

WESTINGHOUSE ELECTRIC CORPORATION ELECTRONICS AND X-RAY DIVISION


## WARNING!

## HIGH VOLTAGE!

THE VOLTAGES ENCOUNTERED IN THIS EQUIPMENT ARE DANGER OUS TO HUMAN LIFE. TO BE SAFE, DISCONNECT THE POWER SOURCE WHEN SERVICING ANY OF THE UNITS.

The use of high voltages which are dangerous to life is necessary for the operation of of the electronic equipment covered by these instructions. While all practical safety precautions have been incorporated in the design of the equipment, they are net infallible; therefore, certain precautionary measures must be carefully observed by the operating personnel during the operation, inspection and maintenance of the equipment.

KEEP AWAY FROM LIVE CIRCUITS .- Do not reach into an enclosure or handle any portion of the externally installed units without first removing the power and grounding the circuit.

OBSERVE EXTREME CAUTION WHEN SERVICING OR ADJUSTING THE EQUIPMENT .- Do not connect any apparatus external to the enclosure, to circuits within the equipment, or apply voltages to the equipment for testing purposes while any non-interlocked portion of the shielding or enclosure is removed or opened. Connection of apparatus external to the enclosure in addition to being a hazard may cause failure of the interlock circuits.

DO NOT TAMPER WITH INTERLOCKS .- Under no circumstances should any door or safety interlock be removed or short circuited, nor should interlocks be relied upon for removing voltages from the equipment.

DO NOT DEFEAT THE MECHANICAL INTERLOCK SYSTEM BY THE USE OF DUPLICATE KEYS.

## TABLE OF CONTENTS

Page
INTRODUCTION ..... 9
Electrical Specifications. ..... 9
Mechanical Specifications ..... 10
Units of the Complete Transmitter ..... 11
Tube Complement ..... 12
DESCRIPTION ..... 13
Electrical Description ..... 13
Mechanical Description ..... 18
RECEIVING, HANDLING, AND STORAGE ..... 22
Inspection of the Shipment ..... 22
Handling Procedure ..... 23
Storage ..... 23
Packing List ..... 23
INSTALLATION PLANNING ..... 26
Building Layout ..... 26
INSTALLATION ..... 27
Transmitter Interconnections ..... 27
Transmitter Cubicles ..... 28
External Power Equipment ..... 28
Ground System ..... 29
Interlocks ..... 30
Cooling System ..... 30
Heating Facilities ..... 31
INITLAL ADJUSTMENT AND TESTS ..... 32
Grounds and Short Circuits ..... 32
Switchgear Adjustments ..... 34
Relay Settings ..... 34
Gas Filled Capacitors ..... 35
RF Component Settings ..... 35
POWER-ON ADJUSTMENTS ..... 37
Power Line Voltage ..... 37
Blowers ..... 37
Air Velocity ..... 37
Distribution Bus ..... 38
Filament Voltages ..... 38
Exciter Bias and Plate Voltages ..... 39
RF Driver Neutralization ..... 40
RF Driver Tuning ..... 41
Power Amplifier Neutralization ..... 41
Low Level Audio Adjustments ..... 42

## TABLE OF CONTENTS (Concluded)

Page
Main Rectifier Regulator Operation ..... 43
Main Rectifier Regulator Adjustments (If Used). ..... 43
Main Rectifier Power Adjustments. ..... 44
Final Tune-Up ..... 44
Antenna Arc Interrupter Adjustments ..... 46
NOISE, FEEDBACK, DISTORTION, AND RESPONSE ..... 47
Noise ..... 47
Power Supply Ripple Voltages ..... 48
Voltage Feedback. ..... 48
Current Feedback ..... 48
Distortion. ..... 48
Frequency Response ..... 49
CONTROL CIRCUITS ..... 49
Fundamental Control Schematic Diagram ..... 49
The Turn-On Sequence ..... 50
Action on Sustained Fault ..... 50
Supervisory Relay Test Position. ..... 51
Supervisory Search Relay ..... 51
Outage Clocks ..... 51
Filament Undervoltage Relay K-8 ..... 52
Bus Breaker S-2001 ..... 52
MAINTENANCE ..... 52
Suggested Schedules ..... 52
Rectox Rectifiers. ..... 54
Normal Meter Readings ..... 55
GUARANTEE AND AVAILABLE WESTINGHOUSE SERVICE ..... 57
Guarantee. ..... 57
Service Available from Westinghouse ..... 58
PARTS AND RECOMMENDED SPARE PARTS LIST ..... (See Tab)

# LIST OF PHOTOGRAPHS 

(See Tab)

Figure
Title
Power Control Cubicle Front View
Power Control Cubicle Drop-Down Panel
Power Control Cubicle Interior
Power Control Cubicle Interior, Left Side
Power Control Cubicle Interior, Right Side
Exciter Cubicle Front
Exciter Cubicle Audio Door
Exciter Cubicle Radio Door
Exciter Cubicle Oscillator
Exciter Cubicle Interior
Exciter Cubicle Interior, Left Side
Exciter Cubicle Interior, Right Side
Modulator Cubicle Front
Modulator Cubicle Interior, Front
Modulator Cubicle Interior
Left Power Amplifier Cubicle Front
Left Power Amplifier Cubicle Interior, Front
Left Power Amplifier Cubicle Interior
Center Power Amplifier Cubicle Front
Center Power Amplifier Cubicle, Lower Front
Antenna Arc Interrupter Unit
Center Power Amplifier Cubicle Interior
Right Power Amplifier Cubicle Front
Right Power Amplifier Cubicle Interior, Front
Right Power Amplifier Cubicle Interior
Main Rectifier Filter Units

## LIST OF DRAWINGS

(See Trab)

Figure
Title
Drawing No.

## INSTALLATION DRAWINGS



## LIST OF DRAWINGS (Concluded)

Figure

Title

Drawing No.
38 Typical Air Exhaust Duct . . . . . . . . . . . . . . . . . . . . . . 7621270
$39 \quad$ Basic Air Supply System 7429905
40 End Radii Drawing . . . . . . . . . . . . . . . . . . . . . . . . . 7619510
41 Desk
7715022
SCHEMATIC AND WIRING DIAGRAMS
42 Interconnection Wire List and Wire Bill . . . . . . . . . . . . . . 7429128
43 Power Room and Distribution Bus . . . . . . . . . . . . . . . . . 55-A-8403
44 RF Wiring (Top of Cubicles) . . . . . . . . . . . . . . . . . . . . 7621267
45 Panel Termination for RG-17/U Coaxial Cable. . . . . . . . . . . 7619445
46 Console, Schematic Diagram . . . . . . . . . . . . . . . . . . . . 7715024
47 Fundamental Control, Schematic Diagram . . . . . . . . . . . . . 7301140
48 50HG-2 Broadcast Transmitter, Schematic Diagram . . . . . . 63-J-60
49 Interlock Connections . . . . . . . . . . . . . . . . . . . . . . . . 7432056
50 Power Control Cubicle, Wiring Diagram . . . . . . . . . . . . . . 7301144
51 Exciter Cubicle, Wiring Diagram . . . . . . . . . . . . . . . . . 63-J-63
52 Modulator Cubicle, Wiring Diagram . . . . . . . . . . . . . . . . 63-J-61
53 Left Power Amplifier Cubicle, Wiring Diagram . . . . . . . . . . 7301195
54 Center Power Amplifier Cubicle, Wiring Diagram. . . . . . . . . 63-J-62
55 Right Power Amplifier Cubicle, Wiring Diagram . . . . . . . . . 7301192
56 Rectifier Wire Bill and Wiring Diagram . . . . . . . . . . . . . 55-A-3921
57 Switchgear, Wiring Diagram . . . . . . . . . . . . . . . . . . . . 7720157
58 Distribution Bus Regulator, Schematic Diagram . . . . . . . . . . 7718453
59 Main Rectifier Regulator, Schematic Diagram (If Used) . . . . . . 7718452
60 Type FA Crystal Oscillator, Wiring Diagram . . . . . . . . . . . 7720555
61 Type FA Crystal Oscillator, Schematic Diagram . . . . . . . . . 7425857
62 Composite Diagram, Antenna Arc Interrupter Unit . . . . . . . . 7724452
63 RF Current Transformer-Rectifier . . . . . . . . . . . . . . . . 7432074
64 Ground Diagram . . . . . . . . . . . . . . . . . . . . . . . . . . 55-A-8424

## LIST OF SUPPLEMENTS

## (See Tab)



## LIST OF SUPPLEMENTS (Concluded)



## INTRODUCTION

The Westinghouse Type 50HG-2 Transmitter is a high-level-modulated standard broadcast transmitter with nominal RF power output of 50 kw . It incorporates the latest developments in electrical and mechanical design and meets all the operational requirements for a modern broadcast transmitter. Years of experience with the problems of the broadcaster has resulted in a Westinghouse transmitter designed for easy installation and economical operation and maintenance.

The following summary of electrical and mechanical specifications, and list of major components will serve to introduce the Westinghouse 50HG-2 Transmitter to the new owner.

## ELECTRICAL SPECIFICATIONS

Type of Emission ..... A-3
Power Output (to transmission line or common point) 53 kw , max.
Frequency Range (single specified frequency)
Lower Limit ..... 540 kc
Upper Limit ..... 1600 kc
Frequency Stability $\pm 10 \mathrm{cps}$
Modulation Capability ( 50 to 7500 cps inclusive) 100 percent
Carrier Shift ( 100 percent modulation with 400 cps sine tone), less than 5 percent
Audio Distortion ( $0-95$ percent modulation from 50 to 7500
cps, including all harmonics up to 45 kc ). less than 3 percent
Modulation high level Class B
Frequency Response ( 30 to $10,000 \mathrm{cps}$ ) ..... $\pm 1 \mathrm{db}$
Carrier Hum better than 60 db below 100 percent modulation
Audio Input Level ( 100 percent modulation at 1000 cps ) ..... $10 \pm 2 \mathrm{dbm}$
Power Line Requirements (see note 1 below):
Incoming Power Lines see note 2
Line volts. ..... 460 volts
Phase ..... 3 phase
Frequency (see note 3 below) ..... 60 cps
Power Input for 0 percent modulation ..... 103.5 kw
Power Input for average modulation ( 25 percent) ..... 113 kw
Power Input for 100 percent modulation ..... 147 kw
Power Factor (approximate) 90 percent
Maximum Permissible Power Line Variation:
Frequency ..... $\pm 2$ percent
Deviation of full load phase-to-phase voltage from 460 volts ..... $\pm 5$ percent
Deviation of full load phase-to-phase voltage from average for the three phases ..... $\pm 2$ percent
Regulation ..... $\pm 2$ percent
Total permissible variation, including regulation from no load to full load, in percentage of 460 volts. ..... - $\pm 5$ percent
Crystal Heater Power Supply Requirements:
Line volts ..... 115 volts
Phase ..... 1 phase
Frequency 50-60 cps
Power ..... 30 watts
Output Impedance (one side of output coil grounded) ..... 40 to 250 ohms
Ambient Temperature Operating Range ..... $\pm 5^{\circ} \mathrm{C}$ to $\pm 45^{\circ} \mathrm{C}$
Distribution Bus Regulator Automatically maintains 230 voltsfor an input variation of approxi-mately $\pm 10$ percent
Main Rectifier Regulator(when furnished)

Note 1: The power requirements specified in this section do not include provision for the lights and convenience outlets in each transmitter cubicle. A 115 volt, single phase supply of approximately 1 kw capacity should be available.

Note 2: Lightning and switching surges on the incoming power lines can damage transmitter equipment. Therefore, it is suggested that the incoming circuits be examined for the probability of such transients and protective devices installed as necessary.

As a minimum requirement, three lightning arrestors, equal to Westinghouse style 1254825 should be used on the incoming 460 volt line, one between each line and ground.
Note 3: The Type 50HG-2 Transmitter can be supplied for operation with a 50 cycle supply.

## MECHANICAL SPECIFICATIONS

| Description | Dimensions in Inches |  |  | Approximate Weight in Pounds |
| :---: | :---: | :---: | :---: | :---: |
|  | Height | Depth | Width |  |
| Power Control Cubicle | 84 | 54-1/4 | 48-1/4 | 2225 |
| Exciter Cubicle | 84 | 54-1/4 | 48-1/4 | 2370* |
| Modulator Cubicle | 84 | 54-1/4 | 48-1/4 | 2100* |
| Left Power Amplifier Cubicle | 84 | 54-1/4 | 48-1/4 | 1920* |
| Center Power Amplifier Cubicle | 84 | 54-1/4 | 48-1/4 | 1550 |
| Right Power Amplifier Cubicle | 84 | 54-1/4 | 48-1/4 | 1920* |
| Switchgear Cubicle | 90-3/8 | 48 | 20 | 1225 |
| Rectox Rectifier and Frame, each of two | 64 | 28 | 41 | 350 |
| Modulation Transformer | 78-7/8 | 46-1/2 | 56 | 5700 |
| Filter Capacitor; each of three | 29-3/16 | 7-1/4 | 18 | 75 |
| Filter Reactor | 17-1/2 | 12-3/4 | 11-3/4 | 175 |
| Distribution Bus Regulator, each of two | 30-3/4 | 10-1/2 | 10 | 250 |
| Audio Filter Capacitor | 5-3/4 | 6-1/2 | 5 | 5 |
| Modulation Reactor | 67-1/2 | 29-1/2 | 40-1/2 | 2450 |
| Auxiliary Audio Choke | 16-1/2 | 22 | 18 | 25 |
| Modulation Coupling Capacitor | 26-1/2 | 18 | 7-1/2 | 75 |
| Blower | 70-5/16 | 65-5/8 | 49-1/4 | 920 |
| Blower Motor and Base | 15 | 22-1/2 $\dagger$ | 20 | 250 |
| Control Box | 24-3/8 | 5-5/8 | 9 | 25 |
| RF Current Transformer-Rectifier | 12 | 12 | 8 | 25 |
| Main Rectifier Transformer | 75 | 50 | 56 | 3300 |
| Main Rectifier Regulator (when furnished) | 75-5/8 | 43-3/4 | 24 | 3325 |
| Distribution Bus Transformer, each of three | 22-1/8 | 14-3/4 | 16-3/4 | 235 |

[^0]
## UNITS OF THE COMPLETE TRANSMITTER

The Westinghouse Type 50HG-2, 50 KW Standard Broadcast Transmitter consists of the following individual units:

1. One Power Control Cubicle . . . . . . . . . . . . . . . . S\#1475118
2. One Exciter Cubicle (less tubes and crystal oscillators and crystals) . . . . . . . . . . . . . . . . S\#1474773
3. One Modulator Cubicle (less tubes) . . . . . . . . . . . . S\#1474774
4. One Left Power Amplifier Cubicle (less tubes) . . . . . . . S\#1475119
5. One Center Power Amplifier Cubicle. . . . . . . . . . . . S\#1474775
6. One Right Power Amplifier Cubicle (less tubes) . . . . . . . . S\#1475120
7. Two Type FA Crystal Oscillators for Exciter Cubicle

S\#1472593
8. Two crystals, Type TMV-129B for Crystal Oscillators . . .Dwg. 7431159
9. One Rectox Rectifier and Frame for Power Amplifier . . . . S\#1474566
10. One Rectox Rectifier and Frame for Modulator . . . . . . . S\#1474565
11. One Modulator P.S. Filter Reactor . . . . . . . . . . . . KR-7822469
12. One Main Rectifier Plate Transformer . . . . . . . . . . . S\#1646118
13. One Main Rectifier Induction Voltage Regulator (Optional Equipment)

S\#1486437
14. One Modulation Transformer . . . . . . . . . . . . . . . S\#1483785
15. One Modulation Reactor . . . . . . . . . . . . . . . . . S\#1453629
16. One Modulation Coupling Capacitor . . . . . . . . . . . . S\#1081020
17. One Auxiliary Audio Choke . . . . . . . . . . . . . . . . S\#1472317
18. Audio Filter Capacitor . . . . . . . . . . . . . . . . . . S\#1471665
19. Three Distribution Bus Transformers . . . . . . . . . . . S\#1483783
20. Two Distribution Bus Induction Voltage Regulators . . . . . S\#1486439
21. One Switchgear Cubicle. . . . . . . . . . . . . . . . . . S\#1474865
22. P.A. and Modulator Filter Capacitors (Three) . . . . . . . S\#1474519
23. One Blower . .. . . . . . . . . . . . . . . . . . . . .Dwg. 7426385 Pt. 11
24. One Blower Motor . . . . . . . . . . . . . . . . . . . . S\#1442202
25. One Control Box for Blower Motor. . . . . . . . . . . . .Dwg. 7426385

Pt. 10
26. One Set of End Radii (to suit installation) . . . . . . . . . . Dwg. 7718801

Pt. 21
27. One RF Current Transformer . . . . . . . . . . . . . . . S\#1471694A
28. 60 Feet of RF Cable . . . . . . . . . . . . . . . . . . . RG-17/U
29. 70 Feet of RF Cable . . . . . . . . . . . . . . . . . . . RG-62/U
30. One Installation Kit (consisting of touch-up paint and miscellaneous hardware) . . . . . . . . . . . . . .Dwg. 7427705
31. One complete set of Operating Tubes.

Dwg. 7503652
GR. 1
32. Two Instruction Books . . . . . . . . . . . . . . . . . . IB 81-120-2A
34. One Station Call Letter Plate . . . . . . . . . . . . . . . Dwg. 7718801

Pt. 25

50 cps
S\#1475121
S\#1474780
S\#1474781
S\#1475122
S\#1474782
S\#1475123
S\#1472593
Dwg. 7431159
S\#1474566
S\#1474565
KR-7822469
S\#1646118
S\#1476438
S\#1483785
S\#1453629
S\#1081020
S\#1472317
S\#1471665
S\#1483783
S\#1486439
S\#1474864
S\#1474519
Dwg. 7426385
Pt. 11
S\#1442202
Dwg. 7426385
Pt. 10
Dwg. 7718801
Pt. 21
S\#1471694A
RG-17/U
RG-62/U
Dwg. 7427705
Dwg. 7503652
GR-1
IB 81-120-2A
S\#1472812
Dwg. 7718801
Pt. 25

Note 1: Interconnection wiring material is not furnished as a part of the Type 50-HG-2 Transmitter.

Note 2: Although not furnished as a part of the transmitter, the following accessory equipment can be supplied by Westinghouse:

Antenna Phasing Equipment
Transmitter Control Console S\#1472247
Precipitron Air Filter
Main Rectifier Induction Voltage
Regulator

Spare Blower, Motor and Control Box
25 KW Power Cutback Facility
10 KW Power Cutback Facility
Spare Tubes
Spare Parts

## TUBE COMPLEMENT

The following tubes are supplied with the transmitter:

| Qty. | Tube Type |
| :--- | :--- |
| 4 | WL-5671 |
| 4 | WL-5736 |
| 4 | WL-813 |
| 3 | WL-807 |
| 2 | WL-802 |
| 2 | OD3/VR-150 |
| 3 | RCA-1V |

These tubes are used as follows:

| Location | Tube Type | Quantity |
| :--- | :--- | :---: |
| Right Power Amplifier | WL-5671 |  |
| Left Power Amplifier | WL-5671 | 1 |
| Exciter, RF | WL-5736 | 1 |
| Exciter, RF | WL-813 | 2 |
| Exciter, RF | WL-807 | 2 |
| Exciter, Oscillator | WL-802* | 1 |
| Exciter, Oscillator | OD3/VR-150* | 2 |
| Center Power Amplifier | RCA-1V | 2 |
| Antenna House | RCA-1V | 2 |
| Modulator | WL-5671 | 1 |
| Exciter, Audio | WL-5736 | 2 |
| Exciter, Audio | WL-813 | 2 |
| Exciter, Audio | WL-807 | 2 |

* These tubes are part of the oscillator units. One complete spare oscillator is mounted in the Exciter.


## DESCRIPTION

The purpose of this section is to familiarize the station engineers with the electrical and mechanical details of the $50 \mathrm{HG}-2$ transmitter.

The text is in two sections: the Electrical Description, and the Mechanical Description. Although there are no specific references to the photographs, they are so identified that they may be used to further clarify the text.

## ELECTRICAL DESCRIPTION

1. Radio Frequency Circuits

The radio frequency system of the transmitter consists of the following stages:
a. A WL-802 crystal oscillator with an OD3/VR-150 regulator tube for stabilizing the screen voltage.
b. A WL-807 buffer amplifier.
c. The first amplifier, two WL-813 tubes, in parallel.
d. The second, or driver amplifier, two WL-5736 tubes, in parallel.
e. The final amplifier, two WL-5671 tubes, in push-pull.

The Type FA Crystal Oscillator is an individual plug-in unit containing the TMV-129B crystal and heater assembly, the oscillator and voltage regulator tubes, and the associated circuitry. Frequency stability is maintained by the use of a highly stable quartz crystal in an electroncoupled circuit. The crystal is kept at a constant temperature in an automatic oven. Approximately 15 watts of 115 volt, single phase, power is required for operation of the oven. To further insure stability, a voltage regulator tube is used in the screen supply.

Two complete crystal oscillator units are included with the transmitter. A relay, operated by a switch on the front panel of the Exciter Cubicle, allows transfer from one unit to the other without noticeable interruption of carrier. The unit not in use is constantly in readiness with crystal heater and tube filaments energized.

The buffer stage uses a lightly loaded WL-807 tube as a Class C amplifier. The grid circuit is untuned and no neutralization is required. A cathode current meter is included. Cathode bias is provided to protect the tube in the event of excitation failure.

The first radio frequency amplifier consists of two WL-813 tubes in parallel as a Class C amplifier. The grid circuit is untuned and is capacitively coupled to the tuned plate circuit of the buffer stage. Grid and plate current meters are provided. The plate circuit is tuned by a motordriven capacitor. No neutralization is required. Cathode bias protects the tubes in the event of excitation failure. A loop coupled to the plate inductor is provided for feeding energy to a frequency monitor.

The second, or driver amplifier, uses two parallel WL-5736 tubes as Class C amplifier. The grid circuit is connected to a tap on the shunt-fed plate tank of the preceding stage. This tap can be adjusted to provide the proper grid drive. Neutralization is accomplished by a variable vacuum capacitor connected between the plates of the WL-5736 tubes and the plate tank inductor of the preceding stage. A motor-driven variable compressed-gas capacitor is used in the plate tank circuit. Total grid current and individual plate currents are metered. The total plate current is indicated by a large scale instrument. Fixed bias is supplied by an individual power supply.

The final amplifier is a Class C stage employing two WL-5671 tubes in push-pull. These tubes have thoriated tungsten filaments. The grid tank circuit is inductively coupled to the plate tank circuit of the driver stage. The coupling inductor is on the same coil form as the plate inductor of the driver stage, and has a motor-driven variable tap for coupling adjustment. An individual bias supply is provided for each half of the push-pull amplifier. Grid current and bias voltage for each tube is individually metered. A motor-driven variable compressed-gas capacitor is used in each grid circuit.

The plate tank circuit of the power amplifier is shunt fed in order that the two motordriven compressed-gas tank capacitors may be mounted at ground. Plate voltage and individual plate currents are metered. Inductive neutralization is used.

