scale. But perhaps the most interesting of the series is a $1-\mathrm{kc} / \mathrm{s}$ bridge for four-terminal network measurements, in which full use is made of transformer arms is cover all four quadrants of the complex plane.

If one terminal of a bridge arm is joined to its screen, as in most of these obtainable separately, its use is thereby
limited. For adaptability is is necessary to have two screens, the outer earthed and the inner joined to the arm; decade resistance boxes so arranged are produced by the Croydon Precision Instrument Company.

Apparatus for displaying valve characteristics on a c.r. tube screen now appears in a form adapted for germanium valves (transistors), by Marconi's W.T. Co. The development of equipment for testing the mechanical properties of valves has been stimulated by the requirement for valves to stand severe conditions, such as being shot from guns. The usual technique is to vibrate the valves by a modified loudspeaker drive and to examine them mechanically and electrically. In the set-up by Electronic Tubes the movements of the electrodes can be seen stroboscopically, and their resonance spectrum recorded photographically from electrical responses. The observing instrument in the Industrial Electronics vibrator equipment is the c.r. panoramic wave analyzer by the same firm.
Measuring apparatus for frequencies over $2,000 \mathrm{Mc} / \mathrm{s}$ centres on the waveguide "test bench" assembled from a wide variety of waveguide sections and components. Most of the work is based on observance of standing-wave ratio and node positions, and some recent devices have the object of facilitating this. In the Decca automatic s.w.r. indicator four crystal detectors mounted in the waveguide and spaced at eighth-wave intervals are connected to a c.r. unit which provides a display in Smith chart form from which the frequency variation of a match can be seen at once. A cylindrical chart enabling displacements measured at one frequency to be seen by inspection for any other frequency in the waveband has been devised by the Admiralty. Among the precision microwave instruments offered by Elliott Bros. is a torque vane wattmeter for absolute measurements of power in the X band. The vane is suspended by a fine quartz fibre at 45 degrees in the waveguide, and the power passing along the guide is measured in terms of the mechanical torque exerted on the vanc. This can hardly fail to remind one of the Raleigh disc absolute method of measuring sound intensity


Above: Torque vone wattmeter. for absolute meosurements of power in the $X(3-\mathrm{cm})$ band (Elliott Bros.).

Above, right: U.h.f. (300-1,000 $\mathrm{Mc} / \mathrm{s}$ ) stondard signal generator, Type L. 1 (Advance Components).

Right: Microwave test bench, fitted with spaced detectors for automatic Smith chart display on the indicator seen on the right (Decca Radar).


5-Applications in Trigger Circuits

EAARLIER articles in this series have dealt rather generally with the nature of the two common forms of transistor and with some of the more elementary linear circuit properties. Following the plan of the series, which is to hop from topic to topic in an effort to cover an enormous field sometime in the foreseable future, we must now look at the applications of transistors to trigger or switching circuits. Here the future is wide open and, from some points of view, rather depressing. As an example of a transistor application here, I have two blocking oscillator circuits performing equivalent functions, one using a valve, power consumption 1 watt, and a transformer, as well as the few resistors and capacitors; the other uses a transistor, three resistors and one capacitor, and consumes only 50 mW . Apart from the difference in bulk and power consumption, the smaller unit should operate in the particular application for ever, while the valve must have its heater operating continuously, so we can expect to change valves at least once a year.
I say this is rather depressing, because it makes the fully automatic factory a much more immediate prospect. As Norbert Wiener has pointed out, we shall then have a community supported by slaves, a state of affairs which can be studied better in Gibbon than


Fig. 1. Characteristics of the two main types of negative resistance.

Fig. 2. N-type negative resistance with load lines. Intersections like B are unstable.

in the works of the economists. This may happen quite quickly, and our only hope is to make sure that the first computing machine can be solving the economic problems faster than the industrial machines are creating them. I do not think we shall get much guidance from either the Georgics or from "Das Kapital." But make no mistake, within 10 years or so we shall see the development of two economies, transistorized and non-transistorized, and if we are to belong to the second class we might as well start planting cabbages now.

The trigger circuit is the key item of any digital device. It produces pulses, re-shapes pulses, accepts them, rejects them. In most existing computer systems a twin-triode circuit has been used, but now the single or double transistor circuits are sweeping the board. Let us consider the general properties of these trigger circuits.
The equations given earlier in parts 2 and 3 of this series showed that the impedances presented at the input or output terminals of a transistor-resistor circuit could be negative, provided that the current gain, $\alpha$, of the transistor was greater than unity. At the present time we can take this to mean that a point transistor must be used. This negative resistance is the first requirement for obtaining the type of



Fig. 3. Collector large-signal negative-resistance characteristic.


Left : Fig. 4. Idealized emitter large-signal negative-resistance characteristic. Right: Fig. 5. Bistable transistor circuit.
non-linear operation which is nowadays called a "switching function." A general investigation of these " switching functions" leads to the view that the most rational method of analysis is obtained by splitting the action into three regions: on, off, and transition. The classic example of such a system is the famous Duke of York, who had 10,000 men (when they were up, they were up . . .). All the important switching functions used in engineering contain some sort of energy storage which drives the circuit through the transition region. A very simple example is the ordinary press type of electric light switch. As you press the button you store energy in a spring until a triggering threshold is reached, when the spring drives the mechanism from one position to the other.

There are two types of negative-resistance characteristic, and it is necessary to be clear which type we are using in any particular circuit. The reason why there are two types is only understood when the full impedance diagram is plotted, because it depends on the way the impedance behaves at the extremes of high and low frequency. This is a topic for an article in itself. Here we can content ourselves with the voltage-current diagrams of what are called, for obvious reasons, the N and S types of negative resistance. Fig. 1 shows the simplified forms of these diagrams. The N type of negative resistance is stable when open-circuited, but is not stable when shortcircuited: the $S$ type is short-circuit stable, but unstable when open-circuited. A rough picture of the difference between the two is obtained by considering some conventional oscillator circuits, in which the tuned circuit may be either resonant, if the negative resistance is short-circuit unstable, or anti-resonant, if the negative resistance is open-circuit unstable.

Let us consider what happens if we have an N-type negative resistance and we connect a positive load resistance R to the terminals. Since the N characteristic is the characteristic of an active network we must put a bias battery in the circuit, too. The load line can then be moved parallel to itself, and three possible positions are shown in Fig. 2. The middle position, marked $\mathrm{R}_{\mathrm{L}}$ is the most interesting. It intersects the N at three
points, of which $A$ and $C$ correspond simply to two positive resistances in series and are thus stable. At B we have a loop consisting of a negative resistance in series with a numerically smaller positive resistance. This is unstable, and if the system is moved to $B$ by some means it will snap (as fast as the reactances in the circuit will allow) to either A or C.

Now suppose that the system is stable at $A$ and we alter the bias to move the load line up to $\mathbf{R}_{\mathrm{L} 1}$. The only stable point is $E$, and the current through the loop jumps smartly from $I_{D 1}$ to $I_{\mathrm{E}}$. Now we change the bias in the opposite direction, to bring the load line down to $\mathrm{R}_{\mathrm{L} 2}$. The current falls slightly to $\mathrm{I}_{\mathrm{E}}^{\prime}$ and then as the load line leaves the right-hand corner the current drops to $I_{D}$ as the only stable point becomes $D$. This sort of snap action will be familiar to anyone who has ever used the Schmitt double-triode trigger circuit.

It does not require much imagination to see that a load line can be imposed on the S-type characteristic in Fig. 1 to give three-point intersection. All the discussion in the last paragraph can be rewritten with the word current replacing voltage and viceversa and it will then apply to the S-type characteristic. These two characteristics are, in fact, duals. The subject of duality has been explored by " Cathode Ray," and will be discussed in detail later.

## Switching Circuits

Now, perhaps, we can turn our attention to transistor circuits. In Fig. 3 and 4, we have two very simple test circuits and the voltage-current characteristics obtained with them. In Fig. 3, the circuit is held under control by using a large value of $\mathbf{R}_{c}$ so that the tests can be carried out even in the negative resistance region II. The same stabilizing function for the emitter characteristic of Fig. 4 is performed by $\mathrm{R}_{c}$. Both these curves belong to the N-type, although region III has got flattened out a bit : but regions I and III are positive resistance regions, linked by the negative resistance region II.

Fig. 5 shows the simple transistor bistable circuit.




Fig. 6. Monostable and astable characteristics resulting from the addition of capacitor $C$.


Fig. 7. Basic circuit values and calculated (dotted) and measured emitter negative resistance characteristics, for a Type 1698 point transistor.

If you compare the characteristic with that of Fig. 2, you will see that there are two stable positions, and the system can be triggered from one to the other by applying a pulse of the right polarity at the " trigger" input. This circuit is equivalent in properties to the resistance-coupled multivibrator using two triodes.

Having this idea of the multivibrator in our heads, let us see how we can introduce capacitors into the transistor circuit to convert it to either an oscillator or a "single-shot" "multivibrator. A single capacitor has been introduced in the circuit shown at the top of Fig. 6. The extra resistance $R_{c}$ is fairly small, and is introduced to provide a convenient way of getting a low impedance output from the circuit. In the case shown in Fig. 6(b), the controlling resistance $\mathrm{R}_{e}$ is low enough for the three-point intersection to be possible. The value of $\mathrm{V}_{e e}$ is such that the circuit is normally stable at $a$. Suppose now we put in a trigger voltage $\Delta$. The load line is lifted up to the apex of the $N$-curve, and can then " see" the single stable point $b$. As soon as the system starts to re-set itself to $b$, however, the capacitor $C$ presents a short-circuit to the emitter, and the operating point jumps along the line 1 to a high emitter current. When the intersection with the N -curve is reached, however, $\mathrm{R}_{e}$ takes control again, and the capacitor starts to discharge along the path 2 . By this time, however, the trigger pulse has ended, and when the discharge brings the emitter voltage to the trough, the working point jumps along the shortcircuit line 3 to meet region I again. Finally, the emitter voltage runs up along 4 to the point $a$, where the system waits for a new trigger.

With a higher value of $\mathbf{R}_{e}$ and positive bias applied to the emitter we have the conditions shown in Fig. 6(c). This arrangement is astable, as the only intersection is in region II. The circuit oscillates steadily round the path $1,2,3,4$.

## Pulse Length and Spacing

Practical values for a circuit of this kind are shown in Fig. 7 for a 1698 point transistor. With the values given in the inset diagram and an emitter load resistance of 15,600 ohms returned to the earth line, frequencies of $2,000-10,000$ pulses/second and pulse lengths of $20-2,000$ microseconds can be obtained with capacitors in the region $0.01-0.5 \mu \mathrm{~F}$. Both experimentally and theoretically it can be shown that pulse length and spacing are proportional to capacitance. Experimentally I have found that pulse repetition rate is fairly linear with emitter bias. The characteristic in Fig. 7 is not extended far enough to enable the peak emitter current to be determined, but a rough estimate is about 12 mA . The pulse available at the collector will be about 40 volts. When very short pulses at repetition rates of the order of 1,000 pulses/second are needed, the most satisfactory arrangement seems to be to use an emitter load resistance of the order of one megohm, and a correspondingly smaller capacitance. The 40 -volt output pulse can then be obtained with collector current of about $1-2 \mathrm{~mA}$, but for reliable operation a positive bias voltage on the emitter is needed to lift the intersection clear of the corner.

More elaborate circuits of this basic kind for bistable operation incorporate diodes in the base or emitter circuit. I hope we shall be able to consider these in more detail later, but for the moment we may note that one form of this arrangement converts the $\mathrm{R}_{e}$ line into a " dog leg," and provides a more certain three-point intersection condition.

A very similar discussion will apply to the arrangements shown in Fig. 8. The N-type collector characteristic enables us to arrange for bistable, monostable or astable working. There is nothing of special interest here, unless it is the danger of excessive currents with the low emitter impedance.

The base connection is rather more interesting. The voltage-current plot shown in Fig. 9(a) on the following page is of the $S$-type and it can be scen that one condition for the three-point intersection load line is that the external base load resistance must be numerically larger than the negative input impedance. By inserting inductance in the base lead we get the instantaneous open-circuit effect, corresponding to the capacitance short-circuit, needed to give the snap action in monostable and astable action. The circuits and conditions are shown in Figs. 9(b) and 9(c), and in any practical circuit a resistance in the collector lead would be added to provide an output. The main disadvantage, of course, is the rather limited range of time constants available using inductances.

This treatment is obviously of great value in considering sinusoidal oscillators. If the capacitor in the emitter or collector astable circuit is replaced by a resonant circuit, the system will act as a sinusoidal generator, limited by overloading. Similarly, the inductance in the base circuit can be replaced by an anti-resonant circuit. The design problem is quite easy now. Looking at Fig .7 we see that the emitter circuit resistance can be just over 9,000 ohms and the emitter bias -10 volts to give a barely astable condition with the other values as shown. The net negative resistance is then very small, so that oscillations will be limited without much overloading.

Refinements of the simple emitter circuit, the most commonly used form, are directed towards improving the pulse shape. With the simple capacitor circuit the collector current pulse has a drooping top caused by the run down path 2 (see Fig. 6). The capacitor can be replaced by an open-circuited delay network, of the ordinary pulse-forming type. This has two results: the pulse top becomes flat, and the pulse duration no longer depends on the time constant ( $\mathrm{C} \times$ emitter resistance), but is fixed by the line. Different samples of transistor give identical pulses. The second refinement is to use diodes in the monostable circuit, so that it takes the form shown in Fig. 10. This circuit is triggered by a negative pulse applied to the base. Once the trigger action starts, the diode CD2 cuts off the input terminal so that it has no further control over the action. As a
result, the output pulse is practically independent, both in width and amplitude, of the input trigger. The other diode, CD 1 , is provided to reduce the time constant of the capacitor discharge in section 4 of the path. This means that the circuit returns very quickly to its quiescent position after producing a pulse, and very high repetition rates are possible. This circuit is used in computers to reform the pulses after they have passed through the various gates. Obviously it could also be used as a repeater in a pulse code modulation system.

Another application of diodes is in stabilizing the position of the junction between regions I and II. In the characteristic shown in Fig. 7 this junction is at 11.5 volts. The value can be calculated, and is approximately $\mathrm{V}_{c} \mathrm{R}_{b} /\left(\mathrm{R}_{b},+r_{c}\right)$, where $\mathrm{V}_{c}$ is the collector voltage, $\mathbf{R}_{b}$ the total base resistance and $r_{c}$ the collector resistance. The weak point is $r_{c}$, which varies with temperature. Typical figures suggest that the junction

may move about 5 per cent, or, say, 0.5 volts. For circuits adjusted to maximum sensitivity this is rather important, especially if the transistor moves into the bistable condition and locks on.

I do not propose to discuss the actual circuits used to prevent this until some later date. A word of warning is perhaps the best conclusion: in using these circuits, always make sure that they will fail safe and that if an oscillator or monostable circuit does lock on it will not allow a destructive current to flow.

Inductive loads are especially dangerous in trigger circuit working because they slow down the passage through the region in which the transistor has a large dissipation.

Acknowledgment.-Figs 3 to 9 are based on Figs. $3,4,6,7,20,9$ and 11 respectively of "Transistors in Switching Circuits"' by A. E. Anderson and Fig. 10 on Fig. 16(a) of "Transistor Trigger Circuits" by A. W. Lo. Both papers appeared in Proc. I.R.E., Vol. 40, No. 11, Nov. 1952.

## Mannifactirers* Literatare

Metal Rectifiers; a brochure giving dimensions and weights of selenium spindle-mounted stacks, with an explanation of the coding system used to identify them. From Standard Telephones and Cables, Rectifier Division, Warwick Road, Boreham Wood, Herts.

Solder, in wire, pellet and fluid form; a leaflet giving a summary of the products of Multicore Solders, Hemel Hempstead, Herts.

Television Receiver, type TUG36; console with a 17-in tube giving a picture $14 i n \times 10 \frac{1}{2}$ in and with five controls on the front panel, described in a leaflet from Bush Radio, Power front panel, Chiswick, London, W. 4

Radio-gramophone, H.M.V. model 1617A, with ten waveband ranges, three-speed record changer and 8 -watt output from a $13 \frac{1}{2}$-in speaker. Circuit description and specification in a leaflet from the Gramophone Company, Blyth Road, Hayes, Middlesex.

Universal Television Servicing Unit ("Klempt" Type FW0200), comprising a versatile a.m./f.m. signal generator and oscilloscope. Technical specification leaflet from Otto Gruoner, Winterbach bei Stuttgart, Germany.

High-energy Permanent Magnets using "Columax," an improved grade of "Alcomax III," and claimed to have the highest magnetic energy per unit of volume yet achieved $\left(8.63 \times 10^{6}\right.$ gauss-oersteds max.). Specification and curves in a leaffet from Swift Levick \& Sons, Clarence Steel Works, Sheffield, 4.

Electro-mechanical Devices, including a.c. and d.c. relays, mercury relays, time-delay relays, solenoids, thermostats and low-inertia motors for instruments. Specifications and operating characteristics in a catalogue from Electro Methods, Caxton Way, Stevenage, Herts.
Anti-vibration Instrument Mountings, in stud form, made of rubber with projecting metal pins. A leaflet giving shapes and sizes available from Howard Clayton-Wright, Wellesbourne, Warwickshire.

Television Converters; alignment instructions for Type AC/4 units in a leafet from Spencer-West, Quay Works, Great Yarmouth, Norfolk.

Surplus Equipment, Government and manufacturers', listed in a catalogue from Clydesdale Supply Co., 2, Bridge Street, Glasgow, C.5. Also a supplementary list of Components and Accessories.

Microwave Test Equipment, for waveguide sizes 10 and 11 , including standing-wave meters, adjustable short circuits, matched loads, waveguide-to-coaxial line transformers, variable attenuators, waveguide bench rails and supports, and a Heiltube test oscillator. Loose-leaf book containing specifications from Decca Radar, 1-3, Brixton Road, London, S.W.9.

Toggle Switches and Signal Lamps, also a number of special-purpose switches, described in an illustrated catalogue with blue-print drawings from Arcolectric Switches, Central Avenue, West Molesey, Surrey.
"Permanent Magnets," a well-produced illustrated book of 58 pages covering the theory of magnetism, design of magnets, materials used, properties of various alloys (with curves and tables), effects of heat, shock and alternating fields, magnetizing and demagnetizing, testing, storage and handling; with a glossary of technical terms. From the Permanent Magnet Association, 301, Glossop Road, Sheffield, 10 , price 10 s .

Waveform Analyser; description and specification (with curves) of the Muirhead-Pametrada instrument and associated equipment, with notes on its use for vibration measurement and waveform analysis in various industries. An illustrated booklet from Muirhead \& Co., Beckenham, Kent. Also a leaflet on their amplifier-maintained tuning forks for frequencies of $480-2,000 \mathrm{c} / \mathrm{s}$.

Fig. 10. Addition of diodes to stabilize pulse width and amplitude.

Fig. 9. Base connection switching circuits.


# Providing technical information, service and advice in relation to our products and the suppression of electrical interference. 

## Gold Plated Components

Considerable interest was aroused by the gold plated contacts on several of our components on view at the recent R.E.C.M.F, exhibi tion.

This finish came about as a result of stringent tests to which many components under clevelopment for the Ministry of Supply and Admiralty are subjected.

These tests, particularly those of R.C.S.II, to which components of the H.i grading have to be submitted, include subjection to temperatures of $100^{\circ} \mathrm{C}$ dry heat, where hitherto the top temperature in many cases was only $70^{\circ} \mathrm{C}$. In addition, there are tests in which the components are exposed to exacting and prolonged conditions of damp heat.

To maintain a low contact resistance under the exhaustive tests described above, considerable attention had to be given to the contact surfaces. After intensive investigation it was found that a gold flash on an appropriate underfinish gave the required durability, togetheriwith low contact resistance.

It will be obvious that once the process had been introduced, its benefits would be applied wherever desirable.

It may be asked why not keep to silver? Silver discolours badly as silver sulphide has an awful appearance, and makes it very ditficult for soldering.

## Birds on the Aerial

When speaking to an audience in a district where horizontal aerials are necessary, one question certain to be asked is, "What

happens if a row of seagulls decide to perch on the elements?" Webfooted birds don't perch in the accepterl meaning of the term. They will sit in rows on the comparatively rounded apex of a roof, or on the flat "bun finial " of a flag pole, but they cannot grasp a
half-inch rod or tube. Starlings might, but they only weigh a few ounces. We have seen rooks that have developed a technique of grasping the top of an " H " aerial, and sitting apparently in comfort, but even a rook has little weight. Birds are built for lightness, eren their bones are hollow and contain air.

## Suppression of Household Appliances

A few days ago we were testing out a new flex lead suppressor on a number of appliances, hair-dryers of various makes, fans, sewing machine motors, etc. The tests were carried out at home. When tried with T.V. on an outdoor aerial, suppression was quite good, making all the difference between intolerable nuisance and entertainment value. On an indoor aerial in the same room as the receiver however, interference was still troublesome. That is why, as we have so often written before, the authorities will have scant sympathy for a complaining viewer who has not done his best for himself by the erection of an aerial suitable for his location.

## A Lightning Tip

A few peals of thunder at Easter reminds us to issue the annual soother regarding lightning. The chance of a strike on your house is very remote, and the presence of an aerial does not increase the risk. If anything, it is bound to reduce the chance, as the presence of the aerial connected to a receiver is constantly discharging that little pocket of air in the immediate vicinity, thereby reducing the voltage gradient.

We can pass on a useful tip for those who feel they should do something to satisfy a qualm. Theoretically, the top element should be connected to the centre conductor of a co-axial feeder and the lower to the screen. We doubt if the average user would notice the difference, therefore reverse the arrangement and take the upper element to the screen, and before it enters the house, remove the P.V.C. outer covering exposing the screen, twist round it a length of heavy copper wire and take to a good earth by the most direct route. Care should be taken to waterproof the join with adhesive tape, otherwise water might syphon into the house via the screening mesh.
"Non-Directional'" 'Multirod',
We had a report from a useful source, that a "Multirod," carefully installed, was apparently " all round looking." The case was sufficiently interesting to warrant sending the mobile research laboratory to examine the situation. We found that the answer was due to the fact that the site was surrounded by hills, there was

apparently no direct signal, all that the aerial received was reflections and diffusions from the high ground.

## Aluminium Corrosion

Most forms of corrosion are very serious to the engineer, and we would prefer to think that there was no such thing associated with our aerials. We ask users to paint aerials on erection and at intervals, but we know that few are so treated. The form that aluminium alloy corrosion takes, is that parts tend to "grow" together, with a reduction of electrical resistance.

Written 27th April, 1953


# Diagnosis of Distortion 

By E. R. WIGAN*

B.Sc.(Eng.) A.M.I.E.E.

The "Difference Diagram" and Its Interpretation

AT the outset it should be emphasized that this article is not concerned with the measurement of distortion; it deals with a method of diagnosis aimed at recognizing, locating and removing the source of any distortion which is found.

The diagnosis is made by examining an oscillosscope trace which represents all the defects of the apparatus which is being tested. By comparing the outline of this picture with certain standard shapes, examples of which are given here, the various sources of distortion can be recognized. For example, typical overload conditions can be recognized at a glance (Figs. 10 and 11). In other photographs the distortion conditions have been artificially exaggerated to bring out the characteristic features.

The technique adopted to generate these pictures can be summarized bricfly as follows :-

A pure sine wave signal is applied to the test object (an amplifier, for example) and also to the X-plates (horizontal axis) of an oscilloscope.

The distorted output signal is applied to the Y-plates after passing through a network which subtracts the pure fundamental wave and leaves only the distortion terms, together with any hum, hummodulation or circuit "noise." Before being applied to the Y-plates this "difference " signal is amplified, generally 30 to 100 times.

When the phase of the X -signal is suitably adjusted the trace shown on the oscilloscope closes into a curved line which is a representation of the transfer

characteristic of the circuit tested with all its defects enormously magnified (see Figs. 1 and 2). Because this display is produced by a subtraction process the term "difference diagram" has been chosen for it.

The technique has the special merit that transient or slowly changing distortion conditions can be observed. Moreover, although it is not put forward as a measuring technique, it is possible to read off from the difference diagram the magnitude of the primary distortion terms with useful accuracy, a procedure which is necessary when correlation with standard harmonic analyses is required.

Since distortion components as small as 0.1 per cent can be recognized under good conditions, this method of diagnosis is applicable to amplifiers, oscillators, and the like, which have to meet even the most stringent performance specifications.

The cquipment required is relatively simple and can be assembled from apparatus generally available in an audio-frequency laboratory.

Details of Apparatus. To understand the difference diagram, consider first the typical input/output transfer characteristic of a single-valve amplifier shown in Fig. 1. The curve for an ideal amplifier is represented by the dotted line with a slope of 45 degrees, and the difference (i.e., vertical intercept) between these two curves represents the departure of the system from the ideal conditions. In Fig. 2 this difference is shown, plotted in the form which has been called the difference diagram.

Left: Fig. I. Ideal (dotted) and actual transfer character-
istic of an amplifier.
Below: Fig. 2. "Difference diagram" corresponding to Fig. 1.


[^2]The block schematic of the apparatus to produce this diagram electronically is shown in Fig. 3. The two upper branches carry out, at (9), the subtraction process illustrated in Figs. 1 and 2. The fourth branch is used only when a large distortion term has to be cancelled to prevent confusion of the fine detail.

The circuits shown are arranged for a test frequency of $1,000 \mathrm{c} / \mathrm{s}$. The filter (8) in Fig. 3 is necessary only if the phase shifter (7) contains valves which may introduce distortion. The ganged attenuators (4) and (6) are used to alter the input level to the test object (5) without changing the output level delivered by (6).

If it is desired to cancel any selected component in the difference signal, the oscillator (15), which can be set to multiples of $1,000 \mathrm{c} / \mathrm{s}$, is locked to the input signal by a "spike" generated by clipping and differentiation at (14). Element (12) is used to adjust the phase of the harmonic frequency generated by (15) relative to the phase of the test signal.

The arrangement shown in Fig. 3 is used when both the pure input signal and the distorted output signal from the test object are available, but if this is not so, and only the output can be obtained, the arrangement of Fig. 4 is employed.

Since the signal equivalent to the missing input signal is necessary for the "subtraction" process, a filter (8) is employed to abstract a pure sine wave from the output signal. Tests of this kind are called here 2 -terminal tests, to distinguish them from the 4-terminal test made when both input and output terminals can be used.

Typical Diagrams. Essentially the difference diagram is a Lissajous figure, the configuration of which will change with the setting of the phase control of the X -amplifier. In some circumstances it follows the shape of the transfer characteristics and it may also be used, with caution, to estimate the harmonic content. To introduce the reader to the kind of information which a difference diagram yields the following examples have been chosen: Fig. 5(a) is the difference diagram generated by a single-valve output stage. The input/output curve of such a stage is similar to Fig. 1, so the diagram of Fig. 5(a)
resembles Fig. 2. When the input voltage is increased the diagram changes to Fig. 5(b) The downward "spike" on the right is due to grid-current which sets in fairly sharply and reduces the output voltage. (The reason for the curve being looped is dealt with in the Appendix.)

The input/output curve of a push-pull stage is like Fig. 1 in the upper part, but in the lower part lies below the dotted line. As a result the difference diagram (see Fig. 6) droops downwards on the lefthand side and tips up on the right.

The distortion component present in Figs. 2 and 5(a) is almost pure second harmonic, shown by the two positive maxima in the difference signal. Fig. 6, however, shows nearly pure third harmonic because there are three positive maxima in the trace on the tube; one on the extreme right, one as the fundamental approaches negative maximum, and one as it returns to the centre again. In this photograph the "go" and "return" traces are, of course, superimposed. The vertical width of the diagram is due to hum in the amplifier. In spite of this the upper and lower edges retain their characteristic $S$-shape.
The flattened parabola of Fig. 7 indicates a heavily driven triode stage and contains both second and third harmonics. It consists of a parabola (characteristic of second harmonic) to which has been added an S-shaped curve which steepens one end and flattens the other. The relative proportions of the two components can be deduced from this. Here again, in spite of a very large proportion of hum, the upper and lower edges of the diagram retain the shape characteristic of the non-linearity of the system. To get this photograph the earlier stages of the amplifier were heavily driven while the gain control at the input to the final stage was turned down.
Fig. 8 shows the presence of hum-modulation in a push-pull output stage in which there was a strong $100-\mathrm{c} / \mathrm{s}$ ripple in the h.t. supply. The test-frequency was set to be exactly ten times the ripple frequency so that ten individual stationary traces could be seen, each corresponding to a different h.t. voltage. Each trace, Fig. 8(a), is a distorted S-shape and oscillates 100 times per second about the centre point of the



Portable test equipment and accessories. Numbering corresponds to that used in Figs. 3 and 4. The twin pre-amplifiers on the left are used to provide either high-level test signals (up to 20 dbm ) or to act as a buffer between the output from the test object and the input to the test gear. All units are housed in the standard ventilated boxes used by the B.B.C. Research Dept. for portable test opparaius.


Fig. 4. "Two-terminal" circuit for use when the input to the apparatus under test is inaccessible.


Fig. 5. Single-valve output stage working (a) just below and (b) jus: above the overload point. Fig. 6. Hum and third harmonic in a push-pull output stage. Fig. 7. Hum at greater level than second and third harmonics (single-valve output stage).
diagram. When the driver stage was balanced the second harmonic term disappeared, yielding Fig. 8(b). Finally the third harmonic was removed by "injection" (see Appendix). The resulting diagram, Fig. 8(c), has nearly straight edges which shows that higher distortion terms were negligible, evidence that the system was operating well within its capacity.

The previous example illustrates very well how effective a picture of the distortion can be, for the amplifier in question had earlier been tested with a wave analyser. The $100-\mathrm{c} / \mathrm{s}$ modulation had not then been noted, whereas the diagram showed at a glance that the modulation term was several times larger than the second or third harmonic.

Figs. 9(a), (b) and (c) show gross distortion in an amplifier of the electro-mechanical type in which a moving-iron loudspeaker movement drives a pair of push-pull carbon buttons. There are some novel features. Fig. 9(a) shows the stepwise response of the carbon granules. Fig. $9(\mathrm{~b})$ shows a double line at bottom centre due to an alternative transient condition. Figs. 9(c) and (d) show an unsuspected phenomenon, the reversal of the phase of the distortion terms when the d.c. voltage fed to the carbon button was increased slowly through a critical value. The distortion, Fig. 9 (c), momentarily disappeared and reappeared in reversed phase, as shown in Fig. 9(d). It will be noted that the "go" and "return" traces are different, owing to friction or other forces between the carbon granules.

The remaining diagrams were obtained with the circuit of Fig. 4. Figs. 10 and 11 show the "spike" characteristic of a system driven beyond its designed limits. Figs. 12(a) and (b) show very clearly the sharp origin distortion produced by a diode. The loop in Fig. 12(b) generally appears when severe overload is associated with a large transient phase shift.

The distortion illustrated in Figs. 11 and 12 is the result of two processes, and neither diagram alone gives any clue to the true cause. Both the recording and the playback equipment combine to produce Fig. 11, and transmitter and receiver combine to produce Figs. 12(a) and (b). From a series of diagrams representing different carrier levels and degrees of modulation it is, however, possible to separate the influence of the receiver from that of the transmitter, but it is difficult to find an equivalent method of dealing with recording distortion.

Fig. 11 is a good example of a difference diagram containing "noise" which has blurred the edges of the trace. Variation of the speed of the turntable caused slight oscillations of this diagram about its centre point. This has slightly lengthened the extremes of the trace and confused details which could
be clearly distinguished when the diagram was directly viewed on the tube face.

Scale of the Diagram. The $Y$ co-ordinate (i.e., the height) of any difference diagram will depend directly upon the gain chosen for the Y-amplifier of the oscilloscope. This gain must be known and included in any photograph of the diagram either for record purposes or to allow one picture to be compared with another. If the procedure set out below is followed the photograph is like Fig. 12(b). The necessary information is given by the scale.

The percentages represent the deviation from linearity of the transfer characteristic; the scale must be used with caution, however, for it can be applied directly only to the extremities of the diagram (e.g., the point A in Fig. 2). At that point the percentage scale reads 4 per cent while the input voltage is 2.0 V peak-to-peak. It follows that the 4 per cent ordinate corresponds to 80 mV . That is to say that if the conventional transfer characteristic were drawn, the instantaneous output voltage would exceed the instantaneous input voltage by 80 mV where the latter was +1.0 volt. Observe, however, that the corresponding ordinate at -1.0 volt input indicates that at this point on the diagram the output voltage will be less than the input voltage by 80 mV . This follows from the simultaneous change of sign of input and output voltage as the left-hand side of the diagram is entered.
This apparent anomaly should be carefully noted, and in practice a test always has to be made to establish whether positive or negative ordinates on the tube face represent gains or losses. A simple test is to apply a biased-off diode to the test-circuit; where the signal voltage exceeds the bias a sharp kink or spike appears in the diagram. The direction of this spike indicates the loss ordinate
Suppose now that the diagram of Fig. 2 were used to predict what the distortion would be if the signal input were reduced from 2 volts to 1 volt peak-to-peak. The diagram of Fig. 2 would then terminate at B. The mV scale shows that the error voltages would be 20 mV ; i.e., 2 per cent of the input signal. The percentage scale reads 1 per cent.

At first sight it appears that this kind of difficulty could be avoided by scaling each diagram in mV instead of percentages. This, however, would involve a new scale for every photograph, which would be impracticable.

On the other hand, if a percentage scale is used, three scales will serve for all purposes. In practice the percentage scale is determined as follows:-
(a) The cancellation circuit (7), (8) in Figs. 3 or 4

Fig. 8. Push-pull output stage with $100-\mathrm{c} / \mathrm{s}$ ripple in h.t. supply. (a) modulation with second and third harmonics. (b) driver stage balanced to remove second hormonic. (c) both second and third harmonics removed.


Fig. 9. (a), (b), (c) Distortion in electro-mechanical amplifier at successively increasing input levels. (d) as (c), but with microphone current slightly increased. (Note phase reversal.)

