

# Radio-Electronics

FOR MEN WITH IDEAS IN ELECTRONICS

## SPECIAL ISSUE — 4-CHANNEL STEREO

**FOUR-CHANNEL FM**  
**9-Ways To 'Go**

**DISCRETE 4-CHANNEL RECORDS**  
**Setting Up A System**

**4-CHANNEL EQUIPMENT**  
**What's Available Now**

**4-CHANNEL**  
**RECORD**  
**REVUE**  
**R-E Rates**  
**The Effect**

**IC FM CIRCUITS**  
**How They Work**

**PLUS**

**State-Of-Solid-State**  
**Voice Actuation For Phone Sent**  
**R-E's Replacement Transistor Guide**



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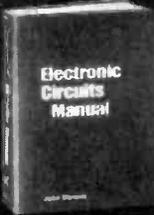
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## SONY PS 2251: a declaration of independence.

Independence of belts, pulleys, idler wheels and all the other paraphernalia that can cause wow, flutter and rumble. Independence from fluctuations in power line voltage that can effect the precise speed of the turntable. And independence of acoustical feedback. The new, direct-drive Sony PS-2251 has declared itself independent of all these potential intruders upon the enjoyment of your records.

Most turntables use belts, pulleys, idler wheels to make their turntables spin at the record's speed, instead of the motor's. Look underneath Sony's new PS-2251 and all you'll see is the motor. We don't need all those extras, because our motor's speed is precisely the same as the record's.

Eliminating all those parts also eliminates the wow and flutter and rumble they can cause. So, our rumble figure is a remarkable  $-58\text{dB}$  (NAB).

And because our motor turns so much slower than conventional ones, the rumble frequency is lowered too, making the rumble even less audible than that  $-58\text{dB}$  figure indicates.

To maintain precise speed accuracy at slow speeds, we use an AC servo system (superior to a DC servo system because of its uniform magnetic field strength). Its precise speed is not affected by variations in line voltage or in line frequency. But its speed can be varied  $\pm 4\%$  by the built-in pitch control and returned to a precise  $33\frac{1}{3}$  or 45 rpm, with the built-in self-illuminated strobe.

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it from externally caused vibrations. At \$349.50 (suggested retail) including arm, wood base and hinged dust cover, the PS-2251 is today's most advanced turntable.

We also offer a moderately priced, single-play component turntable with the convenience of automatic operation, the PS-5520. The complete system: turntable, arm, walnut base and hinged dust cover, \$159.50 (suggested retail) Sony Corporation of America, 9 West 57th Street, New York, New York 10019.



Circle 3 on reader service card

# Radio-Electronics

FOR MEN WITH IDEAS IN ELECTRONICS

More than 65 years of electronics publishing

OCTOBER 1973

## 4-CHANNEL SOUND HI FI AUDIO

- 29 **4-Channel Equipment Roundup**  
If you're ready to move 4-channel sound into your home, there is a wealth of equipment to select from. Here's a thumbnail sketch of what's available.  
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- 33 **Set Up For 4-Channel Discrete**  
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Two new IC's perform as FM detectors. One is for FM tuners, the other for TV audio. See how they work. *by Steve Leckerts*

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Last June we showed how you could build an automatic telephone answering machine. Now you can add voice actuation. *by Roger Smith*
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*compiled by Robert & Elizabeth Scott*

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## ON THE COVER

4-channel equipment shown this month includes four AR-3A speaker systems and a Sansui QRX-3500 4-channel receiver. The girl is optional, and each reader will have to supply his own.



4-CHANNEL DISCRETE records are growing in popularity. Learn how to set up the playback decoder. . . . see page 33



TYPICAL 4-CHANNEL amplifier. For a run-down of available equipment . . . see page 29

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# looking ahead

## Home TV readout

LONDON—A new home television service, designed to provide written material on demand, is currently undergoing on-the-air tests in Great Britain. Set manufacturers and broadcasting authorities are confident that it will be placed in commercial operation as the next major home electronic product.

Two systems are currently under test, and both operate in a similar method—sending written material for on-screen display during the vertical blanking period of the regular broadcast TV period. The technique developed by British Broadcasting Corporation (BBC) is called "Ceefax," while the Independent Broadcasting Authority (IBA) uses the acronym "Oracle" (standing for "Optional Reception of Announcements by Coded Line Electronics").

In each case, the consumer uses a telephone-type pushbutton array to select the material he wishes to view. The material is sent in "pages"—one "page" being one screenfull of information. The first few pages comprise the index. If, for example, the viewer wishes to see the up-to-the-minute weather forecast, he observes from the index that it is on page 28, then dials "2-8" and the forecast instantly starts to unfold on his screen.

Material suggested for these TV "marginal notes" includes news, stock market reports, TV program logs, theater and concert calendars, police and traffic information, ski reports, programmed-learning quizzes (with answers on another page). Generally, the material would be presented in black on a white screen or vice versa, but several pages would be reserved for a line or two of text to be superimposed on the top or

bottom of the screen while the television picture is appearing. Among these would be special services such as subtitles for deaf or foreign-language viewers, and a "news flash" page which would keep the viewer informed of breaking stories of top importance while he's watching TV. For details, he could dial up the "news page." Similarly, the weekend fisherman and small-boat owner might dial-up in-shore weather and the latest dope on what's biting and where.

The transmitting equipment for both systems requires a small computer with storage capacity for the number of pages to be sent. At the receiver end is an integrated-circuit character generator which responds to digital pulses sent by the station during the vertical interval period, and a memory to store the information.

The Ceefax system uses two unoccupied lines in the vertical interval and sends out 32 pages, each with a maximum of 750 letters or numbers. All of these pages are re-scanned (and can be updated) every 15 seconds. Oracle occupies only one line of between-pictures space, accumulates a "book" of 50 pages, each with about the same number of characters as a Ceefax page, updated in a little less than two minutes.

BBC officials estimate that a black-box adaptor to add Ceefax to a standard TV set would cost about the price of a black-and-white TV receiver. If Ceefax were built into new sets, it would add about \$50 to the retail price. BBC hopes to get enough digital information into its signal to permit deluxe receivers which will provide upper and lower case letters and letters or lines in different colors for easier reading, while standard receivers would get the same material in all capital black-

and-white letters.

An alternative or add-on system is also planned. This is a single "page" which is constantly changing. One page—say Page 32—could be devoted to this high-capacity service, which could provide 1,357 different screensfull of information in a day. The viewer could dial the information he wants by finding out exactly what time it's scheduled to be transmitted. Alternatively, his receiver can incorporate a "dial now—read later" feature. Using this system, he would feed into his pushbutton dial the exact time the page he wishes to see will be transmitted. Then it would be stored for later viewing.

Both Ceefax and Oracle are relatively simple first steps toward a home data terminal. Oracle is already being studied by the British Post-office Department (which operates the telephone system) for use in conjunction with the telephone and a central computer to provide vast amounts of information. Under one proposal, the TV set might eventually eliminate the printed telephone directory, permitting the user to get any phone number quickly and automatically on his home screen.

## Shifting to discrete

Although the SQ matrix system is currently dominating the quadriphonic phonograph record and radio scene, audio marketers increasingly are predicting that discrete four-channel systems will end up winning the race. The major discrete system, developed in Japan by Matsushita Electric (Panasonic) and Japan Victor (JVC), is the CD-4 technique, the refinement of which was undertaken by RCA Records under the "Quadradisc" trademark.

One of the early drawbacks of discrete discs was the high cost of cartridges and the precision required in the manufacture of turntables for the system. This threatened to reserve the CD-4 system for the affluent and hobbyists willing to sink plenty of cash into their equipment. Now, a British record-changer manufacturer, Glenburn, says it has come up with a CD-4 record changer to sell at about \$60, including ceramic cartridge. An integrated-circuit CD-4 demodulator, developed by Quadracast Systems Inc.—and said to be the largest linear IC ever developed for a consumer application—is being offered to manufacturers.

While well over 100 FM stations are currently broadcasting 4-channel sound using the SQ matrix system—which requires no special studio equipment—the National Quadraphonic Radio Committee (NQRC), organized by the Electronic Industries Association, has been compiling specifications on 10 proposed discrete 4-channel FM broadcasting systems and plans to begin field tests early next year.

Among the discrete broadcast systems are the pioneer Quadracasting system and techniques developed by both GE and Zenith, which are given joint credit for today's FM stereocast system. Although RCA has been pushing CD-4, Zenith gave the first indication it would go along with discrete record-playing equipment when it showed an "audio center of the future" containing a CD-4 player. To avoid the problem of speaker cables, Zenith's system uses wireless rear speakers which pick up their signals via infra-red transmission.

by DAVID LACHENBRUCH  
CONTRIBUTING EDITOR

# Here's everything you'd expect from a high-priced portable VOM.

## Except a high price.

The VOM is one of the most important tools in your kit—but you needn't pay high prices to get the features and quality you want. Like the high-priced units, the B & K model 120P VOM has features like a front-resettable overload protection circuit, preventing damage to the instrument and components should an overload occur.

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of 35 ranges, measuring DC volts and current with 0.25 volt and 50  $\mu$ A low-range scales; AC RMS volts, output volts, and decibels; and ohms. That makes it one of the most versatile test units ever designed. But it's also one of the most rugged—its meter movement is a taut-band, self-shielding annular type, to withstand damage from shock or vibration.

You'll also appreciate the 120P's easy-access battery and fuse compartment complete

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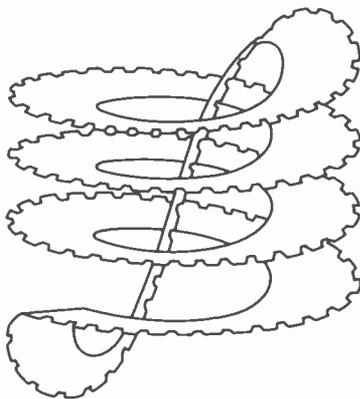
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# new & timely

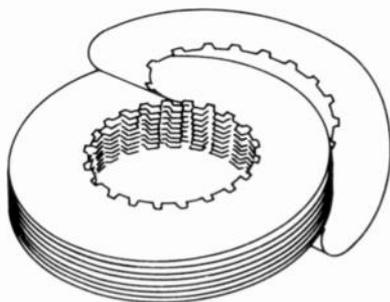
## New continuous-loop tape uses no capstan nor reel

A new tape system for applications where endless tapes are used stacks the tape with one layer resting flat on the preceding one. The tape therefore does not need a reel. Notches in the edge of the tape line up to make the stack a sort of gear, which is engaged by a gear on the drive motor. Thus the tape is driven without the help of a capstan.

The new *Helicassette* tape comes in two types. One, called S, is driven by gear notches on the outside of the stack.



S-TYPE



Z-TYPE

The tape is lifted from the top and returned to the bottom of the stack through the center. The Z-type has the notches on the inside edge of the tape, and the tape is returned to the bottom via the outside of the stack.

Claimed advantages of the new tape are simpler drive mechanism, reversibility (not possible with other continuous-loop tapes), no friction and therefore no need for special lubrication. Tape widths can range from 1/4 inch to 2 inches. One unit now being demonstrated has a 3/4-inch, another a 2-inch tape. Lengths can run to 1200 feet, and a 3/4-inch tape can

have as many as 25 tracks.

The design comes from France, and is being sold in the United States by Y Square Associates of California.

## Survival stretcher saves lives of patients enroute to hospital

Heart disease, America's No. 1 killer, is unique in that the victim of a sudden heart attack may have only sec-



**LIFE SUPPORT SYSTEM** keeps victims of heart attacks alive on the way to the hospital. The oxygen equipment is seen at the head of the stretcher. The upright cylinder with the straps is the heart-lung resuscitator, which compresses the patient's chest, breathing for him. Further down is the combined electrocardioscope and the Pacemaker, with the defibrillator and its large hand-held electrodes. Batteries and an oxygen tank are also built in. The equipment swings up clear of the patient when the stretcher is used.

onds to live if effective aid is not immediately at hand. More than half the deaths due to acute heart attacks occur on the way to the hospital. A New York City heart specialist, Dr. Nicholas A. Pace, has designed an "electronic stretcher" to give the patient immediate assistance, when he needs it.

Besides electrocardioscope equipment, which makes it possible to monitor the victim's heart condition and apply immediate aid, the unit includes a heart-lung resuscitator that breathes for the patient, a defibrillator that can shock a randomly fluctuating heart back into regular pumping action, and a Pacemaker that can synchronize it and keep it beating regularly. The electrocardioscope also provides a graphic record.

Drawers for necessary drugs and

other items are included in the rolling stretcher, as well as batteries and an oxygen supply.

Designed primarily for heart cases, the unit is also useful in cases of electrocution, drowning, wound or other asphyxiation and even drugs. The system is already in production, and a number have been installed in large-city business offices, as well as in the Pentagon.

## Virginia State Association supports national unity

Reaffirmed support of the proposed merger of the national electronics associations and of state licensing highlighted the business sessions of the 9th annual convention of the Virginia Electronics Association, held late in June at Tyson's Corner, Va.

John McPherson of Yorktown was reelected president for the 1973-74 term. Wayne Appelman of Richmond was reelected first vice president, Everett Kilby of Manassas, second vice president; Jane Hudson of Lynchburg, recording secretary, and Joe Jackson, Madison Heights, treasurer. Elected to their first terms were J. Cobb Laine, Suffolk, third vice president, and Art Pearsall, Norfolk, secretary general.

Certified Electronic Technician tests were held throughout the convention. Dick Glass, executive vice president of the National Electronic Associations, addressed a special Saturday luncheon, which honored the state's 74 CET's.

The VEA ladies auxiliary scheduled



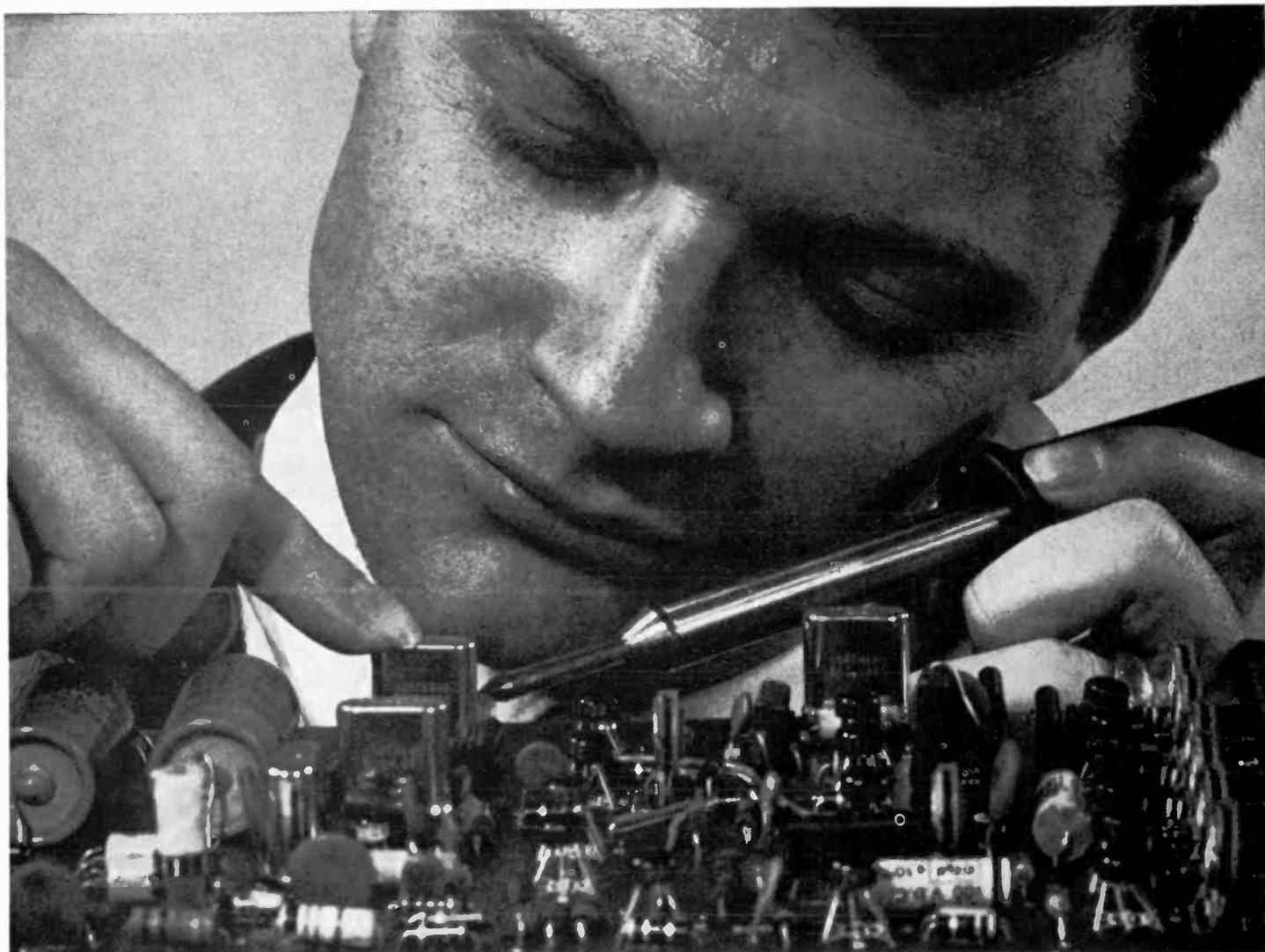
**AT THE VEA SPECIAL CET LUNCHEON.** Left to right: Larry Steckler, Stan Prentiss, Phil Dahlen, Charles Porter and Jim Teeters, all CET's.

an enjoyable evening at the Wolftrap Theater before the convention. Anne Mitchell of Hampton was elected president of the auxiliary; Lu Cole, Colonial Heights, vice president; Anita Laine, Suf-

(continued on page 12)



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Like this phone-cw transmitter (Kit #7 in the Communications course) is engineered from chassis up to demonstrate principles you must know. NRI does not use modified hobby kits for training, but the finest parts money can buy, professionally and educationally applied.

folk, secretary, and Anne Cooke, Hampton, treasurer.

Phillip Dahlen, Editor of *Electronic Technician/Dealer* magazine and chairman of the International Society of CET's, was the featured banquet speaker. He was awarded an honorary membership in VEA for having "proven his friendship and concern for the profession he serves." Others attending and participating were Stan Prentiss (associate editor, *Tab Books*), Larry Steckler (Editor, *Radio-Electronics*), Mary Anne Schurtz (Virginia Consumer Affairs coordinator), Dutch Meyer (General Electric national service manager), Bud Petzold (Motorola Service Manager), Paul King (Sylvania service representative), Jesse Leach (NEA Region 1 vice president) and Walter Cooke (NEA Region 2 vice president, VEA's past president and recipient of the President's Plaque for outstanding services to VEA).

M. L. Finneburgh, Sr., installed the officers at the Saturday evening banquet and drew a resounding ovation with his Sunday dissertation on the need for industry and association unity.

## Nickel-cadmium battery charges in 15 minutes

A newly designed rechargeable battery, the General Electric *PowerUp-15*, reaches 90 per cent of its maximum capacity in 15 minutes of fast charge. At that point the battery may be put into use, or left to charge further. If left on charge, the current immediately drops to a "topping charge" rate, which brings the battery up to full charge in about two hours and can be continued indefinitely without damage to the cells.

The new battery is designed to accept a charge four times the ampere-hour rating (for example, a 4-ampere charge for a 1 ampere-hour battery) and a topping or trickle charge of 0.1 the ampere-hour rate (0.1 A for the same 1 AH battery).

The safe fast charge is made possible by improved design of fast-charge cells, and sensors that monitor independently both the voltage and the temperature rise in a cell. Thus the charger will go into topping charge when the battery either reaches the desired voltage or rises above a predetermined temperature, as signaled by a thermistor or thermostat buried in the battery pack. Maximum charging voltage is 1.5 volts per cell and temperature 120° F (49° C).

(The charger is usually set somewhat below these limits for reliability.) The battery comes in all the standard GE sealed cylindrical cell sizes from 100 mAH to 3.5 AH.

The new battery meets the same performance and reliability specifications as the standard GE nickel-cadmium line. The new 15-minute charge feature will, GE spokesmen believe, make it more useful for a wide range of applications, ranging from cordless industrial and garden tools through a wide range of household and hobby devices to portable communications equipment.

## Harry Secor 1889-1973

We regret to announce the death on May 17 of the oldest Gernsback editor (both in age and in length of service), Harry Secor. He died shortly before his 85th birthday and had been employed in the Gernsback organization over a span of 54 years.



Old timers may remember the byline H. Winfield Secor which first appeared in *Modern Electrics* around 1910 or 1911. He became an employee of Hugo Gernsback in 1913 when he joined the staff of the *Electrical Experimenter*. In 1915, with S. Gernsback and Austin Lescarbourea, he co-authored the pioneer radio text: *Wireless Course in 20 Lessons* which was published by the Electro Importing Company. In the 20's he was on the staff of *Science and Invention* and in the 30's he was the managing editor of *Short Wave Craft* and, for a brief period in 1941, the managing editor of this magazine when it was still called *Radio-Craft*.

During the post-war years and up until his retirement in 1967 when he reached his 80th birthday, Mr. Secor continued work on various editorial projects in the Gernsback organization.

He will be missed by all his associates.



**NEW COLOR SET IS READY FOR CABLE.** Late line of RCA receivers (XL-100) is built for vhf and uhf reception off-the-air, as well as cable TV without an external converter. The photo shows RCA's John Meelan holding in his right hand the built-in unit that replaces the former separate 24-channel selector he holds in his left hand. The new receiver features, as well as vhf, uhf and 24-channel cable reception, wireless remote control, automatic fine tuning, instant picture, and Cable Guard shielding, to eliminate interference from local TV signals.

## New telephone extension operates without wires

A new slant on the cordless telephone is offered by the *Rovafone*, produced by Fonetron of Milwaukee. Unlike the cordless instrument described in the July issue (pages 7, 12) this device is not connected direct into the telephone system, but is an extension working with the user's telephone installation. Also unlike the one mentioned in July, this instrument is in actual production and available.



It consists of two units, an ordinary telephone fitted up with an FM transmitter and receiver with a range of several hundred feet (*Rovafone*) and a *Tele-*  
*(continued on page 14)*

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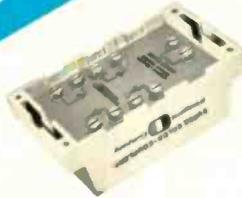
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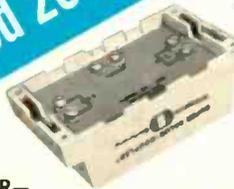
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**CC-282 82 CH. 2-SET COUPLER**—Efficient 300 ohm coupler connects two TV-FM sets to a single 300 ohm download. Input and output connections are handy no-strip type for easy installation. Quality circuitry insures perfect color and black and white reception.



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This is the control center praised by that dean of audio, Ed Canby: "This IC150 . . . is the finest and most versatile control unit I have ever used. For the first time I can hook all my equipment together at once. I find many semi-pro operations possible with it that I have never before been able to pull off, including a first-class equalization of old tapes via the smooth and distortionless tone controls. I have rescued some of my earliest broadcast tapes by this means, recopying them to sound better than they ever did before."

The IC150 will do the same for you. You could record from any of seven sources: tuners, turntables, guitars, tape players, microphones, etc. You could also tape with one recorder while listening to a second one. Even run two copies of the same source at once while monitoring each individually. How about using the IC150's exclusive panorama control to improve the stereo separation of poorly produced program material or to correct that ping-pong effect with headphone listening? It's all up to your creativity.

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Of course, construction is traditional Crown quality, backed with a three-year warranty. The price is \$299. The enjoyment is unlimited. The opportunity is yours. Visit your local Crown dealer to discover if you are ready for a real control center, the IC150.



**CROWN**

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Circle 7 on reader service card

**new & timely** (continued from page 12)

tron base unit, connected to the electric and telephone lines, which makes it possible to receive and dial calls in the usual way.

The equipment is especially useful in restaurants, meeting rooms and other "hospitality industry" areas. The home owner will also find it particularly useful in the back yard—he can get involved in gardening or a barbecue without the fear of missing a phone call. And the *Rovafone*, since it has no electrical connection, is one unit that is absolutely safe in the bathtub or swimming pool.

### Maine ETA elects officers for 1973

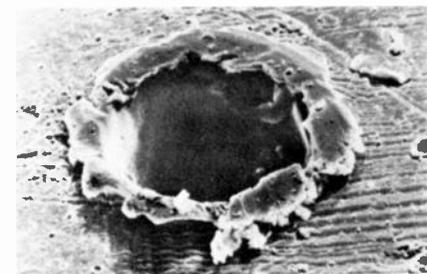
At the Annual Convention of the Maine Electronic Technicians' Association, held June 9 and 10 at Sebasco Estates Lodge, Manley Lane, CET, was elected president for the fiscal year of 1973. Keith Marquis was elected first vice president; Joseph Pomerleau, second vice president; Theodore Stackhouse, CET, treasurer; and Maynard R. Young, Sr., CET, secretary.

The convention was well attended, and attracted a number of outside vis-

itors including Larry Steckler, CET, Editor, **Radio-Electronics**. The members were addressed by Earl Gove, secretary-general of NATESA and State secretary of Vermont, and by Leon Howland, CET, State president of Indiana.

### Electron microscope photo shows tiniest moon crater

A crater made on the moon by a micrometeorite, and brought home by the Apollo 16 astronauts, is only three-hundredths of a millimeter in diameter, the



thickness of the finest of human hair. Under the scanning electron microscope of the Siemens laboratory at Karlsruhe (Germany), it shows the raised rim of a true moon crater. **R-E**

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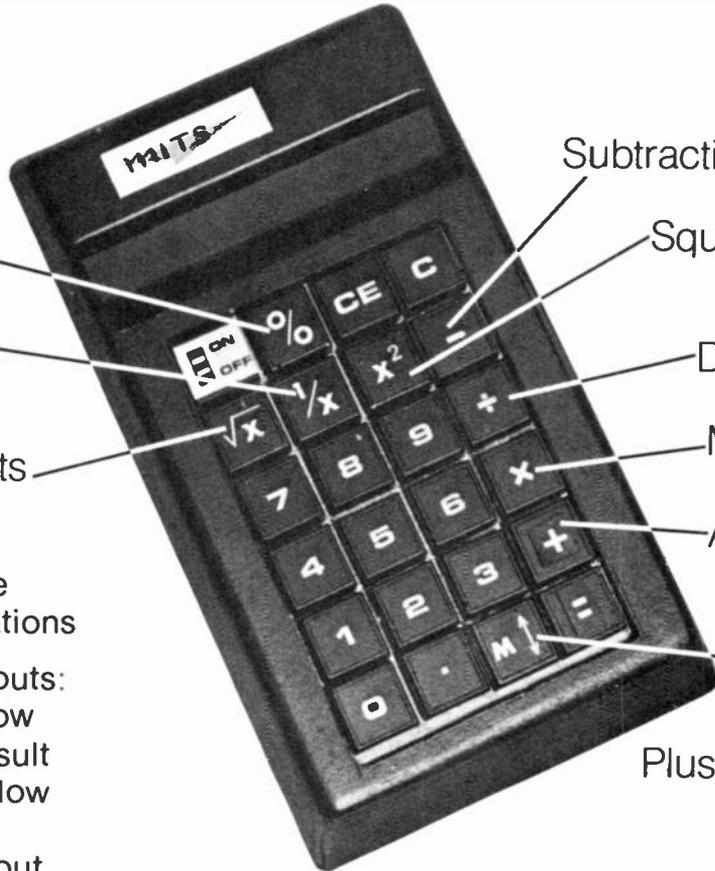
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RE-10

Circle 8 on reader service card

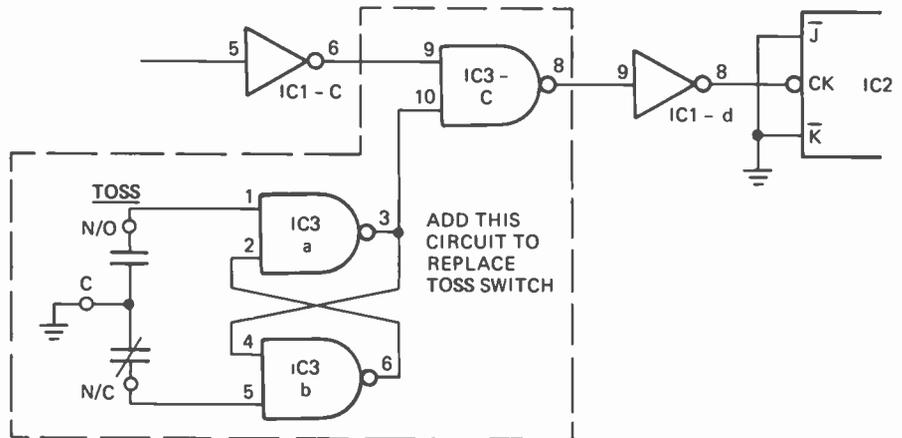
# letters

Mr. Goegl ("Circuits", *Radio-Electronics*, July 1973 page 90) is about to be trapped by a very common bug. I was snared by it a few years ago when I began getting my feet wet in the weird and wonderful world of high-speed logic.

If John will use a small clip-lead and ground pin 6 of IC-1 (assuming the TOSS switch is a common garden variety dry switch), he will find the "dice" to come up as randomly as they did before the short. The reason is simple but elusive; the contact bounce of the switch will toggle the J-K flop several times (in some cases, hundreds) and no matter how carefully or quickly the switch is operated it will bounce.

There are two ways to overcome the difficulty.

1. Use a mercury-wetted contact switch. These switches have no bounce, but are position sensitive and therefore must be operated in an upright position.



2. The second solution is cheaper and simpler but requires more logic and a SPDT switch (see attached sketch). The latch formed by IC3-a and IC3-b squares and deglitches the contact closures. IC3-c then gates the output of

the oscillator to the input of IC1-d (which isn't required and may be omitted.)

I'm not writing this to be a nitpicker, it is a real problem whenever mechanical switches are interfaced with digital logic. I hope this letter, if printed, will save *(continued on page 22)*

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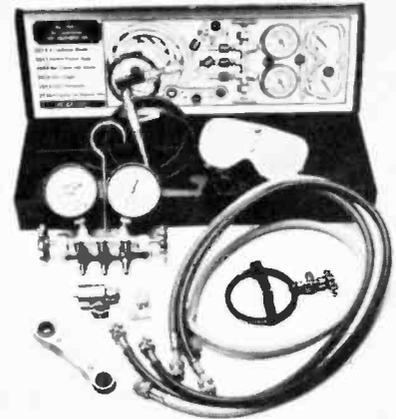
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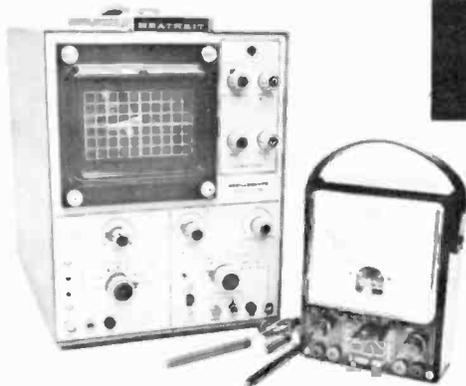
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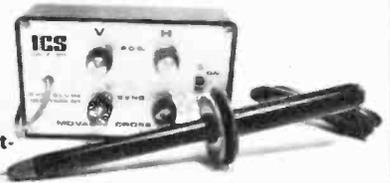


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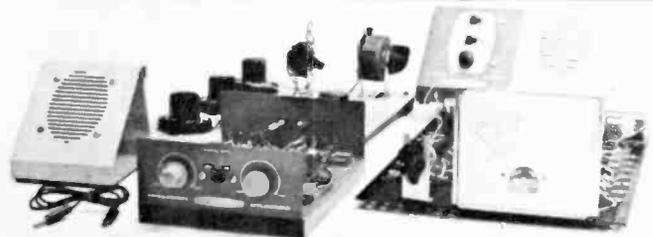


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Circle 10 on reader service card

**LETTERS**

(continued from page 16)

someone the time that can be wasted looking for this kind of problem.  
AL Woods  
Houston, Tex.

**ANOTHER TOSSED COIN**

I am probably one of many people writing to point out a minor error in the July 1973 Reader Circuits (page 90). The J and K inputs of the electric coin tosser, if grounded, will make the toss rather one sided, as the flip flop will be inhibited from changing states. Possibly your artist erred, and J and K should ei-

ther be left open or connected to  $V_{cc}$ .  
STU RASMUSSEN  
Beaverton, Oregon

**AUTHOR REPLY**

Thank you for allowing me the opportunity to comment on Mr. Rasmussen's letter pertaining to my TTL coin tosser circuit.

My comments: Strictly speaking, pins 5 and 9 of the 7470A (DIP) are "complementary" rather than "true" J and K inputs and should be designated  $J^*$  and  $K^*$ . Thus my diagram is correct in showing pins 5 and 9 connected to ground ( $-V_{cc}$ ) as they must if the 7470 is going to toggle.

Additional comments: Connecting

these pins to  $V_{cc}$ , will, in fact, inhibit the 7470 and prevent it from toggling. I suggest that readers interested in building a tosser use DIP type IC's. Then they can wire per my diagram pin-for-pin.

These comments don't apply to Mr. Rasmussen's letter so I'm keeping them separate.

I have been questioned as to the probability of the tosser's output. Frankly, I don't have the time to make a detailed analysis, mathematically. My opinion is that for a single "toss", the circuit will give equal heads-tails odds.

Other published tosser circuits (for example, see "Heads 'N' Tails", *Popular Electronics* Jan. 1972, page 35) have relied on the ac line as a toggling source. One author pointed out that with this approach a symmetrical waveform can be derived, whereas a multivibrator-generated waveform is usually at least slightly asymmetrical. This asymmetry, it was argued, causes a built-in bias which results in unequal heads-tails probabilities.

The multivibrator "clock" which I used in my circuit does generate an asymmetrical waveform. However, since the 7470 J-K F-F is an edge-triggered type (positive) it will only toggle on the positive-going edges of the clock waveform. Thus in practical circuits the degree of waveform asymmetry has no effect on the probabilities.

Aside from the fact that my tosser is compact and portable, its freedom from the ac mains is a definite safety advantage. When used by the inquisitive young set or where used in basement rec rooms, on the patio, or near the pool, battery power is on the way to go. Check?

JOHN GOEGL, WA2LJK  
Union, New Jersey

R-E

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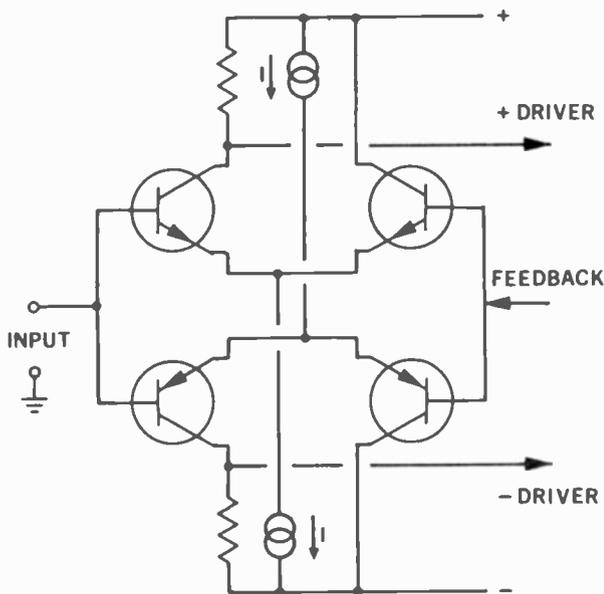
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We think that our new push-pull cross coupled input circuit represents a major advance in amplifier design. Those of you who are familiar with amplifier circuits will recognize this as two complementary differential amplifiers, with the input and feedback points tied together. This elegant little circuit makes possible a completely push-pull amplifier.

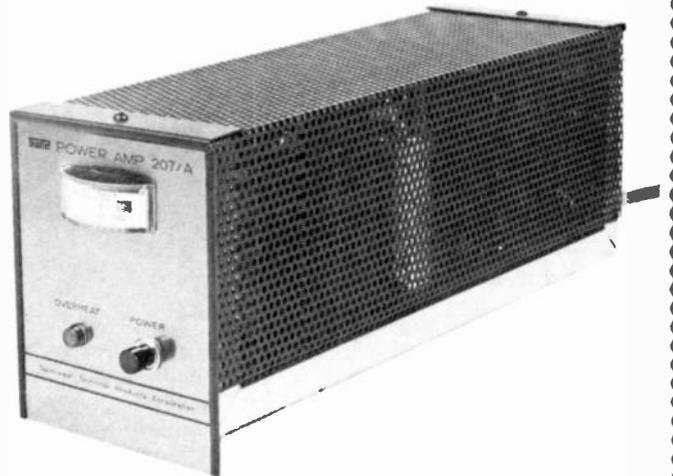
Push-pull circuits produce distortion when they amplify just like any other circuit, but with one important difference. The upper and lower halves of a push-pull circuit produce even harmonic distortions that are equal but opposite in phase. They will therefore cancel each other out for the most part when combined at the output. Almost all transistor amplifiers use push-pull output and driver stages, but only our new #198 preamp and #207 amplifiers are push-pull throughout.



The "Tiger .01" #207/A amplifier using this new circuit is packaged in a neat little quarter rack chassis and is supplied with the perforated cover shown. This allows you to assemble a system with any number of amplifiers you might want and to later expand the system if you wish.

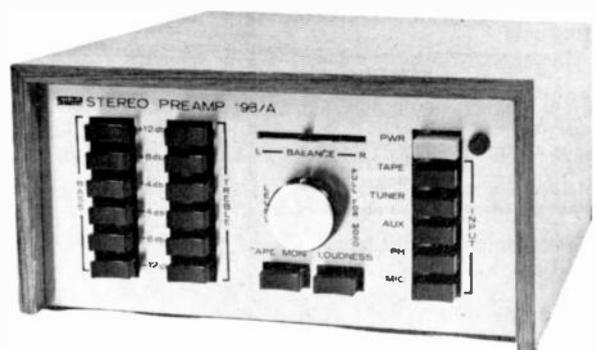
The #198 preamp uses the same basic circuit as the power amplifier and has similar outstanding performance. All inputs and tone control settings on the preamp are push button switch selected. The construction is primarily on two "mother boards" so wiring is kept to an absolute minimum.

For instant shipment, call us and use your Mastercharge, or Bankamericard. For more details on our kits circle on the reader service "bingo" card and I will get a copy of our latest catalog to you as quickly as possible.



### #207/A AMPLIFIER KIT...\$75.00...14 lbs

How much better is this type circuit? Considerably. The total harmonic distortion of the power amplifier is typically .02% up to full rated output of 60 Watts at 1,000 cycles. The really interesting thing though is the fact that the intermodulation distortion is less than .01% up to rated output. This circuit is therefore anywhere from around ten to a hundred times cleaner than previous designs. Now it is generally recognized that IM distortion correlates much better with listening tests than harmonic distortion. Our ears are much more sensitive to distortions that are not harmonically related to the signal. This performance is obtained with a circuit that has only 65 db open loop gain. To even approach this type performance before this required open loop gains from 80 to 120 db, 60 to 100 db of negative feedback will give you low distortion with almost any kind of circuit, but the resulting stability problems might make you wish for a better way.



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# appliance clinic

## ELECTRIC CARVING KNIVES

by JACK DARR  
SERVICE EDITOR

THE ELECTRIC CARVING KNIFE IS A handy thing. It can even make Pop look good when he carves the Thanksgiving turkey or slices fresh bread smoothly. They're pretty simple things; a little motor, a wee gear-box to change round-and-round to back-and-forth (All right; rotary to reciprocal), a pair of blades, and a plastic box to hold the whole thing together. There are two types, ac-powered and battery run, usually called electric and cordless, although both are, obviously, electric.

Repairing one that won't work is pretty simple. The first thing to do is to take out the *blades*. If you don't, and if it wasn't running, but starts up suddenly, you may get to be known as *Three-Finger* from now on.

The cases are usually easy to open. They're made in two parts; one holds the motor, gearbox, etc. and the other is just a cover. Look for small, recessed screws at each end, usually Phillips.

Remove all visible screws, and then (Gently!) try to pry the cover off. If it won't come off, don't use muscle. There's another screw or fastener that you haven't found yet. Some cases have a small tongue on one end of the cover, which slips into a slot on the other half. If one end comes loose, try pulling on it gently, and it will come out. In certain makes, you'll find screws hidden under nameplates, labels and so on. Keep on looking; they're there somewhere.

In a dead one, first find out if you're getting power to the motor. Check for ac voltage where the line cord goes into the case, or read the battery voltage. If it checks out, test the switch. Most switches are spring-return or pushbutton types so the thing won't keep on running if you drop it. A lot of these are built so that you can take them apart, by removing a couple of little screws. The contacts are then visible, for cleaning and adjustment. (I did tell you to pull the line plug before doing this, didn't I? If I didn't, do it now.)

Most of the ac models, and some of the cordless types, have small

brush-type motors. Check the brushes and commutator. Brushes must be long enough and make firm contact with the commutator. Many have flexible leads; check them to make sure they aren't open or shorting to something. Brush holders are usually the open type, so you can see any troubles. The brushes are often held down by small springs.

If the commutator is badly pitted, or dirty, clean it up with fine sandpaper after you get the motor running. If it's smooth and shiny, don't mess with it; it's all right. These motors seldom need lubrication. If the rotor is stiff, or labors, check the gearbox first. If it must be oiled, one drop on each end is *plenty*.

Some cordless models use little sealed dc motors. If you can get the full battery voltage across the motor leads but the motor will not run at all, disconnect one motor lead and check for continuity. If the motor is open, replace it. In fact, if you do get continuity, but it won't run with normal input voltage, replace it. You can't take them apart. (They're like an egg; you *can* take 'em apart, but getting them back together is something else.)

All of the cordless models use rechargeable batteries, usually NiCad. These are permanently connected together with welded straps. The 5-cell 7.5-volt unit seems to be the most common. If the dc voltage is low, measured at the motor with the switch on (full load), check each cell of the battery, holding the switch on. If you read the normal 1.5 volts across four of them, and the meter shows a reverse polarity across one cell, or zero voltage, that cell is dead, and the whole unit must be replaced. All should read practically the same voltage, within about 5% or less.