The output coupling coil is mounted inside the final tank inductor and has a motor-driven variable tap at ground potential. A Faraday shield is between the final tank inductor and the output coupling coil for suppression of harmonics. A thermocouple radio-frequency ammeter is in series with the output lead. This instrument is mounted behind a glass window in the Center Power Amplifier Cubicle and may be shunted out of the circuit by a switch on the lower front panel. A recti-fier-type meter is provided for remote indication of the output current.

A spare tube socket and filament transformer are provided for each of the operating tubes in the final amplifier. Substitution of the spare tube for its associated operating tube can be accomplished quickly.

RF energy for a modulation monitor may be obtained from the power amplifier tank circuit by tapping on to the tank coil end ring at a suitable point.

## 2. Audio Frequency Circuits

The audio frequency system of the transmitter consists of the following push-pull stages:
a. First audio, two WL-807 Class A.
b. Second audio, two WL-813 Class A.
c. Third audio, two WL-5736 Class AB.
d. Modulator, two WL-5671 Class B.

The first audio stage contains a line-to-grid input transformer which can be connected for either a 600 or a 150 ohm line. This stage has individual cathode bias for each tube. The total cathode current is metered. The plate circuit is resistance coupled to the following stage.

The second audio stage has individual bias adjustment for both tubes and is resistance coupled to the following stage.

The driver audio stage is a cathode follower, with an individual bias supply for each tube. Instruments are included for indication of cathode current, grid current and bias voltage for each tube. Cathode current in each tube is indicated by individual large scale instruments. This stage is directly coupled to the grids of the modulator tubes.

The Class B, high-level modulator stage employs two WL-5671 tubes in push-pull. These tubes have thoriated tungsten filaments. Individual bias supplies, adjustable and with separate indicating instruments, are used. Large scale instruments are supplied for plate voltage and individual indication of cathode current, and filament voltage, for each tube.

A spare tube socket and filament transformer are provided for each of the modulator tubes.

The audio power is fed to the final radio frequency amplifier across a modulation reactor, making it unnecessary to pass the plate current for this stage through the modulation transformer. An equalizer circuit stabilizes the modulator load impedance to permit the application of inverse voltage feedback.

## 3. Power Supplies

All power supplies in the transmitter use Rectox rectifiers. Rectox units have essentially unlimited life unless subjected to abuse. All except the two main rectifier supplies obtain primary power from a bus which is maintained at constant voltage by means of two automatic induction regulators connected in open delta. The regulators automatically maintain a constant output voltage of 230 volts for an input supply variation of approximately plus or minus 10 percent. Manual regulator control is also provided. Primary power for filament supplies is also obtained from this regulated distribution bus.

The two main rectifier supplies use a common transformer. By means of mechanically interlocked contactors inside the case of the transformer, the primary can be connected in Wye or Delta for tuning or full power output. Switching any of these contactors is accomplished by an OFF-TUNE-ON switch on the panel of the Center Power Amplifier.

The individual power supplies included in the transmitter are listed and briefly described below:
a. 400 Volt Supply -- this is a single phase, bridge rectifier. It supplies plate and screen voltage to the crystal oscillator and the RF buffer. It also supplies screen voltage to the first and second audio stage and bias to the second audio stage.
b. $1500-3000$ Volt Supply -- this is a 3000 volt, three phase, full-wave rectifier and a 1500 volt, three phase, half-wave rectifier. The 1500 volt supply furnishes plate and screen voltage for the first RF amplifier stage and plate voltage for the first audio amplifier stage. The 3000 volt supply furnishes power for the audio and RF driver stages and it also supplies plate voltage for the second audio stage.
c. Main Rectifier Supplies -- These are two separate high voltage, three phase, full-wave rectifiers using a common transformer. One rectifier supplies approximately 11,500 volts $\mathrm{d}-\mathrm{c}$ to the power amplifier; while the other supplies approximately 13,500 volts to the modulator.
d. Exciter RF Bias Supply -- this is a single phase, bridge rectifier. It supplies bias for the RF driver stage.
e. Audio Driver Bias Supplies -- these are two adjustable single phase, bridge rectifiers. They supply bias for the audio driver stage.
f. Modulator Bias Supplies -- these are two identical single phase, bridge rect fiers. They supply bias for the modulator, one for each of the two operating tubes. Ouiput voltage of each of these rectifiers is controlled from the front panel of the Exciter Cubicle.
g. Power Amplifier Bias Supplies -- these are two identical single phase, bridge rectifiers. They supply holding bias for each of the two operating tubes, and they furnish the fixed portion of the combination fixed and self-bias required to maintain modulation linearity.

## 4. Control Circuits

Controls for all necessary operational circuit and tuning adjustments are provided on the front panels of the cubicles. The associated indicating instruments and lights are coordinated with these controls. Individual switches are provided for all power circuits. These switches are sequence interlocked to prevent possibility of damage to the transmitter components, especially the tubes, which might result from the application of power to a circuit in incorrect sequence. Normally, the transmitter is put into operation by energizing each circuit separately. If desired, however, one switch control of the entire transmitter is possible. The transmitter can be shut down completely by opening the first switch in the sequence which controls power for the filaments and blowers, leaving the other switches in the "on" position. Then to return the transmitter to operation, it is necessary only to close the first switch; the other circuits will be energized in proper sequence and timing.

The transmitter includes a complete supervisory control system which provides indication of abnormal conditions such as overloads and open interlocks. This system is coordinated with the protection and safety provisions described in the following section. Overloads are registered even if they are only momentary; lock-in supervisory relays energize circuit identifying indicator lamps which remain lighted until the operator resets the relays by means of a reset switch on the control panel. This feature assists in locating trouble which can be investigated during normal maintenance period, decreasing future outages.

The supervisory control system includes individual indicator lamps for the following:

400 Volt Overload 1500-3000 Volt Overload
Power Amplifier Rectifier DC Overload
Modulator Rectifier DC Overload
Main Rectifier AC Overload
813 RF Overload
Left 5736 RF Overload
Right 5736 RF Overload
Left Power Amplifier Overload
Right Power Amplifier Overload
Left 813 Audio Overload
Right 813 Audio Overload
Left 5736 Audio Overload
Right 5736 Audio Overload
Left Modulator Overload

Right Modulator Overload<br>Antenna Arc-over<br>Carrier Interruption<br>Power Control Door Interlock<br>Exciter Door Interlock<br>Modulator Door Interlock<br>Left Power Amplifier Door Interlock<br>Center Power Amplifier Door Interlock<br>Right Power Amplifier Door Interlock<br>Rectifier and Filter Door Interlocks<br>Antenna Phasing Door Interlock<br>Search Relay<br>Supervisory Relay Test<br>Spare<br>High Voltage Enclosure Door Interlock

The search relay can be connected into any one of the other transmitter protection systems that are not listed above in order to check the operation of that system in searching for faults. The spare relay is provided for such uses as an antenna house interlock indicator, etc.

The major switching functions, together with their associated indicators, can be duplicated at a transmitter console.

Two clocks are provided. One registers Outage Duration and the other registers the time
outage occurred. at which outage occurred.
5. Overload and Safety Protection

The basic overload protection in the Type 50HG-2 Transmitter is designed around two draw-out-type Westinghouse DB-25 Air breakers in the Metal-Enclosed Switchgear Cubicle. These breakers have their own a-c trip coils. One breaker supplies the main rectifiers. The other supplies all other power except that for the breaker trip circuits, blowers, crystal heaters, cubicle lights, and convenience outlets in the transmitter cubicles.

Protection is provided by fast-acting relays and circuit breakers. Any overload, undervoltage, or open interlock will remove the primary power from the supply or supplies involved. The design of the transmitter provides for a choice of automatic or manual return of the transmitter to operation.

With the OVERLOAD PROTECTION CONTROL set in the AUTO position, an overload will trip the set off but power will be reapplied immediately. In the event of successive overloads, the transmitter will trip off three times but, after the third time, power will not be reapplied for a predetermined period of time, normally set for five seconds. After this delay time, power will be automatically reapplied and the transmitter returned to normal operation. If the overloadcondition persists, the sequence will be repeated until the transmitter is turned off manually.

With the OVERLOAD PROTECTION CONTROL in the MANUAL position, any overload which trips the 400 volt supply off will leave the transmitter off until the operator resets the control. Any other overload will trip the transmitter off three times, if the condition persists, and then leave it off until reset by the operator.

A partial list of the overload and undervoltage relays in the transmitter is given below:

```
Undervoltage relays, a-c:
    Main rectifier
    Distribution bus
    Filament
Undervoltage relays, d-c:
    Exciter bias supply
    Left audio driver bias supply
    Right audio driver bias supply
    Left modulator bias supply
    Right modulator bias supply
    Left power amplifier bias supply
    Right power amplifier bias supply
Overcurrent relays, a-c:
    Distribution bus
    Main rectifier
Overcurrent relays, d-c:
    400 volt supply
    1500-3000 volt supply
    Power amplifier supply
    Modulator supply
    RF }813\mathrm{ stage
    Left 5736 RF tube
    Right 5736 RF tube
```

Left modulator tube
Right modulator tube
Left power amplifier tube
Right power amplifier tube
Left 813 audio tube Right 813 audio tube
Left 5736 audio tube
Right 5736 audio tube
De-ion a-c thermal overload breakers: Exciter filaments
Left power amplifier filament No. 1 Left power amplifier filament No. 2 Right power amplifier filament No. 1
Right power amplifier filament No. 2
Left modulator filament No. 1
Right modulator filament No. 2
Left modulator filament No. 3
Right modulator filament No. 4
Switchgear control bus
Panel lights
Transmitter control bus
Bus regulators
Audio bias
RF bias
400 volt supply
1500-3000 volt supply

Other relays employed in the control and supervisory circuits are the time-delay, auxiliary supervisory, stepping, etc., which have not been classified above.

In the entire transmitter there is only one fused circuit affecting operation. That circuit supplies closing power to the distribution bus breaker.

Protective provisions not mentioned above which are included in the transmitter are air interlocks, door interlocks, and the Antenna Arc-Interrupter Unit.

Every reasonable precaution for the safety of personnel is incorporated in the design of the transmitter. All components except those to be installed in the power room are of the deadfront type. The switchgear cubicle uses draw-out type breakers. All cubicle doors which allow access to dangerous potentials are electrically interlocked. In addition, the cubicles are provided with grounding sticks and with automatic mechanical shorting switches which ground dangerous voltages when access doors are opened. It is possible to extend the interlock system to include electrical interlocks on vault doors, phasing cubicle doors, antenna tuning houses, and any other enclosure which the purchaser may desire to protect. The purchaser may also use the keys from the switchgear as the basis for a mechanical door interlock system. The necessary ordering information for such a system may be found under the SUPPLEMENTS in the back of this book.

## MECHANICAL DESCRIPTION

The six transmitter cubicles have welded steel frames and aluminum panels. Each cubicle has four leveling screws. A detachable wiring trough is built into the lower rear of each cubicle, thus providing a full length wiring trough for the interconnection cables. Full length, full width front and rear doors are provided, and each door has a large, unobstructed window. Four large scale meters are mounted on an inclined panel on the top front of each cubicle. Instrument and control panels are illuminated, and each cubicle is equipped with a convenience outlet and a service light. All controls and indicators are completely identified. Details of particular cubicles are listed below:

## 1. Power Control Cubicle

This cubicle functions as the basic power control center for the entire transmitter, and contains the following:

1500-3000 volt supply
De-ion switches
Bus regulator controls Supervisory control relays and lamps
Outage time clock

Outage duration clock
Blower controls
Bias supply controls
Miscellaneous relays

The four large meters at the top of the cubicle indicate Line Current, Line Voltage, Bus Current, and Bus Voltage. Line and Bus Phase Selector switches are provided for the meters. These switches also have an off position. The drop-down panel in the front door provides access to the supervisory control indicators and switches, the two outage clocks, the blower control switches and lamps, and the bias supply switches and indicators.

The front door provides access to all De-ion switches, the bus regulator controls, the meter switches and the elapsed hour meter, all of which are mounted just above the control panel. This door is not interlocked. The rear doors are electrically interlocked and a grounding switch automatically grounds the output of the 1500 volt and 3000 volt supplies.
2. Exciter Cubicle

This cubicle contains the driver sections for the modulator and the power amplifier stages. It also contains the following:

400 volt supply
Exciter RF bias supply
Both audio 5736 bias supplies
Both modulator bias supplies

> Both type FA crystal oscillators
> First, second and driver audio stages
> RF buffer, amplifier, and driver stages

The four large scale meters at the top of the cubicle indicate Left 5736 Audio Cathode Current, Right 5736 Audio Cathode Current, 3000 Volt Rectifier volts and 5736 RF Total Plate Current.

The drop-down panel in the front door allows access to the control panel. This panel, which is hinged to facilitate servicing, mounts the switches and lamps for the 400 volt supply, the 1500-3000 volt supply, and the crystal heater circuits. It also mounts the audio 5736 bias controls, the modulator bias controls, the 813 tank tuning motor drive control, the 5736 tank tuning motor drive control, and the crystal oscillator selector switch. In addition to the position indicating meters associated with the motor driven tuning elements, the following meters are mounted on this panel:

400 Volt Rectifier Voltage
1500 Volt Rectifier Voltage
Left 5736 Audio Driver Bias
Right 5736 Audio Driver Bias
807 Audio Cathode Current
Left 813 Audio Power Amplifier
Cathode Current
Right 813 Audio Power Amplifier
Cathode Current
Left 5736 Driver Grid Current
Right 5736 Driver Grid Current

Left Modulator Bias
Right Modulator Bias
Oscillator Cathode Current
807 RF Buffer Cathode Current
813 RF Amplifier Total Grid Current
813 RF Amplifier Total Cathode
Current
5736 RF Driver Total Grid Current
Left 5736 RF Driver Plate Current
Right 5736 RF Driver Plate Current

The audio circuits are contained in the left side of the cubicle and the radio frequency circuits in the right side, viewed from the front. The controls and indicators on the control panel are correspondingly grouped. When the front door is opened, two smaller doors below the control panel and two tube compartments above the control panel are exposed. The low level audio stages are mounted on the inside of the lefthand door, and the low level RF stages are mounted on the inside of the righthand door. Components and wiring are accessible when these doors are open. The crystal oscillators are individual plug-in units.

The left compartment above the control panel houses the audio 5736 stage, and the right compartment houses the RF 5736 stage.

Audio and RF components mount at the rear on the side walls of the cubicle. A partial partition divides the left and right sides of the cubicle to isolate the audio circuits from the radio frequency circuits. All doors are interlocked, except the drop-down panel.

## 3. Modulator Cubicle

This cubicle contains four tube sockets and four filament transformers (two of each are spares), transfer switches, two feedback dividers, and two gas surge suppressor resistors. The four large scale meters at the top of the cubicle indicate Left Modulator Plate Current, Modulator Filament Volts, Modulator Plate Volts, and Right Modulator Plate Current.

The panel in the front door is fixed in position as there are no controls on this cubicle. On the upper part of this panel are mounted four indicator lamps and a switch. The lamps are "ON" indicators for Left Filament, Bias, Plate, and Right Filament. The switch is used to connect any one of the four filament transformers to the filament voltmeter at the top of the cubicle.

The lower part of the cubicle is used as the plenum chamber for the cooling air. The four filament transformers are mounted from the top of the cubicle, each one directly above its associated tube socket. The plate suppressor resistors and the plate transfer switches are mounted between each front and rear tube. The grid transfer switches are mounted on the side walls between each front and rear tube.

The plenum chamber is equipped with removable metal panels in the front and rear and these panels are interlocked with the air supply. The front and rear cubicle doors are interlocked. The electrical interlocks remove the modulator and driver plate voltage and bias voltages. The mechanical switch grounds the modulator plate supply.
4. Left Power Amplifier Cubicle

This cubicle encloses one side of the push-pull amplifier circuit. It contains one of the power amplifier tubes with provisions for mounting and switching a spare tube, two filament transformers, bias supply, plate choke, neutralizing coil, plate tank capacitor, grid tank circuit, grid leak, overload and under-voltage relays.

The four large scale meters mounted at the top of the cubicle indicate Left PA Filament Volts, Left PA Grid Volts, Left PA Grid Current and Left PA Plate Current.

The basic construction of the cubicle is identical to that of the Modulator Cubicle previously described.

The panel in the front door is fixed and mounts four indicator lamps and a filament voltmeter selector switch. The lower part of the cubicle is used as the air plenum chamber. It has two removable metal access panels which are interlocked with the air supply.

The filament transformers are mounted from the top of the cubicle directly above the tube sockets. The compressed gas plate tank capacitors are mounted in the plenum chamber with their tops protruding for connection to the tuning motor drive. The plate selector switch is mounted between the two tube sockets. A grid parasitic suppressor and a switch are mounted on both side walls near the grid connections to the tubes. The grid tank inductor and capacitor are mounted from the top of the cubicle. The plate choke is mounted in the plenum chamber and the neutralizing coil and its associated capacitors are mounted on the top of the plenum chamber.

The front and rear doors are both interlocked. The electrical interlocks remove the power amplifier and driver plate voltage and bias voltages when either door is opened. The mechanical switch grounds the plate supply.
5. Center Power Amplifier Cubicle

This cubicle is similar in general construction to the Power Control and Exciter cubicles previously described. It contains the power amplifier circuit controls, the plate tank inductor, and the output coupling inductor assembly with the Faraday shield. It also contains the Antenna Arc Interrupter control panel, current transformer-rectifier, the thermo-couple output ammeter and the remote output ammeter and its current transformer-rectifier.

The four large scale meters at the top of the cubicle indicate PA Plate Volts, Total PA Plate Current, RF Output Current, and Total Transmitter Input Power. The drop-down panel in the front door covers the control panel which mounts the following controls and indicators:

> Antenna Arc Protector Control Switch and Indicators Main Rectifier Control Switch and Indicators
> Main Rectifier Regulator Selector Switch
> Main Rectifier Regulator Automatic Voltage Control
> Main Rectifier Regulator Manual-Raise-Lower Switch Main Rectifier Regulator Indicators

The front door, which is not interlocked, provides access to the tuning controls and indicators mounted above the control panel. They are:

> Left Grid Tuning
> Right Grid Tuning
> Ganged Grid Tuning
> Left Plate Tuning

The indicating instruments are:

Left Grid Current<br>Right Grid Current<br>Left Plate Current<br>Right Plate Current<br>Left Grid Tuning Position

> Right Plate Tuning
> Ganged Plate Tuning
> Driver Coupling
> Output Coupling

> Right Grid Tuning Position
> Driver Coupling Position
> Left Plate Tuning Position
> Right Plate Tuning Position Output Coupling Position

On the left, below the center control panel, is the plug-in Antenna Arc Interrupter Unit. To the right is a glass window behind which is mounted the output thermocouple RF ammeter. Near the window is a handle which operates a make-before-break shorting switch for the ammeter.

The interior of the cubicle is partitioned into three sections. The lower half houses the tank inductor, the output coupling inductor, and the output coupling motor drive. The current transformer-rectifier for the output ammeter and the current transformer-rectifier used in the antenna arc interrupter system are also mounted in this section. The upper half of the cubicle is divided into two sections by a vertical partition. These two sections are provided for housing optional antenna phasing components. Cutouts are provided on either side of the upper front panel for bringing out controls for these components.

The rear doors, which are electrically interlocked, provide immediate access to the upper two sections. In addition, removable panels in the lower front and rear of the cubicle allow access to the tank inductor compartment.
6. Right Power Amplifier Cubicle

This cubicle contains the other side of the push-pull amplifier circuit. It is identical to the Left Power Amplifier Cubicle in construction and contents except that the arrangement is reversed for symmetry.
7. Equipment External to the Cubicles

The equipment external to the transmitter cubicles consists of the Switchgear Cubicle, the Power Amplifier and Modulator Rectox Rectifier, the Filter Capacitors and Reactor, the Main Rectifier Induction Regulator if used, the two Bus Induction Regulators, the Main Rectifier Plate Transformer, the three Distribution Bus Transformers, the Modulation Transformer and Reactor, the Blower and Control Box, the Auxiliary Audio Choke, the Modulation Coupling Capacitor, and the

Arc Interrupter Current Transformer-Rectifier. The design of the transmitter provides for control of this equipment from the transmitter cubicles or from a console in the transmitter room. No oil-cooled components are used, making it unnecessary to provide a fire-proof vault.

The Switchgear Cubicle houses the two DB-25 air breakers and associated control system. The cubicle is standard Westinghouse Metal-Enclosed Switchgear and will match other switchgear the purchaser might obtain from Westinghouse for other purposes. This cubicle is intended for installation near the power room, preferably in the wall of the room with the front panel exposed so that manual operation or inspection is possible without entering the room.

The main Rectifier Filter Capacitors and Reactor are intended for installation in the power room.

The Auxiliary Audio Choke is an air core inductor intended for mounting on the wall of the power room.

The Blower is a Sturtevant Silentvane horizontal bottom discharge unit, clockwise rotation. The blower is equipped with a $7-1 / 2$ horsepower motor. Adjustable-pitch sheaves are provided to allow adjustment of blower speed to suit the particular air duct installation. The Blower is intended for installation outside the power room, discharging into the room through the two Rectox units. A Wall Mounting Control Box is supplied for the Blower.

The Current transformer-rectifier used in connection with the Antenna Arc Interrupter system is intended for connection in series with the lead to the antenna in the antenna tuning equipment. It may be wall or bracket mounted.

## RECEIVING, HANDLING, AND STORAGE

Any obvious shortages or damage should be noted by the customer on the waybill and claim made to the transporation company immediately. It is imperative that when unpacked, the equip. ment be inspected mechanically and electrically and a concealed damage claim submitted within the time limit set by the carrier.

## INSPECTION OF THE SHIPMENT

To assist in inspecting and identifying the equipment, the $50 \mathrm{HG}-2$ Transmitter Packing List, which follows, should be used. Note that some of the master items, such as the transmitter cubicles, are shipped with the more fragile components removed. These components will be found separately boxed.

All boxes of the shipment will have stencilled on the outside surface the following information:

1. The box number.
2. Westinghouse style numbers, if applicable.
3. Description and assigned symbol number of units and separately packed components.

Uncrating should proceed as follows:

1. Begin by selecting box No. 1 .
a. Place it in a position near the selected permanent location for this unit.
b. Unpack carefully.
c. Move the unit into place using the section on Handling Procedure as a guide.
2. Select box No. 2, etc.

To further assist in the inventory, identification and assembly of all units and component parts, the following references are submitted:

1. Units of the complete transmitter listed in the INTRODUCTION.
2. Photographs.
3. Wiring Diagrams.

## HANDLING PROCEDURE

1. Lifting and Skidding

Each of the $50 \mathrm{HG}-2$ transmitter cubicles is separately crated and is provided with a standard skid base. This skid base permits the use of rollers and fork lift.

Eye bolts are provided in the top of each cubicle permitting the use of an "A" frame or other hoisting device for lifting. Care should be used to insure that the pull on the eye bolts is largely vertical and that there is little horizontal strain because of the danger of breaking the bolts or bending the cubicle frame. Never use a short sling.

## 2. Uncrating the Cubicles

After the crated cubicle has been rolled into place, remove the crating from the cubicle, leaving the skid base intact. Use care in the removal of the crating to prevent scratching the finish. Next remove the lag screws from the clamps which secure the cubicle to the skid base. From this point the procedure for installation is described in the section on INSTALLATION.