(a)

(b)

(c)

(d)
is interrupted, the X -signal removed, and the gain of the Y-amplifier adjusted to bring the resulting vertical line to a chosen height on the oscilloscope graticule. Let this height be D units.
(b) Having restored the cancellation circuit (7), (8) and the X -signal, the gain of the Y -amplifier is increased by a known amount (usually not more than 30 times) so as to make the details of the diagram clearly visible. Let the gain increase by N times.
(c) The percentage scale to be associated with this diagram must have an interval of DN/100 between the 1 per cent marks on the scale.

It is convenient to arrange that the Y -amplifier (A1) has several fixed steps of gain which are exactly known (say $\mathrm{N}=10,30,100$ ), and to prepare in advance the corresponding percentage scales, which can be fixed to the face of the tube and photographed together with the diagram.
Simplifications. The somewhat claborate networks of Figs. 3 and 4 can be simplified if no more than a general impression of the distortion is required. If changes of régime are considered unimportant, and only the larger distortion terms are of interest, the ganged attenuators and the "slave" oscillator chain (12) to (15) may be omitted.

Bridge-type circuits are a common feature of apparatus designed to measure total harmonic distortion, but although they provide an output which contains only the distortion terms, they cannot be used to generate a difference diagram, because the various distortion products are "dispersed," i.e., shifted in relative phase, by passing through the bridge network.

The essential components of a 2-terminal circuit are the phase-shifter and filter, (7) and (8). A 4-terminal circuit requires, in addition, a bandpass or possibly a low-pass filter at (2). The performance of these filters need not be superlative, for many commercial oscillators generate no more than 1 per cent or 2 per cent of second or third harmonics, which can be reduced to 0.1 or 0.2 per cent by 20 db attenuation at (2). If a valve stage, which may generate distortion, is incorporated in (7), filter (8) should have a slightly better performance.

Photographing the Diagram. For the illustrations a Cossor oscilloscope, Type 1035, with a green tube, Type 89D, was used.

The photographs were obtained with a Leica II camera on Kodak 35 mm orthochromatic film R55, with an exposure of $1 \frac{1}{2} \mathrm{sec}$ at $\mathrm{F} / 6.3$. The brightness of the trace was adjusted for each exposure by the following procedure. The trace was dimmed until only just visible in its weakest part while being traversed to and fro by the X -shift control. The brightness control was then advanced by a fixed amount predetermined by trial exposures.

This procedure makes allowance for the influence of mains-voltage variations upon the brilliance of the spot, and also for the large variations in writing speed which are caused by changes of test frequency or size and degree of detail of the diagram.

The percentage scale will appear in the photograph if it has been attached to the face of the tube and is given local illumination.

Conclusion. It is not easy to bring out in a short survey the full merits of this techniquc; the informa-

Fig. 10. Oscillator running into grid current. Fig. 11: Disc recording grossly over-modulated. Fig. 12. Radio receiver with "delayed" a.v.c.; modelation (a) just below and (b) just above 100 per cent.

tion given should, however, be sufficient to guide those who wish to explore its possibilities. The method has been in use in the Research Department of the B.B.C. in the course of the last $2-3$ years, its development being part of a general investigation into distortion in a.f. systems.

The illustrations in this article are taken from a stock of several hundreds collected over this period. It should be noted that, in order to simplify discussion, the most elementary examples have been chosen, whereas in practice much more complex forms may occur. Fig. 9 has therefore been included to demonstrate the application of this new technique to a more complex problem.

For the investigation of distortion in recording systems the difference diagram has unique value, for unless the speed of the medium (disc or tape) is practically constant only the simplest of the conventional distortion measuring systems can be applied in such work. It is justifiable in such cases to attempt to deduce the harmonic content from a geometrical analysis of the diagram, should a numerical expression of the distortion be required. In general, the diagram serves its most useful purpose in bringing to light the nature of the distortion and its relationship to hum and circuit noise. The history of Fig. 8 is a striking example of this.

It is not unreasonable to suppose that there is a relationship between the shape of the diagram and the aural assessment of the resulting distortion. Indications of such relationship have been found, but cannot be discussed here.

## APPENDIX

Operational Procedure. The circuits of Figs. 3 and 4 are used for 4 -terminal and 2-terminal tests respectively. Their operation will be described for a $1,000 \mathrm{c} / \mathrm{s}$ test tone. For tests at any other frequency the filters must be changed. The figures marked against the filters refer to the attenuation peaks adjacent to the cut-off points.

In setting up the difference diagram of an amplifier the first operation is to put 20 db at (4) and zero at (6) (see Fig. 3). Add attenuation at (3) to bring the overall attenuation from (3)-(6) to about overload point. Vary (7) and slightly adjust (3) until the difference signal contains no fundamental tone. This will be shown by minimum vertical deflection of the oscilloscope trace. Turn up the gain of the X-amplifier of the oscilloscope to get a nearly horizontal line.

Now transfer attenuation from (4) to (6) thus driving (5) harder. The $Y$-deflection will grow and a loop will form. Adjust (11) until this loop closes to a line. When the input to (5) is small this line will resemble Fig. 2 if the output stage is a single valve. As the input increases a difference diagram like Fig. 5(a) will appear. The centre shouid be tangential to the X-axis of the tube. If not, adjust (3) very slightly to tilt the diagram correctly. If a loop appears as in Fig. 5(b) first adjust (7) and then (11) to remove it. The final curve is a representative difference diagram.

The phase shifter (7) should be designed to shift the phase without changing the amplitude of the $1,000-\mathrm{c} / \mathrm{s}$ signal, otherwise any adjustment will cause the diagram to tilt about its centre point and this has then to be corrected by readjusting (3).

The 2-terminal network is adjusted in much the same way, except that (3) is adjusted initially to equal the loss in (7) and (8).

In some ampifiers a change of operating regime occurs as the drive increases. This is shown up by a 4 -terminal test but not by a 2 -terminal test. The gain at $1,000 \mathrm{c} / \mathrm{s}$ alters and the diagram tilts about its centre point. The change in gain can be measured by introducing a slight
compensating loss in the (7) (8) chain to restore the diagram to its original position.

The most difficult adjustment is the setting of phase shifter (11). If there are "overload spikes" as in Figs. 10 and 11 there is no difficulty, for it is clear that these must be located at the extremities of the X -axis. Sometimes artificial "spikes" have to be introduced (by a biased-off diode or rectifier) before the correct setting of (11) can be found.

When, as in Figs. 9(c) and (d), the "go" and "return" traces are different and have to be displayed separately for examination, the diagram is opened into a loop by a slight readjustment of (7).
If oscillator (15) uses a 2 -valve zero-phase-shift RC circuit, it can be locked by injecting the "spike" from (14) into the common anode lead. No frequency calibration is needed, since the harmonic number can be read from the trace which appears when the output of (15) is made large enough. The magnitude of the spike signal must be adjustable so that it locks the oscillator without introducing visible distortion.

Cancellation of the unwanted distortion term can be observed on headphones connected temporarily to the output of the Y-amplifier of the oscilloscope. Phaseshifter (12) can be of a simple type in which the output voltage is not strictly independent of the phase adjustment, for the size of the locking "spike" will not seriously affect the output of the oscillator (15).

# EABL'S COUBT 

Preliminary List of Exhibitors

AS a result of the recent ballot for space at the 20th National Radio Show to be held at Earl's Court from September 1st to the 12th, the Radio Industry Council has issued a preliminary list of exhibitors. In addition to the 80 manufacturers, traders and journals, etc., listed below, four banks, British Railways, the Electrical Trades Union, and the Association of Radio Battery Manufacturers have also taken space.
Aerialite, Ambassador, Antiference, Argosy, Automatic Coil Winder.
B.B.C., Baird, Balcombe, Belling \& Lee, Bernards, Boosey \& Hawkes, B.B.C., Buird, Balcombe, Belling \& Lee, Bern
Bowmaker, Brown Brothers, Bulgin, Bush.
C.W.S., Cole, Collaro, Cosmocord, Cossor.

Decca, Dubilier, Dynatron
Econasign, Edison Swan, English Electric, Ever Ready, Electrical $\mathcal{F}^{\circ}$ Radio Trading.
Ferguson, Ferranti.
G.E.C., Garrard, Goodmans, Gramophone Co.

Hobday, Hunt.
Invicta.
J. Manufacturing

Keith Prowse, Kerry's, Kolster-Brandes.
Linguaphone, Lugton.
McMichael, Marconiphone, Masteradio, Mullard, Multicore, Murphy. Peto Scott, Philco, Philips, Pilot, Plessey, Portogram, Practical Wireless, Pye.
R.G.D., Regentone, Reproducers, Roberts, Rola-Celestion.
R.G.D., Regentone, Reproducers, Roberts,
S.T.C., Simon Sound Service, Sobell, Stella.
S.T.C., Simon Sound Service, Sobell, Stella. Telerection, Thompson, Diamond \& Butcher, Truvox.
Ulita.
Valradio, Vidor.
Westinghouse, Whiteley, Wircless World and Wircless Engineer, Wircless Trader, Wolsey, Wright \& Weaire.
Plans for the exhibition, which will be open to the public from September 2nd, include considerable space for displays of radio and electronic equipment to be provided by the Services and manufacturers. It is also planned to have an educational and training exhibit on the lines of that introduced last year. Technical training colleges will be represented by Norwood T.C. and the Borough Polytechnic and industrial training establishments by E.M.I. Institutes and Marconi College. The B.B.C. Engineering Training Department will be participating and the universities will also be represented.

Many of the exhibitors will be equipping demonstration rooms and there will be the usual Television Avenue in which manufacturers have the opportunity of demonstrating their receivers.


## New TV Stations

THE temporary low-power mobile stations at Glencairn (Belfast) and Pontop Pike (Newcastle) were brought into regular service by the B.B.C. on May 1st. Pontop Pike is linked with the main radio network, but Glencairn relies on its direct reception of the Kirk o' Shotts transmitter for rebroadcasting. Initially, the Newcastle station used a temporary aerial, but the main radiator, which will eventually be employed by the permanent medium-power transmitter, is now in use.

Both stations use horizontal polarization and their sound and vision carriers are slightly offset from those of the main high-power transmitters using the same channel to reduce interference. Glencairn, shown with its Marconi aerial in the above photograph, operates in Channel 1 (41.5 and $45 \mathrm{Mc} / \mathrm{s}$ ), and Pontop Pike in Channel $5(63.25$ and $66.75 \mathrm{Mc} / \mathrm{s}$ ).

The low-power booster station near Brighton started a regular service on May 9th. It uses vertical polarization, operates in Channel 3 ( 53.25 and $56.75 \mathrm{Mc} / \mathrm{s}$ ) and relies on its direct reception of Alexandra Palace for rebroadcasting. As in the case of the other two low-power stations, Brighton's carriers are slightly offset.

## MSF Schedules

STANDARD FREQUENCY transmissions from the Rugby station MSF are now being radiated continuously for 24 hours a day. In accordance with the Atlantic City Convention (1947), the carrier frequencies will be 2.5,5, 10,15 and $20 \mathrm{Mc} / \mathrm{s}$, but only three of these will be used simultaneously. Initially the transmissions are being radiated on $2.5,5$ and $10 \mathrm{Mc} / \mathrm{s}$ with a power of 0.5 kW .

These frequencies are not the most suitable for reception within the United Kingdom and it has, therefore, been decided to continue the transmissions on $60 \mathrm{kc} / \mathrm{s}$ for a short period each day. A power of 10 kW will be used for this transmission which will be radiated from 1429 to 1530 G.M.T.

The carriers will be modulated in accordance with the following cycle (repeated each quarter of an hour): 0-5 mins, $1,000 \mathrm{c} / \mathrm{s}$ tone; $5-10 \mathrm{mins}, 1 \mathrm{c} / \mathrm{s}$ pulses ( 59 th pulse in each minute being omitted); 10-14 mins, unmodulated; and $14-15$ mins, speech announcement. The carrier and modulating frequencies are derived from the same 100 $\mathrm{kc} / \mathrm{s}$ standard and are maintained to within $\pm$ two parts in $10^{8}$ of their nominal values.

Results of N.P.L. measurements of these transmissions are given each month in our sister journal Wireless Engineer.

# Mobile Television Transmitters - Standard Frequencies - New Amateur Band 

## Coronation Radio

BIGGEST-EVER radio hook-up has been planned by the B.B.C. For the Coronation Day broadcasts. In addition to the television arrangements (which include the relay to Europe detailed on pages 274 and 275) and those for home listeners, the entire transmitting equipment of the External Services of the Corporation will be employed. This includes thirty-six high-power and two mediumpower short-wave transmitters in this country, six in Malaya, two in Canada and two in Ceylon as well as m.w. transmitters in this country, Germany and Austria.

The B.B.C. has also been asked to provide land lines for a large number of overseas broadcasting authorities, while many other countries are retransmitting the received programme. It is estimated that in all some 1,000 stations throughout the world will be broadcasting some part of the day's proceedings. Eighty-four microphone positions for commentaries in 44 foreign languages have been provided by the B.B.C.

## Amateur 2-Mc/s Band

SINCE MAY 1ST amateurs in the U.K. have not been permitted to use the band $1715-1800 \mathrm{kc} / \mathrm{s}$, but instead have been granted the $200-\mathrm{kc} / \mathrm{s}$ band above $1800 \mathrm{kc} / \mathrm{s}$. This change was necessitated by the enforcement of part of the Atlantic City allocation table and the Geneva frequency plan covering that band.

It will be recalled that in the Atlantic City Radio Regulations there was no $2-\mathrm{Mc} / \mathrm{s}$ allocation in Region I (Europe and Africa) for amateurs. A footnote to the frequency allocation table, however, reads "In the band 1715-2000 $\mathrm{kc} / \mathrm{s}$, Austria, Ireland, the Netherlands, Northern Rhodesia, Southern Rhodesia, Switzerland, the Union of South Africa and the United Kingdom may assign up to $200 \mathrm{kc} / \mathrm{s}$ for the amateur service provided that the mean power of any amateur station does not exceed 10 watts and that no harmful interference is caused to the authorized services of other countries."

The Radio Society of Great Britain in giving details of the change lists the marititne stations (see p. 214 of our last issue) in the band which are likely to be particularly vulnerable to interference.

## "Trader Year Book"

THE "Wireless and Electrical Trader Year Book, 1953," to give it its full title, is a veritable mine of inform-ation-technical, legal and general-for the radio and electrical trader. This 24th edition includes thumbnail specifications of current broadcast and television receivers, i.f. values of broadcast receivers marketed between 1947 and 1951, valve base connections and mains voltages in the principal towns in Great Britain. It also includes in its 264 pages directories of trade organizations, manufacturers, wholesalers and proprietary names. It is published by the Trader Publishing Co., Dorset House, Stamford Street, London, S.E.1, price 10 s 6 d .

## Modern Navigational Aids

AN EXHIBITION "Navigation Today" has been arranged from now until September at the Science Museum, South Kensington, to show the basic principles of navigation and the changes which have taken place in
navigational methods under the impact of high-speed flying and the developments of radio and radar.

There are demonstrations of such radio aids as Consol, Gee, Decca Navigator, v.h.f. omni-range, ground controlled approach and, of course, radar. The latter includes an interesting supersonic simulator by Kelvin and Hughes of the Thames approaches in which model craft in motion on water are reproduced on a standard p.p.i. display.
Firms contributing to the exhibition include S. G. Brown, Cossor, Decca, G.E.C., Kelvin and Hughes, Kol-ster-Brandes, Marconi, Siemens, Sperry and Ultra.

## PERSONALITIES

Wing Commander R. Stanford-Tuck, D.S.O., D.F.C., who joined Marconi's W.T. Co. in 1949, and earlier this year was appointed sales manager of the Aeronautical Division, has been released by the company to join the Aircraft Division of the English Electric Co. Marconi's is a member of the group of which English Electric is the parent company.
H. R. L. Lamont, Ph.D., M.A., B.Sc., A.M.I.E.E., has recently joined the scientific staff of the European Technical Representative of the Radio Corporation of America whose office is in London. Dr. Lamont, who is well known for his book on waveguides, will be principally concerned with technical liaison. Until his present appointment he was senior lecturer in electronics at the Roval Technical College, Glasgow, and was formerly at the G.E.C. Research Laboratories, Wembley.
C. L. G. Fairfield, M.A., M.I.E.E., A.M.I.Mech.E., who has joined the Telegraph Construction and Maintenance Co., Ltd., as manager of the overseas division, had been with Mullard, Ltd., since 1947, latterly as manager of the valve division. He has been a director of Mullard Equipment, Ltd., for the past two years, and was a Mullard representative on the board of Telcon Telecommunications, Ltd.


Wilfred Sampson, B.A., A.M.I.E.E., has been appointed commercial manager of Telcon Telecommunications, Ltd. (owned iointly by Mullard, Ltd., and the Telegraph Construction and Maintenance Co., Lid.). A graduate of Queen's, Cambridge, Mr. Sampson joined the transmission systems division of Standard Telephones and Cables, Ltd., in 1929, where he gained wide experience in the field of telecommunications both in this country and abroad, particularly in South Africa.
J. Foster Veevers, M.I.E.E., has resigned his recent appointment as general manager of the Swindon lactory of the Plessey Company to become managing director of Peto Scott Electrical Instruments, Lid. Before joining Plessey's he was for many years manager of the Stockport factory of Salford Electrical Instruments, Ltd.

Until his recent appointment as senior liaison engineer of the Components Division of the Plessey Co., E. Morgan, B.Sc., A.M.I.E.E., had been in the Engineering Division of the B.B.C. since 1950. He had held the positions of superintendent engineer (transmitters) and assistant head of the Valve Section. Before joining the Corporation he was a member of the technical sales staff in the Osram Valve Department of the General Electric Co.

## OUR AUTHORS

Ralph W. Hallows, who has been a frequent contributor to Wireless World for the past 21 years, writes in this issue on the efficiency of the dry cell and suggests ways in which its design and construction might be improved. He has been European Consultant to the Burgess Battery Co. Inc. since 1925. During the war he was a major in the Royal Artillery and became chief instructor (radar) at the 6th A.A. Group School. Maior Hallows, who was an open exhibitioner at Magdalene College and an honours M.A. (Cantab.), is author of a number of books including "Radar Simply Explained " which has been translated into six European languages.
E.R. Wigan, who writes in this issue on the diagnosis of distortion, spent some 14 years in industry (graduating from d.c. and $50 \mathrm{c} / \mathrm{s}$ on the test beds of the G.E.C., Witton, in 1924 to audio and carrier frequencies in the laboratories of Siemens Bros., Woolwich, before joining the Signals Research and Development Establishment, Ministry of Supply, in 1938. At S.R.D.E. he was primarily concerned with the design of acoustic and a.f. field equipment and the associated test gear. Since 1949 Mr. Wigan has been in the B.B.C. Research Department, Kingswood Warren, Surrey, dealing with problems associated with distortion.

Eric Griffiths, contributor of the article on the design and construction of portable equipment in our last issue, is in the Lines Department of the B.B.C. Since joining the Corporation in 1941 he has worked at both transmitter and studio centres, and was for some time an instructor in the Engineering Training Department. Before joining the B.B.C. he was in the Research Laboratory of Callender's Cables (1936-39) and with the Ministry of Supply (1939-41).

## OBITUARY

It is with regret that we record the sudden death of Simon Orde, manager of the B.B.C. Engineering Information Department, on April 23rd at the age of 59. Mr. Orde joined the Corporation in 1942 as a censor and in 1943 transferred to the Engineering Division.

We record with regret that Charles Walter Eve, a former director of Standard Telephones and Cables, Ltd., and a director of Kolster-Brandes, Ltd., died on April 19th aged 66. He joincd S.T.C. in 1906 and retired in 1947. Mr. Eve was closely associated with the formation of the Radio Industry Council, the Radio Communication and Electronic Engineering Association and the Telecommunication Engineering and Manufacturing Association, and was at one time vice-chairman of the British Radio Valve Manufacturers' Association.

## IN BRIEF

Broadcast Receiving Licences totalled 12,892,231, including $2,142,452$ for television sets and 183,996 for car radio at the end of March. The month's increase in television licences totalled 69,472.

Stand-by Equipment has now been installed at the Sutton Coldfield television station and the switching arrangements permit it to be used with either the main or stand-by aerials. The powers are vision 5 kW , sound 2 kW . The last of the main stations to be equipped with stand-by gear is Alexandra Palace, where similar Marconi transmitters are now being installed.
Radio Exports.-Of the $£ 2.2 \mathrm{M}$ worth of radio equipment exported in March, $£ 855,084$ was for capital goods-transmitting gear, etc. According to Customs and Excise figures, components and test gear accounted for $\mathcal{L} 45,580$, domestic receivers $£ 442,072$, sound reproducing equipment $£ 253,128$, and valves $£ 216,531$.

Plastics Exhibition.-Among the 90 exhibitors at the British Plastics Exhibition, which will be held at Olympia from June 8 th to 18 th ( 10 a.m. to 6 p.m. daily) are the following radio and electronic manufacturers:-E. K. Cole, G.E.C., Radio Heaters, Rediton and T.C.M. Admission to the exhibition costs 2 s 6 d , but free tickets for the convention which runs concurrently with the show are available from British Plastics (the organizers), Dorset House, Stamford Street, London, S.E.1.

Instruments.-The second British Instrument Industries Exhibition opens in the National Hall at Olympia on June 30th for 12 days. The Scientific Instrument Manufacturers' Association is among the five supporting organizations. The exhibition will be open daily, except Sunday, from 10 to 6.30 .

Canadian Trade Fair.-Eight British publishers are combining to present a display of 55 technical, trade and specialized journals at the sixth Canadian International Trade Fair, to be held in Toronto from June 1st to 12 th. Our own publishers will be exhibiting 24 journals including Wireless World and Wireless Engineer. Among the British companies participating in the fair is the G.E.C., who will be exhibiting the BRT 400 E communication receiver and v.h.f. gear.

Communications in the widest sense will be featured at the German Communication and Transport Exhibition which opens in the 670,000-sq yd Munich Exhibition Park on June 20th. The exhibition, which will remain open until October 11th, will include sections devoted to broadcasting, radio-telegraphy and telephony and navigation.

German Radio Show, which was to have been held last August and has twice been postponcd, will open in Dusseldorf on August 29 th for nine days.
A.P.A.E. Officers.-At the annual general meeting of the Association of Public Address Engineers, L. W. Murkham was re-elected president. The vice-presidents are A. V. Sharp, J. F Doust, C. Clarabut (who is also chairman of the Courcil), A. H. Middleton and Alex J. Walker, who is also honorary general secretary. The Council consists of G. F. Baker, A. B. Hulme, W. O. Mannerings, A. E. Buchan, F. Hedges, A. E. Ward, R. Jackson and S. W. Lewis (trade members), and R. E. Owen, J. F. Doust, F. Poperwell, S. Norley, A. V. Sharpx S. Kelly, C. T. Wright and P. Whiteley (manufacturing members).
"Solid-State Electronics," which is at the fourdation of such practical applications as germanium diodes, transitors and other semi-conducting devices, will be dealt with by Dr. Karl K. Darrow of Bell Telephone Laboratories, in a series of four lectures at King's College, Strand, London, W.C.2, at 5.30 on June 22 nd , $23 \mathrm{rd}, 25 \mathrm{th}$ and 26 th . Although the lectures are addressed to students of London University, admission is free to others interested in the subject.
Transistor circuitry and applications will be dealt with by G. C. Sziklai of the R.C.A. Research Laboratories, Princeton, U.S.A., at a meeting at the Royal Society of Arts, Iohn Adam Street, London, W.C.2, at 5.30 on July ist. Dr. R. L. Smith-Rose will be in the chair. Tickets are available from the R.C.A. European Technical Representative, The Tower, Brook Green Road, London, W.6.

Electro-Acoustics.-A series of 10 lectures covering the narure, generation, propagation, measurement, recording and reproduction of sound has been planned by the Department of Radio and Musical Instrument Technology at the Northern Polytechnic, Holloway, London, N.7. The lectures by E. H. Jones, B.Sc., A.M.Brit.I.R.E., will be given on Tuesdays and Thursdays, commencing on June th. The fee is two guineas.
Fringe-area Reception.-A series of papers on this subject will be given at the summer meeting of the Television Society, which will be held at Bedford on June 27th.

Photographing TV Pictures.-Readers interested in the photographing of television pictures from the cathode-ray tube may like to know that in the Coronation number of Amateur Pholographer (May 27th) there is an article dealing with the subject.
"Designing a Tape Recorder."-In the complete circuit diagram (Fig. 7, p.231, May issue) the cathode resistor $\mathrm{R}_{20}$ of $V_{0}$ should be 470 ohms and in Fig. 4 ( $p .165$, April issue) $\mathrm{C}_{27}$ should be $0.5 \mu \mathrm{~F}$.


SIR NOEL ASHBRIDGE. The Radio Industry Council is to present him with this portrait by Frank O. Salisbury. Sir Noel was recently elected an honorary member of the Eirit.I.R.E. " in recognition of his services to the radio engineering profession of Great Britain and as a tribute to his outstanding work in developing the technical services of the B.B.C."

## LITERATURE

Engineering Education.-A booklet setting out the full-time and part-time courses in technical education available at colleges and institutes in London and the Home Counties has been issued by the Regional Advisory Council for Higher Technological Education. It includes a list of courses in radio and television servicing, in telecommunications for the C. \& G. certificates and in electrical engineering for the Higher National certificate. It is available from Tavistock House South, Tavistock Square, London, W.C.1, price Is.

Metric Edition of the British Standard for enamelled round copper wire (oleo-resinous enamel) has recently been published as B.S.1961:1953. It differs from the 1951 edition of B.S. 156 only in that all quantities are expressed in metric units. Copies may be obtained from the British Standards Institution, 24 , Victoria Street; London, S.W.I, price 4 s .
Technical Papers issued by all departments of the Department of Scientific and Industrial Research, including the National Physical Laboratory and the Radio Research Station, are listed in the 31-page catalogue "Government Publications, Sectional List No. 3 D.S.I.R.", revised to March lst. It is obtainable free from H.M. Stationery Office, York House, Kingsway, London, W.C.2.

Scientific Literature published by and for the Institute of Physics is listed in a catalogue which is obtainable gratis from the Institute, 47, Belgrave Square, London, S.W.1. A summary is given of some 30 books, monographs and pamphlets including "Physics as a Career" by N. Clarke, which deals with the fields of work open to physicists and the training necessary.

## BUSINESS NOTES

Emitron Television, Ltd., are to supply two flying-spot film channels for the new television station being built by the Italian broadcasting organization (Radio Audizioni Italiano) at Turin. They will operate on 625 lines and are fitted with magnetic heads for reproduction of sound tape recordings. Either married or single picture and sound films can be used.

Mullard is to transfer the manufacture of cathode-ray tubes from its factory at Mitcham, London, to a new Governmentfinanced factory of approximately $250,000 \mathrm{sq} \mathrm{ft}$ to be built in the North-East Lancashire Development Area. The vacated space at the Mitcham factory will be utilized for the production of other electronic devices.
B.I. Callender's Cables, Ltd., have formed a new company in Australia to co-ordinate the activities of agents in the Commonwealth and to establish a technical service organization. The registered office of British Insulated Callender's Cables (Australia), Pty., Led., is $84 / 88$, William Street, Melbourne, C.I., Victoria, Australia. B.I.C.C. has also formed a Canadian company. It has acquired the business of Phillips Electrical Works, Let., of Montreal and Ontario, which will now be known as Phillips Electrical Company (1953), Lid.

Modern Acoustics, Ltd., of Manor Way, Boreham Wood, Herts, (Tel.: Elstree 3636), has been formed to manufacture "Lectrona" loudspeakers which were previously produced and marketed by Acoustic Products, Led. E. L. Edwards, late of Edstone, Ltd., is managing director of the new company.

Mattis Industries, Ltd., of 4, John Adam Street, London, W.C.2, (Tel.: Trafalgar 5502), inform us that they have been appointed sales representatives for London and the Home Counties for the "Milaflex" range of insulating silks, tapes and cloths manufactured by Miller \& Ferguson, Ltd., of Glasgow.

Decca's Glasgow office, which deals with both radar and navigation business, is now at 67, Blythswood Street, Glasgow, C.2, (Tel.: City $6457 / 8$ ). The manager is R. E. G. Simmons.

London Docks servicing depot of Rees Mace Marine, Ltd., is now at Yabsley Street, Poplar, E.14, (Tel.: East 4216). It is under the management of $R$. Aveyard.

Exporting Computers.-The second electronic digital computer to be produced by Ferranti, Ltd., for export has been ordered by the Royal Dutch/Shell Group for installation in their research establishment in Amsterdam.
B.T.H. has received an order from the European Headquarters Command of the U.S. Army for $\$ 4 M$ worth of mobile fire-control radar equipment for supply to N.A.T.O. countries.

Marconi Marine radio and navigational equipment is being supplied by Marconi's associates Deutsche Betriebsgesellschaft für Drahtlose Telegrafie M.B.H., for four motor vessels being built at Rendsburg on the Kiel Canal.

## TRANSISTOR AMPLIFIER

PROBABLY the first piece of commercial apparatus on the British market to make use of a transistor is a small pocket amplifier for boosting the outputs of hearing-aids. Designed by Multitone, it is
 intended for hearing-aid users who get adequate output from close-range sounds but not enough from sounds at a distance. The G.E.C. Type GET1 point transistor used gives a power gain of about 15 db , and it has to be used with a high-impedance earpiece which is supplied with the instrument. The cylindrical housing has a plug at one end to fit into a standard hearing-aid battery $\left(22 \frac{1}{2} \mathrm{~V}\right.$ or 15 V$)$, and two sockets at the other for the input and output plugs and cords. Multitone have also produced a hearing-aid with a transistor output stage, the main object being to reduce l.t. consumption.

## No More "Reliable" Valves

VALVE manufacturers in this country deplore the use of the term "reliable valves" because it implies that all other valves are not reliable. Their trade association, the B.V.A., now announces that it intends to describe these valves as "Special Quality" in future. A "Special Quality" valve is defined as "a valve which has certain design and manufacturing features making it suitable for use under conditions different from or in excess of those experienced in normal radio or television receivers and when operated under stated or agreed electrical or mechanical conditions it has ,", an acceptable statistically determined expectation of life."

This definition covers several classes of valves, for example, those which will withstand severe mechanical shock but do not necessarily have long lives; those which have particularly long lives or high electrical stability but not so much ability to withstand shock; and those giving normal lives under moderate conditions of shock and vibration. Thus the term "Special Quality" has quite a wide meaning, and does not really distinguish the particular class of valves hitherto known as "reliable" from valves with other special qualities such as long life or stability.

## Books Received

Television Picture Faults. By John Cura and Leonard Stanley. Contains 150 photographs of television pictures illustrating various faults together with explanations of their cause. These explanations are printed in contrasting types for readers with and without technical knowledge. The faults mainly comprise those resulting from incorrect adjustment of the controls, but various forms of interference are also illustrated. Pp. 68. Television Times, Ltd., 39a, Bartholomew Close, London, E.C.1. Price 3 s 6 d .

Radio Engineering (Second Edition). By E. K. Sandeman, Ph.D., A.C.G.I., M.I.E.E. Method of approach is fundamentai and general, though specifically related to practical ends. The book grew from an instruction manual written primarily for maintenance engineers at B.B.C. stations. Pp. $613+$ xxi; Figs. 204. Chapman and Hall, 37, Essex St., London, W.C.2. Price 55s.

Télévision Dépannage. By A. V. J. Martin. A practical book on the installation, adjustment, fault-tracing and
repair of television receivers. Pp. 176; Figs. 197. Société des Editions Radio, 9, Rue Jacob, Paris, 6. Price 600 francs.
Modulators and Frequency-changers. By D. G. Tucker, D.Sc. An analytical and largely mathematical approach to the subject as applicable to amplitude-modulated radio and line systems. The book is intended for design and maintenance engineers. Pp. 218+xiv; Figs. 115. Macdonald and Company, 16, Maddox St., London, W.1. Price 28 s .
The Living Brain. By W. Grey Walter, M.A., Sc.D. (Cantab). Basically a book about research into the mechanics of the brain by means of electro-encephalography (and intended for general reading), but contains technical information on EEG apparatus developed by the author with appendices describing his electronic analogues of physiological mechanisms. Pp. 216+xii; Figs. 23. Gerald Duckworth \& Co., 3, Henrietta Street, Covent Garden, London, W.C.2. Price l5s.

## "Radio Designer's Handbook"

MANY thousands of copies of earlier editions of "Radio Designer's Handbook" have been sold throughout the world. The fourth edition of this popular work, just issued by our Publishers (price 42 s ; by post 43 s 6 d ) is more than four times as large as its predecessors. The book deals in detail with basic principles and the practical design of all types of modern radio receivers, audio amplifiers and record-reproducing equipment. It is the work of 10 authors and 23 collaborating engineers, under the editorship of $F$. Langford-Smith.

## CLUB NEWS

Birmingham.-The June programme of the Slade Radio Society includes two direction-finding contests. On the 12 th there is to be an evening contest and on the 13th-14th the second event for the Harcourt Trophy. There will be a technical discussion evening on the 26 th at 7.45 at Church House, Erdington. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

Coventry Amateur Radio Society"s "night on the air" has been suspended for the summer months, but meetings continue to be held on alternate Mondays at the Y.W.C.A., Queens Road, at 7.30 . On June 8th G2BVW will talk about 70 -centimetre operation. There will be a v.h.f. field-day on Sunday, June 21 st. Sec.: K. G. Lines (G3FOH), 142, Shorncliffe Road, Coventry.

Hastings and District Amateur Radio Club, of which L. H. Thomas, M.B.E. (G6QB), assistant editor of Short Wave Magazine, is president, is participating in the Hobbies Exhibition to be held in the town during Carnival Week, July 4th-1lth. Membership of the club, which during the summer meets only once a month, is now over 30 . Sec.: W, E. Thompson, 8, Coventry Road, St. Leonards-on-Sea.

Manchester.-The South Manchester Radio Club (G3FVA) meets on alternate Fridays at 7.30 at Ladybarn House, Mauldeth Road, Fallowfield, Manchester, 14, and is planning a course of instruction for the Radio Amateur Examination. Sec.: M. Barnsley (G3HZM), 17, Cross Street, Bradford, Manchester, 11.
Reading.--Meetings of the Reading Radio Society, of which W'. A. Smallcombe, B.Sc., was recently elected president, are held on the second and last Saturdays of each month at 7.0 at the Abbey Gateway, Reading. The programme for the coming session includes lectures, debates and demonstrations. Sec.: L. A. Hensford (G2BHS), 30, Boston Avenue, Reading.