If all cells show low voltage, the battery could be discharged. Recharge it overnight, then recheck. It would be a good idea to check the charging unit first of all. Plug it in, and read the dc voltage across its terminals, no-load. This should be just a little more than the battery voltage. Say about 8.5 volts for a 7.5-volt battery and so on. To check the charger for current, connect a small pilot light across the terminals; for a 7.5 volt unit use a No. 47 (6-8 volts, 150 mA). If the bulb

(continued on page 90)

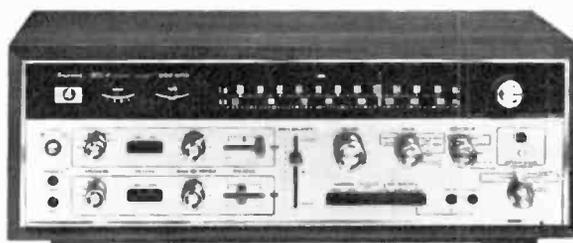


# vario matrix: the magic matrix by Sansui

The heart of the new Sansui QRX6500 is a unique electronic circuit called the vario matrix. There are other receivers with matrix decoding circuitry, and there probably will be receivers that claim to handle many different four-channel systems. But the Sansui vario matrix does more than just about any component available. For instance, it:

- decodes records, tapes and broadcasts made with the superior Sansui QS matrix encoding process;
- decodes SQ program material (and does it superbly);
- creates magnificent four-channel sound from regular two-channel sources (instead of offering you two two-channel amplifier sections strapped together for "double stereo" which doesn't sound nearly as good as synthesized four-channel);
- can position sound anywhere you choose, with a "Mode" switch that rotates the sound field 90°, 180° or 270° to create a totally-variable four-channel environment;
- accepts the output of a discrete four-channel demodulator via its "discrete" input position;
- can take auxiliary two- and four-channel inputs, as well as monitor one four-channel and two two-channel tape decks.

The vario matrix, coupled with a low distortion (less than 0.5%) four-section amplifier that delivers a whopping 280 watts (IHF) of power, makes this receiver a standout in its field. See it at your nearest franchised Sansui dealer soon.



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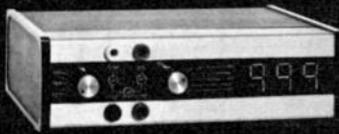
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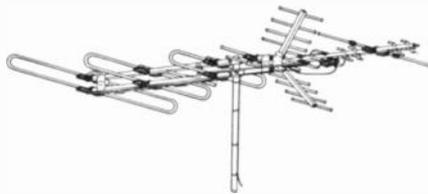
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# equipment report

## Kay-Townes ICA 500 TV antenna



Circle 92 on reader service card

WHAT A SURPRISE! HERE'S A RELATIVELY small antenna (boom length only 150 inches) intended for deep fringe areas, that weighs a mere seven pounds yet delivers outstanding results. The secret appears to be a matched package of carefully designed antenna plus a built-in high-gain low-noise amplifier.

We put the antenna up at a Long Island, New York location some 35 miles from the transmitters in New York City and about 80 miles from transmitters in Connecticut. The antenna we replaced was an 18-element log-log type that we had been using for the past three years.

The new Kay-Townes antenna, though smaller, is doing a better job than the antenna it replaced. We not only get near perfect reception from New York, but snow-free reception of the more distant Connecticut stations by merely rotating the antenna. This effectively adds two more (extra?) channels of viewing.

The ICA-500 is a vhf-uhf antenna with built-in preamp, designed for 75-ohm coax lead-in. Manufacturer's specifications show vhf gain to be 50 dB, uhf gain, 32 dB. Vhf front-to-back ratio 27 dB; uhf front-to-back, 29 dB. Beam width is a quite narrow 28°.

As you can see in the photo, the antenna uses folded dipoles cut for half-wave operation at low-band vhf. They are mounted on a sturdy twin boom. Since the folded dipole, not too common in modern TV antenna design, is comparatively broadband in normal operation, only three folded dipole elements are needed to give full coverage of the low uhf band. For high-band vhf reception passive elements are staggered along the two

booms to assure proper reception. A director element close to the front of the boom aids low-band gain while the corner reflector for uhf also contributes to high-band vhf reception.

The uhf portion of the antenna system also uses folded dipoles. Here two such elements serve as broadband driven elements. These in combination with a corner folded array plus a group of x-type directors assure excellent uhf response.

The gain of the antenna is, however, a combination of its design plus a built-in integrated circuit signal amplifier. This low-noise high-gain wide-band IC is specially made for Kay Townes and the specifications claimed for it are 20 dB gain, flat from 50 to 1000 MHz, and a noise figure of less than 4 dB across TV spectrum.

This also leads to one potential problem. When operating this antenna close to strong transmitters it is possible to overload it. When this happens you don't have to add a pad at the antenna terminals. Just turn down the ZOOM CONTROL to reduce gain and avoid overloading. If overload occurs on only one channel plug-in pads are available to eliminate the problem.

The ICA-500 that we tested is a middle-of-the-line antenna. There are two others. One, the ICA-100 is the smallest in the group and has a boom length of only 42 inches. It is recommended for fringe areas. The top-of-the-line unit, which we have not tested (it was not available at the time this report was prepared) is said to be engineered for ultimate television reception in hard to receive locations and ultra fringe areas. Vhf gain is said to be 33 dB, uhf gain, 35 dB and beam width is a narrow 24°.

One extra gained from an antenna of this type is its small size for the performance it offers. This means low wind resistance which in turn means simpler, less costly installation.

Our summary. This is a first rate TV antenna. It has special advantages in difficult locations where physical size, high gain, and narrow reception angle are vital. A worthy competitor in the battle for first-rate fringe area TV reception. **R-E**

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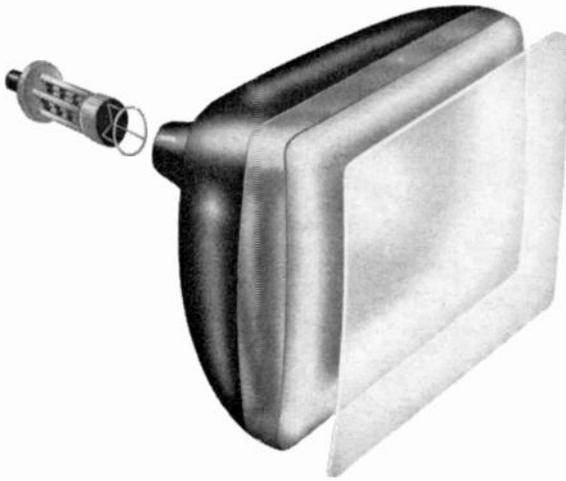
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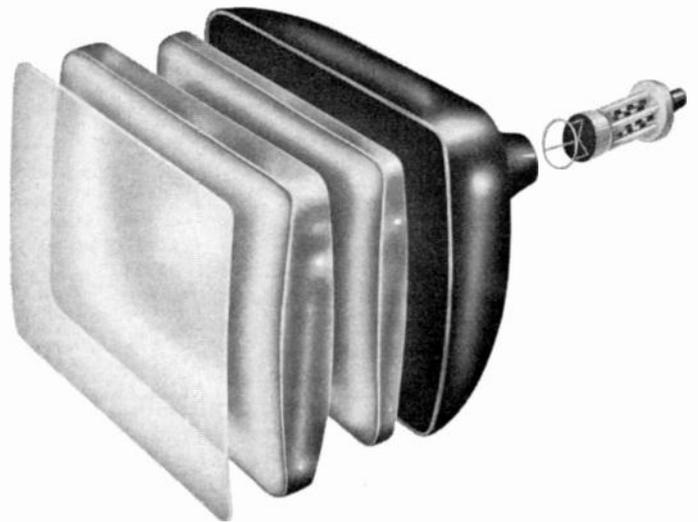
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**GTE SYLVANIA**

# 4-CHANNEL TAKES OFF

Ready to take the 4-channel plunge? Before you dive off the deep end, read this article and make sure you're up to date on the latest developments in equipment

by FRANCOIS MARKETTE

At just about the time the *Stereo Mat*, the newsletter of the Hi-Fi Dealers Association of Delaware was knocking 4-channel, the CES show in Chicago was jam-packed with displays of 4-channel hardware and customers looking to order that hardware. The truth of the matter is that quadriphonic sound has taken off like a rocket: the audiophiles are pounding on showroom doors trying to get a listen to 4-channel and the manufacturers are going all out to provide *quality* surround-sound hardware at the first go-around.

Unlike the situation that occurred

through pickups to speakers.

As far as amplifier and receivers are concerned nearly everyone is trying to touch all bases by using "strapped" or "bridged" output circuits, which for the purpose of "shorthand" I will refer to as *strapping*. Strapping is an electrical connection of the front and rear power output so that the present stereo-only enthusiast can utilize the available rear channels power output for stereo listening. For example, if the quadrisound amplifier provides four channels of 20 watts each, for stereo listening it becomes two channels of approximately 40

consumer with just the faintest thoughts of going 4-channel to upgrade in stereo *now* without fear his purchase will be obsolete in just a few months should he get the quadrisound itch.

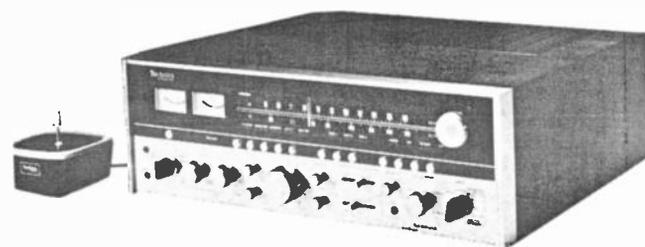
## The matrix war

For all practical purpose the so-called "matrix war" (which never really existed for practical purpose) is a dead issue. With few exceptions— and possibly no exceptions by the time you read this—equipment with QS decoding (or RM for *Regular Matrix* as it is termed in Japan) also has



HEATHKIT AA-2010 (left) is a complete 4-channel integrated amplifier and preamp. It includes front-panel speaker switching.

TECHNICS SA-6800X (below) is a new 4-channel receiver. Note the joystick remote control for setting up the 4-channel balance.



when stereo was first introduced, where virtually everyone listened to the pundits who claimed stereo was not that much better than mono so why upgrade, the manufacturers are not getting trapped into dipping their toes in to see if the water's warm, nor are they waiting to see if anyone salutes when they run up the flag. They tried this when stereo was introduced and dealers were stuck with "mountains" of add-ons, adaptors and second-rate equipment no one wanted. Virtually every manufacturer of truly hi-fi equipment has introduced an extensive line of *quality* 4-channel hardware—everything from receivers,

watts each. (Depending on the type of strapping circuit used the combined power output will range from slightly less to slightly more than two times the per channel output. For more details, see "Amplifier Strapping", *Radio-Electronics*, July 1973, by Len Feldman.) Among the many manufacturers who have chosen to follow the strapping idea originally pushed by Harmon-Kardon are Kenwood, Fisher, Pioneer, Toshiba, Sherwood, Pilot, Sanyo, Marantz, Sony, Akai and Onkyo. Though most still retain a line of quality stereo-only equipments the extensive selection of strapped 4-channel receivers and amplifiers allows the

SQ decoding. For example, the latest Sansui equipment has a matrix selection termed *phase matrix* which is their description of SQ. More typical examples, on the other hand, are Pioneer and Toshiba who use the standard terms QS and RM on the matrix selector switch.

The primarily American companies such as Lafayette Radio, Radio Shack and Marantz, whose equipment is made essentially for the U.S. market, are going all the way with SQ, for SQ is the "accepted" matrix standard for U.S. matrix records.

On some amplifiers and receivers you will find matrix decoders of the

"universal" type, such as used in Heathkit's AA-2010 and some Toshiba models. As proven by Electro-Voice's 4X-44 "universal" decoder, good results are obtained from universal decoders though SQ decoders are rapidly replacing the universal models.

As a general rule basic decoders with rather limited separation are used in lower priced models, with some form of logic-SQ or Vario-Matrix QS (RM) used in the higher priced models; an exception is Harman-Kardon, who has chosen to use an SQ decoder

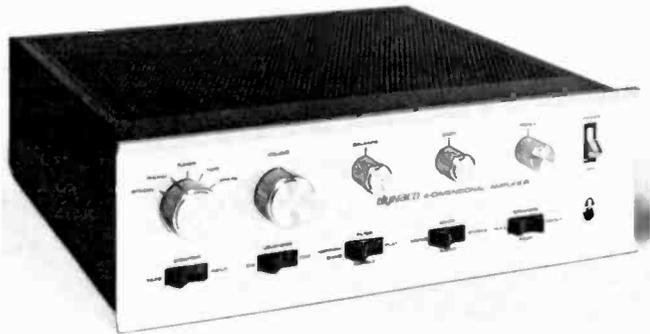
featuring wideband response and phase linearity approaching the specifications of the professional encoding equipment, thereby obtaining a surround-sound without the logic-pumping to which some listeners find objection.

### Synthesizers: 2-channel into 4-channel

Many amplifiers and receivers presently feature some form of ambience sound extraction from stereo records, often termed *synthesizer*. In

many instances this is obtained with a simple, or no, phase shift in the QS or SQ matrix decoder; in others the ambient sound is obtained through a "Dyna" circuit connection (passive) in the rear speakers. The advantage of the Dyna ambient sound extraction is that it provides a form of surround-sound at rock-bottom costs as the equipment is basically stereo, with just two power amplifiers. Teledyne-Olson, Sherwood and, of course, Dynaco are presently equipping their stereo equipments with the Dynaco "synthesized" rear output.

Though the biggest noise is presently being made over matrix decoders, discrete CD-4 is making heavy inroads into the better grades of 4-channel receivers and amplifiers. Pioneer already incorporates a built-in CD-4 demodulator in three receiver



DYNACO SCA-80Q is their 4-Dimensional amplifier combining both preamps and amplifier in one package.

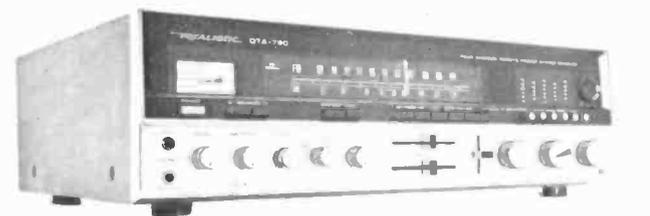
BSR McDONALD TD8QW (below) is a 4-channel 8-track tape player that automatically handles both 2-channel and 4-channel cartridge tapes.



TWO FISHER RECEIVERS, 4020 top and 4060 bottom, are equipped for 4-channel playback.



TOSHIBA SA-304 4-channel stereo receiver includes playback selector for regular matrix, SQ, and discrete.



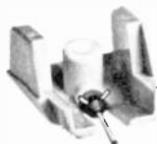
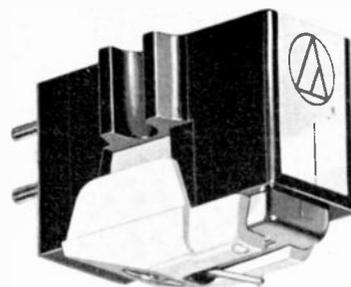
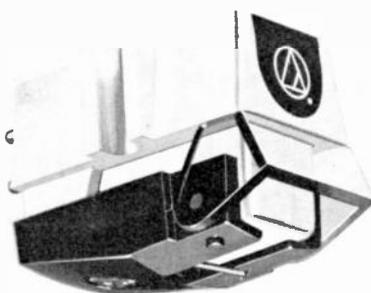
REALISTIC QTA-790 from Radio Shack (left above) is a 4-channel remote/preset stereo receiver. Favorite FM stations can be preset.



PILOT 366 (above) four-channel receiver offers matrix, decoder, and discrete modes for 4-channel playback.



LAFAYETTE LR-4000 (left) 4-channel receiver delivers several different 4-channel modes for playback of stereo and matrix discs.



AUDIO-TECHNICA AT14S (above) and AT15S (above center) are two new photo cartridges for playing CD-4 discrete records. Frequency response ranges to beyond 40,000 Hz to permit playback of subcarrier information. Both are dual-magnet stylus assemblies and are available with a variety of stylus types and sizes.

AUDIO TECHNICA AT12S (above) and a closeup of the dual-magnet stylus assembly (left). This unit is lowest-cost CD-4 cartridge in the line. Stylus assembly can be easily replaced when diamond stylus becomes worn. The cartridge will also play regular stereo as well as matrix discs without modification.

models, many other outfits such as Sanyo and Kenwood have at least one receiver model with a built-in CD-4 demodulator. Panasonic (Technics) and JVC, of course, have an extensive selection of equipments with built-in CD-4, while Marantz provides plug-in CD-4 demodulators for several models.

To accommodate quadraphiles who can't decide on CD-4 now, just about every receiver and amplifier manufacturer does what Onkyo does, providing several discrete hi-level and tape recorder connections for add-on

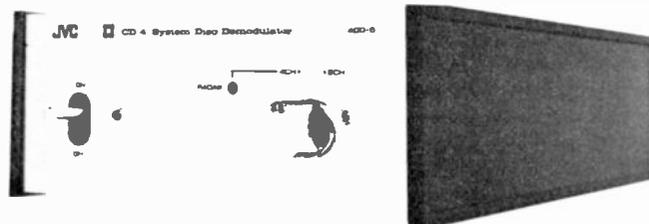
there's an endless assortment of quadraphonic automotive cartridge players from companies such as Hammond, names generally unfamiliar to the hi-fi enthusiast. Even matrix 4-channel is finding its way into the car through a matrix cartridge player by Tenna.

#### Tape & records

Virtually every manufacturer of hi-fi quality reel-to-reel recorders such as Pioneer, Panasonic, Sony and TEAC already has available or is ready to announce at least one model 4-channel recorder. The few holdouts

in the super quality and mass-market lines got burned in the past by coming out with half measures such as stereo record/4-channel play, but with top-of-the-line reel recorders still selling well, most of us expect the holdouts to join in just as soon as they're certain quadrisound isn't another passing fad. (But can you imagine the price of a 4-channel Revox A77?)

Though there is considerable talk about discrete 4-channel FM broadcasts and much interest in 4-channel 8-track cartridges and reel-to-reel tapes, the primary thrust of qua-



SONY HQR-600 4-CHANNEL stereo receiver (left). JVC 4DD5 CD-4 System Disc Demodulator (above).

CD-4 demodulators.

Though CD-4 demodulators were originally available only from Panasonic and JVC, several other manufacturers among them Pioneer and BSR-/Metrotech, have supplied photographs (but no specs) of upcoming add-ons, while Lafayette is firmly committed to a CD-4 add-on in their latest catalog (specs supplied so there's a working model).

Toyo, who virtually stood alone with RCA promoting 4-channel from 8-track cartridges is now being joined by the thundering herd. JVC, Akai and Wollensak are just a few of the big names into 4-channel cartridge players and recorders of high fidelity capacity. For those who like to be surrounded by sound while sitting behind the wheel of their Detroit Special

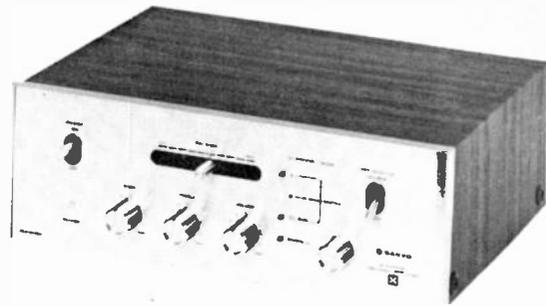


KOSS K/2+2 headphones (above) for silent listening to 4-channel music. 4-channel phones are fun to try. They do work.

SUPEREX QT-48 (left) Quad-tete four-channel headphones. One plug is for the front channels the other for the rear pair.



PIONEER QD-240 is a CD-4 demodulator for playing discrete records. Panel meter shows separation adjustment.



SANYO DCA-1600X 4-channel decoder amplifier is added to existing 2-channel stereo equipment setup.



AKAI AS-980 receiver includes CD-4 demodulator. Accessory remote balance control (right) is optional.



PIONEER QX-747 Quadraphonic Stereo Receiver has built-in CD-4, SQ, and RM (QS) decoders and demodulators.

drisound—both matrix and CD-4—is from records, where final sound quality is sharply determined by the performance level of the turntable, pickup arm and pickup. While the quality equipment from Empire, Thorens, Philips, Panasonic and JVC, among the turntable brands, is, of course, perfectly suitable for 4-channel because it's darn good from any point of view, CD-4 does require the most optimum tracking conditions, and the latest model automatic turntables from Garrard (the new Zero 100), Dual and BSR bring to CD-4 the same optimum "automatic" performance they delivered for stereo and matrix. For those who prefer to assemble their own turntable assemblies the Shure SME and Rabco arms remain among the best you can combine with any quality turntable.

### Phono pickups

As far as phono pickups are concerned we are fortunate because the accepted high fidelity models from all the top manufacturers such as ADC, Empire, Shure, Stanton, Pickering, B & O, Elac, etc., do an admirable job when it comes to matrix 4-channel, for the pickup that delivers optimum sound from standard stereo has proven to be as good when it comes to matrix.

CD-4 records, however, require an extended frequency response pickup for optimum results. At the time this article goes to press the selection of quality CD-4 pickups is limited to a handful from Technica (with Shibata stylus), JVC (selected Technica units), Pickering (special Pick-

ering design stylus) and a non-magnetic from Panasonic. In actual fact, most of the highest quality stereo pickups can be used for CD-4 reproduction with but a slight loss in overall performance. On the flip side of the coin, the quality CD-4 pickups are also suitable for high fidelity stereo reproduction.

### Speakers & headphone

Finally, we come to loudspeakers and headphones. The question most common in quadraphonic showrooms—after the usual "What is four channel sound?"—is "How do we squeeze two more speakers into the room?" This is the same question asked when stereo came along, only then the problem was to fit two speakers, not four. If quadrisound follows the same pattern as stereo the hi-fi purist will somehow manage to squeeze two more relatively large speakers into his listening room. For the rest of us, who will be sticking the "extra" speakers behind curtains, chairs and tables, the solution will be smaller speakers; just as stereo gave the impetus to the so-called "bookshelf" speaker, we can expect quadrisound to result in a multitude of "vest pocket" models, or some other descriptive term implying a speaker that can be tucked just about anywhere. Anticipating the need for smaller speakers AR and Dynaco introduced mini-models just about when surround-sound got rolling, and ADC, of course, has had a line of smaller high-fidelity speakers for quite a while. Though there are presently no hard facts concerning specific models of other "vest pocket" speakers, sev-

eral manufacturers or their reps have hinted at new, smaller speakers for the 4-channel market. If previous experience in stereo serves for quadrisound, by the time you're reading this you'll have an almost endless selection of miniature "quadraphonic speakers".

It's a shame to close on "4-channel" headphones because unlike all other aspects of quadrisound, where *quality* appears to be the keyword, much of the 4-channel headphone hardware is a ripoff on the consumer. We have reached the stage in 4-channel headphone design where each ear-piece consists of two relatively *large* speakers—supposedly front and rear. Now there is just not enough room around the ear for *two* transducers, so one, at least, radiates its highs into the side of the head where they are absorbed. The end result is "full range" sound from one transducer directly into the ear while the other delivers a muddy, dull sound. In no sense is this *high fidelity*. So far, the true high fidelity 4-channel phones come from those few outfits who chose to design around sound, rather than the *appearance* of front and rear transducers. The 4-channel phones from Koss, Superex and Radio Shack (Realistic) look like ordinary stereo phones, but really deliver four channels.

### Summing up

As you can see, though quadraphonics is virtually a brand new idea—if not to "pros" at least to the average audiophile, there is already an extensive assortment of equipments available.

R-E

# Setting-Up for CD-4 Records



*Discrete 4-channel records can produce some really fine sounds when your equipment is properly set up. Here is how to install it right the first time.*

by **HERB FRIEDMAN**

THE COMPLETE QUADRIPHONIC SYSTEM includes both matrix and CD-4 (discrete) systems, but unfortunately, at the time this is being written, there is no high-fidelity equipment (in the true sense of the term) which includes both an advanced matrix decoder (such as full-logic SQ) and a CD-4 demodulator. Though virtually every major hi-fi manufacturer now includes some sort of matrix decoder in his quadriphonic amplifiers and tuners (as contrasted to the "synthesized surround-sound" which can be a stereo amplifier with speaker circuit "ambient decoder"), CD-4 record reproduction requires an add-on optional such as the JVC 4DD-5 demodulator, not to forget a suitable Shibata stylus pickup and low-capacitance shielded cables (12 pF per foot) for the pickup to demodulator connections.

In very basic terms, adding CD-4 to an existing quadriphonic system requires only replacement of the phono pickup with the Shibata stylus model, installation of the low-capacitance cables, and finally, connection of the demodulator's four line-level outputs to matching line-level inputs on the quadriphonic amplifier. However, as with all good things, life isn't that

simple. While you can make a handful of blunders when installing stereo equipment and still come out with some really fine sound, a few minor blunders with a CD-4 add-on can just about wipe out the surround-sound and leave you with four channels of stereo, or mono.

The first consideration in upgrading to CD-4 is the amplifier line-level inputs. Many of the early quadriphonic amplifiers have little or no provision for "external" accessories; they were intended solely as matrix amplifiers or as something called a *4-channel control center*, the control centers being basic stereo amplifiers with a *master volume control* for future 4-channel equipments (a volume control mounted piggyback or tandem on the regular amplifier volume control had its connections brought out to rear apron jacks, the thought being that a single volume control could serve for two separate front and rear stereo amplifiers). Then there is the "quadriphonic" amplifier which is basically a stereo amplifier with an ambient sound decoder in the speaker circuits. In no instance can any of these so-called quadriphonic, quadrisonic, 4-channel or surround-sound amplifiers

be used with a CD-4 add-on.

Whether you have a fully integrated quadrisound amplifier, or are using your stereo amplifier with an amplifier/decoder for the rear output, you must have four separate power amplifiers—for left front, right front, left rear and right rear; and you must have an independent line-level input to each amplifier; in short, four line-level inputs for CD-4.

Many of the latest 4-channel amplifiers, even if they contain matrix decoders, have, at the least, one discrete 4-channel line-level input(s) labeled AUX or auxiliary. Some amplifiers have two discrete 4-channel AUX inputs. When a discrete 4-channel input is not provided for the AUX position of the input selector switch there will probably be a separate discrete 4-channel input—usually labeled DISCRETE or 4-CHANNEL—which is controlled by the stereo/mono mode selector switch. Your CD-4 demodulator can be connected to this connection.

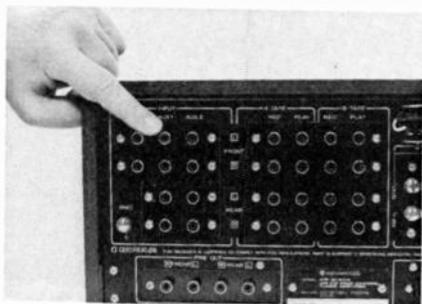
Finally, some quadrisound amplifiers intended primarily for matrix signal processing have no discrete 4-channel inputs. The tape monitor input, however, is discrete 4-channel and can be used for the CD-4 demodula-

tor (though you lose the tape monitor facility).

When you have established that your quadrisound amplifier has a discrete 4-channel line-level input (as we said, some amplifiers don't have this connection), then you are ready to purchase and install a CD-4 demodulator system.

### Replace the cables

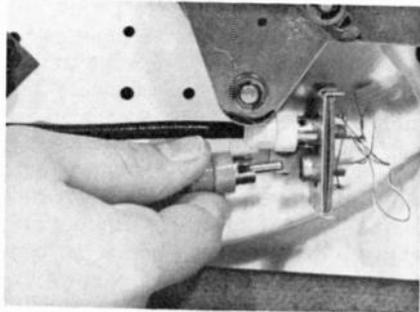
First step in the installation is replacement of the turntable's existing shielded signal patch cords with the low-capacitance patch cords (12 pF per foot) supplied with the CD-4 demodulator. The relatively high capacitance of the normal shielded au-



**SOME QUADRIPHONIC RECEIVERS** and amplifiers are basically stereo equipments, or have no provisions for optional discrete 4-channel hardware. To add a CD-4 demodulator to your system the amplifier must have four independent line-level inputs, such as the AUX 1 and AUX 2 shown above. A discrete 4-channel tape monitor input can also be used.

dio patch cords will "short circuit" a substantial part of a CD-4 record's ultrasonic subcarrier signal, resulting in partial or complete loss of the front-to-rear separation. Actually, you will hear a *stereo* output, for the L-R and R-L signals which are provided by the ultrasonic signal, and which are used to decode the sum stereo signals in 4-channel, will be filtered by normal shielded patch cords before the signal gets to the demodulator.

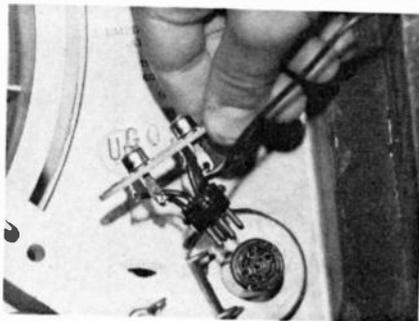
The low-capacitance cables sup-



**ON BETTER QUALITY TURNTABLES** the output patch cords usually connect to phono jacks concealed under the motorboard. Connect the low-capacitance cables provided with the CD-4 demodulator to these jacks. If your turntable has the output cords soldered to a terminal strip make certain you double check the shield connections when installing the low-capacitance cables.

plied with the demodulator are shorter than the standard shielded cords supplied with turntables; if they don't reach the amplifier you must use *low-capacitance* extension cords which are available from JVC.

As a general rule the turntable's cables are easily replaced because most quality turntables have twin or duplex phono connectors under the motorboard, generally accessible by removing the bottom cover or the base. Empire turntables use a special multi-terminal connector at the base of the pickup arm pedestal. There is an optional JVC adapter which converts the Empire connector to duplex phono jacks. Some turntables do not



**JVC PROVIDES AN OPTIONAL ADAPTER** for converting the multi-terminal connector used on Empire turntables to a duplex phono jack.

have plug-in cables; the connections are soldered. You'll have to cut the connector off one end of each low-capacitance cable and solder to the turntable's connection strip. In many instances you won't be able to tell which turntable wire is the shield, or ground; so before you solder the new cables double check the shield wires with an ohmmeter.

The pickup installation is the most critical part of the CD-4 upgrading. Whereas a slight misalignment might not have any noticeable affect on stereo records, an improperly installed CD-4 pickup can sharply degrade the demodulator's performance. (It is important to keep in mind that Shibata stylus CD-4 pickups are excellent stereo pickups, so if the pickup is installed for optimum CD-4 it is also optimum for stereo.)

### Overhang adjustment is critical

The most critical part of the pickup installation is the "overhang", the distance the stylus extends beyond the platter's spindle. Most quality turntables are provided with some sort of overhang gauge. *Use it.* If the gauge is a plastic assembly with cross-hairs that fits on the pickup holder (or shell) make certain the stylus is directly under the cross, with the stylus as close as possible to the cross-hair support. Use spacers between the pickup and holder if necessary—just

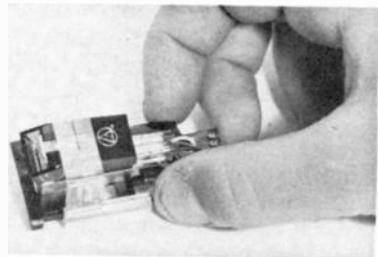
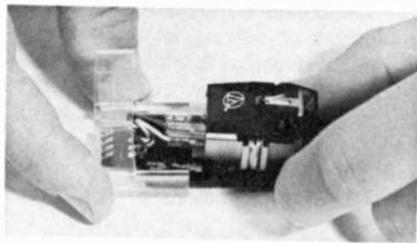
get the stylus raised where indicated by the gauge. If the gauge has a V-notch make certain the stylus is inside the V. If the stylus is centered but under the V-notch use spacers to get the stylus into the notch. If no plastic gauge is provided there is most likely a paper overhang gauge that was supplied with the turntable. Maybe you tucked it away with the warranty—dig it out. Make certain the gauge is positioned precisely as specified on the platter—don't fudge its position. Then check that the stylus falls precisely on the guide line when the tone arm is lowered.

If you have one of those turntables that was supplied without an overhang gauge you are stuck. Better to make your own out of paper than try to slide the pickup across a ruler—even a wood ruler can chip a diamond stylus. Finally, be extra careful when installing the signal connections to the pickup. Crossed or reversed leads will cause some very odd sound distribution. Not all manufacturers use the so-called standard color code, so the best thing is to check each signal wire with an ohmmeter before clipping it to the appropriate pickup terminal.

(Take note that some CD-4 pickups we have tested do not give sufficient overhang adjustment on a few of the finest turntables; it is impossible to get the stylus under the gauge's cross-hair. If you run across this problem with the CD-4 pickup *you* purchase don't fool around with home-brew remedies. There is nothing you can do short of modifying the pickup arm. Take the pickup back to the dealer and try a different model.)

### Final checkout and adjustment

Make certain your pickup arm is applying the correct stylus pressure as



**CD-4 PICKUP INSTALLATION** is critical. If a stylus position or overhang gauge is provided with your turntable be sure to use it. Don't guess. If you don't have an overhang gauge make one.

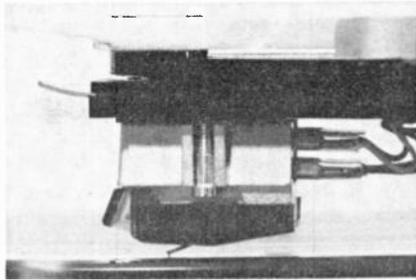
specified by the pickup manufacturer. Don't fudge the value. If 2 grams stylus pressure is suggested use 2 grams, not 1.5 grams. If a range is specified, such as 1.5 to 2 grams, you're better off starting out on the high side at 2 grams. Be sure that the anti-skate is set to the correct *elliptical* stylus value.

When you are certain the pickup is correctly adjusted place the test record supplied with the demodulator on the platter, fire up the amplifier and play the test record, making the demodulator adjustments as specified. If you find that the record specifies a left adjustment and only the right adjustment has an effect, the signal leads from the pickup to demodulator are in error. If the adjustments are made correctly but the positioning announcements are incorrect, such as left front appearing at right rear, the connections between the amplifier and demodulator are incorrect.

### A word about speaker phasing

As a general rule all speaker connections should be in the same phase with the positive speaker terminals connected to the positive amplifier output terminals. Actually, it doesn't matter which speaker terminal goes to what amplifier terminal as long as all speakers are connected the same way. Now it is possible for room acoustics to reverse the phase from one or more speakers *at the listening (seating) location*, and the bass—the low frequencies—will sound thin. In fact, it can sound as if one speaker was connected in reverse-phase. Normally, when acoustic reversal of low-frequency phasing occurs the common recommendation is to deliberately reverse the wiring to *one* speaker to compensate for the acoustic phase reversal. While this technique almost always works for stereo, and usually works for CD-4, it can create some really weird effects from matrix surround-sound.

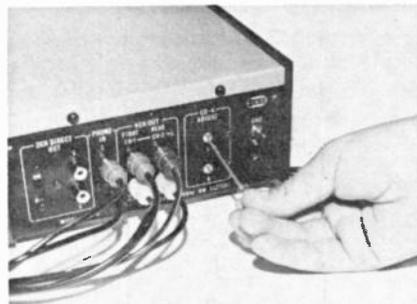
If you run into an acoustic phase-



**AFTER THE PICKUP IS INSTALLED** in the arm place the stylus on a record and sight-in from the side. The stylus should appear to be almost at right angles to the surface of the record. If the stylus appears to be "digging into" the record place some spacers between the pickup and shell until you obtain almost a right angle. The stylus and its reflection from the surface of the record should form almost a straight line.



**ALL SPEAKERS SHOULD START** out connected in-phase. If you are not using two-color wire (gold, silver) wrap a small piece of tape around one wire to denote either the positive (+) or negative (-) speaker and amplifier connections.



**WHEN PLAYING THE CD-4** adjustment record, the left decoder adjustment should affect only the left test signal. If it affects the right test signal the connections between the pickup and demodulator are reversed.

reversal problem first try to determine which speaker is causing the problem by shutting down two speakers at a time. When you have located the problem speaker reverse the connections to that speaker. Then listen to all speakers in CD-4 and matrix. If it sounds OK, leave it be. If it sounds good in CD-4 but appears to have "frequency holes" in matrix, or if both CD-4 and matrix sound good at first but appear to be causing fatigue after 15 or 20 minutes of listening then your best bet is to re-connect the proper speaker wiring phasing and physically move one or more speakers until you eliminate the acoustic phase reversal. And if you still can't eliminate the problem you'll have to select a new listening location.

Experimentation with speaker phasing is particularly important if your basic 4-channel equipment consists of a stereo amplifier or receiver with a *separate* rear-channel amplifier or amplifier/decoder. It is perfectly possible for the rear amplifier to have a 180° phase reversal compared to the front amplifier. For example, if a pulse waveform was applied simultaneously to all four inputs, the speaker cones connected to the front amplifier would move forward while the cones connected to the rear speakers moved backward—an exact 180° phase reversal. The perceived sound will be quite "hairy" under these conditions.

To check, feed a mono sound source through all inputs (mono record with both stereo amplifiers set to the mono mode); then turn off both the left front and left rear speakers. Reverse the wiring to *one* of the *right* speakers. If the bass at the listening location gets "thin", indicating cancellation of the lows, the original speaker wiring was correct. If the bass response is improved by the speaker wiring reversal, reverse the wiring to the matching *left* speaker. Then give it the overall listening test for acoustic phase reversal as previously described. R-E

## superconductivity breakthrough

The possibility of a breakthrough that may result in making superconductivity practical and useful in commercial applications was presented to the recent American Physical Society meeting in San Diego, CA, by two University of Pennsylvania physicists. Recent experiments conducted by Drs. Anthony Garito and Alan Heeger indicate that superconductivity may be attained at temperatures high enough to make superconductive transmission lines, generators or motors economically possible.

A superconductive transmission line would carry current with practically no

losses. It has been estimated that at present 75 per cent of the power generated in the country is lost because of the resistance of the material through which it has to travel.

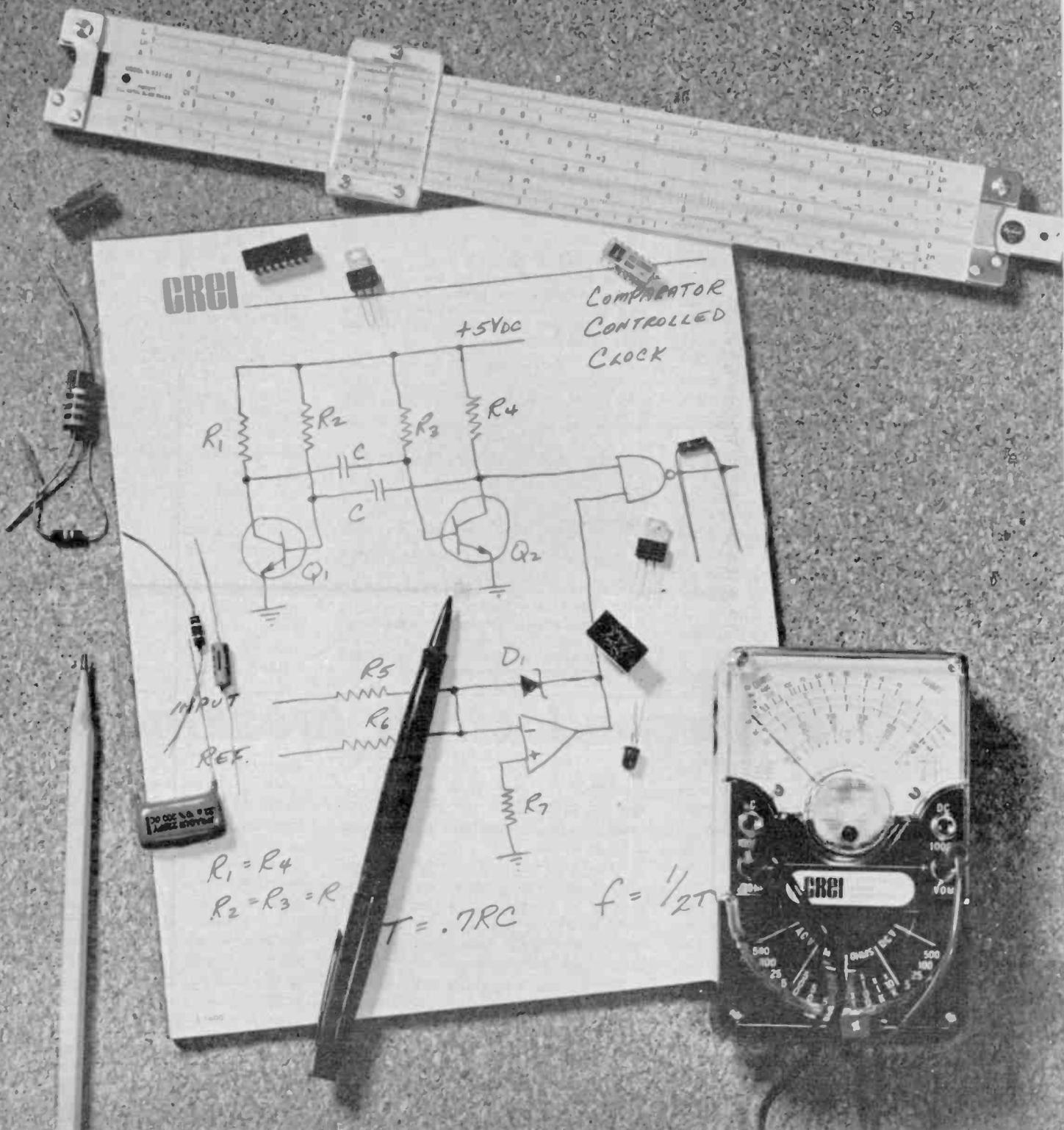
Up to the present, it has been possible to obtain superconductivity in some metals at temperatures up to 21°K (-252°C). Using an organic salt, Drs. Heeger and Garito have observed fluctuating superconductivity at about 60°K, a temperature that might make superconductive lines and electrical equipment economically practical.

The results may fall far short of the

expectations of the scientists at the meeting, or they may exceed them. It is by no means certain that the attempt to stabilize the fluctuations and obtain a consistent superconducting material will be successful. On the other hand, since the scientists are working with a complex organic compound (dimethyltetrathiofulvalene - tetracyanoquinodimethan for any reader who might like to make his own) there is the possibility that organic chemists could build up superconductors with special molecular structures to attain specific electronic characteristics.