## STORAGE

The 50HG-2 transmitter may be stored in a clean, dry, well ventilated room for an indefinite period provided that the gas pressure is maintained in gas filled capacitors.

## PACKING LIST

This list only includes units of a standard 50HG-2 Transmitter. Any accessory units ordered such as Antenna Phasing Cubicle, Console, etc., will appear on the packing lists included with the shipment.

## 1. Method of Packing

Some of the components within the cubicles such astransformers, chokes, capacitors, and resistors are tied down or supported by bracing or blocking. The interlocks are tied down or removed from their mountings and tied down. The contactors and relays are tied down and their moving contacts secured firmly with tape or blocked with paper. The fluorescent lamps are removed from their sockets, packed separately and placed within the cubicle. The ceramic lead-in bowls are removed, packed separately and placed within the cubicle. Sets of door keys are tied to the front doors, door keepers are removed, packed separately, and placed in the cubicle.

The fragile components which cannot be properly supported within the cubicle are removed from the cubicle and packaged separately as indicated in the packing list below.

Box \#1 Power Control Cubicle - style 1475118
Box \#2 Exciter Cubicle - style 1474773
Box \#3 Exciter Cubicle components
a. Six Metal Rectifier units

| RX-101 | RX-104 |
| :--- | :--- |
| RX-102 | RX-105 |
| RX-103 | RX-106 |

b. Two RF coils

L-109 - WL-813 RF plate tank coil
L-112 - WL-5736 RF plate tank coil
c. Three Capacitors

C-122 - WL-5736 neutralizing capacitor
C-127 - WL-5736 plate coupling
C-129 - WL-5736 plate tank capacitor
Box \#4 Exciter Cubicle components
a. Two crystal oscillator units - style 1472593
b. Two oscillator crystals - the resonant frequency to be specified by the customer

Box \#5 Modulator Cubicle - style 1474774
Box \#6 Modulator Cubicle components
a. Two feedback divider assemblies consisting of 4 resistors in each assembly.

R-210-1 to R-210-4
R-212-1 to R-212-4
b. Two voltage feedback capacitors, C-207 and C-209.
c. Two parasitic chokes, RL-201 and RL-202
d. Four micarta air ducts

Box \#7 Left Power Amplifier Cubicle - style 1475119
Box \#8 Left Power Amplifier components
a. One metal rectifier unit - RX-301
b. One WL-5671 plate RF choke - L-304
c. One WL-5671 plate blocking capacitor - C-319
d. One WL-5671 grid blocking capacitor - C-316
e. One WL-5671 grid tank coil - L-301
f. One WL-5671 neutralizing blocking capacitor - C-318
g. Two WL-5671 grid parasitic suppressors - RL-302 and RL-303
h. Two micarta air ducts

Box \#9 One WL-5671 Neutralizing Coil - L-303
Box \#10 Center Power Amplifier Cubicle - style 1474775
Box \#11 Center Power Amplifier components
a. One WL-5671 plate tank coil - L-401
b. One Load current ammeter - M-415

Box \#12 Right Power Amplifier Cubicle - style 1475120
Box \#13 Right Power Amplifier components
a. One metal rectifier unit - RX-501
b. One WL-5671 plate RF choke - L-504
c. One WL-5671 plate blocking capacitor - C-519
d. One WL- 5671 grid blocking capacitor - C-516
e. One WL-5671 grid tank coil - L-501
f. One WL-5671 neutralizing blocking capacitor - C-518
g. Two WL-5671 grid parasitic suppressors - RL-502 and RL-503
h. Two micarta air ducts.

Box \#14 One WL-5671 neutralizing coil - L-503
Box \#15 Switchgear cubicle - style 1474865, including levering mechanism and 2 instruction books
Box \#16 Switchgear Cubicle component - Type DB-25 breaker - S-2001
Box \#17 Switchgear Cubicle component - Type DB-25 breaker - S-2002
Box \#18 Filter Reactor - Dwg. 7822469
Box \#19 One PA Rectox Rectifier - style 1474566
Box \#20 One Modulator Rectox Rectifier - style 1474565
Box \#21 One Auxiliary Audio Choke - style 1472317, symbol L-1502
Box \#22 One set of Lefthand End Radius
Box \#23 One set of Righthand End Radius
Bqx \#24 One installation kit per Dwg. 7427705
Box \#25 One audio coupling capacitor - style 1081020, symbol C-1502
Box \#26 One RF current transformer-rectifier for antenna arc interrupterstyle 1471694A
Box \#27 One set of vacuum tubes consisting of:

| Qty. |  | Type |
| :---: | :--- | :--- |
|  |  | WL-5736 |
| 4 |  | WL-813 |
| 3 |  | WL-807 |
| 2 |  | WL-802 |
| 2 |  | WL-VR-150 |
| 3 |  | RCA 1V |

Box \#28, 29, 30, 31, Contain one each of the WL-5671 thoriated tungsten tubes Box \#36, 37, 38 One each of the three distribution bus transformers - style

1483783, symbols T-1502A, B, C
Box \#39 One main rectifier plate transformer - Dwg. 50-D-5771, symbol T-1501
Box \#40 One modulation transformer - style 1483785, symbol T-1503
Box \#41 Filter Capacitor - style 1474519, symbol C-1503
Box \#42 Filter Capacitor - style 1474519, symbol C-1504
Box \#43 One each of two Distribution Bus Regulators, style 1486439, symbol YR-1301
Box \#44 One each of two Distribution Bus Regulators, style 1486439, symbol YR-1302
Box \#45 One modulation reactor - style 1453629, symbol L-1501
Box \#46 One blower fan and housing assembly per Dwg. 7426385, symbol BM \#1
Box \#47 Line Starter - Dwg. 7426385, Pt. 10
Box \#48 One 7-1/2 HP motor - S\#1442202 Two R-150 Belts - Dwg. 7426385, Pt. 8
Box \#49 One Vari-pitch Texrope drive - Dwg. 7426385, Pt. 6
Box \#50 One Sheave "Magic-Grip" - Dwg. 7426385, Pt. 7
Box \#51 One Motor Base "Texslide \#3" - Dwg. 7426385, Pt. 9
Box \#52 One each of the items listed below:
a. Station call letters
b. Nameplate S\#1472812
c. RG-17/U cable - 60 ft .
d. RG-62/U cable - 70 ft .
e. One Audio Filter Capacitor S\#1471665, symbol C-1501

## INSTALLATION PLANNING

The 50HG-2 Transmitter has been designed for maximum installation flexibility to fit various situations. This section on installation planning is intended to assist the architect, station engineers and consultants, in planning the building layout and should NOT be considered an exact specification.

## BUILDING LAYOUT

The building plans must include provisions for:
The Transmitter Cubicles
The External Components
The Cooling System
Cables and Conduits
These items are discussed below.

1. Transmitter Cubicles

A suggested equipment layout for a single floor installation appears on figure 27, and for a two floor installation in figure 28.

These figures illustrate the installation of the six transmitter cubicles and their related external equipment.

The cubicle construction of the transmitter provides adaptability to meet individual installation requirements, but it is preferable to install the cubicles in line. If it is necessary to install the cubicles in a different arrangement, however, Westinghouse will assist the purchaser in planning the installation.

Figure 36 and figure 37 illustrate in-line layouts for the six cubicles. The first figure shows the cubicles built into the wall, and the other shows the cubicles installed free-standing. In either case, appropriate end radii are supplied to provide a finished appearance to the transmitter. The installed length of the six cubicles is $289-1 / 2$ inches and the end radii add 12 inches, making a total of $301-1 / 2$ inches. The cubicles are all $54-1 / 4$ inches deep and a minimum clearance of 60 inches should be allowed in front of and behind the cubicles.

A typical $50 \mathrm{HG}-2$ Transmitter cubicle is shown on figure 35. All six cubicles are identical in general construction and the basic installation requirements are the same. The transmitter room floor should be designed to carry a minimum dead load of approximately 4000 pounds per cubicle, although none of the transmitter cubicles actually weigh that much. The floor should include two parallel "I" beams, 50 inches apart, with top faces level with the floor. The cubicles are set on these beams. After all the cubicles are in place and leveled, they are bolted together and the two end cubicles are bolted down to the "I" beams to prevent creepage. Note that the wooden blocks shown on figure 35 are to prevent either: the drill or the tap from contacting concrete.

## 2. The External Components

The equipment external to the six transmitter cubicles is illustrated on figure 33. All of the items on this figure are individual units and installation is mostly a matter of placement and electrical interconnection. However, it is necessary to install the Rectox Units directly in the main air stream.

The remaining power components should be installed in the power room, with the Switchgear Cubicle built into the wall and its front panel available from outside the room.

A suggested layout for these components is shown on figure 27 and figure 28.

## 3. The Cooling System

The basic air supply system is illustrated on figure 39. For a two floor layout, the supply air duct is the power room and for a single floor layout, it is a concrete trench built into the floor. A 26 by 26 inch hole in the floor beneath each cubicle allows the air to flow into the cubicles. See the Transmitter Floor Plan, figure 29.

The cubicles are constructed to direct the cooling air properly through the cubicles and out through the exhaust grills. An exhaust air duct with a cross-section area of at least 12 square feet is required above the cubicles. This duct should be equipped to allow for direct exhaust or for recirculation of air. A Typical Air Exhaust Duct is shown in figure 38. Recirculation of the air may be provided to assist in heating of the building in cool weather.

Two Blowers are installed so that either may be used to supply the cooling air in case a spare blower is purchased. Air Filters for use with these blowers may be installed directly at the intake to the blowers or in the walls of the building, depending on the situation. If desired, a Precipitron electronic air cleaner may also be used in connection with the air supply system. The Blower Outline showing overall dimensions appears on figure 34.

The Rectox Units must be installed in the air stream from the Blowers. These units are constructed to facilitate such installation, the frames themselves actually forming part of the air duct. It is not necessary to provide any direct cooling for the other components in the power room, but allowance should be made for convection air circulation as in the single floor installation.
4. Cables and Conduits

The cable and conduit runs appear on the Power Room Layout figure 31 (Two Floor) and figure 30 (One Floor). These figures illustrate in a general way the cross wiring of the external power equipment. In a two floor plan, two floor openings, in addition to those provided for the cooling system should be provided, directly beneath the transmitter proper. Other openings are required when a control desk and an audio rack are used with the transmitter; see the Transmitter Floor Plan and Power Room Layout on figure 29 and figure 31.

In a single floor installation, two troughs for high voltage conductors and one trough for power and control wires are required. See Power Room Layout (one floor) on figure 30.

## INSTALLATION

The basic installation plan for the $50 \mathrm{HG}-2$ Transmitter includes two centers of placement of the transmitter components. One is the transmitter room, where the transmitter cubicles are installed, and the other is the power room where the equipment external to the transmitter cubicles is installed.

## TRANSMITTER INTERCONNECTIONS

1. The complete interconnection wiring information appears on figures 42 and 43 . Figure 42 lists point-to-point wiring between cubicles and between cubicles and the power room. Figure 43 shows point-to-point wiring for power room components.
2. The types of wires and lugs and their electrical ratings appear on the last sheet of figure 42. Only items so marked in the figure are supplied as part of the transmitter.
a. The wires and lugs shown on figure 42 are suggested types only. If these are not available or not convenient to use, a satisfactory equivalent may be substituted.
b. Other materials, not listed on figure 42 but required for installation are:
(1) Cable clamps and brackets
(2) Conduit and conduit brackets
(3) House breaker box
(4) Hardware

## TRANSMITTER CUBICLES

The transmitter proper consists of six cubicles. Additional cubicles may be added when necessary for directional antenna arrays. Figure 35 (Typical Cubicle) shows all important dimensions and general constructional details of the cubicles. It should, however, only be used to supplement the layout drawings. These cubicles house the major electronic elements of the transmitter as well as all the low voltage supplies, supervisory control circuits and transmitter controls.

The transmitter is generally installed in conjunction with an operating console, as well as racks containing the audio frequency and measuring equipment. For suggested arrangement of the cubicles with the transmitter room, please turn to Building Layout of this instruction book. Proceed to install the transmitter as follows:

1. Place each cubicle in its permanent position by carefully following instructions under Handling Procedure of this instruction book.
2. Align and level all cubicles on the floor rails.
3. Bolt all cubicles together securely by means of $1 / 2^{\prime \prime}-13$ studs, washers and nuts supplied in the Installation Kit. Make sure of good electrical contact between cubicles.
4. Mark hold-down bolt holes in first and last cubicle.
5. Move first and last cubicles back after removing bolts from sides. Drill and tap $1 / 2^{\prime \prime} \mathbf{x}$ 13 holes in the floor rail.
6. Replace cubicles; align and level and bolt cubicles together tightly, making sure of good electrical contact between cubicles. Bolt end cubicles down with two inch $1 / 2^{\prime \prime}-13$ bolts and washers.

At this time the caulking should be done to prevent air leakage. With a caulking gun, apply compound around all the inside and accessible outside edges of the base of each cubicle. The inside may be reached through the air opening in the floor beneath cubicles. This completes the cubicle installation.
7. Install two RG-17/U coaxial cables to connect the RF driver terminals located on the Exciter Cubicle with the RF input terminals on the Power Amplifier cubicles. The four cable plugs for the RG-17/U cable are shipped assembled to the panel terminations mounted on the top of the cubicles. Figure 44 and figure 45 show RG-17/U wiring and termination respectively. In order to preserve circuit balance, the RG-17/U cables must be cut to the same length.
8. Install two . 375 OD hard-drawn copper tube leads to connect the audio driver terminals (two porcelain feed-through bowls) located on top of the Exciter Cubicle with the audio input terminals (located on top of the Modulator Cubicle). Figure 44 shows the audio driver connection between Exciter and Modulator.

## EXTERNAL POWER EQUIPMENT

The Auxiliary Power Equipment shown on figure 33 is installed in the power room adjacent to the transmitter room.

For suggested arrangements of the Auxiliary Power Equipment within the power room, refer to the Auxiliary Components under INSTALLATION PLANNING.

Proceed to install the Auxiliary Power Equipment as follows:

1. The Switchgear Cubicle houses the two DB-25 Air Breakers and associated control system This cubicle is intended for installation near the power room, preferably in the wall of the roon with the front panel exposed and accessible from outside.
2. The two Rectox Frames house the metal rectifiers for the power amplifier and modulatod supplies. They are intended for installation in the air stream, serving as part of the air duct Clearance shall be provided for the spark gaps mounted on top of the frame.
3. The two filter capacitors and the filter reactor should be mounted adjacent to the rector frames and with at least one foot of clearance on all sides.
4. The Main Rectifier Induction Voltage Regulator, if used, should be installed with clear ances of at least two feet from the top and the sides which mount the primary relay, De-ionswitch and potential transformer.
5. The Distribution Bus Induction Voltage Regulators should be installed with clearances of al least one foot on all sides.
6. The Main Rectifier Plate Transformer, and the Modulation Transformer and Modulatior Reactor are floor-mounted. Access to these units is through the front and rear panels and clear ances should be provided accordingly.
7. The three Distribution Bus Transformers are floor-mounted adjacent to the bus regulators. At least $1^{\prime \prime}$ of clearance should be provided about these units.
8. The Auxiliary Audio Choke is an air core inductor intended for wall mounting adjacent to the Modulation Reactor.
9. The Modulation Coupling Capacitor may be floor-mounted (terminals up) near the Modula. tion Transformer, or wall-mounted on a special bracket (bracket is not supplied).
10. The Audio Filter Capacitor is mounted on top of the Modulation Transformer. It is connected to and mounted on secondary terminal $\mathrm{X}-1$ and a ceramic standoff insulator supplied in the Installation Kit.
11. Install all copper tubing conductors using figure 43 as a reference.
a. The Power Room Layout, figure 30 for a one floor building, and figure 31 for a two floor building, may be used as a reference for the copper tubing conduction layout.

## GROUND SYSTEM

Install the transmitter ground strap using figure 43 as a reference.

1. The transmitter cubicle ground strap is placed in the wire trough and runs from cubicle \#1 to cubicle \#6.

This ground strap runs along the inside surface of the rear " I " beam. It is fastened to the center of the "I" beam in each cubicle base using a $1 / 2$ " -13 bolt. The Exciter Cubicle base is then grounded to the transmitter ground system.
2. Each unit of external equipment is grounded to the cubicle ground strap and thus returned to the transmitter ground system.

## INTERLOCKS

## 1. Electrical

Each cubicle is equipped with interlock switches. Additional switches in the air duct, power room, doors to vaults, etc., should be connected into the transmitter control circuit as shown on figure 49, so that any interruption of the interlocking series will remove power from the transmitter.

## 2. Mechanical

In addition to electrical interlocking, the power room can be protected from entry by a mechanical key interlocking system. Inspection of the Switchgear will disclose two keys marked \#RE-1130. These keys, removable only after the switches are locked in their "off" position, can be used to gain entry into the power room, which should be provided with two identical locks so that both switchgear keys are required to gain admittance.

It would be desirable for the air tunnel trap door to be included in this interlock system. See attached copy of "R. and I. E. Kirk Catalog" for suggestions. All door locks other than the two on the Switchgear should be supplied by the customer. To obtain locks using the keys supplied in the Switchgear, it is necessary to supply R. and I. E. Co. with three items of information: (1) Neg. \#4708179, (2) Key \#1130, (3) Type of locks selected as listed in the Kirk Catalogue. A duplicate set of keys is necessary in case the first set is misplaced, but it is recommended that the duplicate set be kept behind non-removable glass so that breakage is necessary to obtain them. A word of warning at this time: Defeating the key interlock or electrical interlock system is dangerous. THE PURPOSE OF THESE SYSTEMS IS TO PROTECT LIFE.

## COOLING SYSTEM

1. Ducts

After the transmitter is bolted down in its final location, the exhaust air duct can be installed. A typical installation is shown on figure 38. If sound-proof duct lining is used, it must be of fire-proof material. The duct work should be extended to all locations requiring heat and should be equipped with automatic or manually controlled registers. See figure 39, Basic Air Supply System.

For discharge of the heated air to the outside, a ventilator in the roof or ventilators on two sides of the building should be provided to take advantage of the prevailing winds. Self-closing shutters to prevent back-draft are extremely important to prevent back pressure from reducing the flow of cooling air to a dangerous level. Screening should be provided to prevent entry of small animals and birds.

## 2. Air Returns

An unrestricted air return circuit to the blowers should be planned for normal recirculation. This may be in the form of gratings in the floor, doors, walls or a combination of gratings and filters so arranged as to disperse the flow of air and reduce the velocity. Care should be taken to see that the total back resistance pressure of the return circuit is not excessive for the volume of air handled, (approximately 12, 000 CFM). The exhaust duct should not present more than $1 / 4^{\prime \prime}$ water gauge pressure drop.
3. Air Requirements

Normal air requirement for the $50 \mathrm{HG}-2$ Transmitter at sea level in the ambient range $+5^{\circ}$ to $+45^{\circ} \mathrm{C}$, is approximately $12,000 \mathrm{CFM}$ at a resistance pressure of $2^{\prime \prime}$ water gauge. The fan speed for this delivery is 570 RPM ( 4.6 HP ). If necessary, the fan speed can be regulated between 460 RPM and 875 RPM by means of the "Vari-Pitch" sheave. The oil level indicators on the bearings should be installed and the bearings filled to proper level with a good quality oil (SAE 10). Check frequently for the first week after filling to be sure that the fan bearing cups maintain a safe oil level.
4. Blower

The Blower supplied with the transmitter is a Sturtevant "Silentvane," size 90 shown on figure 34. Make certain the Blower is mounted on a level surface.
5. Motor

The motor supplied is Westinghouse Type CPS "Life-line" with standard NEMA frame No. 284. The electrical characteristics are $7-1 / 2 \mathrm{HP}$, three phase, $50 / 60$ cycles, $220 / 440$ volts with medium starting torque. The slide base is an Allis-Chalmers "Texslide No. 3." Some slipping of the belts will be noticed upon starting. This is a normal condition and helps to limit the motor starting current.
6. Sheaves and Belts

The motor is equipped with an Allis-Chalmers "Vari-Pitch" wide-range, two groove sheave allowing a variation from $5-1 / 4$ inch pitch diameter to 10 inch pitch diameter. The Blower has a fixed, two groove sheave of 20 inch pitch diameter. Belts for the above are of a special section to allow for the wide range of speed variation and are known as R-150 "Texrope." A word of caution when replacing belts; always replace both belts, since a new belt will have a shorter circumference than a used one.

## 7. Starter

The motor starter is a combination switch (with magnetic trip overload protection) and contactor (with thermal trip overload protection). Connections to the starter should be made as shown on figure 43. It is recommended that the starter be installed within sight of the blower motor.

## 8. Filters

Some means of cleaning the circulated air should be employed. This may be in the form of spun glass filters or the highly efficient Westinghouse Precipitron. In many cases both are used. The Precipitron is used to clean air brought in from the outside and the spun glass filters are used to clean the recirculated air.

The recommendation of Owens-Corning to filter $12,000 \mathrm{cfm}$ of air is to use 15 of their \#2, 20 " x 20 " "Dust Stop" filters. This allows each filter to pass 800 cfm and thus maintain maximum cleaning efficiency. The average resistance of the \#2 filter when clean is $.13^{\prime \prime}$ water gauge. (This drop doubles when they are stacked double.) A loss of more than $.15^{\prime \prime}$ water gauge for the inlet is not recommended.

The Westinghouse District Office has among its personnel a specialist in Precipitron installation and filter problems. He will be glad to give assistance and make recommendations.

## HEATING FACILITIES

Approximately 50 kw is available for use in heating the transmitter building, when the transmitter is in full power operation.

## INITIAL ADJUSTMENT AND TESTS

Before proceeding with these tests, the following should be observed:

1. Transmitter installation should have been completed according to the section on RECEIVING, HANDLING, AND STORAGE and the section on INSTALLATION of this book.
2. Make a thorough mechanical inspection of the transmitter installation, noting particularly that good wiring practice is used throughout. Check all wires to make sure that the lugs have been properly applied. Burndy-type lugs depend entirely upon the success of the clamping operation for electrical continuity, therefore it is imperative that the proper size lug is properly installed.
3. Check mechanical operation of all doors to make sure that the latches are functioning properly, and that the mechanical and electrical interlocks which depend upon door operation have been installed in their proper places and have been adjusted for positive action.
4. Check the mechanical operation of all relays and make sure that all traces of packing, olocks, twine, tape, wires, etc., have been removed.
5. Remove VR-150, 802, 807, and 813 tubes from their sockets. Disconnect filament leads from the 5736 and 5671 tubes.
6. Make sure that all switches and breakers are off and that the 460 volt, three phase, incoming line is deenergized.