Southend.-At the meeting of the Southend and District Radio Society on June 12th S. W. F. Asquith, A.M.I.E.E., will talk on frequency measurement. The winners of the recently awarded Pocock and Hudson Cups for home-built gear-J. Wallace and D. Whitworth, respectively-will demonstrate their equipment at the meeting on June 26th. Meetings are held on alternate Fridays at 7.30 in the Queen's Road Annexe of the Municipal College, Victoria Circus. Temp. Sec.: J. H. Barrance, M.B.E. (G3BUJ), 49, Swanage Road, Southend-on-Sea.

# LETTERS <br> TO <br> THE EDITOR 

The Editor does not necessarily endorse the opinions expressed by his correspondents

## Two-band Television Reception

WHEN alternative television programmes are provided, whether by the B.B.C. or by sponsoring or by both, it is plain that the new stations must operate on frequencies higher than the present $40-70 \mathrm{Mc} / \mathrm{s}$ band. New television sets will be designed to cover the new band as well as the old and must obviously include some station-selection mechanism.

The problems of design are technically straightforward ones, but what about the several million existing sets? Has anyone yet thought seriously about the problem of making them suitable ? The usual glib answer is that cheap, mass-produced converters will be produced which will enable the frequency of the new station to be changed to that for which the receiver is designed.

That is a satisfactory solution provided that the converter does what it is supposed to do, but will it ? It seems to me that there are a great many technical snags.

It so happens that most existing television sets are not readily tunable from one channel to another and some cannot be changed at all without a major operation. In order that normal reception of the station in the 40-70 $\mathrm{Mc} / \mathrm{s}$ band may be retained, therefore, the receiver must be left tuned to this station and the converter must operate to change the frequency of a signal in the higher band to this lower frequency. There is then a possibility of interference due to the direct pick-up of signals from the $40-70 \mathrm{Mc} / \mathrm{s}$ station by the carly circuits of the receiver. For the avoidance of interference a disparity of some 50 db between the two signals is required. In some areas and with some receivers this may be casily obtainable, but when the receiver is used near a $40-70 \mathrm{Mc} / \mathrm{s}$ station and remote from one of the new ones, the interference may well be intolerable. This is especially likely to be so with some of the earlier receivers which were not very well screened.

The solution would seem to lie in having the television set permanently tuned to a channel other than the local one-say to Sutton Coldfield in the London area-and to include in the converter provision for changing the frequency of the local $40-70 \mathrm{Mc} / \mathrm{s}$ station to this chosen channel. The converter then becomes necessary for all reception. This will increase its cost and the changing of the tuning of the set itself may be an expensive matter with some sets, although negligible with others.

In addition to this, where the television set is a superheterodyne, as most now are, the set plus converter will be a double superheterodyne having two oscillators. The almost limitless possibilitics of self-generated interference by beats between their harmonics are well known and it seems likely that satisfactory operation would be largely a matter of chance and would depend on the precise frequencies of the signal, the input of the set (lst i.f.), the i.f. of the set (2nd i.f.) and upon whether the oscillator of the television receiver is above or below the signal. The converter oscillator will have to be always below the signal to prevent inversion of the sound and vision channels.

The development and rapid growth of competitive television services will depend very much on the finding of satisfactory solutions to all these problems.

London, N. 14.
W. T. COCKING

## Broadcast Transmitter Distortion

THE letters of Ian Leslie in your April issue and A. Yates in your May issue both deal with the overall performance of the broadcasting chain, and a few notes on B.B.C. practice may be of value

There is, of course, no such thing as completely dis-
tortionless transmission, and the problem facing any authority engaged in broadcasting is to what extent shall distortion be permitted. If no restriction of volume range is used between microphone and transmitter, and the modulation is adjusted to such a level that 100 per cent modulation is never reached, then distortion may be very slight, but the average level of modulation will be extremely low, and listeners will rightly complain of excessive background noise due to interference and receiver noise in the quiet passages. For these reasons it is the practice in this and every other country to adjust levels manually so as to bring up the quiet passages and to keep down somewhat the level of the loud passages. This is done at the originating point in the programme chain. Sharp transients will, however, aîways occur, probably of such short duration as to be unobserved at the manual control position, and in any case so short as to make it impossible to take any human steps to limit their amplitude. In order to deal with this situation automatic means of amplitude limitation are incorporated at the transmitter input. These ensure that such transients cannot cause the transmitter to be modulated more than 100 per cent. Admittedly while so doing a certain amount of distortion is necessarily introduced by a very short period of time, but this distortion is very much less than that which would be heard by listeners if the transmitter were modulated more than 100 per cent. In that case the carrier amplitude would be reduced to zero for short periods of time and a very noticeable distortion radiated. Also, of course, heavy over-modulation can be very dangerous for the transmitting equipment.
The extent to which the average programme level is raised, and the extent to which limitation is used, is, of course, very much dependent on judgment of the degree to which distortion is acceptable, and on a balance being made between the amount of such distortion and the improvement in signal-to-noise ratio for the general listener. This improvement in signal-to-noise ratio is particularly important at times like the present, when on certain wavelengths there is appreciable interference from continental broadcasting stations.
The B.B.C. has arrived at its present standards after very careful listening tests, and believes that in the existing circumstances these represent the best compromise between distortion and interference.

Within the restricted band of frequencies available for medium-wave broadcasting there seems to be no prospect whatsoever of any appreciable reduction in interference from stations in other parts of Europe, and in fact a probability that this may increase. To increase the power of the medium-wave stations is not permitted by the Copenhagen Plan, and in any case to increase by an adequate amount would in most cases be impracticable. The hope for furure improvements in transmitting conditions lies therefore in the development of a v.h.f. broadcasting service. The B.B.C. has published the results of its experimental transmissions from Wrotham, and the development of a regular service is now under consideration by the Advisory Committee set up by the Postmaster General under the terms of the Government White Paper on Broadcasting.
Mr. Yates is in error in stating that we rarely give live transmissions. Of the programmes radiated after 6 p.m. in the week ending May 2nd, recorded programmes represented 25 per cent of the Home Service, 40 per cent of the Light Programme, and 62 per cent of the Third Programme. In any case, for the vast majority of recorded programmes the quality of reproduction is indistinguishable from that of a live programme. The continued introduction of new recording and repro-
ducing equipment should in time eliminate all unsatisfactory recorded items.

The quality of transmissions over the land lines from the studio to the various transmitters is subject to continual careful check. Only very occasionally does the quality of transmission deteriorate, and in such cases it is rectified at the earliest possible moment.

Consideration has been given to the use of the sound channels of the television service for the transmission of a sound programme, but the continued development of the television service and the fact that the equipment is in use for television purposes at times when the greater part of the public would wish to listen precludes such use.

The conclusion drawn by Mr. Yates that the general average of performance has deteriorated in the last twenty years is, I think, not justificd, as the improvements in the design of the equipment in the transmitting chain over the last twenty years have been very appreciable, while every care in the operation and maintenance of the equipment continues to be taken.

London, W.1.
Deputy Chief Engineer, B.B.C.

I WAS interested to see A. Yates' letter, supporting my plea for better B.B.C. iransmission quality, in your May issue.

As regards the use of recordings, I wrote to the Director of the Third Programme last autumn deploring the trend towards the development of a "transcribed service" and pointing out that, apart from questions of optimum signal quality, those shortcomings which identify the medium used-rumble, regular clicks due to a scratch, the change in quality as between the end of one dise and the start of the next-produce a mental image of the revolving turntable and destroy the illusion of reality, that psychological factor so important in a live service.
In reply I was informed that the extensive use of recordings is both necessary and expedient in a comprehensive service. Further, I was invited to Broadcasting House and shown that on direct playback (pickup tracking the groove freshly made by the cutter, with monitor switched instantaneously to input line or replay amplifier at will) the reproduced signal is almost indistinguishable from the input signal and total background noise imperceptible. I was told, and it was evident, that deterioration in the signal finally radiated is due to deterioration in the equipment of the playback channels, and in the recorded discs, due to careless handling by staff other than that of the recording department. There can be no excuse for this.

That improvement is possible in landline quality is indicated by the fact that excellent quality is in fact obtained from landline relays-sometimes. It is doubtful whether the use of television transmitters for sound services would serve any useful purpose in view of the fact that they would only be available at odd, "off-peak" hours. As regards the development of a comprehensive f.m. service, clearly the B.B.C.'s hands are tied by the financial powers-that-be.

Regarding automatic volume compression, the B.B.C.'s Parthian shot was a suggestion that I should see the matter in perspective; that "there is nothing more annoying than a strong carrier with low average modulation." I strongly disagree. Average level means nothing; minimum level matters but can be maintained by manual monitoring. Various measures can be undertaken by the listener to improve signal pick-up and/or mitigate interference of all types, but nothing can be done to correct a signal that contains non-linearity distortion. Many aspects of the interference problem are out of the B.B.C.'s control, but radiated signal quality is entirely their responsibility; in this at least let them set their house in order.

London, N. 10.
IAN LESLIE.

## Flywheel Sync

THE observation made in the opening paragraph of K. G. Beauchamp's letter in the April issue on the flywheel synchronizing circuit, described by B. T. Gilling in your March issue, we consider to be incorrect when it is stated without reservation that neutralization of impulsive interference is effected across the common load resistance of the diodes. This is true during the sync period; i.e., when the fly-back has been initiated and point B (B. T. Gilling's Fig. 2) is neutral, but prior to the sync pulse the circuit does not appear to be immune to noise. For example, during the period between the middle and end of the scan, point $\mathbf{B}$ is negative and thus noise spikes appearing 180 degrees out of phase at V2 (a) and V2 (b), anode and cathode respectively, will result in the greater conduction by V2 (a), and hence a positive signal voltage developed across the common load.

The operation of the d.c. amplifier, as shown in Fig. 5, is obscure, since the valve is without cathode bias and will be driven by positive excursions during the sync period into grid current which can find no d.c. path to cathode.

We support your correspondent in identifying the circuit as a phase discriminator, and it is to be hoped that the discriminator as used in frequency modulation applications, which for so long has assumed a similar identity, will be regarded more correctly as a frequency discriminator. W. J. CROSSLEY, S. L. FIFE.

English Electric Company, Liverpool.

## Lamp Interference

THE problem of lamp interference, raised by K. Robinson in your May issue, is quite well known, though it does seem extraordinary that a lamp with a continuous filament can give trouble.

Whilst the complete mechanism is, so far as I know, not fully understood, it is quite normal for vacuum lamps to act as quite powerful energy generators, and interference from them can cover a range of at least $\frac{1}{4}$-mile.

The functioning of a lamp as a r.f. generator, and the frequency, depends on instantaneous voltage, and thus when a.c. is used the interference only occurs on certain parts of the voltage cycle, and the frequency also varies, this accounting for "herringbone" and similar effects.

Luckily, this phenomenon is restricted to vacuum lamps normally of 25 watts or more, and these lamps are only used in special installations, such as traffic signs and "keep left" bollards, and are not on salc to the general public. The "gasfilled" lamp is quite innocent. Enfield, Middx.
A. P. HALE.

## "Desiguing a Tape Recorder"

REFERRING to the above article in your April issue, I should like to make two further suggestions for a level monitor. Both incorporate the refinement, particularly desirable in home-built equipment, of monitoring bias oscillator and audio output voltages simultaneously.

The first uses the two meters from an aircraft direction indicator (see Wireless World article of September, 1951, and remember the warning about beta radiation-January, 1952). Each meter is put in a bridge rectifier circuit which is fed through a high resistance from either the crase oscillator or the anode of the audio output valve. Because of the high sensitivity of these meters, there is no trouble concerning the load they will put on the two outputs.

The second method is very suitable if a 500 -volt h.t. line is available. A 1CP1 type cathode ray tube is used as the indicating device, the oscillator volts being fed across one set of plates whilst the audio output is fed across the other. This gives a rectangular fluorescent area the width of which is proportional to oscillator output and the depth to audio output.

Cussins and Light, Ltd.
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## TYPE M-1

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Average characteristics :

| Self Capacitance | ... |  | 22 |
| :---: | :---: | :---: | :---: |
| Forward resistance at S V D.C. | .... |  | $10 \mathrm{k} \Omega$ |
| Reverse resistance at 5 V D.C. | .... |  | $1000 \mathrm{M} \Omega$ |
| Maximum peak inverse voltage |  |  | 68 |
| Minimum A.C. input |  |  | 0.5 |

## TYPE M-3

Has similar characteristics and application with a maximum frequency of $100 \mathrm{kc} / \mathrm{s}$.


## Standard Telephones and Cables Limited



# Television Standards Converter 

Mobile Equipment in Holland for the Coronation Relay

READERS will see from our route map of the Coronation relay to Europe (following page) that the British 405 -line signals are converted to the continental 625 -line standard at Breda in Holland. The converter equipment, designed by the Philips Research Laboratories at Eindhoven, is basically the same as that used by the B.B.C. at Cassel last year for changing from French to British standards-a c.r.t. monitor displays the incoming picture and this is viewed by a camera working on the new standards. The situation is rather different at Breda, however, in that the pictures are going in the opposite direction and are being converted from a low number of lines to a higher number of lines. Moreover, the equipment is a good deal smaller than the B.B.C.'s, and is actually installed in a trailer-which also contains a reserve converter (in case of breakdowns) and a quantity of menitoring and test gear. This trailer is stationed outside a church known as the Grote Kerk in Breda, and from it cables run up the side of the building to the centimetre-wave transmitting and receiving equipments which are mounted on the steeple.
The smallness of the converter has been achieved mainly by the use of a c.r. tube with a screen diameter of only 5in to display the incoming picture. Normally, with a screen of this diameter, the definition would not be very good because of the relatively large size of the spot; but the tube is actually a flying-spot scanner with a very small spot and has a definition of 1,000 lines. The camera has an image iconoscope pick-up tube, and this is fitted with a mask at the edge of its viewing window to provide a black reference for the 625 -line signal.
As in previous converter equipments, the monitor c.r. tube uses a long-persistence screen as a means of light storage. Without this, the camera pick-up tube would tend to act as a simple photo-cell and would respond to the instantaneous variations of intensity of the light spot. Thus it would produce a spurious waveform corresponding to the $405-$ line vision signal, and this would beat with the normal 625 -line signal to give a completely meaningless output. With the long-persistence screen, however, a large component of unmodulated light is introduced, so that the intensity variations of the spot are made negligible in comparison and have little or no effect on the pick-up tube.
At the same time, of course, the persistence must not be made long enough to preserve one picture into the next picture period, otherwise blurring would occur with moving images. Actually the decay characteristic of the phosphor is such that the brightness of a point on the screen falls to about ${ }^{\frac{3}{4} \text { ths }}$ of its original value by the end of one frame period.
Another important point is that the scanning beam of the camera is arranged to "read" the picture at a more-
or-less constant time interval behind the "writing" spot of the c.r. tube. (This is possible because, although the line periods of the two systems are different, the frame periods are the same.) If this were not done there would be a phase drift between the two scanning systems, and sometimes the camera would be "reading" the picture while it was still bright from the spot and sometimes while it was fading out a long way behind the spot, and the result would be that the outgoing picture would fluctuate in brightness. The two scanning systems are actually locked together by synchronizing the camera waveform generators with the frame sync pulses of the incoming 435-line signal.

Since the conversion is from a low number of lines to a higher number, it has been necessary to "fill in the gaps " in the 405 -line picture by spot-wobbling. Without this device, the scanning lines of the camera would sometimes coincide with those of the 405 -line picture and sometimes fall between them, and an interference pattern would appear on the outgoing picture.

Recently Wireless World had an opportunity of seeing the converted pictures at Amsterdam, after they had been transmitted from Lopik, and we were agrecably surprised by their quality. Inevitably there was some degradation, but not enough to worry the average viewer, and we have seen worse on receivers in this country.

The converter equipment, with the monitor unit on the left and the camera on the right, is shown above, and below is the trailer in which the equipment is installed.


## International Television:



With the recent opening of the temporary, mobile, low-power television stations at Glencairn (Belfast) and Pontop Pike (Newcastle) and the booster station near Brighton, approximately $80 \%$ of the population are now within the B.B.C. television service area, indicated on this mab by the $100 \mu \mathrm{Vm}$ contours. The estimated coverage of the Glencairn transmitter, which relies on its direct reception of Kirk o'Shotts, is Belfast and its immediate surroundings. Using the permanent aerial, Pontop Pike serves an area within a radius of approximately 20 miles of the transmitter. The Brighton booster station, which re-transmits the Alexandra Palace transmission, is intended to serve the town and district.

Cable 2,000-mile Network for the Coronation Transmissions

THE international exchange of television programmes has been brought a stage nearer by the unqualified success of the recent tests conducted on the Continent, preparatory to the re-radiation of the B.B.C. Coronation day transmissions by stations in France, Holland and Western Germany. On these two pages we reproduce sketch maps of the British Isles and northern Europe showing the 2,000 -mile radio and cable network which will convey the B.B.C. television transmissions on June 2nd to viewers in four countries. On the opposite page is shown the complete chain of British television stations, the methods of linking and the service areas of each of the five high-power and three low-power transmitters now in use.
For the continental relay the vision signal will be transmitted from London to France by relay stations provided by Standard Telephones \& Cables, Ltd. It will be picked up at a point near Cap Blanc Nez, Calais, and re-transmitted to Cassel. It will be seen from the map that the 405 -line signal is carried by the French P.T.T. and Radiodiffusion et Télévision Françaises south from Cassel to Paris for conversion to 441 and 819 lines for re-transmission by Paris and Lille. The 405 -line signal is also carried east from Cassel to Lille where it is conveyed over a chain of centimetre-wave links across Belgium, which has not yet a television service. It is, however, planned to monitor the transmission in Brussels where a
limited number of people will see the 405 -line picture probably on large-screen equipment.

The key point for the 625 -line transmissions by the Dutch and West German stations is Breda, where, as described on page 273, the Philips organization has set up a conversion unit. The 625 -line signal will be taken by direct links to Hilversum and Eindhoven and via four centimetre-wave relays to Wuppertal to be fed into the permanent network recently inaugurated by the Nordwestdeutsche Runfunk to link the five N.W.D.R. television stations. The longest hop in this chain of relay stations is that linking the Berlin transmitter with the last station in Western Germany-a distance of nearly 100 miles. The frequency used for this hop is $196.25 \mathrm{Mc} / \mathrm{s}$. In addition to the five N.W.D.R. stations the Frankfurt transmitter in the American Zone and possibly the Weinbiet station near Baden Baden (French Zone) will be radiating the 625-line transmission.

The complementary sound transmissions will be carried by cable to the Continent, where broadcasting organizations will have the choice of two of the following three circuits: 1, background sound free from any commentary; 2, English commentary; and 3, French commentary. It will, therefore, be possible for Dutch and German commentators to hear the English or French commentary which they can then translate for superimposition on the background sound.

Centimetre-wave links covering some 1,200 miles form the chain for the re-transmission of the B.B.C.'s Coronation day broadcasts by Continental television stations. Against each transmitter is indicated the standard employed.


# Improving the Dry Cell 

Making Better Use of the Raw Materials

By R. W. HALLOWS, M.A.(Cantab), M.I.E.E.

WHEN zinc was plentiful and little accounted, a run-down dry battery, whose cell-cans might still contain from two-thirds to four-fifths of their original weight of the metal, could be thrown light-heartedly into the dustbin. To-day, there is a world shortage of zinc, and it is a matter of some importance that it should not be used wastefully. The dry Leclanché cell, which has proved itself to be the most convenient, the least messy and the most foolproof source of what the late Dr. C. F. Burgess aptly termed portable power, is nowadays one of the major callers on the world's zinc supplies, for the number of such cells in use at any moment runs into astronomical figures. Apart from the fact that most of the world's homes are now within range of some source of broadcast entertainment, and that the majority are still without mains supplies of electricity, portable wireless receivers of various kinds enjoy wide popularity; much of any army's wireless equipment must be battery-operated; hearing-aid appliances, developed from the a.f. side of the wireless receiver, are being used in larger and larger numbers. If one thinks, too, of the flashlamps, the cycle lamps and other small electrical appliances used now by millions of people in all parts of the world, it is quickly realized that the term astronomical is no exaggeration when applied to the number of dry cells in use the world over at any time.

The purpose of the present article is to investigate the efficiency, or otherwise, of the dry cell as we know it and to suggest ways in which its design, composition and construction might be improved. A second article will deal with the possibilities of using relatively cheap power from the supply mains to bring dry cells after discharge back to something like their original condition.

As almost everyone knows, the Leclanche cell " generates a current of electricity by consuming zinc as a fuel." Or, to put it a little less unscientifically, such a cell maintains a flow of electrons through an external closed circuit by converting into electrical
energy the chemical energy involved in the recombination of ammonuim-chloride and zinc into zincchloride, ammonia and hydrogen. As the textbooks have it,

$$
2 \mathrm{NH}_{4} \mathrm{Cl}+\mathrm{Zn}=\mathrm{ZnCl}_{2}+2 \mathrm{NH}_{3}+\mathrm{H}_{2} .
$$

That is a considerable over-simplification, for every manufacturer has his own pet electrolyte, which may contain calcium, lithium, magnesium, zinc and possibly other metals in the form of chlorides. This, however, is not the place to discuss such a complex matter, and we may accept for working purposes that the primary reaction is on these lines.

## Depolarizing Process

The word "primary" is used because the cell is really a two-part affair. Part 1 consists of the electrolyte and the zinc, between which (on open circuit) there is a potential difference of about 1.1 volt. This portion is very efficient, in so far as it does not suffer from polarization: it gets rid of its surplus hydrogen in the form of positive ions. In Part II we have a p.d. of 0.4 V between the carbon and manganesedioxide clement and the electrolyte; hence the overall open circuit p.d. between the terminals of the cell is about $1.1 \mathrm{~V}+0.4 \mathrm{~V}=1.5 \mathrm{~V}$. But in this second part of the cell we run into considerable trouble when the external circuit is closed.

Each positive hydrogen ion, on reaching the carbon element, exerts an attraction which causes one electron to leave the negative pole, to travel through the external circuit and to turn the positive ion in question into a neutral hydrogen atom. Were nothing done about it, the carbon would soon be surrounded by a blanket of inert hydrogen molecules. Part II of the cell would be clogged and the action of Part I would also be brought to a standstill, for it would no longer be able to discard its surplus hydrogen ions.

Many textbooks lightly show the action of the man-


Fig. 1. Curve A shows typical end voltages during intermittent discharge of high-grade cells under ideal conditions of load, temperature and rest periods. A considerable proportion of the ampere-hours potentially available from the zinc in the can is useless, since the e.m.f. is too low. B is the discharge curve of moderately good cells under similar conditions.
ganese-dioxide depolarizer usually employed as :

$$
2 \mathrm{H}+2 \mathrm{MnO}_{2}=\mathrm{Mn}_{2} \mathrm{O}_{3}+\mathrm{H}_{2} \mathrm{O}
$$

If that were a complete statement of the case polarization would be eliminated; or, in any event, complete depolarization, with a return to its original e.m.f., would occur in a cell "rested" for a short time. That this does not happen is common knowledge. The reactions involved are far more complicated. It would be nearer the truth to write: "In time, a certain amount of the hydrogen molecules become dissociated into ions and some of these react with some of the manganese dioxide to form another oxide of manganese and water. Other slow and complex reactions are involved, and this process of depolarization is never sufficiently rapid to keep pace with the clogging that takes place during discharge, or complete enough to restore the original load e.m.f., no matter how long the cell is rested."

Now let us see how effectively the zinc is used. My experiments were made with cells of the $1 \frac{1}{4} \times 2 \frac{1}{4}$-inch size. Each maker has his own designation for these. The Ever Ready "U2" will be familiar to most readers and will be used as a general term, though cells of a number of different makes, British and American, were subjected to the series of tests on which the present articles are based. The cans of such cells vary somewhat in weight from make to make; nor is it always easy to determine the exact weight of zinc, for seamed cans contain a certain amount of solder. Some cans are thicker than others and there are slight variations in dimensions. On the whole, though, we shall not be far out if we put the average weight of zinc in cans of this size at 19 grams.

There is no difficulty about discovering the number of ampere-hours of current which 19 grams of zinc would furnish, could it be used with complete efficiency. An ampere is a flow of one coulomb a second, and a coulomb consists of $6.3 \times 10^{18}$ electrons. Zinc is bivalent; each atom passing into the electrolyte is a doubly positive ion, $\mathrm{Zn}^{++}$. This means that for every zinc atom removed from the can two electrons are available at the negative terminal of the cell. To maintain a current of one ampere, then, $3.15 \times 10^{18}$ atoms must leave the can every second. The atomic weight of zinc is $65.38(\mathrm{O}=16)$, and from Avogadro's Number we know that 65.38 grams of zinc contain $6.0234 \times 10^{23}$ atoms. Hence the weight of $3.15 \times 10^{18}$ zinc atoms is 0.000338 gram; and that is the electrochemical equivalent of zinc. Multiplying by $60 \times 60$, we have, in round figures, 1.2 grams of zinc per ampere-hour.

In other words, the current obtainable if 19 grams of zinc were used a hundred per cent efficiently, would be 15.8 Ah. Discharged under ideal conditions of load, temperature and time allowed for recuperation, average cells of " U 2 " size give 3-4 Ah, and those of the highest quality from 5.5 to a little over 6 Ah . In other words, cells in common use may turn only from 19 to 24 per cent of their zinc to good account, while for the very best the figure does not exceed 40 per cent.
Many factors contribute to this low efficiency. One of the most important of these is that most apparatus intended to be operated by dry cells is designed to work satisfactorily down to, but not below, an e.m.f. of 0.9 V per cell. Curve A of Fig. 1 shows typical lumped end voltages (that is, the average e.m.f.s at the end of each day's run) of a group of first-rate cells, discharged under the ideal conditions mentioned. It will be seen that much of the current potentially avail-


Fig. 2. Discharge curve showing the effects of perforotion of the con at a moment when the e.m.f. is still 1.05 V .


Fig. 3. Construction of modern dry cell. It will be seen that no sac is used. Perforation often occurs in line with the top of the electrolyte paste.
able from the zinc is useless, since the e.m.f. has fallen below cut-off as a result of progressive polarization. The first requirement, then, if cells of high quality are to be made more efficient, is to speed up the depolarizing process and to make it more thorough. Possible means to this end will be considered later. Curve B of Fig. 1 shows the curve for moderately good cells, discharged under similar conditions.

Though their overall performance is poor, the cells are classed as moderately good because they do not show one shocking and all-too-common fault; perforation of the can when the e.m.f. is still above (sometimes well above) cut-off. Fig. 2 indicates what happens in such cases. The e.m.f. begins to fluctuate and then falls almost like the proverbial stone. The electrolyte paste oozes from the hole in the can and may do serious damage. Perforation of one or more cans is in my experience one of the commonest causes of the breakdown of h.t. batteries. I have many times known it occur in batteries which had till then been giving readings of from 0.95 V to 1.15 V per cell. A curious point is that the cans perforated are nearly always near the middle of the battery; that is, in an 80 -cell ( 120 -volt) battery untimely perforation is most liable to occur between the 20th and 60th cells from the negative end.

## Causes of Perforation

Premature perforation is in most instances due to poor design or construction. Fig. 3 (which may come as a surprise to any who have not examined the inside of a dry cell for some time) shows how most of these cells are made to-day. There is no sac, the depolarizing "mix" being in direct contact with the


Fig. 4. Suggested "inside-out" cell. Only a small part of the zinc used is now unemployed. By designing the cell so that the carbon forms a lining to the plastic container, the depolarizer is given a much larger surface area on which to act.
paste electrolyte. As Fig. 3 indicates, a position at which the first signs of perforation very often occur is in the part of the can on a level with the top of the electrolyte. When a cell which has failed in this way is opened one frequently finds evidence of a considerable amount of "creeping" of salts from the electrolyte in the vicinity of the puncture. Small differences in the concentrations of such salts may give rise to undesirable local action.

Creeping does not occur to any marked extent inside really good dry cells. It may be due to one of two causes, or to both together. The first of these is the use of too strong a concentration of sal-ammoniac in the electrolyte; the second is failure to make the seal perfectly air-tight. These two causes are probably inter-connected. When a cell is not air-tight, evaporation takes place from the electrolyte, with the result that the ratio of sal-ammoniac to water increases. Another cause of the perforation of cans before cut-off e.m.f. is reached, is the use of zinc of too light a gauge.

There is another important reason why a considerable amount of the zinc in the can is not available for the production of current. A glance at Fig. 3 will show that all that part of the can which surrounds the air-space, the washer and the seal is out of the running: it is merely acting as part of a container and has no electrical role. Again, there is very little electro-chemical action at or near the bottom of the can; and here again zinc as zinc is mainly wasted.

## New Design of Cell

Could not the dry cell be entirely redesigned on lines more in keeping with the present availability of raw materials? I think I am right in saying that, when the first dry cells were made, suitable carbon was most readily obtainable in the form of rods or plates. Zinc being then plentiful and cheap, the line of least resistance led to the familiar design of the dry cell. Great changes have occurred in the sixty-odd years that have passed since these cells began to come into anything like general use-changes, that is, in everything except their general make-up. High-density carbon, for example, is now readily shaped-or deposited-in any required way.

It is some time now since it occurred to me that a good many advantages might accrue, were the dry
cell turned, so to speak, inside out. I have not the facilities for making up the dry cell illustrated in Fig. 4 -or, for that matter, any kind of dry cell. But experiments made with wet Leclanché cells using carbon elements of large area have given very promising results. The main purpose of these has been (a) to put the zinc element where the greatest possible proportion of it plays a useful part; (b) to provide the depolarizer with the largest possible surface of carbon on which to act; (c) to make the greatest use of cheap and easily obtainable materials; (d) to evolve a cell which cannot play havoc by perforating; and (e) to produce a cell of exactly the same dimensions as the zinc-cased cell and fitting into any apparatus designed to be operated by it.
Fig. 4 illustrates more or less diagrammatically the suggested new look for the dry cell. The case is of plastic and into the bottom is moulded a "collar-stud" carbon (or metal) contact, with a metal cap on its external end. Immediately inside the case is a thin carbon lining; it need not be more than a few hundredths of an inch in thickness, for in the cell the carbon is chemically inert.

The zinc element is hollow and made of sheet metal, possibly perforated. Or again, it may be a finned diecasting. Its exact shape and mass must be the subject of experiments. The zinc is "pasted" with electrolyte in the ordinary way. The parts between the electrolyte and the button forming the negative contact are protected from chemical and electro-chemical action by a plastic coating.

## . . . And its Advantages

A cell made on the proposed lines cannot perforate; by far the greater part of the zinc is usefully employed; polarization must be much slower and depolarization quicker and more complete owing to the far larger area of carbon over which the hydrogen ions are distributed and on which the depolarizer is free to act. The surface area of the carbon walls is actually more than four times greater than that provided by the rod element now used. It will be seen that the proposed cell appears to be also inside-out, or perhaps one should say upside-down, as regards the polarity of its terminals. That protruding from the seal is the negative, while the cap at the bottom is the positive. This, however, is not a matter of importance, so long as the terminals are plainly marked + and -.

Though the idea of designing a dry cell on the lines described was original, in so far as it was based on my own line of thinking and on nothing that I had read, seen or heard, I cannot claim to be first in the field in trying to make the dry cell more efficient by turning it inside-out. Somebody always seems to have thought a little sooner than oneself of any new conception that occurs!

Explaining my scheme recently to an American friend, I learnt that an "inside-out" dry cell had made its appearance in the United States. I have not been able to acquire American cells of this type, or to find out anything more about them. Whether or not they bear any resemblance to the design suggested in Fig. 4 I do not know. What I venture to hope is that this article may stimulate British designers of dry cells to break away from tradition and to give us (and the all-important export market) something far more efficient and more economical than the familiar dry cells of to-day.

# VORTEXION <br> <br> TAPE RECORDER 

 <br> <br> TAPE RECORDER}

FEATURES WORTH

NOTING . . . . .
$\star$ Extremely low distortion and background noise, with a frequency response of $50 \mathrm{c} / \mathrm{s}$. $-10 \mathrm{Kc} / \mathrm{s}$., plus or minus 1.5 db . A meter is fitted for the measurement of signal level and bias level.
$\star$ Sufficient power is available for recording on disc, either direct or from the tape, without additional amplifiers.
太 The 15 to 30 ohms microphone balanced line input is fully loaded with 20 microvolts.

* Input 1 , which requires 35 millivolts on .5 megohm, is suitable for crystal P.U.s, microphones or radio inputs.
* A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of the play back signal.
* The power output is 3.5 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.
$\star$ Facilities are provided for using the amplifier alone and using power output or headphones while recording or to drive additional amplifiers.
$\star$ Total power consumption is approximately 50 watts.
* The hum and noise level which was already very low has been still further reduced.


The amplifier, speaker and case, with detachable lid, measures $8 \frac{1}{4} \mathrm{in} . \times 22 \frac{1}{2} \mathrm{in} . \times 15 \frac{3}{4} \mathrm{in}$. and weighs 31 lb .

PRICE, complete with WEARITE TAPE
DECK ..................................... 8400

POWER SUPPLY UNIT to work from 12 Volt Battery with an output of 230 v ., 120 Watts. 50 cycles within $1 \%$. Suppressed for use with Tape Recorder. PRICE $\mathrm{fl8} 00$.

## TYPE C.P.20A AMPLIFIER

For A.C. Mains and 12 volt working giving 15 watts output, has switch change-over from A.C. to D.C. and "Standby " positions. Consumes only $5 \frac{1}{2}$ amperes from 12 volt battery. Fitted with mu-metal shielded microphone transformer for 15 ohm microphone, provision for crystal or moving iron pick-up with tone control for bass and top. Outputs for 7.5 and 15 ohms. Complete in steel case with valves.


Manufactured by
VORTEXION LIMITED, 257-263, The Broadway, Wimbledor, London, S.W. 19
Telephones: LIBerty 2814 and 6242-3 Telegrams: "Vortexion, Wimble, London."


## MODERNIZING THE

# Wireless World Television Receiver 

Part 2.-Time-Base Circuits

IN the original Wireless World Television Receiver the frame and line time-bases were built on two separate chassis and the sync-separator circuits were included with the frame time-base. A similar arrangement is adopted for these new time-bases and the sync-separator is included with them.