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# 4-CHANNEL FM

## 9 ways to go

The 4-channel record has found its groove  
now let's see what's in store for 4-channel FM

by LEN FELDMAN  
CONTRIBUTING HI-FI EDITOR

FOUR-CHANNEL SOUND, AT LEAST FROM THE PHONOGRAPH record, has clearly settled into a "two-world" situation. At the moment, matrix discs outnumber discrete discs by a wide margin. CBS continues to champion its SQ matrix system in this country, while in Japan, the Regular Matrix (RM) system of matrixing, akin to Sansui's QS system, is the front-runner. Meanwhile, late-starter RCA has increased its output of discrete Quadradiscs (more often referred to as CD-4 discs—the name given to them by Japan Victor Company which is credited with their initial development).

Many of the high-quality, high-priced component receivers which are now available include facilities for decoding or demodulating one or more types of matrix discs as well as the new discrete four-channel records. Coexistence of "matrix" and discrete discs seems assured, at least for the present, and purchasers of new four-channel receivers seem less concerned about possible obsolescence—at least as far as record playing is concerned.

In the case of four-channel FM broadcasting, the situation is much more complex and unresolved at this time. Many stations throughout the country have been playing matrixed four-channel discs on a regular basis. Because these discs contain *two* audio channels—however complex they may be—present FCC rules need not be modified in any way, since the two encoded matrix channels are simply treated as two conventional stereo channels. Since all matrix discs are compatible with stereo (and, to a greater or lesser degree, with mono), the listener equipped with either a stereo or a mono receiver hears a balanced program, with *all* left information coming from the left-front speaker and *all* right program coming from the right stereo speaker during stereo playback. All four channels are blended together for monophonic listening. The listener equipped with a matrix decoder and a full, four-channel set-up, uses his matrix decoding facilities in much the same way as he would when listening to a matrix quadraphonic disc played over his own phonograph system.

The recently formed NQRC (National Quadraphonic Radio Committee), sponsored by the Electronic Industries Association and recognized by the FCC is now hard at work studying the problems involved in broadcasting four *discrete* signals over a single FM station. There are no less than eleven systems currently being analyzed. Not surprisingly, one of these, proposed by CBS, suggests that no significant rule changes be made by the FCC, since CBS maintains that their SQ matrix system, embellished with sophisticated logic circuits at the receiving end (*Radio-Electronics*, June 1973, page 44) can provide four-channel sound that is as satisfying as that produced from any discrete system. Most of the other proposals submitted to the NQRC, however, involve techniques for actually transmitting a composite signal over an FM station which would be separable into four, fully discrete signals in much the same way that the present stereo composite signal is separated by currently produced stereo FM tuners and receivers.

The earliest four-channel broadcasting system offered for industry and FCC consideration was developed by Louis Dorren, whose Quadracast Inc., in cooperation with San Francisco FM station KIOI, has already demonstrated the feasibility of their system in several months of experimental broadcasting. Many of the other systems currently under consideration (proposed by such companies as RCA, Motorola, G.E., Zenith and Nippon Columbia) are, to a greater or lesser degree "variations on a theme" developed by Dorren, and an understanding of the technical aspects of his proposal will make the other systems equally understandable.

### The present stereo composite signal

The make-up of the presently approved stereo composite signal is in Fig. 1. The main channel modulation

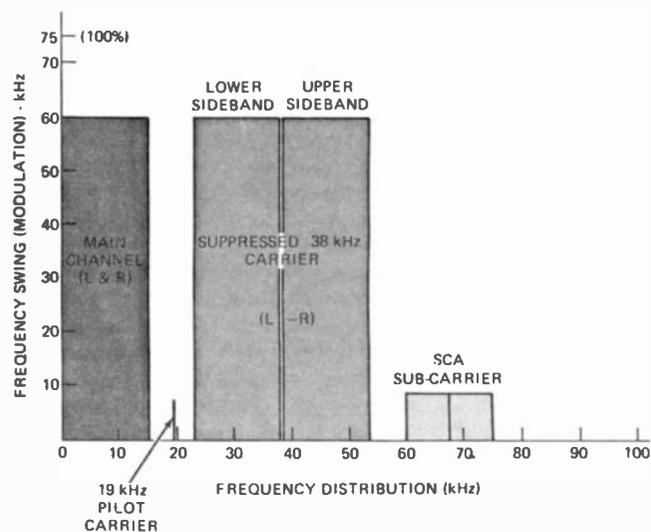
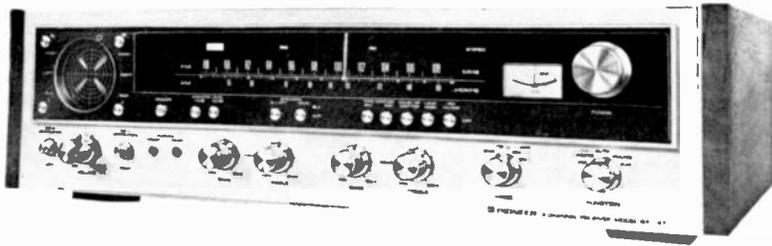


FIG. 1—SIGNAL COMPONENTS in the presently used stereo broadcast system. The 38-kHz subcarrier is suppressed.

consists of left-plus-right audio information in the frequency range from 50 Hz to 15 kHz. Upper and lower AM modulation sidebands, centered about a 38-kHz suppressed carrier are used to transmit *difference* information (L-R), while a 19-kHz pilot, modulating the main carrier approximately 10% of total, is sent along so that the 38-kHz subcarrier can be reconstituted in the receiver for proper demodulation of the L-R information.

At the receiver, once the L+R and L-R audio information has been recovered, the simple addition of these two audio signals yields a separated "L" signal  $[(L+R)+(L-R)=2L]$ , while subtraction results in the recovery of a discrete "R" signal  $[(L+R)-(L-R)=2R]$ .

Another component shown in Fig. 1, but unrelated to stereo broadcasting, is a 67-kHz SCA subcarrier that contributes 10% to the total modulation of the station carrier. It is this extra subcarrier that is used to transmit "back-



QUADRIPHONIC RECEIVER, Pioneer's QX-747, can handle CD-4, SQ and RM quadraphonic discs.

ground music" to private subscribers such as restaurants, hotels and other public establishments which is not heard by the general public listening to conventional FM sets.

It is this service, too, which poses one of the many problems inherent in the transmission of discrete quadraphonic broadcasts, since the FCC has indicated that provision for such Subsidiary Communications must be maintained in any future quadraphonic broadcast system. More than 600 FM stations now derive extra income by "leasing" this extra facility to companies such as Muzak which supply such musical programming and other specialized subscriber services.

### The Quadracast composite signal

Figure 2 illustrates the makeup of the composite signal

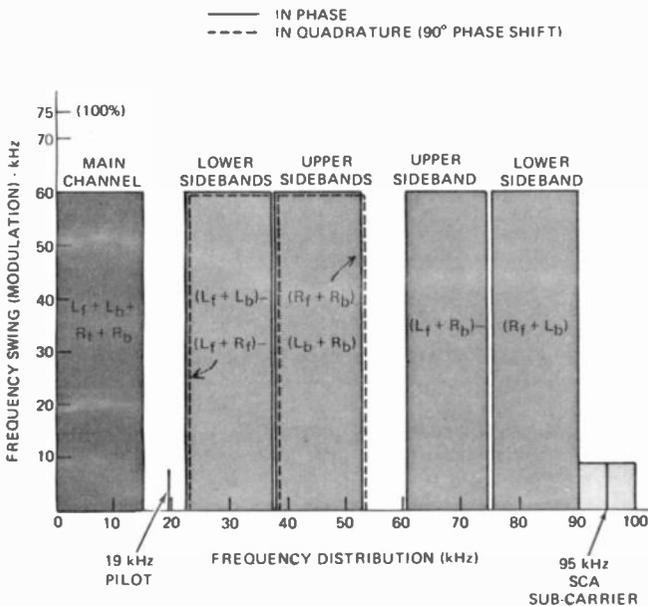


FIG. 2—QUADRACAST 4-CHANNEL FM system distributes its signal components as shown here.

proposed by Dorren for discrete four-channel broadcasting. Again, "main channel" audio extends from 50 Hz to 15 kHz, but in this instance it contains the sum of all four audio program signals ( $L_f$ ,  $L_b$ ,  $R_f$  and  $R_b$ ). The subscript "b" stands for "back" signals and this term, rather than "rear", is used to avoid confusion in abbreviations of right and rear. The 19-kHz pilot signal remains exactly the same as for stereo broadcasting.

Two sets of upper and lower sidebands related to the 38-kHz suppressed sub-carrier are now used—one similar in phase to that used for stereo, the other leading the first by 90 degrees. Because of this quadrature relationship between the pairs of sidebands, it is possible to detect the audio information modulating each independently by locking the reconstituted 38-kHz sub-carrier in the receiver to the

phase of each of the pairs of sidebands.

The first of these pairs of sidebands contains audio modulation corresponding to the difference between the left and right sets of information  $(L_f + L_b) - (R_f + R_b)$ , while the second, quadrature related sidebands are modulated by the difference between front and back audio for the left side, plus the difference between right-front and right-back audio  $(L_f - L_b) + (R_f - R_b)$ .

Mathematically, to solve for four "unknowns" (in this case, the four separate audio signals which make up a quadraphonic program), it is necessary to have four separate equations. It is for this reason that *no* matrix four-channel system (working with only two "equations") can ever recover four fully separated signals. Accordingly, Dorren adds still another sub-carrier, whose center frequency is located at 76 kHz (four times the frequency of the 19-kHz pilot reference carrier). Again, the new subcarrier is suppressed and only the upper and lower sidebands are transmitted. Their modulation consists of "diagonal difference" information of the form  $(L_f + R_b) - (L_b + R_f)$ . Now, with four separate equations of signal entities capable of being recovered by a properly designed receiver, the following mathematical manipulations are used to recover the four separate signals:

$$\begin{aligned} (L_f + L_b + R_b + R_f) - [(L_f + L_b) - (R_b + R_f)] + [(L_f + R_f) - (L_b + R_b)] - [(L_f + R_b) - (R_f + L_b)] &= 4R_f \\ (L_f + L_b + R_b + R_f) + [(L_f + L_b) - (R_b + R_f)] + [(L_f + R_f) - (L_b + R_b)] - [(L_f + R_b) - (R_f + L_b)] &= 4L_f \\ (L_f + L_b + R_b + R_f) + [(L_f + L_b) - (R_b + R_f)] - [(L_f + R_f) - (L_b + R_b)] - [(L_f + R_b) - (R_f + L_b)] &= 4L_b \\ (L_f + L_b + R_b + R_f) - [(L_f + L_b) - (R_b + R_f)] + [(L_f + R_f) - (L_b + R_b)] + [(L_f + R_b) - (R_f + L_b)] &= 4R_b \end{aligned}$$

Quadracast provides for an SCA sub-channel by moving its subcarrier up to 95 kHz, beyond the upper sideband of the 76-kHz subcarrier (required for quadraphonic service) which ends at 91 kHz and also suggests that this extra-service subcarrier be "phase locked" to the 19 kHz, since it would be the fifth harmonic of that frequency.

### Extra bandwidth

Those not intimately acquainted with the present FCC spectrum rules will, at first glance, conclude that the presence of program information above 75 kHz in the "baseband" of this proposed composite signal will lead to "out-of-channel" radiation and possible problems with adjacent-channel interference in FM. Actually, many tend to confuse *maximum deviation* of the FM carrier with frequency distribution or content. The fact is that even present stereo transmissions create measurable sidebands well beyond the 75-kHz point, and present rules merely require that any sidebands existing between 120 kHz and 240 kHz removed from carrier "center frequency" be attenuated by at least 25 dB. Dorren has already shown mathematically that his composite system meets these requirements despite its increased bandwidth occupancy.

While FCC regulations in this regard may prove to be no problem, present day receiver design practices may cause problems for those consumers who may someday attempt to convert their existing receiver to this or any other approved system of quadraphonic broadcasting. Better quality stereo tuners and receivers have fairly linear response and phase characteristics up to and beyond the 53-kHz limit which defines the end of the upper sideband in the stereo composite signal. Further increases in bandwidth are often compromised so as to obtain better adjacent-and alternate-channel selectivity—particularly in view of the “crowded” conditions of the FM band brought about by the recent popularity of this radio medium. Just as some monophonic receivers (which had even narrower bandwidth) did not lend themselves to satisfactory stereo conversion in the 1960’s, when “multiplex adapters” were sold for this purpose, it is likely that many high quality stereo tuners and receivers will not lend themselves to good conversion to quadraphonic reception, however plentiful good-quality quadraphonic adapters may become when and if a system is approved.

### Other quadraphonic broadcasting proposals

Zenith has offered two proposed variations of the basic Dorren proposal which leave the 67-kHz SCA service unaltered in frequency. The first of these, shown in Fig. 3, has a main channel and two quadrature-related 38 kHz sub-

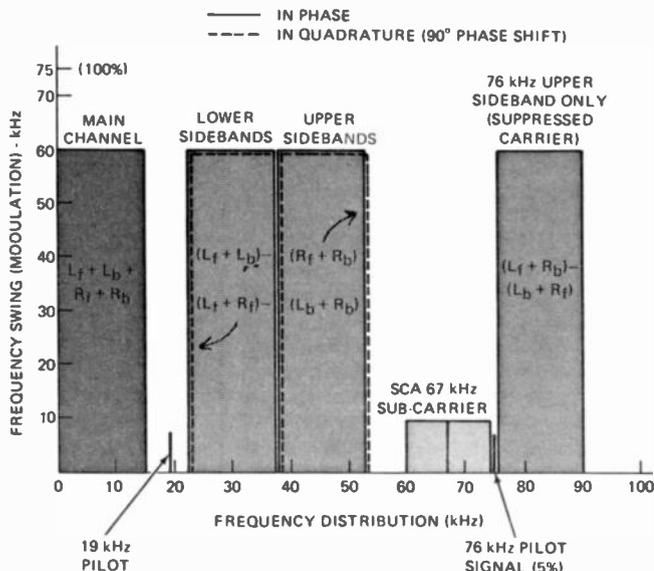


FIG. 3—ONE OF ZENITH'S PROPOSED SYSTEMS permits 67-kHz SCA operation by using only upper sideband of extra 76-kHz subcarrier.

carriers much like the Dorren system. The 76-kHz subcarrier, however, is limited to the transmission of the upper sideband only, thus freeing the frequencies around 67 kHz for continued SCA service. In this system, however, a second pilot carrier at 76 kHz, using 5% of total modulation of the main station carrier is required.

Another Zenith proposal, its spectrum is plotted in Fig. 4, would shift the upper subcarrier to a frequency of 90.25 kHz and would use lower vestigial sideband modulation, thus leaving the frequencies around 67 kHz still available for SCA use.

General Electric's proposal is quite similar to Zenith's second proposal, as can be seen in Fig. 5, except that the upper subcarrier would again be located at 76 kHz and require no separate pilot signal of its own. The upper sideband modulation would be steeply attenuated using vestigial sideband techniques, as shown. SCA service would then be able to occupy the spectrum between 90 kHz and 100 kHz, and if a center frequency of 95 kHz were selected, it could be phase-locked to the 19-kHz pilot signal,

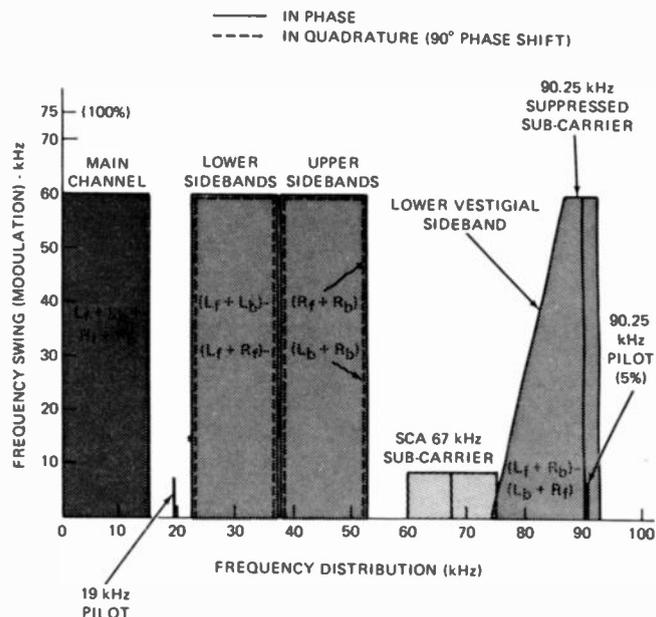


FIG. 4—ALTERNATE ZENITH PROPOSAL uses lower vestigial sideband of 90.25 kHz suppressed carrier, still permitting SCA operation at 67 kHz.

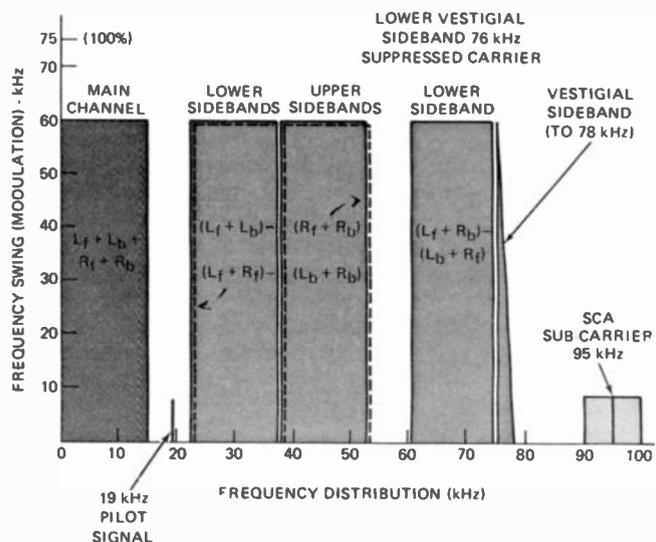


FIG. 5—GENERAL-ELECTRIC'S SYSTEM uses vestigial sideband for upper subcarriers, providing greater isolation between 4-channel and SCA signals.

since its frequency would be the fifth harmonic of 19 kHz.

Both RCA and Motorola have offered “dual-option” proposals which suggest that a three-channel system be used when SCA service is required and that a full, four channel system be used when the station does not engage in SCA service. The two RCA variations are shown in Figs. 6 and 7. In Fig. 6, only the first three types of audio composite signals detailed for the Dorren system are transmitted. Solving for “four unknowns” with only “three audio equations” does not, of course, result in complete isolation of the four original quadraphonic signals but does offer better separation than a simple “matrix” or “two equation” system such as that proposed by CBS. By offering this dual option, the second RCA system shown in Fig. 7 extends frequency spectrum to a maximum of 91 kHz, since in full four channel operation, SCA service is eliminated entirely.

One interesting innovation suggested by CBS in connection with their “matrix” two-channel proposal involves a means of identification for matrixed four-channel broadcasting. At the present time, listeners have no way of

(continued on page 98)

# 4-channel record review

There are many 4-channel records available now. Here's how we rate the 4-channel effectiveness of these discs

by RADIO-ELECTRONICS EDITORIAL STAFF

DURING THE PAST YEAR THE EDITORS of *Radio-Electronics* have been testing 4-channel matrix recordings and equipment extensively. We have set up a scoring system to evaluate our impression of the effectiveness of these records.

The scoring runs from one to four stars. One star is the lowest and four stars are highest on our scoring system. Note well that we are only evaluating the records from the standpoint of 4-channel technical effectiveness. The ratings shown here have nothing to do with performance or artistic merit.

## The equipment

The mechanical and electronic chain of equipment used for playing the records includes the following: Shure V15, Mark III improved cartridge; Shure-SME arm; Thorens TD 124 turntable; Dynaco PAT-4 preamp and Dynaco Stereo 120 amplifiers; a pair of AR-3A speakers for the front channels and a pair of Dynaco A-25 speakers for the rear channels.

A second equipment setup consists of a Shure M91ED cartridge; a Garrard SL95B changer; a Scott model 499 Stereomaster Quadrent stereo amplifier and four Dynaco A-25 speakers.

## 4-Channel Record Review

Two different SQ decoders were used: The Lafayette SQL and the Sony SQD-2020. The Lafayette unit incorporates logic circuits to improve front-to-back separation. The Sony unit is more sophisticated and includes not only front-to-back logic circuits, but also wave matching circuits which further improve left-right separation.

## 4-Channel Recording Techniques

When matrix four-channel recordings were first introduced, there were two distinct recording techniques. In

Pop music the listener was placed in the middle of the recording group so that the sound would come at him from all directions.

And in some records pan effects were incorporated so that individual instruments and voices would sometimes move around the listening room during a selection.

With Classical music, however, the record makers adopted a more conservative approach and tried to create the illusion of the listener being in an auditorium with the performers in front of him.

The rear speakers picked up the delayed reverberation, giving the listener the effect of the hall ambiance in which the recording took place.

In the past year, four-channel classical record producers became more innovative and in some records, have copied the pop record technique, putting the listener in the middle of a symphony orchestra. This Surround Sound technique has caused controversy among classical music record buyers. Traditionalists rebel at the idea of being surrounded by the music. But many (including some classical musicians) find Surround Sound exciting. A lot depends on the selection and the record producer's style. In the reviews which follow, we have noted those classical records using the Surround technique.

## COLUMBIA

- CQ-30322—Janis Joplin, Pearl \*\*
- CQ-30750—Paul Simon \*\*
- CQ-30768—The Raiders, Indian Reservation \*\*
- CQ-30797—Andy Williams, You've Got A Friend \*\*
- CQ-30800—Percy Faith, Black Magic Woman \*\*\*
- CQ-30810—Jim Nabors, Help Me Make It Through The Night \*\*
- CQ-30961—Johnny Cash At San Quentin \*\*\*
- CQ-31096—Upendo Ni Pamoja, The

Ramsey Lewis Trio \*\*

CQ-31170—Blood, Sweat & Tears Greatest Hits \*\*\*

MQ-31193—E. Power Biggs, Music For Organ, Brass and Percussion Recorded in St. George's Church, New York City \*\*\*\*

SQ-31237—Jim Nabors, Man Of La Mancha \*\*\*

CQ-31247—Peter Matz Spectacular \*\*\*\*

MQ-31368—Bartok, Miraculous Mandarin—Boulez And The New York Philharmonic Orchestra \*\*\*\*

QX-31403—An Introduction To The World of Quadraphonic Sound \*\*\*\*

MQ-31425—Isaac Stern, Romance \*\*

MQ-31520—Stravinsky, La Sacre Du Printemps—Bernstein And London Symphony Orchestra. Surround Sound \*\*

CQ-31629—Alone Again (Naturally), Ray Conniff \*\*

CQ-31641—Lynn Anderson's Greatest Hits \*\*

CQ-31748—Lagins And Messina \*\*

CQ-31776—Azteca \*\*\*

MQ-31798—Pinchas Zukerman, Conducts English Chamber Orchestra And Plays Vivaldi—The Four Seasons. Surround Sound \*\*\*

MQ-31960—Highlights From Leonard Bernstein's Mass \*\*\*\*

MQ-32051—Mozart's Greatest Hits \*\*

MQ-32054—Bach's Greatest Hits \*\*

MQ-32055—Tchaikovsky's Greatest Hits \*\*

MQ-32056—Beethoven's Greatest Hits \*\*\*

MQ-32058—Chopin's Greatest Hits \*\*

MQ-32059—Strauss' Greatest Hits \*\*

CQ-32079—The Best Of Mountain Featuring Leslie West And Felix Pappalordi \*\*\*

(continued on page 79)

THE LITERATURE IS OVERFLOWING with ambitious schemes for improving all phases of communications reception. The profusion of really novel ideas is amazing. Until recently though, the great majority of this wealth of information was kept at a theoretical level for a very simple reason. They were just too complicated for the existing discrete circuit techniques. The IC has completely changed the picture. Circuit complexity is not nearly as costly as it used to be, and looking at the two circuits we are going to explore here, the buyer of these circuits is getting a tremendous bargain. Not only is he getting a bargain in pure number of devices, but he is getting the benefit of many hours of highly skilled innovative development time. The age of the integrated circuit is allowing the many ideas filed away in the various periodicals and journals to be re-explored and is also inspiring new invention and thinking in how to use the new techniques to practical advantage.

We are going to look at FM detection by exploring two very impressive devices. Two reasons prompt us to use FM as an illustration of what can be done. First, the initial appearance of an IC in a television receiver was a sound detector, and second, we will examine two methods of detection which may be unknown to many of you. The devices under question are the RCA CA3065 i.f. amplifier-limiter, FM detector, electronic attenuator and audio driver and the CA3089 FM i.f. system. We feel in no way prejudiced by choosing two RCA devices since RCA was the first to implement the detection systems which are now widely copied by other major manufacturers. At first glance, the FM detector portion of the two IC's may seem similar because of the symmetrical differential type circuits. They are in fact completely different in concept, each one chosen for a particular advantage in its specific operating environment. These circuits are all ready and will continue to find their way into all manner of communication equipment, some far afield from their original design intent.

Fig. 1 is the block diagram of the CA3065 television sound system shown in its natural milieu, the TV receiver. With a minimum of external components the circuit does all FM functions between the sound take-off transformer and the audio output transistor. Note that one of the novel features obvious in this diagram is the dc volume control. A bypassed potentiometer controls the audio gain of the system by means of an electronic attenuator. A single wire can be used to control the volume with almost com-

plete disregard as to its length and its route.

With the aid of the schematic of Fig. 2 let us work our way through the maze of some 34 transistors, 9 diodes, 45 resistors and 5 capacitors. The first thing you might notice in a cursory examination is that there are 5 Zener diodes in the schematic. Because of the limited value of capacitors that can be integrated other methods of bypassing must be used. Capacitors of more than a few picofarads consume inordinate amounts of chip area and so are undesirable. When a Zener diode is biased beyond its avalanche breakdown knee its impedance becomes quite low and it becomes an effective bypassing element. (The old gaseous VR tube was used for a similar purpose in early vacuum-tube hi-fi amplifiers.) D3 and D4 in series regulate the power supply bus for the circuit at a specified typical 11.2 volts. D1 in series with R1 and D2 in series with D9 and R2 provides dynamic bypassing for portions of the limiter circuitry that require it.

Q11 through Q19 are three stages of limiter amplifiers to help attain the specified 50 dB typical AM rejection. This is one of the more important FM specifications since it is an indicator of the receiver's ability to reject amplitude modulated noise which is what FM is all about. These three amplifiers are differential types which have always been the backbone of integrated circuit design. The differential amplifier is convenient to bias without using capacitors since the low emitter impedance of the complementary device gives the desirable ac signal bypassing. Another reason for its wide popularity is that it behaves well when overloaded—limiting by cutting off transistors rather than by saturating them. A large positive signal at IC pin 2 pulls up the emitter junction of Q11 and Q12 cutting off Q12 with a resulting positive swing on its collector. A relatively large negative swing at the base of Q11 cuts it off, allowing Q12 to conduct the full current in R25 reducing the collector voltage of Q12. The action of the limiters result in a

# NEW IC's For FM CIRCUITS

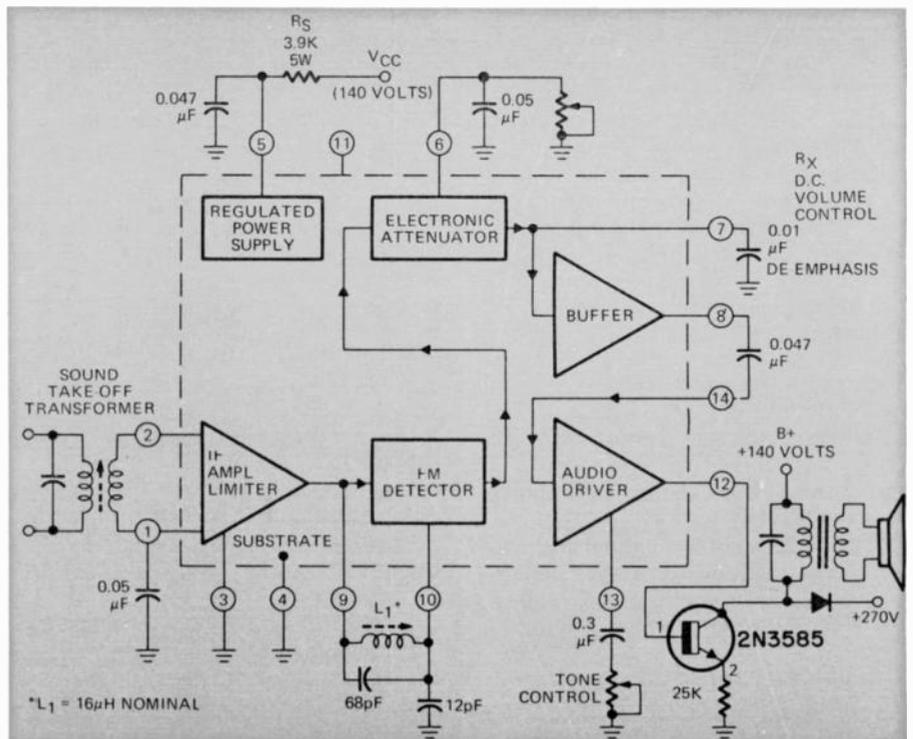


FIG. 1—BLOCK DIAGRAM of the CA3065 IC incorporating an FM i.f. amplifier, discriminator and an amplifier for use in television receiver circuits.

See how old techniques—made practical through new IC's—can improve performance from TV sound and FM receivers.

by STEVE LECKERTS

limiting knee of 200 microvolts typical which is the signal level 3 dB below where the amplifier levels off with increasing input.

Transistors Q22 through Q28 are the differential-type FM detector. It detects the difference in two responses of a low-pass filter in such a way as to perform the desired demodulation. Figs. 3 and 4 show how this detector works. The responses of the two inputs to the detector are different since one is taken at its input and one at its output. The nulls in the two responses are at different frequencies. Q23 and C3 peak-detect one response, Q26 and C4 the other and differential amplifier Q24, Q25 subtracts the two detected dc voltages.

If the two curves in Fig. 3 are

subtracted point by point as done by the differential amplifier the detector response of Fig. 4 results. This is the familiar S curve essential to all frequency detectors since the straight central portion gives a linear changing dc voltage with frequency. Although we previously said AM rejection is the function of the limiter amplifier a contribution is also made by the detector. Those of you familiar with the ratio detector are aware of this fact.

This differential detector enhances the receiver's AM rejection because the center or zero crossing of the S curve is formed by the difference of two signals. This point can be made virtually independent of input level. We have described how the difference detector produces the demodulated

audio current which is the collector current of Q25.

The circuitry of Q6 through Q10 along with Q29 forms the electronic attenuator. The collector current of Q25 feeds the emitter of transistor pair Q7-Q8. The differential dc voltage appearing on the bases of these two transistors determines how the detected audio signal is split between the two transistors. If the base of Q8 is at a higher potential than the base of Q7, Q8 will conduct more than half of the demodulator's output current. The audio output is taken off the collector of Q8 (it's developed across R3) to drive the output follower Q2. By varying the resistance to ground at pin 6, the bias on differential pair Q7-Q8 is adjusted and the output signal level is controlled. If nothing else were added the system would work but there would be an annoying shift in dc level at the output as the attenuation is changed. Transistors Q9 and Q10 fed by dc current source Q29 solve this problem by adding in a dc current equal to the amount subtracted by the audio attenuator portion. As the ac and dc signals in Q8 are reduced the dc current in Q10 increases. Since the two collectors are tied together their currents are added and the net dc current shift is zero keeping the dc out-

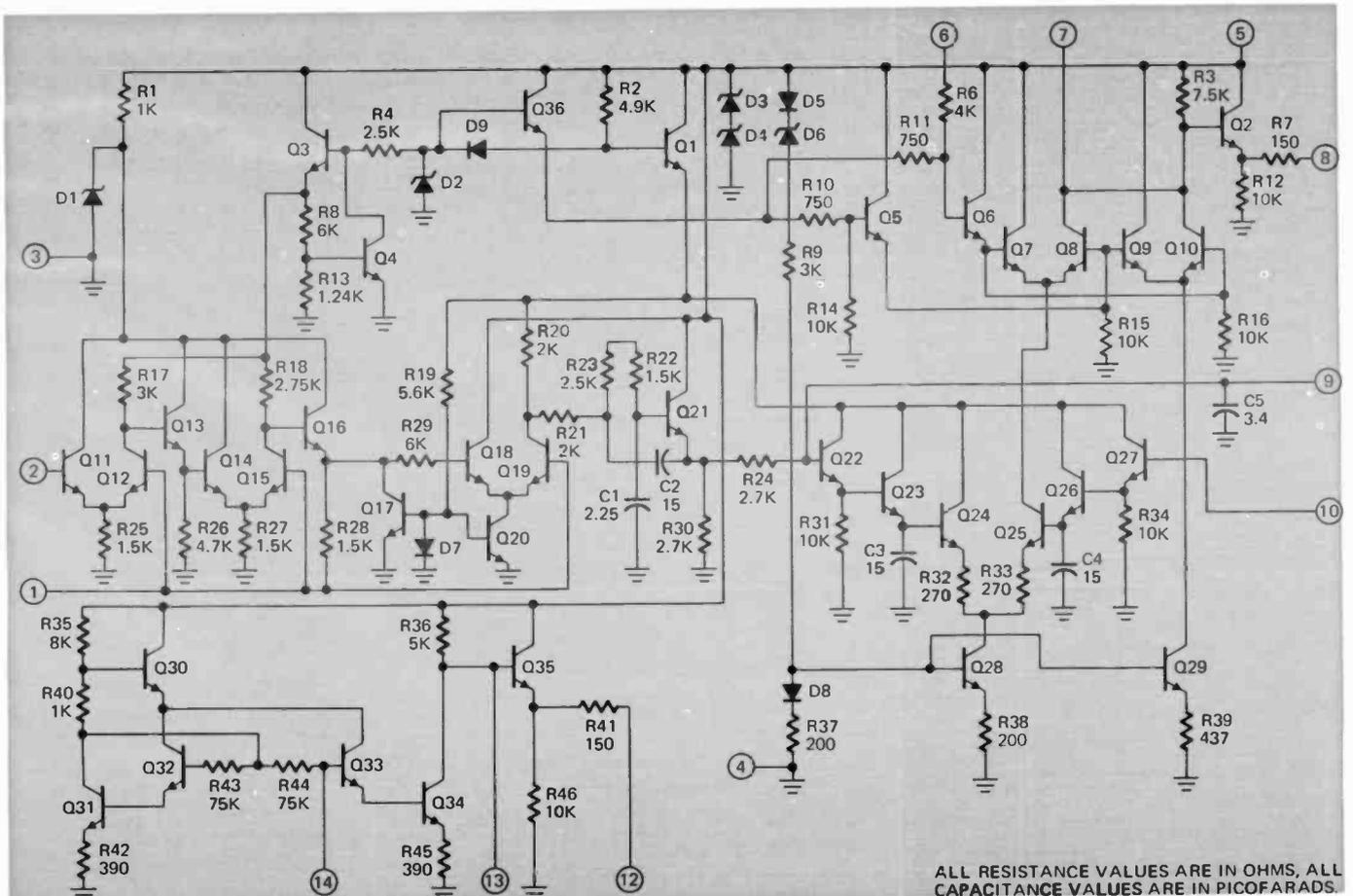


FIG. 2—SCHEMATIC DIAGRAM of the CA3065 IC. Formidable looking with its 34 transistors, 9 diodes and maze of resistors and capacitors; the device is housed in a 14-lead DIP case.

put voltage fixed. This system gives an attenuation range of 60 dB with an output distortion rated at 1.5% typical.

### Now for the CA3089

This more complex FM i.f. system was designed for use in the more critical FM receiver where specifications such as capture ratio and distortion are paramount. The CA 3089 can provide exceptionally low distortion (typically 0.1%) using a double-tuned circuit in its detector. With an ideal front-end, a capture ratio as low as 0.5 dB can be achieved. This is the number which tells the difference in two signal levels at the same frequency which results in the smaller one being rejected. The smaller the number the better the performance. While we don't know what receiver capture ratio has been actually achieved combining front-end design with this IC, 0.5 dB is a great

place to start. To get these results a quadrature detector is used which pivots around a double-balanced phase detector circuit that has become one of the building blocks of many integrated circuits.

Looking at Fig. 5, the block diagram of the CA3089 FM i.f. system, we see that in addition to the i.f. amplifier-limiter and detector, the circuit contains level detectors used to operate a tuning meter and a squelch circuit to mute the receiver. This IC chip does not have an attenuator as such but an audio muting control amplifier which is used to switch off the audio while tuning between stations. The simplified schematic (Fig. 6) is more complex than the first circuit we discussed. Working at an i.f. of 10.7 MHz it is more difficult to design an integrated limiter, or any limiter for that matter, since the frequency is roughly double that of the 4.5-MHz TV sound i.f. The limiter-amplifier is similar to the previous one using differential amplifiers except that it is completely balanced. Both collectors of the amplifiers are used to couple signal to the next stages. Also phase compensation is included by positive feedback using the small 1- and 0.2-pF capacitors. (The 0.2-pF capacitors are not shown.) Each amplifier has its

own level-detector circuit. The detector outputs are combined to operate a signal-strength meter over a large signal range. RCA points out that this is not just an agc metering scheme but a system that gives a true signal-strength indication.

Figure 7 explains the operation of the doubly-balanced phase detector. The diagram shows that as the relative phase between the two inputs changes, the detector output voltage changes. To convert this voltage change so the FM quadrature detector can process it, the frequency shift of the received signal must be changed into phase shift. An inductor-coupled tank does the job. As the frequency changes the phase shift of the tank circuit feeding Q21 and Q26 (across pins 9 and 10) is compared to the phase of the input signal feeding Q27 and Q28. The circuit is adjusted so that with no frequency modulation there is a 90° phase shift between the two inputs resulting in no demodulated output.

The audio output of this amplifier exists as currents in the collectors of Q23, Q24 and Q22, Q25. These currents feed two identical mute circuits. They appear in duplicate because of the way the audio output is formed by a subtractor circuit. A second subtractor circuit produces an AFC current directly from the chip which can be connected through a resistor circuit to control a varactor-tuned local oscillator. The audio output is squelched while the afc output is not. The muting circuit Q43, Q44, Q47 is controlled by the dc voltage on the base of Q47. When this base is driven positive by the squelch output Q43 is turned on harder, turning off Q44 and reducing

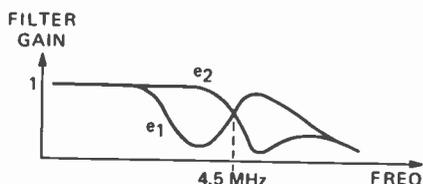
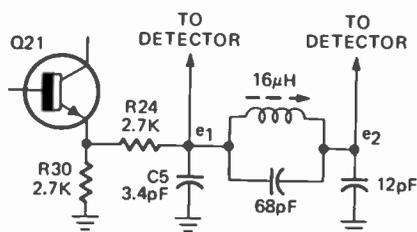


FIG. 3—EXTERNAL LOW-PASS FILTER and the responses of signals sent to detector.

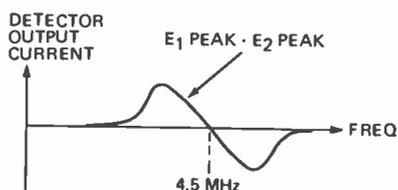


FIG. 4—FAMILIAR S-CURVE shows the response of the differential FM detector.

ALL RESISTANCE VALUES ARE IN OHMS  
 \*L TUNES WITH 100 pF (C) AT 10.7 MHz  
 Q<sub>0</sub> ≅ 75 (G.I. EX22741 OR EQUIVALENT.)

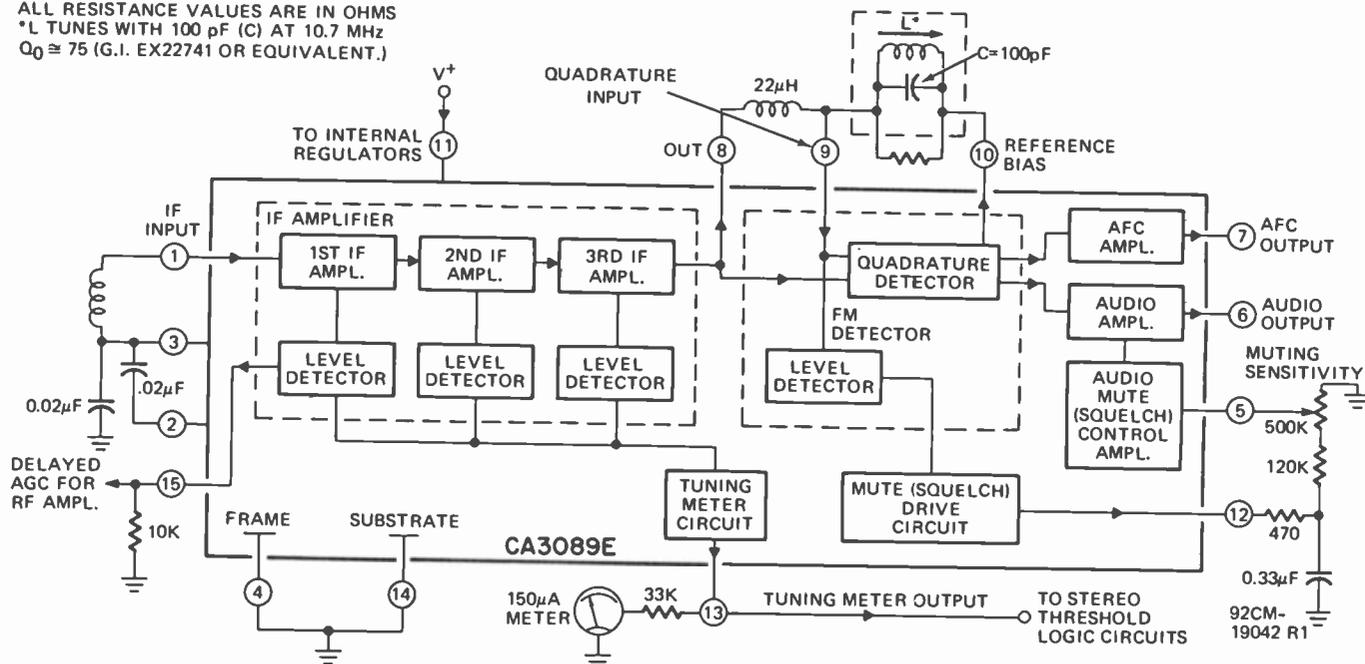


FIG. 5—BLOCK DIAGRAM OF THE CA3089E IC, an elaborate device designed for top-notch FM receivers. The integrated limiter is more complex than the one in the CA3065.