## GROUNDS AND SHORT CIRCUITS

1. Open fuses F-2001, F-2002, F-2003, F-2006, F-2007 in Switchgear Cubicle and test 460 volt lines for short circuits and grounds. Use megger ( 500 volts d-c).
2. Replace fuses, check 460 volt line for grounds.
3. Remove two primary line wires from Distribution Bus Transformers, T-1502, A, B, C. Check for short circuits and grounds. Replace wires.
4. If a Main Rectifier Regulator has been purchased, disconnect leads No. 1 and No. 3 from Main Regulator YR-1201, two leads from primary of Main Rectifier Plate Transformer T-1501, and one fuse from potential transformer on Regulator YR-1201. Check lines for short circuits and grounds. Replace connections.
5. Remove ground from secondary of Distribution Transformer T-1502-B and remove two incoming bus wires from TS-20 in the Power Control Cubicle. Remove fuse F-1C from tube hour meter M-7. Check both ways for shorts and grounds on all wires of bus. Check only for grounds in Distribution Transformer direction.
6. Replace fuse and wires in Power Control Cubicle, but do not replace ground on Distribution Transformer secondary.
7. a. Connect an ohmmeter between ground and a distribution bus wire, then close in sequence the power control De-ion switches shown below:
```
S-1, LEFT PA FILAMENT NO. 1
S-2, LEFT PA FILAMENT NO. 2
S-3, RIGHT PA FILAMENT NO. 1
S-4, RIGHT PA FILAMENT NO. 2
S-5, LEFT MODULATOR FILAMENT NO. 1
S-6, RIGHT MODULATOR FILAMENT NO.2
S-7, LEFT MODULATOR FILAMENT NO. }
S-8, RIGHT MODULATOR FILAMENT NO. 4
```

S-10, PANEL LIGHTS
X S-11, TRANSMITTER CONTROL BUS
S-12, EXCITER FILAMENTS
S-13, AUDIO BIAS
S-14, RF BIAS
S-15, 400 VOLT SUPPLY
S-16, 1500 VOLT - 3000 VOLT SUPPLY
S-22, BUS REGULATOR

No ground should appear.
7. b. If a Main Rectifier Regulator has been purchased, turn on VRS-1201 on the Main Regulator. Operate AUTO/MANUAL, LOWER/RAISE switches S-19 and S-20 in the Power Control Cubicle and VOLTAGE CONTROL SELECTOR and MANUAL VOLTAGE CONTROL switches S-411 and S-412 in the Center Power Amplifier Cubicle. No ground should appear.
8. Close manually, in sequence, the DN magnetic contactors $\mathrm{K}-37$ to $\mathrm{K}-40$ in the Power Control Cubicle. No ground should appear.
9. Remove ground from secondary of switchgear control transformer (T-2005) and check for grounds. No ground should appear. Replace lead.
10. Open TRANSMITTER CONTROL BUS switch and observe 27.5 ohms d-c resistance between Power Control terminals No. 61 and No. 73 with all cubicle doors open.
11. Measure (with ohmmeter or bridge using less than 10 volt battery) the resistance at terminals of the following Rectox units. (Do not remove Rectox from circuit, since this is primarily a check of the associated circuit and not of the Rectox Units.) The resistance should be approximately as indicated.

| Unit | Term. | Res. |  |  | Term. |
| :--- | ---: | ---: | ---: | ---: | :---: |

12. Measure insulation resistance, using potential not less than 500 volts d-c, of high voltage conductors in power room.
a. Conductors from T-1501 to both high voltage rectox units.
b. Conductors from high voltage rectox units to filter capacitors and reactor.
c. Conductors from filter units to Modulation Transformer and Modulation Reactor.
d. Conductors from Modulator and Power Amplifier to Modulation Transformer and to Audio Auxiliary Choke. Do not disconnect leads from transmitter: Doors to Modulator and Power Amplifier cubicles must be closed.
e. Investigate any of above, a to d readings, if less than 50 megohms.
f. Connect automatic capacitor shorting switches on the three filter capacitors to the voltage bus with No. 28 bare copper wire. Bend the springs up so ends are level with the high voltage terminals. (Note: This fuse wire is supplied in the Installation Kit.)

## SWITCHGEAR ADJUSTMENTS

Before application of power the two type DB-25 circuit breakers S-2001 and S-2002, mounted in the Switchgear Enclosure should be withdrawn part way out of the enclosure using the extension rails and levering handle.

Inspect the two breakers with the aid of the inspection list furnished on page 7 of I.B.35-225-1, Check the overcurrent tripping devices for proper settings as follows:

1. Long time delay setting

| S-2001 | $100 \%$ of rated current |
| :--- | ---: |
| S-2002 | $80 \%$ of rated current |

2. Instantaneous settings
$\begin{array}{ll}\text { S-2001 } & 1000 \% \text { of rated current } \\ \text { S-2002 } & 1000 \% \text { of rated current }\end{array}$
The above adjustments are normally accomplished at the factory but should be checked prior to the application of power to the equipment. For details of adjustment, consult I.B. 35-225-1 pages 15 through 18.

## RELAY SETTINGS

1. Set overload relays as follows, and using battery, rheostat, and ammeter, check operating point by application of test leads to relay coil terminals. Do not remove shunting resistors.

| Symbol | Description | Scale Setting | Operating Point |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\times \mathrm{K}-9$ | 1500/3000 Volt | $5.5 \mathrm{amp} / 0.7$ | 4.5 | to | 5.5 |  |
| $\times \mathrm{K}-11$ | Modulator Rectifier | $9.5 \mathrm{amp} / 1.4$ | 8.5 | to | 9.5 |  |
| 入 K-12 | Power Amplifier Rectifier | $11.5 \mathrm{amp} \mathrm{i4}$ | 11.0 | to | 12.0 |  |
| $\times \mathrm{K}-105$ | 400 Volt | 0.4 amp 6 | 0.45 | to | 0.65 | amp |
| $\times$ K-106 | 813 RF | 0.6 amp 75 | 0.5 | to | 0.7 | al |
| K-107 $\times \mathbf{K}-108$ | Left 5736 RF | $1.4 \mathrm{amp} / .6$ | 1.05 | to | 1.35 | amp |
| Y K-108 | Right 5736 RF | $1.4 \mathrm{amp} /$ | 1.05 | to | 1.35 | amp |
| K-110 | Left 813 Audio | 0.15 amp | 0.14 | to | 0.16 | amp |
| K-111 | Right 813 Audio | 0.15 amp .16 | 0.14 | to | 0.16 | amp |
| K-114 | Left 5736 Audio | 0.25 amp , 3 | 0.5 | to | 0.7 | amp |
| $\mathrm{K}-115$ $\times \mathrm{K}-201$ | Right 5736 Audio | 0.25 amp , 3 | 0.5 | to | 0.7 | amp |
| ${ }^{\text {¢ }}$ K-202 | Left Modulator | 3.5 amp | 4.2 | to | 4.8 | amp |
| K-301 | Left Power Amplifier | 3.5 amp 3.0 amp 3.8 | 4.2 | to | 4.8 | amp |
| $\times \mathbf{K}-501$ | Right Power Amplifier | $3.0 \mathrm{amp} 3,8$ 3.0 amp | 4.4 4.4 | to | 4.8 4.8 | $\mathrm{amp}$ |

2. Set bias undervoltage relays:

| Symbol | Description | Scale Setting |
| :---: | :---: | :---: |
| X K-109 | Exciter | 90 volts |
| $\chi_{\chi} \mathrm{K}-112$ | Left Audio Driver | 50 volts |
| K-113 | Right Audio Driver | 50 volts |
| X K-203 | Left Modulator | 90 volts |
| $\times$ K-204 | Right Modulator | 90 volts |
| $\times \mathrm{K}-302$ | Left Power Amplifier | 60 volts |
| $\times \mathbf{K}-502$ | Right Power Amplifier | 60 volts |

I. B. $81-120-2 \mathrm{~A}$

## GAS FILLED CAPACITORS

Capacitors which are identified with symbols C-129, C-320, C-517 and C-520 are Lapp gasfilled, variable capacitors.

Observe the following precautions when handling these capacitors, (also refer to Lapp Bulletin 266 in the SUPPLEMENT section of this instruction book):

1. When first received:
a. Check for possible damages.
b. Check gauge pressure. This should be between 50 and 65 psi .
c. Measure safety gap spacing and record for future reference.
d. Check gauge pressure frequently to make no leaks.
2. Before installation:
a. If gauge pressure is between 50 and 65 , add oil pumped dry nitrogen to 150 .
b. If gauge pressure is below 50, add Freon gas ( $\mathrm{F}-12$ ) to 65 and then add oil pumped dry nitrogen to 150 .
c. Check safety gap spacing.
3. After installation:
a. Inspect periodically to see that the proper gauge pressure $(150 \pm 20)$ is maintained.
b. If gauge pressure is less than 85 , drain to 2.5 and refill to 65 with Freon ( $\mathrm{F}-12$ ) and then to 150 with oil pumped dry nitrogen.
c. If $\mathrm{g}_{\mathrm{g}}$ gauge pressure is 85 or more, refill to 150 with oil pumped dry nitrogen.
d. Keep ceramic bowl clean and dry.

## 4. Storage

a. See that the gauge pressure is between 100 and 150 so that the gaskets will be held in proper position to prevent leakage.

## RF COMPONENT SETTINGS

The following information is to be used as a guide in adjusting the Type 50HG-2 Transmitter for operation on a specific carrier frequency. At frequencies for which a choice of adjustments exists, either will be suitable.

1. Crystal Oscillator, Type FA
a. L-102

540 to 650 KC - connect tap 6 to tap 5
650 to 840 KC - connect tap 6 to tap 4
840 to 1300 KC - connect tap 6 to tap 3
1300 to 1600 KC - connect tap 6 to tap 2
b. L-103

540 to 650 KC - connect plate to 1 , output to 2
650 to 840 KC - connect plate to 2, output to 3
840 to 1000 KC -connect plate to 2, output to 4
1000 to 1300 KC - connect plate to 3 , output to 4
1300 to 1600 KC - connect plate to 4 , output to 4
2. 807 Buffer Amplifier
a. L-105

540 to 660 KC - use all sections
660 to 808 KC - short out one section (nearest panel)
808 to 985 KC - short out two sections (nearest panel)
985 to 1300 KC - short out two sections (nearest panel)
1300 to 1600 KC - short out three sections (nearest panel)
3. 813 RF Plate Tank
a. L-109

540 to 660 KC - use all (62) turns


X 660 to 800 KC - short out 7 turns on each end
800 to 900 KC - short out 11 turns on each end
900 to 1020 KC - short out 15 turns on each end
1020 to 1300 KC - short out 19 turns on each end
1300 to 1600 KC - short out 23 turns on each end
b. L-109-Grid tap and neutralizing tap

540 to $660 \mathrm{KC}-17$ turns above and below center tap
660 to $800 \mathrm{KC}-15$ turns above and below center tap
800 to $900 \mathrm{KC}-13$ turns above and below center tap
900 to $1000 \mathrm{KC}-11$ turns above and below center tap
1000 to $1100 \mathrm{KC}-9$ turns above and below center tap
1100 to $1300 \mathrm{KC}-7$ turns above and below center tap
1300 to $1400 \mathrm{KC}-6$ turns above and below center tap
1400 to $1600 \mathrm{KC}-5$ turns above and below center tap
4. 5736 Plate Tank
a. L-112 - Tap location

540 to 600 KC - 13-3/4 turns from ground
600 to $660 \mathrm{KC}-12-3 / 4$ turns from ground
660 to $800 \mathrm{KC}-12-3 / 4$ turns from ground
800 to $1000 \mathrm{KC}-12-3 / 4$ turns from ground 1000 to $1300 \mathrm{KC}-11-3 / 4$ turns from ground 1300 to $1500 \mathrm{KC}-10-3 / 4$ turns from ground 1500 to $1600 \mathrm{KC}-8-3 / 4$ turns from ground
b. $\mathrm{C}-129$ - A

540 to 600 KC - use 4 adders $560 \mu \mu \mathrm{f}$ each
600 to 660 KC - use 3 padders $560 \mu \mu \mathrm{f}$ each
660 to 800 KC - use 2 adders $560 \mu \mu \mathrm{f}$ each
800 to 1000 KC - use 1 badder $560 \mu \mu \mathrm{f}$ each
1000 to 1600 KC - none
5. Left and Right Power Amplifier Grid Circuit
a. L-301 or L-501

540 to 600 KC - use all turns
600 to 660 KC - short out 2 turns
660 to 800 KC - short out 7 turns
800 to 1000 KC - short out 13 turns
1000 to 1300 KC - short out 15 turns
1300 to 1600 KC - short out 18 turns
6. Left and Right Power Amplifier Neutralizing Circuit
a. L-303 and L-503 - See Power Amplifier Neutralization

540 to 660 KC - total turns 196
660 to 1000 KC - total turns 156
1000 to 1600 KC - total turns 96
7. Power Amplifier Plate Tank
a. $\mathrm{L}-401-\mathrm{A}$

540 to 750 KC - use all turns
750 to 800 KC - short out one turn each end of coil
800 to 1000 KC - short out two turns each end of coil
1000 to 1200 KC - short out three turns each end of coil
1200 to 1500 KC - short out four turns each end of coil
1500 to 1600 KC - short out five turns each end of coil
b. C-320-A and C-520-A

540 to 800 KC - one $450 \mu \mu \mathrm{f}, 45 \mathrm{KV}$ Capacitor

## POWER-ON ADJUSTMENTS

## WARNING

THE USE OF HIGH VOLTAGES IS NECESSARY FOR THE OPERATION OF THE ELECTRONIC EQUIPMENT COVERED BY THESE INSTRUCTIONS. WHILE ALL PRACTICAL SAFETY PRECAUTIONS HAVE BEEN INCORPORATED IN THE DESIGN OF THIS EQUIPMENT, THEY ARE NOT INFALLIBLE; THEREFORE, ALL PRECAUTIONARY MEASURES MUST BE CAREFULLY OBSERVED BY THE OPERATING PERSONNEL DURING THE OPERATION, INSPECTION AND MAINTENANCE OF THE EQUIPMENT. SEE WARNING IN THE FRONT OF THIS BOOK.

## POWER LINE VOLTAGE

Apply 460 volts a-c to Switchgear. All De-ion switches should be off and all control switches turned to left (if no duplicate controls have been connected). Observe that the line voltage meter reads 460 volts, and the line current meters reads zero.

## BLOWERS

Turn on as follows:

1. Turn S-30 (BLOWER CONTROL) to BLOWER ONLY position.
2. Turn S-29 (BLOWER SELECTOR) to No. 1 position.
3. Close S-9 (SWITCHGEAR CONTROL BUS).
4. Turn S-28 (BUS BREAKER) on. Observe:
a. Indicator I-40 (BUS BREAKER SWITCH ON) lights.
b. Blower No. 1 starts; check direction of rotation.

If not same as arrow on blower housing, reverse two leads on blower motor.
c. After Blower No. 1 comes up to normal speed, S-515 (air flow interlock) operates allowing I-36 (BLOWER NO. 1 ON) to light.
5. If a spare blower has been purchased, turn BLOWER SELECTOR to NO. 2 position. Observe: Blower No. 2 starts; check direction of rotation. I-41 (BLOWER NO. 2) lights.

## AIR VELOCITY

1. Measure air velocity at following points using an integrating vane-type anemomett * such as the four-inch diameter "CENCO" anemometer, (Central Scientific Co., Chicago, Ill. Cat. No. 78605).

Measurements on the power tubes should be the average of maximum readings around the tube with the instrument held horizontal just above the radiator fins and midway between the glass bulb and the outside edge of the radiator. The Rectox units must be installed, all tubes in tube sockets, all cubicle doors must be closed, and exhaust ducts in normal condition when measurements are taken.

| Location | Component | Minimum Velocity, Fpm |
| :---: | :---: | :---: |
| Power Control | RX-1 | 1000 |
| Exciter | RX-104 | 800 |
| Modulator | Each WL-5671 | 1000 l/w |
| Left Power Amplifier | Each WL-5671 | 10001025 |
| Left Power Amplifier | RX-301 | $800{ }^{1025}$ |
| Right Power Amplifier | Each WL-5671 | $1000 / 800$ |
| Right Power Amplifier | RX-501 | $800$ |

2. Remove one 5736 tube from its socket on the left side of the Exciter and measure air velocity to be 800 fpm minimum. Replace tube and remove one 5736 from right side and measure air velocity to be 800 fpm minimum.
3. Orient the air nozzles in the Modulator, Left Power Amplifier and Right Power Amplifier cubicles so that air is directed on the 5671 tube filament seals.
4. If necessary, change speed of Blowers by adjusting "Vari-Pitch" sheave or install baffles to meet above minimum air requirements.

## DISTRIBUTION BUS

Check that primary switch positions on T-1502-A, B, C are all on position 3. Positions 1 and 5 are $\pm 5$ percent and positions 2 and 4 are $\pm 2-1 / 2$ percent. Switches are mounted on transformers, under top cover plates.

1. Turn BLOWER CONTROL to TRANSMITTER AND BLOWER position. Observe:
a. The Distribution Bus Breaker closes. (Do not allow breaker to "pump." If abnormal operation is encountered, see Switchgear Instruction Book I. B. 35-225-1 in SUPPLEMENT Section.)
b. I-35 (BUS BREAKER ON) lights.
c. M-4 (BUS VOLTAGE) indicates 230 volts on each of the three phases selected by S-18 (BUS METERS PHASE SELECTOR). Note that if the phase voltages are not in balance, throw S-19 (BUS REGULATOR SELECTOR CONTROL) to MANUAL position; throw S-22 (BUS REGULATOR) to its ON position; hold S-20 (BUS REGULATOR MANUAL CONTROL) in its LOWER position until both regulators have reached their lower limit positions and all three phases are balanced. Next, hold S-20 in its RAISE position until all three phases show 230 volts.
d. With S-19 in AUTOMATIC position, note that the bus voltages on each of the three phases are equal ( 230 volts). See Regulator Instruction Book 5521-A for adjustment of regulator relays in case the three phases are unbalanced or not 230 volts.

## FILAMENT VOLTAGES

1. Throw S-12 (EXCITER FILAMENTS) to ON position. Observe:
a. K-8 (Exciter filament undervoltage) timing relay begins to operate and should close after a 22 -second delay, lighting I-42 (EXCITER FILAMENT NORMAL VOLTAGE) indicator. Note that K-8 should be adjusted to close in 22 seconds and drop out in 5 seconds. See Instruction Leaflet 41-291D in SUPPLEMENTS Section of this book.
b. The Exciter filament transformers should be energized.
2. Voltages at the filament terminals of the following tube sockets: (bus voltage 230 volts)

|  | Without Tubes | With Tubes |
| :---: | :---: | :---: |
| Audio WL-807 | 6.3 to 6.6 volts | 6.1 to 6.3 volts 6,3 |
| RF WL-807 | 6.3 to 6.6 volts | 6.1 to 6.3 volts 6.2 |
| Audio WL-813 | 10.0 to 10.4 volts | 9.7 to 10.3 volts 10.0 |
| RF WL-813 | 10.0 to 10.4 volts | 9.7 to 10.3 volts 10.0 |

3. Voltages at all 5736 filament connectors:

|  | Filaments Not <br> Connected |  | Filaments <br> Connected |
| :--- | :---: | :---: | :---: |
| Audio WL-5736 | 5.9 to 6.5 volts |  | 5.7 to 6.3 volts 5.8 |
| RF WL-5736 | 5.9 to 6.5 volts | 5.7 to 6.3 volts 5.7 |  |

4. Modulator and Power Amplifier filament voltages.
a. Make sure that filament connectors are not touching filament terminals of 5671 tubes in Modulator, Left Power Amplifier, Right Power Amplifier.
(1) Turn ON all filaments in Modulator, Left Power Amplifier and Right Power Amplifier.
(2) Observe, using filament voltmeter selector switch on each cubicle, that each voltage is 10 to 11 volts.
(3) Try combinations of Power Amplifier Filament Switches, S-1, 2, 3, 4. Check voltages to be same as above.
(4) Turn Bus Breaker OFF and connect all 5671 filaments.
(5) Repeat (1), (2), (3) above, and observe each filament voltage to be between 9.6 and 10.2 volts. (Bus voltage 230 volts on all three phases.) Using an accurate laboratory-type voltmeter, measure voltage at filaments of the 5671 tubes. Adjust the indication on $\mathrm{M}-202, \mathrm{M}-301, \mathrm{M}-501$ to be the same as the laboratorytype voltmeter (adjust zero set screw). Do this after the set has been checked and operated long enough for voltmeters to have reached operating temperature.

## EXCITER BLAS AND PLATE VOLTAGES

Adjust Bus Voltage to be 230 volts.

## 1. Audio Bias

Close S-13 (AUDIO BIAS). Turn on S-31 (AUDIO BIAS). Observe:
a. I-43 (AUDIO BIAS SWITCH ON) lights, (amber).
b. K-37 (audio bias contactor) operates.
c. M-111 (LEFT 5736 AUDIO DRIVER BIAS), 130 volts - adjusted by R-119.
d. M-112 (RIGHT 5736 AUDIO DRIVER BIAS), 130 volts - adjusted by R-120.
e. M-116 (LEFT MODULATOR BIAS), 330 volts - adjusted by S-108.
f. M-117 (RIGHT MODULATOR BIAS), 330 volts - adjusted by S-109.
g. The following undervoltage relays operated, and bias ON indicators light.

K-112, I-38, Power Control AUDIO BIAS ON (red)
K-113, I-403, Center Power Amplifier AUDIO BIASES ON (green)
K-203, K-204, I-202, Modulator BIAS (green)
2. $R F$ Bias

Close S-14 (RF BIAS). Turn on S-32 (RF BIAS). Observe:
a. I-44 (RF BIAS SWITCH ON), (amber).
b. K-38, RF bias contactor operates.
c. M-302 (LEFT PA GRID VOLTS), 340 to 360 volts.
d. M-502 (RIGHT PA GRID VOLTS), 340 to 360 volts.
e. K-109 (exciter bias undervoltage) closes, I-39 (RF BIAS ON), (red) and I-404 (RF BIASES ON), (green) light.
f. K-302 (left power amplifier bias undervoltage) closes, I-302 (BIAS), (green) lights.
g. K-502 (right power amplifier bias undervoltage) closes,I-502 (BIAS), (green) lights.
h. Using a d-c voltmeter, observe 300 to 400 volts negative from RF 5736 tube grids to ground.
3. 400 Volt Supply

Close S-15 ( 400 VOLT SUPPLY) on Power Control Panel. Turn on S-103, ( 400 VOLT SUPPLY) switch on Exciter Control Panel. Observe:
a. I-105 (amber) lights. (SWITCH ON).
b. K-39 closes - contactor, 400 -volt supply.
c. I-106 (red) lights - (POWER ON).
d. M-118 (400 VOLT RECTIFIER) indicates between 440 and 460 volts.

14 mae. M-101 (OSCILLATOR CATHODE CURRENT) indicates between 10 and 14 milliamperes. Note that as the oscillator is tuned through resonance by adjusting C-105, that the 802 cathode current goes through a sharp dip, a gradual rise and then a sharp rise.
f. M-102 (807 RF BUFFER CATHODE CURRENT) indicates between 35 and 55 ma . Tune to minimum with $\mathrm{C}-112$ (plate tank capacitor).
g. M-103 (813 RF AMPLIFIER TOTAL GRID CURRENT) indicates between 14 and 18 ma .
4. 1500 Volt Supply

Put S-110 in OPERATE and S-111 in TUNE and put S-113 in OPEN position. Close S-16 ( 1500 VOLT - 3000 VOLT SUPPLY) in Power Control. Turn on S-104 (1500-3000 VOLT RECTIFIER) on Exciter Control Panel. Observe:
a. I-107 (green) lights (SWITCH ON).
b. K-40 closes - contactor, 1500-3000 volt supply.
c. I-108 (red) lights - (POWER ON) and K-104 operates 807 and 813 screen interlock relay).
d. Using S-106 ( 813 RF AMPLIFIER PLATE TUNING), tune for maximum reading on M-108 (1500 VOLT RECTIFIER).