The circuit diagram is shown in Fig. 1. $V_{1}$ is the sync-separator and is fed wirh the combined sync and picture signal from the cathode of the tube. It is actually fed through a $10-\mathrm{k} \Omega \frac{1}{2}-\mathrm{W}$ resistor suspended
in the lead from the tube cathode to the sync-input connector on the time-base. This resistor is shown dotted in the diagrams to indicate that it is external to the chassis. In the original time-bases, $C_{1}$ was so mounted and can be still if desired, but it is normally convenient to include it in the chassis. It must be so mounted that it has a low stray capacitance to earth.
D.C. restoration is effected in the grid circuit in the usual way and the separated negative-going sync pulses appear in the anode circuit. They are applied

Internal view of the frame time-base unit wita some of the chief components indicated. The sync-separator compc.lents are on the extreme right.


through a differentiator and attenuator $\mathbf{R}_{5}, \mathrm{C}_{15}, \mathrm{R}_{29}$, to $V_{5}$ of the line saw-tooth generator. They are also applied through a semi-differentiator $C_{3}, R_{6}$, to the limiter $\mathrm{V}_{2}$ which produces sharp output pulses from the trailing edges of the frame pulses. These are negative-going and are applied to the anode of the frame saw-tooth generator $V_{3}$.

This generator is a blocking oscillator using a transformer $T_{1}$. This transformer is identical with the one used in the original receiver. The saw-tooth appears across $C_{7}$. Instead of using a variable charging resistance for the Hold control, the charging resistance $\mathrm{R}_{14}$ is now fixed and is taken to a variable
voltage point provided by $\mathrm{R}_{134}$. The main reason for this is that a lower value variable component can be used and therefore one which can be wire-wound.

The saw-tooth voltage across $\mathrm{C}_{7}$ is fed to the grid of $\mathrm{V}_{4}$, the frame output valve, through $\mathrm{R}_{15}$ and $\mathrm{R}_{10}$, the latter of which is variable as a Height control. The deflector coil is transformer-coupled to the valve by $\mathrm{T}_{2}$ and the $150-\Omega$ resistance $\mathrm{R}_{20}$ across the deflector coil is for the purpose of reducing the line-frequency voltages set up in the deflector coil by unavoidable coupling to the line deflector coil.

Since it is not possible to make the inductance of the transformer anything like high enough to avoid


Fig. 1. Complete circuit diagram of the new time-bases. The resistor shown dotted is mounted in the wiring between the tube cathode and the input to the sync separator. $C_{21}$ is mounted on the deflector-coil assembly. $R_{45}, R_{46}$ and $R_{47}$ have no circuit function but are included merely so that the current waveforms can be checked easily with an oscilloscope.
severe waveform distortion, very heavy correction is needed to obtain linearity. This is obtained by a feedback circuit of the Blumlein type. There are in all four circuits introducing distortion of the same form ; the initial charging circuit $\mathrm{R}_{11}, \mathrm{C}_{7}$, the coupling $\mathrm{R}_{17}, \mathrm{C}_{9}$, the cathode-bias circuit $\mathrm{R}_{24}, \mathrm{C}_{10}$, and the transformer coupling. The transformer is the major source of distortion and the bias circuit the next in importance.

The correction circuit comprises $\mathrm{C}_{11}$ with $\mathrm{R}_{22}$ and $\mathrm{R}_{23}$, the latter being variable as a linearity control. It is the main such control and affects the linearity generally over the picture. The next elements $R_{25}$ and $R_{26}$ with $C_{13}$ affect the linearity at the extreme top of the picture only. In practice, $\mathrm{R}_{25}$ opens or closes the top half-inch of the picture. The remaining components $\mathrm{R}_{27}, \mathrm{R}_{28}, \mathrm{C}_{14}$ and $\mathrm{C}_{8}$, are unusual ones, but were found experimentally to improve the linearity at the extreme bottom of the picture.

The linearity is affected by valve curvature, and so the settings of the linearity controls are slightly affected by the Height control. The dependence is small, however, and causes no practical inconvenience. In initial setting up the Height control should be adjusted for a picture of about three-quarters normal height and the two linearity controls roughly adjusted. Height should then be increased until the picture is just a little smaller than the mask and the linearity controls finally adjusted. Linearity 1 can easily be adjusted at any time for uniform line spacing at the top of the picture. Linearity 2 should be adjusted on Test Card C if possible. Height can then be increased to the proper value

A very hard frame lock is usually obtained, with the result that over a large part of its range a variation of Hold only affects the picture Height. Usually it is sufficient to set Hold at about the middle of the hold range and leave it there.
In the line time-base the saw-tooth generator is a cathode-coupled multivibrator $\mathrm{V}_{5}, \mathrm{~V}_{6}$. The charging capacitance is $\mathrm{C}_{17}$ and the charging resistance is $\mathrm{R}_{33}$. The applied voltage is varied by $\mathrm{R}_{35}$ as a width control. This varies the amplitude of the generated saw-tooth and hence the drive on the output valve $V_{7}$.
The valve $\mathrm{V}_{6}$ is normally held beyond cut-off by the charge on $\mathrm{C}_{10}$, thus enabling $\mathrm{C}_{17}$ to charge. $\mathrm{V}_{5}$ is conductive. A negative-going sync pulse on the grid of $V_{5}$ reduces its anode current and causes a rise of voltage on its anode which is passed to $\mathrm{V}_{6}$ by $\mathrm{C}_{16}$. This makes $V_{8}$ conductive and its anode current is drawn from $\mathrm{C}_{17}$ to discharge it. Grid current also flows to charge $\mathrm{C}_{16}$. These currents flow through $\mathrm{R}_{31}$ and raise the cathode potential of both valves. which still further reduces the current in $\mathrm{V}_{5}$. The action is regenerative. When $\mathrm{C}_{17}$ is discharged, the current in $\mathrm{V}_{6}$ drops and so the cathode potential falls and the current in $\mathrm{V}_{5}$ rises. The action is again regenerative and $V_{6}$ is cut off. It is held cut off by the charge on $\mathrm{C}_{16}$ until the next sync pulse comes along or until $C_{16}$ has discharged sufficiently to let $V_{6}$ conduct again. The grid-return potential of $V_{6}$ is adjustable by $\mathrm{R}_{36}$ as a hold control.
$A$ resistance $\mathrm{R}_{34}$ is included in series with $\mathrm{C}_{17}$ in order to produce a large negative-going pulse on flyback. This is necessary in order to cut off the output valve rapidly and hold it cut off during flyback. The value of this resistance has an appreciable effect on the e.h.t. voltage produced and some effect on the linearity at the start of the scan.

No coupling transformer is used between the valve and the deflector coil and the circuit is one using a resonant flyback with an energy-recovery diode. Because of losses, the natural overshoot is less than $100 \%$, and to obtain h.t. boost either a step-down transformer must be used or energy must be fed into the deflector-coil circuit during flyback so that the overshoot does become $100 \%$. This energy is derived from a second circuit comprising $\mathrm{L}_{1}$ and stray capacitances which is coupled to the deflector coil by $\mathrm{C}_{20}$.

For a detailed explanation reference should be made to a previous article, but, briefly, $\mathrm{L}_{1}$ and the deflector coil form two tuned circuits with their self- and straycapacitances and they are coupled together by $\mathrm{C}_{20}$, which acts as a "top-end" coupling capacitance. When $V_{T}$ is cut off during flyback, energy is stored in the magnetic fields of both coils. In the case of the deflector coil, it is required that the energy in its field be turned into electric form in the capacitance and then back again into magnetic form ready for the next scan. A loss of energy inevitably occurs, and this is made good by a transference of energy from $L_{1}$ through $\mathrm{C}_{0}$.

The capacitance needed for this coupling is formed partly by the anode-cathode capacitance of $\mathrm{V}_{7}$ and partly by a $20-\mathrm{pF}$ capacitor $\mathrm{C}_{20}$. This capacitor actually comprises six $120-\mathrm{pF}$ capacitors in series, each of $750-\mathrm{V}$ rating, in order to obtain the required voltage rating of 4 kV total.

A metal rectifier is used as a diode for energy recovery and avoids any difficulty over heater supply. It recovers about $50-60 \mathrm{~V}$ at the mean anode current of $\mathrm{V}_{7}$ and this appears across $\mathrm{C}_{22}$. With the $300-\mathrm{V}$ h.t.


The line time-base unit. The e.h.t. voltage-tripler components are mounted near the cen're on a sub-panel of Paxolin: slots are cut around the fixing holes to lengthen the leakage paths.
line the anode supply for the output stage is thus $350-360 \mathrm{~V}$.

Linearity is controlled by the variable resistor $\mathrm{R}_{41}$, which varies the magnitude of a control voltage injected by $\mathrm{T}_{3}$ in series with the diode and derived from the anode current of $V_{7}$. This transformer is a simple scramble-wound component which needs no special insulation in itself and is, therefore, easy to make. As a whole it needs insulating for up to 2 kV from the chassis, because the peak voltage of the deflector coil appears on it. Magnetostriction in the core produces a whistle and the two are remedied together by enclosing it in sponge rubber to provide both electrical and acoustical insulation.
The resistors $\mathrm{R}_{15}, \mathrm{R}_{16}$ and $\mathrm{R}_{47}$ have no circuit function. They are included merely to enable the current waveforms to be checked with an oscilloscope. If an oscilloscope is not used they need not be included. If they are employed they should be wire-wound resistors of $1 \%$ accuracy so that they can be used for actual measurement purposes. The mean anode current can be measured, for instance, by measuring the voltage drop across $\mathrm{R}_{45}$ or $\mathrm{R}_{46}$. The reading in volts multiplied by 100 gives the current in milliamperes.
E.h.t. is obtained through a voltage-tripler rectifier system from the peak voltage which appears on flyback across $\mathrm{L}_{1}$ and the deflector coil. The tripler gives a multiplication of about 2.5 times and produces some 8.5 kV from the $3.4-\mathrm{kV}$ peak. The magnitude of the e.h.t. voltage is governed by the rate of cut-off of the output valve and by the value of $\mathrm{C}_{20}$. Increasing
linearity on Test Card C. It is not a critical control. When $\mathrm{R}_{4}$ is too small the picture tends to be gradually compressed towards the right. As $R_{41}$ is increased the linearity is improved and, if it is too high, it may expand towards the right. Adjust Width to the proper value and lastly, Hold.
A large range of width is available without losing synchronization but, after adjusting it, Hold should be readjusted because, even if synchronizing has not been lost, it may be nearly lost, and a slight change of mains voltage may send it over.
Some adjustment to $\mathrm{C}_{21}$ may be required. If this component is omitted, a series of grey and white bars will appear over the left-hand side of the picture. They are produced by ringing in the deflector coil itself and are quite independent of the time-base. They can only be avoided, in the absence of heavy coil losses, by equalizing the capacitances on the two coils of the line assembly. Ideally, $\mathrm{C}_{21}$ would be an adjustable component and would be adjusted to the critical value at which the bars disappear from the picture. In practice a suitable component is difficult to obtain, for it must be stable and withstand $1-\mathrm{kV}$ peak. An approximate balance using a fixed capacitor has been adopted, therefore, with the result that the bars may not be completely absent.

The balance is normally good enough if the bars are just visible on a blank raster, for they are then unnoticeable on a picture. Precise adjustment of $\mathrm{C}_{21}$ will make them disappear even on a blank raster, but sufficient precision for this is hard to obtain without using an adjustable component.
This capacitor is not mounted in the chassis but
directly on the deflector-coil assembly and across the " unearthy" coil of the line pair. If the deflectorcoil connections as a whole have to be reversed, $\mathrm{C}_{21}$ must be changed over to the other coil.

Adjustment of $\mathrm{C}_{21}$ is best carried out on a blank raster, which need not be synchronized. Without it, a series of vertical grey and white bars on the left-hand side of the picture will be seen gradually decreasing in intensity towards the right and ceasing about the middle. As $\mathrm{C}_{21}$ is increased in value up to the optimum they decrease in intensity, but reappear again when it is too large.

In practice, if the bars are more than just detectable with a blank raster and a $200-\mathrm{pF}$ capacitor, one should try different values for $\mathrm{C}_{21}$. The first step is obviously to try an extra $20-30 \mathrm{pF}$ capacitor in shunt with it, and to note whether this increases or reduces them. If it reduces them try a bit more, but if it increases them reduce the main capacitor to 150 pF and then start adding more capacitance.

The precise value for the complete elimination of the bars is quite critical. However, a value which renders them undetectable on anything but a blank raster is far from critical, and no difficulty should be experienced in finding one. If, by any mischance, the proper value cannot be found, it is a good plan to replace $\mathrm{C}_{21}$ temporarily by a variable air capacitor of 500 pF or so. This can be smoothly adjusted while watching the picture, and if a sharp balance point cannot be found, something is wrong somewhere.

Before turning to the constructional side it may be as well to say something about what parts of the original time-bases can be retained in making a change to the new one. The original sync-separator $\mathrm{V}_{1}$ and $V_{2}$ can be retained unaltered with the original circuit values; but $\mathrm{R}_{5}, \mathrm{C}_{15}$ and $\mathrm{R}_{29}$ of Fig. 1 must be included and have their new values. It may be found desirable in this case to reduce $R_{29}$ to 4.7 kS , for the original sync separator gives a larger output than the new one.

In the frame time-base the EF37 can be retained for $V_{3}$ and the EL33 for $\mathrm{V}_{4}$, but using all the new circuit values of Fig. 1. In the line time-base the EL38 is the only thing that can be retained. Although this has not been tried, it is probable




that the EF50 can be used in place of the EF91 without change of values. A 6SN7 double-triode has been employed successfully in place of $V_{5}$ and $V_{6}$ without changing component values.

The use of an 807 in place of the EL38 has not been tried and can hardly be recommended. It has a screen dissipation rating of 3 W only, compared with the 6 W of the EL38, and its rating is therefore exceeded in this circuit. Apart from this, it would probably work satisfactorily but it might well have a short life.

The time-bases give ample scan for a tube operating at $8-9 \mathrm{kV}$, and this is an adequate voltage for a $12-\mathrm{in}$ tube. Many will consider it enough for larger tubes, although the trend is to operate such tubes at higher voltages. The use of higher voltages is not recommended to the inexperienced, however, on account of the difficulty of avoiding corona troubles. These are
small for voltages below 8 kV , but become very considerable above 10 kV . In the region $9-10 \mathrm{kV}$ corona can be troublesome, but is not unduly so. To minimize these troubles the voltage is limited to 9 kV in the present design and, allowing for the inevitable variations, may be 8 kV in some models.

It may be remarked in passing that a major effect of slight corona, which may be otherwise unsuspected, is poor line synchronizing. The discharge produces pulses which fire the time-base erratically. The visible effect is a ragged edge to the picture.

The waveforms in various parts of the circuit are shown in Figs. 2 and 3 for the line and frame timebases respectively. These were all taken using the "Television Oscilloscope*." In the case of the frame time-base, most were taken using a $10-\mathrm{M} \Omega$ resistor as a probe to minimize the effect of the oscilloscope on the time-base. In conjunction with the capacitance of the cable, this acts as a filter and removes the small content of line pulses which appear on some of the waveforms. If such a filter is not used, several of the frame waveforms will not appear as traces with clean lines but rather as fuzzy outlines.

In the line time-base the oscilloscope was connected across $R_{45}, R_{46}$ and $R_{47}$, so that its case was live to h.t. If this is not done, the small ripple on the h.t. line appears also on the trace to distort it. Since this makes the case of the oscilloscope live, care must be taken in handling it.

* "Tclevision Oscilloscope", by W. Tusting, Wireless World, June and July 1952.


## LIST OF PARTS

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| $\mathrm{R}_{1}$ | 2.2M | dW | Erie |
| $\mathrm{R}_{2}$ | $100 \mathrm{k} \Omega$ | $\frac{1}{2} W$ | Erie |
| $\mathbf{R}_{3}{ }^{2} \mathbf{R}_{26}, \mathbf{R}_{29}$ | $10 \mathrm{k} \Omega$ | W | Erie |
| $\mathrm{R}_{4}$ | $33 \mathrm{k} \Omega$ | $\frac{1}{2} \mathbf{W}$ | Erie |
| $\mathrm{R}_{5}, \mathrm{R}_{8}, \mathrm{R}_{30}$ | $22 \mathrm{k} \Omega$ | 相 | Erie |
| $\mathrm{R}_{6}$ | $220 \mathrm{k} \Omega$ | dW | Erie |
| $\mathrm{R}_{7}, \mathrm{R}_{12}, \mathrm{R}_{22}$ | $47 \mathrm{k} \Omega$ | W | Eric |
| $\mathrm{R}_{9}$ | $2.2 \mathrm{k} \Omega$ | $\frac{1}{2} \mathrm{~W}$ | Eric |
| $\mathrm{R}_{10}, \mathrm{R}_{11}$ | $22 \mathrm{k} \Omega$ | 1 W | Eric |
| $\mathrm{R}_{13}{ }^{\text {a }}$ | $50 \mathrm{k} \Omega$ | potentiometer, wire-wound, linear, 5W | Reliance $\text { Type T.W./ } 1$ |
| $\mathrm{R}_{13 \mathrm{~B}}$ | $39 \mathrm{k} \Omega$ | 1W | Erie |
| $\mathrm{R}_{14}, \mathrm{R}_{17}, \mathrm{R}_{27}, \mathrm{R}_{28}$ | $1 \mathrm{M} \Omega$ | ${ }_{2}^{1} \mathbf{W}$ | Erie |
| $\mathrm{R}_{15}, \mathrm{R}_{32}, \mathrm{R}_{33}, \mathrm{R}_{37}$ | 470 kS | $\frac{1}{2} \mathrm{~W}$ | Eric |
| $\mathrm{R}_{16}$ | $2 \mathrm{M} \Omega$ | variable, linear | Rcliance <br> Type S.G. 1 |
| $\mathbf{R}_{18}, \mathbf{R}_{19}, \mathbf{R}_{39}, \mathbf{R}_{40}$ | 33, | $\frac{1}{2}$ W | Erie |
| $\mathrm{R}_{20}$ | $150 \Omega$ | ${ }_{2}^{1} \mathrm{~W}$ W | Eric |
| $\mathrm{R}_{21}$ | 6.8 k , | 2W | Erie |
| $\mathrm{R}_{23}$ | $250 \mathrm{k} \Omega$ | variable, loglaw | Reliance <br> Type S.G./1 |
| $\mathrm{R}_{24}$ | $470 \Omega$ | $\stackrel{1}{2} \mathrm{~W}$ | Erie |
| $\mathbf{R}_{25}, \mathbf{R}_{35}, \mathbf{R}_{36}$ | $20 \mathrm{k} \Omega$ | variable, wirewound, linear, 5W | Reliance <br> Type T.W./1 |
| $\mathbf{R}_{31}$ | $1 \mathrm{k} \Omega$ | $\frac{1}{2} \mathrm{~W}$ | Erie |
| $\mathrm{R}_{34}$ | $8.2 \mathrm{k} \Omega$ | $\frac{1}{2} \mathrm{~W}$ | Erie |
| $\mathrm{R}_{38}$ | $120 \Omega$ | 2W | Erie |
| $\mathrm{R}_{41}$ | $300 \Omega$ | variable, wirewound, linear, 5W | Reliance <br> Type T.W./1 |
| $\mathrm{R}_{42}$ | $330 \Omega$ | 6W | Welwyn |
| $\mathbf{R}_{43}, \mathbf{R}_{44}$ each $2 \times$ | $470 \mathrm{k} \Omega$ | 1W | Erie |

## Capacitors

$\mathrm{C}_{1}, \mathrm{C}_{4}, \mathrm{C}_{5}, \mathrm{C}_{8}, \mathrm{C}_{9},\left\{\begin{array}{c}0.1 \mu \mathrm{~F} \text {, tubular paper, } 350 \mathrm{~V} \text {, Dubilier } \\ \mathrm{C}_{31}, \mathrm{C}_{13}\end{array}\right.$
$\mathbf{C}_{21}, \mathbf{C}_{6}, \mathbf{C}_{12} \quad 8 \mu \mathrm{~F}$, electrolytic, $500 \mathrm{~V}, \stackrel{\text { Type } 460}{\text { Dubilier }}$ Drilitic BR850
$\mathrm{C}_{3}, \mathrm{C}_{18}$
200pF, silvered mica, 350 V , Dubilier
Type 635
$C_{7}, C_{14}$
$0.05 \mu \mathrm{~F}$, tubular paper, 350 V , Dubilier Type 450 $\mathrm{C}_{10 \mathrm{~A}}, \mathrm{C}_{10 \mathrm{~B}}, \mathrm{C}_{19} \quad 50 \mu \mathrm{~F}$, electrolytic, 50 V, Dubilier $\mathrm{C}_{15}$

$$
20 \mathrm{pF}, \text { ceramic }
$$ Drilitic BR505

Dubilier Type
$\mathrm{C}_{17} \quad 0.001 \mu \mathrm{~F}$, moulded mica, 350 V , Dubilier
Type 635
$\mathrm{C}_{18} \quad 0.01 \mu \mathrm{~F}$, tubular paper, 350 V , Dubilier
$\mathrm{C}_{20} \quad 6 \times 120 \mathrm{pF}$, silvered mica, 750 V , Dubilier
$\mathrm{C}_{21} \quad 200 \mathrm{pF}$, mica (see text), Dubilier Type
$\mathrm{C}_{22} \quad 0.5 \mu \mathrm{~F}$, tubular paper, Dubilier $\begin{array}{r}680 \\ \text { Type }\end{array}$
$\mathrm{C}_{23}, \mathrm{C}_{24}, \mathrm{C}_{2}, \mathrm{C}_{2} 0.001 \mu \mathrm{~F}, 10 \mathrm{kV}$, Dubilier Type 4706 B
Valves
$\begin{array}{ll}\mathrm{V}_{1}, \mathrm{~V}_{2}, \mathrm{~V}_{3}, \mathrm{~V}_{5}, \mathrm{~V}_{6} & \text { EF91 Mullard } \\ \mathrm{V}_{4} & \text { EL42 Mullard }\end{array}$
$\mathrm{V}_{7}$
$\mathrm{D}_{1}, \mathrm{D}_{2}, \mathrm{D}_{3}$
EL38 Mullard
Westinghouse 36 EHT60
Westinghouse 14 D134
(to be concluded)

## Short-wave Conditions

Predictions for June

THE full-line curves given here indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during June.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period


[^3]
## Marconi Television for Italy



## Equipment purchased <br> by R.A.I. through Italian <br> Marconi Company includes:

- $7 \frac{1}{2} \mathrm{~kW}$ vision transmitters
- $2 \frac{1}{2} \mathrm{~kW}$ sound transmitters
- Marconi Image Orthicon Cameras
- Complete studio installations
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# Radio 

How the Magnetic and Electric Fields Support Each Other

I)URING the war, when thousands of people had to be trained in the shortest possible time to look after radar equipment, it surprised everybody, I think, how in a few months any reasonably intelligent lad, starting right from scratch, seemed to be quite at home among unprecedentedly complicated circuitry. Some of them, not noticeably bright in other respects, could quite readily reproduce diagrams of such circuits from memory. We, who were called upon to do our spot of instructing, sometimes wondered what we could have been doing during our years of study! But when questions were asked that required the application of basic principles to a new situation some of the most outstanding memorizers failed the most dismally. It was not that they couldn't recite all the necessary principles from memory. The difficulty was-and is-first to know which to pull out of the bag, and secondly, how to use it. A, who relies entirely on memory and practical experience can go far astray when he comes up against something unfamiliar ; B, who works things out from principles may be hopelessly slow at routine stuff but can find his own way over new ground.

Exactly what happens between radio sender and receiver doesn't concern most of us very deeply most of the time; we are taken up with what happens before and after, and may not have to dig out our basic principles often enough to prevent them from getting rusty. So a little practice here and now may be all to the good.

Two months ago, you may remember, I mentioned that radio waves-electromagnetic waves, to be precise -consist of equal electric and magnetic fields. People sometimes ask, "Which part produces the signal in the receiving aerial ; the magnetic, the electric, or both ?" If the receiving aerial were close enough to the source to be affected by induction fields, this would be quite a sensible question, because the induction fields are those parts of the total electric and magnetic fields that depend directly on the source, so it is possible for them to be mainly electric or mainly magnetic, depending on whether the source is energized mainly by voltag: or current. That is why G. Bramslev was able to show (in the Nov. 1952 issue) how to use a frame aerial to discriminate against noise interference from sources producing mainly electric fields. When no clear distinction is made between induction fields, tied to their mother's apron strings, and radiation or wave-motion fields, making their own independent way through the world, it is not surprising that there are confused ideas about wave reception, such as a belief that an open-wire aerial responds to the electric part of a radiated wave and a frame aerial to the magnetic part, so that one can choose whichever one wants. Actually, asking
which part of the wave causes the signal in either kind of aerial is rather like asking whether things blown over by the wind are affected by the movement or the pressure of the wind. Without movement there would be no one-way pressure, and without pressure there would be no movement. The two are inseparable, so you can please yourself which you say is the cause.

If you still feel puzzled about this, even after the difference between induction and radiation has been made clear, I am not surprised. It does seem contradictory. Fact One is that an open-wire aerial responds to an induction electric field and a frame aerial or coil to an induction magnetic field, but not vice versa. Fact Two is that there is no difference between induction and radiation fields themselves but only in the way they are organized. And yet one is asked to believe that with radiation fields the type of aerial cannot be used to distinguish between the electric and magnetic parts, and that this is not simply because the electric and magnetic fields happen to be present in equal proportions. The only possible explanation must lie in the difference in organization between induction and radiation fields.

That is quite so, but to see it one needs to fall back on first principles. And it is just as well to remember that these principles are not mere armchair theory but are the results of actual experiments. One of the greatest of all experimenters was Faraday. He it was who discovered how to generate electricity by magnetism. (The generation of magnetism by electricity had already been discovered.) He found there were two ways of generating an e.m.f. in a coil of wire. One was to push a magnet in or pull it out. He found the e.m.f. lasted only while the magnet was moving relative to the coil. Of course the same result was obtainable with a fixed magnet and moving coil. The principle of the thing was summed up by saying that whenever any part of a circuit is cut by the flux of a magnetic field the circuit receives an e.m.f. proportional to the rate of cutting. If you were to get a large magnet and a small piece of wire as in Fig. 1, and move the magnet at right angles to the wire (i.e., towards or away from you in (a), and to left or right in (b)) the magnetic field extending between the poles of the magnet would cut across the wire and generate in it an e.m.f. The rate of cutting, and hence the e.m.f., would obviously be proportional to (i) the strength of the field, or flux density, (ii) the speed of movement, and (iii) the length of the wire.

The other epoch-making experiment of Faraday was to generate an e.m.f. in a coil without any movement, by varying the strength of the magnet. He did this, of course, by using a coil of wire as the magnet,
switching the current on and off. Again, the e.m.f. lasted only while the magnetism was varying. This result was generalized by saying that if the amount of magnetic flux linked with any circuit is varied the circuit will receive an e.m.f. proportional to the rate of variation.

On the first cxperiment is based the generation of nearly all the world's electricity supplies, and on the second the transformers needed to make those supplies economically available; so no wonder Faraday is the " patron saint " of electrical engineers.
As sometimes taught, the flux-cutting idea (Fig. 1) is given as the basic principle, and the flux-varying idea is brought into line with it by supposing that when a current is switched on the resulting flux springs out from it and cuts across any close-up circuits, and when it is switched off it returns inwards and cuts them again in the opposite direction. This mental picture is none too clear when it is called upon to explain the e.m.f. of self-inductance. How does the flux springing out from a wire cut that wire itself ? And this is not the only dubious aspect of the fluxcutting idea. The "experiment" purporting to demonstrate it (Fig. 1) is quite phoney. Unlike those of Faraday, it is not an experiment that can be per-


Fig. 1. The basic principle of how electricity is generated in a power station is often expressed something like this, by saying that if a magnetic field is moved across a length of circuit I an e.m.f. is generated in it, proportional to 1 and to the rate at which the field is moved across. Here the field is shown as due to a permanent magnet, moved towards or away in (a) and to right or left in (b), which is a crosssection of (a).


Fig. 2. When an attempt is made to verify Fig. 1, it is necessary to take account of the voltmeter leads. Moving the magnet couses no reading in (a); the arrangement shown in (b) is successful, but the action can ot least equally well be explained as change of magnetic field passing through the whole circuit.
formed. To demonstrate the existence of the e.m.f. it is necessary to connect a voltmeter between the ends of the wire; then what about the voltmeter leads? If they are kept within the field as in Fig. 2(a) they too are cut by the flux so they receive an e.m.f. which (assuming the field is uniform) exactly counterbalances the e.m.f. in the wire and one is none the wiser. If the leads are taken horizontally as in Fig. 2(b) so that they are not cut, the e.m.f. now shown by the voltmeter can be explained equally well by the fact that moving the magnet in the direction of the arrow increases the flux linking the circuit. The absence of result in Fig. 2 can likewise be explained on the same basis; the assumption that the field is uniform means that moving the magnet does not alter the flux linked with the circuit. So both of Faraday's methods of inducing an e.m.f. can be visualized and calculated as flux-linkage variation, without any need to bring in the rather shaky and experimentally undemonstrable flux-cutting picture.

## Example of Flux Linkage

Just to consolidate the matter, let us take a simple example; say the Fig. 2(b) situation, making the assumption that the flux density is uniform between the pole-pieces and zero elsewhere-no " edge effect." Wire, flux, and motion are all mutually at right angles. Field calculations are easiest if one uses the m.k.s. system of units, as most modern books do. The voltage generated is equal to the rate of flux cutting or linkage if that is in webers per second ( 1 weber $=$ $10^{8}$ " lines"). Suppose the flux density (B) is 1.2 webers per sq metre ( 12 kilogauss in the old units), the wire is 0.02 metre long, and the magnet is moved at 0.5 metre per sec. Then the cross-section area of flux passing through the circuit increases at the rate of $0.5 \times 0.02=0.01 \mathrm{sq}$ metre per sec , so the rate of flux linkage, and hence the induced voltage, is $0.01 \times$ $1.2=0.012$. If the process is pictured as flux cutting the original vertical wire, the figures are of course the same, but the result (0.012) must not be taken as the measurable voltage until one has made sure that no other parts of the circuit are being cut by any flux. Because of this the flux-linkage way of looking at it is both safer and (in less absurdly simple examples) may be easier.

So far we have supposed this moving magnetic field to be produced by a permanent magnet. But of course it could be an electromagnet. Fig. 3(a) shows a single-turn coil of wire carrying d.c. Its magnetic field is at right angles to the paper, and with an anticlockwise current as shown it is towards us, as suggested by the dots. Next (b) imagine the loop to be whisked rapidly to the right. The effect of this is that paths such as those shown dotted experience an e.m.f. tending to drive current in the directions shown. But because no circuits are provided there, it is only a tendency. One can say that within the area covered by the loop at any instant there is an upward e.m.f.

## Electric-Field Current

At this stage a little digression may be necessary to recall what happens when an e.m.f. is applied across a space. This is done in Fig. 4 by connecting a battery to a pair of parallel plates. The e.m.f. of the battery sets up a potential difference between
the plates, which is another way of saying that there is an electric field between them, indicated conventionally by the lines in Fig. 4. This field is reckoned in volts per metre. But before it can exist the battery must have driven a current from the lower to the upper plate in order to charge it positively. (Actually what happens, of course, is that electrons are driven downwards on to the lower plate to charge it negatively, but that is just another way of saying the same thing.) To anybody who thinks in terms of circuits and current electricity rather than charges and static electricity, this charging current is something of an anomaly. How can a current flow in a circuit that is not complete? Maxwell, the genius who brought his mathematics to bear on Faraday's experimental results and predicted electromagnetic waves, argued that what happened in the space occupied by the field was equivalent to a current ; it flowed only so long as the field strength was varying, so could not continue indefinitely in the same direction, and to distinguish it from conduction or circuit current he called it displacement current. It is like the limited movement in a fixed block of rubber while pressure is being increased across it. So we think of the temporary current that flows upward through the battery in Fig. 4 when it is connected as being continued back to the start by a downward displacement current in the space between the plates.

To fit this Fig. 4 picture into Fig. 3 it is necessary to imagine that the battery fills the whole of the space covered by the loop, because it is all occupied by upward e.m.f. So the downward displacement current must all flow outside the loop area. Finally, since the e.m.f. is not produced by a battery at all but by a moving magnetic field, the upward current too must be a displacement current. Since space at the top of the loop is positively charged, an upward displacement current must have just occurred in order to make it so ; in fact, at the extreme right-hand side of the loop the space is actually in the process of becoming positive at the top, and so a displacement current must still be occurring here. Note that it is in the same direction as the magnetizing current produced by the loop battery. At the left-hand side the positive charge must disperse as the edge of the loop passes by, so here there is a downward displacement currentagain in the same direction as the magnetizing current.

Now any current causes a magnetic field; no questions are asked as to whether it is a conduction current or a displacement current. So when the loop is moved there is no need to supply quite so much current from the battery; the difference is made good by the displacement current caused by the motion. The faster the loop is moved the greater the electric field developed by a given magnetic field and the greater the displacement current. If the loop were moved fast enough, could it be dispensed with altogether, the moving magnetic field being sustained entirely by displacement currents?

That is the question that Maxwell answered and expressed in the celebrated Maxwell equations. These don't mean a thing to anybody who is not rather unusually bright at mathematics, so I shall try to arrive at the answer by an easier route, even if it may not altogether satisfy the stricter mathematicians.

What we know already is that the electric field (denoted by $\epsilon$ ) is equal to the voltage per metre p.d. set up by the movement of the magnetic field. (If an


Fig. 3. If a simple loop electromagnet as shown, producing a magnetic field pointing towards the reader, is moved to the right it causes an upward e.m.f.