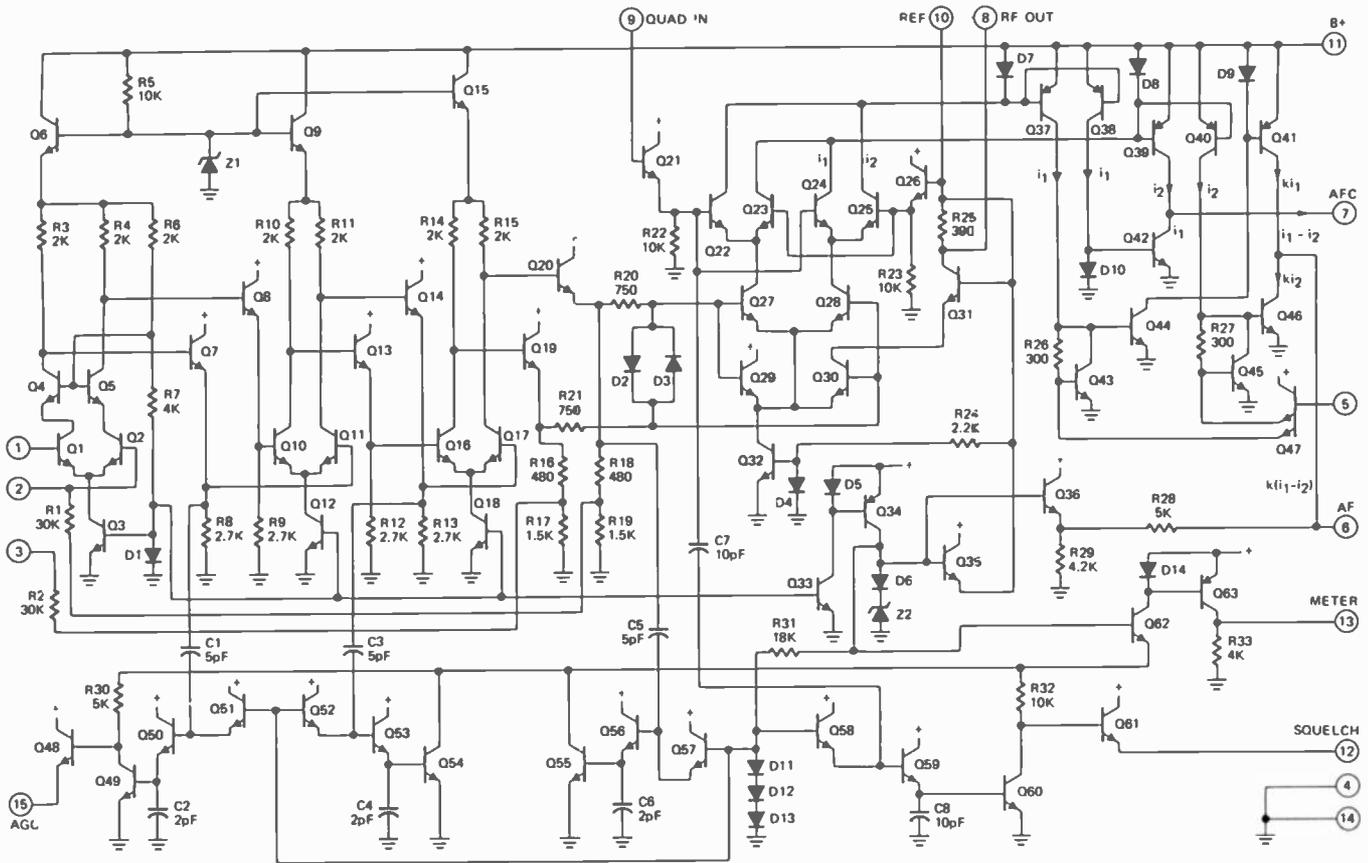


FIG. 6—SIMPLIFIED SCHEMATIC DIAGRAM of the CA3089E. The device features squelch or muting, afc for the tuner, drive for tuning meter and a balanced phase detector.

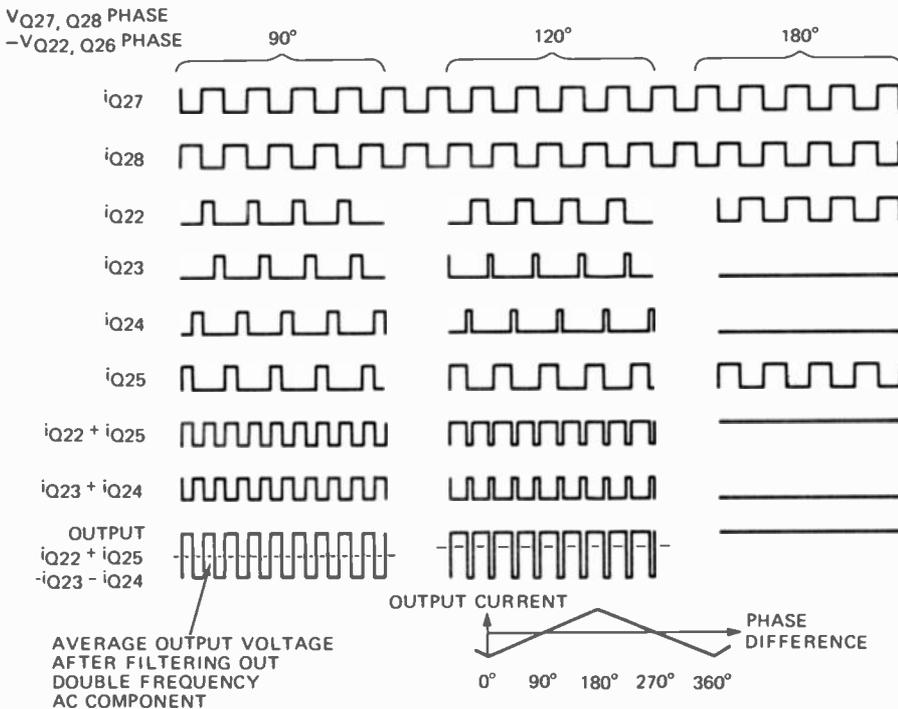


FIG. 7—PULSES SHOW PHASE RELATIONSHIPS of currents in various sections of the phase detector. Phase difference produces a voltage difference that is processed by the detector.

the audio signal flowing through it. The second circuit (Q45 and Q46) stabilizes the dc voltage at the audio output similarly to the way it was done on the CA3065.

### Other applications

There are many imaginative ap-

plications and variations possible with these two circuits. For example the detector-gain control part of the CA3065 can be used as a variable-gain audio amplifier without using the limiter-detector functions at all. All that has to be done is to feed audio into pin 10 and bias pin 9 at the same dc

voltage as pin 10 by using a resistor and bypass capacitor.

An interesting extension of the CA3089 is to use the meter circuit to detect multipath transmission. If we feed filtered afc output at pin 7 to the horizontal input of an oscilloscope and the meter signal into the vertical input we will set up the required display. The horizontal axis now corresponds to frequency and the vertical deflection indicates received signal strength. Deviations from a straight line show multipath reception. The same effect will be seen if the rf and i.f. filter responses are not flat.

We hope we have stirred up some interest in the modern sophisticated integrated circuit and at the same time enlightened you on the operations of two types of now practical FM detectors considerably different from the common diode types. IC manufacturers provide a mass of information in their manuals in the way of detail-packed data sheets and application notes and these are a good investment for learning, or a necessary one to profitably use the devices. For those interested in reading further on the devices we have discussed here we recommend hunting up copies of the CA3065 and CA3089 data sheets. The August 1971 issue of the *IEEE Transactions on Broadcasting and Television Receivers* has a detailed report on the CA3089, "Advances in FM Receiver Design" by Jack Avins of RCA. **R-E**

TV ANTENNA INSTALLERS HAVE KNOWN for a long time what antenna manufacturers were a little slow to pick up: that the most widespread reception problem today is not weak signal, but electrical interference. Or, put another way, the principal antenna requirement in most areas is not higher gain, but better interference rejection characteristics.

Ten years ago—even five years ago—antenna engineering centered almost entirely on producing higher gain. There was always a fringe area that needed just another dB or two to pick up a distant channel. Fringe areas still exist, of course, and gain is still an essential antenna characteristic. But another quality has become just as important, if not more so: noise rejection.

The Institute of Electrical and Electronics Engineers defines noise as, "Unwanted disturbances superposed upon a useful signal that tend to obscure its information content."

An installer trying to deal with practical TV reception headaches might more graphically define noise as "interference from trucks, trains, appliances, and unwanted broadcast transmission that throw patterns and streaks across what would otherwise be a fine TV picture."

This article deals with external noise sources only, principally of the man-made variety.

The importance of a noise-free environment to good reception is suggested by the care taken in the siting of radio-telescopes (such as the large parabolic array at Green Bank, West Virginia) and other antennas used in space communications and exploration, to find an area as free as possible from interference.

### Interference sources

What are the sources of external interference and their significance to TV reception?

**Atmospheric noise** is caused by lightning, whose low-frequency radiation is trapped between the earth's surface and the ionosphere, affecting reception at global distances. At radio broadcast frequencies below about 20 MHz, it is the limiting factor on reception—many times greater than internal receiver noise. For this reason, the typical broadcast receiver operates fairly well with an extremely short, low-gain ferrite rod antenna: any increase in antenna gain would increase both signal and noise but would not change the signal-to-noise ratio. At TV frequencies, this source of noise is unimportant except on a local basis.

**Cosmic noise**, first discovered by Jansky in 1932, originates outside the earth's atmosphere, and includes radiation from the sun, from other por-

# New Antenna For Fringe-Area Reception

*Co-channel and adjacent-channel interference are common problems in fringe areas. Here's an approach to antenna design that minimizes these problems*

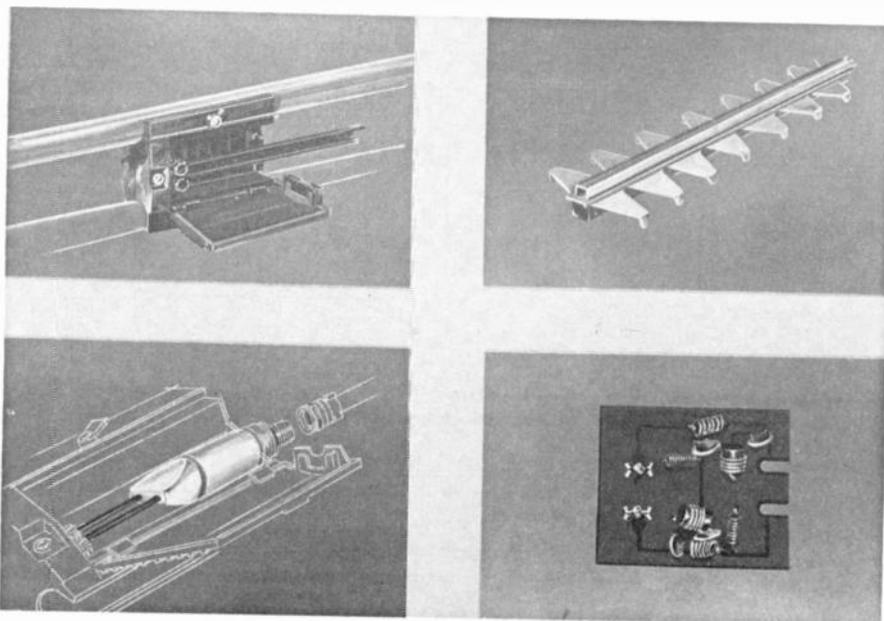
by JULIUS GREEN  
Channel Master

tions of our galaxy, and from other galaxies. Because of attenuation by the atmosphere, its magnitude decreases with increasing frequency. Furthermore, it does not appear equally from all directions. Location of the particular sources of this noise has attracted great interest and effort, and has given birth to the field of radio astronomy. On the average, this noise is slightly greater than typical internal receiver noise on Channels 2 to 6, less than set noise on Channels 7 to 13, and insignificant at uhf frequencies.

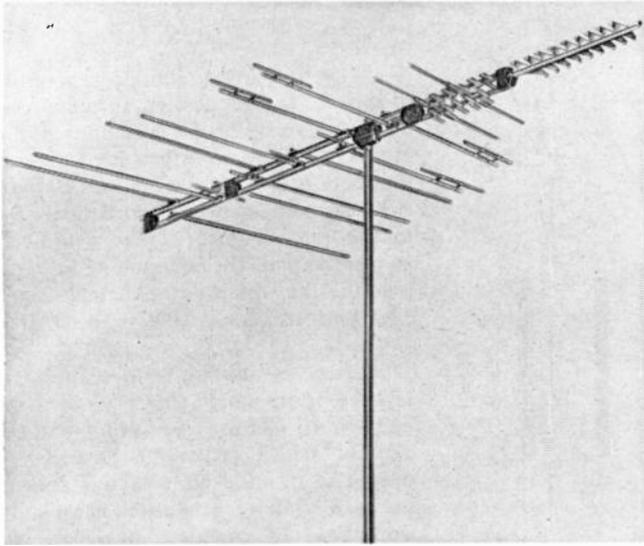
**Man-made noise**, constantly increasing, is the result of our endless proliferation of electrical devices. Consequently, its continued rapid growth is guaranteed. Noise sources include appliance motors, switches, ignition

systems (especially busses and trucks), generating stations and power transmission lines, diathermy equipment, amateur radio, FM stations, and TV stations. Ghosts (reflections off natural or man-made structures and topographic features), adjacent-channel interference, and co-channel interference might also be placed in this category. This distressing situation has given the term "air pollution" a new meaning for the TV industry and the unhappy home viewer.

Obviously, the level of man-made noise varies considerably with the particular location, but some generalizations can be made. Like cosmic noise, it decreases with increasing frequency. In metropolitan areas it can be much greater than the internal set



ACCESSORIES FOR THE QUANTUM ANTENNA. Top left is the weatherproof terminal housing, top right is the uhf antenna segment. Lower left and right are coax balun and FM trap.



ONE OF THE CHANNEL MASTER QUANTUM ANTENNAS for deep fringe vhf and uhf TV. An FM trap and balun for coax are useful.

noise. As one moves out into less densely populated areas, it becomes less of a factor.

Experienced technicians are only too painfully familiar with the visual results of such interference, particularly but not entirely on the low band: herringbone and moire patterns, venetian blinds, sync bars, windshield wiper effect, and so on.

Since neither the TV set location nor the noise sources are likely to be moved away, the most effective way—indeed, perhaps the only way—to eliminate interference is to eliminate antenna and transmission line pickup of the offending signals.

High-gain antennas, with extremely narrow forward beams, have been a valuable step in this direction. However, a narrower beam width implies higher gain, and the engineering efforts to achieve higher gain, and thus narrower beams, are approaching the practical limits imposed by size and cost. Therefore, little more can be done to reject interference coming from the same direction as the TV

transmitter other than using an array.

However, there is at least a 50-50 chance that much of the interference may come in from the rear or sides of the antenna. When faced with co-channel or adjacent-channel interference, probably 90% of the undesired signals come from the rear because of the FCC's geographical allocation of channels.

Despite this growing problem, high gain has continued to be the principal target of TV antenna engineers. Other characteristics have remained secondary considerations, and often are even sacrificed for additional gain.

This is in contrast to the design of large radar arrays and radio telescopes where control of side and back lobes is the primary design objective to assure the best possible performance.

However, the scope of the interference problem became glaringly apparent following a national field survey of reception conditions by Channel Master engineers in late 1970. This led to a design project

which had, as its *principal objective*, the development of a TV antenna with a higher Interference Rejection Factor (IRF) than ever before attained. High gain, of course, remained a major objective, but was not to be achieved by any sacrifice of IRF. The project was completed in the spring of 1972 with the successful development of the Channel Master "Quantum" antenna.

The IRF is defined as the ratio of an antenna's *maximum* sensitivity normally the front) to its *average* sensitivity in the rear 180° sector. The peak IRF of high-gain antennas to date has been 15 to 18 dB. The Quantum antennas (there are eight VHF/UHF/FM models and seven VHF/FM models) have an average IRF of 25 dB, and they go as high as 35 dB. Remember, they are high-gain antennas designed from scratch to eliminate rear and side interference.

In a reception area where the predominant interference originates at the rear or sides of the antenna, a 10 dB improvement in signal-to-noise ratio occurs: *note that this is equivalent to a 10 dB increase in antenna gain.*

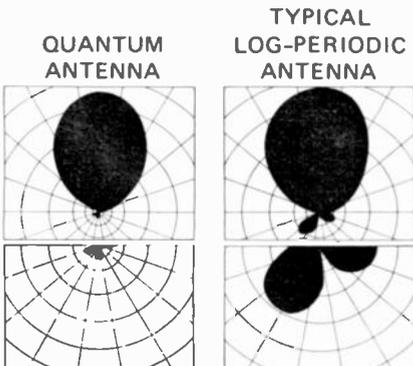
The importance of this concept cannot be over-emphasized. In many deep-fringe reception situations, eliminating interference by an antenna with improved IRF will bring about the same dramatic improvement in picture quality that technicians normally expect only from higher antenna gain. And in near-fringe and suburban areas, where the TV signal is usually ample, but where interference sources are numerous, the use of a high IRF antenna will usually eliminate all signs of interference.

It is generally known that the "orchestration" of current distribution on the elements of an antenna determines its gain, bandwidth, and pickup patterns. Several years ago, Channel Master introduced the principle of Proportional Energy Absorption in its high-gain Crossfire. The impedance of each element was adjusted so that every driven element in the array absorbed approximately the same amount of current, since uniform current distribution was a key to high broadband gain.

However, equal current distribution does not produce the best possible front-to-back ratios. For the next step to occur, the state of the art had to await development of sophisticated new measuring equipment which permitted, for the first time, the application of Fourier Transform Theory to TV antenna design.

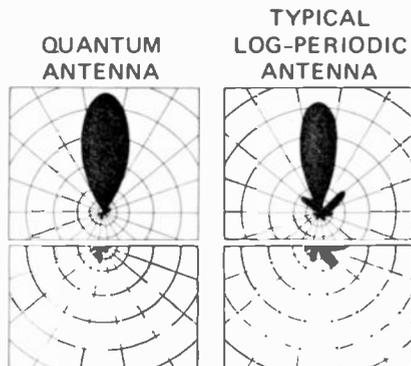
Fourier Transform Theory, widely applied in radio-telescopes and space communications, states that a *tapered*, symmetrical distribution of current over an antenna's elements will yield

RADIATION PATTERN CHANNEL 3



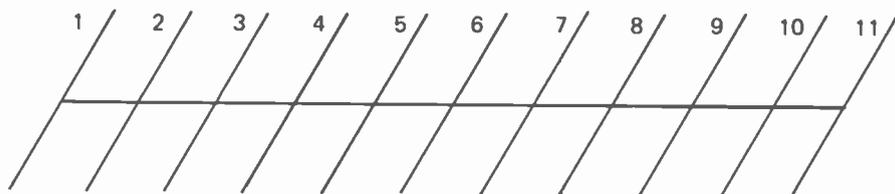
REAR LOBES MAGNIFIED BY 10dB

RADIATION PATTERN CHANNEL 10

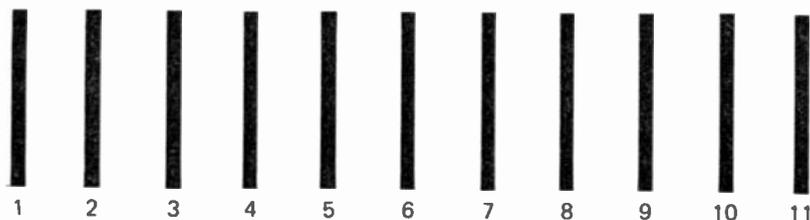


REAR LOBES MAGNIFIED BY 10dB

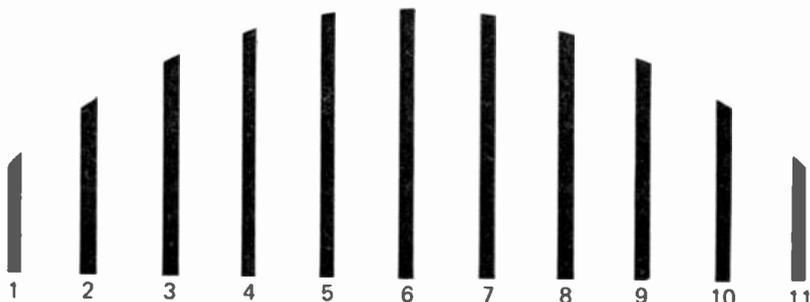
REAR-LOBE RESPONSE OF QUANTUM ANTENNA compared to a typical log-periodic on channels 3 and 10. Quantum has the best front-to-back ratio.



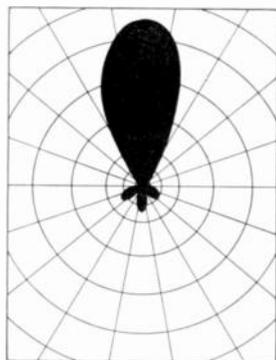
TYPICAL ANTENNA



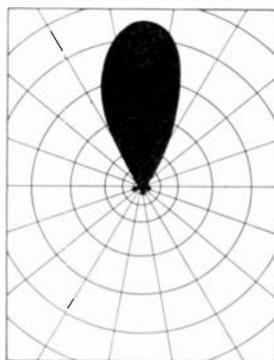
UNIFORM CURRENT DISTRIBUTION



TAPERED CURRENT DISTRIBUTION



Radiation Pattern  
UNIFORM CURRENT



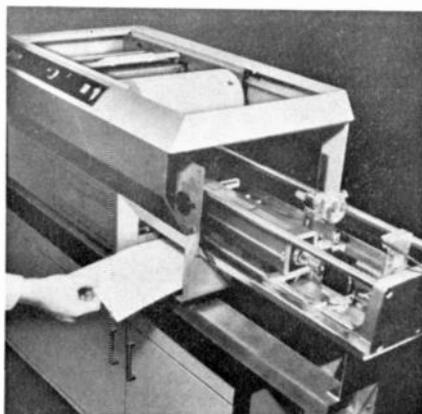
Radiation Pattern  
TAPERED CURRENT

**ANTENNA GAIN AND RADIATION PATTERN** is determined largely by the amplitude and phase of the currents in the driven and parasitic elements. The Quantum antenna parasitic elements are designed for tapered current distribution which results in minimum pickup of signals arriving from directly behind and from the right-rear and left-rear sectors.

### New high-speed laser printer operates with ultrasound

A non-impact experimental high-speed printer recently demonstrated by Zenith prints as fast as most computers can deliver the data. Operating at a rate of 5,000 lines a minute, it turns out four pages (64 lines of 132 characters each) in a second. Most printers work at about one-fourth of that speed, and their inability to keep up with the computer makes the printer a bottleneck in data processing.

The new machine can print on photo-sensitive paper or microfilm, with a resolution of 1,000 spots (almost



patterns with the smallest side and rear lobes.

The new instrumentation referred to above provided new insights into the functioning of TV antennas and a greater ability to measure currents precisely in both phase and amplitude. Advanced engineering also contributed to the maintenance of the symmetry and balance of the antenna system. As a result the Quantum antennas reach new performance levels in both IRF and gain.

There is another source of interference problems: transmission line pickup. In theory, the input impedance of the TV receiver is balanced; it does not respond to a signal present on both wires of a twin-lead transmission line. In practice, however, the balance is never perfect. This degrades picture quality, since interference signals induced on the twin lead appear on the picture tube. For this reason, about 10% of installations today use coax with a balun at each end.

There is an optional balun available for the Quantum, specially designed to fit into a terminal housing on the antenna crossarm.

One source of interference is particularly difficult to eliminate—local FM transmission. The growing number of FM stations has made this a problem of major dimensions—especially in areas where the TV signals are weak. The effectiveness of the Quantum can be augmented in such situations with printed circuit FM trap, model 0091, that fits into the Quantum's terminal housing.

The Quantum is engineered to provide excellent FM reception, with the same high IRF as for the TV frequencies. There are 15 models in all, ranging from city-metropolitan to deep fringe. The 82-channel models feature an adjustable high-gain uhf antenna, mounted on the front end, that can be peaked for a range of selected channels in any reception area. The Quantum is a new generation of antenna. It is more signal-selective and sets new standards of color reception in every area. **R-E**

double the resolution of a home television receiver).

Information from a computer is converted into ultrasonic frequencies that control the brightness and the scanning of the laser beam. One ultrasonic signal modulates the beam; a second, by varying in frequency, causes it to scan (the higher the frequency, the greater the beam deflection).

The operation is entirely electronic—the only mechanical system in the printer is the transport that carries the paper at 90 feet a minute through the rapid dry-development process and delivers the pages to the operator. **R-E**

# STATE-OF-SOLID-STATE

This month's selection of semiconductor devices is diverse and interesting.

The more unique of these include a receiver in a 3-lead IC package and a digital alarm clock on a single IC chip.

by LOU GARNER

FROM THE REPORTS RECEIVED, MANY OF YOU were fascinated by the Lithic Systems' LP2000 microtransmitter IC discussed in February. In fact, a number of readers wondered why no manufacturer offered a comparable "receiver IC."

Actually, such a device is available, although designed to operate over a different frequency range than the LP2000. It's Ferranti's ZN414, a 10-transistor trf (tuned radio frequency) receiver IC assembled in a 3-lead TO-18 package and selling, in 1-4 quantities, for \$5.00 each plus \$0.50 for postage and handling. A detailed applications circuit booklet is offered by the U.S. subsidiary, Ferranti Electric, Inc. (East Bethpage Road, Plainview, N.Y. 11803).

The ZN414 consists of a high-impedance (4 megohm) input stage, several capacitively-coupled rf amplifier stages, and a transistor detector stage, as illustrated in Fig. 1. Requiring but six external components for operation as an AM broadcast band receiver or tuner, the device is suitable for use from 150 kHz to 3 MHz. It can be powered by dc sources from 1.2 to 1.6 volts (a single cell) and draws less than 0.5 mA. With a 1.3-volt dc source and a high-Q coil, the ZN414 has a threshold sensitivity of 50 $\mu$ V and can deliver a typical power gain of 72 dB. Its agc range is 20 dB. Selectivity is quite good for a single-tuned design and, according to the manufacturer, a 4-kHz bandwidth is possible with suitable coils.

Although the ZN414 can drive a sensitive earphone, the manufacturer suggests that the device be used in conjunction with an audio amplifier for greater sensitivity and power output, using an arrangement similar to the circuit shown in Fig. 2. The audio section may be as simple as a single transistor driving an earphone, a multistage complementary push-pull design, or an audio amplifier IC.

## OOPS!

Have you ever considered the unemployment situation and economic chaos that could result if people stopped making mistakes? No longer would pencil manufacturers have to include eraser tips on their products. The "CE" key could be eliminated from electronic calculators, reducing the demand for these components. The manufacturers of erasers, correction fluid, and ink eradicators would face economic ruin. Supervisors would be hard pressed to find fault with their underlings and thus encourage them to greater efforts. Psychiatrists' offices would be jammed. Teachers would have to develop completely new grading systems. Editors would be frus-

trated. The world, in short, would totter on the brink of disaster.

Frankly, I wouldn't want to see all of this happen, so I manage to do my bit in avoiding such a catastrophe by making an occasional mistake (sic). Not deliberately, of course, and I try my best to avoid overdoing it (after all, others are helping), but one does manage to slip in from time to time.

My latest goof occurred in the June issue when I inadvertently described the Signetics ULN2111 FM limiter/detector IC as if it were a completely new device. This rather miffed my (former??) friend Sidney Chertok, Director of Information Services for the Sprague Products Company (North Adams, Mass. 01247), who wasted no time in letting me know that the ULN2111 was first introduced by Sprague some time ago, and, further, that Signetics was but one of several "second-sources" for the interesting and versatile device.

As Napoleon may have said after the battle of Waterloo . . . *c'est la vie!*

In any case, my personal apologies to Sprague, and, most of all, to my readers, for the boo-boo.

## Tick-tock-tick-tock . . .

With single-chip calculator circuits a reality and available from several sources, and interest in electronic clocks booming, it was only a matter of time before someone introduced a single-chip digital clock circuit. The latest here is the MM5316, a complete self-contained digital alarm clock circuit capable of directly driving fluorescent tube or liquid crystal displays, announced recently by the National Semiconductor Corporation (2900 Semiconductor Drive, Santa Clara, Calif. 95051).

As shown in Fig. 3-a, the MM5316 provides all the logic and decoding needed to assemble several types of clocks and timers, including 12- or 24-hour alarm clocks and desk clocks, clocks for radios and automobiles, stop watches, appliance timers, and industrial timers. The unit is a monolithic integrated circuit that uses both

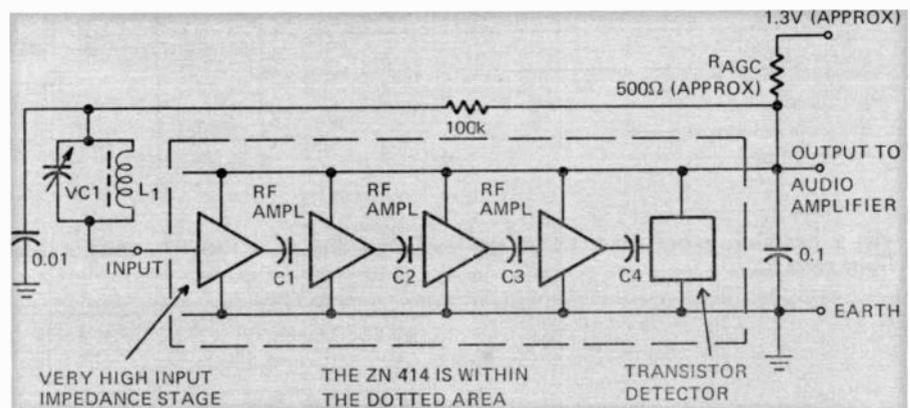


FIG. 1—FERRANTI'S ZN414 RECEIVER IC—Internal block diagram.

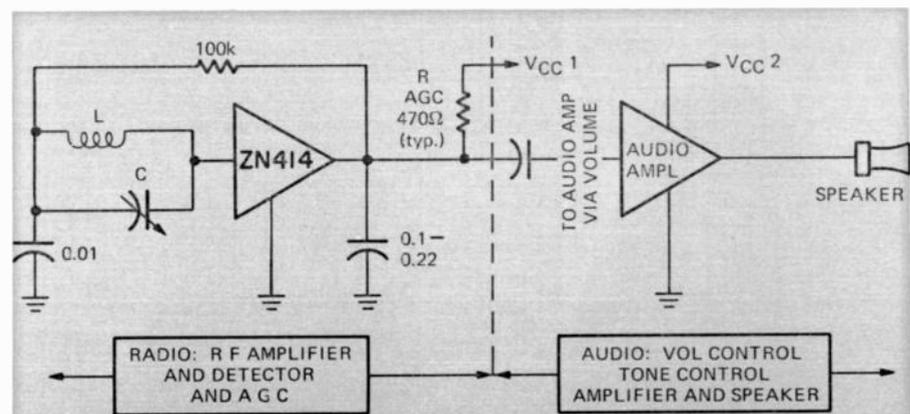


FIG. 2—TYPICAL RECEIVER BLOCK DIAGRAM for the ZN414.

low-threshold P-channel enhancement mode and ion-implanted depletion mode devices. It is supplied in a 40-pin plastic DIP, Fig. 3-b, and is designed to operate from 8- to 29-volt unregulated dc sources.

The MM5316's timekeeping function is triggered by either a 50 or 60-Hz input, with the display format either 12 hours with leading zeros suppressed and an AM/PM indication, or 24 hours. In addition, the device offers the user four possible display modes: 1) time in hours and minutes, 2) time in minutes and seconds, 3) alarm set time, and 4) sleep time. Outputs are provided for display drives, alarm enable, and sleep or timed radio turnoff.

In operation, a Schmitt trigger shaping circuit built into the MM5316 permits the

use of a simple filtered sine wave at 50 or 60 Hz as the input signal, providing about 6 volts of hysteresis and driving the counter chain that performs the actual timekeeping function. Either 50 or 60-Hz operation is programmed via a single pin connection, while two other pins are used for fast and slow time and alarm setting.

Alarm operation is controlled by a comparator that senses the coincidence between the alarm counters (i.e., the alarm setting) and the time counters (real time). The comparator output sets a latch which turns on the alarm output driver. The latch remains set for 59 minutes, during which time the alarm sounds unless it is reset with the ALARM OFF input, or the SNOOZE ALARM input which temporarily inhibits the alarm

for 9 minutes.

The MM5316 also contains an interval timer which can be set for up to 59 minutes. This may be used in clock radios, for example, to allow the user to fall asleep to music, with the radio shutting off after the preset interval. In desk clocks, the interval timer could be used to sound an alarm after a preset period to remind the user of an event, such as the end of a three minute phone call.

Abstracted from NSC's technical bulletin on the MM5316, a complete schematic diagram for a general purpose digital alarm clock using the device and a standard fluorescent tube display is in Fig. 4. An external alarm sound generator is required, of course, as well as an external control device

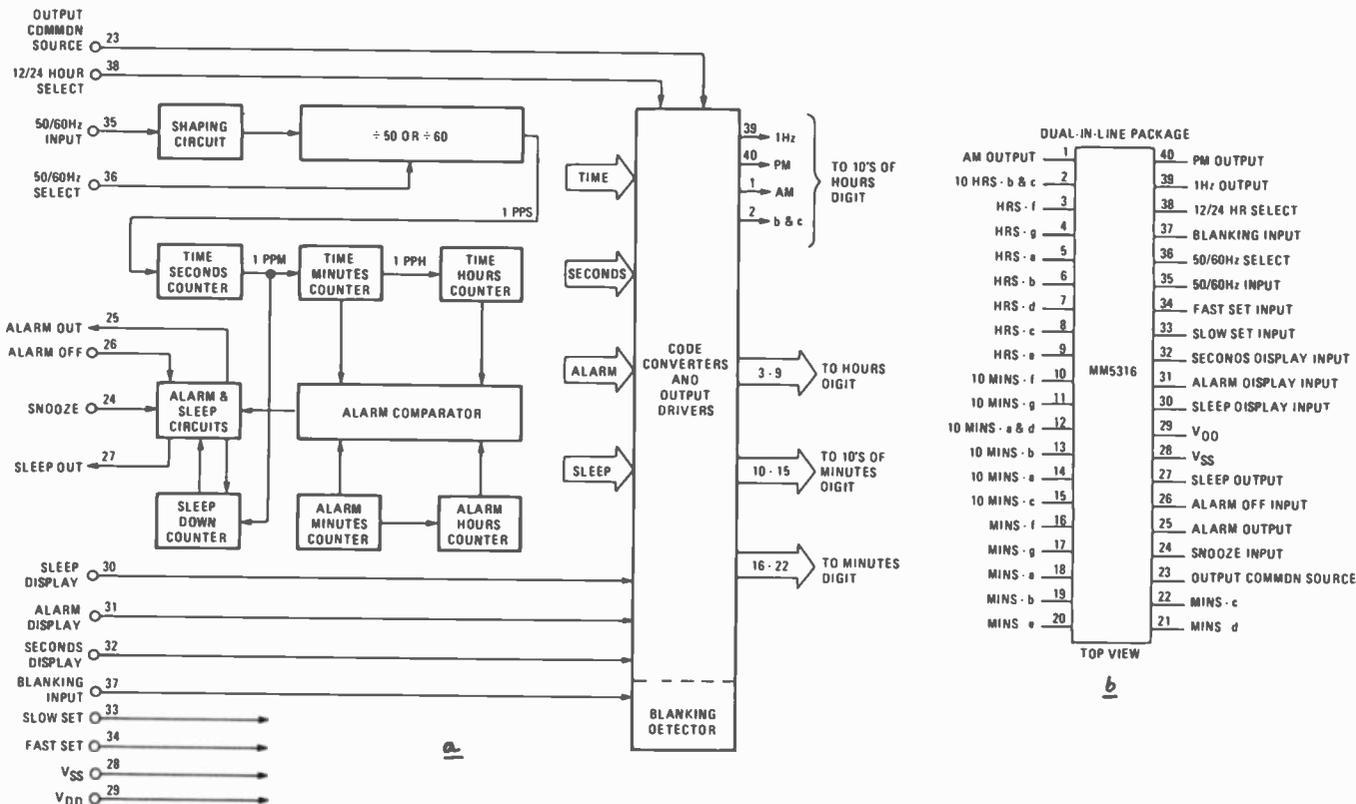


FIG. 3—INTERNAL BLOCK DIAGRAM (A) AND lead connections (B) of National's MM5316 digital alarm clock IC.

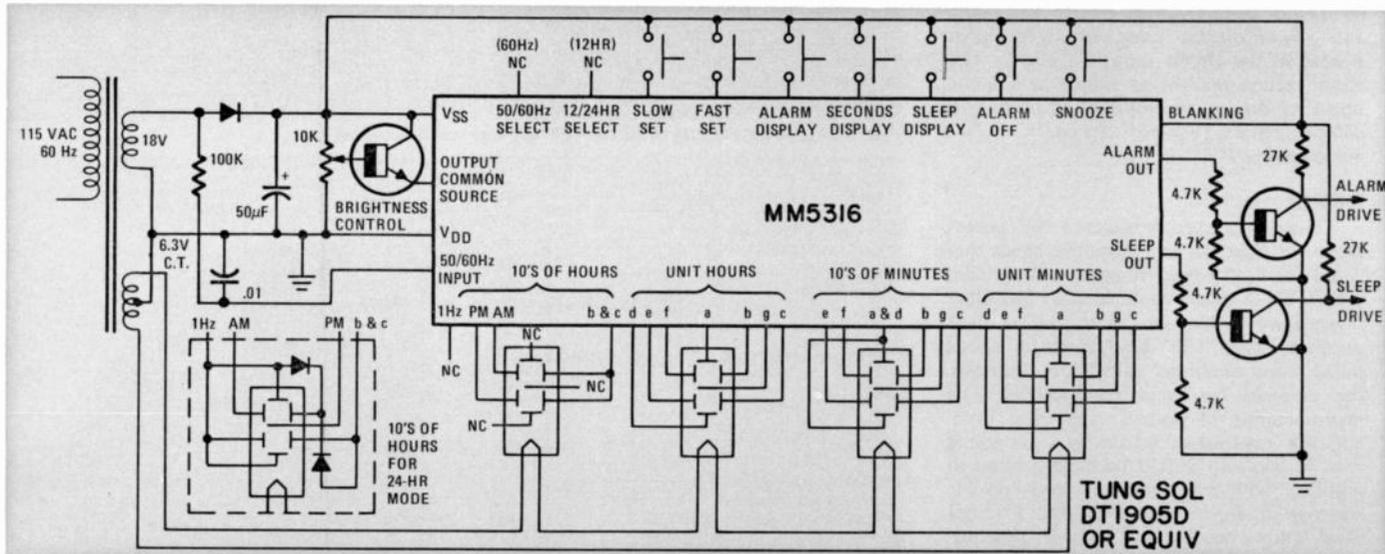


FIG. 4—COMPLETE SCHEMATIC DIAGRAM FOR a digital clock using the MM5316.

for "sleep" switch operation, should these features be desired.

### Let there be light

Undismayed by continuing inflationary pressures, both Hewlett-Packard (1501 Page Mill Road, Palo Alto, Calif. 94304) and Motorola (P.O. Box 2953, Phoenix, Ariz. 85036) are doing their bit to hold down the prices of light emitting semiconductor devices. H-P initiated the fight against higher prices with their introduction of a LED priced at only 17 cents each in 100,000 lots, as reported in my May column. Motorola was not far behind with their announcement of a 10-cent LED (in 1,000,000 lot quantities). Now both have announced low-cost digital readouts.

H-P's offering, Fig. 5, is a 0.3-inch

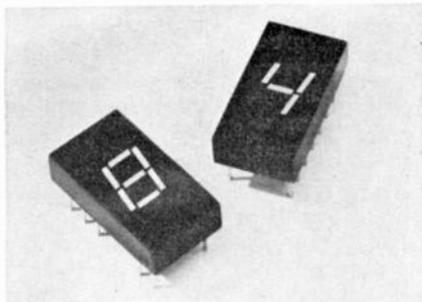


FIG. 5—H-P's NEW LED numeric displays are low cost.

high, seven-segment single-digit device in a DIP package. Their type 5082-7730 contains a left-hand decimal point, while type 5082-7731 features a right-hand decimal. Both displays are IC compatible.

Forward voltage per segment or decimal point is 1.6 volts; luminous intensity is typically 250 microcandelas per segment; typical operating current is 10 mA per segment when strobed. Each display makes use of but one LED per segment (eight in all), with a funnel-shaped "light pipe" used to stretch the light source optically to a bar five times the length of the LED chip.

Suitable for applications in calculators, TV sets, radio receivers, counters, test instruments, and digital clocks, H-P's new displays are priced at only \$2.95 each in quantities of 1,000.

Recognizing that hobbyists and experimenters, too, are interested in low-cost digital readouts, Motorola's HEP Semiconductor group has introduced a four-device, seven-segment readout kit at a net price of only \$9.98 per kit. This is equivalent to a price of less than \$2.50 per readout device.

Designated the HEK-5 kit, the new HEP item includes a valuable booklet that contains basic information about readouts, their characteristics, applications, and capabilities, as well as a number of suggested "thought starter" projects. Complete parts lists and schematic diagrams for each project are featured in the booklet.

### Product/device news

In addition to its digital alarm clock IC, described earlier, the National Semiconductor Corporation has introduced a number of other new devices, including a quad comparator, a one-chip calculator IC, and a family of solid state transducers.

Designated type LM359, National's new quad comparator, is the first comparator specifically designed for use with

both CMOS and bipolar logic. It can operate over a wide range of power supply voltages . . . from 2 to 36 volts on a single supply, or from  $\pm 1$  to  $\pm 18$  volts on dual supplies . . . and requires only about 0.8 mA total current; with a 5 volt supply, the device draws only 1 mW per comparator.

Input offset voltage on all four comparators is typically 2 mV, with a guaranteed maximum of 5 mV at room temperature. Suitable for use as an interface between different logic levels or in interfacing sensors, such as those used in speed control systems and level sensing to logic circuits, the LM359 is offered in both plastic and ceramic 14-lead DIP's.

National's new calculator IC, type MM5725, is a complete 8-digit calculator on one MOS/LSI chip. It uses three registers to provide the four arithmetic functions—addition, subtraction, multiplication, and division—and also contains a 16-place decimal point register and self-contained oscillator and clock driver.

Calculations in the device are handled in floating decimal point for both entry and display, while internal timed key-bounce protection circuits permit the use of low-cost keyboards without affecting calculator performance.

The unit can be used with virtually any type of display, including LED's, Panaplex II neon readouts, and fluorescent display tubes. Designed for operation with a -28-volt and a -35-volt supply, the MM5725 is available in a 28-pin DIP.