## RF DRIVER NEUTRALIZATION

1. Turn off 1500-3000 VOLT RECTIFIER and couple a wavemeter, or some other RF indicating device to the RF 5736 plate tank ( $L-112$ ). A suggested method is to use link coupling, with one $6^{\prime \prime}$ turn on each end of link, and place the wavemeter outside the cubicle.
2. Remove cable plugs (RG-17/U from sockets on top of cubicle.
3. Turn on 1500-3000 VOLT RECTIFIER and adjust S-107 (5736 RF DRIVER PLATE TUNING) for maximum indication on wavemeter.
4. Readjust 813 RF AMPLIFIER PLATE TUNING for maximum indication on wavemeter.
5. Adjust neutralizing capacitor ( $\mathrm{C}-122$ ) for minimum indication on wavemeter. (A piece of cord may be wrapped around the sleeve of C-122 to permit adjustment from outside the cubicle.)
6. Place S-111 in OPERATE position and repeat 3, 4, and 5 above.

## MAIN RECTIFIER REGULATOR OPERATION

When a Main Rectifier Regulator (YR-1201) is supplied with $50 \mathrm{HG}-2$ equipment, power wiring should be according to figure 43 and control circuit wiring according to figure 42.

1. With S-421 (MAIN RECTIFIER CONTROL) in the off position, YR-1201 has run down to minimum position and the DELTA-WYE contactors are deenergized. No power is applied through the switchgear breaker, S-2002.
2. With switch S-421 in the "TUNE" position, power is applied to the primary of T-1501 through the WYE contactor. The regulator will automatically run up to a predetermined voltage when S-411 (REGULATOR CONTROL SELECTOR) is in the "AUTOMATIC" position.

With S-411 in the "MANUAL" position, the regulator is controlled by S-412 (MANUAL VOLTAGE CONTROL) and any desired voltage in the range 6 to 10 kv approx. may be obtained.
3. With switch S-421 in the "ON" position, power is applied to the primary of T-1501 through the "DELTA" contactors. If $\mathrm{S}-411$ is in the "AUTOMATIC" position when going from "TUNE" to "ON", the regulator will have reached its "HIGH LIMIT" and the increase in voltage is brought about by the change in transformer primary connections from WYE to DELTA. If S-411 is in the "MANUAL" position when S-421 is placed in the "ON" position, any desired voltage in the range 9 kv to 12 kv approx. may be obtained.

## MAIN RECTIFIER REGULATOR ADJUSTMENTS (IF USED)

1. Remove conductors from primary terminals of T-1501 (Main Rectifier Plate Transformer).
2. Connect secondary links on Main Rectifier Plate Transformer from No. 4 to No. 6 on all three phases.
3. Place S-411 (REGULATOR CONTROL SELECTOR) in MANUAL position.
4. Release brake on YR-1201 (Main Rectifier Induction Voltage Regulator).
5. By hand, rotate regulator to full LOWER position (full counterclockwise on regulator LOWER-RAISE dial). Observe:

> I-407 (LOW LIMIT) indicator on Center Power Amplifier Control Panel lights.
6. Rotate regulator to full RAISE position (full clockwise on regulator LOWER-RAISE dial). Observe:

> I-408 (HIGH LIMIT) indicator on Center Power Amplifier Control Panel lights.
7. Rotate regulator to mid-range (zero on LOWER-RAISE dial).
8. Set brake on regulator.
9. Block the undervoltage relay on the primary relay panel of regulator in the closed position. This can be done by inserting insulating material between the righthand contact (as seen from the front) and the movable contact, and then screwing up the adjustments on the contacts until the movable contact is firmly against the lefthand contact of the undervoltage relay.
10. Close VRS-1201 (De-ion breaker mounted on side of regulator).
a. If motor runs the regulator toward RAISE, immediately open breaker and interchange two leads from the regulator motor. (Terminals for the motor are under the limit switch cover.)
b. Close breaker and allow motor to run regulator down to lower limit and stop.
11. Turn S-421 (MAIN RECTIFIER CONTROL) ON. Observe:
a. I-406 (green) lights - (SWITCH ON).
b. K-1601 and K-1602 (Modulator bleeder contactors on Rectox Frame) operate.
c. S-2002 (Main Rectifier Breaker in Switchgear) closes.
d. I-203 (PLATE), I-303 (PLATE), I-405 (MAIN RECTIFIER POWER ON), I- 503 (PLATE) (all red) light on Modulator, Left Power Amplifier, Center Power Amplifier, and Right Power Amplifier, respectively.
e. Determine that three phase output voltage of Main Rectifier Regulator is between 350 and 380 and that all three phase voltages are equal.
12. Operate S-412 (MANUAL VOLTAGE CONTROL) and determine that regulator runs in proper direction.
13. Turn MAIN RECTIFIER CONTROL off and observe that regulator runs downto lower limit stops.
14. Turn MAIN RECTIFIER CONTROL on and S-411 (VOLTAGE CONTROL SELECTOR) to AUTOMATIC and observe that regulator setting is under control of R-417 (AUTOMATIC VOLTAGE CONTROL).

## MAIN RECTIFIER POWER ADJUSTMENTS

1. Remove conductors from primary terminals of T-1501 (Main Rectifier Plate Transformer).
2. Connect secondary links of Main Rectifier Plate Transformer from No. 4 to No. 6 on all three phases.
3. Turn S-421 (Main Rectifier Control) to the TUNE position. Observe:
a. I-406 (green) lights - (SWITCH ON).
b. K-1601, K-1602 (bleeder contactors in Rectox Frame) operate.
c. K-1503 in High Voltage Transformer operates connecting primaries in Wye.
d. S-2002 (Main Rectifier Breaker in switchgear) closes.
e. I- 203 (PLATE), I-303 (PLATE), I-405 (MAIN RECTIFIER POWER ON), I-503 (PLATE), (all red) light on Modulator, Left Power Amplifier, Center Power Amplifier, and Right Power Amplifier, respectively.
4. Repeat 3 above except turn S-421 to the ON position and in (c) K-1501 and K-1502 should close in sequence connecting the Transformer primaries in Delta.

## FINAL TUNE-UP

1. Replace primary leads on Main Rectifier Plate Transformer.
2. Protective gap settings:
a. Set the protective gap on the Modulator Reactor to 0.2 inch. A number 8 or 13/64 straight shank twist drill may be used as a gauge. Set the protective gaps on the Modulation Transformer to 0.15 inch each. A No. 25 or $5 / 32$ straight shank twist drill may be used as a gauge. These are initial settings. If sparking of the gaps occurs during program operation, each gap may be opened up an additional .05 inch.
b. Set the two protective ball gap assemblies in the Rectox Frame to $1 / 16$ inch each
3. Set up for audio input level, response, distortion and modulation measurements as follows: a. Obtain sample of carrier for modulation monitor and distortion analyzer from two separate lines each connected across a portion of the end ring on the PA inductor L-401.
b. Using a Western Electric Type 111-C (or equivalent) repeat coil for isolation between a 500 ohm attenuator and the input of the transmitter, read level in dbm with volume indicator meter on the audio oscillator side of the attenuator. This applies to all audio input level and audio response measurements.
4. Turn MAIN RECTIFIER CONTROL to tune. Power Amplifier plate volts should be approximately 8.1 kv . Tune Power Amplifier for minimum plate current indicated on M-402 (TOTAL PA PLATE CURRENT).
a. Observe:
(1) M-415 (LOAD CURRENT) 10.6 to 11.0 amperes RF (230 ohm load).
(2) M-304, M-413 (LEFT POWER AMPLIFIER PLATE CURRENT) 1.7 to 1.8 amperes.
(3) M-504, M-414 (RIGHT POWER AMPLIFIER PLATE CURRENT) 1.7 to 1.8 amperes
(4) M-203 (MODULATOR PLATE VOLTS) 9.7 to 10 kv .
b. Adjust C-101 in the Type FA Crystal Oscillators for correct carrier operating frequency. The shaft of $\mathbf{C - 1 0 1}$ (screwdriver adjustment) is accessible through holes in the RF door of the Exciter. The range of C-101 is approximately $\pm 30$ cycles.
c. Reduce MODULATOR BIAS until the tubes draw 0.1 amperes plate current each.
d. Apply 1000 cycle tone to transmitter input at a level of about -14 dbm in order to produce 50 percent modulation of the carrier.
e. Allow transmitter to run at this level for 15 minutes. During this period an occasional Modulator or Power Amplifier plate overload may occur with no apparent reason. If no other abnormal indications are encountered, it may be assumed that the interruptions are "gas flashes" in the WL-5671 tubes.
f. At the end of the 15 minute run, shut down the transmitter completely, including blowers. Inspect and feel all components for indications of abnormal operation or heating. Inspect and feel metal rectifiers, including all stacks of the Modulator and Power Amplifier Rectox Units.
5. If no overloads occurred in e. above, switch main rectifier control to ON and readjust MODULATOR BIAS so that tubes draw 0.2 amperes each with modulation.
a. Modulate 50 percent with 100 cycle tone for 15 minutes. Repeat f . above. If more than one gas flash occurs in a 10 minute period, the run must be extended until the gas "cleans up." Note that with all feedback disconnected, the carrier envelope as seen on an oscilloscope will be considerably distorted. At 11.5 kv on M-401 (POWER AMPLIFIER PLATE VOLTS), observe:
(1) LOAD CURRENT 14.7 amp . RF (230 ohm load). Operate $\mathrm{S}-405$ (OUTPUT COUPLING) as required to give 50 kw output.
(2) LEFT POWER AMPLIFIER PLATE CURRENT 2.55 amp maximum, and equal to Right Power Amplifier plate current.
(3) RIGHT POWER AMPLIFIER PLATE CURRENT equal to Left Power Amplifier plate current.
Note: The plate currents for (2), (3) above must be obtained with equal (or within 3 percent of average) capacitance in C-320 and C-520. Check capacities after tuning to maximum plate efficiency.
(4) M-402 (TOTAL PLATE CURRENT) 5.1 amp maximum.
(5) M-203 (MODULATOR PLATE VOLTS) 13.4 to 13.8 kv .
(6) M-201 (LEFT MODULATOR PLATE CURRENT), M-204 (RIGHT MODULATOR PLATE CURRENT) 0.2 amp each. Operate $\mathrm{S}-108$ and S-109 (LEFT AND RIGHT MODULATOR BIAS) switches on Exciter control panel to give 0.2 amp Modulator plate current each.
(7) M-404 (TOTAL TRANSMITTER INPUT POWER) 98.5 to 103.5 kw .
b. Apply 1000 cps sine tone to the input of the transmitter to give 85 percent modulation. Observe:
(1) Modulator plate currents do not differ from each other by more than 0.2 amps .
c. Repeat (b) except use 50 cps sine tone modulation.
d. Repeat (b) except use 7500 cps sine tone modulation.
e. Input level for 50 percent modulation at 1000 cps should be between -12 and -14 dbm .
6. Shut down all power and bias supplies and:
a. Reconnect wire to TS-125 terminal 325 (audio relay removed in Low Level Audio Adjustments, 807 Stage).
b. Reconnect wires TS-126, terminal 340, and terminal 342. Remove grounds from terminals 340 and 342.
7. Turn on transmitter, observe same conditions as in 5 a above.
a. Apply 1000 cycle sine tone to the input of the transmitter at an input level of +8.6 dbm . Adjust voltage feedback potentiometers R-1117 and R-1118 until Modulator plate currents are equal at 85 percent modulation. Observe that:
(1) The noise level is better than 60 db below 100 percent modulation.
(2) The modulation capability is at least one hundred percent from 50 to 7500 cycles.
(3) The frequency response from 30 to 10,000 cycles is uniform within $\pm 1 \mathrm{db}$.
(4) The distortion is less than 3 percent up to 95 percent modulation from 50 to 7500 cycles.
(5) The carrier shift is less than 5 percent for 100 percent modulation at 1000 cycles.

## ANTENNA ARC INTERRUPTER ADJUSTMENTS

1. Disconnect lead from Center Power Amplifier TS-408, terminal 114 and from the tower tuning RF Current Transformer-Rectifier Unit.
a. Measure capacitance to ground of the above lead.
b. Obtain fixed paper or mica capacitor, 600 volt rating, within 10 percent of above measured value and connect the capacitor between terminals 359 and 362 on TS-414 in the Center Power Amplifier.
2. Replace leads removed in 1 above. Note: If station does not employ pattern change, place permanent jumper between terminals 111 and 112 of TS-408.
3. Remove Antenna Arc Interrupter Unit from Center Power Amplifier.
a. Turn ARRAY BALANCE, ANTENNA BALANCE, and LINE BALANCE controls full counterclockwise.
b. Connect Interrupter Unit to Center Power Amplifier by means of the extension cable supplied.
c. Turn on transmitter ( 50 kw carrier).
d. Turn S-409 (OFF-CALIBRATE-OPERATE) to CALIBRATE.
4. With d-c voltmeter of $1 / 4$ megohm or more resistance, observe 75 to 100 volts icross R-1405 (LINE BALANCE) and across R-1403 (ANTENNA BALANCE). The two voltages must be of same polarity. If not, reverse output leads on tower tuning RF Current transformer-rectifier. If voltages are not between 75 and 100 volts, adjust tap switches on RF Current transformer-rectifier Units to bring them within the above range.
5. Observe:
a. Clockwise rotation of $\mathrm{R}-1405$ (LINE BALANCE CONTROL) causes M-1401 (BALANCE INDICATOR) to deflect, and that with S-1401 (METER SHUNT) button depressed, a deflection of 300 microamperes causes K-1401 (sensitive relay) to close, which closes K-1402 and lights J-401 (ANTENNA SYSTEM UNBALANCE).
b. Similarly, deflecting the BALANCE INDICATOR 300 microamperes in the opposite direction by turning ANTENNA BALANCE CONTROL, should cause the same operations as in a. above.
c. If station employs pattern change, switch ANTENNA ARRAY to DIRECTIONAL, and note action similar to above with R-1404 (ARRAY BALANCE).
d. Increase sensitivity by turning all controls clockwise, keeping BALANCE INDICATOR near zero.
6. Turn OFF-CALIBRATE-OPERATE switch to OPERATE and observe that a 300 mic roampere unbalance causes momentary interruption of the carrier and lights I-26 (ANTENNA ARC-OVER). Note that if the unbalance is done deliberately by turning one of the controls, the transmitter will be keyed on and off at a rapid rate which may cause one or more overloads to operate if allowed to continue for more than about one second. In normal operation, the cause of an unbalance is removed by momentary inter ruption of the carrier.

## NOISE, FEEDBACK, DISTORTION, AND RESPONSE

## NOISE

1. Power Amplifier

Carrier noise is caused mainly by a-c heating of the Power Amplifier filaments. It is minimized in the 50HG-2 by:
a. Operating the Left Power Amplifier filaments and Right Power Amplifier filaments iquadrature.
b. Current feedback.
c. Adequate grid drive.
d. Symmetry of the Power Amplifier - (circuit balance).

With normal meter indications as listed in the Section on MAINTENANCE, Normal Meter Readings with the Modulator tube plates connected together, the carrier hum should be better than 60 db below 100 percent modulation. With Modulator tubes darkened and with the plates not connected together, the carrier hum should be better than 60 db below 100 percent modulation.

## 2. Modulator

Modulator noise is caused by a-c heating of the tube filaments, and is minimized k
a. In-phase operation of filaments and out-of-phase operation of plates (push-pull).
b. Symmetry of Modulator circuit (plate current balance, uniformity of tubes).
c. Voltage feedback.

With Modulator grids connected together, the carrier noise should be better than 54 dbb low 100 percent modulation.
3. Exciter
a. RF Amplifier: The RF amplifiers in the Exciter operate Class C, and do not contribute appreciable hum.
b. 5736 Cathode Follower Audio Stage: The large amount of inherent inverse feedback ? vided by the cathode follower circuit suppresses hum originating within this s
c. 813 Audio Stage: Filament hum is reduced by negative feedback within the stage by the use of a cathode resistor. The hum measured between an 813 plate and ground with the modulator tubes dark, should be less than 3 volts rms.
d. 807 Audio Stage: Very little carrier noise should be contributed by this stage. the tubes, however, must have no loose elements or heater-cathode leakage. A cathode resistor provides negative feedback.

## POWER SUPPLY RIPPLE VOLTAGES

With a 60 cycle supply and normal operating loads, the ripple voltages should be approximately as shown below:

Left 5736 Audio Bias<br>Right 5736 Audio Bias<br>Left Modulator Bias<br>Right Modulator Bias<br>400 Volt Supply<br>Exciter RF Bias<br>1500 Volt Supply<br>3000 Volt Supply<br>Left Power Amplifier Bias Supply<br>Right Power Amplifier Bias Supply<br>Modulator Plate Supply ( 0.4 amp load)<br>Power Amplifier Plate Supply (5.0 amp load)

> 0.02 volts rms
> 0.02 volts rms
> 0.03 volts rms
> 0.03 volts rms
> 0.04 volts rms
> 0.12 volts rms
> 0.70 volts rms
> 1.2 volts rms
> 0.10 volts rms
> 0.10 volts rms
> $10 \quad$ volts rms
> 100 volts rms
> (out of rectifier)

## VOLTAGE FEEDBACK

Voltage feedback is most effective at frequencies greater than 400 cycles. Voltage feedback is used to reduce noise and distortion appearing at the plates of the modulator tubes.

Enough feedback is used at the hum frequencies to bring the hum output of the Modulators well below the power amplifier filament hum.

## CURRENT FEEDBACK

Current feedback is most effective at frequencies below 400 cycles. The change from voltage to current feedback in the feedback loop is accomplished by a cross-over network such that flat overall frequency response within the audio system is maintained, eliminating the need for equalizing.

Current feedback also eliminates instability in the audio system such as may be caused by lieavy low frequency modulation (below 30 cps ).

Turntable rumble, program amplifier "thumps," antenna arcs are familiar examples of low frequency phenomena which cause audio instability and overloads.

This audio stability is accomplished by taking the sample of current feedback from the primary side of the modulation transformer. Then in the event of heavy low frequency modulation, the magnetizing current which tends to saturate the transformer and cause overloads is limited by the "eedback loop.

## ISTORTION

1. In a correctly adjusted transmitter, the chief reasons for distortion are:
a. Shift of Modulator plate supply voltage with modulation level. The effect of the Modula tor plate voltage change is minimized by utilizing the increase in driver cathode current to change the operating bias on the modulator tubes.
b. Modulator driver regulation.

Each of the above reasons cause "symmetrical" or even-order harmonic distortion since תe same effect occurs during each half cycle. The first (a) may be seen at medium audio frequencies on the modulation envelope as a slight departure from a sine wave at the abscissa. The econd (b) is evidenced as a slight flattening of sine wave peaks.
2. If the two sides of the audio system do not have the same gain, "non-symmetrical" distortion will be produced as evidenced by inequality between positive and negative modulation peaks. Distortion from this source is minimized by symmetry of circuit components and by proper set-up of the audio system to compensate for non-uniformity of tubes.
3. Insufficient emission capability of the Power Amplifier tubes can cause distortion due to flattening of positive modulation peaks.

## FREQUENCY RESPONSE

The frequency response between 30 and 10,000 cycles is controlled mainly (1) by the characteristics of the voltage and current feedback divided networks, (2) by the "step circuit" network consisting of C-163 and R-143 or C-164 and R-144 for high frequencies and R-145 and C-1105 or R-146 and C-1106 for low frequencies of the grid of the second audio stage.

The input level in dbm required to produce 50 percent modulation in a representative $50 \mathrm{HG}-2$ is as follows:

Current and
Feedback
Connected
$+5.9 \mathrm{dbm}$
$+5.4 \mathrm{dbm}$
$+5.5 \mathrm{dbm}$
$+5.8 \mathrm{dbm}$
$+5.4 \mathrm{dbm}$
$+4.8 \mathrm{dbm}$
$+4.4 \mathrm{dbm}$
$+4.0 \mathrm{dbm}$
$+4.0 \mathrm{dbm}$
$+4.0 \mathrm{dbm}$
$+5.0 \mathrm{dbm}$

Voltage Feedback Disconnected

- 3.8 dbm
- 7.8 dbm
$-10.5 \mathrm{dbm}$
$-12 \mathrm{dbm}$
$-12.1 \mathrm{dbm}$
$-12.1 \mathrm{dbm}$
$-11.6 \mathrm{dbm}$
$-10 \mathrm{dbm}$
- 9 dbm
- 6.5 dbm
- 4.2 dbm


## CONTROL CIRCUITS

## FUNDAMENTAL CONTROL SCHEMATIC DIAGRAM

The Fundamental Control Schematic, figure 47, should be used as a reference in following the operation of the control circuits. Information pertinent to this diagram follows:

1. All switches are shown in the OFF position. All power is off.
2. All relays and contactors are shown deenergized. A normally closed contact is designated by a diagonal line through the contact.
3. All door and enclosure interlock switches are shown in the "door open," or "enclosure open" position.
4. The air interlock switch, S-515, is open.
5. Reference numbers that appear on coils, contacts, switches, etc., also appear on the same component terminals or are terminal board numbers in the wiring diagrams. This makes it possible to correlate points on the control schematic with terminals or terminal board connections in the transmitter cubicles themselves.

## THE TURN-ON SEQUENCE

With all switches on the upper Power Control Panel turned ON except SWITCHGEARCONTROL BUS, TRANSMITTER CONTROL BUS, and the filament switches for the spare Modulator and Power Amplifier Tubes, the turn-on sequence is as follows:

| S-9 | SWITCHGEAR CONTROL BUS | S-11 | TRANSMITTER CONTROL BUS |
| :--- | :--- | :--- | :--- |
| S-30 | BLOWER CONTROL (This will | S-31 | AUDIO BIAS |
|  | nOrmally be left in the | S-32 | RF BIAS |
|  | TRANSMITTER AND BLOWER | S-103 | 400 VOLT RECTIFIER |
| position) | S-104 | $1500-3000$ VOLT RECTIFIER |  |
| S-28 | BUS BREAKER | S-410 | MAIN RECTIFIER CONTROL |

The manner in which the above sequence is maintained can be followed on the Fundamental Control Schematic, figure 47. This is facilitated by the dotted lines which connect each relay or contactor coil to all of its contacts.

ACTION ON SUSTAINED FAULT
The sequence is as follows:
With S-27 in AUTOMATIC position, assume that K-301, L PA overload has operated due to excessive plate current.