Fig. 4. In order to set up a potential difference between two plates it is first necessary for a temporary charging current to flow, and this is supposed to be continued as a displacement current along the directions of the electric field, shown
 here.
air capacitor with plates 1 mm apart is charged to 50 V , the electric field in the space between is 50,000 $\mathrm{V} / \mathrm{m}$.) And we know that the voltage is equal to the rate at which the flux is changing in the space concerned. The flux ( $\Phi$ ) is equal to the flux density (B) multiplied by the area of its cross-section. And B is equal to the magnetic field strength ( H ) multiplied by the permeability ( $\mu$ ). And in m.k.s. units $H$ is equal to the ampere-turns per metre of field length. We can greatly simplify the putting of all this together if we make our chunk of space a one-metre cube. The original magnetizing loop would appear in Fig. 3 as a one-metre square, but this would be an edge-on view of a turn made of strip one metre wide. Suppose that at the instant considered it exactly contains our stationary cube of space. And let the current round the loop be I amps. Then H is equal to I, and B (and therefore $\Phi$ in this case) is equal to $\mu \mathrm{I}$. The rate at which $\Phi$ is changing in this space depends on the speed with which the loop is moved across the space. By the time it has been shifted one metre the whole of the flux $\Phi$ has been taken away, so if the speed is $v$ metres per second the rate of change of $\Phi$ is $v \Phi$, and we know this is equal to $\epsilon$. So the final upshot is $\varepsilon=v \mu \mathrm{I}$

## Doing Without the Loop

Now to render the magnetizing loop entirely unnecessary, I has to be the displacement current generated by the charging of the space. A current is the rate at which clectric charges are being moved. If a charge amounting to one coulomb is transferred at a steady rate in one second the current is one amp. The amount needed to charge $C$ farads to $V$ volts is CV coulombs. Our chunk of space can be regarded as a capacitor with plates one metre in area spaced one metre apart. Its capacitance in m.k.s. units is equal to the permittivity ( $\kappa$ ) of space. The movement of the magnetic field at $v \mathrm{~m} / \mathrm{s}$ causes it to be charged to $\epsilon$ volts $v$ times per second, so the rate at
which charging takes place (which is I) is $\kappa \in \mathcal{V}$ coulombs per second. So now we know that $I=\kappa \epsilon v$. But our previous result told us that $l=\epsilon / v_{\mu}$, So putting these together we get

$$
\begin{aligned}
\kappa \in v & =\frac{\epsilon}{v \mu} \\
\therefore \kappa v & =\frac{1}{v \mu} \\
\text { and } v^{2} & =\frac{1}{\mu \kappa} \\
\text { so } v & =\frac{1}{\sqrt{\mu \kappa}}
\end{aligned}
$$

For reasons that arc too involved to explain in passing, the m.k.s. electrical units are based on the $\mu$ of empty space-air is practically the same-being equal to $4 \pi / 10^{7}$. Measured in the same units, $\kappa$ is found to be almost exactly $1 /\left(36 \pi \times 10^{9}\right)$, so

$$
\begin{aligned}
v & =\sqrt{ }\left(\frac{10^{7}}{4 \pi} \times 36 \pi \times 10^{9}\right) \\
& =\sqrt{ }\left(9 \times 10^{16}\right. \\
& =300,000,000 \text { metres per second approximately* }
\end{aligned}
$$

That is the speed at which fields have to move through space in order to be self-supporting. This apparently formidable requirement is in fact quite easily met, for any change in the magnitude of any current or voltage anywhere starts the process and launches an electromagnetic wave. But as we have seen in recent issues, it is only when the originating circuit is large and the rate of change rapid that the resulting wave is likely to be substantial.

If we did the above calculation more thoroughly, using a chunk of any dimensions, these would cancel out, giving the same result. I suggest you try it, just to convince yourself. Maxwell, being the bright boy he was, arrived at it by strict mathematical processes, before anybody knew definitely that electromagnetic waves were possible. It was Hertz who came along later and proved Maxwell right by demonstrating such waves produced by electrical means.

In case anyone thinks I have been trying to pull a

[^4]

Left : Fig. 5. Showing how any number of current loops can be put together to form a larger one, becouse the currents along internal frontiers cancel out.

Below: Fig. 6. Elaboration of Fig. 3 to show a procession of magnetic fields on the move, with the resulting displacement currents that help to maintoin the magnetic fields and therefore themselves.

fast one by quietly forgetting about the current in the top and bottom of the magnetizing loop that was necessary to produce the magnetic field, I would hasten on to Fig. 5, which shows what happens when 1 -metre " bricks" are put together as a start towards unrestricted open space. The currents in adjacent parts cancel out, so the dimensions of the bricks don't matter at all.

Another thing : the result does not depend on using m.k.s. units. Any system of units, recognized or unrecognized, will do, provided it is a system.

## Procession of Fields

Before finally knocking away the visible scaffolding that has helped us to build a picture of electromagnetic radiation, let us multiply it a little as in Fig. 6, showing three links in a whole chain of loops all moving to the right, with currents alternately clockwise and anticlock. The middle one, $S$, is just our old Fig. 3 friend, now escorted fore and aft by R and T . Between $R$ and $S$ the space which a moment ago, while $R$ was passing, was positive below is becoming positive above, so an upward displacement current is necessary. Between $S$ and $T$ it must clearly be downward. Now accelerate the procession to the speed at which battery magnetization is unnecessary, and what remains is a sequence of moving fields, alternately positive and negative; each bunch of magnetic field pointing towards us being accompanied by an upward-pointing electric field, and followed by an away-pointing magnetic field accompanied by a downward electric field. Since there is now no apparatus to maintain either field, each relies entirely on the other for its existence. It is the perfect marriage; they cannot be parted even by death.

So there is really not very much point in arguing about which partner causes the signal in a receiving acrial. Radiation can only exist as a combinationan electromagnetic wave. The logical view is that the electric field is primarily responsible, because that is what the free electrons in the aerial respond to. But since the radiated electric field is generated by the magnetic field the same answer is obtained if one supposed the e.m.f. in the aerial to be generated by the magnetic field as in ordinary Faraday induction. In practice the strength of a radio wave is usually given in terms of its electric field, in microvolts per metre, because this gives the aerial e.m.f. directly.

Fig. 6, you remember, was a sample of what we imagined to be a long chain of " links." A pair of them, say $S$ and $R$, makes up one complete wave, with positive and negative half-cycles. So wavelength is represented by twice the width of one link.

All the way through we have, for simplicity, been assuming that the fields are uniform over a whole link, loop, chunk, or brick. So Fig. 6 represents square waves. In practice one is more often concerned with sinusoidal patterns of field strength, and the calculations are usually made on that basis, which does not alter the main conclusions.

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# Voltmeter Loading 

Use of Potentiometer Method

$T$ is very well known that the measurement of voltage in high-resistance circuits is liable to be inaccurate because of the load imposed by the voltmeter. It is surprising, therefore, that more use is not made of a method which is described in all text-books of electricity-the potentiometer method.

A voltmeter requires some power to operate it and this power is normally supplied by the circuit under test. If this circuit is of high resistance it cannot supply the necessary power without a drop in voltage. In the potentiometer method, a separate source of power is used to operate the voltmeter and the circuit under test has to supply no power at all. It is, therefore, quite unaffected by the connection of the measuring circuit.

The arrangement is shown in Fig. 1, where $M_{1}$ is any ordinary voltmeter. The associated apparatus comprises a second meter $M_{2}$, which is preferably a centre-zero galvanometer, a potentiometer $R$ and $a$ battery $V$ of voltage greater than that to be measured. The circuit under test is represented by a box with two terminals AB . The measuring circuit is connected to $A B, R$ is adjusted so that $M_{2}$ indicates zero and the voltage is read from the voltmeter $M_{1}$.

If R is adjusted so that there is no current in $\mathrm{M}_{2}$, then AB neither supplies current to nor draws current from the measuring circuit. The voltage between A and B is thus the same as if the measuring circuit were not connected. If there is no current in $M_{2}$ the voltage across $\mathrm{M}_{2}$ must be zero and so the voltage between C and D must be the same as that between $A$ and $B$. The voltmeter $M_{1}$, however, indicates the voltage between C and D ; therefore, it gives a true indication of the voltage between $A$ and $B$. The power for operating the voltmeter is drawn entirely from the battery V.

In practice, it is not very convenient to have to use a separate power supply in this way. In most radio apparatus, however, the voltages appearing at highresistance points are derived by voltage-dropping from a common higher-voltage supply of relatively low resistance. Screen-grids, for example, are fed from the main h.t. line through dropping resistors or potential dividers. In most cases, therefore, the main h.t. line of the apparatus can be used for the voltmeter supply and the battery of Fig. 1 becomes unnecessary.

The basic circuit of Fig. 1 can be simplified by the omission of the battery but in other ways it requires some elaboration. It is necessary to have something to protect the meter $M_{1}$ in case $R$ is a long way from the proper adjustment when the circuit is connected. Let the voltage under test be $V_{d B}$ with a source resistance $R_{A B}$. If the slider of $R$ is at the bottom, the current in $M_{2}$ will be $V_{A B} /\left(R_{A B}+R_{m}\right)$, while if it is at the top it will be $\left(\mathrm{V}_{\mathrm{AB}}-\mathrm{V}\right) /\left(\mathbf{R}_{\mathrm{AB}}+\mathbf{R}_{m}\right)$, where $\mathbf{R}_{m}$ is the resistance of the meter.

It is necessary to make $\mathrm{R}_{m}$ large enough so that under these extreme conditions the current will not exceed the full-scale value of $\mathbf{M}_{2}$. The worst conditions
are when $\mathrm{V}_{\mathrm{AB}}$ is much less than V or nearly equal to V and, for complete safety under all conditions, it is desirable to have $\mathrm{V} / \mathbf{R}_{m}$ no greater than the full-scale current of $M_{2}$. In effect, this means that $M_{2}$ must be a voltmeter having $V$ within its range.

The resistance of $\mathrm{M}_{2}$ will then be high and this will make the meter an insensitive indicator of the balance condition and it will be difficult to determine the proper setting of $R$. To overcome this, the resistance can be short-circuited by a switch as balance is approached.

A second defect of the arrangement of Fig. 1 is that a potentiometer of ordinary quality does not give a fine enough control of voltage, particularly at low-voltage settings. It is often desirable to supplement it by a variable resistance. The circuit then takes the form shown in Fig. 2. $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$ should be of about the same value and $20 \mathrm{k} \Omega$ is suitable in most cases. With a $300-\mathrm{V}$ h.t. supply they will draw up to 15 mA and the power will be up to 4.5 W , so components of at least $6-W$ rating should be used. If $M_{2}$ is a centre-zero instrument reading 1 mA f.s.d., $\mathrm{R}_{m}$ should be $300 \mathrm{k} \Omega$ to avoid any possibility of overloading it.

In use, terminals 1 and 3 are connected to positive and negative h.t. of the apparatus under test and 2 is joined to the point at which it is desired to measure the voltage. With $\mathrm{R}_{1}$ about mid-way on its travel, $\mathbf{R}_{2}$ is adjusted for zero reading on $M_{2}$ (if this comes at the top of $R_{2}, R_{1}$ is reduced). Then $S_{1}$ is closed and $R_{2}$ (and $\mathbf{R}_{1}$ if necessary) is re-adjusted more precisely.


Fig. I. Basic potentiometer circuit for voltage measurement.

Fig. 2. Proctical circuit. $\quad M_{2}$ is a centre-zero milliammeter.



Fig. 3. Circuit for use with a left-hand zero meter for $\mathrm{M}_{2}$. The metal rectifiers ensure that the meter deflects one way only irrespective of the direction of the current.

When a centre-zero meter is not available, the ordinary left-hand zero type can be used in conjunction with a bridge-type metal rectifier of the kind used in a.c. instruments, as shown in Fig. 3. This makes the meter reading independent of polarity and so the adjustment for zero current becomes one for minimum deflection of the pointer. The sensitivity obtainable is not quite so great because the resistance of the rectifier elements increases as the balance point is approached, but the adjustment of $R$ is easier to carry out for a minimum reading than for zero.

It is, of course, possible to elaborate the scheme. By introducing switching, for instance, one meter can be used for both purposes. The voltmeter $M_{1}$, for instance, is only a milliammeter with series resistors. The meter itself can, therefore, be switched to do duty for $M_{2}$ if its voltage-range resistors are left in place to keep the proper load on $\mathrm{R}_{2}$.

## NEW IBTIKS

Television Receiver Design: Monograph 1 ; I.F. Stages. By A. G. W. Uitjens. Pp. $17 \bar{j}+$ xii ; Figs. 123. Philips Technical Library: distributors; Cleaver Hume Press, Ltd., 42a, South Audley St., London, W.1. Price 21 s .
THE Philips organization (Holland) have already published English translations of a series of books on broadcast receivers by members of their staff, and they are now embarking on a similar series on television receivers. This, the first, deals with the i.f. stages; the translation is, on the whole quite satisfactory; printer's errors are few and, except in one instance, of minor importance. At the end is a list of symbols, some of which will be unfamiliar to the English reader. It is a pity that the opportunity was not taken to bring all the symbols into line with English usage, as this would greatly enhance the value of the book to a student reader. There are seven chapters on single and coupled tuncd i.f. circuits with staggered tuning ; gain-bandwidth, distortion, noise and valve interelectrode feedback problems are thoroughly explored. The text is illustrated by numerical examples and the last chapter details a particular design of staggered tuning with five single circuits as well as indicates the response to a modulation envelope step function; a circuit diagram of the complete amplifier would have been helpful. The effect of trap circuits protecting from adjacent channels is considered, and reasons are given for the choice of the circuit to which they are connected. To preserve continuity proofs of many expressions used in the test are relegated to appendices. In Appendix 1, the attenuation and phrase responses of a single tuned circuit are derived,
and input, output and transfer impedances, and admittance locus diagrams are developed for dissimilar as well as similar runed circuits coupled by mutual inductance. Constant reference must be made to the list of symbols if the derivations are to be followed. In section $1 g$ it is not immediately clear that the primary is the coupling circuit and the secondary an absorber circuit when discussing trap circuits in terms of tuned coupled circuits. A diagram including values, such as Fig. 74 with suitable captions, would have made this clear. Appendix 2 develops the expression for determining the response of staggered tuncd circuits as used in Chapter 2 where the principle of "flat" staggered tuning is clearly set out.
In television receiver design it is important to know how the pulse shapes of the input signal are modified in their passage through the i.f. stages, and Appendix 3 shows how the modifications can be determined from the attenuation and phase response characteristics. A misprint makes Appendix 4 on noise factor calculations difficult to follow; Fig. 31 should read Fig. 56. Appendix 5 develops expressions used in Chapter 6, where feedback effects due to valves are considered. Table 1 provides information on the characteristics (gain-bandwidth, etc.) of Philips valves suitable for use in wideband amplifier stages. The remaining three tables are concerned with factors of importance in staggered tuned circuits. There is no indes.
The inexperienced designer will find much of value in this book but the expert will discover little that he does not already know.
K. R. S.

Sound Reproduction (Third Edition) by G. A. Briggs. Pp. 368; Figs. 315. Wharfedale Wireless Works, Bradford Road, Idle, Bradford, Yorks. Price 17s 6 d .

WRITTEN professedly in non-technical language and addressed primarily to the layman, this book contains, nevertheless, much material of interest to the knowledgeable enthusiast, and the terms non-technical and semitechnical, often used by the author, should be liberally interpreted. The field covered is wide-literally all aspects of sound reproduction not dealt with in greater detail in the author's other books on "Loudspeakers" and "Ampiifiers"-and this third edition has been brought up to date by extensive revision of the original text and by the addition of eight new chapters.

Mr. Briggs has been fortunate in his collaborators and the chapter on vented (reflex) cabinets by R. E. Cooke is probably the best exposition of the underlying principles so far published. This is backed by tables giving specific recommendations for cabinet dimensions to suit typical sizes of loudspeaker and cone resonances. R. L. West and S. Kelly contribute new material on the design of pickups, and the practical aspects of successful magnetic tape recording are ably dealt with by C. H. Banks and L. J. Bradley. The chapter on cross-over networks is detailed and contains much useful coil-winding data, together with some concrete facts about phase shifts near the cross-over frequency-hitherto a somewhat nebulous bogy.

Mr. Briggs is an indefatigable experimenter and he has photographed countless cathode-ray oscillograms to verify the axiomatic as well as to illuminate the controversial in his search for better quality of reproduction. His conciusions are generally sound, but occasionally hasty as when he states (p. 37) that there is no "vibration" at the mouth of a quarter-wave pipe. A "velocity" instead of a "pressure" microphone would have given quite a different picture. There is also some confusion of thought on the role of density, Young's modulus and viscosity sic of materials involved in the production and transmission of sounds. Weight rather than density (p. 102) is the criterion for confining low-frequency sounds, and a high Young's modulus is not a necessity for producing high frequencies as his "odd man out" example of hand clapping (p. 183) secms to prove.

Whether one is learning from or disagreeing with the author-and no one interested in sound reproduction can fail to do both-there is little fear of falling asleep while reading this book.
F. L. D.

# Proposed Television Stations 

Plans for British Two-programme Service

0N July 1st the Stockholm Plans for broadcasting in bands 41-68, 87.5-100 and $174-216 \mathrm{Mc} / \mathrm{s}$, which were signed on June 30 th last year, officially come into force. So far as this country (which was among the 21 signatories) is concerned, the signature is effective only for Band I. The British delegation would not commit this country to the plans for Bands II and III until it had been finally decided by the Government whether a.m. or f.m. was to be used for the sound service in Band II and also precisely how Band III was to be used. The Atlantic City Convention (1947), which allocated frequencics en bloc to the various services, contains a footnote permitting the U.K. to use Band III for other than broadcasting; actually for point-to-point communication ( $174-200 \mathrm{Mc} / \mathrm{s}$ ) and air navigational aids ( $200-216 \mathrm{Mc} / \mathrm{s}$ ).
Provision is made in the Stockholm Plans for 40 television stations in this country-12 in Band I (including the existing and projected 10 stations) and 28 in Band III. In view of the recent statement by Sir Ian Jacob, director-general of the B.B.C., that the Corporation hopes to erect 10 lowpower stations when the present scheme is completed, we give below a list of the 30 additional British stations provided for in the Stockholm Plans.
It must, of course, be pointed out that this list, which provides for a dual service for the whole country, was drawn up before any decision had been reached regarding sponsored television.

| Vision <br> (Mc/s) | Sound <br> (Mc/s) | Station | E.R.P.* (kW) |  | Polariz ation |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Vision | Sound |  |
| BAND I |  | Isle of Man Channel Islands | 255 | $\begin{aligned} & 6 \\ & 1.25 \end{aligned}$ | $\begin{aligned} & \mathrm{H} \\ & \mathrm{H} \end{aligned}$ |
| 61.75 | 58.25 |  |  |  |  |
|  |  |  |  |  |  |
| BAND III |  | Channel Islands <br> London <br> Pontop Pike | 20050 | 1.255012 | H |
| 179.75 | 176.25 |  |  |  |  |
|  |  |  |  |  |  |
| 184.75 | 181.25 | Aberdeen Holme Moss South Devon | $\begin{array}{r} 50 \\ 200 \\ 50 \end{array}$ | 1250 | HVH |
|  |  |  |  |  |  |
|  |  |  |  | 12 | H |
| 189.75 | 186.25 | Kirk o' Shotts Norfolk North Wales | $\begin{array}{r} 200 \\ 50 \\ 50 \end{array}$ | 501212 | VV |
|  |  |  |  |  |  |
|  |  |  |  |  | H |
| 194.75 | 191.25 | Northern Ireland South East Kent Sutton Coldfield West Cornwall | $\begin{array}{r} 50 \\ 50 \\ 200 \\ 50 \end{array}$ | 12125012 | $\begin{aligned} & \mathrm{H} \\ & \mathrm{~V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| 199.75 | 196.25 | Cumberland Wenvoe | $\begin{array}{r} 50 \\ 200 \end{array}$ | 1250 | $\stackrel{\mathrm{H}}{\mathrm{V}}$ |
|  |  |  |  |  |  |
| 204.75 | 201.25 | Isle of Man <br> Isle of Wight Londonderry North Scotland West Wales | $\begin{aligned} & 50 \\ & 50 \\ & 50 \\ & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \\ & 12 \\ & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{H} \\ & \mathrm{~V} \\ & \mathrm{H} \end{aligned}$ |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| 209.75 | 206.25 | Cumberland South East Kent West Wales | $\begin{array}{r} 50 \\ 5 \\ 50 \end{array}$ | $\begin{aligned} & 12 \\ & 1.25 \\ & 12 \end{aligned}$ | $\begin{aligned} & \mathrm{H} \\ & \mathrm{~V} \\ & \mathrm{H} \end{aligned}$ |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
| 214.75 | 211.25 | Londonderry Norfolk North Scotland North Wales West Cornwall | $\begin{aligned} & 50 \\ & 50 \\ & 50 \\ & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \\ & 12 \\ & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & \mathrm{H} \\ & \mathrm{~V} \\ & \mathrm{H} \\ & \mathrm{H} \\ & \mathrm{~V} \end{aligned}$ |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

* Effective radiated power.
H. Horizontal.

V, Vertical.

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# RANDOM RADIATIONS 

By "DIALLIST"

## The Components Show

That such numbers of visitors should have made special journeys to the Components Show from twentyone countries is an outsize feather in the cap of the R.E.C.M.F. This year there were more of them than ever. How important the exhibition has become in the eyes of the world may be gathered from the fact that not a few technical journals in other countries didn't just send reporters: their editors came themselves. Two whom I was delighted to meet (and who expressed unbounded admiration for what they had seen) were the editor of Audio Engineering from America and the editor of Toute la Radio from France. There were buyers, manufacturers, journalists. and others from all over the Empire, and from many countries in Western Europe, Asia, America and Africa. It is indeed a tribute to British components that so many people should find it well worth while to make long journeys to attend this small, private, three-day exhibition. The R.E.C.M.F. has been wise in adopting and adhering to the world's strictest and most rigid standards in materials, design and workmanship. Quality pays-and goes on paying.

## Striving for Inefficiency

So powerful are the a.m. and f.m. signals that I receive from the $20-\mathrm{kW}$ Wrotham transmitter at a range of 50 miles with a pukka dipole mounted on a chimney stack, that I've been trying out aerials of lower and lower electrical efficiency with a view to discovering how far one can go before any marked falling off occurs. The arrangement I'm using at the moment cost 1 s 8 d , including the feeder. It consists of four yards of PVC-covered flex, the last $2 \frac{1}{2} \mathrm{ft}$ of which were untwisted and straightened out, the single wires being stapled to right and left along a picture rail 8ft above the floor of a ground-floor room. Signal strength is still so ample that I shall have to work out something a good deal less effective before the answer is found. Metre-wave broadcasting when it comes (and may that be soon!) looks like having very great advantages over medium- and long-wave transmission. Among these, if f.m. is
selected, are: (1) coverage of the same service area with about a quarter of the transmitter output power; ( 2 ) excellent reception (except in fringe areas) with the simplest and cheapest of indoor aerials; (3) far greater freedom from background hiss and impulsive interference; and (4) much better quality.

## A Nice Point

Settle a couple of wireless enthusiasts into comfortable armchairs of an evening and it won't be long before they start an argument on one of the finer points of their pet subject. Man has probably been an argumentative animal ever since he found out how to use speech to convey his thoughts and ideas to others. Our discussions and debates to-day carry on his age-old attempt to arrive at the truth about this or that. On a recent chilly evening a friend and I got on to the subject of valves as we basked in the warmth of a welcome fire. He's a bit of an authority on matters wireless; but I had to take him up when he described the thermionic valve as basically a voltage amplifier. His thesis was that voltage changes applied to the grid give rise to similar but much larger changes at the anode when a load is provided. By choosing the kind of anode load suitable for the work in
hand you can pass these voltages on to another valve; or, you can use them as e.m.f.'s to drive current through a power-operated device such as a loudspeaker. I hold that the valve is essentially a power amplifier. There must be some resistance in the grid circuit and you can't get away from the fact that $V^{2} / R=$ W, however small the figures may be. An amplified copy of these small applied powers appears in the anode circuit and you can use it as suits your purpose by selecting the right kind of anode load. I firmly believe that that is the best way of picturing the working of an amplifying valve. What are your views?

## Room for Improvement

Sorry though I am to have to say it, there cannot be much doubt that too many of the h.t. batteries available nowadays are pretty poor things. I am thinking particularly of those made up of $\frac{3}{4}$ in $\times 2 \frac{1}{8}$ in cells, for they are by far the most widely used; but my criticisms apply equally to those with larger and smaller cells. If you care to work it out from the electrochemical equivalent of zinc, you'll find that a $\frac{3}{4} \mathrm{in} \times 2 \frac{1}{8} \mathrm{in}$ can, weighing about 12 grams, has, in theory, a possible current output of 10 Ah . Of course, you cannot expect to get anything like that from it since the cell is usually discarded when the e.m.f. has fallen from 1.5 V to 0.9 V . Still, with a load of $8-10 \mathrm{~mA}$ you should justifiably hope for a good bit more than the 0.7 Ah to 1.1 Ah that is all that I've been able to obtain of late from h.t. batteries with cells of this

size. Again and again the overall e.m.f. of a battery has become unsteady after far too short a period of intermittent use. Once that happens, the set becomes increasingly noisy for an hour or two, and then packs up altogether. Test the battery with a high-resistance voltmeter and you'll find only tiny fractions of their stated c.m.f.s between certain tappingsusually near the middle. I have conducted post-mortems on scores of such batteries and have found in each case one or more perforated cells. Cell-perforation after a short period of intermittent use under a moderate load is something which, in my opinion, should not occur in a well-designed and well-made dry battery.

## Full Speed Ahead

Towards the end of March an American friend asked me in one of his letters whether the imminence of the Coronation was producing record sales of television receivers. I replied that sales weren't too bad, except in Scotland, where comparatively few sets were being sold. "Possibly," I added, "the hardheaded Scots are holding their hands in the hope that the Budget will bring a reduction in purchase tax. If so, they are likely to be disappointed." My prediction could not have been more erroneous and I'm very glad of that. The reduced tax will mean bigger sales everywhere and, therefore, more money for research and development. It isn't always realized that television has had a hard battle to fight in this country. Our television service, the first in the world, was just getting nicely into its stride when the outbreak of war closed it down in the autumn of 1939. The TV research men were mobilized as the "backroom boys" of radar and had, so to speak, to beat their viewing screens into p.p.i. diṣplays. Then when the war was over shortages of men, money and materials prevented the rapid development of our national television system. The heavy purchase tax imposed on receiving sets led inevitably to restricted sales and meant that with us television had to amble, instead of galloping, into its rightful position as the best of all sources of domestic entertainment. With the lowering of the tax, this Coronation year may well see a boom in television comparable with that which occurred in the early nineteen-twenties in " sound" radio.

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| S.530/A <br> $5.531 / \mathrm{A}$ | 25-35 35-50 <br> 50-100 | $\begin{gathered} \mathrm{At} 125 \mathrm{~V} . \\ =3.0 \mathrm{~A} . \\ \text { and at } \\ 250 \mathrm{~V} \\ =1.5 \mathrm{~A} \\ (\mathrm{~A} . \mathrm{C} .50 \sim) \end{gathered}$ | S.530/B S.531/B <br> S.532/B | $\begin{aligned} & 25-35 \\ & 35-50 \end{aligned}$ <br> 50-100 | $\begin{gathered} \text { At } 125 \mathrm{~V} \\ =3.0 \mathrm{~A} . \\ \text { and at } \\ 250 \mathrm{~V} . \\ =1.5 \mathrm{~A} . \\ \text { (A.C. } 50 \sim \end{gathered}$ |

* = Surge-current (as from back-E.M.F., etc.) if greater than steady current of eireuit. Switching-on surge, if any, should not exceed rating x 1.5 max. value, for longest life.

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## UNBIASED

## Forestalling the Future?

WHEN our descendants celebrate the Queen's Golden Jubilce fortynine years hence, the newspapers will doubtless publish many articles dealing with various aspects of life in England during the early years of her reign. Our descendants are bound to be struck forcibly by the amazingly primitive and comfortless

condition in which we were content to live having regard to the degree of scientific knowledge attained.

I think that one of the things at which the people of the year 2002 will marvel most will be that we early Elizabethans of 1952 could make an atom bomb but failed to use the resources of radio to enable us to maintain communications with the rest of the world when journeying by land. The provision of radio-telephonic facilities on trains and other public vehicles, although technically possible is, I suppose, banned by bureaucrats. This is, however, equally true of private cars, for the P.M.G. has never bothered to equip each telephone exchange with v.h.f. radio apparatus so that car owners, who installed the necessary equipment, could be linked with the national telephone system while travelling.

It is, however, a strange thing that if you own a boat and take your pleasure in it anywhere in the Thames Estuary the P.M.G. does provide a specially equipped telephone exchange for you so that you are as much "on the phone" as if you were at home. Recently I was visiting a friend who, like others of his kind, enjoys himself by spending his weekends on a small but well-equipped sailing craft.

I congratulated him on being "on the phone" in this special manner and said I wondered that he and others like him were not tempted, when temporarily abandoning ship
on Monday mornings, to transfer the radio gear to their cars.

No reply was made to my observation but I did reccive from my friend rather a queer look which might have been meant for silent reproof at my harbouring such subversive ideas; on the contrary, it might have been meant for withering contempt at my lack of sophistication. I just don't know. I merely record the facts and leave you to draw your own conclusions.

## Silent TV

I WAS greatly interested in "Diallist's" prediction in the May issue that sets of the future may be provided with a three-position switch: sound and vision; vision only; sound only. But I certainly do not agree with him that more often than not the switch will be turned to the "sound-only" position. On the contrary, I think that if such a switch be provided it will almost invariably be turned to " vision only," and eventually the B.B.C. will radiate only silent TV.

I am led to this conclusion by the fact that owing to the development of a fault (which I have not yet found time to trace) in the "sound" side of my television set I have lately been looking at silent TV. As a result I have become quite expert at lip reading. I can, in fact, follow the dialogue by this means far more easily than I could when I had to rely on my ears, as the sound was so often rendered unintelligible by the ceaseless chatter of Mrs. Free Grid and her fellow females discussing the shortcomings of their respective husbands.

Even when I have the house to myself the peace and enjoyment of watching this silent TV has to be experienced to be believed. It does mean, of course, that I have to give the programme full concentration if it is to be intelligible, but this is as it should be. I have no more patience with people who use sound broadcasting as a sort of soporific background to their other activities than I have with those who go to the cinema and divide their attention between the screen and their own amateurish imitations of the amatory activities displayed on it. In common fairness, however, I must add that there is some excuse for their use of the cinema as an osculatorium as the proprietors fail to provide what used to be known in the U.S.A. as "necking niches" for those who don't want to see the film.

## Inter-departmental Quiz

ANYTHING that smacks of the Totalitarian Police State is anathema to me. I must, therefore, register a very strong protest at the P.M.G.'s attempt to get the myrmidons of the Ministry of Transport to act as his Gestapo.
The current form which we all have to fill up when we want to renew our car licence asks bluntly "Is, the vehicle fitted with a radio set?" If the answer is "Yes" we have to answer a further question which asks us if the set is separately licensed. These questions are, in my opinion, wholly irrelevant to the licensing of a car.
I presume that if the wretched motorist answers "No" to the question which asks him if the set is licensed, the information will be passed on to the P.M.G. Supposing the motorist declines to answer this question on the grounds that no man is compelled to answer a question which might incriminate him, I wonder if the authorities would refuse to issue him a Road Fund licence? I wonder, too, whether the police have instructions and the necessary authority to ask about the licensing of any set they may see


Decibelless dialogue.
installed in the car when taking particulars for some misdemenour?

This sort of inter-departmental quiz is probably reciprocal and there is a danger that before long, when buying a radio licence at the local Post Office we may be asked if we have a clean driving licence. When applying for a marriage licence the bridegroom may, one day, be asked offensive questions about his income-at present the prerogative of the intended bride's father.

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ete., which have been imported ete., which have been imported
into this Country. Names include into this Country. Names include
Sparton, Emmerson. Admiral, Crossley, R.C.A. Victor etc. Each sheet gives circuit diagrams and component values alignment procedure, etc., etc. Price for the folder of 100 sheets is $\$ 1$. Post frec.

## FRE T.V. SERVICE

 SHEETSThe supplement to a new publication "Television Faults" contains complete circuit diagrams, component values, technical descriptions etc., of 6 popular T.V. receivers as follows:

Baird Everyman, T.29; Murphy, V.120C; English Electric, 1150 M ; Philips projection model 704A and 1800; Marconi, VT.53DA; Ultra V.711.
The book itself in the introductory chapter tabulates over 60 common faults from complete common faults from complete shadows in the corner. Against shadows in the corner. Against each fault symptom is given
probable causes and a reference probable causes and a reference
to the part of the book where to the part of the book where
more detailed information can be found. Following the quick fault finding guide are 10 chapters, each giving typical circuits and data indicating the actual components likely to be at fault. The book is invaluable to novice and experienced T.V. serviceman alike because it contains a wealth of practical experience and priced at only 5/- it will undoubtedly save its cost the first time you save to cofer to 1 Order now have to refer to it. Order now to
ensure getting the free suppleensure
ment.

## THE ELPREQER

This describes a completely effective but most inexpensive Signal Tracer that can be built in one hour at a total cost of $12 / 6$. Price $1 / 6$.
FOR VIBRATOR UNIT RECEIVERS
Describes how an inexpensive unit, which will save its cost many times over, can be built and operated. Price $2 / 6$. With Blueprint.

A VIBRATOR UNIT FOR 1.4 VOLT BATTERY RECEIVERS
Shows how to make a unit which will permit you to dispense with expensive dry batteries. You can work your little set from a 2 volt accumulator which can be re charged. Price 2/6 with blueprint.

## FOR OUTSTANDING PERFORMANCE

Model B. Six Wavebands 11-15 metres continuoua in 5 ranges (4 Bandspread) and M. W. 185-550 metres. Six position Tone Switch (3 Radio $\rightarrow 3$ Gram). Price $£ 15 / 15 /$-, plus $7 / 6$ carr. and insurance, or H.P. terms $55 / 9 /$ - deposit Model B3. Three waveband, Long, Medium, Short, Gram switching on wave change switch. 3 position Tone. Price $£ 12 / 12 /=$, plus $7 / 6$ carr and insurance, or H.P. terms
 \&4/6/=deposit.
Both chassis 11 it $\times 7$ in $\times 8 \mathrm{in}$, high, Latest type valves: 6BE6, 6BA6, $6 \mathrm{AT} 7,6 \mathrm{BW} 6,6 \mathrm{X} 4$. $\times$ A.C. mains operated, fyywheel euning, negative feedback over entire audio section, engraved knobs, fully negative fe

BUILT TO HIGHEST PERFORMANCE STANDARD AND SPECIFICATION
7 VALVE 5 WAVEBAND RADIO CHASSIS


## GIVE AWAY PRICE

## only

 47/deposit.Less valves and power pack.