Claimed to be the industry's first full family of IC transducers, National's new line is designed for applications in such industries as automotive, medical, altimetry and air data, computer peripherals, communications, air conditioning and refrigeration, heating and ventilation, food and chemical processing, hydraulics, numerical control, and process control.

Each device in the line contains in a single small package all four of the basic transducer elements—diaphragm and vacuum reference, piezoresistive sensor, signal discriminator and conditioner, and signal amplifier and processor. The first three functions are contained on a single die, the fourth provided by standard IC op amps. Various models are offered for measuring absolute, gage, and differential pressures.

Designed for complete rf amplifier or driver applications in uhf land mobile communications systems, two new amplifier modules have been introduced by Motorola Semiconductor Products, Inc. (P.O. Box 20912, Phoenix, Ariz. 85036). Designated types MHW709 and MHW710, both hybrid units are intended for operation on 12.5-volt dc sources.

The MHW709 delivers 7.5 watts output with a driving power of approximately 100 mW for a power gain of 18.8 dB, while the MHW710, Fig. 6, supplies a full 13.0 watts with only 150 mW of driving power and a power gain of 19.4 dB.

Two versions of each model are offered, one covering the 400 to 440 MHz range, the second the 440 to 470 MHz band. Harmonic suppression is at least -40 dB down across the frequency range with all spurious outputs more than 70 dB below the desired signal. Input impedance is 50-ohms for both modules, and operation with a 20:1 load mismatch produces no damage to the units.

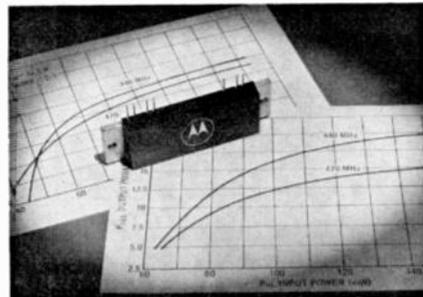


FIG. 6—MOTOROLA'S MODULAR uhf hybrid amplifier, type MHW710.

A new hf power transistor offered by the Amperex Electronic Corporation (Hicksville, N.Y. 11802) produces up to 150 watts in class A, B, C, CW and SSB service up to 70 MHz with  $IMD \leq -30$  dB. Designated type BLX15, this new npn silicon planar transistor, is ruggedized against mismatch failures and offers a gain-bandwidth product of 300 MHz at collector currents as high as 10 amps. Intended for use in industrial, military and commercial applications, the BLX15 operates on 28 Vdc.

Meanwhile, back in the great southwest, Texas Instruments, Inc. (P.O. Box 5012, Dallas, Tex. 75222) has introduced a number of new devices, including a family of six optically-coupled isolators and a chopper-stabilized op amp IC.

TI's new opto couplers, identified as types TIL114 through TIL119, are supplied in 6-pin DIP's. Each coupler consists of a gallium-arsenide LED and a high-gain standard or Darlington phototransistor.

The TIL117, for example, has a minimum 50% current transfer ratio at a forward current of 10 mA. The TIL114 has a minimum 12.5% current transfer ratio at a forward current of 16 mA. The TIL115, TIL116, TIL118, and TIL119 are rated at 10 mA forward current with current transfer ratios of 2, 20, 6, and 300 percent.

Electrical isolation for the TIL114-117 is  $\pm 2.5$  kV, while the TIL118 and 119 are rated at  $\pm 1.5$  kV. The devices may be used as solid state relays, for circuit isolation, and as interface devices between systems, as well as for line driver/receiver applications.

Designated type SN62/72088, TI's new chopper-stabilized op amp, is believed to be the first of its kind to be integrated and made available in a standard 14-pin plastic DIP. The unit's characteristics include a 35- $\mu$ V input offset voltage, a 130 dB voltage gain, a slow rate of 25V/ $\mu$ s, a small signal rise time of 65 ns/pe, and a low 0.6  $\mu$ V/ $^{\circ}$ C offset voltage drift.

The SN62/-72088 comprises two IC chips encapsulated in a single package. One is a P-channel MOS chip, the other a JFET bipolar chip. Fabricated on the MOS chip are three linear amplifiers, a clock generator, multiple stages of flip flops, associated logic decoding, and MOS analog switches; this chip performs chopper control, synchronous demodulation control, and some sample and hold functions.

The second chip contains two amplifiers, with the main one an internally-compensated high-frequency wideband amplifier and the second an active low-pass filter which provides nulling of the main amplifier's offset voltage.

That concludes our look at the solid state field for now.

R-E

# CIE graduate builds two-way radio service business into \$1,000,000 electronics company!

**How about YOU? Growth of two-way transmitters creates demand for new servicemen, field and system troubleshooters. Licensed experts can make big money. Be your own boss, build your own company. And you don't need a college education.**

Two-way radio is booming. There are already nearly seven million two-way transmitters for police cars, fire department vehicles, taxis, trucks, boats, planes, etc., and Citizens Band uses. And the number keeps growing by the thousands every month. Who is going to service them? You can — if you've got the know-how!

## Why You'll Earn Top Pay

One reason is that the United States Government doesn't permit anyone to service two-way radio systems unless he's *licensed* by the FCC (Federal Communications Commission).

Another reason is that when two-way radio men are needed, they're *really* needed! A two-way radio user must keep those transmitters operating at all times. And, they *must* have their frequency modulation and plate power input checked at regular intervals by licensed personnel to meet FCC requirements.

As a licensed man, working by the hour, you would usually charge at least \$5.00 per hour, \$7.50 on evenings and Sundays, plus travel expenses.

Or you could set up a regular monthly retainer fee with each customer. Your fixed charge might be \$20 a month for the base station and \$7.50 for each mobile station. Studies show that one man can easily maintain at least 135 stations — averaging 15 base stations with 120 mobiles! This would add up to at least \$12,000 a year.



Edward J. Dulaney, Scottsbluff, Nebraska, (above and at right) earned his CIE Diploma in 1961, got his FCC License and moved from TV repairman to lab technician to radio station Chief Engineer. He then founded his own two-way radio business. Now, Mr. Dulaney is also President of D & A Manufacturing, Inc., a \$1,000,000 company building and distributing two-way radio equipment of his own design. Several of his 25 employees are taking CIE courses. He says: "While studying with CIE, I learned the electronics theories that made my present business possible."

## Be Your Own Boss

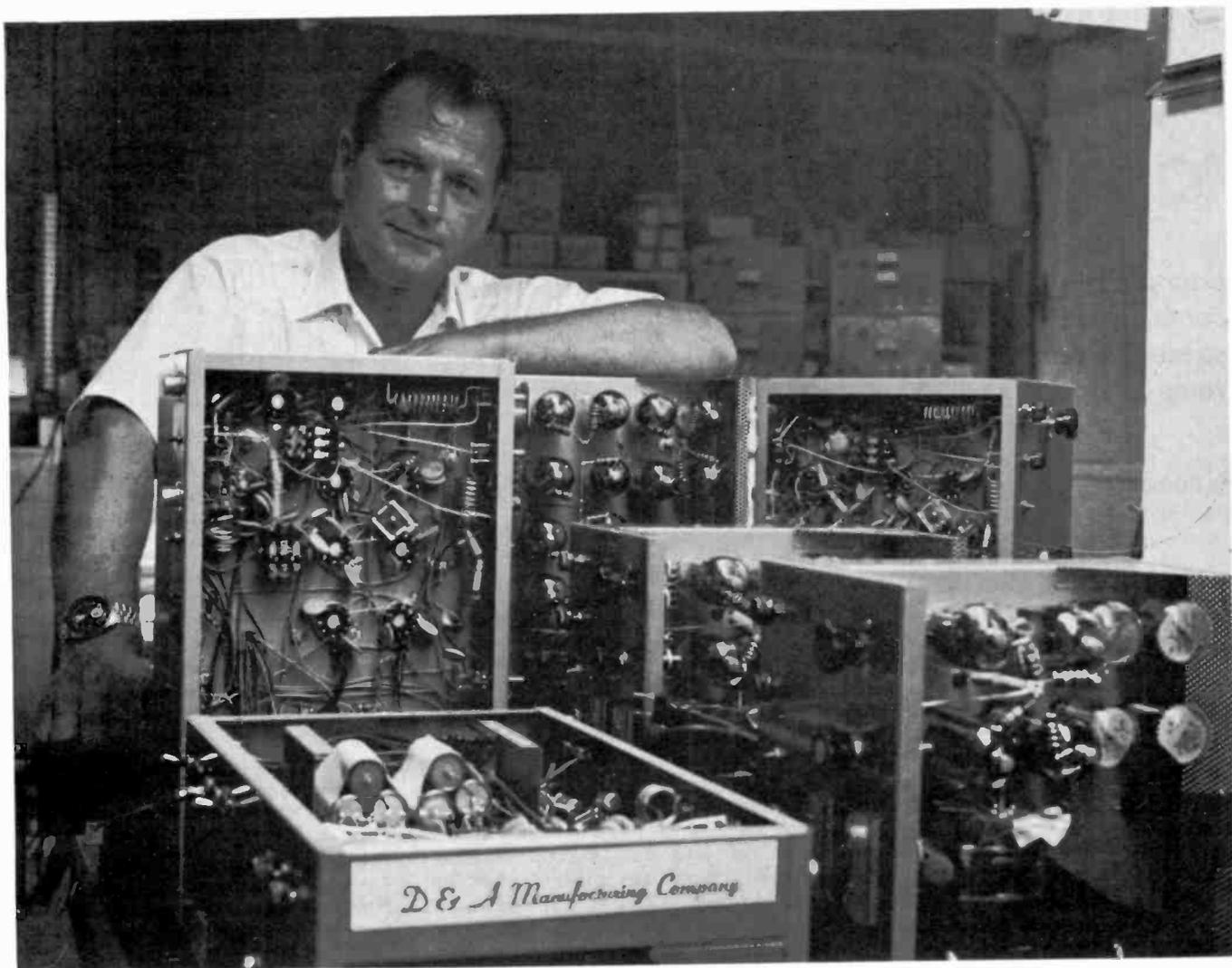
There are other advantages, too. You can become your own boss — work entirely by yourself or gradually build your own fully staffed service company. Of course, we can't promise that you will be as successful as Ed Dulaney, or guarantee that you'll establish a successful two-way radio business of your own, but the opportunities for success are available to qualified, licensed men in this expanding field.

## How To Get Started

How do you break in? This is probably the best way:

1. Without quitting your present job, learn enough about electronics fundamentals to pass the Government FCC exam and get your Commercial FCC License.
2. Then get a job in a two-way radio service shop and "learn the ropes" of the business.
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RE-23

Circle 16 on reader service card

# add voice actuation to your phone sentry

A simple and inexpensive adapter described in the June issue contains the control electronics that lets you use two cassette recorders as a phone-answering device. Here is how voice-actuation removes the time limit on the caller.

by ROGER L. SMITH

HERE'S A USEFUL ADDITION TO THE Phone Sentry automatic telephone answering machine (Radio-Electronics, June 1973). The original Phone Sentry circuit contains a 30-second monostable that times the recording of the incoming messages. With the addition of this voice-actuated circuit, your incoming message recorder will run for as long as the caller talks.

An advantage to adding this circuit (apart from recording long messages) is that it stops your recorder 6 to 8 seconds after the caller hangs up. Thus when you play back the messages, you have a maximum of 8 seconds of dial tone between messages. Since most callers leave only a short message, you will find this a welcome change and also you will be able to

record more messages on less tape.

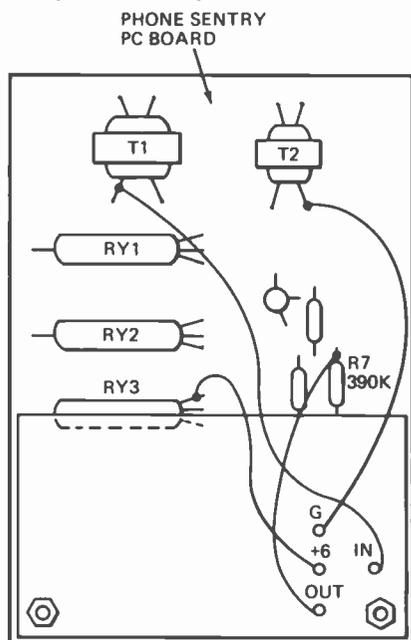
One word of caution. This voice-actuated circuit can't be used on all phone lines. You can quickly tell if your line will accept the circuit by picking up your receiver and listening to the dial tone for 30 to 40 seconds. If you hear nothing but dial tone for this time, or dial tone for 20 seconds and then silence, the circuit *can* be used on your line. On phone lines where a recording is heard after 20 seconds (asking you to dial again), or if an intermittent tone is heard (an out of order signal), then the circuit

will *not* work. Also, if there is a high level of noise on your line, you will have difficulty with the circuit.

A feature of this circuit is that by simply disconnecting the output lead, you can restore your answering machine to the original 30-second operation. You could even put a switch in this lead if you expect to change locations in the future and you find you can't use the circuit.

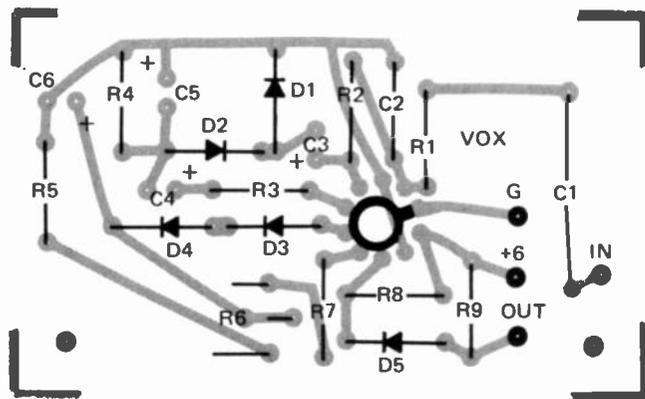
## How to build it

Build up the circuit on a 2 x 3/4-inch board. You can use perf-board or



VOICE-ACTUATED BOARD MOUNTED ABOVE PHONE SENTRY BOARD

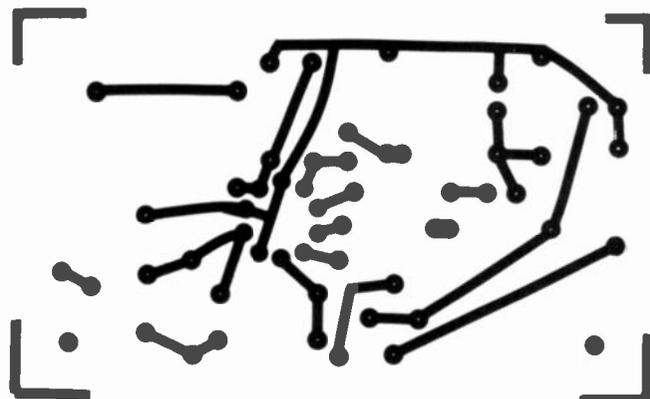
THERE IS ADEQUATE SPACE inside the Phone Sentry for the VOX circuit PC board.

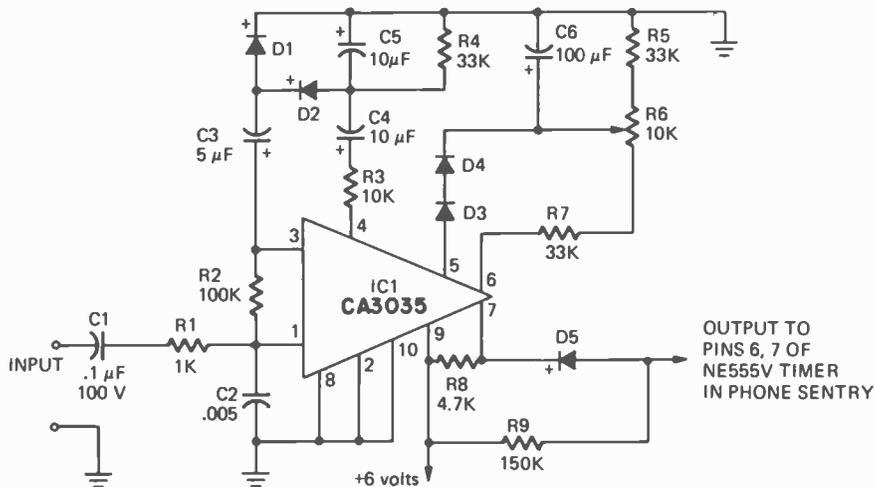


P.C. BOARD PATTERN COMPONENT LAYOUT

LAYOUT OF PARTS on the PC board used to add voice-actuation to the Phone Sentry. Diodes D1-D5 are ordinary 1-amp silicon devices

PC FOIL PATTERN is shown full-size. Trace or photograph it or use it as a model as you design your own board.





THE VOICE-ACTUATED (VOX) CIRCUIT is designed around an IC that contains an array of three ultra-high-gain wide-band amplifiers. Average gain per stage is about 44 dB.

#### PARTS LIST

All resistors 1/4-watt 10% unless noted

- R1—1000 ohms
- R2—100,000 ohms
- R3—10,000 ohms
- R4, R5, R7—33,000 ohms
- R8—4700 ohms
- R9—150,000 ohms
- R6—10-ohm trimmer control
- C1—0.1 μF, 100V
- C2—.005 μF
- C3—5 μF, 15V electrolytic

- C4, C5—10 μF, 15V electrolytic
- C6—100 μF, 15V electrolytic
- D1 thru D5—1A silicon diodes
- IC1—CA3035 integrated circuit (RCA)
- Circuit board, hook up wire and mounting hardware as required
- NOTE: A circuit board is available for \$2.25. A kit of all of the above parts can be obtained for \$9.95 (plus postage) from Southwest Technical Products Co., 219 W. Rhapsody, San Antonio, Tex. 78215

the foil pattern shown in this article. Watch capacitor and diode polarities and don't overheat leads. Mount the board by two corners with 3/4-inch spacers and 1/4-inch 6-32 screws directly above the board in the Phone Sentry (over the end nearest IC1). Four 6-inch leads are necessary to connect up the board. Follow the dia-

gram for their connections.

After you have installed the board, you will have to make some final adjustments. Adjust R6 (10,000-ohm trimmer) so the output (pin 7) will go high when there is no input signal. Also, you may have to change the value of R1 to alter the gain of amplifier 1. This would only be neces-

sary if you had a noisy line; so do not make this change unless you have to.

#### How it works

The signal from the phone line is coupled thru a 0.1-μF, 100-volt capacitor to pin 1 of the CA3035 amplifier (do not use a lower voltage capacitor for C1). The CA3035 contains three separate amplifiers. The output of the first amplifier (pin 3) is ac coupled to diodes D1 and D2. The rectified signal appearing across R4 is coupled thru C4 and R3 to amplifier 2 (pin 4). This ac coupling means that a steady tone signal (dial tone) or silence will generate no output from the second amplifier. Only variable signals such as voice signals are amplified. The output of amplifier 2 (pin 5) is rectified by D3 and D4 (two are required to give the proper dc level shift), and filtered by capacitor C6. This final dc signal is then coupled to amplifier 3 which is used as an inverter and as isolation.

When voice signals are present at the input of the circuit, the output (pin 7) is held low. Since this output is coupled to the timing capacitor of the NE555v thru D5, the timing capacitor will not charge up and the NE555v will net "time out." When the input signal is a steady tone signal or silence, the output (pin 7) rises toward +6 volts and the timing capacitor is allowed to charge up. Resistor R9 (150,000 ohms) is in parallel with the 390,000-ohm resistor in the Phone Sentry timing circuit, so this reduces the charging time from 30 seconds to about 8 seconds.

R-E

## electronic news

A high-efficiency optical fiber just developed by Bell Laboratories scientists makes it possible to fabricate an efficient light-carrying fiber from a single material. Up to the present, optical fibers have been made with two materials: a center core—glass or liquid—and a surrounding outer cladding. Fibers made

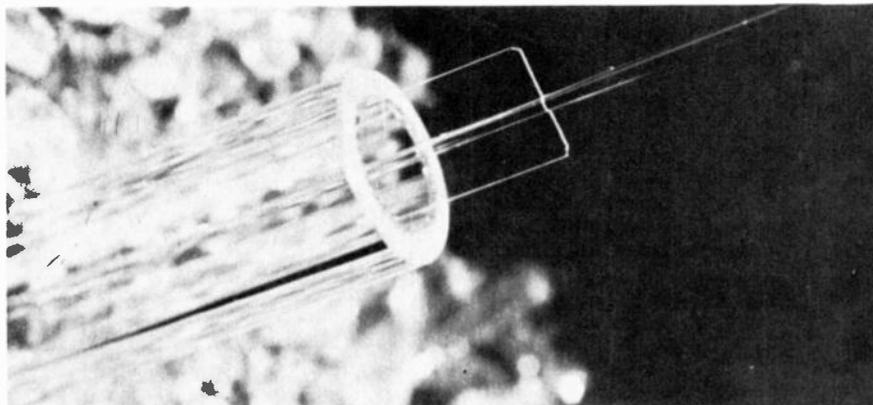
with different glass materials may have contained impurities that caused transmission losses.

Three Bell scientists, S. E. Miller, E. J. Marcattili and P. Kaiser, selected a glass that showed a very low transmission loss as an unclad fiber. Then they developed a unique configuration that

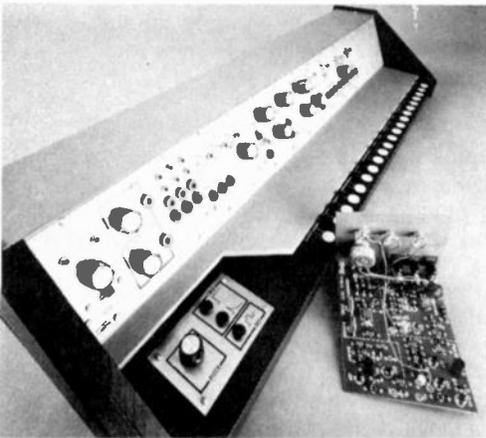
made it possible to form the glass into an optical fiber without any additional materials. One design has three components, as shown in the photograph: an outer tube, a transverse partition across the tube that acts as a supporting plate for the center rod, which is the optical conductor.

The assembly is then drawn into a hair-thin fiber. In drawing, all parts are brought into close contact, but the contact is not intimate enough to permit escape of light from the rod, even though plate, rod and tube are made of the same type of glass.

The excellent light conduction (losses of 5 dB per kilometer) would make it possible to space signal amplifiers farther apart than in land cable systems now in use, and scientists are looking ahead to the day when such glass fibers, packed into cables perhaps a quarter inch thick, may carry as many signals as thousands of the present telephone wires.



THE NEW LIGHT-CARRYING FIBER has three main parts: the central light-conducting rod, the flat plate or partition that supports it and the outer glass tube that protects it.



Now that you have your synthesizer completed you must be ready to start playing it. Here's the instructions you will need to get started

# Using the SYNTHESIZER

by JOHN S. SIMONTON, JR.\*

IF YOU'VE BEEN FOLLOWING THE development of the **Radio-Electronics**, synthesizer (May, June, July, August, September, 1973) it's a good bet that after the last article you spent a couple of weeks plugging cables and pushing buttons. In the process you probably discovered that you could make some pretty interesting noises with the gear even if you didn't understand exactly why. This month we're going to fill in the why's and try to cover some of the not-so-obvious how's.

Since the greatest part of understanding any new field is learning the vocabulary we'll begin with preliminary definitions of *pitch* as the dominant frequency of a sound, *dynamics* as the time varying intensity changes of a sound and *timbre* as the time varying spectral changes of a sound (how the harmonic content varies with time.)

Notice that *pitch* was defined as the dominant frequency, not the fundamental frequency. The difference is mostly technical but still important from a musical standpoint. To the technician, the fundamental frequency of a waveform is by definition its lowest frequency component. To the musician, the dominant frequency is in all probability not the lowest, but the one that has the greatest impact on the listener. Because of his understanding of sound a musician will consistently refer to the subharmonics of a sound, whereupon the technician will probably begin to twitch and loudly proclaim that there's no such thing as a subharmonic.

The human ear is more sensitive to changes in pitch than any other musical parameter. Tuning is ordinarily expressed in "cents" with one cent being a frequency deviation equal to 1% of the interval between the note being tuned and the next highest note in the chromatic scale. Even an unskilled listener can spot a 3-cent change in pitch.

Finally, kind of a reverse point regarding pitch is that not all musically interesting sounds have it. Unpitched "noise" is composed of all frequencies and is typically generated by such non-resonant mechanical systems as the wind, surf, explosions, etc. When noise is used to excite a resonant system the result is "pink noise", a term that at one time denoted noise composed only of lower frequencies but lately is used to designate any bandwidth limiting. Noise

\*President, PAIA Electronics, Oklahoma City, Okla.

will be covered by examples in a later part of this text.

In Fig. 1 we have drawn a line that represents the change in overall amplitude of a sound as a function of time. Radio engineers are familiar with modulation envelopes of radio frequencies. This is the modulation envelope of an audio frequency. There are an unlimited number of possible envelopes and each has its own distinctive sound regardless of the pitch of the note involved. This is dynamics.

As it happens, Fig. 1 is an envelope

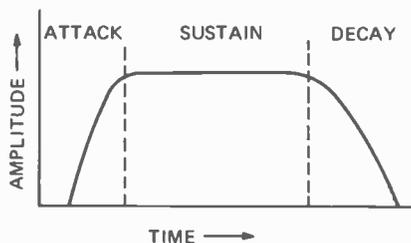


FIG. 1—WOODWIND SOUNDS have rapid attack and decay; sustain period is in between.

that would impart to the listener the feeling that he is hearing an instrument in the wood-wind family. These instruments are characterized by a moderately rapid rise in volume (attack), a steady period (sustain) followed by a moderately rapid return to zero output when the performer stops playing (decay.)

Instruments in the percussion family generally have an envelope similar to Fig. 2, characterized by very sharp attack followed immediately by an exponential decay. If the resonant member is a string as in guitar or piano the decay period can be quite long—on the order of seconds. The decay is relatively shorter if the resonant member is a steel bar as in vibs and very short if the resonant element is a tightly stretched membrane as in drums. In no case will a natural percussion instrument have a sustain period simply because the energy that causes the sound is applied in a single pulse—or possibly rapid succession of pulses.

One of the advantages that a synthesizer offers over conventional instruments is illustrated in Fig. 3. This envelope would be highly improbable in a natural instrument because it has the sharp attack of percussion followed by a sustain period

typical of reeds or horns and the long decay found in percussion strings. Considerable skill on the part of the performer would be required to produce this envelope using a conventional instrument but with a synthesizer it's simple.

## Function generator at work

In a synthesizer dynamics are handled by the combination of the function generator—which is often called an envelope generator—and the VCA (voltage-controlled amplifier). The attack and decay controls of the function generator are set to produce a time varying voltage that if viewed on the screen of an oscilloscope would look essentially the same as the envelopes shown in Figs. 1, 2 and 3. This voltage is then applied to the control inputs of the VCA. As the control voltage rises so does the gain and consequently the output of the amplifier. While the control voltage is constant when the control voltage decays the output of the amplifier decays in a similar manner.

As a demonstration, connect the modules as shown in Fig. 4 with the function

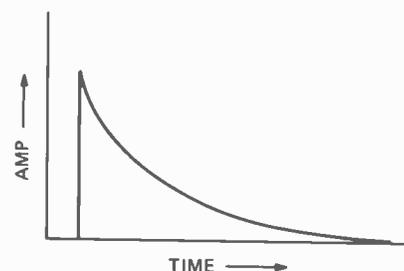


FIG. 2—TYPICAL TONE WAVEFORM produced by the attack and decay controls.

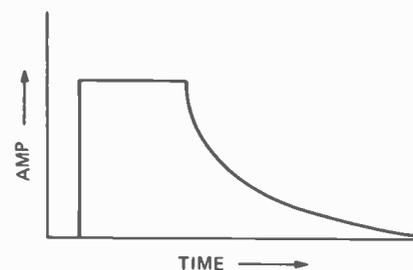


FIG. 3—INSTANT RISE, moderate sustain and logarithmic decay are possible with VCA.

(continued on page 62)

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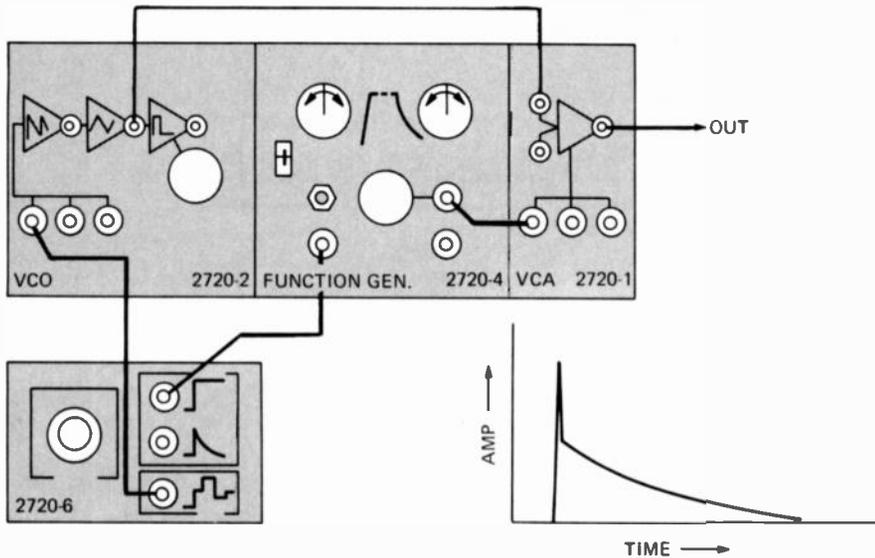


FIG. 4—WITH MODULES CONNECTED AS SHOWN the output of the function generator (see waveform) rises to its sustain level and remains there until the controller key is released.

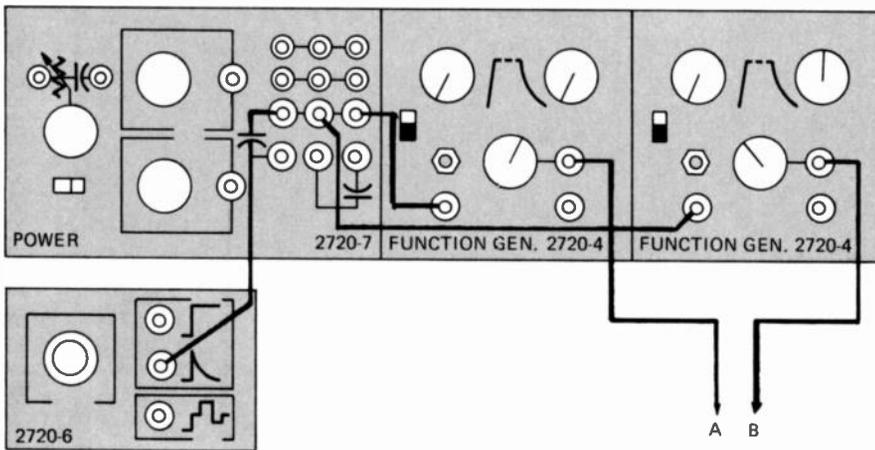


FIG. 5—TWO FUNCTION GENERATORS ARE CONNECTED as shown, to simulate certain percussive sounds. The resulting waveforms are determined by attack and decay settings.

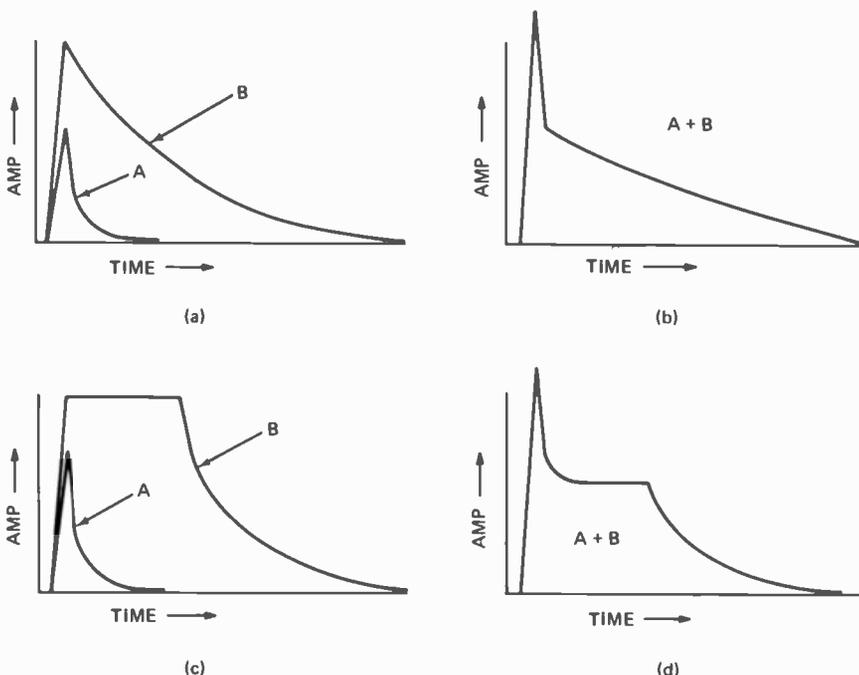


FIG. 6—HOW THE TWO FUNCTION GENERATORS, triggered by the common output of the controller are summed together to form the desired percussive waveform. Diagrams (a) and (c) show how the decay controls can be adjusted to develop various percussive effects.

generator being triggered from the controller's step output. (The operation of the controls for each module were covered in the first parts of this series. In the interest of brevity this information will not be repeated.) In this configuration the output of the function generator will rise to its sustain voltage at a rate determined by the setting of the attack control, remain at that level as long as any one of the controller keys is held down and then decay at the rate determined by the setting of the decay control.

A little experimentation with the settings of the attack and decay controls will quickly show the importance of these parameters to the total effect that the sound produces. To completely eliminate the sustain portion of the envelope, switch the trigger input of the function generator from the controller's step output to its pulse output. The short trigger pulse causes the function generator to cycle through the attack and immediately advance to decay.

Remember that we said that the arrangement of Fig. 4 could produce almost any imaginable envelope? Here's the exception. Fig. 5 shows a situation that is quite common for percussion instruments, it illustrates a case in which the instrument is played particularly hard. So hard that what can be thought of as an "overload" occurs, a short time during which the instrument is incapable of dissipating in a uniform exponential manner the applied energy.

As is shown by the envelope, the result is a brief time during which a large amount of energy is dissipated followed by the normal exponential decay. The function generator that we assembled doesn't provide for this type of envelope primarily because of cost but also because the envelope can be generated using two function generators with the added advantage of being able to, at other times, use the two modules separately. Our example illustrating this coincidentally makes a good point of the advantages of control voltage summation.

Fig. 6-a shows two function generators being triggered by the pulse output of the controller. Notice that A is set for the shortest possible decay while B is set for a significantly longer period. The outputs of these modules are routed to two of the control inputs of a single processing module—typically the VCA—where they are summed together to produce the equivalent envelope shown in Fig. 6-b.

If function generator B is triggered from the step rather than the pulse output of the controller the result is individual envelopes as shown in Fig. 6-c which sum together to produce another envelope that would be rare to the point of impossibility in a natural instrument.

There is one important point to note regarding multiple function generator arrangements and that is that the peak amplitude of the equivalent envelope is the sum of the amplitudes of the individual waveforms. For most of the equipment we've built this sum should not exceed the 5-volt design limit placed on control voltages. This same consideration also applies to any multiple control voltage situation.

### How to add timbre

As important as pitch and dynamics are, they pretty obviously don't account for all the differences between the sounds of

various instruments. For example, the trumpet and French horn are both brass instruments with approximately the same attack, sustain and decay characteristics. They even overlap in pitch range but there would be little danger of mistaking the blaring, brassy sound of the trumpet for the muted, mellow tones of the French horn. The difference between the two is what we ordinarily call timbre and as was stated earlier, differences in timbre are essentially differences in the harmonic structure of the sound the instrument generates.

Since any imaginable waveform can be constructed by summing together sine waves of the proper frequency, amplitude and phase, the most obvious way to impart timbral differences to an electronic musical instrument is to get a bunch of oscillators going and sum their outputs together as needed to produce the desired waveform. This technique is known as frequency synthesis and is most often employed in electronic organs. Fig. 7 shows the result of summing a fundamental with its half amplitude second harmonic to produce the wave form shown by the solid line.

Mother Nature has developed a different method that she uses in what is probably the most versatile of all synthesis systems, the human voice. Most electronic music synthesizers employ the same technique, known as formant synthesis.

In formant synthesis the starting point is not a group of oscillators producing precisely time-related sine waves but a single oscillator that is cranking out a waveform rich in harmonics from the start. Rather than adding in sine waves as needed to produce a given voice, component frequencies are removed from the source as needed.

As an example, Table I gives the harmonic content of the three common waveforms that our VCO produces; ramp, triangle and square wave. Referring back to the wave in Fig. 7 again and comparing it to Table I we quickly see that if we remove all of the harmonics above the second that are present in a ramp the result will be the same as summing together a fundamental and its second harmonic. Granted, this is a specially chosen, simple example but the basic principle applies to any waveform.

Some people will read that last paragraph and disagree because of the phase differences that cause one waveform to look entirely different from another even though the harmonic contents are identical. The answer to that is that as far as the sound produced is concerned constant phase differences have no effect. As evidence of this we offer the fact that a sawtooth that ramps up as time goes on sounds the same as one that ramps down even though the phase differences between the harmonics are as great as any you'll find. We can further state that phase differences cannot be heard unless they are changing in which case they are perceived as an apparent frequency shift.

### Filters on the job

To use formant synthesis there must be some way of eliminating those unwanted harmonics and this is where our filters come in. Probably neither of the filter types we've built needs any explanation but briefly, the band-pass filter allows for attenuation of frequencies outside of a given frequency band while the frequencies

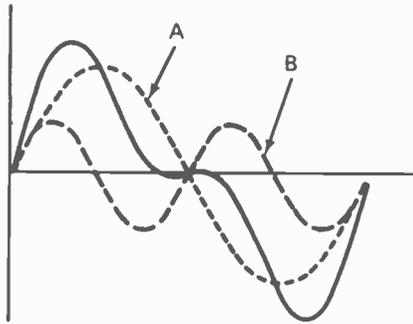


FIG. 7—SUMMING A FUNDAMENTAL with its half-amplitude second harmonic produces the waveform shown by the solid line.

TABLE I

harmonic \ wave	triangle	ramp	square
fundamental	$8/\pi^2$	$2/\pi$	$4/\pi$
2nd	--	$1/\pi$	--
3rd	$8/9\pi^2$	$2/3\pi$	$4/3\pi$
4th	--	$1/2\pi$	--
5th	$8/25\pi^2$	$2/5\pi$	$4/5\pi$
6th	--	$1/3\pi$	--
7th	$8/49\pi^2$	$2/7\pi$	$4/7\pi$
8th	--	$1/4\pi$	--
9th	$8/81\pi^2$	$2/9\pi$	$4/9\pi$

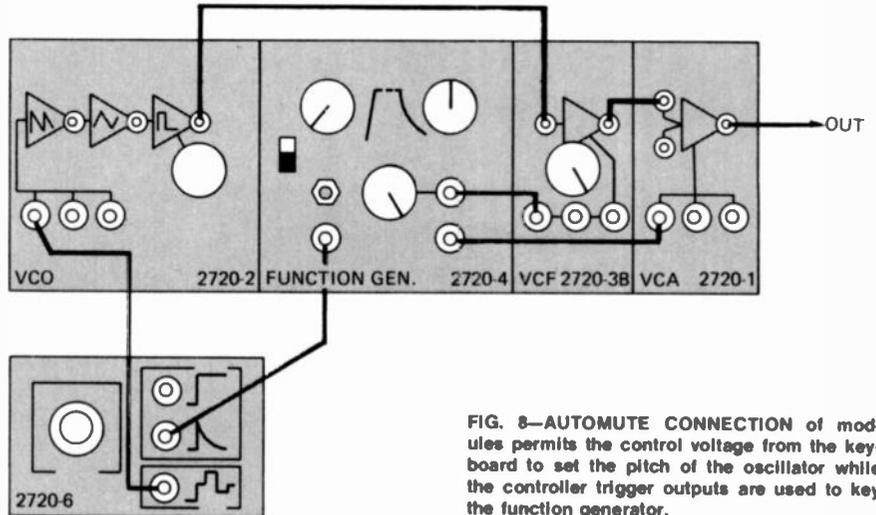


FIG. 8—AUTOMUTE CONNECTION of modules permits the control voltage from the keyboard to set the pitch of the oscillator while the controller trigger outputs are used to key the function generator.

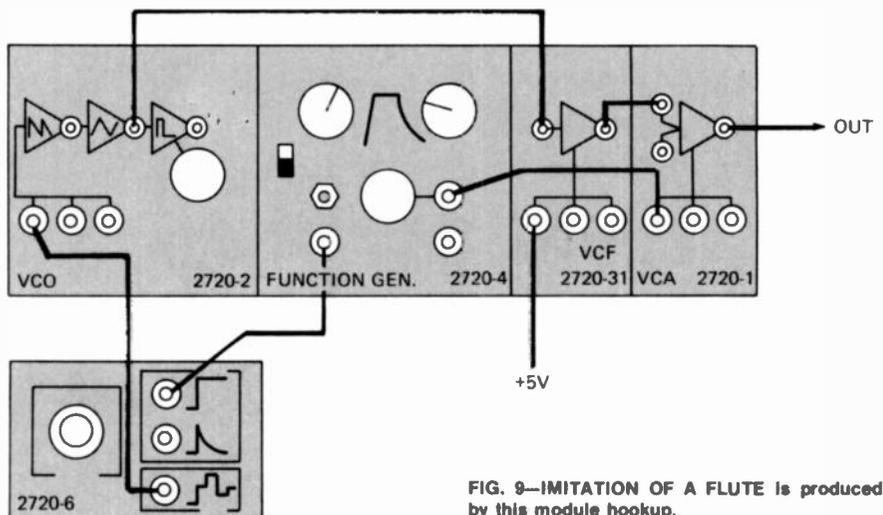


FIG. 9—IMITATION OF A FLUTE is produced by this module hookup.

within the band are passed without alteration. In our filter the "Q" (how well the filter does its job of attenuating out-of-band signals) is adjustable with a front panel control while the sum of the input control voltages determines the center frequency of the filter. Likewise, the low-pass filter attenuates all frequencies above the frequency of interest while allowing frequencies below that point to pass unaltered. In our low-pass filter increasing the control voltage simultaneously lowers the cut-off frequency and increases the rate at which higher frequencies are attenuated.