1. K-16, Main Master overload operates.
2. K-7, Main Rectifier Breaker Auxiliary, is deenergized.
3. K-7 normally closed contacts energize trip coil of S-2002, the Main Rectifier Breaker.
4. S-2002 opens.
5. S-2002 normally closed contact energizes K-2014 (MG-6 in Switchgear Cubicle).
6. K-2014 normally open contact energizes K-47, Stepping Switch Auxiliary No. 1.
7. K-47 normally open contact energizes step coil of $\mathrm{K}-13$, stepping switch and $\mathrm{K}-13$ advances one step.
8. K-13 normally open contact closes.
9. K-4, Time Delay, starts.
10. Removal of power by S-2002 will remove the overload and allow K-301 to drop out.
11. K-16 opens, closing K-7, energizing the breaker pull-in coil "CC" in the Switchgear. When breaker is nearly closed, a normally open breaker auxiliary contact energizes the "anti-pump" relay K-2008, which in turn opens the circuit to the pull-in coil "CC" which no longer needs to be energized since the breaker latches in mechanically. With the breaker closed, the Main Rectifier is again connected and the transmitter is returned to operation. The function of switches S-2010 and S-2011 is to allow the breaker toggle mechanism to reset before the closing coil is re-energized. This is accomplished by keeping K-2008 energized through switch S-2013 until the closing coil plunger reaches the bottom of its travel, thus opening switch S-2012 and allowing the closing coil to be energized.
12. Application of power again operates overload relay $\mathrm{K}-301$ if the fault condition is still present and the above sequence ( 1 to 11) is repeated ( $\mathrm{K}-13$ advancing one step each time) until the arms on $\mathrm{K}-13$ reach the fourth contact. Then:
13. K-16 is locked in by its own normally open contact, thus holding the Main Rectifier off.
14. K-4 continues to run until it closes, energizing K-5.
15. K-5, Time Delay Auxiliary, normally closed contact opens K-13 step coil, and K-5 normally open contact energizes $\mathrm{K}-13$ release coil.
16. $\mathrm{K}-13$ resets and the entire sequence listed above is repeated until stopped by the operator.
17. The operator may stop the sequence by turning off the Main Rectifier, or any switch ahead of it in the turn-on sequence, or by switching S-27 to MANUAL.

## NOTE

A sustained fault in the 1500/3000 Volt Supply causes a similar performance, with the supply held off when the stepping relay reaches the fourth contact. ( $\mathrm{S}-410$ must be closed and S-27 in AUTOMATIC for the $1500 / 3000$ Volt Supply to operate the step sequence.) Note that an overload on the 400 Volt Supply will cause K-13 to step up, but will not shut down the supply. That must be done with S-103 or some switch ahead of it in turn-on seauence.

## SUPERVISORY RELAY TEST POSITION

Socket X-20 is provided in the Power Control Cubicle for use as a test position for the supervisory system relays. As can be seen from the Fundamental Control Schematic, figure 47, a relay plugged into X-20 will be energized, closing both normally open contacts and causing I-32 (SUPERVISORY RELAY TEST) to light, the relay is working properly.

## SUPERVISORY SEARCH RELAY

As a special supervisory search relay, K-1 may be employed to detect erratic operation of enclosure interlocks, air switch, undervoltage relays or other circuits not equipped with supervisory relays and indicator lights. Terminals of K-1 and I-31 (SEARCH RELAY) appear on TS-2, terminals 13 to 20, at the rear of the Power Control Cubicle where they are conveniently accessible and may be connected to other circuits as desired by the station engineer.

## OUTAGE CLOCKS

The OUTAGE TIME and OUTAGE DURATION clocks on the Power Control Panel are set as follows:

1. With Transmitter in operation, set the OUTAGE TIME clock to correct time and start it by pressing the RESET button below it.
2. Set the OUTAGE DURATION clock at 12. The clock will run with the transmitter in operation as long as the RESET button is pressed, thus making it possible to set the second hand accurately.

Operation of the clocks can be followed on the Control Schematic, figure 47. Briefly, whenever the Main Rectifier Breaker S-2002 trips, the OUTAGE TIME clock stops, the OUTAGE DURATION clock starts and I-25 (CARRIER INTERRUPTION) lights.

## FILAMENT UNDERVOLTAGE RELAY K-8

The operation of $\mathrm{K}-8$ is as follows:

1. K-8 begins a timing cycle when the exciter filament circuit is turned on.
2. After approximately 22 seconds, depending on the voltage slider setting, (see I. L. 41-291D in the Supplement Section) the normally open contact closes, lighting I-42 (EXCITER FILAMENTS NORMAL VOLTAGE) and "latching-in" relay K-46, the Filament Delay Auxiliary.
3. An interruption in supply voltage will cause the normally open contact to open and after a delay of approximately 8 seconds (depending on the time lever setting of $\mathrm{K}-8$ ) the normally closed contact to close.

Note that reapplication of power before the 8 seconds have expired will return the transmitter to the air without delay.

BUS BREAKER S-2001
The operation of the Bus Breaker is as follows:

1. With switches S-28 and S-30 closed and series interlocks closed, relay K-3, Bus Breaker Auxiliary, is energized.
2. The normally open contacts of $\mathrm{K}-3$ close, energizing the "pull-in" coil "CC."
3. When the breaker is nearly closed, a normally open breaker auxiliary contact energizes and seals in the "anti-pump" relay K-2004 which in turn opens the circuit to the "pull-in" coil "CC" which no longer needs to be energized since the breaker latches in mechanically. Switches S-2010 and S-2011 function the same as switches S-2012 and S-2013 in the high voltage breaker S-2002.
4. With the breaker closed, the normally open contact in series with the trip coil "T" of S-2001 closes, but the trip coil receives no energy until K-3 becomes deenergized. When this occurs, the breaker is returned to its original "off" position.
5. Note that the breaker will follow relay K-3 off and on; however, the presence of K-2004 in the circuit prevents "pumping" of the breaker due to tripping from a-c overloads or undervoltage. It also prevents the breaker from coming back on automatically if it is manually tripped.

## MAINTENANCE

## SUGGESTED SCHEDULES

1. Daily
a. Check pressure in all gas filled capacitors.
b. Check and polish, if necessary, protective gaps on gas filled capacitors, on 5736 audio driver cathode chokes, on Modulation Transformer, on Modulation Reactor, and on Rectox units.
c. Inspect fuse wires on high voltage capacitors in Filter.
2. Weekly
a. Check operation of all control circuit devices, door interlocks, and other protective devices.
b. Check air interlock as follows: With the distribution bus on, but with filaments off, open the Blower line starter breaker (shutting down blower). This should cause I-36 or 1-41 light to go out and the distribution bus to be deenergized.
c. Thoroughly clean interior and exterior of transmitter cubicles. Clean power equipment external parts with special attention to insulators.
d. Inspect and oil Blower bearings. Use light machine oil, (SAE No. 10).
3. Monthly
a. Inspect and, if necessary, clean contactors and relays in the transmitter cubicles. Take particular care to keep the contacts clean on K-3, K-7, and K-13 in the Power Control. Abrasives should not be used on silver contacts, because particles of the abrasives may become embedded in the contact surface. Cleaning the contact fingers and contact arcs of relay $\mathrm{K}-13$ should be done with a soft rag saturated in carbon tetrachloride. After cleaning, remove all lint, and lubricate the contact fingers, bearing pins, and ratchets sparingly with a light mineral oil.
b. Inspect and, if necessary, clean Main Rectifier and Distribution Bus Switchgear, Type DB-25, Refer to I.B. 35-225-1.
c. Inspect, clean and lubricate Bus Regulators, also Main Rectifier Regulator if used. Refer to I. B. 5521-A.
d. Inspect and, if necessary, tighten all electrical connections.
e. Operate the spare Modulator and Power Amplifier tubes with reduced plate voltage and increase to full power in approximately 15 minutes. Check modulation capability with tone or program material.

## 4. Quarterly Schedule

a. Lubricate the exposed parts of the motor operated tuning controls. The reduction gears are packed in grease and with normal usage will require no attention during the life of the equipment. Put a drop of light machine oll on the motor bearings once or twice a year.
b. Metal rectifiers age slightly during the first several thousand hours of use resulting in a small decrease of output voltage. This decrease may be cancelled by changing the transformer primary taps of the 400 volt and RF bias supplies and by adjusting the controls of the audio bias supplies. Following this initial period, the rectifiers should be closely inspected regularly for evidence of overheating or corrosion. A casual inspection is usually unsatisfactory, because in practice first evidence of these effects usually shows up in individual cells rather than a general deterioration.
c. The dry type power transformers may require cleaning to prevent clogging of the ventilating ducts if the air contains an excessive amount of dust or lint. If a dry type transformer gets wet, it must be removed from service and thoroughly dried.
d. The air inlet filter cleaning schedule will depend on local air conditions. The condition of the filters may be determined by inspection or by checking the air flow through the transmitter as specified in the section on Air Velocity under the main heading POWERON ADJUSTMENTS. Any indication of a reduction in the normal flow of air should call for replacement or cleaning at once.

If a Precipitron, the Westinghouse Electronic Air Cleaner is used, little maintenance is required besides periodic washings according to instructions furnished with the equipment.

## RECTOX RECTIFIERS

The following is a general discussion of the characteristics of rectox rectifiers.

1. Forward Aging
a. A small increase in resistance to the flow of load current is normal. The resulting reduction in output voltage should not be more than about 5 percent over a period of years. Most rectifier transformers are provided with "aging" taps whereby the voltage can be increased after a year or so of operation. Thereafter no further adjustments should be necessary. A further indication of normal forward aging is a slight increase in output hum of three-phase full-wave rectifiers.
2. Reverse Aging
a. Normal aging: The reverse resistance will decrease somewhat with age. This is normal and will have no appreciable effect on the rectifier operation.
b. Effects of excessive reverse aging: If the aging in the reverse direction becomes excessive, the rectifier will overheat. The overheating may damage the cells, or may accelerate forward aging. An abnormal increase in reverse current may overload and damage the rectifier transformer.
c. Indication of reverse aging: Excessive reverse aging may be detected from any of the effects listed in b. above. In addition, it is possible to measure directly the reverse current in any stack by following the procedure as set forth in paragraph 3 "Replacement of Rectifier Stacks."
d. Allowable limits of reverse current: It is not possible to give the exact limits of reverse current which may be considered normal. The following general statements apply, however:
(1) Using the original reverse current measurements supplied by the manufacturer as a standard, the current should not increase over four times this value as aging takes place.
(2) The reverse current will increase with increasing temperature.
(3) The reverse aging rate will be less with selenium than with copper oxide.

## 3. Replacement of Rectifier Stacks

The condition of selenium or copper oxide rectifiers can usually be determined by checking output d-c voltage and rms ripple voltage. A sudden increase in normal ripple with a simultaneous decrease in the output may be the fault of the rectifier and would warrant further investigation. A gradual decrease of approximately 5 percent in the output d-c voltage is to be expected from the normal aging of the rectifier. This also may result in some increase in hum due to some of the rectifiers aging more rapidly than others. If it is decided that the rectifier may be at fault, the following test should be made.

Ordinarily a faulty rectifier stack can be located by running the unit at full load for a short time and then immediately after shutting off the power, checking the temperature of the various rectifier stacks with a thermometer or with the hand. A faulty stack will usually be hotter than the rest. This stack should be disconnected and checked as follows:

Use a d-c power supply capable of supplying the current and voltage shown in the following chart. To check the forward rectifier resistance, connect the positive terminal of the d-c test supply to the negative terminal on the rectifier and the negative terminal of the test supply to the opposite end of the rectifier stack or center tap as noted in some cases. Adjust the test voltage to the proper value. The resulting forward current should be approximately as shown in the table. In checking the back resistance of the rectifier, connect the positive lead of the test supply to the positive rectifier stack terminal.

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I.B. $81-120-2 \mathrm{~A}$


I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

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I. B. $81-120-2 \dot{2}$

I. B. 81-120-2A


I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

1.B. 81-120-2A

I. B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

| ORAWIN | $\begin{aligned} & \text { NG NO. } \frac{50-B-8600}{}{ }^{\circ} \text { PARTS } \\ & \text { ATUS } 50 \mathrm{HG}-2 \quad \text { A. } \mathrm{M} . \end{aligned}$ | ET 19 OF STY SHEETS <br> AND RECOMMENDED SPARE <br> BROADCAST TRANSMITTER |  | $\begin{aligned} & \text { ST } \\ & \text { נT- } \\ & \text { No } \end{aligned}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CIRCUIT SYMBOL | FUNCTION | DESCRIPTION | STYLE OR CAT. NO. | MFR | WESTINGHOUSE DRAWING NO. |  |  |  |
|  |  |  |  |  |  | QUANTITY |  |  |
|  |  | P.C. (CONTINUED) |  |  |  |  |  |  |
| K-33 | RELAY, R.P.A., O.L. Aux. | Same as K-17 |  |  | 7619418 P7. 153 |  |  |  |
| $k-34$ | Relay, garrier inter. Aux. | Sakc as K-17 |  |  | 7619418 Pt. 154 |  |  |  |
| K-35 | Relay, sparc | Same as K-17 |  |  | 7619418 Pt. 155 |  |  |  |
| K 36 | Relay, spari | Same as K-17 |  | . | 7619418 Pt. 156 |  |  |  |
| K-37* | Contactor, audio Blas | TYPE DN-00 10 AMP. CONTACTOR, 3 POLE N. O., 230 V., 60 crGLES. | $\begin{aligned} & \text { STYLE } \\ & 1301694 \end{aligned}$ | 1 | 7619418 Pr. 157 | 1 |  |  |
| K-38 | Contactor, R.f. bias | TYPE DN-00 10 amp. CONTACTOR, 4 POLE N. O., 230 V., 60 creles | Strle 1190560 | 1 | 7619418 Pt. 158 | 1 |  |  |
| K-39 | $\text { CONTACTOR, } 400 \mathrm{~V} .$ SUPPLY | Samz as K-37 |  |  | 7619418 PT. 159 |  |  |  |
| K-40 | COntactor, $\begin{aligned} & \text { Cupplr } \\ & \text { Sup }\end{aligned}$ | CLASS $15 .-$ E25 N 2 SIZE2. <br> TYPE N-24O 45 AMP. CONTACTOR. 4 POLE <br> N. O., 230 V., 60 crcles (SEE NOTE FOR 50 CYCLE OPERATION ON PAGE 59 ). | Strle tratit69 1614216 | 1 | 7619418 Pr. 160 | 1 |  |  |
| K-41* | Relay, aux. frames | trpe Sg aux. relay, $230 \mathrm{~V} ., 50 / 60 \mathrm{cr}$. | $\begin{aligned} & \text { STYLE } \\ & 1008540 \end{aligned}$ | 1 | 7619418 Pr. 161 | 10 | 1 |  |
| K-42 | Relay, p.C. intla. | Same as K-41 |  |  | 7619418 PT. 162 |  |  |  |
| K-43 | Relay, Exc. \& MOD. Intlk. | Same as $\mathrm{K}-41$ |  |  | 7619418 Pr. 163 |  |  |  |
| $x-44$ | Relay, L.P.A. Intlk. | Same as K-41 |  |  | 7619418 Pr. 164 |  |  |  |
| K-45 | RELAY, C.P.A. \& R.P.A. INTLK. | Same as K-41 |  |  | 7619418 Pr. 165 |  |  |  |
| K-46 | Relay, fil. delay Aux. | Trpe MG-6 aux. relay, 230 V., 60 cy . (SEE NOTE FOR SO CYCLE OPERATION ON page 59) : | Sirle <br> 1163957 | 1 | 7619418 Pr. 166 | i |  |  |
| K-47 | Relay, aux. No. 1 STIPPING | Same as K-41 |  |  | 7619418 Рт. 167 |  |  |  |
| K-48 | Relay, Aux. No. 2 StEPPINa | Same as K-41 |  |  | 7619418 Pr. 168 |  |  |  |
| K-49 | Relay, gus breaker time delay | Same as K-41 | . |  | 7619418 Pr. 169 |  |  |  |
| K-50 | Rglay, HV brcaker rime dilay | Same as K-41 |  |  | 7619418 PT. 174 |  |  |  |
|  |  | EXCITER |  |  |  |  |  |  |
| k-101 | Relay, audo inpuy SHORTING | SAME AS K-41 |  |  | 7619373 Pr. 172 |  |  |  |
| K-102 | Relay, osc. selector | D.p.D.t. latching relay, 24 V., D.c. COIL | Similar <br> TO 2759 | 37 | 7619373 Pr. 173 | 1 |  |  |
| K-103 | Relat, carrier inter. | Same as K-41. |  |  | 7619373 Pr. 174 |  |  |  |
| K-104 | Relay, 807 \& 813 AVOIO SCREEN INTLK. | Sami as K-41 |  |  | 7619373 Pr. 175 |  |  |  |
| K-105* | REl.AY, 400 V., D.C. O. L. | Type SC current relay, $0.25-1.0$ amp. RANGE | $\begin{aligned} & \text { STYLE. } \\ & \text { 1096937- } \\ & (\text { MODIFIED }) \end{aligned}$ | 1 | 7619373 PT. 176 | 2 |  |  |
| K-106 | felay, 813 k.f., Pl. (). L. | Same as k-105 |  |  | 7619373 P7. 177 |  |  | , |
| k-107* | Relay, L. 5736 , R.f. D.L. | Type sC current relay 0.5-2.0 amp. range | $\begin{aligned} & \text { STYLE } \\ & 1096937 \end{aligned}$ | 1 | 7619373 Pt. 178 | 4 |  |  |
| n. 108 | $\begin{aligned} & \text { RELAY, R.S736, R.F. } \\ & \text { FI. O. L. } \end{aligned}$ | Same as K-107 | - |  | 7619373 Pr. 179 |  |  |  |
| 2.109 | Kitay, Exc. Bias, U. V. | Trpe SV voltage relay, 50-150 V.D.C. | $\begin{aligned} & \text { STYLE } \\ & 1096958 \end{aligned}$ | 1 | 7619373 Pt. 180 | 7 |  |  |
| -110* | helay, l. Audio blz fi. O. I. | Type SC current relay, 0.1-0.4 amp. range | $\begin{gathered} \text { STYLE } \\ 1096937- \\ \text { (M001FIED) } \end{gathered}$ | 1 | 7619374 PT. 181 | 4 |  |  |
| 11 | Gutay, R. Auble 813 | Sami as K-110 |  |  | 7619374 Pt. 182 |  |  |  |
| , | (1AN, A. AUGIO BiAS | Same as K. 109 |  |  | 7619374 Pr. 183 |  |  |  |

I.B. $81-120-2 \mathrm{~A}$

I. B 81-120-2A

I. B. 81-120-2A


1. B. 81-120-2A


1.B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

| ORAWIN <br> APPARA | PA NO. $50.8 \cdot 8600$ SHE PARTS $50 \mathrm{HG}-2 \quad$ A | T $\qquad$ OF $\qquad$ SHEETS <br> ND RECOMMENDED SPARE PAR <br> M. BROADCAST TRAAM MITTER | $\begin{array}{r} \text { RTS L } \\ \text { INP } \\ \text {-STYLE } \end{array}$ | T |  | $\begin{aligned} & \frac{k}{2} \\ & \underset{y}{\alpha} \\ & \frac{\alpha}{u} \\ & \hline \alpha \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CIRCUIT <br> SYMBOL | FUNCTION | DESCRIPTION | STYLE OR | MFR | WESTINGHOUSE DRAWING |  |  |  |
|  |  |  | GAT. NO. |  | NO. | QUANTITY |  |  |
|  |  | POWER CONTROL (CONTINUED) |  |  |  |  |  |  |
| M-4 | Meter, gus volt | Trpe KA-24, SIMILAR TO S\#1274679, EXCEPT DIAL TO BE BLACK WITH WHite <br> lettering; calibrated 0-300 volts full scale. Meter face windoy to be glass. | $\begin{aligned} & \text { SINILAR } \\ & \text { TO } \\ & 1274679 \end{aligned}$ | 1 | 7619419 PT. 196 | 1 |  |  |
| M-5 | Clock, outage DURATION | (SEE nOtE, for SO cy. operation, on PAGE 59 ) $115 \mathrm{~V} . / 60$ cYCLE, 12 hour CLOCK. | $\begin{gathered} G-1 \\ .7620240 \end{gathered}$ | 1 | Pr. 197 | 1 |  |  |
| M-6 | Clock, Time of OUTAGE | (SEE NOTE, POR 50 CY. OPERATION, ON PAGE 59.).). 115 V ./60 cYCLE, 12 hOUR CLOCK. | $\begin{gathered} G-2 \\ 7620240 \end{gathered}$ | 1 | Pr. 198 | 1 |  |  |
| M-7 | mettr, tuee mour | TrPE RH-35, $240 \mathrm{~V} . / 60 \mathrm{cr}$. (SEE NOTE for 50 CYCLES OPERATION, ON PAGE 59.). | S\#1205874 | 1 | 7619419 Pt. 199 | 1 |  |  |
|  |  | EXCITER |  |  |  |  |  |  |
| M-101* | MEtER, osc. cathode CURRENT | TrPE RX-33, 0-30 MA., D.C. | S\#1203597 | 1 | 7619374 Pr. 237 | 4 |  |  |
| M-102* | Meter, 807 (R.f.) CATHODE CURRENT | Trpe RX-33, 0-100 MA., D.C. | S\#1203602 | 1 | Рт. 238 | 3 |  |  |
| M-103 | METER, 813 (R.f.) GRID CURRENT | Same as M-101 |  |  | Pr. 239 |  |  |  |
| M-104* | Meter, 813 (R.f.) CATHODE GURRENT | Type RX-33, 0-500 MA., D.C. | S\#1203608 | 1 | 7619374 PT. 240 | 2 |  |  |
| M-1 05 | Meter, 5736 (R.f.) GRID CURRENT | Same as M-104 |  |  | 7619375 Pr. 241 |  |  |  |
| M-106* | Mcter, L. 5736 <br> (R.F.) plate curremt | Type RX-33, 0-2 Amps., D.C. | S\#1203486 | 1 | Pr. 242 | 2 |  |  |
| M-107 | Meter, R. 5736 <br> (R.F.) plate curaent | Same as M-106 |  |  | Pr. 243 |  |  |  |
| M-108 | Meter, 1.5 KV., RECT. | Trpe RX-33, 1.0 MA. D.C. movement, SIMILAR TO S\#1203584, EXCEPT DIAL calibrated 0-2 KV. and marked with "KV. D.C." SUPPLY WITH MULTIPLIER RESISTOR S\#1158215 AND TWO MTGS. S\#1202797. | $\begin{gathered} \text { SIMILAR } \\ \text { TO } \\ 1203584 \end{gathered}$ | 1 | Pt. 244 | 1 |  |  |
| M-109* | METER, 813 (R.f.) <br> PLATE TUNING IND. | Trpe RX-33, 1.0 MA., D.C. movement, SIMILAR TO S\#1203584, EXCEPT DIAL caligrated 0-100 and markeo with "Position". | $\begin{aligned} & \text { SIMILAR } \\ & 1203584 \end{aligned}$ | 1 | PL 245 | 2 |  |  |
| M-110 | Meter, 5736 (R.f.) PLATE TUNING JND. | Same as M-109 |  |  | Pr. 246 |  |  |  |
| M-111* | METER, L. 5736 AUDIO BIAS VOLTAGE | TYPE RX-33, 0-500 V., D.C. SUPPLY WITH MULTIPLIER RESISTOR SA\#1158́́11 AND TWO mountings S\#1202797. | S\#1203860 | 1 | Pr. 247 | 4 |  |  |
| M-112 | Meter, R. 5736 AUDIO BIAS YOLTAGE | Same as M-111 |  |  | Pr. 248 |  |  |  |
| M-113 | meter, 807 auolo CATHODE CURRENT | Same as M-102 |  |  | PT. 249 |  |  |  |
| M-114 | Meter, L. 813 audio CATHODE CURRENT | Same as M-102 |  |  | Pr. 250 |  |  |  |
| M-115 | Meter, R. 813 aijolo CATHODE CURRENT | Same as M-102 |  |  | Рт. 251 |  |  |  |
| M-116 | METER, L. MOD. BIAS VOLTAGE | Same as M-111 |  |  | Pr. 252 |  |  |  |
| M-117 | meter, R. mOD. bias vOLTAGE | Same as M-111 |  |  | Pt. 253 |  |  |  |
| M-118 | meter, 400 V. RECTIFIER | Type RX-33, 1.0 MA., D.C. novement, SIMILAR TO S\# 1203584 , EXCEPT DIAL caligrated 0-750 and marked "Volts, D.C." SUPPLY WITH MULTIPLIER RESISTOR style \#1158212 ano two mountings S\#1202797. | $\begin{aligned} & \text { SINILAR } \\ & \text { TO } \\ & \text { S\# } 1203584 \end{aligned}$ | 1 | Pt. 254 | 1 |  |  |
| M-119 | Meter, L. 5736 AUDIO GRID CURRENT | Same as M-101 |  |  | Pt. 255 |  |  |  |
| M-120 | Meter, R. 5736 <br> AUDIO GRID CURRENT | Same as M-101 |  |  | Pt. 256 |  |  |  |