A famous set by a famous manufacturer. Undoubtedly a serious listener's receiver. Among many special features are an H.F. stage and tuning indicator. Tunes up to 11 metre band. Price complete with valves but less speaker, $£ 14 / 19 / 6$. H.P. terms $55 / 10 /=$ deposit and 12 monthly payments of $£ 1 / 10 /-$
We have a few left, less valves and power pack, otherwise in good condition; they definitely have never been used. Price £6/19/6, or £2/7/- deposit and 11 monthly payments of $10 / 9$, plus $15 /$ - carriage.


## 5-VALVE I.F。/A.F. AMPLIFIER

(For A.C./D.C. working) This is on an aluminium chassis, size $11 \frac{1}{2} \mathrm{in} . \times 7 \mathrm{in}, \times 3 \mathrm{in}$. deep The layout is neat and simple and provision is made and in fact holes are drilled so that tuning condenser and coil pack may be easily fitted if same may be easily fitted ifnatively are required. Alternatively for mounting a control panel to which various points of the circuit can be brought to plugs, thus making a signal tracer which is invaluable for radio and T.V. servicing. It uses one of the latest valve line-ups, as follows: 1457 Triode Hexode, 7B7 I.F. Amplifier, 7C6 D.D.T., 35 A 5 output, 3523 Rectifier. The I.F.s are present at $465 \mathrm{kc} / \mathrm{s}$., but are variable over a fairly wide range. Price $£ 6 / 10 /$ - complete with valves and 8 in. speaker. H.P. is $63 /=$ deposit.
R1155 COMMUNICATION RECEIVER FOR ONLY £2/14/=


## DEPOSIT

This set, as most will know, is considered to be one of the finest communications ble to-day The able to-day. The is 75 racy range is $75 \mathrm{kc} / \mathrm{s}$ to 18 $\mathrm{Mc} / \mathrm{s}$. It is complete with 10 valves and is fitted in a black metal case. Made for the R.A.F.; so obviously a robust receiver which will give years of service. Slightly used but completely overbauled and guaranteed in perfect working order. PRICE £7/19/6 or will be sent against a deposit of £2/14/balance of 12 monthly payments of 11/6. If you cannot call to collect please include an additional $10 /$ to cover cost of transit and carriage. This partly returnable to you if and when you return the transit case.

## MAINS POWER PACK FOR R. 1155

With Pentode output stage. Plugs into socket on receiver so no internal modifications are required. Price $55 / 10 /=$ complete with 5 in internal modifications are required.
speaker ready to work, carriage $3 / 6$.

BOOKS \& PUBLICATIONS

"DEMOBBED VALVES."
Gives the commercial equivalents of many thousands of service valves, and conversely gives the service equivalent of many thousands of commercial type valves, an invaluable publication valves, an invaluabie pubieation
recently revised.
"AN ELECTRONIC TIMER." Shows how to build a device for controlling timed operations. The timer can be set to any timing up to 3 minutes. Price 2/3. "THE ELECTRONIC SWITCH." Shows how to make a device for switching without mechanical contact Price 2/3.; "THE IMPULSE RELAY." Explains the working of an ingenious relay, and gives several circuits including radio control. Price $1 / 9$.
"THE OCCASIONAL T.R.F."" Shows how to build a T.R.F. Receiver for medium and long wave reception, of looks and quality output comparable with sets priced between $£ 10$ and $£ 14$. This costs less than $f 6$ to build including cabinet. Price 1/6.
"VALVE EQUIVALENTS." These are the best equivalents charts available today. Also the booklet can be used for keeping records of valve stocks. Price 2/6. VISUAL ALIGNMENT SIGNAL GENERATOR. Reprint from " Radio Constructor " describes a very useful combined signal generator and oscilloscope. 9 d .
RADIO HEARING AIDER
The world for a deaf person must be particularly blank and monotonous, and a hearing aid which will function as a radio when not needed for hearing should help considerably. Constructional data and technical notes dealing with this are available. Price $2 / 6$. Only standard parts are incorporated therefore the constructor will have no difficulty in making this up.
1.F. ALIGNMENT PEAKS

This book gives the I.F. frequen cies of more than 4,700 receivers including British, American and Continental types. Every popular British set is covered, and in addition hints on finding the frequencies of unknown British sets are also given. Sale price 3/9.

EX-GOVT. CIRCUTS
These give circuit diagrams and details of Ex-Government receivers and equipment In practically all cases the information has been extracted from official publications.

## AR.88D Ind. 62

## Ind. 62

A. 1368 Ind. 6 K Ind. 62 A
A. 1368

AN/APAl
R. 76
R. 78

| A.S.B. 3 | R. 103 |
| :--- | :--- |

BC. 221 R. 107
BC. 312
${ }_{\mathrm{BC}} \mathrm{C} 342$
BC. 348
BC. 453
BC. 453
BC. 4545
BC. .624
BC. 625 A
BC. 433 G
BC. 1206
I.F.F.
I.F.F.
R. 1355
R.F. 24
R.F. 25
R.F. 26
R.F. 27
R.F. 27

R28/ SCR269A SCR522 T. 1154
TR 1196 TR. 18 All 1/6 each or assorted
dozen os

## ELECTRONIC PRECISION EQUIPMENT LTD.

## TOOLS, ETC.

" Q-MAX " CHASSIS CUTTERS.
The simplest and quickest tool for cutting holes in aluminium or steel chassis. Comprises die and steench operated by Allen key. punch operated by Allen key. A separate die and
required for each size.
$\frac{s^{*}}{}{ }^{*}$ hole (B7G, etc.)
11/6
名" hole (B8A, etc.) ...... . . $11 / 6$
** hole ................ $12 / 6$ 10 d .
$1^{*}$ hole
$1{ }^{1}{ }^{\text {N }}$ hole hole (Octal base) ..... 14/9
$1{ }^{*}$ " hole (English bases)
18" $^{\prime \prime}$. hole
14/9
15 hole (EF50, etc.).
16/6
$1 \mathbf{8}^{*}$ hole
16/6
$2^{2} 3 / 32^{\prime \prime}$ hole
18/6
21 hole ................... 35/-
$1 \times 1^{*}$ square hole...... 23/-
Same key fits these nine, price 1/3.

## METAL DIVIDERS.



Really well made for Government workshops. Ideal for marking out on metal chassis. Price $3 / 6$.

## HARMONIC GENERATOR

A harmonic generator is well worth making up, because it oscillates with a wave form having harmonics extending right into the radio frequencies. To trim s straight set therefore it is only necessary to inject its output into the aerial and adjust trimmers for maximum audio output, similarly with a superhet a great saving of with a superhet a gre
time can be effected.
time can be effected. as a kit of
We will supply this as We will supply this as a kit of
parts, with constructional details price 15/- for battery, and 30/for mains operation ; data available separately, price $1 / 6$.

## SPRING <br> TERMINAI BLOCK Fully insula-

 ted so is ideal for mains,

## terminal point

fitted on bench of workshop or laboratory. Also suitable for temporary hook ups when testing comporary hook etc., will save its cost the first week of use. Price cost
$3 / 6$.


SPRAY GUN
Hand orerated, ideal to put a good finish on a completed chassis, and for respraying valves etc. (completes the perfect job) Price $15 / 6$ complete with atructions, plus 9d. postage.


BULLD AN OUTPUT METER Switch, Transformer, meter and rectifier to build a dual range O.P Meter with instructions. E1/15/-.

## LOW PRICED TEST GEAR, ETC.

## T.V. SIGNAL AND PATTERN GENERATOR

Cost of all components, valves, etc., only 29/6.
Although this generator can be built and used by any beginner it is at the same time a most useful instrument for the more advanced worker.
It can be tuned to the vision channel and will produce a pattern on the face of the C.R. tube. Alternatively if tuned to the sound channel it will produce an audible ignal in the loudspeaker.
Thus its owner will become independent of B.B.C. transmissions and can fault-find or test at any time. It operates entirely from A.C. mains and is quite suitable for use with superhet or straight receivers.
A complete kit of parts (in fact
 everything except the cabinet
with onala buy the kit later). buy the kit later).
NOTE. Cabinets as per the illustrated prototype are available price 17/6

## VISUAL ALIGNMENT

SIGNAL GENERATOR.
An interesting article in the
October Radio Constructor described an instrument which is a combination oscilloscope and signal generator. It is designed to generate a signal into a superhet then permit visual inspection
of same signal after passing through the superhet. The article further shows how the instrument could be made for the very low price of $£ 5$
This uses a small tube and is quite a compact instrument, so if it's only use is that of checking the band pass on the 1.F. transformers, in a high fidelity receiver, its construction is justified. It can, of course, be used for a variety of different jobs other than the alignment of I.F.'s, in fact, it is a good servicing 'scope.

We can supply a complete kit of parts for $£ 5$ containing valves, tube and all components except shassis and case. A re-print of the article and all components except shassis and case. A
from the Radio Constructor is available price 9 d .
from the Radio Constructor is available price 9d.
The power pack not shown on the block diagram is, nevertheless, included in the kit.

## CONTINUOUSLY VARIABLE MAINS TRANSFORMER

As described in the " Wireless World," August 1951 issue, this has a primary tapped at 81 v . and four secondaries of $1 \mathrm{v} ., 3 \mathrm{v}$. , 9 v . and 27 v . respectively.
By suitable selection of windings, voltage in steps of 1 v . up to 40 v . can be obtained with isolation from the mains at 100 watt rating, e.g., 20 amps at 5 v . and $2 \frac{1}{2} \mathrm{amps}$ at 40 v . By adding the primary the voltage can be varied in steps of 1 v . up to 280 v . This is undoubtedly an essential piece of equipment in all experimental laboratories. Price $£ 3 / 10 /$ e each.


TRIMMER TOOL KIT.
Invaluable for aligning radio or T.V. sets. Kit comprises: 10 precision tools set in polished ebonite and each tool has been carefully designed with the minimum of metal to avoid upsetting the circuits being aligned. There are ten tools comprising

4 box spanners
3 screw drivers
and 3 special tools.
All packed in strong folding case. Price 35/m complete.

## WELD TYPE WIRE JOINTER

This jointer melts the wires and causes the metal of each to run together, thus making a strong and permanent weld. It obviously is not intended to replace the soldering iron but nevertheless is ideal for making joints that have, for instance, to withstand heat, vibration, chemical action, etc. In many cases also this method is faster than soldering and there can be a considerable saving of current. Price $9 / 6$. Or complete with enclosed mains transformer 29/6.

## SUNDRIES

SPINDLE EXTENDERS \& COUPLINGS
Small type. Solid Brass
 with type. Solid Brass 7 d . each. d. each. Fexible Type. These so insulate, $2 /$ - each Ordinary Insulated. These have additional spindle moulded permanently and they extend the control spindle by 1-1 $\frac{1}{2}$. $1 / 6$ each.
Bellows Coupling. These are ideal for slug tuning as they extend as well as bend. $1 / 9$ each.


CLEAR CEMENT.
Almost instantaneous drying for coil winding and all repairs, $1 / 6$ per tube.

# HARD <br> WARE. <br> Service <br> man's 3 <br> gross asorted nuis 


bolts and washers
all useful sizes. all useful sizes. Price 6/6. We endeavour to maintain stocks of wood screws, steel and brass round head and counter sunk Parker Kalon self cutting screws, washers and studding. Send us your orders and enquiries.

## RUBBER GROMMETS


Serviceman's packet of 24 assorted sizes, $2 /-$.

## CROCODILE CLIPS

Small instrument, 6d. Large Car Battery type, 9d.


TERMINAL BI.OCKS
Heavy duty type, 5 way 4 in . long $x 1$ in. wide $x$ $1 \frac{1}{4}$ in. high. 30 amp. rating. Price $1 / 6$. Heavy Duty type, 6 way porcelain 15 amp. rating. Price 1/6. Heavy Duty type, 5 way porcelain 15 amp. rating. Price 1/3.
Heavy Duty type, 3 way porcelain 15 amp. rating. Price 9d.

## OCTOPUS CLIPS



An ideal clip for fixing anything to a rod or pole, this is self adjusting from $1 \frac{1}{2}$ in. to $4 \frac{1}{2}$ in. Price 1/- each.

## MILLIBAR

BARO-
METER, 7/6
The heart of a barometer is a metal bellows which will ex pand and con

ract with the varying air pressure The aircraft altimeter works on the same principle, a series of gears and lever amplifying the expansion and contraction of the bellows and so works the pointer. We can offer the ex-R.A.F. Sensitive Altimeter slightly faulty bensitive Altimeter containing the essential bellows, gears, wheels, etc., from which a good barometer can be made. Price only $7 / 6$, plus $1 /=$ post.

## ELECTRONIC PRECISION EQUIPMENT LTD

ELECTRICAL BARGAINS In addition to our large range of radio accessories we also carry a good stock of electrical wiring accessories; details of a few of these can be found below:-
T.R.S. CABLES. 250 v. CLASS 1/.044 Twin flat
3/.029 Twin flat
3/.029 Twin with earth
$3 / .0203$ Core flat
3/.036 Twin flat
3/.036 Twin with earth
3/.0363 core flat
7/.029 Twin fla
7/.029 Twin with earth
7/.036 Twin flat
7/.036 Twin with earth
7/.064 Twin flat
LEAD COVERED CABLES 250 v. CLASS

$\underset{2 / 3}{\text { yard }}$

## WAR EMERGENCY TYPE

CABLES 250 v. CLASS
These are P.V.C. or rubber in-
yard
2/-
$2 /-$
$3 / 3$
MULTICORED FLEXIBLES All are suitable for mains work as well insulated, then they covered overall either with hard rubber, plastic or waterproof braiding :-

1/-
5 AMP SURFACE -HICRAFT Plastic 1-way $1 / 3$ each Oblong White Plastic 1-way, $1 / 3$ each.
Oblong Brown 2-way
Oblong White 2 -way Round Brown 1-way Round White 1 -way Round Brown 2-way Round White 2-way $1 / 6$,
$1 / 3$, 1/6,

## SPECIAL THIS MONTH

 Customers ordering quantities of bakelite accessories can take discounts as follows 1 dozen of one item $25 \%$ 1 gross mixed or one item $334 \%$.

CEILING SWITCHES HICRAFT
With cordand acorn. Brown or acorn.
White,
I-way,
$3 / 9$ cach; 2 -way, $4 / 3$ each.

## LAMP HOLDERS

Bakelite, 1/- each or $10 / 6$ doz. Bakelite skirted Batten holder, 1/6 or 15/- doz.
Bakelite type threaded for 8 in . Bakelite type threa
with HO skirt, $1 / 6$.
10 per cent. discount if bought 10 per cen
in dozens.

## BARGAIN FOR CONSTRUCTORS

Special this month is the Portable illustrated alongside. We offer a bakelite cabinet with carrying handle, metal chassis, battery housing and two waveband dial, all for 27/6, plus 5/-carr. and insurance. This cabinet and set of parts is ideal for making up either an all dry battery receiver for holidays, picnics, etc., or a battery mains set for everyday use. Constructional details of two suitable circuits using 1.5 v . valves 1R5, etc., will be given free with cabinet assembly, or is available separately price $1 / 6$ post free.

SPECIAL RADIOGRAM OFFER
To those who want an auto radiogram at a low price, we offer the cabinet illustrated alongside complete with Collaro three speed record changer with dual purpose crystal pick up, at a special bargain price of $£ 17 / 16 / 8$, plus 12/6 carriage and insurance or H.P. terms £6/7/- deposit

3 colour scale, scale pan, chassis, pulley, drivinig head, springs, etc., etc., to suit the radiogram and two radio cabinets are available as a parce. at $15 /-$, plus $1 / 6$ post.

Cabinet separately $£ 7 / 10 /$ - (or £2/10/- deposit), plus 10/- carriage and insurance.


A Superhet Chassis to fit these two cabinets is now available. L.M. and S. waves, 3 colour scale, A.V.C. Tone control etc., complete with 8 in. P.M. Speaker. Price £9/19/6 or H.P. £ $3 / 7 /$ - deposit. Carriage $7 / 6$ extra.

## TABLE MODEL RADIO

 This very nice-looking cabinet will take the same scale and chassis as the radiogram above, and we are able to offer this at the bargain price of 37/6, plus $3 / 6$ post and insurance.
## THE REGINA

T.V. Console Cabinet, undrilled, but cut for 12 in . tube, with adjustable platform. This cabinet looks really superior and is ideal for all popular sets-Viewmaster, Tele-King, etc. Price $\Sigma 7 / 17 / 6$. Carriage $10 /=$ extra.

The table mode illustrated is avail able in fair quantity at $£ 3 / 17 / 6$, plus $7 / 6$ carriage and insurance which price includes the armour
 plate glass and surround.
Mechanical details for this Table Model are available as a parcel Punched and prepared metal chassis, punched outrigger valve plate with spacers, 12 in . Tube Clamping ring, tube rear support brackets, etc. Price $25 /-$, plus $2 / 6$ post.

" MIDGETRONIC" Radio Cabinet
This pleasing small cabinet is in bakelite and is supplied complete with dial ring, pointer as illustrated but less knobs, also included is metal chassis and hardboard back. Price 15/-, plus 2/6 postage and packing.

To ensure receiving prompt reply, please enclose stamped addressed envelope, when writing for additional details.

ELECTROLYTIC CONDENSERS


1 mfd .150 v.
1 mfd .250 v .
1 mfd .450 v .
2 mfd .350 v.
2 mfd .450 v.
4 mfd .350 v .
4 mfd .450 v .
8 mfd .150 v
8 mfd .350 v .
8 mfd .450 v .
8 mfd .500 v
8 mfd. 500 v . centre-screw
fixing 600 .................
mid.
fixing
16 mfd .350 v .
16 mfd .450 v
16 mfd .500 v .
32 mfd .150 v .
32 mfd .250 v
32 mfd .350 v
$8 \mathrm{mfd} \times 8 \mathrm{mfd}$.
$8 \mathrm{mfd} . \times 8 \mathrm{mfd} .450 \mathrm{v}$
$8 \mathrm{mfd} . \times 8 \mathrm{mfd} .500 \mathrm{v}$.
$8 \mathrm{mfd} . \times 16 \mathrm{mfd} .450 \mathrm{v}$
$8 \mathrm{mfd} . \times 16 \mathrm{mfd} .500 \mathrm{v}$.
$16 \mathrm{mfd} . \times 16 \mathrm{mfc} .450 \mathrm{v}$.
$16 \mathrm{mfd} . \times 16 \mathrm{mfd}, 500 \mathrm{v}$.
$20 \mathrm{mfd} . \times 20 \mathrm{mfd} .200 \mathrm{v}$.
$24 \mathrm{mfd} . \times 24 \mathrm{mfd} .200 \mathrm{v}$
$25 \mathrm{mfd} . \times 25 \mathrm{mfd} .200 \mathrm{v}$.
$32 \mathrm{mfd} \times 25 \mathrm{mfd} .200 \mathrm{Y}$.
$32 \mathrm{mfd} \times 32 \mathrm{mfd} .450 \mathrm{v}$.
$100 \mathrm{mfd} \times 100 \mathrm{mfd} \mathbf{v}$.
$100 \mathrm{mfd} .25100 \mathrm{mfd} .150 \mathrm{v} .5 / 6$
10 mrd .25 v.
12 mad. 50 v .
20 mfd .50 v.
25 mfd .50 v
50 mfd .12 v .
50 mfd .50 v
250 mfd .12 v
250 mfd .25 v . .......... $2 / 6$
$8 \mathrm{mfd} . \times 8 \mathrm{mfd} \times 8 \mathrm{mfd}$.
450 v .
3/9


0005 2-GANG CONDENSER
Ceramic insulation with " no back lash " gear drive Drive easily lash gear drive. Drive easily removed if required, when conwenser becomes a standard type


Two socket engraved L.S., 6d. each. Bin. Cl6B.
Two socket engraved A.E., 6d. each. Bin. CI8A.
Two socket engraved P.U., 6d. each. Bin. C19B.
Two socket engraved Dipole 6d. each. Bin. C19B
Two socket plain, 5d. each. Bin. C18B.
Three socket engraved DIP and E, 9d. each. Bin. C16D.
Three socket engraved A1, A2 and E, 9d. each. Bin. C19D
Four socket engraved A.E. Pickup, 9d. each, Bin. C19E.
Four socket engraved P.U. Ext. L.S., 9d. each. Bin. C16E.

Five socket plain, 9d, each. Bin. CI6C.

## ELECTRONIC PRECISION EQUIPMENT LTD

RADIO HEARING AIDER
The world for a deaf person must be particularly blank and monotonous, and a hearing aid which will function as a radio when not needed for hearing should help considerably. Due to Purchase Tax no kit of parts for this will be made available, but constructional data and technical notes dealing with this are available, price $2 / 6$. Only standard parts are incorporated, therefore the constructor will have no difficulty in making this up.

HIGH VOLTAGE VALVE HOLDERS

For four or five pin valves. Price 2/9 each.

## 2 isin. TUBE MOUNTING

 This comprises metal cased moulded rubber tube mounting, front escutcheon, 4 . screws and l'erspex window with engraved cursor lines, 5/- complete.
## V.C.R. 139

Tube base with mu-metal screen, 4/6.

## MU-METAL SHIELD

For 6in. tube V.C.R.97, etc., 10/- per pair.

6in. TUBE MOUNTING Shock proof rubber mounted and adjustable, i.e., tube may be turned, with tube holder, 4/6 each.

## HIGH VOLTAGE

Insulated spindle couplers, $1 / 6$ each.


AUTO-
MATIC
STARTER
For remote control of D.C. motor between 1 and 3 kw . adiustment for 100 v . or 230 v . Unused and in first-class condition, complete with metal and wired glass cover. Price on request.

6KV. EHT FOR 35/-
6KV. R.F. EHT kit, comprises 2 valves, mains transformer, condensers, coil formers and wiring instructions. Price $35 /-$ complete. Data available separately, price 2/6.

## SPECIAL LOW PRICES

AMPLIFIER UNIT A 1134A This is a 2-stage intercom and Tx pre-amplifier with transformers, etc. Easily modified as gram etc. Easify modined or dictaphone, etc. Complete with 22 v. valves, Complete with 2 Price 2 Priode. QPP and Triode. Price only 96, pius $1 / 6$ post and packing. Circuit diagram,
or separately, $1 / 6$.
MORSE OSCILLATOR UNIT
Variable note and variable output, fitted with jack for external modulation, complete with 2 2 v , valves. Price $8 / 6$, plus $2 /-$ post and packing.

## STOP PRESS

Weymouth miniature Coil Packs at half price. Long, Medium and Short wavebands with gram position. Size, $3 \frac{1}{1 / \mathrm{in} .} \times 3 \mathrm{in} . \times 1{ }_{8}^{3} \mathrm{in}$., single hole fixing.
Limited quantity, price $22 / 6$,
plus $1 / 6$ post.
12 for $£ 12$, post free.

## RADIO DIALS AND SCALES



Note-Type A. Pointer moves from side to Type B. Pointer moves up and down. Type C. Pointer rotates centrally.
Type D. Pointer rotates in semi-circle rotates in semi-circle from bottom centre.
Minimum dial openings
are quoted to help you if you cannot find the right size listed, and the figures indicate to what size the dial could be cut down.
Post and packing charges. Owing to the fragile nature of these dials, 2/- extra must be included to cover post and packing.
Quantity Prices. Where 12 or more of one type are required discount is 25 per cent.; 144 or more, $33 \frac{1}{3}$ per cent. (there are no carriage charges on quantity orders).

| GLASS DIALS |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type | GlassSizeWide High |  | Min. Dial Opening | Wavebands | Colours | Price | List No. |
| A | $\begin{aligned} & \text { in. } \\ & \text { in } \end{aligned}$ | $\operatorname{in}_{6 \frac{1}{2}}$ | $\begin{aligned} & \text { in. in. } \\ & 8 . \end{aligned}$ |  | 4 | 3/6 | C73A |
| B | 6 | 71 | $5 \frac{1}{4} \times 6 \frac{1}{2}$ | M., S1 \& S2 | 3 | 3/6 | C74A |
| B | $4{ }^{4}$ | $11 \frac{1}{2}$ | $2 \times 6$ | L., M. \& S. | 3 | 3/6 | C77A |
| A | 13 | $3 \frac{1}{2}$ | $7 \frac{1}{2} \times 24$ | L., M. \& S. | 3 | 3/6 | C78A |
| C |  | 3 | $21 \times 3$ | L. \& M. .- | 2 | 1/6 | C81A |
| A | 8 ¢ | $5 \frac{1}{2}$ | $7 \times 4$ | L., M. \& S. | 3 | $4 / 6$ | C83A |
| B | 6 | 71 | $51 \times 5$ | L., M. \& S. | 2 | $2 / 6$ | C84A |
| B | 6 | 73 | $5 \mathrm{f} \times 5 \frac{1}{2}$ | M., S1 \& S2 | 3 | 3/6 | C85A |
| A | 9 | 73 | $6 \frac{1}{} \times 5$ | L., M. \& S. | 1 | $2 / 6$ | C88A |
| D | $6 \frac{1}{2}$ | 5 | $5 \frac{1}{2} \times 3 \frac{1}{2}$ | L. \& M. | 2 | $2 / 6$ | C89A |
| B | 7 h | 7. | $6 \times 5 \ddagger$ | L., M. \& S. | 3 | $3 / 6$ | C90A |
| D | $6 \frac{1}{2}$ | 5 | $5 \frac{1}{2} \times 3 \frac{1}{2}$ | L. \& M. ${ }^{\text {c }}$ | 1 | $2 / 6$ | C91A |
| B | $7 \frac{1}{1}$ | 7 L | $6 \times 51$ | L., M. \& S. | 3 | $3 / 6$ | C92A |
| A | 81 | 31 | $7 \times 21$ | L., M. \& S. | 2 | 2/6 | C93A |
| A | 10 | 4 | $6 \times 2$ | L., M. \& S. | 3 | 3/6 | C94A |
| B | 5 | 87 | $4 \times 64$ | L., M. \& S. | 3 | $3 / 6$ | C95A |
| B | 71 | $7 \frac{1}{2}$ | $6 \times 5$ | M., S1, S2 | 3 | 3/6 | C96A |
| A | $11 \frac{1}{2}$ | 42 | $6 \times 5$ | L., M. \& S. | 3 | 3/6 | C97A |
| C | $5 \frac{1}{2}$ | 7 | $4 . \times 54$ | L., M. \& S. | 3 | 2/6 | C98A |
| B | 41 | 10 | 3) $\times 6$ | L., M. \& S. | 3 | 3/6 | C99A |
| A | 5. | $4 \frac{1}{2}$ | 31.2 | L., M. \& S. | 3 | $2 / 6$ | Cl00A |
| C | $7 \frac{1}{2}$ |  | $5 \times 5$ |  | 3 | $3 / 6$ | C101A |
| C | 5 | $6 \frac{1}{2}$ | $4 \mathrm{k} \times 5$ | L., M. \& S. | 3 | 2/6 | C102A |
| C | 5 | $6 \frac{1}{2}$ | $4 \times 48$ | M., S1 \& S2 | 3 | $2 / 6$ | C103A |
|  |  |  | Metal, | Fibre and Card | Dials |  |  |
| A | $10 \frac{1}{2}$ | 31 | $8 \times 21$ | $M_{S 3} S_{\&}, \underset{S}{S}$ | Metal | 2/6 | C75A |
| C | 4 | $5 \frac{1}{2}$ | $3 \times 3$ | L. \& M. | Fibre | 1/6 | C82A |
| C | 33 | 3 | $21 \times 23$ | L. \& M. | Card | 9 d . | C86A |
| D | 51 | 5 | $4 \times 21$ | L., M. \& S. | Card | 9 d . | C87A |

## EXCEPTIONAL I.F. TRANSFORMERS

Ferro enclosed and cored, 465 KC adjustable, very high $Q$ and gain. Ideal for car radios, personnel sets, etc. Dimensions: $1 \frac{4}{4} \mathrm{in}$, high $\times$ lin. dia. Price $8 / 6$ per pair.

## THIS MONTH'S SNIP

Owing to a fortunate bulk purchase we are able to offer .1500 v . Tubular Condensers at $7 / 6$ per dozen. These are not Government surplus but are recent manufacture of one of our most famous condenser firms and have been stored in air-tight tins.

## COLLARO AUTO-CHANGER

Last year we purchased a large quantity of the Collaro Auto record changers type RC/511, 3 speed, suitable for all types of records with the latest crystal pick-up, but these have been selling very rapidly, and it may well be that unless you buy one this month you will not be able to again, at this special price. We urge you, therefore to order right away, the price is 11 gns., plus 7/6 carriage and insurance.


## ELECTRONIC TIMER

With this instrument processes which operate over a specified time can be controlled automatically, e.g., in photography use it to control exposures, etc. The instrument can be set to any length of time from a fraction of a second up to three minutes, and it can be made to switch the appliance on or off. Circuit diagram and instructions, $2 / 3$. Complete kit of parts, including valves, mains transformer, power pack, sensitive relay, potentiometer and metal case, 69/6.


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We carry a full range of standardsize volume controls from 2 K to
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also supply midget-type controls, also supply midget-type controls,
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## SHORT WAVE TUNING HEART

Coil Prack, 2 gang condenser, IF transformers and calibrated scale for frequency coverage of 13-37 metres, $37-100$ metres and 200500 metres. Price $39 / 6$ complete with circuit diagram.


A POWER PACK FOR 15/Efficient power supply, O.K. for operating a receiver, amplifier, instrument or other device requiring up to 60 mA . at approx 250 v . Parcel consists of filament transformer, rectifying valve, smoothing resistor and $16 \times 16$ mfd .350 v . electrolytic condenser. Note the filament transdenser. Note the filament cransto operate 3 or 4 other 6.3 valves.
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## CEILING FAN

This model, made by Revo, incorporates a series-wound totally enclosed ball bearing motor of robust construction and noiseless operation. The fan has a blade diameter of 36 in . and is supplied with 20 in . suspension tube and ceiling canopy. All finished white cellulose enamel. The voltage working is $230-250 \mathrm{v} . \mathrm{D} . \mathrm{C}$ Revo catalogue number Di2288. Price £ $7 / 10 /-$
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Complete kit comprises 2 valves, smoothing condenser, filament transformer and all necessary parts. Price $20 /-$, plus $1 / 6$ post. Constructional and operational data free with kit or available separately, price $2 / 6$.
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The kit comprises a veneered and polished wooden surround, special mask, oil filled enlarger and four chrome-head fixing screws.
Has these advantages:-
(a) It gives the impression of being a standard 9in. tube.
(b) Saves the cost of a 6in, mask. (c) Protects magnifier from accidental damage.
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 INSULATORS

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TELEVISION. This is an A.C. chassis of Superhet Design employing 14 valves, viz.: 7 6F1 Mazda, 1 CP25 Mazda, 2 6D2 Mazda, 1 6L18 Mazda, 1 EY51 Mullard, 1 EL38 Mullard, 1 6SN7 Brimar. Tube is Cossor 85 K
Special features: Focus, PM with pre-set centring and tilting facilities, and continuously adjustable focus control, accessible to the user.
Picture Tone Control: 3-position Gradation Control which adjusts the level of vision interference suppression.
Aerial Attenuation: A screen Aerial Attenuator Box is provided on the chassis for use in the vicinity of transmitters.
Sensitivity: 50 micro volts for peak white on the screen giving extremely good results in fringe areas.
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| :---: | :--- | :--- |
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| 32 | $1 / 10$ | $3 / 2$ |
| 33 | $1 / 11$ | $3 / 3$ |
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| 36 | $2 / 2$ | $3 / 6$ |
| 38 | $2 / 2$ | $3 / 10$ |
| 40 | $2 / 4$ | $4 / 2$ |

TINNED COPPER WIRE

| S.W.G. | 2 oz. <br> Reel | 4 oz. <br> Reel |
| :---: | :--- | :--- |
| 16 | $1 / 3$ | $1 / 10$ |
| 18 | $1 / 5$ | $2 /-$ |
| 20 | $1 / 4$ | $2 / 2$ |
| 22 | $1 / 5$ | $2 / 5$ |

DOUBLE SILK COVERED

| S.W.G. | $2 \mathrm{oz}$ <br> Reel | $4 \mathrm{oz},$ |
| :---: | :---: | :---: |
| 16 | 1/3 | 1/10 |
| 18 | 1/3 | 1/11 |
| 19 | 1/5 | 2/3 |
| 20 | 1/6 | $2 / 6$ |
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| 32 | 2/6 | 4/6 |
| 33 | 2/9 | 5/- |
| 34 | 2/10 | 5/2 |
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TELEVISION AERIALS. From the same source. Small quantity of Antiference PD5RM Dipole and Reflector, with IOft. metal mast and chimney lashing equipment. For Holme Moss. Listed currently at $£ 7$. Our price $\ddagger 4$ each, carr. 4/-.
1155 AC POWER PACK AND OUTPUT STAGE. With built-in

G.E.C. VHF RECEIVERS complete with 10 valves. Ex-Govt. As used by police. Used but guaranteed in excellent condition. Valves comprise ZA2's, 954's or EF50's in
$H F$ and lst Det. stages. Det 19 in local oscillator, KTW63's in three IF stages, D63 Det and AVC, LF H63, Output KT63, Noise suppressor D63, Power requirements 6 v 3 a , 270v 80ma, 78.5-82 Mc/s. Intermediate frequency adjustable 8.3-9.8 Mc/s. Oscillator Crystal controlled (No crystal included). Sensitivity 3 microvoles for 50 mw audio output. Input impedance 72 ohms. Housed in Grey enamel steel case with lid $10 \times 8 \times 7 \mathrm{in}$. Weight 22lbs. Note the amazingly low price, $49 / 6$ plus'5/-carr.