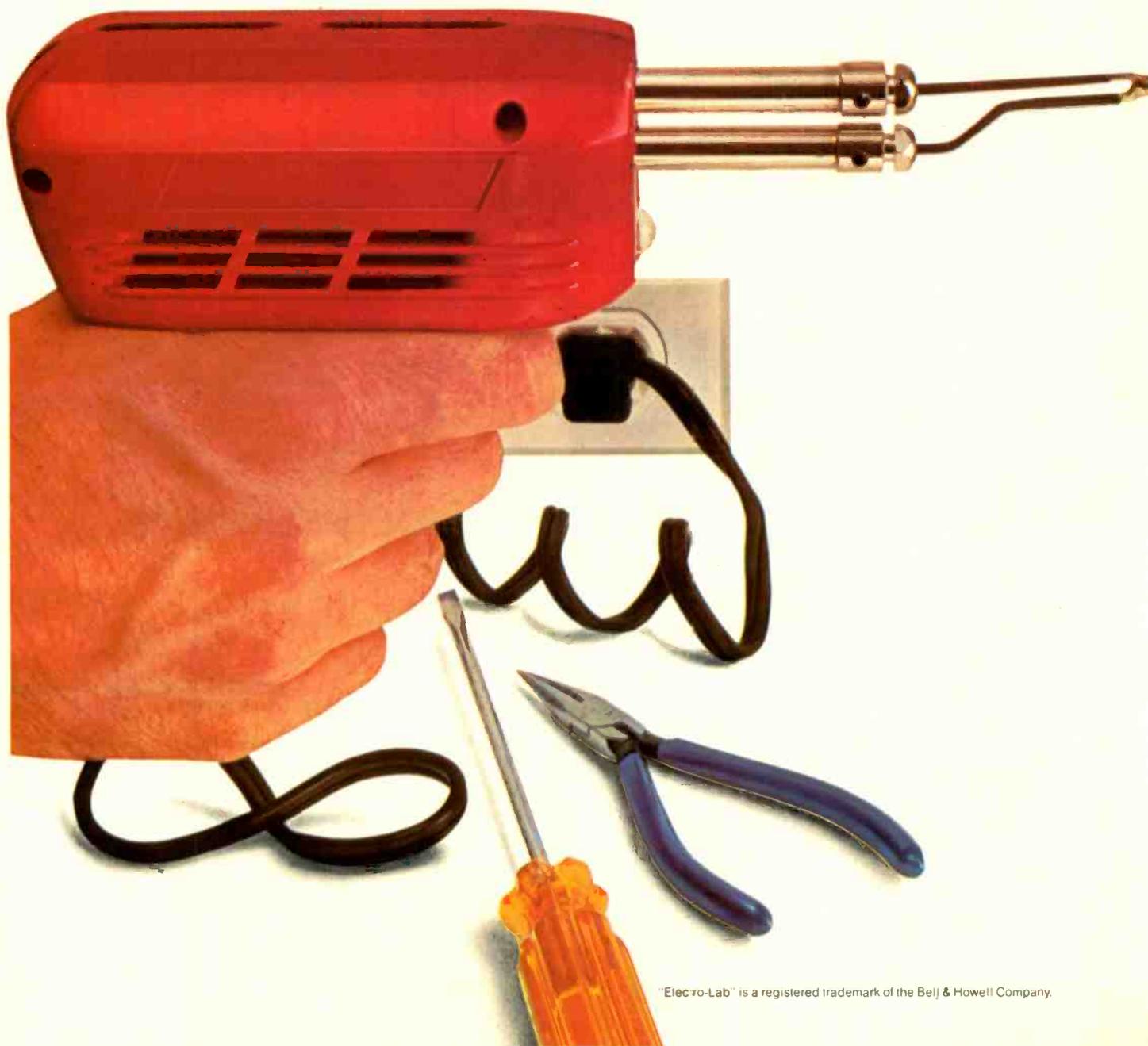
Due to space limitations we will leave the more subtle uses of the filters to the experimental discovery of the user and con-

centrate instead on some of the more spectacular effects that can be achieved. Fig. 8 shows a module arrangement that for lack of a better name we will call the "automute" connection. The arrangement is such that the control voltage from the keyboard sets the pitch of the oscillator while either of the controller trigger outputs (pulse works better than step) are used to key the function generator. As in the previous example the function generator output controls the VCA to provide appropriate attack and decay times. Unlike the previous example, however, the output of the VCO is routed through the band-pass filter before it passes through the VCA. The filter is also

(continued on page 88)

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# R-E's Service Clinic

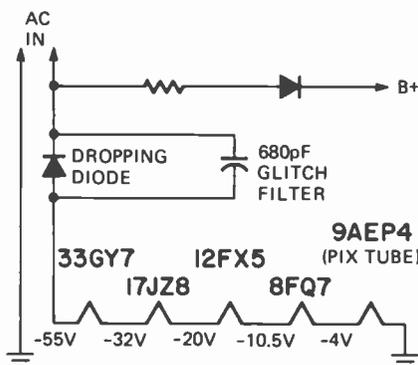
## A dropping diode— what is it?

*A diode is a cool substitute  
for a filament resistor*

**JACK DARR**  
SERVICE EDITOR

WHAT IN THE WORLD IS A "DROPPING diode"? Just what it says. A diode connected in series with the heater string of a hybrid TV set—the kind with four or five tubes, in the high-power stages. You might say it's a "heater rectifier", and in fact, it's marked FIL RECT in some Sams Photo-fact schematics. True, in a sense. Actually, it looks to me as if it's used to drop the ac line voltage to about half normal. One case of this is in RCA's KCS-176A portable chassis.

The use of these can lead to some confusion, and some funny voltage readings, if we're expecting them. The heater circuit is in the diagram. Here,



**THE DIODE RECTIFIES** half of the input sine-wave, reducing effective voltage to half.

we're not rectifying ac to get dc. in the regular sense; note that there aren't any filter capacitors on the load-side. What is happening here is that the rectifier is cutting off one half of each sine-wave. (Doesn't matter which half; happens to be the positive halves.) So, we get approximately "half-power." The *heating effect* of the current is reduced, referred to full-wave ac.

This gives us some unusual readings if we use our regular rms-reading ac voltmeters. Note the voltages shown along the heater string. The 33GY7 for example shows 55 volts on one side and 32 volts on the other; total (55-32) = 23 volts! Yet, the tube

works. Note that these voltages are read with a *dc voltmeter*; it shows -55 volts, etc. The normal ac drop across the heater string adds up to 76 volts, but we see only -55 volts at the input. The "heating-effect" of the half-wave rectified ac is enough to get the cathode up to the correct operating temperature.

We set up an experiment, using a 33GY7 tube, in a tube-tester, on an adapter. Setting the heater at the rated voltage we got the readings shown in the table. We used a standard vom, a

**TABLE OF MEASUREMENTS**  
33GY7 tube, in test adapter, in tube-tester. Heater set to 33 volts ac.

<b>METER</b>	Set on ac volts.
<b>VOM</b>	33V
<b>FETVOM</b>	33V
<b>DVM</b>	34.1V
<b>With diode in series, one side of heater.</b>	
<b>METER</b>	Set on ac volts
<b>VOM</b>	15V
<b>FETVOM</b>	18V
<b>DVM</b>	18.6V
<b>METER</b>	Set on dc volts.
<b>VOM</b>	15V
<b>FETVOM</b>	18V
<b>DVM</b>	14.88V

(Polarity of reading depends on how diode is connected; unimportant)

FET vom and a digital vom. On ac volts, the readings were correct. Then, one side of the heater was opened, and a standard silicon rectifier diode was connected in series. The heater voltage was not changed.

Now look at the readings! On ac volts, we get roughly half the applied voltage, which makes sense. Setting them on dc volts, we got about the same readings. (Oddly enough, the *emission* of the tube didn't seem to go down too much. Perhaps I didn't wait long enough for the cathode to cool down; tests took only about 3 minutes.)

(continued on page 71)

This column is for your service problems—TV, radio, audio or general and industrial electronics. We answer all questions individually by mail, free of charge, and the more interesting ones will be printed here.

If you're really stuck, write us. We'll do our best to help you. Don't forget to enclose a stamped, self-addressed envelope. Write: Service Editor, Radio-Electronics, 200 Park Ave. South, New York 10003.

# R-E's Transistor Substitution Guide

	ARCH	DM	G-E	ICC	IR	MAL	MOT	RCA	SPR	SYL	ZEN
2N1729	NA	NA	GE-53	NA	TR-05	PTC 102	HEP-629	SK 3005	RT-118	ECG 100	NA
2N1730	RS276-2002	T-641	GE-54	ICC-641	TR-08	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1731	RS276-2004	T-353	GE-53	ICC-253	TR-05	PTC 102	HEP-253	SK 3005	RT-118	ECG 100	ZEN 304
2N1732	RS276-2001	T-641	GE-54	ICC-641	TR-08	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1742	RS276-2003	T-3	GE-9	ICC-3	NA	PTC 102	HEP-3	NA	NA	ECG 160	ZEN 301
2N1743	RS276-2004	T-253	GE-9	ICC-253	TR-05	PTC 102	HEP-253	SK 3005	RT-118	ECG 100	ZEN 304
2N1744	RS276-2004	T-253	GE-9	ICC-253	TR-05	PTC 102	HEP-253	SK 3005	RT-118	ECG 100	ZEN 304
2N1745	RS276-2003	T-3	GE-51	ICC-3	TR-17	PTC 107	HEP-3	NA	NA	ECG 160	ZEN 301
2N1746	RS276-2003	T-3	GE-9	ICC-3	TR-17	PTC 107	HEP-3	SK 3006	NA	ECG 160	ZEN 301
2N1747	RS276-2003	T-3	GE-9	ICC-3	TR-17	PTC 107	HEP-3	SK 3006	NA	ECG 160	ZEN 301
2N1748	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3006	NA	ECG 160	ZEN 300
2N1749	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3006	NA	ECG 160	ZEN 300
2N1750	RS276-2003	T-3	GE-51	ICC-3	TR-17	PTC 107	HEP-3	SK 3007	NA	ECG 160	ZEN 301
2N1751	NA	NA	NA	NA	NA	NA	NA	NA	RT-147	ECG 179	NA
2N1752	NA	T-2	GE-51	ICC-2	NA	PTC 107	HEP-2	NA	NA	ECG 160	ZEN 300
2N1753	NA	T-2	GE-1	ICC-2	TR-17	PTC 109	HEP-2	NA	NA	ECG 160	ZEN 300
2N1754	NA	T-2	GE-9	ICC-2	NA	PTC 107	HEP-2	SK 3005	NA	ECG 160	ZEN 300
2N1755	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1756	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1757	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1758	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1759	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1760	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1761	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1762	NA	NA	GE-3	NA	NA	PTC 105	NA	SK 3009	RT-124	ECG 104	NA
2N1763	RS276-2009	T-53	GE-18	ICC-53	NA	PTC 123	HEP-53	SK 3124	RT-100	ECG 123	ZEN 102
2N1764	RS276-2009	T-50	GE-20	ICC-50	TR-22	PTC 136	HEP-50	SK 3024	RT-114	ECG 128	ZEN 100
2N1765	NA	NA	NA	NA	NA	NA	HEP-R1307	NA	NA	NA	NA
2N1768	NA	NA	GE-66	NA	NA	NA	HEP-S5003	NA	NA	NA	NA
2N1769	NA	NA	GE-66	NA	NA	NA	HEP-S5000	NA	NA	NA	NA
2N1770	NA	S-300	NA	ICC-300	NA	NA	HEP-R1241	NA	NA	NA	NA
2N1771	NA	S-300	NA	ICC-300	IR-1771	NA	HEP-R1241	NA	NA	NA	NA
2N1772	NA	S-302	NA	ICC-302	SCR-04	NA	HEP-R1243	NA	NA	ECG 122	NA
2N1773	NA	S-302	NA	ICC-302	SCR-04	NA	HEP-R1243	NA	NA	ECG 122	NA
2N1774	NA	S-302	NA	ICC-302	SCR-04	NA	HEP-R1243	NA	NA	ECG 122	NA
2N1775	NA	NA	NA	NA	NA	NA	HEP-R1306	NA	NA	NA	NA
2N1776	NA	NA	NA	NA	IR-1776	NA	HEP-R1306	NA	NA	NA	NA
2N1777	NA	NA	NA	NA	IR-1777	NA	HEP-R1307	NA	NA	NA	NA
2N1778	NA	NA	NA	NA	IR-1778	NA	NA	NA	NA	NA	NA
2N1779	RS276-2002	T-641	GE-6	ICC-641	TR-10	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1780	RS276-2002	T-641	GE-5	ICC-641	TR-10	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1781	RS276-2002	T-641	GE-5	ICC-641	TR-10	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1782	RS276-2003	T-3	GE-2	ICC-3	TR-17	PTC 109	HEP-3	SK 3005	NA	ECG 160	ZEN 301
2N1783	RS276-2003	T-641	GE-1	ICC-641	TR-10	PTC 109	HEP-641	SK 3005	RT-119	ECG 101	ZEN 315
2N1784	RS276-2003	T-3	GE-1	ICC-3	TR-17	PTC 107	HEP-3	SK 3005	NA	ECG 160	ZEN 301
2N1785	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3006	NA	ECG 160	ZEN 300
2N1786	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	S 3006	NA	ECG 160	ZEN 300
2N1787	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3006	NA	ECG 160	ZEN 300
2N1788	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3006	NA	ECG 160	ZEN 300
2N1789	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3006	NA	ECG 160	ZEN 300
2N1790	NA	T-2	GE-9	ICC-2	TR-17	NA	HEP-2	NA	NA	ECG 160	ZEN 300
2N1800	NA	NA	GE-53	NA	NA	NA	NA	NA	NA	NA	NA
2N1808	RS276-2001	T-641	GE-8	ICC-641	TR-08	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1837	NA	NA	GE-18	NA	TR-87	PTC 144	HEP-S3011	NA	NA	NA	NA
2N1838	RS276-2009	T-53	GE-63	ICC-53	IRTR-21	PTC 144	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1839	RS276-2009	T-53	GE-27	ICC-53	IRTR-78	PTC 144	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1840	RS276-2009	T-53	GE-27	ICC-53	IRTR-78	PTC 144	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1841	NA	NA	NA	NA	NA	NA	HEP-S3010	NA	NA	NA	NA
2N1842	NA	S-304	GEMR-3	ICC-304	NA	NA	HEP-R1301	SK 3505	NA	NA	NA
2N1843	NA	S-304	GEMR-3	ICC-304	IR-1843A	NA	HEP-R1301	SK 3505	NA	NA	NA
2N1844	NA	S-306	GEMR-3	ICC-306	IR-1844A	NA	HEP-R1304	SK 3505	NA	NA	NA
2N1845	NA	S-306	GEMR-3	ICC-306	NA	NA	HEP-R1304	SK 3505	NA	NA	NA
2N1846	NA	S-306	GEMR-3	ICC-306	IR-1846A	NA	HEP-R1304	SK 3505	NA	NA	NA
2N1847	NA	NA	GEMR-3	NA	NA	NA	HEP-R1306	SK 3505	NA	NA	NA
2N1848	NA	NA	GEMR-3	NA	IR-1848A	NA	HEP-R1306	SK 3505	NA	NA	NA
2N1849	NA	NA	GEMR-3	NA	IR-1849A	NA	HEP-R1307	SK 3505	NA	NA	NA
2N1850	NA	NA	NA	NA	IR-1850A	NA	NA	SK 3505	NA	NA	NA
2N1853	RS276-2004	T-253	GE-2	ICC-253	TR-05	PTC 102	HEP-253	SK 3005	RT-118	ECG 100	ZEN 304
2N1854	RS276-2004	T-253	GE-2	ICC-253	TR-05	PTC 102	HEP-253	SK 3004	RT-120	ECG 102	ZEN 304
2N1858	NA	NA	GE-20	NA	TR-08	PTC 108	NA	SK 3010	RT-122	ECG 103	NA
2N1864	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3008	NA	ECG 160	ZEN 300
2N1865	RS276-2003	T-3	GE-9	ICC-3	TR-17	PTC 107	HEP-3	SK 3008	NA	ECG 160	ZEN 301
2N1866	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3008	NA	ECG 160	ZEN 300
2N1867	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	SK 3008	NA	ECG 160	ZEN 300
2N1868	NA	T-2	GE-9	ICC-2	TR-17	PTC 107	HEP-2	NA	NA	ECG 160	ZEN 300

NA = NOT AVAILABLE

(turn page)

	ARCH	DM	G-E	ICC	IR	MAL	MOT	RCA	SPR	SYL	ZEN
2N1869	NA	NA	NA	NA	NA	NA	HEP-R1215	NA	NA	NA	NA
2N1870	NA	NA	NA	NA	NA	NA	HEP-R1215	NA	NA	NA	NA
2N1871	NA	NA	NA	NA	NA	PTC 107	HEP-R1216	NA	NA	NA	NA
2N1872	NA	NA	GE-50	NA	TR-17	PTC 107	HEP-R1217	NA	NA	NA	NA
2N1873	NA	NA	GE-50	NA	TR-17	PTC 107	HEP-R1218	NA	NA	NA	NA
2N1874	NA	NA	GE-50	NA	TR-17	PTC 107	HEP-R1218	NA	NA	NA	NA
2N1871	NA	NA	GE-50	NA	TR-17	PTC 107	NA	NA	NA	NA	NA
2N1881	NA	NA	NA	NA	NA	NA	HEP-R1101	NA	NA	NA	NA
2N1882	NA	NA	NA	NA	NA	NA	HEP-R1101	NA	NA	NA	NA
2N1883	NA	NA	NA	NA	NA	NA	HEP-R1102	NA	NA	NA	NA
2N1884	NA	NA	NA	NA	NA	NA	HEP-R1103	NA	NA	NA	NA
2N1885	NA	NA	NA	NA	NA	NA	HEP-R1103	NA	NA	NA	NA
2N1886	NA	NA	GE-66	NA	NA	NA	HEP-S5003	NA	NA	NA	NA
2N1889	NA	NA	GE-18	NA	NA	PTC 125	HEP-714	NA	NA	NA	NA
2N1890	NA	NA	GE-18	NA	NA	PTC 125	HEP-714	NA	NA	NA	NA
2N1891	RS276-2002	T-641	GE-5	ICC-641	TR-08	PTC 102	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1892	RS276-2002	T-641	GE-54	ICC-641	TR-08	PTC 108	HEP-641	SK 3011	RT-119	ECG 101	ZEN 315
2N1893	RS276-2009	T-714	GE-27	ICC-714	TR-87	PTC 125	HEP-714	SK 3024	RT-114	ECG 128	NA
2N1894	NA	NA	NA	NA	NA	NA	HEP-S5003	NA	NA	NA	NA
2N1895	NA	NA	NA	NA	NA	NA	HEP-S5003	NA	NA	NA	NA
2N1896	NA	NA	NA	NA	NA	NA	HEP-S5003	NA	NA	NA	NA
2N1897	NA	NA	NA	NA	NA	NA	HEP-S5000	NA	NA	NA	NA
2N1898	NA	NA	NA	NA	NA	NA	HEP-S5000	NA	NA	NA	NA
2N1905	RS276-2006	T-232	GE-16	ICC-232	IRTR-88	PTC 105	HEP-232	SK 3014	RT-115	ECG 129	ZEN 326
2N1906	NA	T-626	GE-25	ICC-626	TR-27	PTC 138	HEP-626	SK 3014	RT-147	ECG 179	NA
2N1907	RS276-2006	T-232	GE-25	ICC-232	TR-27	PTC 105	HEP-232	SK 3014	RT-147	ECG 179	ZEN 326
2N1908	RS276-2006	T-232	GE-25	ICC-232	TR-27	PTC 105	HEP-232	SK 3014	RT-147	ECG 179	ZEN 326
2N1917	RS276-2021	T-51	GE-22	ICC-51	TR-88	PTC-103	HEP-51	SK 3114	RT-115	ECG 159	ZEN 101
2N1918	RS276-2021	T-51	GE-22	ICC-51	TR-88	PTC 103	HEP-51	SK 3114	RT-115	ECG 159	ZEN 101
2N1919	RS276-2021	T-51	GE-21	ICC-51	TR-88	PTC 131	HEP-51	SK 3114	RT-115	ECG 159	ZEN 101
2N1920	RS276-2021	T-51	GE-21	ICC-51	TR-80	PTC 131	HEP-51	SK 3114	RT-115	ECG 159	ZEN 101
2N1921	RS276-2021	T-51	GE-21	ICC-51	TR-88	PTC 131	HEP-51	SK 3114	RT-115	ECG 159	ZEN 101
2N1922	NA	NA	GE-21	NA	IRTR-88	PTC 103	NA	NA	RT-115	ECG 129	NA
2N1924	RS276-2007	T-629	GE-2	ICC-629	IRTR-85	PTC 102	HEP-629	SK 3004	RT-121	ECG 102A	NA
2N1925	RS276-2005	T-254	GE-2	ICC-254	IRTR-85	PTC 135	HEP-254	SK 3004	RT-121	ECG 102A	ZEN 305
2N1926	RS276-2005	T-254	GE-2	ICC-254	IRTR-85	PTC 135	HEP-254	SK 3004	RT-121	ECG 102A	ZEN 305
2N1929	NA	SR-1241	NA	ICC-R1241	NA	NA	HEP-R1241	NA	NA	ECG 5400	NA
2N1930	NA	SR-1241	NA	ICC-R1241	NA	NA	HEP-R1241	NA	NA	NA	NA
2N1931	NA	SR-1243	NA	ICC-R1243	SCR-04	NA	HEP-R1243	NA	NA	ECG 122	NA
2N1932	NA	SR-1243	NA	ICC-R1243	SCR-04	NA	HEP-R1243	NA	NA	ECG 122	NA
2N1933	NA	SR-1243	NA	ICC-R1243	SCR-04	NA	HEP-R1243	NA	NA	ECG 122	NA
2N1934	NA	SR-1005	NA	NA	NA	NA	NA	NA	NA	NA	NA
2N1935	NA	SR-1005	NA	NA	NA	NA	NA	NA	NA	NA	NA
2N1936	NA	T-247	NA	NA	NA	NA	NA	NA	NA	NA	NA
2N1937	NA	T-247	NA	NA	NA	NA	NA	NA	NA	NA	NA
2N1940	NA	T-250	GE-2	NA	TR-05	PTC 102	NA	SK 3005	RT-118	ECG 100	NA
2N1941	NA	NA	NA	HEP-S3011	NA	NA	HEP-S3011	NA	NA	NA	NA
2N1942	NA	NA	NA	HEP-629	NA	NA	HEP-629	NA	NA	NA	NA
2N1943	NA	T-714	GE-18	HEP-S3020	TR-87	PTC 125	HEP-S3020	NA	NA	NA	NA
2N1944	RS276-2009	T-53	GE-63	ICC-53	TR-86	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1945	RS276-2009	T-53	GE-63	ICC-53	TR-86	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1946	RS276-2009	T-53	GE-63	ICC-53	TR-25	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1947	RS276-2009	T-53	GE-17	ICC-53	TR-87	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1948	RS276-2009	T-53	GE-17	ICC-53	TR-86	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1949	RS276-2009	T-53	GE-17	ICC-53	TR-25	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1950	RS276-2009	T-53	GE-17	ICC-53	TR-87	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1951	RS276-2009	T-53	GE-17	ICC-53	TR-86	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1952	RS276-2009	T-53	GE-17	ICC-53	TR-25	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1953	RS276-2009	T-53	GE-18	ICC-53	TR-65	PTC 125	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1954	RS276-2005	T-254	GE-2	ICC-254	NA	PTC 135	HEP-254	SK 3005	RT-121	ECG 102A	ZEN 305
2N1955	RS276-2005	T-254	GE-2	ICC-254	NA	PTC 135	HEP-254	SK 3005	RT-121	ECG 102A	ZEN 305
2N1956	RS276-2005	T-254	GE-2	ICC-254	NA	PTC 135	HEP-254	SK 3005	RT-121	ECG 102A	ZEN 305
2N1957	RS276-2005	T-254	GE-2	ICC-254	IRTR-85	PTC 135	HEP-254	SK 3005	RT-121	ECG 102A	ZEN 305
2N1958	RS276-2009	T-53	GE-63	ICC-53	TR-25	PTC 123	HEP-53	NA	RT-102	ECG 123A	ZEN 102
2N1959	RS276-2009	T-53	GE-63	ICC-53	TR-25	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1960	RS276-2003	T-3	GE-2	ICC-3	TR-17	PTC 102	HEP-3	SK 3123	NA	ECG 160	ZEN 301
2N1961	RS276-2003	T-3	GE-2	ICC-3	TR-17	PTC 102	HEP-3	SK 3123	NA	ECG 160	ZEN 301
2N1962	RS276-2009	T-50	GE-20	ICC-50	IRTR-51	PTC 123	HEP-50	SK 3122	RT-102	ECG 123A	ZEN 100
2N1963	RS276-2009	T-50	GE-20	ICC-50	IRTR-51	PTC 123	HEP-50	SK 3122	RT-102	ECG 123A	ZEN 100
2N1964	RS276-2009	T-50	GE-20	ICC-50	IRTR-51	PTC 123	HEP-50	SK 3122	RT-102	ECG 123A	ZEN 100
2N1965	RS276-2009	T-50	GE-20	ICC-50	IRTR-51	PTC 123	HEP-50	SK 3122	RT-102	ECG 123A	ZEN 100
2N1969	RS276-2005	T-254	GE-1	ICC-254	IRTR-85	PTC 135	HEP-254	NA	RT-121	ECG 102A	ZEN 305
2N1970	NA	T-233	GE-4	ICC-233	TR-03	PTC 106	HEP-233	SK 3012	NA	ECG 105	ZEN 327
2N1971	RS276-2006	T-232	GE-25	ICC-232	TR-01	PTC 105	HEP-232	SK 3009	RT-127	ECG 121	ZEN 326
2N1972	RS276-2009	T-53	GE-63	ICC-53	TR-21	PTC 123	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1973	RS276-2009	T-53	GE-18	ICC-53	TR-21	PTC 123	HEP-53	SK 3124	RT-102	ECG 123A	ZEN 102
2N1974	RS276-2009	T-53	GE-18	ICC-53	TR-21	PTC 125	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1975	RS276-2009	T-53	GE-18	ICC-53	TR-21	PTC 125	HEP-53	SK 3122	RT-102	ECG 123A	ZEN 102
2N1980	NA	T-231	GE-4	ICC-231/233	TR-03	PTC 106	HEP-231/233	SK 3012	NA	ECG 105	ZEN 327
2N1981	NA	T-231	GE-4	ICC-231/233	TR-03	PTC 106	HEP-231/233	SK 3012	NA	ECG 105	ZEN 327

NA = NOT AVAILABLE

(continued next month)

## substitution guide PART VIII

compiled by **ROBERT & ELIZABETH SCOTT**

- ARCH**—Indicates the Archer brand of semiconductors sold only by Radio Shack and Allied Radio stores. Allied Radio Shack, 2725 W. 7th St., Ft. Worth, Texas 76107
- DM**—D. M. Semiconductor Co., P.O. Box 131, Melrose, Mass. 02176
- GE**—General Electric Co., Tube Product Div., Owensboro, Ky. 42301
- ICC**—International Components, 10 Daniel Street, Farmingdale, N.Y. 11735
- IR**—International Rectifier, Semiconductor Div., 233 Kansas St., El Segundo, Calif. 90245
- MAL**—Mallory Distributor Products Co., 101 S. Parker, Indianapolis, Ind. 46201
- MOT**—Motorola Semiconductors, Box 2963, Phoenix, Ariz. 85036
- RCA**—RCA Electronic Components, Harrison, N.J. 07029
- SPR**—Sprague Products Co., 65 Marshall St., North Adams, Mass. 01247
- SYL**—Sylvania Electric Corp., 100 1st Ave., Waltham, Mass. 02154
- ZEN**—Zenith Sales Co., 5600 W. Jarvis Ave., Chicago, Ill. 60648

Radio-Electronics has done its utmost to insure that the listings in this directory are as accurate and reliable as possible; however, no responsibility is assumed by Radio-Electronics for its use. We have used the latest manufacturers material available to us and have asked each manufacturer covered in the listing to check its accuracy. Where we have been supplied with corrections, we have updated the listing to include them. The first part of this Guide appeared in March 1973.

## SERVICE CLINIC (continued from page 68)

This type of circuit can lead to some unexpected problems, if you don't know it's being used. In one, although the customer's complaint was "poor focus", the tubes suddenly started glowing very brightly, then the fusible resistor in the B+ supply popped out. Checks showed that the diode in the heater string had shorted. This applied the full 120-volt line voltage to the heaters.

The diode was replaced, and the B+ checked. A heavy short was still there. This turned out to be the audio tube, a 12FX5, with a big fat short. It's possible that the heater overload had caused this. Although the other tubes had been overloaded too, they weren't damaged. Note: this diode seems to be used *only* in the "A" series of the KCS-176 chassis. In later runs, higher-voltage tubes were used, and a small dropping resistor (15 ohms) was added.

In other sets, you'll find other things used as droppers. In fact, anything having either resistance or reactance can be used. Small chokes can be used, but these are much more expensive than diodes; so are big resis-

tors, nowadays. In some imported TV sets, a special non-polarized electrolytic capacitor was the dropping "resistor"! Needless to say, this was a very odd value, and practically impossible to get. We finally began replacing these with stock resistors, which worked beautifully.

If you run into a set with some kind of unusual dropper, and you can't find a replacement, good old-fashioned resistors will solve the problem. You can find the value needed with Ohm's Law. Don't forget to figure the wattage too. Some of these will get pretty warm. Most can be mounted in some place on the chassis where they'll stay cool enough.

Suspect the use of some odd thing whenever you see that the heater voltages of the tubes do not add up to the line voltage. As in the RCA mentioned, where they add up to only 76 volts. Here's how to get the right value; add up the heater voltages of all tubes in the string. Now, subtract this value from the line voltage at 120 volts. In the example above, this would be  $120 - 76 = 44$  volts drop, across the dropper. The current will be the same in all tubes, so you need only look up one type. Here, it's 450 mA. So, Mr. Ohm says that  $R = E/I$ , or 100 ohms. If you come out with an

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oddball resistance value, use the next higher stock value; this will give you a little "cushion" in case of line-surges, and the tubes will never know the difference. You can run them at least 5% below rating, with full output.

The dropping resistor must have an ample wattage rating. Here, we'd have  $P = I^2R$ , or  $.45^2$  times 100; comes out around 20 watts. Use a 25-watt type, for safety-factor. You can mount this on a couple of small metal brackets, so that it will be held away from the chassis, for best air-circulation.

So, there you are. With good ol' fundamentals, and some scratch paper,

it's not too hard to cope with some of the more unusual things you run into. Just keep your eyes (and your mind) open. **R-E**

## reader questions

**REGULATED SUPPLY LOW**  
*The 20-volt regulated supply on a Sylvania D-12 color chassis reads only 10 volts. I have no raster or sound.*

**Higher dc voltages OK.—T.D., Bellevue, Ohio**

One of two things: either you have a high leakage or short in some of the many circuits fed by that 20-volt source, or the regulator transistor itself is bad.

Check: disconnect the output of the 20-volt supply. Turn the set on. If this reads exactly 20 volts, it's OK. If it reads 10 volts no-load, try a new regulator transistor. Should hold the dc output constant at 20 volts, with line voltage all the way from 105 to 120 volts.

Loss of video and raster could be due to low supply voltage on the first and second video amplifier transistors, biasing the pix tube off

### INTERMITTENT CONVERGENCE

*We've got an odd case of intermittent convergence in a Magnavox 938. The customer complains bitterly, but we had an awful time making it show up in the shop. When we did, it looked like a sudden displacement of the three colors, by about 1/8 inch each.—T.D., Bellevue, Ohio.*

Check the Molex plug on the convergence yoke for intermittent contacts or loose wires to the male pins. Possibility 2, check the 50- $\mu$ F electrolytic in the vertical output tube

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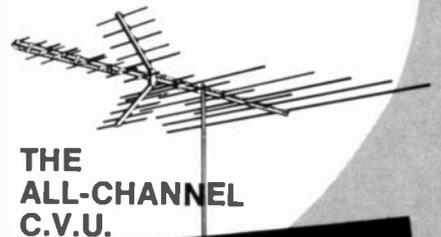
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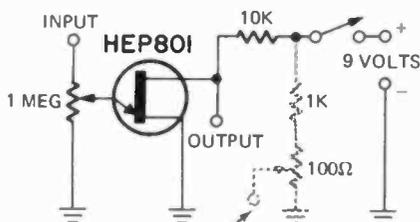
Circle 19 on reader service card

cathode circuit. If it is opening intermittently, it can cause some strange and wonderful symptoms. While you're at it, hit the diode unit on the convergence board a couple of smart raps with a screwdriver. These can "loosen up" and cause just this type of trouble. If it's loose, replace it.

### REDUCE FULL-SCALE READING OF VTVM?

*I've got an old, but good vtvm, with a 5-volt full-scale as the lowest range. Do you know how I could modify this to get something like a 0.5 or 1.0-volt full-scale?—A.K. Elmhurst, Ill.*

Frankly, no. This uses a standard vtvm bridge circuit. In these, the maximum voltage for full-scale deflec-



OPTIONAL CIRCUIT TO OBTAIN OUTPUT DOWN TO ZERO, USE THIS TERMINAL AS THE "GROUND" POINT FOR THE OUTPUT. (ADJUST POTENTIOMETER TO GIVE ZERO OUTPUT WITH INPUT GROUNDED)

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tion is applied to the "hot grid" of the dual-triode, through the multiplier resistors. In your instrument, the lowest voltage seems to be 5 volts, since there are no resistors in circuit on that scale. (In other words, no matter what voltage range you're on, you get 5 volts on the grid of the tube for full-scale; the multiplier does this.)

I don't think you could modify this without a complete redesign. However, you might build up a little "preamp", with the circuit for a "dc amplifier" (see diagram) that comes from Motorola's HMA-33 Fet folder! This could be used ahead of the vtvm for a lower range. Adjust its gain so

that you get a 5V. output for say 0.5V input, and away you go.

### POOR HORIZONTAL SYNC

*I've checked and replaced every part in the horizontal asc in this RCA KCS-144—diodes, capacitors, resistors, etc. Still won't work. It will hold pretty well, until anything disturbs it; change of camera, commercial, etc, then out it goes. I'm at my wit's end.—R.S.G., Provo, Utah.*

Last resort, on this type of problem. If it will hold fairly well, or hold at all, apparently without any sync, the oscillator is working, and the asc (continued on page 78)



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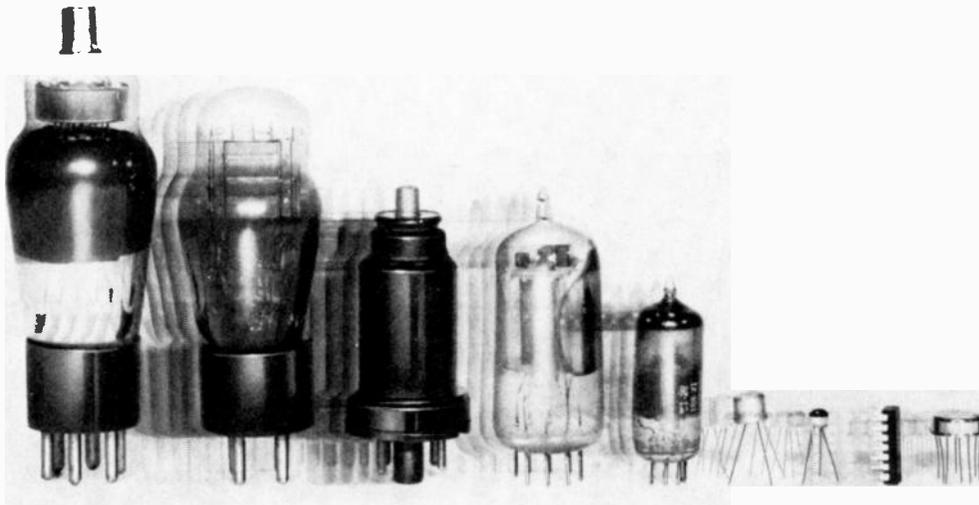
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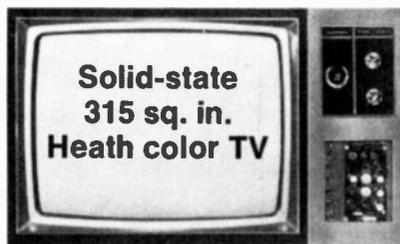
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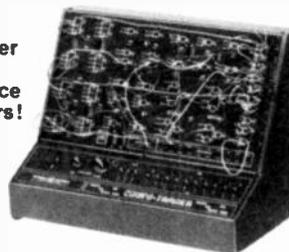
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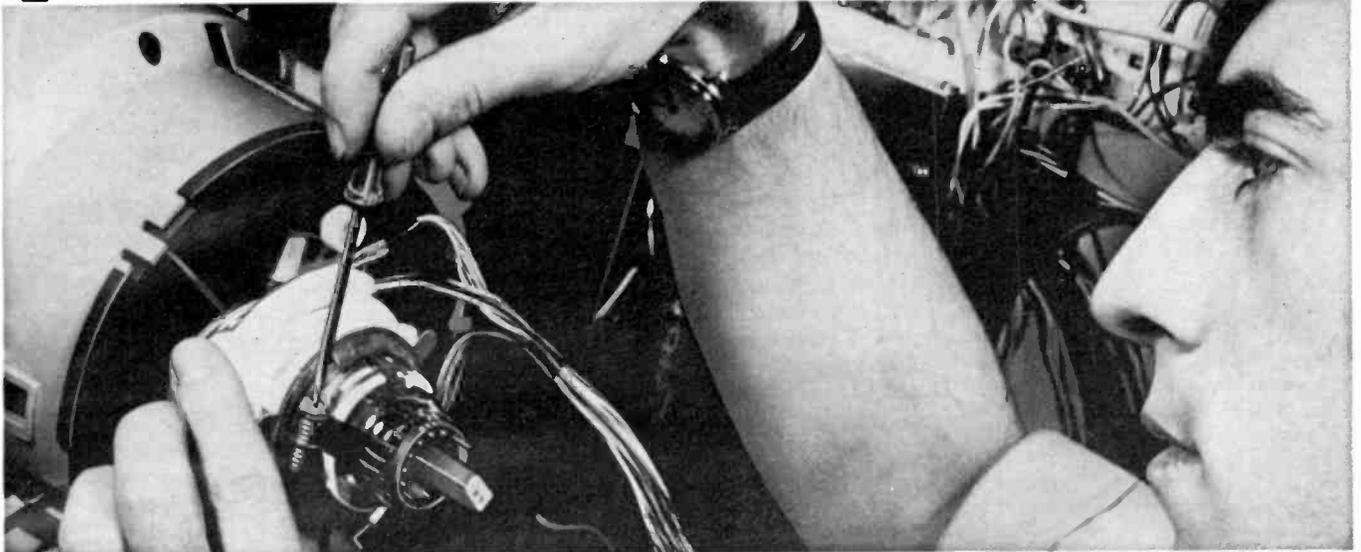
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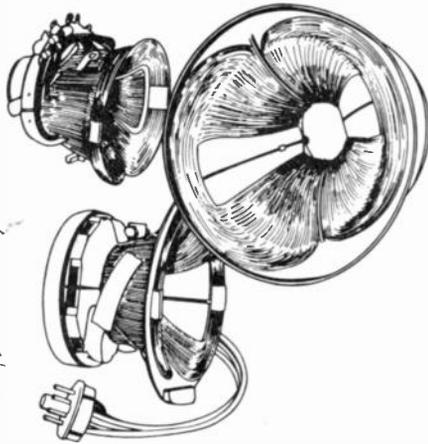
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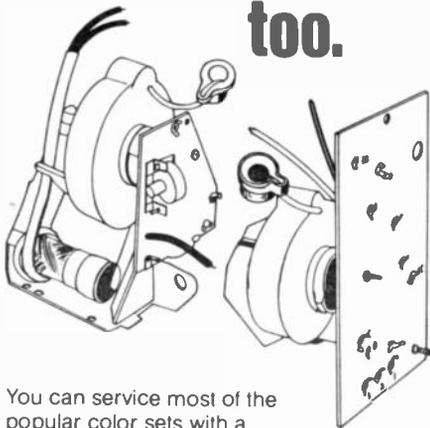
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Litton Distributor Services

## READER QUESTIONS

(continued from page 73)

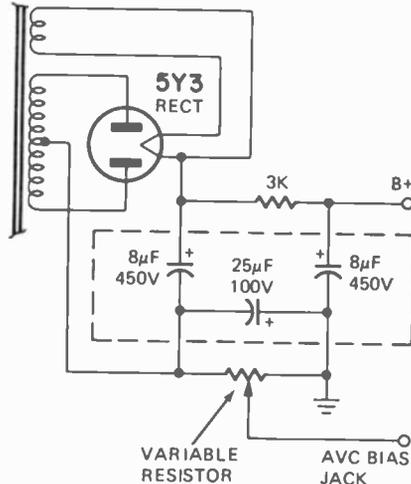
circuit itself is probably OK. One thing that has caused exactly this problem, in this and many others, is broken PC-board conductors. These will be in the conductors which feed the horizontal sync from the sync-separator into the afc. I found one with a 1/4-inch break in it, where a screwdriver had slipped at some time in the past. (Under a metal brace, so I couldn't see it, naturally.) Check all of these with an ohmmeter.

## FILTER CAPACITORS

*My old Precision E-200 signal generator has a shorted filter capacitor. I can't find the value of these on the can, and I don't have a service manual. What are they?—J.P., Louisville, Ky.*

The main filters in this generator are 8- $\mu$ F at 450 volts. There is also a 25- $\mu$ F at 100 volts in the same can. Watch out for the connections on any replacements. There are actually four terminals: see the diagram.

PART OF  
POWER TRANS



You'll probably be better off using three separate capacitors; you might have a hard time finding a single unit type with this exact hookup.