I.B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 A$

| CRAWINE NO.50-9.8600 SHEET $\qquad$ OF $\qquad$ SHEETS <br> PARTC AND RECOMMENDED SPARE PARTS L |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { MINIMUM SFARE } \\ & \text { FARTS LIST } \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
| CIPRCUIT SYMBOL | gUNCTION | DESCRIPTION | STYLE OR GAT. NO. | MFR | WESTINGHOUSE DRAWING NO. |  |  |  |  |
|  |  |  |  |  |  |  | QUA | ANTIT | TY |
|  |  | EXCITER |  |  |  |  |  |  |  |
| R-101 | Res., osc. grio | . 22 hegonm, 1 W. | S-1471204 | 1 | 7720527 | Pr. 17 | 1 | 5 | 2 |
| R-102 | Res., osc. catmode | 400 онms, 10 W. | 10F | 44 |  | Pr. 18 | 1 |  |  |
| R-103 | Res., osc. volts DIVIOER | 6000 оннs, 20 W. | 20x | 44 |  | Pr. 19 | 1 |  |  |
| R-104 | Reg., osc. yoty DIVIDER | 20,000 onms, 10 W. | 10F | 44 |  | Pт. 20 | 1 |  |  |
| R-105 | $\begin{aligned} & \text { RES., IND. GURRENT } \\ & \text { LINIT } \end{aligned}$ | 47,000 оннS, $1 / 2 \mathrm{~W}$. | S-1471167 | 1 | 7720527 | Pr. 21 | 1 | 5 | 2 |
| R-106 | Res., R.F. 807 Grid | 15,000 OHMS, 2 W . | S-1471266 | 1 | 7619375 | Pr. 271 | 1 | 5 | 2 |
| R-107 | $\text { Ris., R.F. } 807$ CATHODE | 200 OHms, 13 W. | JAN-R-26 RW20J201 |  |  | Pr. 272 | 1 |  |  |
| R-108 | Res., R.F. 807 screen | 0.1 meg., 2 W . | S-1471276 |  |  | Pr. 273 | 1 | 5 | 2 |
| R-109 | Ress.0. QRID | 5,000 OnMs, 6 W. | JAN -R-26 RW15E502 |  |  | Pt. 274 | 1 |  |  |
| R-110* | RES., R.f. 813 GRID SUPPRESSOR | 56 OHMs, 1 W. | S-1471012 |  |  | Pr. 275 | 2 | 5 | 2 |
| R-111 | Sane as R-110 |  |  |  |  | Pr. 276 |  |  |  |
| R-112* | Res., R.F. 813 CATHODE | 500 omms, 86 W. | JAN-R-26 <br> RW12G501 |  |  | Pr. 277 | 2 | 2 | 1 |
| R-113 | Res., R. F., B13 SCREEN DIVIDER | 40,000 OHAS, 20 W. | $20 \%$ | 46 |  | Pt. 278 | 1 |  |  |
| R-114 | $\text { Res., R.F. } 813$ SCREEN DIVIDER | 25,000 OnMs, 120 W . | JAN-R-26 RW1 1G253 |  |  | Pt. 279 | 1 | 2 | 1 |
| R-115* | Res.. grid balancing | 100 omms, 50 W . | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RW13G101 } \end{aligned}$ |  |  | Pr. 280 | 3 | 2 | 1 |
| R-116 | Res.egrid oalancing | Same as R-115 |  |  |  | PT. 281 |  |  |  |
| R-117A | Res., R.f. Exc. bias | Same as R-112 |  |  |  | Pr. 282 |  |  |  |
| R-1178 | Res., R.f. Exc. sias | 310 omms, 86 W. | $\text { JAN -R-2 } 6$ RW12G311 |  |  | Pr. 283 | 1 | 2 | 1 |
| R-119* | $\text { Рот., L. AUOIO } 5736$ BIAS | 10,000 ohns, 50 Wo | 1106-22 | 46 |  | Pt. 285 | 2 | 2 | 1 |
| R-120 | $\begin{aligned} & \text { POT., R. AUDIO } 5736 \\ & \text { BIAS } \end{aligned}$ | Sane as R-119 |  |  |  | Pt. 286 |  |  |  |
| R-121* | Reg., L. Mod. bias | 200 orms, 90 W . | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RW12G201 } \end{aligned}$ |  |  | Pr. 287 | 2 | 2 | 1 |
| R-122 A* | Res., L. Mod. bias | 2500 OHMS, 90 W. | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RW12G252 } \end{aligned}$ |  |  | Pr. 288 | 4 | 2 | 1 |
| R-122日 | Same as R-122A | Same as R-122a |  |  |  | Pr. 289 |  |  |  |
| R-124 | Res.e R. MOD. bias | Same as R-121 |  |  |  | Pr. 291 |  |  |  |
| R-125A | Res., R. MOD. sias | Sams as R-122a |  |  |  | Pr. 292 |  |  |  |
| R-125f | Same as R-125A | Same as R-122A |  |  |  | Pr. 293 |  | - |  |
| R-126* | Res., M-123 shunt | . 47 megohm, 1 W . | S-1471200 | 1 |  | Pr. 294 | 2 | 5 | 2 |
| R-127 | Res., M-108 shunt | Same as R-126 |  |  |  | Рт. 295 |  |  |  |
| R-128* | fot., R.F. 813 plate TUNING CAL. | 7500 ohms, 2 W. . Linear taper pot. | $\begin{aligned} & \text { HAN-R=19 } \\ & \text { FA15A1SA- } \\ & \text { TSEAKK: } 43 \end{aligned}$ | 44 |  | Pт. 296 | 8 | 2 | 1 |
| R-1:9 | POT., R. F. 5736 plate tuning cal. | Same agrol28 | TYPE 43 |  |  | Pт. 297 |  |  |  |
| R-130 | Pot., R. F. 81.3 plate TUNING INO. | 300 Ohms, $\pm 10 \%, 2 \mathrm{~W}$. | $\begin{gathered} \text { Pr.a } \\ 7422247 \end{gathered}$ | 1 | 7619375 | Pt. 298 | 1 | 2 | 1 |
| R-131* | Fiot., R.f. 5736 plate TUNING IND. | 250 онms | JAN=R=19 <br> RA25A1FG- | 44 | 7619375 | Ft. 299 | 7 | 2 | 1 |
| R-132 | fot., R.F. 5736 plate COUPLING IND. | Same as R-131 | $\begin{aligned} & 251 A K \\ & \text { SERIES SE } \\ & \text { TYPE S8 } \end{aligned}$ |  | 7619375 | Pt. 300 |  |  |  |
| R-134* | KEs. A AUD. INPUT trans. load | Nomimal regigtance 33,000 ohms, 2 W. USED ONLY IN MATCHED PAIR WITM R-185. | $\begin{aligned} & 29,700 \\ & \text { ro } \\ & 36,300 \text { OHm } \\ & \text { SELECT } \begin{array}{l} \text { FRO } \\ \text { S } \# 1471270 \end{array} \end{aligned}$ | $\int_{1}^{1}$ | 7619376 | Pt 302 | ONE MATKHE PAIR |  | ONE |
| R-125 | SAME AS R-134 | Nominal resistance 33,000 ohms, 2 W . (USEO ONLY IN MATCHED PAIR UITM R-134) | Matched WITHIN 660 OHMS Of R1: SGLESI...EROI | $\begin{aligned} & 1 \\ & \frac{21}{2} \# 1 \end{aligned}$ | 7619376 | Pr. 303 |  |  |  |

I.B. $81-120-2 \mathrm{~A}$

| DRAWIN APPARA | $\begin{aligned} & \text { G NO. } \frac{50 \cdot 8 \cdot 8600}{\text { PARTS }} \\ & \text { TUS } 50 \mathrm{HG}-2 \quad \mathrm{~A} . \end{aligned}$ | T30OF SHEETS <br> ND RECOMMENDED SPARE <br> BROADCAST TRANSMITTER | ARTS LIST STYLE INPU | ST |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CIRCUIT SYMBOL | FUNCTION | DESCRIPTION | STYLE OR <br> GAT NO. | MFR | WESTINGHOUSE DRAWING NO. |  |  |  |
|  |  |  |  |  |  | QUANTITY |  |  |
|  |  | EXCITER (CONTINUED) |  |  |  |  |  |  |
| R-143* | Res., Grio | Nominal resistance 33,000 ohms, 2 W . (USED ONLY in matcheo pair with r-144) | $\begin{aligned} & 29,700 \\ & 36,30 \\ & \text { rELECT } \\ & \text { FAON } \\ & \text { SH1471270 } \end{aligned}$ | 1 | 7619376 P7. 313 | $\begin{array}{\|l\|} \hline \text { ONe } \\ \text { Marker } \\ \text { PAlR } \end{array}$ | PUTEH | mix |
| R-144 | $\underset{\substack{\text { Res., } \\ \text { RRID }}}{ } \text { AUOIO } 813$ | Nomimal resistance 33,000 ohms, 2 W . (USED onty in matcheo pair with R-143) | matched <br> VITHIN <br> 330 onms <br> of R-143 <br> SCLET <br> FROM <br> S\#1471270 | 1 | Pr. 314 |  |  |  |
| R-145* | Res., L. StEP CIRCUIT | 2200 ohms, 2 W., nomimal resistance (useo onty in matcheo palr with r-146) | $\begin{aligned} & 1980 \text { ro } \\ & 2420 \text { OHMS, } \\ & \text { SELECT } \\ & \text { FROM } \\ & \text { S\# } 1471256 \end{aligned}$ | 1 | Pr. 315 |  | ane | Mane |
| R-146 | Res., R. Avoio 813 step circuit | Nomimal resistance 2200 ohms, 2 W. (USED ONLY IN MATCHED PAIR NITM R-145) | Matched <br> WITHIN <br> 44 OHMS <br> of R-145 <br> SELECT <br> fROM <br> S\#1471266 | 1 | Pr. 316 |  |  |  |
| R-149A* | $\begin{aligned} & \text { Res., L. AVO } \\ & \text { PLATE } 813 \end{aligned}$ | Nomimas resistance 20,000 onms, 50 W. | WITMIN <br> $\pm 1 / 2 \%$ <br> of NOM. <br> RESISTANCE <br> JAN-R-26 <br> RW13G203 | 1 | Pr. 319 | 2 | 2 | 1 |
| R-1498* | $\underset{\substack{\text { Res., } \\ \text { PLAté }}}{\text { L. AUOIO }} 813$ | nomimal resistance 16,000 onms, 50 W . | WITHIN <br> $\pm 1 / 2 \%$ <br> OF NOM. <br> RESISTANCE <br> JAN -R-2 6 <br> RW13G163 | 1 | 7619376 Pr. 320 |  |  |  |
| R-150A | $\begin{aligned} & \text { RESi, } \\ & \text { PLATE. AUDIO } 813 \end{aligned}$ | SAME AS R-149A. |  |  | 7619376 PT. 321 |  |  |  |
| R-1508 | REs., R. Audio 813 PLATE | SAMC AS R-1498. |  |  | Pr. 322 |  |  |  |
| R-151 | $\begin{aligned} & \text { Por., L. AUDIO } 813 \\ & \text { BIAs } \end{aligned}$ | Same as R-138. |  |  | Pт. 323 |  |  |  |
| R-152 | $\begin{aligned} & \text { Por., R. Avoio } 813 \\ & \text { B1Ag } \end{aligned}$ | Same as R-138. |  |  | Pr. 324 |  |  |  |
| R-153* | $\underset{\text { GRID. }}{\substack{\text { Res. }}}$ | 31,000 оHms, 35 W. | Trpe <br> 4-1/8 T. <br> ferrule <br> 312 | 46 | Pr. 325 | 2 | 2 | 1 |
| R-154 |  | Same as R-153. |  |  | Pт. 326 |  |  |  |
| R-157 | Sabe as R-9 |  |  |  | Pr. 329 |  |  |  |
| R-158 | Same as R-9 |  |  |  | Pr. 330 |  |  |  |
| R-159 | Same as R-9 |  |  |  | Pr. 331 |  |  |  |
| R-160 | Same as R-9 |  | , |  | Pr. 332 |  |  |  |
| R-161 | Same as R-9 |  |  |  | Pr. 333 |  |  |  |
| R-162 | Same as R-9 |  |  |  | Pr. 334 |  |  |  |
| R-165* | Res., 1.5 KV . rect. | 10,000 онкs, 140 W. | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RWIOG103 } \end{aligned}$ |  | Pr. 337 | 5 | 2 | 1 |
|  |  |  |  |  |  |  |  |  |

I.B. 81-120-2A

I. B. $81-120-2 \mathrm{~A}$



WESTINGHOUSE ELECTRIC CORPORATION ELECTRONICS AND X-RAY DIVISION


## WARNING!

## HIGH VOLTAGE!

THE VOLTAGES ENCOUNTERED IN THIS EQUIPMENT ARE DANGER OUS TO HUMAN LIFE. TO BE SAFE, DISCONNECT THE POWER SOURCE WHEN SERVICING ANY OF THE UNITS.

The use of high voltages which are dangerous to life is necessary for the operation of of the electronic equipment covered by these instructions. While all practical safety precautions have been incorporated in the design of the equipment, they are net infallible; therefore, certain precautionary measures must be carefully observed by the operating personnel during the operation, inspection and maintenance of the equipment.

KEEP AWAY FROM LIVE CIRCUITS .- Do not reach into an enclosure or handle any portion of the externally installed units without first removing the power and grounding the circuit.

OBSERVE EXTREME CAUTION WHEN SERVICING OR ADJUSTING THE EQUIPMENT .- Do not connect any apparatus external to the enclosure, to circuits within the equipment, or apply voltages to the equipment for testing purposes while any non-interlocked portion of the shielding or enclosure is removed or opened. Connection of apparatus external to the enclosure in addition to being a hazard may cause failure of the interlock circuits.

DO NOT TAMPER WITH INTERLOCKS .- Under no circumstances should any door or safety interlock be removed or short circuited, nor should interlocks be relied upon for removing voltages from the equipment.

DO NOT DEFEAT THE MECHANICAL INTERLOCK SYSTEM BY THE USE OF DUPLICATE KEYS.

## TABLE OF CONTENTS

Page
INTRODUCTION ..... 9
Electrical Specifications. ..... 9
Mechanical Specifications ..... 10
Units of the Complete Transmitter ..... 11
Tube Complement ..... 12
DESCRIPTION ..... 13
Electrical Description ..... 13
Mechanical Description ..... 18
RECEIVING, HANDLING, AND STORAGE ..... 22
Inspection of the Shipment ..... 22
Handling Procedure ..... 23
Storage ..... 23
Packing List ..... 23
INSTALLATION PLANNING ..... 26
Building Layout ..... 26
INSTALLATION ..... 27
Transmitter Interconnections ..... 27
Transmitter Cubicles ..... 28
External Power Equipment ..... 28
Ground System ..... 29
Interlocks ..... 30
Cooling System ..... 30
Heating Facilities ..... 31
INITIAL ADJUSTMENT AND TESTS ..... 32
Grounds and Short Circuits ..... 32
Switchgear Adjustments ..... 34
Relay Settings ..... 34
Gas Filled Capacitors ..... 35
RF Component Settings ..... 35
POWER-ON ADJUSTMENTS ..... 37
Power Line Voltage ..... 37
Blowers ..... 37
Air Velocity ..... 37
Distribution Bus ..... 38
Filament Voltages ..... 38
Exciter Bias and Plate Voltages ..... 39
RF Driver Neutralization ..... 40
RF Driver Tuning ..... 41
Power Amplifier Neutralization ..... 41
Low Level Audio Adjustments ..... 42

## TABLE OF CONTENTS (Concluded)

Page
Main Rectifier Regulator Operation ..... 43
Main Rectifier Regulator Adjustments (If Used). ..... 43
Main Rectifier Power Adjustments. ..... 44
Final Tune-Up ..... 44
Antenna Arc Interrupter Adjustments ..... 46
NOISE, FEEDBACK, DISTORTION, AND RESPONSE ..... 47
Noise ..... 47
Power Supply Ripple Voltages ..... 48
Voltage Feedback. ..... 48
Current Feedback ..... 48
Distortion. ..... 48
Frequency Response ..... 49
CONTROL CIRCUITS ..... 49
Fundamental Control Schematic Diagram ..... 49
The Turn-On Sequence ..... 50
Action on Sustained Fault ..... 50
Supervisory Relay Test Position. ..... 51
Supervisory Search Relay ..... 51
Outage Clocks ..... 51
Filament Undervoltage Relay K-8 ..... 52
Bus Breaker S-2001 ..... 52
MAINTENANCE ..... 52
Suggested Schedules ..... 52
Rectox Rectifiers. ..... 54
Normal Meter Readings ..... 55
GUARANTEE AND AVAILABLE WESTINGHOUSE SERVICE ..... 57
Guarantee. ..... 57
Service Available from Westinghouse ..... 58
PARTS AND RECOMMENDED SPARE PARTS LIST ..... (See Tab)

# LIST OF PHOTOGRAPHS 

(See Tab)

Figure
Title
Power Control Cubicle Front View
Power Control Cubicle Drop-Down Panel
Power Control Cubicle Interior
Power Control Cubicle Interior, Left Side
Power Control Cubicle Interior, Right Side
Exciter Cubicle Front
Exciter Cubicle Audio Door
Exciter Cubicle Radio Door
Exciter Cubicle Oscillator
Exciter Cubicle Interior
Exciter Cubicle Interior, Left Side
Exciter Cubicle Interior, Right Side
Modulator Cubicle Front
Modulator Cubicle Interior, Front
Modulator Cubicle Interior
Left Power Amplifier Cubicle Front
Left Power Amplifier Cubicle Interior, Front
Left Power Amplifier Cubicle Interior
Center Power Amplifier Cubicle Front
Center Power Amplifier Cubicle, Lower Front
Antenna Arc Interrupter Unit
Center Power Amplifier Cubicle Interior
Right Power Amplifier Cubicle Front
Right Power Amplifier Cubicle Interior, Front
Right Power Amplifier Cubicle Interior
Main Rectifier Filter Units

## LIST OF DRAWINGS

(See Trab)

Figure
Title
Drawing No.

## INSTALLATION DRAWINGS



## LIST OF DRAWINGS (Concluded)

Figure

Title

Drawing No.
38 Typical Air Exhaust Duct . . . . . . . . . . . . . . . . . . . . . . 7621270
$39 \quad$ Basic Air Supply System 7429905
40 End Radii Drawing ..... 7619510
41 Desk ..... 7715022
SCHEMATIC AND WIRING DIAGRAMS
42 Interconnection Wire List and Wire Bill ..... 7429128
43 Power Room and Distribution Bus ..... 55-A-8403
44 RF Wiring (Top of Cubicles) ..... 7621267
45 Panel Termination for RG-17/U Coaxial Cable ..... 7619445
46
Console, Schematic Diagram ..... 771502447
Fundamental Control, Schematic Diagram ..... 7301140
50HG-2 Broadcast Transmitter, Schematic Diagram ..... 63-J-60
48
Interlock Connections ..... 7432056
50 Power Control Cubicle, Wiring Diagram ..... 7301144
51 Exciter Cubicle, Wiring Diagram ..... 63-J-63
Modulator Cubicle, Wiring Diagram ..... 63-J-61
Left Power Amplifier Cubicle, Wiring Diagram ..... 7301195
Center Power Amplifier Cubicle, Wiring Diagram ..... 63-J-62
Right Power Amplifier Cubicle, Wiring Diagram ..... 7301192
Rectifier Wire Bill and Wiring Diagram ..... 55-A-3921
Switchgear, Wiring Diagram ..... 7720157
Distribution Bus Regulator, Schematic Diagram ..... 7718453
Main Rectifier Regulator, Schematic Diagram (If Used) ..... 7718452
Type FA Crystal Oscillator, Wiring Diagram ..... 7720555
Type FA Crystal Oscillator, Schematic Diagram ..... 7425857
Composite Diagram, Antenna Arc Interrupter Unit ..... 7724452
RF Current Transformer-Rectifier ..... 7432074
Ground Diagram ..... 55-A-8424

## LIST OF SUPPLEMENTS

## (See Tab)



## LIST OF SUPPLEMENTS (Concluded)



## INTRODUCTION

The Westinghouse Type 50HG-2 Transmitter is a high-level-modulated standard broadcast transmitter with nominal RF power output of 50 kw . It incorporates the latest developments in electrical and mechanical design and meets all the operational requirements for a modern broadcast transmitter. Years of experience with the problems of the broadcaster has resulted in a Westinghouse transmitter designed for easy installation and economical operation and maintenance.

The following summary of electrical and mechanical specifications, and list of major components will serve to introduce the Westinghouse 50HG-2 Transmitter to the new owner.