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Established 1935

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Specially wound on transparent perfectly balanced plastic spools which fit easily to all popular types of tape recorders． The advantages of FERROVOICE are now available to all． FERROVOICE improves the performance of all recorders．It provides twin－track recording of the highest standards of quality and faithfulness．Tape wear and rotation noises are reduced to the minimum．
FERROVOICE is the most modern and most efficient tape available．
It brings to all tape recorders the highest standards of recording． and reproduction．
Technical features：Super Calendered Kraft Paper－breaking strain approximately 4 lb ．－Tape width $0.247^{\prime \prime} \pm 0.001^{\prime \prime}$ ．Medium coercivity－ ease of erasure－frequency response $50 \mathrm{c} / \mathrm{s}^{\circ}$ to $10 \mathrm{Kc} / \mathrm{s}^{\circ}$ at $7 \mathrm{t}^{\prime \prime}$ per second． Length of tape $1,200 \mathrm{ft}$ ．Spool $7^{\prime \prime}$ diameter．
NOTE THESE OUTSTANDING FEATURES $\star$ TWIN－TRACK RECORDING WITH UNIFORM RESPONSE． $\star$ HIGH PLAYBACK LEVEL AND LO W NOISE COMPONENT， \＃LIGHTWEIGHT PRECISION BALANCED SPOOL， NOISE TO A MINIMUM．


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THE

## World 3 －Valve Set

 ＂PRE－SET＂REGEIVER complete Kit to build 4－stathon＂Pre－set＂Superbet Recolver for A．C．maina operation．
The set is designed to recelve any three stations on medium waveband and one on long
wave，each station being Wave，each station being
recelved by the turn of a rotary switch－no tunlag belog necessary．It is of midged size，belng 8 gin．$\times$ stin．$\times 7 \mathrm{ln}$ ． high，and has the performance of a far more expensive ready－made set，but can be built cr half the price This Heceiver，as llustrated，can bu Instructions，inctudute component layout and component price tist，are avallable for $1 / 9$
A MAINS OR BATTERY PORTABLE KIT

long and medium wavebends We are able to supply all of the components to build this set，as designed and specifled in the Feb． 1950 issue，inclut 1 ng
the driyled chassis．Valves and moving the dritled chassis，Valves an
speaker，etc．，at the following
complete chasgis，less lial and complete chassis，less dial and drive assembly， $25 / 5 /=$ ．Ditto
including dial and drive assernbly，f6．To construct the complete set，Including dia and drive assembly and cabinet，£．£／3／6．overall size of cabinet is 7 in ．$\times 3 \mathrm{zin} \times$ $11 \frac{1}{1}$ A reprint of the designer＇s artlcle，giving circuit and assembly instruction （this is available separately for gd．）together with a practlcal component layout is jucluded with each of above tssemblies

## ＂PERSONAL SET＂BATTERY ELIMINATOR

 A complete K3t of parts to build Midget ＂Alldry＂Battery Eliminato Thls ellmalnator is for usc on malns and is buitable for any requiring H．T．and Ler． voltago as above，or approz．to 69 volts． The Kit is quite easily and quickly asgembled amit is easy－to－follow assambly instractions， $42 / 6$ In addition we can offer a similar COMPLEETE KIT to provide approx． 90 volts and

## THE＂MINI－TWIN＂1－VALVE BATTERY SET

 dum and long waverand and hiving exceptionalls on Drilled chassls and practical diagrams make th the The complete chassls，includ－ ing valve，can be built for
$3 \% / 6$ ，the attractive plastic $37 / 6$ ，the attractive plastic
case is $9 / 6$ ，and suitable case is $9 / 6$, and
headphones $14 / 9$. The complete assembly in structions，layouta and a component price
evailable for $1 / 6$ ．
This Receiver also performs excellently，without modifica． udition with simpie modifications for whe a complete dingram is provided makes a first－clase pre－amplifler for pick－up or microphone

TWO BATTERY PORTABLES
（a）THE＊＇MINI TWO－THREE＊
An＂Alldry＂Battery Portible of midget aize， 6 解in．$\times$ metres，with nuse of ahort traller aerial
The aimple deeign of thils Ewecolver in 50 arranged that either a spalve set or a t－valve（afterwards easily converted to the 3－raive）can bernade－
Consists of a T．R．E．circrut using a regenerative detector with H．F．stage andia h hygh gasn output pentode litue up $\mathrm{IT} 4-\mathrm{IT} 4-\mathrm{OL94}$ ．
The 2 －valve set call be completely built for $54 / 3 / 6$（less oase），and the s－varve for $£ 5 / 3 /$（less casc）
Send $1 / 9$ for the assembly Instructiona：they 1 nolude nimple and complete practical component layouts and diai－ grams，which enalile the most Inexperienced coustruc－

（b）THE＂MINI－FOUR＂
A 4 －valve Baklery Supernet ikeceiver designed to receive 4 pre eset stations，three cin medium waveband and one on long wave to suit local corsitions．Each station is obtalned
on the set by the surn of a rotary spitch．No tuming is It ineceseary．
It is of midget size，hielng ouly $43 \mathrm{In}^{2} \times 6 \mathrm{Kin}^{2} \times 4 \frac{1}{2} \mathrm{In}$ ．when completely built ald $\frac{1}{8}$ very easily assembled trom diagrams Cost of all components to build this set，in accordance with the design，including a driled and cut chassla and panel and new valves，is $\mathrm{f} 9 / 10 /$－（o．less valves for $£ 6 / 7 / 6$ ），Attrac－ tive carrying case frished in blue leatherette，16／9．Com－ plete constructional data with a blue print，which shows the practical componcit laycut and firing diagram，together separately，1／6．Our battery eliminators（Illustrated above） available in kit form are eultable for use with thia set

## THE FAMOUS＂SHAFTESBURY＂ RIBBON MIKE

Incorporating Internal line transformer haviagtrans－ formstlon ratio Irom ribbon lmpedance up to 500－600 hms．．．reduced iroms 10 gas to \＆6．A opecial hine | to 25 jril |
| :--- |

## DENCO I．F．LINER

For accurately giving 46.5 Kc ．and 1.0 Mc．I．E．channels completely self－contalned， $58 / 6$ pplus battery $1 / 8$ ）．

## THE＂WIRELESS WORLD＂ MIDGET A．C．MAINS 2－VALVE RECEIVER

Wo can supply ald the components to build this set，
includlug valves and moving coil apeaker，for es 310 ， including valves and moving coil apeaker，for fisil10／－．
including designers
complete building instructions （these are available separately for $\theta d$ ．）．

## THE VIEWMASTER TELEVISOR

We have had very considerable experience in aesisting
customers to build this T／V and can supply a SPECI－ customers to build this T／V and can mpply a SPECI－ FLED COMPONENTS EX．STOCK．The assembly instructions showing practical layouts and price ust are Moss，Kirkeo＇s ${ }^{\circ}$ botts and Wenvoe．Complete television price Hist is contained in our general sTOCK LIST at $\theta$ d．，including Haynes，ete．，components．

THE DENCO ULTRA MIDGET SUPERHET COIL TURRETS WITH A ROTARY TURRET ACTION
ype Cis consists at a sour station pre－set win from onen any three stations od by at tarn of the turret ewitch Price $39 / 6$
ype CT10，is a 8 waveband coll pack lucorporating a sourth witch position for Gram．Complete coverage ts，long wave short wave 15050 metres，Price $\mathrm{E} 2 / 8 / \mathrm{F}$
A completc receiver circuit and all necessary data ia tncluder with each turret．These can be aupplied separately for $8 d$.

## HOME CONSTRUCTORS

## 左

design of a 5 Valve Superhet Recoiver，employing an R．F．Stage for $t$ or 12 Volt supply． Nend 28 for the complete set of Assembly Instruc－ tions，CIRCOIS，LAAYOUTS，and POINT－TO－POINT wimine DLaglams，together with a complete component Price List．
THIS IS NOT AN EX GOVT．RECEIVER，IT IS A NEW DESIGN EMPLOYING NEW COM－
PONENTS．


## BATTERY CHARGER KITS

All kits incorporate metal rectiliers and are for use on A．O．mains $220-250$ volts．All kits include an enaily
followed wirthg diagram．All prices include a TApPbU RESTSTOR and a five－position SELECTOR SWITCH RESISTOR and a five－position sELECTOR SWITCH For 6 or 12 volt batteriea at max．I amp．，f1／18／日 （excluding Resistor and $\$$ witch，£1／3／6）．
For 6 or 12 polt batterles at max．1f ampa．，£2／4／ （excluding Resistor and Switch，$£ 1 / 8 / 8$ ）． For 6 or 12 volt batterics at max． $2 / 2$ ampa．，$£ 2 / 14 / 6$
（exeluding Resistor and Switch，$£ 1 / 19 / 6$ ）． （exeluding Resistor and Switch，$£ 1 / 19 / 6$ ）．
For 6 or 12 volt batterie at max． 4 anigs．，$£ 3 / 2 / 6$ （excluding Resistor and 8 witch，£2／7／3）．

Send 9d．for our STOCK LIST it shows hundreds of RADIO AND TELEVISION COMPONENTS aud many KITS OF PARTS for both Sets and Battery Chargers． When ordering please include approx．cost of Post and Packing．

TWO COMPLETELY ASSEMBLED "ALL-WAVE" SUPERHET CHASSIS
(a) MODEL B.s. A s-valve 3-waveband superhet Recelver
(b) MODEL R. A 6 -valve 6-waveband (4 bandspread) Superhet Reckiver. Both Recelvers ars for operation on A.C. mains $100 / 200$ volts and $200 / 250$ volts, and employ the very latest mintature valves, they are designed to the most modern specincation, clarlty of speoch and music on both gram and radlo, making them the ideal replacement chansif for that "old Radiogram," etc.

## A GENUINE SPECIAL OFFER!

PLESSEY 3-SPEED AUTO CHANGE UNITS
Brand New in maker's Cartons, complete with mounting imstructions. E11-3-6 (Normal price is $£ 23 / 10 /=$ )


## MODERNISE YOUR OLD RADIOGRAM FOR

『25> with (plus 10/- carriage andinsurance) with the very lazest equipment. We will supply the 3 waveband chassis on the left with the Plessey auto changer on the right, complete with $10^{\circ}$ speaker for 625 ( $\epsilon 28 / 7 / 6$ with the 6 waveband chassis). This is less than half the price of comparable commercia three speed auto radiograms.


Negative feedback is employed over the entire andio stages. Chassis size: $11 \times 7 \times 81 \mathrm{hn}$
 E12/12/a, (Carr, and Pkg. 7/6 extira). H , as the B.3, but covers 6 wavebanda, Short wave $11-16,16-25,22-23,31-46$ and $43-120$ metres, and mediura wave 187-550 metrea. The arst four short bands are bandspread. The controle employed are as osed on the B. model, but the tone control operates a siz-positton switch, having three additional positions for varying bass and treble on gram reproductlon. Negative feedback is amployed over the entire audlo stage. Slze of chassis and dlal la as given for B.3. Price complete and READY FOR USE, excluding speaker $515 / 15 /=$. Carriage, packing and insursnce $7 / 6$ extra.

## !! AMPLIFIERS ! !

## TWO COMPLETE KITS OF PARTS

 A 6-8 wast QUALTTY "PUEE-PULU" AMPLIFIER destgned for A.C. mandar 200 to 250 volta, Incorporatling a or ifghtwelght pick-up to be used, and in suitable for nas with standard or long-playisy records a tome control is incorporated, and the 10 -wnts output transtotmer is dealgned to match 2 to 10 ohm speakers The overad size of the ausembled chassis in $104 \mathrm{n} \times 8 \mathrm{to} . \times$ 7 inin. high, and full practlcal dilagrama are mpplled. Price, includirg drilied chassis and valves, of complete kit, £6/17/6. Price of assambled chassis, supplied ready for uso, $28 / 12 / 8$, Full descriptivo leafleta are avallableA 12-watt HIGH FIDELTTY "PUSE-PULL" AMPLA 12-wait HIGH FIDELITY "PUSE-PULL" AMPLL 6 valves plus rectifler, wilh negative foedback, and com.
prises a main amplifler chassig and a remote controlled prises a main ampllfer chassis and a remote controlied Preamplifer and Tone Control Unit, incorporating four controll-bass, treblio, gram, microphone, selector stitch. This control unit measures only $7 \times 4 \times 2 \mathrm{in}$. The measured frequency range of the ampllier with this unlt ahows an excellent response from 14,000 cycles down to 20 cycles, the bass and treble controls allowing ladependent contral of gain at
both ends of the frequency ratage from zero to a caln of 50 . it can be erean, therefore, that ample correction to provided to suit any type of plek-up with any type of recording. Input voitage for maximnom output if 70 miv., 6.3 volts st 2 amps and 30 mA ㅍ.T, ts provided for toring unit, etc. Price of completo kith, inciuding drilled chassis and valves, $£ 14$. Completo spectication snd layout, $2 /=$,
We can
THIS AMPLIFLER COMPARES WELL WTTH THE WILLTAMSON AND SLMIIAR DESIGNS AT A FRAC-

## the units will auto change on all three speeds, Tin., 10 inm and 12 in .

 They play MIXED 10 in , and 12 in , records.They have separate sapphires for L.P. and 78 r.p.m., which are moved into position by a simple switch.
() Minimum baseboard size required 16 in , $\times 12 \mathrm{tin}$. with He.ght above $5 \frac{1}{4} \mathrm{in}$. and height below baseboard $2 \frac{1}{2} \mathrm{in}$. A bulk purchase
Please add 7/6 packPlease add $7 / 6$ pack-
ing, carriage and ing, carri
insurance.

A Complete Kit of Parts to build a 3-4 WATT HIGH GAIN AMPLIFIER

This amplifler will give 3 watis oulput for the small input
voltage of only 75 mallivolte, and is therefore sultable for use with any type of pick-up from the sryatal type to the miniature H/F Magnetic type.
A tone control is incorporated and the guallty produced is
 Frive line ap 2575-beH7-25 L6.
Price of completa kit, including driled chassio and valves,
SA/2/9, plual 6itn. P.M. (which fits on chasaie), $16 / \mathrm{s}$, or 8tn. P.M, $18 / 9$.
Price of fully assembled cheade ready for use, $\mathbb{L 5 / 5 / -}$ (plus cont of speaker).
Copy of assembly instructions and components price list
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 We can also TION OF THE COST.

## A 5-VALVE "ALL-WAVE'" SUPERHET RECEIVER

For use on A.C. Maius 200 to 250 volts.
This umall attractive Receiver, embodylng modern circuit technique, is designed to cover ghort, Medium and Long waveband, and incorporate the following outatanding leatures:

- A superhet circult designed for high effclency on all - three Wavebancs. - A 3uin. P.M, speak
- The latest range of new 6-volt B.V.A. minlatare valves - Buitt-in frame aerlal with provition for external aerial for distant atations.
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- THE RECEIVER AS ILIUSTRATED CAN 13 L BUILT FOR APPROX. £10/10/Send $2 / 6$ for the folly descriptive stage by rtago assembly and wiring diagrams, with which complet price details are given.



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A DUAL CHANNEL PRE-AMIPLIFIER and TONE CONTROL UNIT This comprehendvo PRE-AMPIIENES and TONE CONTROL UNIT provides a full control of bas and treble
in conjunction with a main Volumeimler Contirol.


It can be used with any annplifter and with stry pick-up, the range of frequency contral provided by the unit afiording ample compensation or an types of pick-tp long playing, without recoures to piek-up correction, The extreme texibility of the tasa and tweble controln is such that the lovel of basa and treble can be net to suit any conditions irrespective of the volume ontput of the amplifler.
Responge characteriatica are given in 12-with amplifler The unit meacures only 7in. $\times 4$ in. $\times 2$ in.,. imetuding self contalned power eupply, and can be accorcmodated elther en or a way from the main ampMiter, Let, on the front
panel of a cabinet or ang other joodion. Price, Including panel of a cabinet or any other poathon. PTice, Including
drilled chasib, valvea (68N7 and BJ5), E3/18iB. Complete arsoombly data ia arailablo andantely for 1 ja Sompletely assembled and ready for uso, $25 / 5 / 5$

CRYSTAL DIODES. Germanium Vacuum sealed glass type with wire ends, $2 / 8$ each or $30 /=$ per dozen. (P)
WHANDA WIRE AND CABLE STRIPPERS, to take allsize flexes and cables up to $\frac{7}{3}$ in. diameter, with 3 alternative heads and triple serew adjustment. These are brand new and boxed, and the original price was 15/- each. Our Price 4/3 each or 48/- per doz. (P)
CARBON RESISTORS. $\frac{1}{4}-\frac{1}{2}$ watt, 3 d . each. Virtually all standard values in stock. Nearest value supplied, unless otherwise stated. ( PorG )
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WAX TUBULAR CONDENSERS. . 1 mfd . 350 v. 4d. each or $3 / \cdot$ per doz. (G)
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SPEAKER FRET. Expanded Metal, finished Silver $6 \times 6,1 / 3 ; 9 \times 9,2 / 6 ; 12 \times 12,3 / 9 ; 18 \times 18,8 / 6$. (P) SPEAKER FRET. Expanded metal, finished gold $6 \times 6,1 / 6 ; 12 \times 12,4 /=$. (P)
SPEAKER FABRIC. Fawn or brown, $12 \times 12$, 2/-; $18 \times 18,4 / 6$. (P)
HEADPHONES. 4,000 ohms, per pair, 11/(G)

METAL RECTIFIERS. RMI, 125 r @ 80 mA , 3/II. RM2,125v.@100mA,4/3.RM4,250v.@ $250 \mathrm{~mA}, 17 /-14 \mathrm{D} / 972,250 \mathrm{Y}$. @ $25 \mathrm{~mA}, 6 / 6$. $12 \mathrm{v}, \frac{3}{4} \mathrm{~A}, 6 / 2.6 \mathrm{v}, 1 \mathrm{~A}_{4}, 4 / 6$. $12 \mathrm{v}, 2$ A., $12 / 6$.

SWITCH SOCKETS. Flush mounting 250 vole 3 pin, 5 amp., bakelite. Price 3/6. (M)


BELLINGANDLEE PLUGS AND SOCKETS. 5 way 2/-, 7 way, $2 / 3$ complete. (G) JONES PLUGS AND SOCKETS. 6 way, $1 / 9$; 8 way 2/-complete. (G)
E.H.T. PLUGS AND SOCKETS. I/-complete. (G)

PYE Z COAXIAL PLUGS AND SOCKETS. 1/- per pair, complete. (G)
4-WAY MOULDED PLUGS A ND SOCKETS 2/6 per pair. (G)
ZINC PLATED CHASSIS. $13 \frac{1}{2} \times 6 \times 2 \frac{1}{2} \mathrm{in}$. drilled for five valves, $2 / 6$. (M)
DUMMY AERIAL LOADS. Tapped at 20 , 10 and 5 ohms, 100 watts. British 5 -pin base. Callers only, $1 / 6$ each. (G)
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FLEX CONNECTORS. $2 \frac{1}{4} \times \frac{1}{2} \mathrm{in}$, for 250 v ., I/- complete. (G)
TWO GANG TUNING CONDENSERS. 0.0005 mf ., with fixing feet. Price $7 / 9$ each. (P) THYRATRONS. Type NGTI (CVII4I), 4 volt heater. Price $5 / 6$ each. (G)
TRIMMERS. $50+50 \mathrm{pF}, 100+100 \mathrm{pF}, 100+$ $500 \mathrm{pF}, 500+500 \mathrm{pF}$, ceramic mica, 9 d . each. $250 \mathrm{pF}, 1,000 \mathrm{pF}, 9 \mathrm{~d}$. each; $50 \mathrm{pF}, 75 \mathrm{pF}$, airspaced pre-set. $1 / 3$ each; 75 pF , air-spaced, 2 in . spindle. 2/-each. (G) foot, $1 / 9$ per yard. (P) amp. Price $3 / 9$ each. (P) coils. (M) (M) bunching. Price $1 / 6$ each. (G) each. (P) Price $10 /-$ each. (P)

LINE CORD. 3 -way, $0.3 \mathrm{amp}, 60$ ohms per
ELECTROLYTIC CONDENSERS. These are current production, not surplus stocks. 32 mfd ., 450 volts, 250 mA ripple, can., $4 / 6$; 8 $\mathrm{mfd} ., 450 \mathrm{v} ., 1 / 9 ; 8+8 \mathrm{mfd}$., 450 v., $3 / 3 ; 8+16$ $\mathrm{mfd}, 450 \mathrm{v} ., 4 /-; 8+32 \mathrm{mfd}, 450 \mathrm{v}, 4 / 6$; $16+16 \mathrm{mfd} ., 450 \mathrm{v} \cdot \mathrm{s} / \mathrm{-} ; 32+32 \mathrm{mfd} ., 350 \mathrm{v}$., 3/6; 25 mfd., 25 v., $1 / 9 ; 50$ mfd., $12 \mathrm{v}, 1 / 9$. (P)
MAINS DROPPERS. Standard 0.2 and 0.3
AERIAL AND OSCILLATOR COILS. FOR medium and short waves. Price $5 /-$ per set of 4

HEATER TRANSFORMERS. 230 v . input, 6.3 v., 1.5 amp . output, $5 / 6$ each. (P)

MOULDED BAKELITE ESCUTCHEONS.


GENERAL PURPOSE TRIODES. Type 7193, 6.3 v . heater. Similar to 615 G . Price $2 / 6$ each. (G) ROTARY TOGGLE SWITCHES. 4-pole

OUTPUT TRANSFORMERS. Standard pen. tode matching to $2 / 4$ ohms. Price $4 / 6$ each. (M) L.F. CHOKES. 10 Henry, 70 mA . Price 4/9

ENGRAVING TOOL. For $200-240$ v. A.C. mains. Suitable for use on metals or plastics.

COAXIAL CABLE. Stranded centre conductor, $\frac{1}{d}$ in. diameter, 80 ohms, 9 d . per yard. ( $\mathbf{P}$ ) CONDENSER CLIPS. Vertical mounting lin. 4d.; lif. $4 \frac{1}{2}$ d.; Horizontal mounting, $1 \frac{3}{3}$ in 4d.; Double, $\frac{3}{4}$ in., elips, 4d. ( $\sigma$ )

## d

6 APE RECORDER OSCILLATOR COILS.
$6.3 \mathrm{mH}, 45 \mathrm{kc} / \mathrm{s}$, for high impedance heads only. Price 6/9 each. (P)
TELEVISION MAGNIFYING LENSES. 6 in clear, 19/6; 9 in , clear or filter, $50 /=$; 12 in ., clear or filter, 70/=. Please state which and add $5 /$ - for carriage and packing. (P)
DIAL BULBS. $6-8 \mathrm{v} .0 .3 \mathrm{amp} ., \mathrm{M} . E . S$, fitting Price 3 for t/9. (P)
PAPER CONDENSERS 0.01 mfd ., 500 v ., 6d ; $0.01 \mathrm{mfd} ., 750 \mathrm{v}, 6 \mathrm{~d} . ; 0.25 \mathrm{mfd}, 500 \mathrm{v} .:$ 6d.; 1 mfd. 400 v., 6 d . : i mfd. $500 \mathrm{v} ., 9 \mathrm{~d}$.; $1 \mathrm{mfd} .600 \mathrm{v}, 1 / \mathrm{m}$; 1 m mid. $800 \mathrm{v} ., 1 / 3$ (all G) ; $3 \mu \mathrm{fd} ., 750$ v., $1 / 9$. (U)
OILFILLED CONDENSERS. $1 \mathrm{mfd} .600 \mathrm{v},. 3 / \mathrm{h}$ (G)

AERIAL FILTER UNIT. No. 112. IOP/13089 2/-each. (G)
ALADDIN 곻N. COIL FORMERS. Ex-Govt. wound. No slugs or cores. 2/- per doz. Iron dus cores for above $3 / 6$ doz. (G)
ADMIRALTY TRANSFORMERS. 36 VA. $500 / 1,000 \mathrm{c}$. Pri. 0-80-180 v. See. $0-900-2,400 \mathrm{v}$ Can be used in reverse on 50 c., 3/9. (G)
DIMMER SWITCHES. SC/725. Wire wound, approx. 300 ohms, with off position. $1 / 3$ each. (G) ELECTRON COPPER AERIALS. $50 f \mathrm{f} ., \mathbf{2 / - ;}$ 100ft., 3/9. (PZ)


MINIATURE MUMETAL TRANS. FORMERS. Auto-wound, giving approx. $2 / 1$ ratio. Ideal rewind as head lift transformer, or lams can be used for recording heads. 2/6 each. (G)

DECALS. $500 \frac{1}{6}$ in. high white transfer letters and words for marking electronic equipment Price 4/9 per book. The new Decals book for the amateur now available. 29 words per page, 4 pages radio and audio, 4 pages $T / V$ and Scope, 2 pages mise. incl. Tx. and Tape Recording. 3/6 per book. (PZ)
INSTRUMENT WIRES. Enamellod, silk and cotton covered, available in upwards of 2 oz. reels. Send S.A.E. for list of lowest prices. (P)
ROTARY TRANSFORMERS. Type 31, input 18 v .12 A . ; output 7.2 v .13 A . and 225 v .0 .11 A . Price 22/6. ' (U)
VOLTAGE STABILISERS. Type VSIIO (SI30), With loose bases but otherwise sound. Price With (00
$3 / 6$. (U)
GOODMANS OUTPUTTRANSFORMERS 10 watts push-pull to match into 10,000 ohm., with two 3.75 ohm . secondaries for 3 or 15 ohm speaker. Price 14/9. (P)
SMALL PAPER CONDENSERS. in tubular metal cases with wire ends. $0.25 \mathrm{mfd} ., 250 \mathrm{v}$. $\frac{1}{1} \mathrm{in} . \operatorname{diam} \times \frac{7}{8} \mathrm{in} ., 1 /-$ each $(\mathrm{M})$; $1 \mathrm{mfd} .150 \mathrm{v.}$, $\frac{5}{8} \mathrm{in}$. diam. $\times 1 \frac{t}{2}$ in., $1 / 3$ each (M) ; 2 mfd .250 v ., in. diam. $\times 2 \frac{1}{2}$ in., in Neoprene sleeve, l/9 each. (M)
TYANA SOLDER GUNS. Weight 30 oz., for 220-2j0 v. A.C. mains only ; consumption 100 watts. The low voltage bit can be easily bent to reach into corners and is insulated from the earthed case. Price 3 guineas. (PY)
CONNECTION BLOCKS. 3-way on porcelain base, 6d. each. (P)
WINDSOR SAPPHIRE NEEDLES. Available in the following three patterns: trailer type for magnetic or heavyweight pick-up ; straight type for erystal pick-up; midget type for lightweight or high fidelity piek-up. Price $2 / 9$ each. (P)
MIDGET 2-GANG CONDENSERS. American manufacture, 500 pF ., $7 / 6$ each. (M)
VARIABLE RESISTORS. 50 ohm, I amp., with calibrated very fine worm drive. Price 7/6. (U)

## IDENTIFICATION CODE

$\mathbf{G}=$ Government unused ： $\mathbf{U}=$ Ex－equipment， used ： $\mathbf{P}=$ Current production，unused $M$ Manufacturers surplus，unused； $\mathbf{X}, \mathbf{Y}, \mathbf{Z}$ Varying trade discounts available．Particulars on request by bona－fide traders．

Post and packing extra on all items（minimum parcel post 1／－）．Post orders to our Deptford address．Kindly print name and address．Early closing Thursday，open all day Saturday
GARLAND UETB RECORD PLAYBACK AMPLIFIER．A revised version of our popular amplifier designed to suit Truvox Tape Desk or Lane Tape Table．New features include higher gain， margic eye record level indicator，and smaller size for insorporation in portables．Oscillator and power supplies included．Standard valves throughout．Formica control panel．Supplied complete with Bin．P．M．loudspeaker．Price f13／2／6 plus 7／6 carriage，etc．Trade supplied．（PX）
UNDRILLED CHASSIS．In 20 s．w．g．，bright mild steel：Four－sided size $13 \mathrm{in} \times 7 \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$ ．， 5／－each ：two－sided with two straps， $12 \mathrm{in} . x$ $4 i n . \times 2 \frac{1}{3}$ in．，price 3／－each．Two－sided with two straps，size $6 \times 5 \times 2 \mathrm{in}$ ．，price 2 －
each．Add one－third to above
prices if chassis required in alu－
minium．（ $\mathbf{P}$ ）

## （2）鹿

ELECTROLYTIC CONDENSER OFFER． Tubular cardboard cased，with wire ends， 8 mfd ． 4／5 v．wkg．， 525 v．surge，2／－each．（P）
RECTANGULAR KNOBS．Size $1 \frac{1}{4} i n . \times \frac{3}{4} \mathrm{in}$ ． with gold indicating spot ；to fit standard $\frac{1}{4} \mathrm{in}$ ．
spindles． spindles．Price 6d．each．（G）

BOOKS FOR RADIO ENGINEERS Mullard Valve and Service Reference Manual Mullard Amateurs Guide to Valve Selection Osram Valve Manual，Part $I$
Brimar Radio Valve and Teletube Manual．．．
Wireless World Radio Valve Data，3rd
edition
Radio Valve Gude．By W．．May Mal，latest
The Williamson Amplifier Manual，
he Will
Wireless World High Quality Amplifier Manual
T．V．Fault Finding
Television Faults
Television Explained（Miller）
View master Envelope（state transmitter for which required）．
Tele－King Envelope
The Osrilloscope Book
Magnetic Recording（Quartermaine）
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TYANA SOLDERINGIRONS．Lightweight， 40 watt irons with easily interchangeable elements and $3 / 16 \mathrm{in}$ ．diameter bits．Voltage ranges， 6 v ．， $100 / 110 \mathrm{v} ., 200 / 220 \mathrm{v}$ and $230 / 250 \mathrm{v}$ ．Price $18 / 9$ ；，
The iron that makes soldering a pleasure（PY）
WIRE WOUND RESISTORS．Open，cement coated or vitreous enamelled． 4 watt．50， 90 ， Price $1 /$－each． 6 watt， $30,145,27010 \mathrm{k}$ ．， 15 k ．Price $1 / 6$ each． $10-15$ watt， $5,90,100$ ， $120,170,175,200,400,700,950,1 \mathrm{k} .13 .5 \mathrm{k}$. ， 4.5 k． 4.7 k．， 11 k．． 15 k． 25 k．． $1 / 9$ each． 15 watt， 650 ohm．Price $2 /$／．（Mor $G$ ）
CERAMIC SWITCHES．Single pole，eight－ way， $3 / 6$ each．（G）
VARLEYMAINS TRANSFORMERS．Primary 0－0－200－220－240 volts．Secondary $300-0-300$ volt at 150 mA ．， 5 volt at 3 amps．， 6.3 volt at 4 amps ．， 6.3 volt at 1 amp．Open type construction． Price $45 /=$ ．（P）

Tyour
HIGH CAPACITY PRECISION MICA CON DENSERS．We have still a few thousand of these left，but as we can no longer offer our original comprehonsive range，we are clearing the balance， in the values shown hereunder，at $1 /$－each，or 9／－per dozen．Accuracy in all cases is plus or minus point five（ 0.5 ）per cent．Ruby mica and copper foil or sifver．（a） $0.017970 \mu \mathrm{~F}$ ，（bl） $0.027400 \mu \mathrm{~F}$ ，（d） $0.040710 \mu \mathrm{~F}$ ，（e） $0.055820 \mu \mathrm{~F}$ ， （g） $0.087460 \mu \mathrm{~F}$ ，（h） $0.108435 \mu \mathrm{~F}$ ．（G）
ENGRAVED KNOBS．Itin．diameter，fluted in Walnut or Ivory，with the following markings： Volume，Vol－On－Off，Treble，Bass，Tone，Tuning， Wavechange．S－M－L－Gram，On－Off，Brilliance， Brilliance－On－Off，Contrast，Focus，R1－R2－PB． Price $1 / 6$ each．Plain knobs to match， $1 / 3$ each． （PZ）
VALVE TYPE 954， 6.3 volt Acorn pentodes． Brand new Westinghouse，boxed in 25 ＇s．Special offer per box of $25,30 /=$ ．Supplied separately at offer per box
$2 /-$ each．（G）
CONN二CTION BLOCKS．Moulded pla
with brass inserts．3－way，10d．；4－way，1／－．
（P）

T．R．F．COILS．Medium and long wave，aerial and H．F．， $6 /-$ per pair ：with reaction winding， $6 / 9$ per pair．（P）

TOROIDAL CERAMIC POTENTIO－ METERS． $260 \Omega 50 \mathrm{w} ., 6 / 6 . \quad 17 \mathrm{k} .100 \mathrm{watt}, 8 / 6$.
MAGNETIC TAPE．Scotch Boy MCl－III： I，200ft．，35／＝； 600 ft ．，21／－； 300 ft ．，12／3．Spare 7 in ． spools，4／3．Ferrovoice，the new kraft－based medium coercivity tape：1，200ft．，22／6．Spare 7in．spools，4／6．（P）
BRIMISTORS．Non－linear resistors to protect valves from current surges：CZI，0．3A，3／6； $\mathrm{CZ} 2,0.3 \mathrm{~A}, 2 / 6 ; \mathrm{CZ3}, 0.2 \mathrm{~A}, \mathrm{I} / 6 ; \mathrm{C} 24,1.25 \mathrm{~A}$ ， CZ2，0．3A， $2 / 6 ;$
$5 /-: C Z 6,0.45 A, 3 / 6$.
MOULDEDBROWN BAKELITE CABINETS．Suitable for fitting Decca 3－speed gram．motor，amplifier or loudspeaker．Outside dimensions（closed） $15 \frac{1}{4}$ in．$\times 10 \mathrm{in}$ ．$\times 5$ in．；thick－
ness of wall， $1 / 16 \mathrm{in}$ ．Price，22／6，to callers only．（M） ness of wall， $1 / 16 \mathrm{in}$ ．Price，22／6，to callers only．（M） AMPLION TESTMETER． 10 ranges A．C．anu D．C．up to 500 v ．Resistance up to 200,000 ohms，
1,800 ohms per volt A．C．and D．C．Price 65 ．
HIGH WATTAGE WIRE WOUND RESIS－ TORS．Capped end type，porcelain covered，at he following prices： 20 watt， $1 /-$ ； 40 watt $1 / 3 ; 80 \mathrm{watt}, 1 / 6$ ； $100 \mathrm{watt}, 1 / 9 ; 200$ watt， 2／6： 3 ohm，semi－variable， 20 watt； 4 ohm 40 watt： $13.852+1.352+8.352$ ohm， 40 watt $80 \mathrm{ohm}, 40$ watt ； $350 \mathrm{ohm}, 40$ watt； 430 ohm ， 200 watt； $5 k, 40$ watt； $7.5 \mathrm{k}, 40$ watt ； $12 \mathrm{k}+2 \mathrm{k}$ ， 80 watt ； $20 \mathrm{k}, 80$ watt； 50 k ． 100 watt ； $75 \mathrm{k}, 40$ watt： $100 \mathrm{k}, 200$ watt．Packing and carriage extra on all of these resistors．（G \＆M） TWIN SCREENED CABLE．Suitable tor carrying currents of up to 5 Amps．Cotton carrying currents of up to 5 Amps．Cotton
covered， 9 d ．per yard．Ditto uncovered， 8 d ． covered， $9 \mathrm{d}$. pe
per yard．
RUBBER TUBING．External diameter， 0.25 in ． internal diameter， 0. lin．Price 2d．per yard．（G） WALNUT VENEERED CABINETS．SIZe $12 \mathrm{in} . \times 7 \mathrm{in} . \times 5 \frac{1}{2} \mathrm{in}$ ．Suitable for housing a T．R．F． receiver or inter－com．Complete with back， chassis，dial and clips．Price．to callers only，22／6．
LARGE DIAMETER SLEEVING．Transparent plastic，in．diameter，6d．per yard length．（M） LITZ WOUND INDUCTORS． 199 micro Henry，wound on Aladdin 音in．coil former（no iron dust core）．Price，2／6 per half－dozen．（G）