## BURNED OUT FLYBACK

*The flyback has burnt out in this Admiral 4G13 color chassis. There are two horizontal output tubes, in parallel. I'd like to protect the new flyback against tube-shorts. No fuses used, that I can see. How would I do this?—C.G., Mountain Top, Pa.*

Open the cathodes, tie them together, and add about a 3/4A fast-blow fuse to ground. Don't use slow-blow fuses; they have enough resistance to cause degeneration. Beside that, you want that circuit to open as quickly as possible if anything happens! R-E



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**RECORD REVIEWS**

*(continued from page 43)*

- CQ-32114**—Johnny Mathis, Me And Mrs. Jones \*\*
- MQ-32132**—Bartok, Concerto For Orchestra—Boulez And The New York Philharmonic Orchestra. Surround Sound \*\*\*\*
- CQ-32149**—Liza Minnelli, The Singer \*\*
- MQ-32196**—Haydn, Mass In Time Of War—Bernstein And Orchestra With Soloists, Recorded At Washington National Cathedral \*\*\*

**PROJECT THREE**

- PR-5067QD (QS encoded)**—The Brass Ring Featuring Phil Bodner \*\*\*
- PR-5068QD (SQ encoded)**—4-Channel Dynamite \*\*\*\*
- PR-5068QD (QS encoded)**—4-Channel Dynamite \*\*\*\*

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- EQ-30209**—Poco Deliverin' \*\*\*\*
- EQ-30325**—Sly & The Family Stone Greatest Hits \*\*
- EQ-30472**—Chase \*\*\*
- EQ-30658**—Tammy Wynette, We Can Sure Love Each Other \*\*
- EQ-31584**—They Only Come Out At Night, The Edgar Winter Group \*\*\*

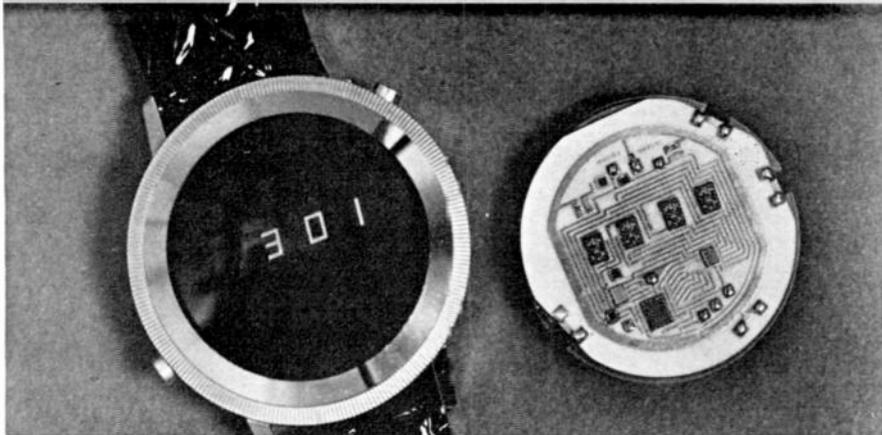
**OVATION**

- OVQD/14-27**—Laura, Comin' Apart \*\*

**VANGUARD**

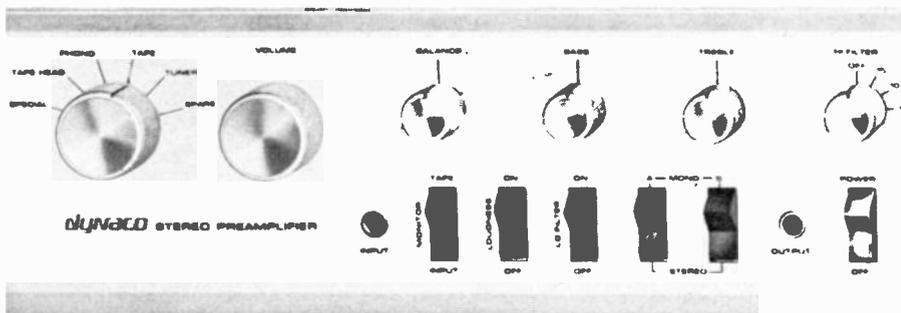
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- VSQ-30021**—Stravinsky, Petrushka, Mackerras And London Symphony Orchestra. Surround Sound \*\*\*\*
- VSQ-30025/7**—Rossini, La Pietra Del Paragone (Opera Buffa)—Jenkins And Clarion Concerts Orchestra, Chorus And Soloists \*\*\*\*
- VSQ-30008/9**—Mahler, Third Symphony—Abravanel And Utah Symphony Orchestra (Fifth Movement is especially effective) \*\*\*\*
- VSQ-30013/4/5**—Handl, Judas Macabaeus \*\*\*\*
- VSQ-30020**—Handl, Royal Fireworks Music, The Water Music \*\*\*

That's our list, complete as of now. As we receive and listen to more new 4-channel records, we'll report on them too. We think you'll find this report useful and would appreciate comments. R-E



**MICROELECTRONICS MAKE WATCHES RUN** accurate to 3 minutes per year. Using quartz crystal and a CMOS (complementary metal oxide semiconductor) chip, the accuracy is five times that of the "tuning fork" watch. The module, one eighth inch square, is made by Hughes Aircraft Co. for watch manufacturers, and contains the equivalent of 1,500 transistors. Other IC's drive the displays. With average use, the watch will run a year on a single change of batteries.

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# new products

More information on new products is available from the manufacturers of items identified by a Reader Service number. Use the Reader Service Card inside the back cover.

**TOOL CASE**, model TC-200ST contains assortment of screwdrivers, nutdrivers, pliers, cutters, stripper/cutter, etc., all mounted in see-thru plastic pockets on a removable pallet of heavy-gauge vinyl located in the lid of the case. Bottom of case is empty to allow ample space for individualized selection of additional

tools, test instruments, parts boxes, soldering gun, etc. Lid contains a full-width pocket for literature, manuals or other printed matter. Case alone, without tools, is available as model TC-200/MT. 18" x 13½" x 4¾".—Xcelite Inc., Orchard Park, N.Y. 14127.

Circle 31 on reader service card

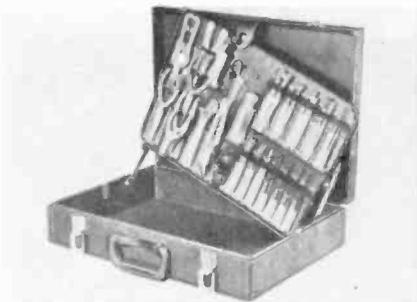
**HI-FI RECEIVER**, SA-8000X is an FM/AM 4-channel/2-channel receiver with a built-in CD-4 demodulator plus matrix

circuitry for direct demodulating or decoding 4-channel source material without external accessories. Includes 64 watts of total continuous rms power, all 4-channels driven at 8 ohms in the 4-channel mode; 84 watts total continuous rms power, both channels driven at 8 ohms in the 2-channel mode. Total IHF power is 160 watts.

Can accommodate all auxiliary 4-channel sources, including discrete 4-channel tape equipment, reel-to-reel and cartridge. Has separate level control for each channel, 4-channel/2-channel speaker outputs and multiple tape-monitor and dubbing facilities. \$499.95.—Technics by Panasonic, 200 Park Avenue, New York, N.Y. 10017.

Circle 32 on reader service card

**VOM MULTITESTER**, model VM-100K features ±1% temperature stabilized carbon film resistors. Long mirrored scale to eliminate parallax in reading. Polarity changeover switch; 23 ranges. Dc volts; 7 ranges, from 0-0.6, 3, 12, 60, 300, 600,



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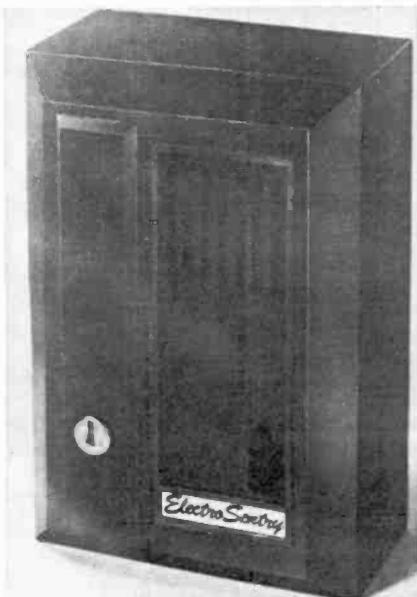


1,200. Ac volts; 5 ranges, from 0-6, 30, 120, 300, 1,200. Dc current; 6 ranges, 0-12  $\mu$ A, 300  $\mu$ A, 6 mA, 60 mA, 600 mA, 12 A. Ac current; 0-12 A. Ohms; 4 ranges, 0-20 K, 200 K, 2 meg, 20 meg. Db; 6 ranges, -20 to +17, 31, 43, 51, 63. Sensitivity: 100,000 ohms/volt dc, 10,000 ohms/volt ac. Accuracy:  $\pm 3\%$  dc,  $\pm 4\%$  ac (of full scale). 180 x 135 x 65 mm; 2 lbs., 4 oz.; \$65.95.—**Finney Company**, 34 West Interstate, Bedford, Ohio 44146.

Circle 33 on reader service card

**SECURITY SYSTEMS.** *Ultrasonic-Sentry*, model 30-9030, detects anyone within 25 feet. Needs no installation. Features a delayed-action electronic timing circuit, automatic shutoff, adjustable sensitivity control and comes complete with power supply/battery charger to extend battery life.

*Electro-Sentry*, model 30-9020, pro-



TECTS any door or window against intrusion. Features built-in electronic timer and a piercing 100-dB horn that sounds until silenced with a special key. Battery operated.

*Magna-Sentry*, model 30-9010, is a versatile alarm that is installed by self-adhesive backing. Battery operated unit has built-in fire alarm that sounds any time temperature reaches 135°F—even when burglar alarm is turned off. All models are do-it-yourself and solid-

state.—**GC Electronics**, Div. of Hydro-metals, Inc., 400 South Wyman Street, Rockford, Ill.

Circle 34 on reader service card

**AUTOMOBILE SPEAKER SYSTEMS** feature instant-mount, hardware-less installation, air-suspension cones, high-temperature voice coils and aluminum tweeters. May be used indoors as well as outdoors—for patio, poolside, camper and boat. Prices range from \$14.95 for a pair of 5" speakers in black and chrome-trimmed, recess-mount enclosures to \$39.95 for top-of-the-line model SA1000, a 30-watt rms, 2-way stereo sys-



tem that uses 4" x 6" air-suspension woofers, 2 1/4" supertweeters and cross-over networks in black leather-finished and chrome-trimmed enclosures.—**Ampere Electronic Corp.**, 230 Duffy Avenue, Hicksville, N.Y. 11802.

Circle 35 on reader service card

**HF SWEEP GENERATOR**, PM5334. Frequency range from 3 MHz to 860 MHz in eight panel-selected sweep ranges. Settling accuracy is better than 1%. Sweep frequency is continuously adjustable from 8 to 50 Hz on any band. Fixed frequency markers at 5.5, 10.7 and 38.9 MHz—each with 0.1% stability. Variable frequency marker is also available.

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Circle 36 on reader service card

**SSB & AM MOBILE CB TRANSCEIVER**, *Spartan SSB* has selectivity of  $\pm 3.5$  KHz at 6 dB and sensitivity of 0.4  $\mu$ V for 10 dB S/N. Up front controls include PA/CB

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Circle 26 on reader service card

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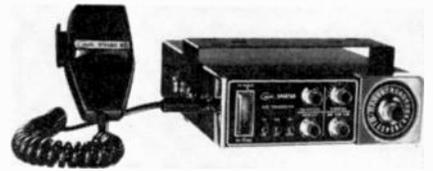
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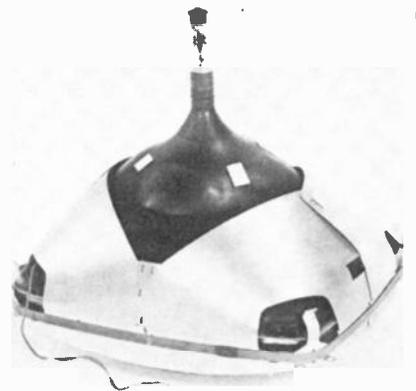


switch, noise blanker, local/distance RF control and AM/upper sideband/lower sideband selector switch. Features illuminated channel indicator and S/RF and power indicator. Has  $\pm 600$  Hz clarifier.

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Circle 37 on reader service card

COLOR PICTURE TUBES, *Speed Fit* are fitted with pre-assembled and pre-mounted straps and hardware. These units replace tubes in Motorola chassis 908, 914 and 914A; all RCA 25" (23v) chassis; and nine Zenith chassis from 20" to 25". CRT's for Zenith chassis



have a premounted one-piece shield, built-in degaussing coil, premounted pads for repositioning the yoke and pre-assembled strap and corner brackets.—Channel Master, Ellenville, New York.

Circle 38 on reader service card

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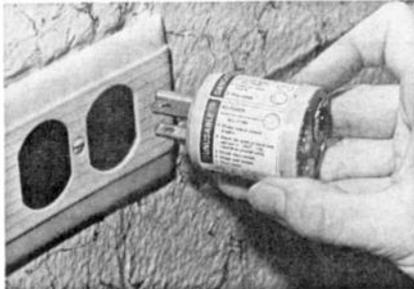
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Circle 39 on reader service card

**GROUNDING OUTLET TESTER, GT-20** checks for faulty wiring circuits. Simply plug the tester into any wall outlet and observe the indicator lights. Amber lights



show presence or absence of power. Reverse polarity, faulty connections or missing grounds are immediately evident. \$6.95.—Alco Electronic Products Inc., 1551 Osgood Street, North Andover, Mass. 01845.

Circle 40 on reader service card

**STEREO MODULATION/FREQUENCY MONITOR, TBM2200A.** In addition to simultaneous metering of left and right channel modulation, this model features continuous monitoring of the 19-KHz pilot frequency deviation. The modulation meters also measure channel separation, crosstalk, 38 KHz suppression and individual channel stereo signal-to-noise ratios. Internal calibration of pilot injection level and frequency is featured as well as full remote metering plug-in options and rear access to all critical circuits



that appear on individual plug-in cards. 7" rack height; \$1,350.00.—McMartin Industries, Inc., 605 North 13th Street, Omaha, Neb. 68102.

Circle 41 on reader service card

**SPEAKER SYSTEM KITS. CK10-2** is a two-way system. 6 1/2" woofer and 2" tweeter. Response 35 to 18,000 Hz. Maximum power input 20 W, 8 ohms. 13"H x 8"W x 8"D; 12 lbs.; \$34.95 each, \$59.95 pair. **Model CK20-2** is a two-way system. 8" woofer and 2 1/4" tweeter. Response 40 to 20,000 Hz. Maximum power input 60 W, 8 ohms. 20"H x 10 1/4"W x 9 1/2"D; 22 lbs.; \$59.95 each, \$99.95 pair. **Model CK20-3** is a three-way system. 8" woofer, 5" mid-range and 2 1/4" tweeter.

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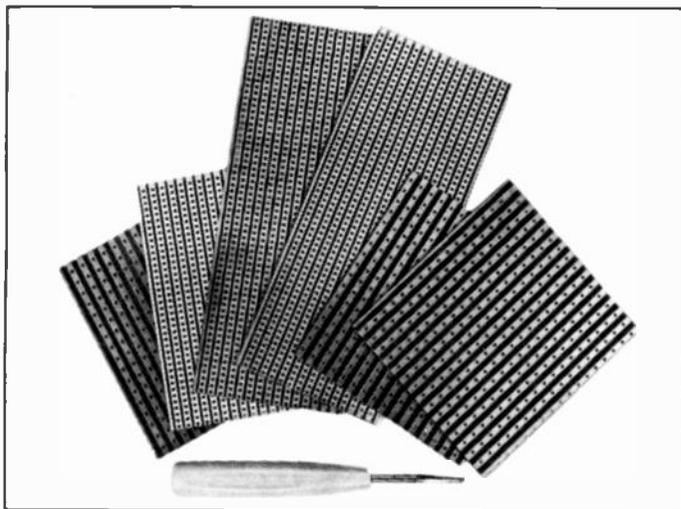
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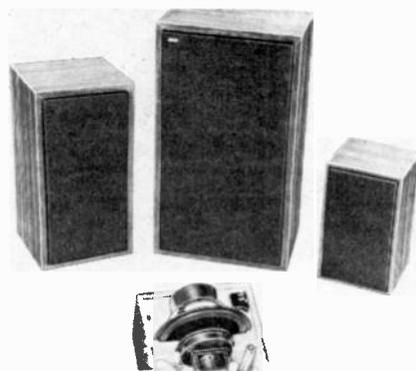
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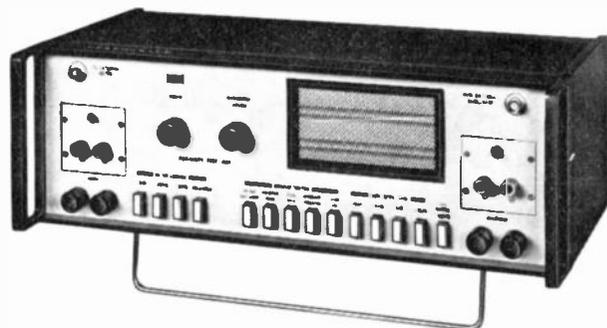
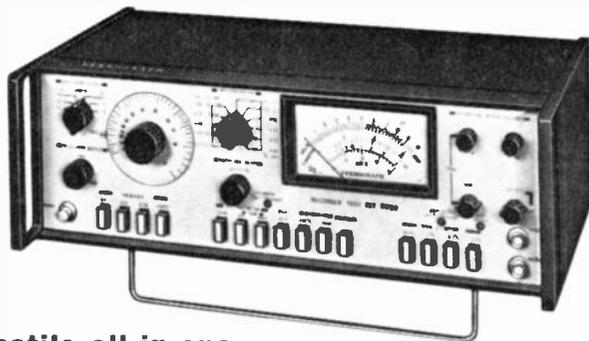
Response 40 to 20,000 Hz. Maximum power input ohms. 20"H x 10 1/4"W x 9 1/2"D; 23 lbs.; \$69.95 each, \$119.95 pair. Model CK50-4 is a four-way system. 10" woofer, 5" x 7" mid-range and two 2 1/2" tweeters. Response 30 to 18,000 Hz. Maximum power input ohms. 26 1/2"H x 15"W x 10 1/2"D; 30 lbs.; \$99.95 each, \$179.95 pair.—National Tel Tronics, 98 Cutter Mill Road, Great Neck, N.Y. 11021.

*Circle 42 on reader service card*

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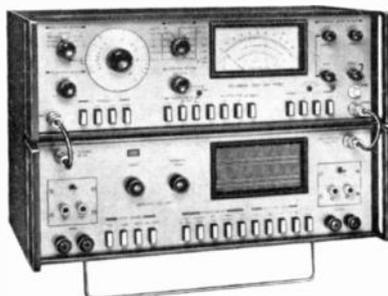


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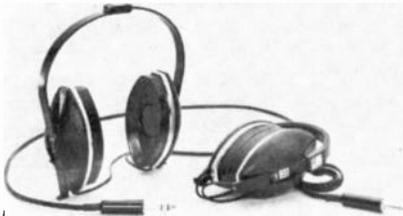
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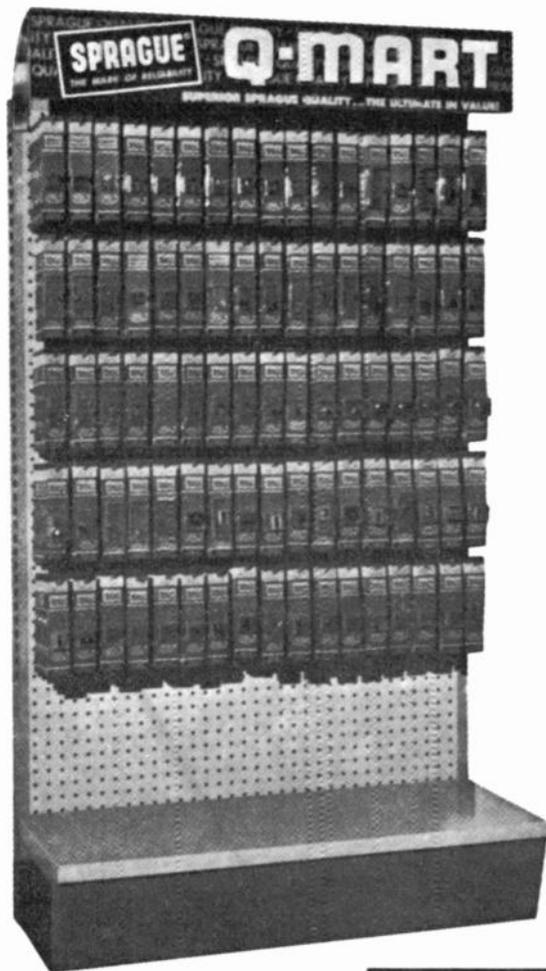
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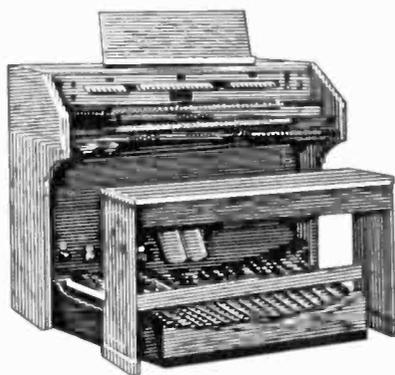


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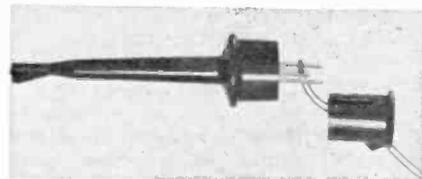
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Circle 63 on reader service card

cord; 9 oz.; \$29.95.—Koss Corp., 4129 North Port Washington Avenue, Milwaukee, Wisc. 53212.

Circle 44 on reader service card

MINI TEST CLIPS, model 3925 permits user to assemble his own test leads for specific testing requirements. Will accept any wire up to .090" in diameter. Features a plunger-action contact hook that connects with and holds component leads or terminals without damage. Spe-



cially constructed probe tip slips down over a .025 square Wire-Wrap pin to make positive connection.—Pomona Electronics Co. Inc., 1500 East Ninth Street, Pomona, Calif. 91766.

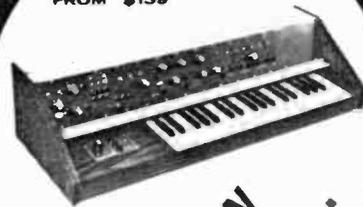
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PTS Electronics, Inc. has announced three more service centers. They are at: P.O. Box 5794, 5111 University Avenue, San Diego, Calif. 92105, phone (714)-280-7070; 5682 State Road, Cleveland, Ohio 44134, phone (216)-845-4480; and P.O. Box 16855, 1921 South 70th Street, Philadelphia, Pa. 19142, phone (215)-724-0999.

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**ELECTRONIC PARTS 1973 Annual Catalog** presents AM and AM/FM radios, tape recorders, speaker systems, turntables, stereo amplifiers and receivers, headsets, rf connectors, silicon-controlled rectifiers and diodes and semiconductors, relays, power supplies, wire cords and cable, transformers, fuses and holders, capacitors, switches, sockets and security equipment. Also included is a section on test equipment and tools and service aids.—**Electronic Distributors Inc.**, 4900 North Elston Avenue, Chicago, Ill. 60630.

Circle 46 on reader service card

**PARTS CATALOG 16-page** booklet includes silicon rectifiers, circuit breakers, antenna replacements, soldering iron, service kits and sets, hi-fi speakers, microphones, diamond needles, solid-state tubes and TV tuner subber. An order form is included.—**Fordham Radio Supply Co.**, 558 Morris Avenue, Bronx, N.Y. 10451.

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**SOLDER SELECTOR GUIDE** is a 6-page booklet that describes and illustrates soldering problems and the company's full line of solders, fluxes and chemicals. Problems include: icicling, bridging, dewetting and excess solder. Products include: 5-core solders of standard and special alloys and gauges, rosin base, organic acid and inorganic acid fluxes, cleaning solutions, solder creams and tapes and conformal coatings.—**Multicore Solders**, Westbury, N.Y. 11590.

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Write direct to the manufacturers for information on items listed below:

**SERVICING QUASAR COLOR TV** is a 15-page booklet of suggestions to help cut troubleshooting time and present procedures for those sets where the solution is not readily apparent and the problem has not been solved by logical analysis-replacement of panels. Information is arranged according to symptom and by chassis number. Categories included are: audio, high voltage, brightness, raster, Insta-Matic, sync, signal path/picture, sweep, power supply, remote control sets only, and service adjustments. \$1.00, from local Motorola distributors.

**ANTENNA PRODUCTS, catalog CP-2.** 24 pages illustrate and describe more than 230 products that include TV and FM antennas, preamplifiers, couplers, band separators and wire.—**Winogard Company**, 3000 Kirkwood Street, Burlington, Iowa 52601. R-E

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- Selecting & Improving Your Hi-Fi Syst. 224 p Pictorial Guide to Tape Recorder Repairs. 256 pps., 320 illus. \$4.95
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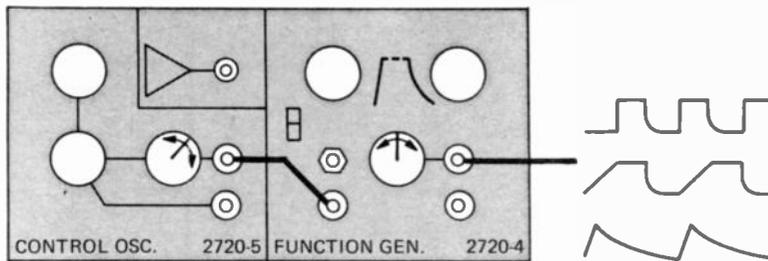


FIG. 10—FOR A LOW-FREQUENCY REPEATING WAVEFORM for percussion repeat effects, use this wiring arrangement. The sinewave output of the control oscillator can't do the job by itself.

under the control of the function generator. A pulse waveform of minimum duration has been chosen as the signal source in this example because of the evenly balanced, harmonic rich spectrum.

When any note is played with the above connection the function generator attacks rapidly and causes the VCF (voltage-controlled filter) to be resonant at some high frequency. During the decay portion of the note the center frequency of the filter slowly slides down through the frequency spectrum of the VCO's output pulses. The result is something like a performer muting a harmonic with his cupped hands but since the spike is a better source of harmonics than the predominantly square wave output of a harmonica and the filter is a more effective resonator than cupped hands the effect is quite naturally more spectacular.

A more standard sound can be achieved by increasing the pulse duration and backing off on pulse filter's Q control. You might also try using the function generator's output attenuator to lower the control voltage to the filter thereby lowering the upper limit of the resonant frequency. Also try summing a constant voltage from the power supply's bias sources into the control inputs of the VCF.

In Fig. 9 we have a simple arrangement that gives a convincing imitation of a flute. The connections are straight-forward; controller to VCO, step trigger to function generator, function generator to VCA. The triangle VCO output goes through the low-pass filter and then to the VCA for envelope shaping. In this example the filter is simply turned on by one of the bias supplies on our power supply module so that it attenuates the higher frequency content of the triangle. In its fully "on" condition the filter rolls off at the rate of about 12 dB/octave and since there is no second harmonic in a triangle and the third harmonic is already 19 dB down from the fundamental there is a total attenuation of the third harmonic of 43 dB. The output of the low pass filter is for all practical purposes a sine wave, the classic flute-like voice. Attack and decay times are adjusted to correspond to those typical of a flute.

#### Control oscillator/noise source

There is one remaining module that we've treated as an orphan child so far, the Control Oscillator/Noise source. This module is peculiar to the R-E synthesizer because in most other equipment the VCO is flexible enough to be used at very low frequencies. Our cost objectives were best met with a separate low-frequency oscillator. Among the effects produced using a low-frequency control voltage source are vibrato—a slow, rhythmic pitch variation—and tremolo, a slow variation in amplitude. These effects are produced by using the output of the control oscillator as one of the control-voltage sources for the VCO and VCA respectively.

There are times when you need a low-frequency repeating waveform with a shape other than a sine wave. For example, percussion repeat effects similar to staccato banjo picking require that the VCA be driven by a waveform such as the one shown in Fig. 10. The sine wave output of the control oscillator won't hack it by itself but it can be used as a repeating trigger

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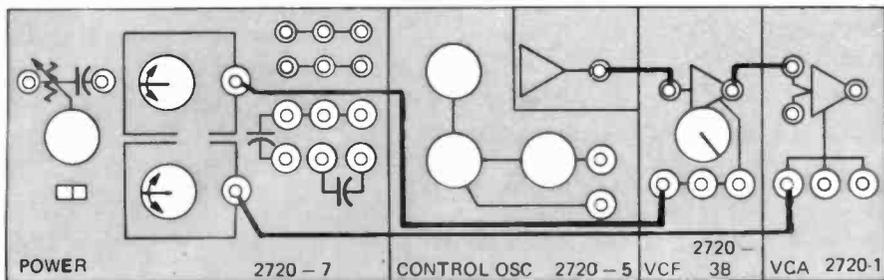


FIG. 11—NOISE IS USEFUL IN MUSIC SYNTHESIS. This hook-up generates wind sounds.

source for the function generator as shown. With this arrangement the attack and decay controls of the function generator control the attack and decay of the final output while the sustain is a function of the point on the sine wave at which the generator triggers and consequently of the settings of the control oscillator's output attenuator.

When Harry Oslon first started work on the old RCA Mark I and Mark II synthesizers back in the 1040's he was pioneering in a number of areas and not the least of these was the first use of noise in an electronic musical instrument. Up until that time the Ondiolines, Martinots, Theremins, etc. had without exception used only pitched sound sources. Because of that they produce less than natural sounds.

There are a number of stock phrases that accurately describe noise, phrases like "white noise is an equal probability distribution of all frequencies" or "pink noise is a Gaussian frequency distribution". While these are answers that display great crudi-

tion on the part of the explainer they don't do a lot for the 'splainee. Simply put, if you tune an FM radio to a spot between stations what you hear is noise in the tech-

nical sense. If you then play with the tone controls you are "coloring" the noise.

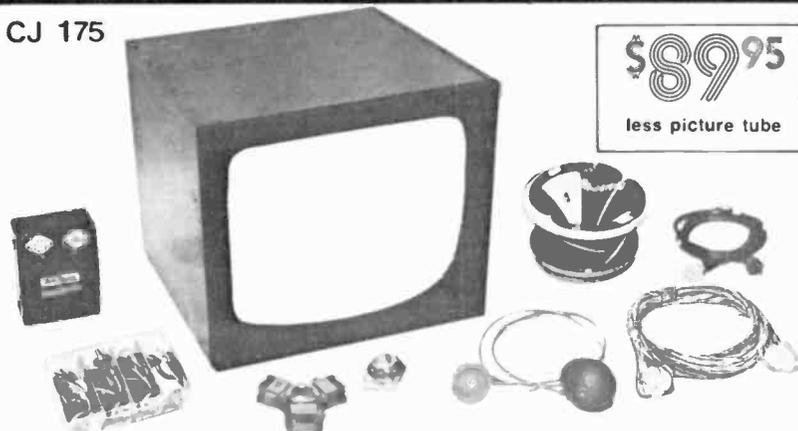
### Noise as sound

It's easy to see why the first artisans of electronic music missed the significance of noise. As you listen to it on the radio it doesn't appear to be the sort of thing that would be musically useful. But to illustrate it's use Fig. 11 shows an arrangement for producing the sound of the wind.

In other words, try everything. We've done a fair job of covering the basics involved but you have at your disposal a complete synthesis system. A few hours constructive play with the machinery will teach you more than a hundred written pages. **R-E**

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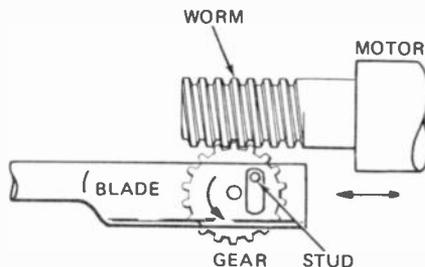
## APPLIANCE CLINIC

(continued from page 24)

lights to a fairly good brightness, the charger can supply normal current. Most of these are trickle chargers, at about 150 to 200 mA maximum.

If the charger is dead, check its line cord; it could be broken at the point where it goes into the housing. Some of these go inside the housing and connect to the rectifier unit with flexible leads. If the ac voltage is present, but no dc output, replace the charging unit. This is literally a Black Box, sealed so you can't get into it.

The gear-boxes are about as simple as you can get. Most of them have only a worm cut into the end of the motor shaft, which drives a gear, usually made of plastic so that it will take the wear. This gear has two small studs, one on each side. These slip into slots in the ends of the knife blades, as shown below. This causes



WORM GEAR CONVERTS rotary motion to reciprocating. One blade shown; other on other side of gear.

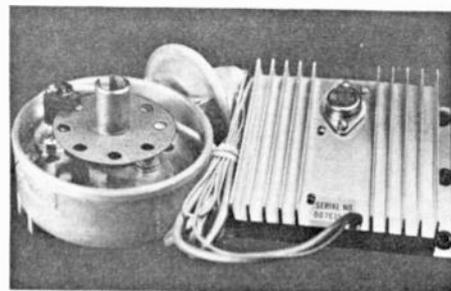
the reciprocating motion of the blades. Replacement gears are available, and easy to install. If one blade moves but the other doesn't, one of the studs is broken off.

The gear box is usually just a cavity molded in one half of the case. A thin metal cover holds the grease inside. If you find grease-leaks, check for missing screws in the cover, or a broken gasket. In emergencies, you can cut new gaskets out of paper or even plastic.

The blade-mountings and slides are usually made out of nylon or Teflon, or something like that. They are not lubricated. Make sure that they can slide freely. The blades are specially ground, and are normally "self-sharpening" as they rub against each other. If they need sharpening, take them apart, and find the flat side. Use a very smooth oil-stone, fine-grained, and hold the blade with the flat side perfectly flat on the stone. Only a few strokes back and forth on the stone will bring back the cutting edge. Most of them are serrated for easier cutting. Do not try to sharpen from the serrated side. That's a job for the manufacturer or a pro.

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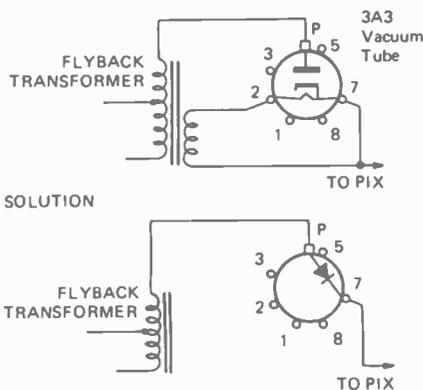
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When the filament winding on the flyback transformer arcs, there is no need to replace the winding or the transformer. Simply remove the filament leads from the set and replace the vacuum-tube rectifier with a solid-state equivalent such as the R-3A3, R-3AT2 and R-DB3 Solid-Tubes by Electronic Devices, Inc.



Do not cut the leads to the picture tube. Completely remove the winding from the transformer core and clean the socket and plate cap. The solder joint on the socket pin to the picture tube should be smooth with no points so that arcing across the unused pins is avoided. Greater protection can be had by putting a drop of RTV silicone rubber such as DOW or GE Silicone Tube Sealer on the connection.—*News From EDI*

## MAGNAVOX T979

An intermittent bright horizontal line that moves vertically through the bottom third of the screen may be accompanied by vertical jitter. In some cases, the condition appears to be corrected by tapping or moving certain components on the "D" panel. This may be caused by a contaminate, such as solder flux, in the "D" panel plug-in socket at pins 5, 6 and 7.

If you encounter this condition, clean both male pins on the chassis and female connectors on the "D" panel with an approved cleaner, such as General Cement's Chloro-Kleen or Dry-Kleen, that will not react with the PC board or adjacent components. The female connector should be cleaned using an applicator such as a

toothpick, and then thoroughly dried.—*Magnavox Service News Letter*

## MAGNAVOX T936/956/957

Snivets on the left side of the screen on uhf channels may be caused by a leaky diode D102. This diode is

located in the horizontal output section and is in series with the center arm of the high-voltage adjustment control. Replace with diode part No. 530088-1004.—*Magnavox Service News* **R-E**

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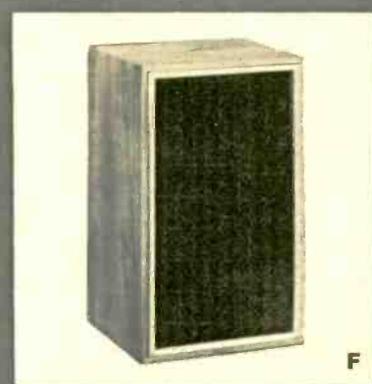
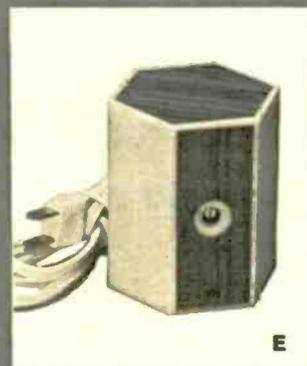
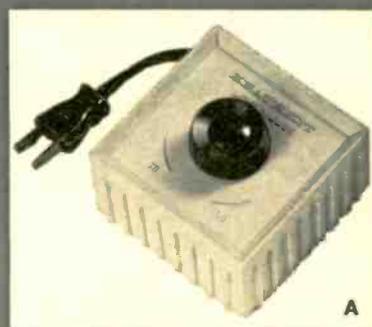
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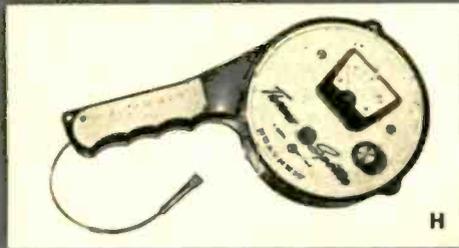
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**C. Heathkit Electronic Metronome** — provides professional accuracy in tempos from 40 to 200 beats per minute. Has adjustable volume control and includes chart relating tempos in time signatures to beats per minute. Uses two 9-volt batteries (not supplied).  
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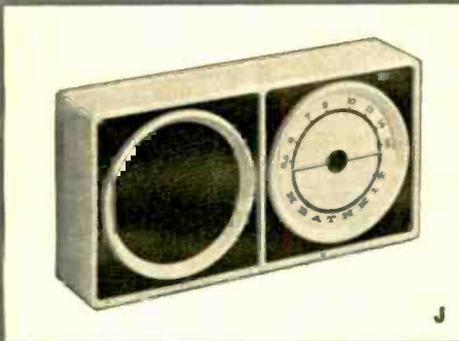
**G. Heathkit Code Practice Oscillator** — great for beginning and novice amateur radio operators. Has tone and volume controls, built-in speaker, headphone jack, blinker light. Includes key, phone plug, cord. Uses two 9-volt and one "C" battery (not supplied).  
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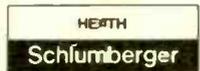
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## VIDEOPLAYER PROGRESS

Video discs and tape systems for the home continue to be glamorous babies of the future in electronics. RCA has lifted the curtain just a little on its plans for its Selecta-Vision videocassette player-recorder. Pilot production will start late this year, but the first units probably won't be on the retail market until early 1975, RCA says. RCA still plans to price the recorder-player attachment with built-in TV tuner at \$795. An optional monochrome TV camera will be \$300, and blank recording cartridges will be available in 15-, 30- and 60-minute lengths, costing a maximum of \$30. RCA will offer a catalog of 100 recorded tapes at the start, available primarily through rental. A feature film will rent for about \$10.

MCA Disco-Vision, which demonstrated its laser-scanned video disc for the first time last December, presented a "progress report" demonstration which showed

sharply improved pictures and longer playing time. Featured was a 12-inch record which provided 18 minutes of color programming, as compared with seven minutes in the earlier demonstration. The goal is a 40-minute video LP, to go on the market in 1975.

Cassette Sciences also demonstrated a videoplayer—this one designed to play back Super-8 film through home TV sets and to interact with a home computer terminal. Production of the player and the terminal, each costing about \$500, is slated to begin late this year or early next. Among the uses cited for the unit are programmed visual instruction and games in which the viewer can compete with the computer. The computer alone, without the videoplayer, can help with such household tasks as checkbook-balancing and homework, will be available to homes at one dollar per hour of actual use. **R-E**

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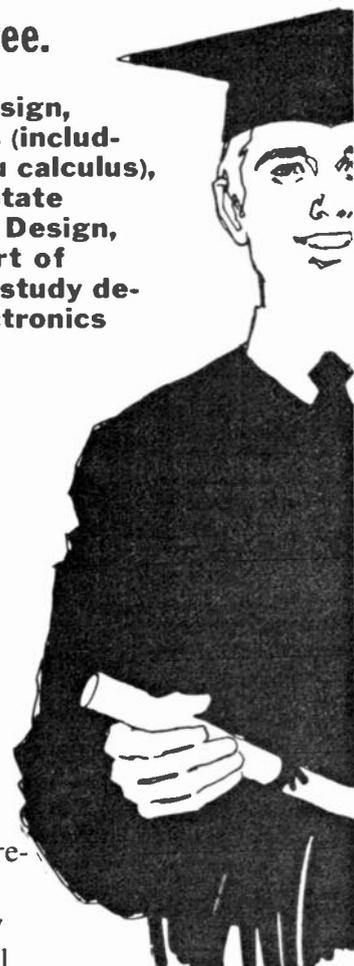
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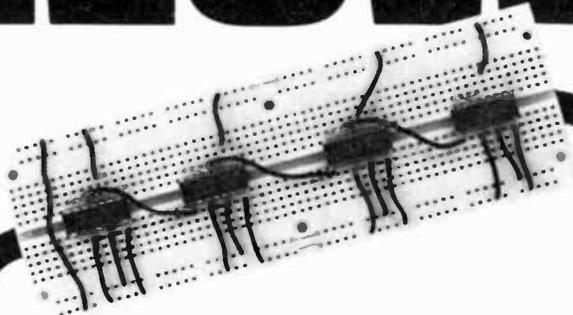
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## 4-CHANNEL FM

(continued from page 42)

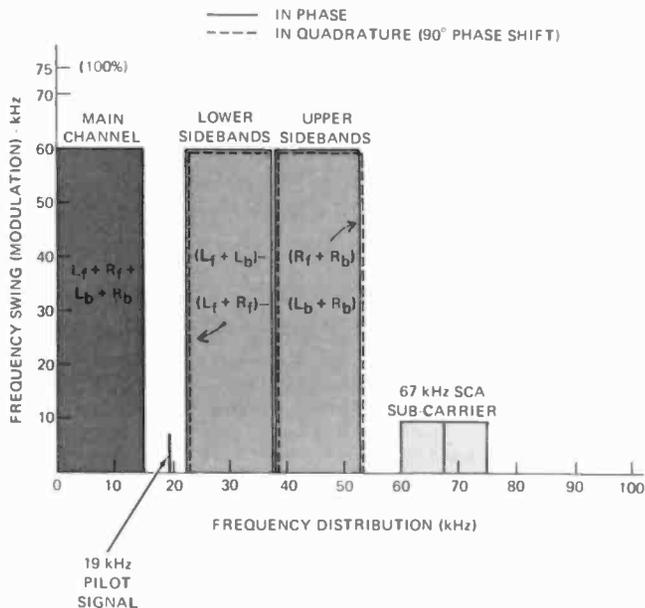


FIG. 6—RCA'S "3 SIGNAL" SYSTEM requires no increased bandwidth, but does not provide total separation between all four channels. SCA remains at 67 kHz.

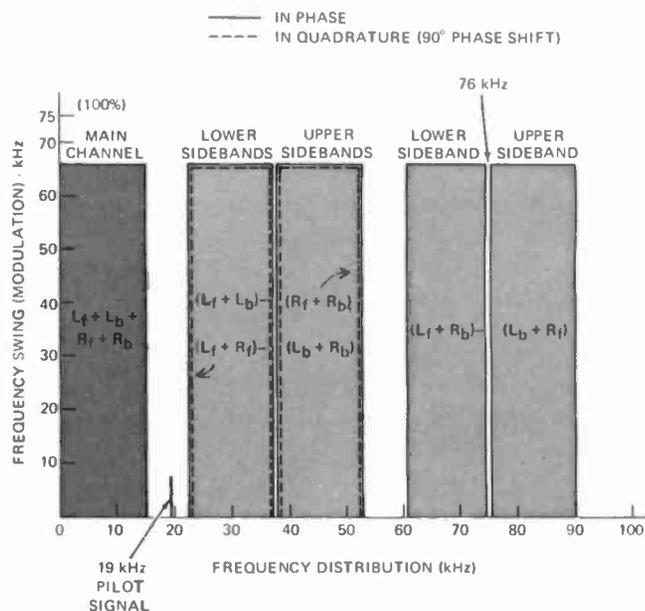


FIG. 7—IN RCA'S ALTERNATE SYSTEM, SCA service is not used. Second subcarrier upper and lower sidebands are transmitted and modulation levels can be somewhat greater.

knowing that a station is broadcasting a matrix disc, unless an announcer indicates that fact.

CBS feels that it would be nice if some sort of indicator light could be activated on a home receiver every time a matrix disc was played. Towards that end, they have proposed that while no major changes need be approved by the FCC for continued transmission of SQ programs, the present unmodulated 19-kHz signal be amplitude modulated by a frequency of 593.75 Hz and that this modulation cause the peak amplitude of the pilot signal to vary by a maximum of 10%.

Since present rules regarding pilot amplitude permit a range from 8% to 10% of total modulation anyway, such amplitude modulation of the pilot signal would not fall

(continued on page 100)

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5" - 900'	.80	8-Track - 84 Min.	1.29
5" - 1200'	.97	8-Track - 80 Min.	1.59
5" - 1800'	1.49	8-Track - Cleaner	1.49
7" - 1200'	.77		
7" - 1800'	1.12	3" TAPE REEL	.08
7" - 2400'	1.79	3 1/4" TAPE REEL	.07
7" - 3600'	2.95	5" TAPE REEL	.14
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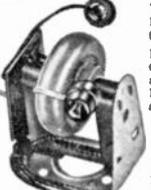


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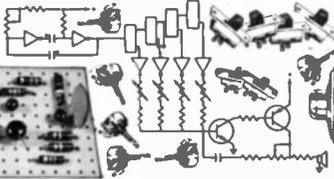
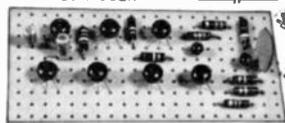
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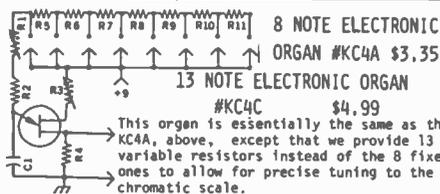
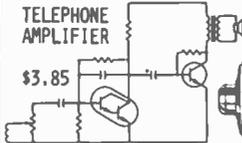


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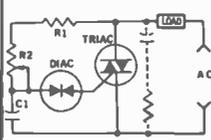
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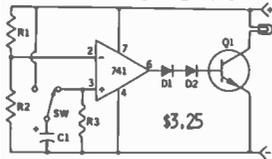
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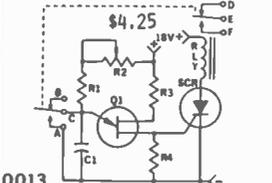
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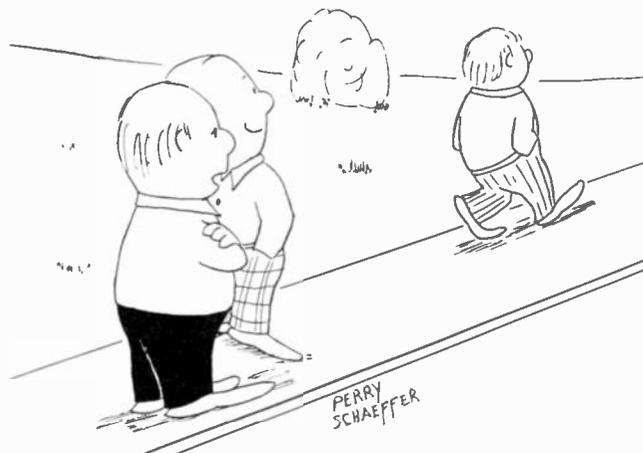
(continued from page 98)

outside these tolerances, and the 593.75 Hz could be detected at the receiver and used to trigger a light or some other indicator every time "matrixed" material were played. In case you're wondering why they chose 593.75 Hz for this modulating frequency—it's because it happens to be the 32nd sub-harmonic of 19 kHz—which was obvious as soon as it was explained!

### Tests, timetables and other considerations

At the present time, it would appear that field testing of all of the proposed systems will take place in early 1974—most likely over the facilities of FM station KIOI in San Francisco. Much analytical work remains to be done by the NQRC before that time, and even after the comprehensive field tests are completed, conclusions will have to be reached, data submitted to the FCC, and formal requests for new rule-making will have to be made. If past history is any criterion, the FCC will examine this work very carefully before reaching a decision. Compared to a monophonic broadcast, stereo FM offers approximately 23 dB poorer signal to noise ratios. In strong-signal areas, this has been relatively unimportant, but at greater distances from the transmitter this degradation of S/N often makes stereo listening unacceptable in areas where mono reception is quite satisfactory.

All of the new quadraphonic broadcast proposals, with the exception of CBS (which really involves no new changes) and the RCA three-channel proposal will introduce still further degradation in signal-to-noise ratios. The calculated figures (compared to a monophonic reference) range from 26.2 dB to 30.8 dB, depending upon which system is used. That means a further decrease in signal-to-noise ratio ranging from 3.2 dB to 7.8 dB which can prove to be quite significant. The FCC will not be satisfied with calculated adjacent and co-channel interference figures, but will want to insure proper protection ratios based upon present frequency allocations to FM stations around the country. In short, the job of selecting and approving new standards for quadraphonic FM broadcasting is a complex one—and one not likely to be finished for the next couple of years. While the presence of a new "four-channel decoder jack" on the back panels of some of the latest tuners and receivers seems like a good act of consumer protection, it does not guarantee that the system ultimately chosen will necessarily lend itself to "adapter" packages implied by the presence of this extra jack. While we're waiting, we can all enjoy good stereo FM as well as "matrix" four-channel broadcasts right now. **R-E**



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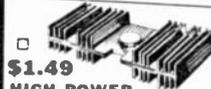
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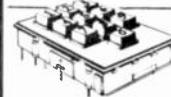
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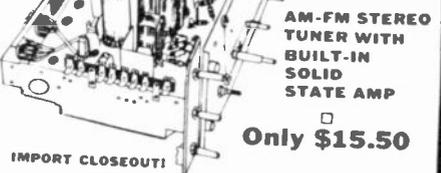
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THE SECOND GENERATION LITE-PIPE REPLACEMENT FOR MAN-1, DL10, ETC. 14PIN DIP—MAN-1 PINOUT

MAN-1 7-SEGMENT DISPLAY - THE REAL THING	\$3.95
MAN-1A LATER, IMPROVED VERSION	\$4.95

MONSANTO MAN-3M	\$2.95
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### XD-7 7-SEGMENT MINIATURE LED DISPLAY

WITHOUT DECIMAL PT. \$2.25 WITH DECIMAL PT. \$2.50

MONSANTO MAN-2 7 BY 5 LED ARRAY	\$8.50
ASCII ALPHANUMERIC CIRCUITRY INCLUDED	
LARGE RED LED .35	THREE FOR \$1.00

7400	7401	7402	7403	7404	7405	7410	
7420	7430	7440	7450	7453	7454	7460	\$ .30
7441	\$1.35	7475	\$ .90	7495	\$ .99		
7442	\$1.20	7476	\$ .65	7496	\$1.25		
7447	\$1.50	7483	\$1.25	74107	\$ .55		
7448	\$1.25	7486	\$ .55	74153	\$1.50		
7472	\$ .40	7490	\$ .99	74154	\$2.00		
7473	\$ .55	7492	\$ .99	74192	\$1.75		
7474	\$ .55	7493	\$ .99	74193	\$1.75		

### LOW POWER TTL ONE TENTH THE CURRENT

74L00	74L02	74L03	74L30	74L51	74L55	\$4.40
74L72	74L73	74L74	\$ .75	74L90	74L93	\$2.00

### NATIONAL "DM" SERIES

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NE 567	TUNE DECODER	\$2.95

74C00	74C04	74C10	\$ .60
74C05	74C76	\$1.25	74C162, 74C163 \$2.75

### DIGITAL CLOCK CHIP 6 DIGIT • 7 SEG. OUTPUT—SINGLE POWER SUPPLY! WITH DATA \$11.95

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Circle 84 on reader service card

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7401N ....32¢.... 28¢	7473N ....52¢.... 45¢
7402N ....32¢.... 28¢	7474N ....52¢.... 45¢
7403N ....32¢.... 28¢	7475N...\$1.00.... 85¢
7404N ....35¢.... 31¢	7476N ....60¢.... 55¢
7410N ....32¢.... 28¢	7487N ....60¢.... 55¢
7420N ....32¢.... 28¢	7490N...\$1.00.... 85¢
7430N ....32¢.... 28¢	7492N...\$1.00.... 85¢
7440N ....32¢.... 28¢	7493N...\$1.00.... 85¢
7441N...\$1.75...\$1.45	7495N...\$1.30...\$1.15
7442N...\$1.35...\$1.15	74107N ..55¢.... 50¢
7447N...\$1.30...\$1.10	74121N ..70¢.... 60¢

\*MIXED TTL PRICES

### LINEAR INTEGRATED CIRCUITS

709C	MINIDIP ..60¢	10/\$ 5.50	100/\$ 51
723C	DIP .....\$1.15	10/\$11.50	100/\$100
741C	MINIDIP ..60¢	10/\$ 5.50	100/\$ 47
748C	MINIDIP ..80¢	10/\$ 7.50	100/\$ 70
558C	MINIDIP \$1.25	10/\$12.00	100/\$110
NE565A	DIP ....\$3.57	10/\$30.00	
LM309K	To-3 ..\$2.50	5/\$11.25	

### GENERAL PURPOSE SILICON TRANSISTORS

2N3638	PNP .....20¢	10/\$1.65	100/\$15.00
2N3638A	PNP .....22¢	10/\$1.80	100/\$16.50
2N3641	NPN .....23¢	10/\$2.00	100/\$17.50
2N3643	NPN .....23¢	10/\$2.00	100/\$17.50
2N5133	NPN .....15¢	10/\$1.25	100/\$10.00
2N5134	NPN .....15¢	10/\$1.25	100/\$10.00
2N5137	NPN .....18¢	10/\$1.50	100/\$13.65
2N5138	PNP .....15¢	10/\$1.25	100/\$10.00
2N5139	PNP .....15¢	10/\$1.25	100/\$10.00
2N3055	NPN .....\$1	10/\$9.50	100/\$86.25

### 1 AMP SILICON RECTIFIERS

1N4001	50PIV ....12/\$1	100/\$6	1M/\$49
1N4002	100PIV ....11/\$1	100/\$6	1M/\$51
1N4003	200PIV ....10/\$1	100/\$7	1M/\$53
1N4004	400PIV ....10/\$1	100/\$8	1M/\$55
1N4005	600PIV .....9/\$1	100/\$8	1M/\$61
1N4006	800PIV .....7/\$1	100/\$9	1M/\$75
1N4006	1000PIV .....6/\$1	100/\$101M/\$83	

### SILICON SIGNAL DIODES

1N4148 (1N914 equiv.) 20/\$1 100/\$4.50 1M/\$35

### ELECTROLYTIC CAPACITORS

Values from 1 usd through 2200 ufd. Competitive prices listed in latest flyer.

### MOLEX IC SOCKET PINS

100/\$1.00	200/\$1.80	300/\$2.60	500/\$4.20
700/\$5.80	1000/\$8.20	ea addn	1000/\$7.50

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5 VOLT 7 SEGMENT TUBE	.....\$3.75
DISPLAY KIT (TUBE+7447+7475+7490)	\$6.15
	3/\$17.50
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DISPLAY KIT (LED+7447+7475+7490+RESISTORS)	.....\$6.40
	3/\$18.25

### 1/4 & 1/2 WATT 10% RESISTORS

1/4W 5¢	30/\$1.20	100/\$3.00	500/\$13.75
	as low as 1.7¢	ea in quantity-see catalog	
1/2W 4¢	30/90¢	100/\$2.50	500/\$11.25
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BOX 126H THIEF RIVER FALLS, MN56701

Circle 86 on reader service card

### MINIATURE POWER SUPPLY

Supply is 2 1/2 x 1 1/2 x 1 1/2 and is 3.0 volts @ 300 ma. Has on-off switch, pilot light & 5 1/2 ft. line cord. Add 2 diodes, which we supply, and supply becomes 6 volts. Ideal for RTL, DTL, TTL IC circuits, battery chargers, portable radios etc. STOCK NO. J5081. with data. 3.75 ea. 3/10.00

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AEMCO, 1 to 15 second solid state precision timer. 3PDT relay closes at selected time. 10 amp. contacts. Operates from 115 VAC. With data sheet. Removed from new equipment. STOCK NO. J9566 4.95 ea. 3/13.00

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This autotransformer can supply more than 90 different voltages, from 10 to over 250 volts, at currents from 15 to 25 amps. Ideal for laboratory experimental and development work, or can be built into equipment. Made by G.E. for use in computers. Data sheet supplied. Original cost \$78.50. In factory boxed cartons. Wt. 20 lbs. STOCK NO. F9467 12.50 ea. 2/22.00

### 8 SECTION PUSHBUTTON SWITCHES

New lot of G.E. 8 section Push button switches, all SPST, rated 8A @250 V. Each button different in color for positive identification. 4 1/2 x 1 1/2 x 2 1/2. Pushing any switch releases any switch that is closed. STOCK NO. J9052 1.25 ea. 5/5.00

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Circle 85 on reader service card

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It can have a 3, 4, 5, or 6-digit readout.

## NOVEMBER ISSUE ON SALE OCT. 18

# Opto Electronics Sale

LIGHT EMITTING DIODE GaAs INDICATORS



- 2-MV1\* Amber, visible jumbo epoxy lens upright . . . \$1.00
- 1-MV2\* TO-18, Dome, green, visible . . . 1.00
- 1-MV-2\* green small dome, green diff. lite . . . 1.00
- 1-MV-2\*, clear small plastic dome, green diff. lite . . . 1.00
- 1-MV-3\* clear mini "pin head" dome, TO18, green lite . . . 1.00
- 1-MV302\* visible, "coax pin pak", red, mini dome lens . . . 1.00
- 1-MV4\* stud, high power, red, 2-watts . . . 3.95
- 1-MV4M\* stud, high power, hi-dome, red, 2-watts . . . 3.95
- 3-MV10B, visible, red, clear, dome lens, TO-18 . . . 1.00
- 3-MV10C, visible, red, diffused, dome lens, TO-18 . . . 1.00
- 3-MV50\*, axial leads, micro-mini dome, clear, red . . . 1.00
- 3-MV5012\*, visible, red, axial, dome lens . . . 1.00
- 3-MV502\*, jumbo red dome, TO-18, visible . . . 1.00
- 3-MV5020\*, jumbo clear dome, TO-18, visible, red . . . 1.00
- 1-MV5040\*, 4-LED red array, with 6-lead pak . . . 1.49
- 3-MV5054\*, visible, red, jumbo dome lens, upright . . . 1.00
- 2-MV5080\*, TO-18, micro-mini, clear dome, red . . . 1.00
- 4-MV5082, visible, red, clear flat lens, TO-18 . . . 1.00
- 1-MV5222\*, green hi plastic dome, diffused green lite . . . 1.00
- 1-MV522\*, green hi plastic dome, diff. green lite . . . 1.00
- 1-MV5222\*, jumbo dome, green, panel snap-in . . . 1.49
- 1-MV5322\*, jumbo dome, GaAsp, panel snap-in Yellow . . . 1.98
- 1-MV9000\*, cartridge panel lamp, sealed, red, clear lens . . . 1.49
- 2-MT-2\*, Photo Transistor, light sensor, TO-18 . . . 1.00
- 2-ME-1\*, infra-red, parabolic lens, pin type . . . 1.00
- 3-ME-4\*, infra-red, "invisible", TO-18, diff. dome . . . 1.00
- 3-ME60\*, infra-red, "invisible", axial, micro-mini . . . 1.00

## OPTO-COUPLERS \*Monsanto Equivalent

- MC2-30\* 1500V Photo Darlington Relay \$1.00
- MCD1\* 4000V Isolation Photo Transistor 3.95
- MCD2\* 1500V Isolation Photo Diode 1.00
- MCT1\* 4000V Isolation Photo Transistor 4.95
- MCT2\* 1500V Isolation Photo Transistor 1.00
- MCT2-D\* 1500V Isolation Twin Photo Transistor 1.49
- MCT5-10\* 10,000V Isolation Photo Transistor 3.95
- MCT5-25\* 25,000V Isolation Photo Transistor 4.95

### LITRONIX-MONSANTO-OPCOA LED Readouts

All fit 14-pin IC sockets, 5V 10 to 20 mA, 0- to 9 numerals, plus letters & decimal. With spec sheets. \* Monsanto Equal. MAN-1 \*\* MAN-1 Spares. † 3-Diode Array.

MONSANTO "ALL LED" Type	Color	Size: Display	Decimal	Driver	Each	Special
MONSANTO MAN-1*	.27	Red	Yes	SN7447	4.50	3 for \$12.
MONSANTO MAN-2*	.32†	Red	Yes	2513	6.50	3 for \$18.
MONSANTO MAN-3*	.115	Red	Yes	SN7448	2.25	3 for \$6.
MONSANTO MAN-3*	.115	Red	No	SN7448	1.49	3 for \$3.
MONSANTO MAN-4*	.190	Red	Yes	SN7448	2.95	3 for \$8.
MONSANTO MAN-4*	.190	Red	No	SN7448	1.79	3 for \$5.
MONSANTO MAN-5*	.27	Green	Yes	SN7447	6.50	3 for \$18.
MONSANTO MAN-8*	.27	Yellow	Yes	SN7447	6.50	3 for \$18.

### "REFLECTIVE LITE BAR" (SEGMENT) LED READOUTS

Decimal right or left

LITRONIX 707*** (MAN-1)	.33	Red	Yes	SN7447	3.80	3 for \$9.
LITRONIX 704*** (MAN-4)	.33	Red	Yes	SN7448	3.80	3 for \$9.
OPCOA SLA-1** (MAN-1)	.33	Red	Yes	SN7447	3.50	3 for \$9.
OPCOA SLA-1** (MAN-1)	.33	Red	No	SN7447	1.95	3 for \$5.
OPCOA SLA-3H Giant Digit	.70	Red	Yes	SN7447	8.60	3 for \$24.
OPCOA SLA-2 Plus/Minus/1	.33	Red	No	SN7447	3.50	3 for \$9.
OPCOA SLA-11C (MAN-5)	.33	Green	****	SN7447	4.95	3 for \$13.
OPCOA SLA-12 Plus/Minus/1	.33	Green	—	SN7447	4.95	3 for \$12.

### HOBBY EXPERIMENTAL "LED" KORNER

- 3-MAN-3\* "The claw", some segments missing, hobby use, readout \$1.00
- 1-MAN-9\* some segments missing, hobby use, readout . . . 1.00
- 1-SLA-7 Opco's MAN-1, 1-segment missing, hobby use, readout . . . 1.49
- 1-SLA-7 Opco's MAN-1, hobby, some segments missing, hobby use, readout . . . 1.00
- 10-LED HOBBY SURPRISE! any types, no-test, . . . 1.00
- 5-MONSANTO's Opto Coupler surprise, asst. no-test . . . 1.00
- 3-PC. KIT, MAN-1, MAN-3, MAN-4, some segments missing . . . 1.49
- 1-SLA-13H Opco, giant 0.7 character readout, some seg missing . . . 1.49
- 1-SLA-11 Opco, like MAN-1, green, some seg missing, readout . . . 1.49
- 2-SPERRY SP332, twin-digit, factory failures, no test . . . 1.00

### SPERRY "ORANGE" TWIN DIGIT ARRAY

Each digit is 7-segment LED (MAN-3 type) and internally "multiplexed" and driven by SN7448. Made by OPTORAY, OND-C-13, intended for calculators, clocks, test equipment, etc. Encapsulated in red transparent epoxy in 14-pin dip pak. With decimals. High brightness, character size .12 x .077. Requires 5V 10 mA.

3 LED DIGITS ON A DIP \$8.88

### LED MITY DIGIT "DCM'S"

Scientific Devices "Digital Counting Modules" outperform any other DCM on the market today. More features than ever before! Not gaseous, not incandescents, not nixie but the modern LED. Choose from such famous manufacturers as Monsanto's MAN-1, MAN-4, Litronix 707 and 704, Opco's SLA-1 (the last 4 having character heights of 0.33 at no extra charge). Each kit includes 3x2" p.c. Board with fingers for a FREE edge connector, side-mounting dip socket, LED readout of your choice, resistors, 3 IC's, and Molex connectors (this ELIMINATES SOLDERING YOUR IC'S), and booklet. INCLUDES P.C. EDGE CONNECTOR — FREE!

Only \$9.99

Buy 3 — Take 10%

READOUT	Char. Maker
MAN-1	.27 h. Monsanto
MAN-4	.19 h. Monsanto
707*	.33 h. Litronix
704*	.33 h. Litronix
SLA-1*	.33 h. Opco

\* Your choice of 5 red LED readout!

### MUX'D DIGITAL CLOCK PC BOARD

Each board properly multiplexed for 6 digits, to hold MAN-1's, MAN-3's, MAN-4's, Litronix 707 (MAN-1) and 704 (MAN-4), and Opco's SLA-1 (MAN-1). Board 6 7/8" long with spec sheets. \* Elec char. same as Monsanto devices MAN-1 or 4.

### 1¢ SALE SCHOTTKY TTL IC

REG.	1¢ MORE
SN74500	\$0.98
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SN74520	.98
SN74522	.98
SN74540	.98
SN74550	.98
SN74551	.98
SN74560	.98
SN74564	.98
SN74573	.98
SN74574	.98
SN74578	.98
SN74582	.98
SN745106	1.98
SN745107	1.98
SN745108	1.98
SN745112	1.98
SN745113	1.98
SN745114	1.98
SN745139	1.98
SN745140	1.98
SN745151	2.50
SN745153	3.98
SN745157	1.08
SN745158	3.00
SN745182	2.50

### ALLEN BRADLEY "TRANSISTOR" POTS

Type F. Screwdriver adjust. Any 4 for \$1

Ohms	7.5K	10.0K	25K	50K	75K	100K	250K	500K															
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### ALLEN BRADLEY "MICRO-POTS"

Type G, 1/2" dia. 1" high, Mounis 1" hole, with shaft, linear, immersion-proof, high precision. 2 for \$1

Ohms	2.5K	5K	10K	25K	50K	100K	250K	500K
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### POLY PAKS STOCKS "C-MOS" IC CIRCUITS

Type	Sale
74C00	\$.95
74C02	.75
74C04	1.15
74C10	.95
74C73	1.79
74C74	1.59
74C76	1.79
74C157	2.50
74C160	3.50
74C161	3.50
74C162	3.50
74C163	3.50
74C195	4.50

### RCA TYPE "C-MOS" IC'S

Type	Sale
CD4001AE	\$.71
CD4002AE	.71
CD4009AE	1.69
CD4011AE	.71
CD4012AE	.71
CD4013AE	1.62
CD4016AE	1.62
CD4023AE	.71
CD4035AE	4.16

### STUD "TRIACS"

PRV	15 amp	25 amp
50	\$5.88	\$8.88
100	.85	1.08
200	1.28	1.48
300	1.48	1.88
400	1.85	1.95
600	2.55	2.25
800	—	2.65

### CALCULATOR KEYBOARD

Etched calculator board with holes, as above, less switches \$2.50 Board

9.95 3 for \$27

### 12-DIGIT "CALCULATOR CHIP"

Similar to Mostek 5001. Outperforms Texas Instruments TMS1802. 40-pin DIP. Adds, multiplies, subtracts, and divides. Use with 7-segment readouts, Nixies, and LEDs. We include schematics, instructions to build calculator.

CT5002-9 Volt version of above — \$9.95

CT5005-Same as above with MEMORY — \$14.95

### OAK FEATHER-TOUCH CALCULATOR KEYBOARD SWITCHES

For RTTY. Printed Circuits. For Unique Panel Switches

No.	Sale	8° .49	CE† .49	+† .49
0° .49	8° .49	CE† .49	+† .49	
1° .49	7° .49	CL† .49	X† .49	
2° .49	8° .49	—† .49	•† .49	
3° .49	8° .49	+ =† .49		
4° .49	8° .49			

\* White (top, black numbers. † Blue top, white characters.

### NATIONAL EQUALS ON "DIGITAL CLOCK ON A CHIP"

Any "Chip" \$12.88

\* Money Back Guarantee!

Mfrs #	Description	Sale
5311	28-pin, ceramic, any readout, 6-digits: A-B-D	\$12.88
5312	28-pin, ceramic, any readout, 4-digits: C-D	\$12.88
5313	28-pin, ceramic, any readout, 6-digits: A-C	\$12.88
5314	24-pin, plastic, LED and incandescent readouts, 6-digits: A-B	\$12.88

Code: A—Hold Count. C—1 PPS Output. B—Output Strobe. D—BCD

### NATIONAL MM5316 EQUAL "ALARM CLOCK ON A CHIP"

MOS 40-pin dip IC. Four display modes time, seconds, alarm and sleep, for a variety of digital clocks. Inter-crystal displays. Requires single power supply, 12 or 24 alarm setting, featuring 9-minute SNOOZE, ALARM silencing only 32mw @ 8V. Operates from 8 to 29 Hz. Has many, many features. The only ALARM CHIP on the market today at this low Poly Pak price. With 6 pages of tech. info, plus applications.

AM RADIO ON A "DIP" Only \$1.49

Over 50,000 pieces purchased from SPRAGUE ULX2187. Designed for superhet AM radio applications. Contains two amplifiers, a mixer oscillator, age detector, and voltage regulator on a single chip. Its inflation-fighting, economy priced because we can't test 'em! With spec sheets and diagrams, 14-pin dip pak. Supply Vec 14. Money back guarantee.

### 9 DIGI-METER READOUT FOR PANEL INDICATION

Imagine! Nine 7-segment MAN-3's mounted in a red plastic molded 2 1/2" x 1" x 1/2" meter like case. Each group of MAN-3's are multiplexed internally on dip substrate red epoxy then mounted on a multiplexed substrate that holds 3 dips, each consisting of 3 MAN-3's. Then connected to 19 fingers and 19 external connecting pins. Attractive panel-like construction lends itself to 1000's of panel mounting DIGI-METER READOUT applications. Complete with instructions. Mounts easily in Molex sockets, with spec sheets.

Only \$18

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**International Electronics Unlimited  
PRE MOVING SALE**

**10% OFF ANY ITEM ANY QUANTITY**

<b>TTL's</b>					
7400	\$.25	7443	\$1.25	7493	\$1.05
7401	.25	7444	1.30	7494	1.10
7402	.25	7445	1.25	7495	1.05
7403	.25	7446	1.45	7496	1.05
7404	.29	7447	1.45	74121	.55
7405	.27	7448	1.50	74123	1.15
7406	.55	7450	.29	74145	1.25
7408	.29	7451	.32	74151	1.05
7409	.29	7453	.32	74153	1.45
7410	.25	7460	.30	74154	1.75
7411	.35	7470	.50	74155	1.35
7413	.95	7473	.55	74157	1.50
7420	.25	7474	.55	74161	1.65
7423	.37	7475	.95	74164	2.95
7425	.39	7476	.55	74165	2.95
7430	.25	7483	1.25	74175	2.95
7432	.30	7485	1.20	74181	4.50
7437	.50	7486	.55	74192	1.65
7440	.25	7489	3.25	74193	1.65
7441	1.25	7490	1.25	74194	1.65
7442	1.15	7492	1.05	75195	1.15

**Low Power TTL**

74L00	.40	74L42	.80	74L85	1.25
74L02	.40	74L51	.40	74L86	.95
74L04	.40	74L71	.60	74L90	1.75
74L10	.40	74L72	.60	74L93	1.75
74L16	.40	74L73	.80	74L95	1.75
74L20	.40	74L74	.80	74L164	2.95
74L30	.40	74L78	.80		

**8000 Series**

8091	.69	8123	1.75	8810	.95
8092	.69	8214	1.95	8812	1.25
8093	.69	8280	.95	8831	1.95
8094	.69	8520	1.45	8836	1.75
8095	.69	8551	1.95		

**Linear**

LM300	T05	.95	LM311	T05	1.25
LM301	T05	.45	LM320-5.2	T05	1.95
LM302	T05	.95	LM320-12	T05	1.95
LM304	T06	1.25	LM320-15	T05	1.95
LM305	T05	1.25	LM380	Dip	1.75
LM307	T05	.45	LM3900	Dip	.50
LM308	T05	1.25	LM709	T05-Dip	.29
LM309K	T03	1.95	LM723	Dip	.75
LM309H	T05	1.25	LM741	T05-Dip	.45
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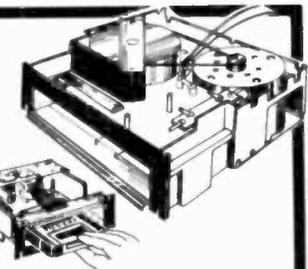
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SN7403	.30	SN7438	.60	SN7474	.52
SN7404	.35	SN7441	1.40	SN7475	.30
SN7405	.35	SN7446	.65	SN7476	.95
SN7406	.35	SN7442	1.25	SN7477	1.30
SN7407	.55	SN7443	1.35	SN7478	.95
SN7408	.55	SN7444	1.35	SN7479	.75
SN7409	.35	SN7445	1.35	SN7481	1.15
SN7410	.30	SN7446	1.50	SN7482	1.95
SN7411	.35	SN7447	1.50	SN7483	1.15
SN7412	.95	SN7448	1.50	SN7485	1.41
SN7413	.55	SN7449	.35	SN7486	.55
SN7414	.55	SN7451	.35	SN7489	4.25
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SN7416	.55	SN7454	.50	SN74139	1.50
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SN7418	.35	SN7461	.35	SN74151	1.25
SN7419	.35	SN7462	.35	SN74152	1.60
SN7420	.30	SN7463	.35	SN74153	1.95
SN7421	.35	SN7464	.50	SN74154	1.40
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\*Litronics or Opco equals to MAN-1 char  
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LM-307	Super 741	.59
LM-308	Hi-Q Fet Type Op Amp	1.50
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LM-311	Comparator	1.50
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LM-371	R-F, I-F, op amp	.69
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561	Phase lock loops (DIP)	3.25
562	Phase lock loops (DIP)	3.25
565	Phase lock loops (A)	3.25
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741CV	Freq. comp 709 (Mini DIP)	.49
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 7446 1.75  
 7447 1.75  
 7448 1.15  
 7450 .35  
 7451 .35  
 7453 .50  
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 SLA-7 Readouts ..... \$2.50

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Burroughs 87971 alphanumeric nixie tube. Giant 2 1/2" character height. Forms all letters of the alphabet, and numerals 0 thru 9. Consists of 15 segments in "star" matrix. When used as numeric display only, it is wired as a seven segment display, requires 170 volts D.C.

- This is the same unit we use in our Giant Clock.
- 87971 tube, brand new with used socket ..... \$7.50
  - 87971 tube, removed from equipment ..... \$2.50
  - Socket for above (only with tube) ..... \$5.00
  - 4 for \$7.50

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We have two new lenses available, both in production quantities. Excellent for opaque projectors, copy cameras, and inexpensive enough to have around the lab for all kinds of optical breadboarding.



- Copy Lens 1, 1 1/2" dia. mount, 4 1/2" focal length, speed F 5.6. Covers 5" x 5", 9 x 9 at 1:1 conjugates. Manufactured by Ednalite. LCEO 1 ..... \$6.00
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Both lenses for \$13.50  
 Two(2) of each type for \$25.00

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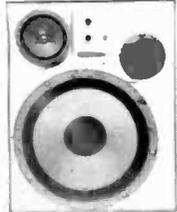
We are always getting requests for power resistors to use in testing amplifiers, power supplies, etc. This is an assortment of resistors of various values ranging in power from 5 watts to 100 watts. If you use just one, it is easily worth twice the cost of the entire assortment.

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This is a useful item to have for variable power supplies, testing, heater control, etc. 0-115 vac in, 0-130 volts out. Removed from equipment ..... \$6.00  
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We have made an excellent purchase of an excess inventory of a local manufacturer's speaker systems, although we are not allowed to mention the mfg.'s name, the specs should make it self-evident. The woofer is a 12" free-edge (acoustic suspension) unit, with 2" voice coil and a No. 2 magnet. The mid-range is a 5" sealed back speaker and 3-1/2" flare dome tweeter for best high frequency dispersion.

Crossover between woofer & mid-range is by an R-L-C network, while high frequency crossover is by an R-C network. Balance controls are provided for both mid-range and tweeter. Plans for a suitable enclosure are provided. The level controls provide frequency response to suit room acoustics, with realism that will delight even the most critical listener. Response - 25 to 20K + Hz., Power - 40 watts RMS. Impedance - 8 ohms.

- Sh. Wt. 12 lbs. .... \$36.00
- LSCS ..... \$36.00
- 2LSCS ..... 2 for \$65.00

**TELSA COIL KIT**



Here's a truly basic kit for those who like to "roll their own." All the parts for an exciting adventure into high-frequency, high voltage. Add your own metal housing - a small chassis or universal box is ideal.

Tesla coils are patterned after the design of Nikola Tesla (1857-1943) an American electrical genius who built entire cities with energy radiated from such coils - but no luck!

Today's Tesla coils are popular with experimenters and students, and especially for science fair and educational demonstrations. Ours is a high-frequency push-pull oscillator coupled to a television flyback transformer, which steps up an external 12 VDC power supply to many thousand volts.

**SPECIAL NOTE:** Although current output is relatively low, some hazard is inherent in all high voltage devices. This kit is intended for the experimenter who is mature enough to observe reasonable precaution in its use.

- TELSA COIL KIT ..... \$7.50

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Always one of B & F's most popular items, now revised to include drilled boards, I.C. sockets, and right-angle socket for readout. Arranged so that units can be stacked side by side and straight pieces of wire bussed through for power, ground and reset. Several different units are available as follows:

- 7490 Basic 10 MHz counter. Used in frequency counters and events.
- 74196 Same as 7490 except presettable 50 MHz unit. Used where higher speed and/or presettable is required.
- 74192 Bi-Directional Counter, 32 MHz operation. Has two input lines, one that makes the unit count up, the other down. Uses include timers, where the counter is preset to a number and counts down to zero, monitoring a sequence of events, i.e., keeping track of people in a room by counting up for entries and down for departures.
- 7475 Adds latch capability. Used in counter so displays continue displaying frequency while new frequency is being counted for uninterrupted display. Basic decoder module. Drives basic seven segment display which is included for all modules.
- 7447

**NEWEST DCU!**

This DCU combines all of the features of our other counting units, that is, high speed counting, up-down operation, storage, and preset. In addition it includes a comparator (7485) and a thumbwheel switch in order to provide comparison and preset capability. With this combination you can do the following:

1. Count up or down at speeds to 33 MegaHertz.
2. Store previous count during new count.
3. Preset to any number, count down (or up) and generate a logic level when count of zero is reached. Stack several units and generate logic level for any count greater than zero.
4. Preset to zero, count up (or down) and generate a logic level for any number greater or equal to the number preset in the thumbwheel switch. Stack several DCU's and generate a logic level showing whether number is greater than, equal to, or less than numbers preset on switches.

- 910 K 7490-7447 Counter ..... \$8.25
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- Sh. Wt. 20 lbs. IBMPSRA ..... \$7.50
- 3 for \$20.00 IBMPSRA ..... \$20.00/3
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- Transistors, 2N441 or 2N442 type, TO-36 case ..... \$1.00 ea.
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- Connectors, 2 for \$1.50 ..... \$1.50/2
- Capacitor, 1 \$5.00 ..... \$1.50 ea.

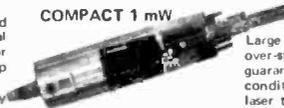
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These fantastic L.E.D indicators have built-in decoder/driver with memory. They use a 4 x 7 dot array for much better readability. They are packaged in a standard Dual-In-Line (DIP) package with built-in contrast filter. Completely DTL TTL compatible. HP part number 5082-7300 (right hand decimal)

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  - 10 for \$850.00 C1mWLT ..... \$850.00/10
  - 100 for \$7500 C1mWLT ..... \$7500.00/100
- Portable supply - operates from 12 vdc input. Useful for field experiments with laser. Available only with purchase of tube.
- Price ..... \$25.00

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Revolutionary! was the reaction of our customers when they saw our latest kit. Measuring only 2 1/2" x 2 1/2" x 2 3/8", and accurate to 10 seconds a month, this chronometer promises to entirely replace mechanical clocks in cars, boats and airplanes.

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- Quartz Chronometer, Kit Form ..... \$69.50
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**New-Style AUTO/BOAT/PLANE QUARTZ CRYSTAL CHRONOMETER**

As you can see from the illustration, we have provided a new enclosure for our most popular kit, the ARIES Model AR-720K Quartz Crystal Chronometer. This enclosure can be mounted in many convenient variations, i.e., over or under the dashboard, over the center drive tunnel, or under the roof above the windshield.

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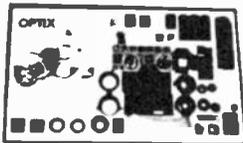
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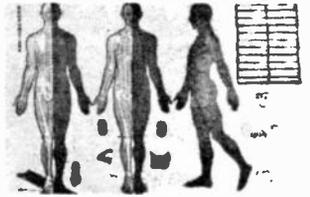
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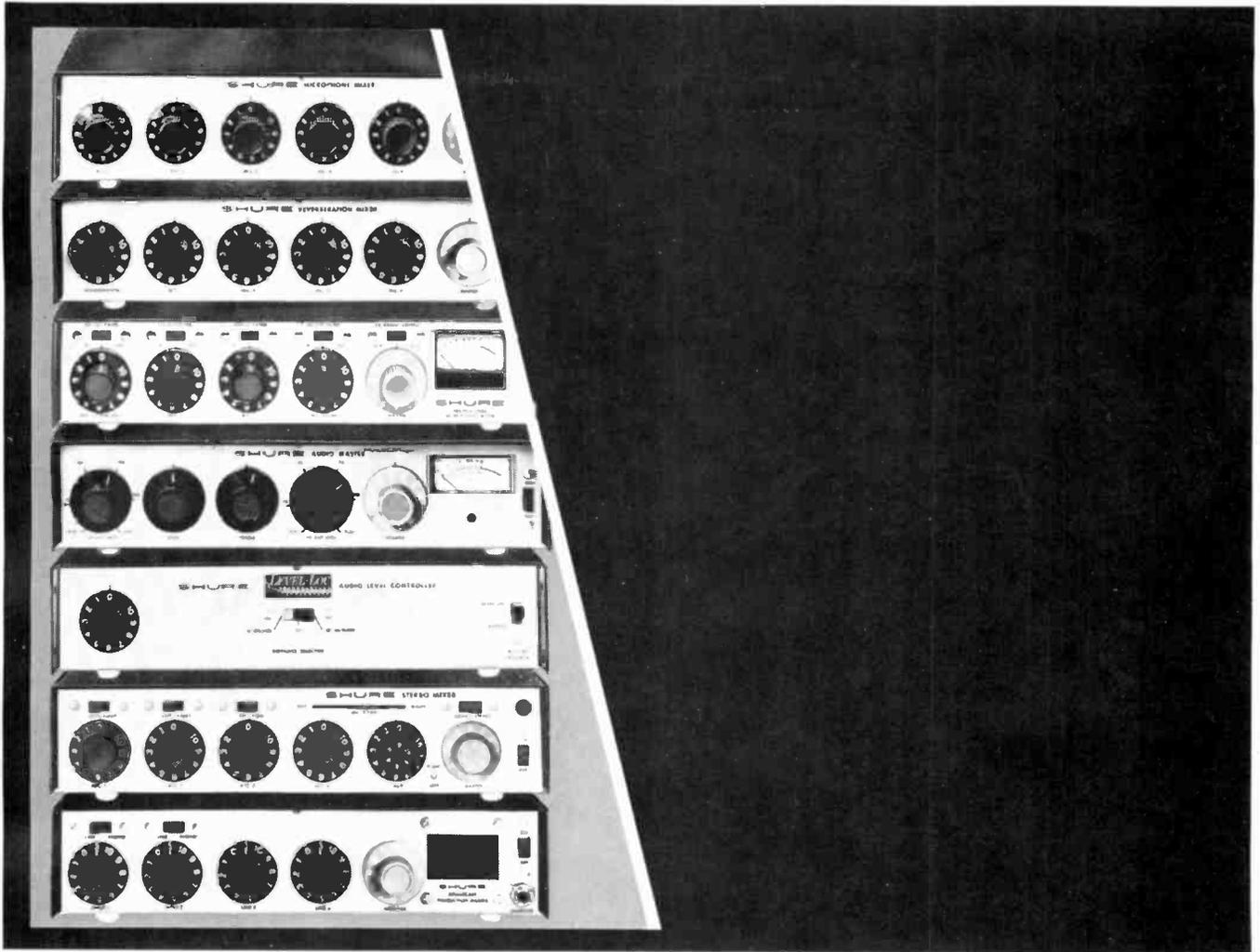
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