ELECTRO－MAGNETIC CONTACTORS．
Energised at $9-14$ volt．$\frac{1}{2}$ Amp：maximumswitched． current 40 Amps．In bakelite case．Price $2 / 9$.
PAXOLIN PANELS． $3 \mathrm{itin}, \times 1 \frac{1}{2} \mathrm{in} . \times 3 / 32 \mathrm{in}$ ．， 1／－per doz．，5／－per $100.2 \frac{1}{2} \mathrm{in}$ ．x 2 in ．x $1 / 16 \mathrm{in}$ ．，
 $1 / 3$ per doz
able．（M）
CABINETS in handsome two－tone Walnut veneer to house $6 \frac{1}{2} \mathrm{in}$ ．extension speaker．Price $16 / 6$ each．（P）
VALVE OFFER．Type 1625．These are the 12 volt heater equivalent of the 807 ．Price complete with Ceramic holder $5 / 9$ each．（G）


POTENTIOMETERS．20k， $10 \mathrm{w}, 10 \%$ by famous maker，Itin．spindle，price 3／6．（G） RADAR REFLECTORS．Type M×138／－A．These consist of $6-2 \mathrm{ft}$ ．$\times \frac{1}{6} \mathrm{in}$ ．dural tubes covered with fine wire mesh．The whole assembly can be used as an omni－directional aerial，and the mesh has many horticultural applications．Price $3 / 9$ each．
BRENETTE MICROPHONES．We are sole distributors in Great Britain and Ireland of these new cell microphones．The following range is now available．Type D7．Directional in black and chromed case Price E4／13／6 Type 9ND．Multi－ directional ball type in black ande directional ball type in black and chrome．Price in brown and chrome．Price $£ 6 / 17 /$ ．Type 13 U ． Highly sensitive with wide frequency response， Highly sensitive with wide frequency respo
in black and chrome．Price $£ 7 / 17 / 6$ ．（PZZ） in black and chrome．Price $67 / 17 / 6$ ．（PZ）
BRENETTE MICROPHONE STANDS．Desk with to mible to ease adjustment． These stands will suit all British and Continental microphone stands．Price $16!6$ each．（PZ） CONDENSER OFFER． 25 mfd .25 v ，ear mounting．Price complete with ear，1／－each or 10／－per dozen．． 1 mid．Condensers 350 v ．screw mounting $1 /-$ each， $9 /$－per dozen．（G）
AMPLIFIER ACII．Incorporating own power supplics ensuring that the chassis is completely isolated from the mains．Maximum output 3 watts；response 3 db ．down at $30 \mathrm{c} / \mathrm{s}$ and 30,000 $\mathrm{c} / \mathrm{s}$ ．Distortion at 2 watts output and $1,000 \mathrm{c} / \mathrm{s}$ ， $.08 \%$ ．Top cut tone control is fitted．Price 66／2／6，plus $5 /-$ carriage．（PX）
ELECTRIC MOTORS．For use on 24 v．D．C． supply，7／6 each．（G）
HIGH QUALITY LOUDSPEAKERS．Wharfe－ dale Bronze 10 in．，E4／12／8．Wharfedale Golden 10 in ．， $67 / 13 / 3$ ．Wharfedale Golden 10 in ．C．S．B．， 68／6／7．Goodmans Audiom 60， 12 in ．， $\mathrm{f11/10/3}$ ． Goodmans Axiom Mk．II， 12 in ．，$£ 13 / 12 / 4$ ．All EX－GOVT．AND SURPLUS POTENTIO－ METERS．Srill available as in April copy of Wireless World＂with the exception of So ohm and 500 ohm．（G）
ROTARY WAFER SWITCHES．3－way，3－pole， 3－bank，2／3 each．4－way，2－pole， 4 －bank，2／6 each．
TAMSA TYPE 100 TAPE RECORDING HEADS．Housed in chromium plated brass case on adjustable mounting．Record／playback heads have $\frac{1}{4}$－thou．gaps and erase heads have 2.5 thou．gaps．These heads are of high impedance． Price 45 －each．（PZ）
PAXOLIN COIL FORMERS．These are of rectangular cross section and are suitable for mains transformer bobbins． $2 \mathrm{tin} . \times 2 \frac{1}{\mathrm{t}} \mathrm{in} . \times 3 \frac{1}{2} \mathrm{in}$ ． long， $1 /=$ each． $2 \frac{1}{8} \mathrm{in} . \times 1 \mathrm{in}$ in．$\times 12 \mathrm{in}$ ．long， $1 / 3$ each．
（M）

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10,000 VALVES IN STOCK. B.V.A., Special Purpose, Transmitring, etc. A few specials : Ravtheon sub miniature CK510AX, pentode, 3/11. 954, 956, VU120, 32, 57, El 148. All at $2 / 6$ each. RK34, 2/-; MS/PEN 3/6; VU111, 3/6. Sylvania (red) EF50, 12/6.

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$12 \times 12 \mathrm{mfd}$. 350 v.w
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75 mfd .12 v.w.
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For 6 and $12 v$. operation Complate with magnetic pick-up, and volume control. In metal cabinet size: $17 \mathrm{in} . \mathrm{x} 14 \mathrm{in}$. x 11 in . Very Limited quantity. $\quad \mathbf{E 5 , 1 9 . 6}$ Carriage 10/- extra.

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R1132 RECEIVERS. New. boxed, with all valves, $£ 3 / 19 / 6$. Carriage 10/-.

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 scale. 86.

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| rice (except Al |  |
| ndra Palace), 28 | Frame trans. |
| er set. Alexandr | $3 \mathrm{Mc} / \mathrm{s}$ boo choke |
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| L9 RF choke, 2 - | Width contro Scanning coil |
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| LEVIS |  |
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| ver | filter and |
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| K3/40, 3.2 kV |  |
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| X. |  |
| $10^{4} \times$ lin. Neutr | 12 in . with fit glass, cream in |
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This unit is complete with 6 valves, 2 EF36, 2 EF39,
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EC32 (Xtal oscillator), 2 EF39's ( $2.9 \mathrm{mc} / \mathrm{s}$ IF), EB34 (det.), 615 and EC32 (Xta oscillator), 2 EF39's ( $2.9 \mathrm{mc} / \mathrm{s} / \mathrm{F}$ ), EB34 (det.), 615 and
6 V 6 (audio). Complete with circuit, $49 / 6$, post $2 /$. Please state which required.
INDICATOR 182A. With VCR5I7 6in. tube, 3 EF50's, 4 SP6I's, $5 \cup 4,9$ pots, resistors, condensers, etc. Ideal for television or 'scope. New in crates (less relay), $65 \%$ Less EFSO's and $5 \cup 4 G$, 50/. (CF)
THE NEW 1355 CONVERSION. To produce a remarkably compact Televisor-Sound, vision. Time bases and power pack on ONE 1355 chassis-without the use of expensive R.F. units : OUR DATA contains full instruction for all five TV channels and calls for a minimum of extra parts. The 182A indicator contains many of these, including a suitable cube.
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1355 RECEIVERS complete with II valves, in wooden cases 15 t grade $45 /$. ; 2nd grade $35 / \mathrm{m}$. (CF).
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MIDGET AMPLIFIERS, complete with full instructions for converting to a really small 'gram amplifier, or a tiny radio receiver (both mains operated). Three valves included. 19/6

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special offers．Germanium Crystal Diodes 2／9．Midget Mains Transformers（size approx $\left.2 \frac{1}{2} \times 3 \times 2 \frac{1}{2} \mathrm{~m}.\right)$ ．Screened Primary $220 / 240$ v． $50 \mathrm{c} / \mathrm{s}$ Output， $250-0-250$ v． 60 m．., 6.3 v． 2.5 a．Only 11／9．Small Filament 1ransformers，220／：34 v input， 6.3 v .1 .5 a．output，5／9．Auto Transformers （with separate l．t． 6.3 v． 1.5 a．）， $0-110-200-210$ ， 230.250 v． 50 watts， $4 / 9$ each．

BATTERY SET CONVERTER KITS．All parts for converting any type of Battery receiver to All Mains．A．C． $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ ．Kit will supply fully smoothed h．t．of 120 v ． 90 v ．or 60 v ．at up to 40 mA ．，and fully smoothed l．t．of 2 v ．at up to 1 a．Price complete with circuit，only $47 / 9$. Supplied ready for use to $7 / 9$ extra．

PERSONAL SET BATTERY SUPERSEDER KIT． Complete with case Supplies $90 \times 10 \mathrm{nld}$ and 1.4 v． 250 mA ．fully smoothed，from norma 200－250 v， $50 \mathrm{c} / \mathrm{s}$ ．Mains．For 4 valve Superhet Receivers．Price with circuit $31 / 6$ ．Or ready for use， $38 / 9$ ．Size of Unit $5 \frac{1}{2} \times 3 \frac{1}{2} \times 1 \frac{1}{2}$ in

H．T．ELIMINATOR AND TRICKLE CHARGER KIT Consists of h．t and lt transformer，h．t and l．t．rectifiers，smoothing electrolytic，choke and steel case．For Mains input of $200-350$ v Output 120 v． 40 mA ．and 2 v．$\frac{1}{2}$ a．Price with circuit，29／6．
Or in working order， $37 / 6$

## BATTERY CHARGER KITS

For $200-250$ v． $50 \mathrm{c} / \mathrm{s}$ ．Mains input
To charge 6 v ．acc．at 2 amp．， $25 / 9$.
To charge $6 v$ or $1: v$ ．acc．at 2 a．， $29 / 6$.
To charge 6 or 12 v ．acc．at 4 a．， $49 / 9$.
Above consists of transformer，full wave rectifier fuse，fuscholder，steel case and circuit． Or in working order， $6 / 9$ extra．

8ELENIUM RECTIFIERS．${ }^{2 / 6}$ v．a．H．W 211 i 120 v． 40 mA ．H．W．， $4 / 6$ ． $2 / 6 \mathrm{v}$ a a． $11 . \mathrm{W}$ $3 / 9 ; 230 \mathrm{v}, 50 \mathrm{~mA}$ ．H．W． $6 / 9.6 / 12 \mathrm{v}$ ．I a． $11 . W$ ， $6 / 12$ v．2 a．F．W．（Bridge）， $10 / 9$ ．6／12 v． 4 a F．W．（Bridge）， $18 / 9$.

ELECTROLYTIGS（Current production．Not

| Tubular Types |  | Can Types |  |
| :---: | :---: | :---: | :---: |
| $8,4 \mathrm{~F} 450 \mathrm{~V}$ ． | 1／11 | $16 \mu \mathrm{~F} 450 \mathrm{v}$ ． | 2／9 |
| $8 \mu \mathrm{~F} 500 \mathrm{~V}$ ． | 2／9 | $24 \mu \mathrm{~F} 350 \mathrm{v}$ 。 | $2 / 11$ |
| $16 \mu \mathrm{~F} 350 \mathrm{v}$ | 2／3 | $32 \mu \mathrm{~F} 350 \mathrm{v}$ ． | $2 / 11$ |
| $16 \mu \mathrm{~F} 450 \mathrm{v}$ ． | 2／9 | 32 mfd .450 v ． | 4／9 |
| $16 \mu \mathrm{~F} 500 \mathrm{v}$ ． | 3／9 | $40 \mu \mathrm{~F} 450 \mathrm{v}$ ． | $4 / 9$ |
| $24 \mu \mathrm{~F} 350 \mathrm{v}$ | 3／3 | $50 \mu \mathrm{~F} 350 \mathrm{~V}$ ． | $4 / 9$ |
| $32 \mu \mathrm{~F} 350 \mathrm{v}$ ． | 3／9 | $8-8 \mu \mathrm{~F} 350 \mathrm{v}$ ． | 3／9 |
| 32 mfd .500 v ． | 5／9 | $8-8 \mu \mathrm{~F} 450 \mathrm{v}$ ． | 3／11 |
| $8-16 \mu \mathrm{~F} 500 \mathrm{v}$ ． | 4／11 | $8 \cdot 16 \mu \mathrm{~F} 450 \mathrm{v}$ ． | 4／6 |
| $25 \mu \mathrm{~F} 25 \mathrm{v}$ ． | 1／3 | $16-16 \mu \mathrm{~F} 450 \mathrm{v}$ ． | 4／11 |
| $50 \mu \mathrm{~F} 12 \mathrm{v}$ ． | 1／2 | $16-16 \mathrm{mfd} .500 \mathrm{v}$ | 5／9 |
| $50 \mu \mathrm{~F} 50 \mathrm{v}$ ． | 2／3 | $16-32 \mu \mathrm{~F} 350 \mathrm{v}$. <br> $32.32 \mu \mathrm{~F}$ <br> 50 v | $\begin{array}{r} 49 \\ 49 \end{array}$ |
| Can Types |  | $32-32 \mu \mathrm{~F} 350 \mathrm{v}$ $32-32 \mu \mathrm{~F} 450 \mathrm{v}$ | $\begin{aligned} & 4 / 9 \\ & 5 / 11 \end{aligned}$ |
| $8 \mathrm{mfd}$.450 v ． | $\begin{aligned} & 2 / 3 \\ & 2 / 11 \end{aligned}$ | $32-32 \mu \mathrm{~F} 450 \mathrm{v}$ <br> 60.100 mfd .350 | $\begin{aligned} & 511 \\ & .76 \end{aligned}$ |
| 10 mfd． 350 v ． | 1／11 | $3,100 \mathrm{mfd} .6 \mathrm{v}$ ． | 6 |
| CANTYPES |  |  |  |

$32-32-8 \mu \mathrm{~F} 350 \mathrm{v}$ ．（Small）
$16-16 \mu \mathrm{~F}^{\mathrm{i}} 450 \mathrm{v}$ ．plus $20 \mu \mathrm{~F} \mathbf{2 5} \mathrm{v}$
$50 \mu \mathrm{~F} 350$ v．plus $250 \mu \mathrm{~F} 12 \mathrm{v}$ ．．．．．．．．．．．．．．．．．．．．．．
CHASSIs．（16 s．w．g．Undrilled Alumin
ceiver tye $6 \times 3 \mathrm{~B}^{\circ} \times$ in 111 Aminal）Re

 $20 \times 8 \times 2$ in．， $8 / 11$ ；Amplifier Type， $12 \times 8 \times$ 2 in．， $7 / 11 ; 16 \times 8 \times 2 \frac{1}{2}$ in．， $10 / 11 ; 14 \times 10 \times 3$ in． 13／6； $20 \times 8 \times 4$ 经．， $13 / 6$ ．

8ILVER MICA CONDENSERS．$\quad 5 \mu \mu \mathrm{~F}, 10 \mu \mu \mathrm{~F}$ $15 \mu \mu \mathrm{~F}, 20 \mu \mu \mathrm{~F}, 25 \mu \mu \mathrm{~F}, 30 \mu \mu \mathrm{~F}, 35 \mu / \mathrm{F}, \quad 50 \mu \mu \mathrm{H}$ $120 \mu \mu \mathrm{~F}, \quad 150 \mu \mu \mathrm{~F}, \quad 180 \mu \mu \mathrm{~F}, \quad 200 \mu \mu \mathrm{~F}, \quad 230 \mu \mu \mathrm{~F}$ ， $\begin{array}{llll}120 \mu \mu \mathrm{~F}, & \quad 150 \mu \mu \mathrm{~F}, & \quad 80 \mu \mu \mathrm{~F}, & 200 \mu \mu \mathrm{~F}, \\ 300 \mu \mu \mathrm{~F}, & 330 \mu \mu \mathrm{~F}, & 400 \mu \mu \mathrm{~F}, & 470 \mu \mu \mathrm{~F}, \\ 100 \mu \mathrm{~F}\end{array} \quad 500 \mu \mathrm{~F}$, $1,000 \mu \mu \mathrm{~F}(.001 \mu \mathrm{~F}), .002 \mathrm{mfd} .(2,000 \mathrm{pfd}$.$) ．All at$ Ed．each． $3 / 9$ dozen one type．

WILLIAMSON AMPLIFIER KIT．To authors specification and complete in every detail．Only 14 Ene．


#### Abstract

A PUSH－PULL 3－4 watt HIGH－GAIN AMPLIFIER FOR $£ 3 / 12 / 6$ ．For Mains input $200-250$ צ． $50 \mathrm{c} / \mathrm{s}$ ．Complete kit of parts including circuit diagram and instructions． （Point－to－point wiring diagrams available for 1／6 extra）．Amplitiet can be used with any type of Feeder Unit or Pick－up．Output is for 2－3 ohm speaker．（We can supply a very suitable 10in．unit by Goodmans at 31／－） The amplifier can be supplied ready for use for £4／17／6．Full descriptive leaflet $1 /$ ．


MASTER INTERCOMM．UNIT with provision for up to 4 ＂Listen－Talk Back Units．＂A high gain amplifier enables speech and other sounds emartating from the rooms containing remote control units to be heard at the master control． The unit is in kit form and point－to－point wiring didgranis are supplied．A bakelite or wood cabinet is included．Mains input is $200.250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ Sound amplification 4 watts Price only f5／19／6＂tisien ample liack Unat ：Price only $\mathbf{2 5} 19 / 6.1$ Lisich Full descriptive leaflet $1 / \mathrm{l}$ ．

CABINETS．BAKELITE（Brown or White） and WOOD（Walnut veneered）．Size appion． $12 \times 64 \times 5 i n$ ．Very attractive appearance．For llustrations see our List．Supplied complete with ［ully punched T．R．F．3－valve Chassis，back， 2 or 3 wave．Glass scale with colonred station names， Dial Backplate， $25 /=$ ，plus Carr． $2 / 6$ ．
All parts available for construction of T．R．F．or Superhet Receiver in above cabinets．
VOLUME CONTROLS with long spiudles，all values less switch $2 / 9$ ，with S．P．switch 3／11．WIRE WOUND POTS．：5K，10K，20k， $25 \mathrm{~K}, ~ 501$ （medium length spindles）， $2 / 9$.
AMMETERS．Moving coil．G．E．C． $0-5$ amps． zin．scale， $12 / 6$.

COAXIAL CABLE，TJ ohtus，fin．，10d．yard．
DIAL BULBS，M．E．S．，1．j． j v． $1.15 \mathrm{di}, 8$ v． 0.15 a ，
6／9 dozen．
VALVE SCREENING CANS．Imernational（）ctal piene，B7G（Hutton IJase）it piece $10 / 6$ doz．， $1 / 3$ each
EX－GOVT．ITEMS．Cathode kay lubes，ICR1：37， $29 / 6$ ，plus carr． 5 ．VR139A， 25 ，- ，plus $4 / 6$ carr－ Slydelock Fuses， 15 a．，19．V1241，4／6，VRb5， 111. Pye coaxial plugs and sockets $7 / 6$ doz．prs．Belling－ Lee moukded lype 5 －pin and 7 －pin plugs and sockets $1 / 11 \mathrm{pr} . .02 \mathrm{mfd} .5,000 \%$ Tubulars， $1 / 9$.

## EX－GOVT．SMOOTHING CHOKES

30 5 12／9 220 mA． 5 H． 50 ohms．Potted type …… $10 / 9$ 150 mA .10 H .200 olins．Potted type 100 mA .5 H .100 ohms．Tropicalised
$\begin{array}{llll}50 \mathrm{~mA} .50 \mathrm{H} .1,250 \text { ohms．Potted type } & \ldots & 8 / 11\end{array}$
EX－GOVT BLOCK PAPER MANSBRIDGE TYPE CONDENSERS
$4 \mu$ F 500
EX－GOVT．RF26 UNITS．Brand new，cartoned， 596 ，plus carr． $5 /$
P．M．SPEAKERS．All－ 3 ohms．，5in．Plessey， 13 ／9． 5in．Goodmans，14／9， $6_{2}^{2}$ in．Elac， $14 / 11$ ，fitifi． Plessey with I＇entode Trans．，14／11，6isin．Good－ mans， $16 / 9,8 i n$ ．Plessey， $15 / 9,10 \mathrm{in}$ ．Goodnans， 31／－，10in．Plessev，18／6．
M．E．SPEAKERS．All 2－3 ohns， $6 \frac{1}{2}$ in．Rola tield 700 ohms． $11 / 9,8 \mathrm{in}$ ．R．A．field 600 ohms， $12 / 9$ ， 10 in ．R．A field 1600 ohms， 23 9． 10 in ．R．A．field 1，500 ohnis．， $23 / 9$.

COLLARO TAPE DESK MOTORS，shated pole type，clockwise or anti－clockwise，29／9 each．

## R．S．C．MAINS TRANSFORMERS（Guaranteed）

Fully interleaved and Impregnated


TOP SHROUDED DROP THROUGH

|  |
| :---: |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |$\begin{array}{ll}350-0-350 \mathrm{v} .80 \mathrm{~mA} ., 4.3 \mathrm{v} .2 \mathrm{a} ., 5 \mathrm{v} .2 \mathrm{a} \ldots \ldots . & 16 / 9\end{array}$$2500-250 \mathrm{v} .100 \mathrm{~mA} ., 6.3$ v． 4 a．， $5 \mathrm{v} .3 \mathrm{a} \ldots .23 / 9$$30000-300 \mathrm{v}, 100 \mathrm{~mA} ., 6.3$ v．－ 4 v．， 4 a．，c．t． $23 / 9$$350-0-350 \mathrm{v} .100 \mathrm{~mA} ., 6.3 \mathrm{v}-4 \mathrm{v}$ ．a．，c．t． $23 / \mathrm{g}$

$350-0-350 \mathrm{v} .150 \mathrm{~mA} ., 6.3 \mathrm{v} .4$ a．， 5 v． 3 a．．．． ..... $23 / 9$
$350-0-350$ と． ..... 29／11
FULLY SHROUDED UPRIGHT
$50-0$－ 250 v． 60 mA ． $\mathfrak{6} .3 \mathrm{v} .2$ a．， 5 v .2 a．Midget type 2 $4-3-3 i n$
$350-0-350$ v． 70 mA ．， 6.3 v． 2 a．， 5 v .2 a．．．． ..... 17／6
$375-0-375$ v． 60 mA ．， 12 v .1 .5 a 5 v a ..... $18 / 11$$550-0-450$ v 100 m Q．3 v． 4 a a．．．
$250-0-250$ v． 10
$0-4-5$ y． 3 a
$50-10-250$ v． $100 \mathrm{mAA}$. ． ..... 25／9
for［＇1355 conversion ..... $29 / 9$
$300-0-300 \mathrm{v} .100 \mathrm{inA}$ ．， 6
351 －0－350 v． $100 \mathrm{mA}$.6.3 v． 4 v． 4 a．c．l．$350-0-350$ v． $150 \mathrm{~mA} ., 6.3$ v． 2 a．， 4.3 v． 2 a．－
5 v． 3 a ． ..... $33 / 9$
5 v． 3 a． ..... $45 / 9$
$350-0-350$ v． $250 \mathrm{~m} .1,6.3 \mathrm{v}$ ． 6 a ．， 4 v .8 a. 0－2－6v． 2 a．， 4 v． 3 a．for Electronic EngTelevisor$67 / 6$
$425-0-425$ v． $200 \mathrm{mb}, 6.3 \mathrm{v}-4$ v． 4 a．c．t．6.8 v .4 v 4 a ．，c．t．， $0-4-5$ v． 3 a．，suitableWilliamson Amplifier，etc．．．．．．．．．．．．．．．．．．．．．51／－
$425-0-425$ v 250 mA .6 .3 v． 6 а．， 6.3 v． 6 a． $425-0-425$
V .3 a ..... $65 / 6$
E．H．T．TRANSFORMERS $2,500 \mathrm{v} .5 \mathrm{~mA}$ ，
$2-(0-2, y . y$
VCR9
1.4，000 v． 5 mA．， 2 v． 2 a$35 /-$
$39 / 6$

## FILAMENT TRANSFORMERS

All with $200-250$ v． 50 c ／s primaries： 1 i .3 v .2 a. 7／6；0－4－6．3 v，2 a．，7／9；12 v． 1 a．， $7 / 11$ ；6．3v 3 a．， $9 / 11 ; 6.3$ v． 6 a．， $176 ; 0-2-4-5-6.3$ v． 4 a． $16 / 9 ; 12 v .4$ a or 24 v． 1.5 a．， $17 / 6$ ．

## CHARGER TRANSFORMERS

All with 200－230－250 v． $00 \mathrm{c} / \mathrm{s}$ ．Primaries ：0－9－15 v 1.5 a．， $14 / 9 ; 0-4-15$ v． 3 a．， $16 / 9 ; 0-9)-15$ v． 6 a． $22 / 9 ; 0-4-4-15 \cdot-24$ v． 3 a．， $22 / 9 ; 0-9-15-30$ v 3 а．， $23 / 9$ ．

## SMOOTHING CHOKES

$250 \mathrm{~mA} .7-70 \mathrm{H}$ ， 20 ohms．Fully shrouded．．． $16 / 9$ $250 \mathrm{~mA} ., 3 \mathrm{H} .50$ ohms．
$150 \mathrm{~mA} .$, ti－10 H． 100 ohns
$100 \mathrm{~mA} ., 10 \mathrm{H} .1000 \mathrm{hms}$.
$100 \mathrm{~mA} ., 5 \mathrm{H} .150$ ohins．
80 in A．, 10 H .350 ohins．
$150 \mathrm{mi}+10 \mathrm{H} .400$ olims． $\qquad$

## ELIMINATOR TRANSFORMERS

Primaries $200-250 \mathrm{v}, 50 \mathrm{c} / \mathrm{s} ., 120 \mathrm{v} .40 \mathrm{~mA} .7 / 11$ $90 \mathrm{v}, 10 \mathrm{~mA}$, ， $0-9 \mathrm{v}, 250 \mathrm{HA} . . . . . . . . .$.

OUTPUT TRANSFORMERS
Midget Battery Pentode 6i： 1 for 3S4，etc． $3 / 6$ Small Pentode， $5,1000 \Omega$ to $3 \Omega$ Small Pentode， $8,000 \Omega$ to $3 \Omega$ Standard Pentode， $5,000 \Omega$ to $3 \Omega$ Slandard Pentode， $8,000 \Omega$ to $3 \Omega$ Sizndard Pentode， 10,000 ohns to 3 ohms Multi－ratio 40 mis． $30: 1$ ， $45: 1$ ，$i 0: 1$ ， $90: 1$ ，Class 13 Pish－Pull．．．． Push－Pull 8 watts five to 3 olims
Push－Pull 10－12 Watts 6V6 to $3 \Omega$ or $15 \Omega 2 . .15 / 9$
Push－Pull 10－12 Watis to match（ive to
3－5－8 or 15 1 ，
$16 / 9$

Push－Pull 20 Watts，high－quality sectionally $22 / 0$

MICROPHONE TRANSFORMERS
$100 ; 1$

6

COMMUNICATIONS RECEIVER RII55. The famous exBomber Command Receiver known the world over to be supreme in its class. Covers 5 wave ranges $18.5-7.5 \mathrm{Mc} / \mathrm{s}$, $7.5-3.0 \mathrm{Mc}$ /s $1,500-600 \mathrm{kc} / 5,500-200 \mathrm{kc} / \mathrm{s}, 200-75 \mathrm{kc} / \mathrm{s}$, and is easily and simply adapted for normal mains use, full details being supplied. Aerial tested before despatch. These are BRAND NEW AND UNUSED IN MAKER'S ORIGINAL TRANSIT CASES, ONLY $£ 11 / 19 / 6$.
A few used receivers, also tested working before despatch are available at $\pm 7196$.
A few of the R1155N model can also be supplied. This is the latest version which covers the Trawler Bands, and in addition is fitted with ultra slow motion tuning. Used, but tested working before despatch, ONLY $£ 17$ 19/6.
A factory made Power Pack, Output Stage and Speaker, contained in a black crackled cabinet to match the receiver, can be supplied at ONLY $\mathbf{6 5 1 / 0}$-. Operates receiver immediately DEDUCT 10 - IF PURCHASING RECEIVER AND POWER PACK TOGETHER.
Please add carriage cosis of 10/6 for receiver, and 5 /. for power pack RECEIVERS Ri355, is specified for "Inexpensive Television. Complete with 8 valves SP61, and I each 5U4G and VU 120 or V U III Used, good condition, ONLY 29.6 (carriage etc. 5 6). RF UNITS TYPE 26 AND 27 for use with the above receiver The very popular variable tuning units, which use 2 valves EF54 and I EC 52. Type 26 covers $65-50 \mathrm{Mc} / \mathrm{s}$, ( $5-6$ metres), and Type 27 covers $85-65$ Mc Mc's, ( $3.5-5$ merres)
BRAND NEW IN MAKER'S CARTONS. CNLY $59 / 6$ each. VIBRATOR UNITS, 2 volt type, American made, delivers 67 volts at $4.7 \mathrm{~mA}, 130$ volts at 20 mA , and 1.4 v . L.T. Easily adapted for use with any battery receiver, full details being supplied ONLY 50- ( oostage $\mathbf{2}^{\prime}$ - ).
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Miniature wire ends mould
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Combined $12 i n$. mask and escutcheon in lightly tinted perspex. New aspect. edged in brown. Fits on front of cabinet 176. P \& P 2/.

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Leevers-Rich Equipment. Ltd. Lockwood \& Co.
London Central Radio Stores
Lowther Mig. Co. Lid
Ludfry Ltd.
Magnetic Coatings Ltd
Mail Order Supply Co.
Marconi Instruments Ltd $\quad$ Wirconi's Wireless Telegraph Co.
Marconis Wireess Teleglaph Co.. Ltd. 76. Marris \& Cartm. Ltd.
Masteradio. Ltd.
MCErroy-Adams Mfg Group itd
McMurdo Instruments Co.. Ltd
Measuring Instruments (Pullin) Ltd
Minnesota Miming \& Mig. Co.. Ltd.
Modern Book Co.
Modern Techntques
Morley Transformers
M.R. Supplies Ltd.
M.S.S. Recording Co. Lit.

Muitard. Ltd.
Mu.ticore soiders. Ltd
Neo EIectrica! Industrles Ltd
Newman. J. \& S., Ltd.
Northern Radio Services
Northern Transformer Co.
Nusound Products

O:ympic Radio Components Osmor Radio Products. Ltd.
Pammer. G. A. S. S. .
Parmer. G. W. F. \& Co.. Ltd.
Partridge Transformers. Ltd.
Partridge Transformers. Ltd
P.C.A. Radio

Philips Electrical, Ltd.
Post Radio Supplies
Pratts Radio $\begin{aligned} & \text { Premier Radio } \mathbf{C o}\end{aligned}$
pye, W. G.. \& Co., Ltd.
Quality Mart Quartz Crystal Co.. L'td.
Radio \& Electrical Mart. The
Radio Exchange CO Padio Experimental Products
Radio Experimental Pioducts. Ltd
Radio Industry Council. The
Radiospares
Radio Supply Co.
Radio Traders. Ltd.
Reproducers \& Amplifiers, Lid.
Reosound Engineering \& Electrical Co.
R.C. Services (Radio

Roding Laboratories
Rogers Development
Rola-Celestion. Ltd.
Roilet, H.. $\&$ Co., Ltd
Rubber Bonders, Ltd
Runbaken Electrical Products
Ealford Electrical Instruments. Ltd.
Sallis, A. T
Samsons surpius stores
Savage Transformers. Ltd
Scharf. Erwin
Sherman's Supply Co
Sifam Electrical Instruments Co.. Ltd.
Sky-Masts
Smith, G. W. (Radio) Ltd.
Smith, H. L., \& Co.. Ltd.
Solartron Laboratory Instruments, Ltd.
Southern Radio Supply, Ltd.
Spencer-West

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Stratton & Co.. Ltd. (Engineers), Lid.
Sugden, A. R., \& Co. (Engineers), Lid.
``` Supacoils Szymanski. S.
Tannoy Products, Ltd
Taylor Electrical Instruments. Ltd.
Technical Suppliers. Ltd.
Telegrapt Lid. ............................. 128
Telegraph Condenser Co. Lid. 6, 7. Cover Iti Telegraph Construction \& Maintenance Telemechanics. Lid

\section*{Telemechanics. Ltd. Lid}

Tele-Radio (1943), Ltd.
Transradio, Ltd. Electrical Co. Lid. Universal Electronics
Universal Engineering Co.
University Electrical Instruments Corpn

\section*{Valradio. Ltd.}

Venner Accumulators, Ltd
Verdik Sales. Ltd.
V.E.S. Wholesale Services. Ltd.

Vickers-Armstrongs. Ltd.
Viscose Development Co.. Lid.
Voigt Patents.
Vortexion. Ltd.
West End Radio. Ltd.
Westinghouse Brake \& Signal Co.. Lid
Wharfedale Wireless Works
Wikinson. L.
Willesden Transformer Co.. Ltd.
Winter Trading Co Ltd.
Woden Transformer Co., Ltd
Wolf Electric Too's, Lid
Woolwich Polytechnic
Wright \& Weaire. Ltd.
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