## ELECTRICAL SPECIFICATIONS

Type of Emission ..... A-3
Power Output (to transmission line or common point) 53 kw , max.
Frequency Range (single specified frequency)
Lower Limit ..... 540 kc
Upper Limit ..... 1600 kc
Frequency Stability $\pm 10 \mathrm{cps}$
Modulation Capability ( 50 to 7500 cps inclusive) 100 percent
Carrier Shift ( 100 percent modulation with 400 cps sine tone) less than 5 percent
Audio Distortion ( $0-95$ percent modulation from 50 to 7500
cps, including all harmonics up to 45 kc ). less than 3 percent
Modulation high level Class B
Frequency Response (30 to 10, 000 cps ) ..... $\pm 1 \mathrm{db}$
Carrier Hum better than 60 db below 100 percent modulation
Audio Input Level ( 100 percent modulation at 1000 cps ) ..... $10 \pm 2 \mathrm{dbm}$
Power Line Requirements (see note 1 below):
Incoming Power Lines see note 2
Line volts. ..... 460 volts
Phase ..... 3 phase
Frequency (see note 3 below) ..... 60 cps
Power Input for 0 percent modulation ..... 103.5 kw
Power Input for average modulation ( 25 percent) ..... 113 kw
Power Input for 100 percent modulation ..... 147 kw
Power Factor (approximate) ..... 90 percent
Maximum Permissible Power Line Variation:
Frequency ..... $\pm 2$ percent
Deviation of full load phase-to-phase voltage from 460 volts ..... $\pm 5$ percent
Deviation of full load phase-to-phase voltage from average for the three phases ..... $\pm 2$ percent
Regulation ..... $\pm 2$ percent
Total permissible variation, including regulation from no load to full load, in percentage of 460 volts. ..... - $\pm 5$ percent
Crystal Heater Power Supply Requirements:
Line volts ..... 115 volts
Phase ..... 1 phase
Frequency 50-60 cps
Power ..... 30 watts
Output Impedance (one side of output coil grounded) ..... 40 to 250 ohms
Ambient Temperature Operating Range ..... $\pm 5^{\circ} \mathrm{C}$ to $\pm 45^{\circ} \mathrm{C}$
Distribution Bus Regulator Automatically maintains 230 voltsfor an input variation of approxi-mately $\pm 10$ percent
Main Rectifier Regulator(when furnished)

Note 1: The power requirements specified in this section do not include provision for the lights and convenience outlets in each transmitter cubicle. A 115 volt, single phase supply of approximately 1 kw capacity should be available.

Note 2: Lightning and switching surges on the incoming power lines can damage transmitter equipment. Therefore, it is suggested that the incoming circuits be examined for the probability of such transients and protective devices installed as necessary.

As a minimum requirement, three lightning arrestors, equal to Westinghouse style 1254825 should be used on the incoming 460 volt line, one between each line and ground.
Note 3: The Type 50HG-2 Transmitter can be supplied for operation with a 50 cycle supply.

## MECHANICAL SPECIFICATIONS

| Description | Dimensions in Inches |  |  | Approximate Weight in Pounds |
| :---: | :---: | :---: | :---: | :---: |
|  | Height | Depth | Width |  |
| Power Control Cubicle | 84 | 54-1/4 | 48-1/4 | 2225 |
| Exciter Cubicle | 84 | 54-1/4 | 48-1/4 | 2370* |
| Modulator Cubicle | 84 | 54-1/4 | 48-1/4 | 2100* |
| Left Power Amplifier Cubicle | 84 | 54-1/4 | 48-1/4 | 1920* |
| Center Power Amplifier Cubicle | 84 | 54-1/4 | 48-1/4 | 1550 |
| Right Power Amplifier Cubicle | 84 | 54-1/4 | 48-1/4 | 1920* |
| Switchgear Cubicle | 90-3/8 | 48 | 20 | 1225 |
| Rectox Rectifier and Frame, each of two | 64 | 28 | 41 | 350 |
| Modulation Transformer | 78-7/8 | 46-1/2 | 56 | 5700 |
| Filter Capacitor; each of three | 29-3/16 | 7-1/4 | 18 | 75 |
| Filter Reactor | 17-1/2 | 12-3/4 | 11-3/4 | 175 |
| Distribution Bus Regulator, each of two | 30-3/4 | 10-1/2 | 10 | 250 |
| Audio Filter Capacitor | 5-3/4 | 6-1/2 | 5 | 5 |
| Modulation Reactor | 67-1/2 | 29-1/2 | 40-1/2 | 2450 |
| Auxiliary Audio Choke | 16-1/2 | 22 | 18 | 25 |
| Modulation Coupling Capacitor | 26-1/2 | 18 | 7-1/2 | 75 |
| Blower | 70-5/16 | 65-5/8 | 49-1/4 | 920 |
| Blower Motor and Base | 15 | 22-1/2 $\dagger$ | 20 | 250 |
| Control Box | 24-3/8 | 5-5/8 | 9 | 25 |
| RF Current Transformer-Rectifier | 12 | 12 | 8 | 25 |
| Main Rectifier Transformer | 75 | 50 | 56 | 3300 |
| Main Rectifier Regulator (when furnished) | 75-5/8 | 43-3/4 | 24 | 3325 |
| Distribution Bus Transformer, each of three | 22-1/8 | 14-3/4 | 16-3/4 | 235 |

[^1]
## UNITS OF THE COMPLETE TRANSMITTER

The Westinghouse Type 50HG-2, 50 KW Standard Broadcast Transmitter consists of the following individual units:

1. One Power Control Cubicle . . . . . . . . . . . . . . . . S\#1475118
2. One Exciter Cubicle (less tubes and crystal oscillators and crystals)
3. One Modulator Cubicle (less tubes)
4. One Left Power Amplifier Cubicle (less tubes)
5. One Center Power Amplifier Cubicle.
6. One Right Power Amplifier Cubicle (less tubes)
7. Two Type FA Crystal Oscillators for Exciter Cubicle
8. Two crystals, Type TMV-129B for Crystal Oscillators . . .Dwg. 7431159
9. One Rectox Rectifier and Frame for Power Amplifier . . . . S\#1474566
10. One Rectox Rectifier and Frame for Modulator . . . . . . . S\#1474565
11. One Modulator P.S. Filter Reactor . . . . . . . . . . . . KR-7822469
12. One Main Rectifier Plate Transformer . . . . . . . . . . . S\#1646118
13. One Main Rectifier Induction Voltage Regulator (Optional Equipment)

S\#1486437
14. One Modulation Transformer . . . . . . . . . . . . . . S\#1483785
15. One Modulation Reactor . . . . . . . . . . . . . . . . . S\#1453629
16. One Modulation Coupling Capacitor . . . . . . . . . . . . S\#1081020
17. One Auxiliary Audio Choke . . . . . . . . . . . . . . . . S\#1472317
18. Audio Filter Capacitor . . . . . . . . . . . . . . . . . . S\#1471665
19. Three Distribution Bus Transformers . . . . . . . . . . . S\#1483783
20. Two Distribution Bus Induction Voltage Regulators . . . . . S\#1486439
21. One Switchgear Cubicle. . . . . . . . . . . . . . . . . . S\#1474865
22. P.A. and Modulator Filter Capacitors (Three) . . . . . . . S\#1474519
23. One Blower . ... . . . . . . . . . . . . . . . . . . . .Dwg. 7426385

Pt. 11
24. One Blower Motor . . . . . . . . . . . . . . . . . . . . S\#1442202
25. One Control Box for Blower Motor. . . . . . . . . . . . .Dwg. 7426385

Pt. 10
26. One Set of End Radii (to suit installation) . . . . . . . . . . Dwg. 7718801

Pt. 21
27. One RF Current Transformer

S\#1471694A
28. 60 Feet of RF Cable

RG-17/U
29. 70 Feet of RF Cable

RG-62/U
30. One Installation Kit (consisting of touch-up paint and miscellaneous hardware)

Dwg. 7427705
31. One complete set of Operating Tubes. . . . . . . . . . .Dwg. 7503652

GR. 1
32. Two Instruction Books . . . . . . . . . . . . . . . . . . IB 81-120-2A
34. One Station Call Letter Plate . . . . . . . . . . . . . . . Dwg. 7718801

Pt. 25

50 cps
S\#1475121
S\#1474780
S\#1474781
S\#1475122
S\#1474782
S\#1475123
S\#1472593
Dwg. 7431159
S\#1474566
S\#1474565
KR-7822469
S\#1646118
S\#1476438
S\#1483785
S\#1453629
S\#1081020
S\#1472317
S\#1471665
S\#1483783
S\#1486439
S\#1474864
S\#1474519
Dwg. 7426385
Pt. 11
S\#1442202
Dwg. 7426385
Pt. 10
Dwg. 7718801
Pt. 21
S\#1471694A
RG-17/U
RG-62/U
Dwg. 7427705
Dwg. 7503652
GR-1
IB 81-120-2A
S\#1472812
Dwg. 7718801
Pt. 25

Note 1: Interconnection wiring material is not furnished as a part of the Type 50-HG-2 Transmitter.

Note 2: Although not furnished as a part of the transmitter, the following accessory equipment can be supplied by Westinghouse:

Antenna Phasing Equipment
Transmitter Control Console S\#1472247
Precipitron Air Filter
Main Rectifier Induction Voltage
Regulator

Spare Blower, Motor and Control Box
25 KW Power Cutback Facility
10 KW Power Cutback Facility
Spare Tubes
Spare Parts

## TUBE COMPLEMENT

The following tubes are supplied with the transmitter:

| Qty. | Tube Type |
| :--- | :--- |
|  |  |
| 4 | WL-5671 |
| 4 | WL-5736 |
| 4 | WL-813 |
| 3 | WL-807 |
| 2 | OL-802 |
| 2 | RCA-1V |
| 3 |  |

These tubes are used as follows:

| Location | Tube Type | Quantity |
| :--- | :--- | :---: |
| Right Power Amplifier | WL-5671 |  |
| Left Power Amplifier | WL-5671 | 1 |
| Exciter, RF | WL-5736 | 2 |
| Exciter, RF | WL-813 | 2 |
| Exciter, RF | WL-807 | 2 |
| Exciter, Oscillator | WL-802* | 1 |
| Exciter, Oscillator | OD3/VR-150* | 2 |
| Center Power Amplifier | RCA-1V | 2 |
| Antenna House | RCA-1V | 2 |
| Modulator | WL-5671 | 1 |
| Exciter, Audio | WL-5736 | 2 |
| Exciter, Audio | WL-813 | 2 |
| Exciter, Audio | WL-807 | 2 |

* These tubes are part of the oscillator units. One complete spare oscillator is mounted in the Exciter.


## DESCRIPTION

The purpose of this section is to familiarize the station engineers with the electrical and mechanical details of the $50 \mathrm{HG}-2$ transmitter.

The text is in two sections: the Electrical Description, and the Mechanical Description. Although there are no specific references to the photographs, they are so identified that they may be used to further clarify the text.

## ELECTRICAL DESCRIPTION

## 1. Radio Frequency Circuits

The radio frequency system of the transmitter consists of the following stages:
a. A WL-802 crystal oscillator with an OD3/VR-150 regulator tube for stabilizing the screen voltage.
b. A WL- 807 buffer amplifier.
c. The first amplifier, two WL-813 tubes, in parallel.
d. The second, or driver amplifier, two WL-5736 tubes, in parallel.
e. The final amplifier, two WL-5671 tubes, in push-pull.

The Type FA Crystal Oscillator is an individual plug-in unit containing the TMV-129B crystal and heater assembly, the oscillator and voltage regulator tubes, and the associated circuitry. Frequency stability is maintained by the use of a highly stable quartz crystal in an electroncoupled circuit. The crystal is kept at a constant temperature in an automatic oven. Approximately 15 watts of 115 volt, single phase, power is required for operation of the oven. To further insure stability, a voltage regulator tube is used in the screen supply.

Two complete crystal oscillator units are included with the transmitter. A relay, operated by a switch on the front panel of the Exciter Cubicle, allows transfer from one unit to the other without noticeable interruption of carrier. The unit not in use is constantly in readiness with crystal heater and tube filaments energized.

The buffer stage uses a lightly loaded WL-807 tube as a Class C amplifier. The grid circuit is untuned and no neutralization is required. A cathode current meter is included. Cathode bias is provided to protect the tube in the event of excitation failure.

The first radio frequency amplifier consists of two WL-813 tubes in parallel as a Class C amplifier. The grid circuit is untuned and is capacitively coupled to the tuned plate circuit of the buffer stage. Grid and plate current meters are provided. The plate circuit is tuned by a motordriven capacitor. No neutralization is required. Cathode bias protects the tubes in the event of excitation failure. A loop coupled to the plate inductor is provided for feeding energy to a frequency monitor.

The second, or driver amplifier, uses two parallel WL-5736 tubes as Class C amplifier. The grid circuit is connected to a tap on the shunt-fed plate tank of the preceding stage. This tap can be adjusted to provide the proper grid drive. Neutralization is accomplished by a variable vacuum capacitor connected between the plates of the WL-5736 tubes and the plate tank inductor of the preceding stage. A motor-driven variable compressed-gas capacitor is used in the plate tank circuit. Total grid current and individual plate currents are metered. The total plate current is indicated by a large scale instrument. Fixed bias is supplied by an individual power supply.

The final amplifier is a Class C stage employing two WL-5671 tubes in push-pull. These tubes have thoriated tungsten filaments. The grid tank circuit is inductively coupled to the plate tank circuit of the driver stage. The coupling inductor is on the same coil form as the plate inductor of the driver stage, and has a motor-driven variable tap for coupling adjustment. An individual bias supply is provided for each half of the push-pull amplifier. Grid current and bias voltage for each tube is individually metered. A motor-driven variable compressed-gas capacitor is used in each grid circuit.

The plate tank circuit of the power amplifier is shunt fed in order that the two motordriven compressed-gas tank capacitors may be mounted at ground. Plate voltage and individual plate currents are metered. Inductive neutralization is used.

The output coupling coil is mounted inside the final tank inductor and has a motor-driven variable tap at ground potential. A Faraday shield is between the final tank inductor and the output coupling coil for suppression of harmonics. A thermocouple radio-frequency ammeter is in series with the output lead. This instrument is mounted behind a glass window in the Center Power Amplifier Cubicle and may be shunted out of the circuit by a switch on the lower front panel. A recti-fier-type meter is provided for remote indication of the output current.

A spare tube socket and filament transformer are provided for each of the operating tubes in the final amplifier. Substitution of the spare tube for its associated operating tube can be accomplished quickly.

RF energy for a modulation monitor may be obtained from the power amplifier tank circuit by tapping on to the tank coil end ring at a suitable point.

## 2. Audio Frequency Circuits

The audio frequency system of the transmitter consists of the following push-pull stages:
a. First audio, two WL-807 Class A.
b. Second audio, two WL-813 Class A.
c. Third audio, two WL-5736 Class AB.
d. Modulator, two WL-5671 Class B.

The first audio stage contains a line-to-grid input transformer which can be connected for either a 600 or a 150 ohm line. This stage has individual cathode bias for each tube. The total cathode current is metered. The plate circuit is resistance coupled to the following stage.

The second audio stage has individual bias adjustment for both tubes and is resistance coupled to the following stage.

The driver audio stage is a cathode follower, with an individual bias supply for each tube. Instruments are included for indication of cathode current, grid current and bias voltage for each tube. Cathode current in each tube is indicated by individual large scale instruments. This stage is directly coupled to the grids of the modulator tubes.

The Class B, high-level modulator stage employs two WL-5671 tubes in push-pull. These tubes have thoriated tungsten filaments. Individual bias supplies, adjustable and with separate indicating instruments, are used. Large scale instruments are supplied for plate voltage and individual indication of cathode current, and filament voltage, for each tube.

A spare tube socket and filament transformer are provided for each of the modulator tubes.

The audio power is fed to the final radio frequency amplifier across a modulation reactor, making it unnecessary to pass the plate current for this stage through the modulation transformer. An equalizer circuit stabilizes the modulator load impedance to permit the application of inverse voltage feedback.

## 3. Power Supplies

All power supplies in the transmitter use Rectox rectifiers. Rectox units have essentially unlimited life unless subjected to abuse. All except the two main rectifier supplies obtain primary power from a bus which is maintained at constant voltage by means of two automatic induction regulators connected in open delta. The regulators automatically maintain a constant output voltage of 230 volts for an input supply variation of approximately plus or minus 10 percent. Manual regulator control is also provided. Primary power for filament supplies is also obtained from this regulated distribution bus.

The two main rectifier supplies use a common transformer. By means of mechanically interlocked contactors inside the case of the transformer, the primary can be connected in Wye or Delta for tuning or full power output. Switching any of these contactors is accomplished by an OFF-TUNE-ON switch on the panel of the Center Power Amplifier.

The individual power supplies included in the transmitter are listed and briefly described below:
a. 400 Volt Supply -- this is a single phase, bridge rectifier. It supplies plate and screen voltage to the crystal oscillator and the RF buffer. It also supplies screen voltage to the first and second audio stage and bias to the second audio stage.
b. $1500-3000$ Volt Supply -- this is a 3000 volt, three phase, full-wave rectifier and a 1500 volt, three phase, half-wave rectifier. The 1500 volt supply furnishes plate and screen voltage for the first RF amplifier stage and plate voltage for the first audio amplifier stage. The 3000 volt supply furnishes power for the audio and RF driver stages and it also supplies plate voltage for the second audio stage.
c. Main Rectifier Supplies -- These are two separate high voltage, three phase, full-wave rectifiers using a common transformer. One rectifier supplies approximately 11,500 volts $\mathrm{d}-\mathrm{c}$ to the power amplifier; while the other supplies approximately 13,500 volts to the modulator.
d. Exciter RF Bias Supply -- this is a single phase, bridge rectifier. It supplies bias for the RF driver stage.
e. Audio Driver Bias Supplies -- these are two adjustable single phase, bridge rectifiers. They supply bias for the audio driver stage.
f. Modulator Bias Supplies -- these are two identical single phase, bridge rect fiers. They supply bias for the modulator, one for each of the two operating tubes. Ouiput voltage of each of these rectifiers is controlled from the front panel of the Exciter Cubicle.
g. Power Amplifier Bias Supplies -- these are two identical single phase, bridge rectifiers. They supply holding bias for each of the two operating tubes, and they furnish the fixed portion of the combination fixed and self-bias required to maintain modulation linearity.

## 4. Control Circuits

Controls for all necessary operational circuit and tuning adjustments are provided on the front panels of the cubicles. The associated indicating instruments and lights are coordinated with these controls. Individual switches are provided for all power circuits. These switches are sequence interlocked to prevent possibility of damage to the transmitter components, especially the tubes, which might result from the application of power to a circuit in incorrect sequence. Normally, the transmitter is put into operation by energizing each circuit separately. If desired, however, one switch control of the entire transmitter is possible. The transmitter can be shut down completely by opening the first switch in the sequence which controls power for the filaments and blowers, leaving the other switches in the "on" position. Then to return the transmitter to operation, it is necessary only to close the first switch; the other circuits will be energized in proper sequence and timing.

The transmitter includes a complete supervisory control system which provides indication of abnormal conditions such as overloads and open interlocks. This system is coordinated with the protection and safety provisions described in the following section. Overloads are registered even if they are only momentary; lock-in supervisory relays energize circuit identifying indicator lamps which remain lighted until the operator resets the relays by means of a reset switch on the control panel. This feature assists in locating trouble which can be investigated during normal maintenance period, decreasing future outages.

The supervisory control system includes individual indicator lamps for the following:
400 Volt Overload 1500-3000 Volt Overload Power Amplifier Rectifier DC Overload
Modulator Rectifier DC Overload
Main Rectifier AC Overload
813 RF Overload
Left 5736 RF Overload
Right 5736 RF Overload
Left Power Amplifier Overload
Right Power Amplifier Overload
Left 813 Audio Overload
Right 813 Audio Overload
Left 5736 Audio Overload
Right 5736 Audio Overload
Left Modulator Overload

Right Modulator Overload<br>Antenna Arc-over<br>Carrier Interruption<br>Power Control Door Interlock<br>Exciter Door Interlock<br>Modulator Door Interlock<br>Left Power Amplifier Door Interlock<br>Center Power Amplifier Door Interlock<br>Right Power Amplifier Door Interlock<br>Rectifier and Filter Door Interlocks<br>Antenna Phasing Door Interlock<br>Search Relay<br>Supervisory Relay Test<br>Spare<br>High Voltage Enclosure Door Interlock

The search relay can be connected into any one of the other transmitter protection systems that are not listed above in order to check the operation of that system in searching for faults. The spare relay is provided for such uses as an antenna house interlock indicator, etc.

The major switching functions, together with their associated indicators, can be duplicated at a transmitter console.

Two clocks are provided. One registers Outage Duration and the other registers the time at which outage occurred.
5. Overload and Safety Protection

The basic overload protection in the Type 50HG-2 Transmitter is designed around two draw-out-type Westinghouse DB-25 Air breakers in the Metal-Enclosed Switchgear Cubicle. These breakers have their own a-c trip coils. One breaker supplies the main rectifiers. The other supplies all other power except that for the breaker trip circuits, blowers, crystal heaters, cubicle lights, and convenience outlets in the transmitter cubicles.

Protection is provided by fast-acting relays and circuit breakers. Any overload, undervoltage, or open interlock will remove the primary power from the supply or supplies involved. The design of the transmitter provides for a choice of automatic or manual return of the transmitter to operation.

With the OVERLOAD PROTECTION CONTROL set in the AUTO position, an overload will trip the set off but power will be reapplied immediately. In the event of successive overloads, the transmitter will trip off three times but, after the third time, power will not be reapplied for a predetermined period of time, normally set for five seconds. After this delay time, power will be automatically reapplied and the transmitter returned to normal operation. If the overloadcondition persists, the sequence will be repeated until the transmitter is turned off manually.

With the OVERLOAD PROTECTION CONTROL in the MANUAL position, any overload which trips the 400 volt supply off will leave the transmitter off until the operator resets the control. Any other overload will trip the transmitter off three times, if the condition persists, and then leave it off until reset by the operator.

A partial list of the overload and undervoltage relays in the transmitter is given below:

```
Undervoltage relays, a-c:
    Main rectifier
    Distribution bus
    Filament
Undervoltage relays, d-c:
    Exciter bias supply
    Left audio driver bias supply
    Right audio driver bias supply
    Left modulator bias supply
    Right modulator bias supply
    Left power amplifier bias supply
    Right power amplifier bias supply
Overcurrent relays, a-c:
    Distribution bus
    Main rectifier
Overcurrent relays, d-c:
    400 volt supply
    1500-3000 volt supply
    Power amplifier supply
    Modulator supply
    RF }813\mathrm{ stage
    Left 5736 RF tube
    Right 5736 RF tube
```

Left modulator tube
Right modulator tube
Left power amplifier tube
Right power amplifier tube
Left 813 audio tube Right 813 audio tube
Left 5736 audio tube
Right 5736 audio tube
De-ion a-c thermal overload breakers: Exciter filaments
Left power amplifier filament No. 1 Left power amplifier filament No. 2 Right power amplifier filament No. 1 Right power amplifier filament No. 2 Left modulator filament No. 1
Right modulator filament No. 2 Left modulator filament No. 3 Right modulator filament No. 4 Switchgear control bus
Panel lights
Transmitter control bus
Bus regulators
Audio bias
RF bias
400 volt supply
1500-3000 volt supply

Other relays employed in the control and supervisory circuits are the time-delay, auxiliary supervisory, stepping, etc., which have not been classified above.

In the entire transmitter there is only one fused circuit affecting operation. That circuit supplies closing power to the distribution bus breaker.

Protective provisions not mentioned above which are included in the transmitter are air interlocks, door interlocks, and the Antenna Arc-Interrupter Unit.

Every reasonable precaution for the safety of personnel is incorporated in the design of the transmitter. All components except those to be installed in the power room are of the deadfront type. The switchgear cubicle uses draw-out type breakers. All cubicle doors which allow access to dangerous potentials are electrically interlocked. In addition, the cubicles are provided with grounding sticks and with automatic mechanical shorting switches which ground dangerous voltages when access doors are opened. It is possible to extend the interlock system to include electrical interlocks on vault doors, phasing cubicle doors, antenna tuning houses, and any other enclosure which the purchaser may desire to protect. The purchaser may also use the keys from the switchgear as the basis for a mechanical door interlock system. The necessary ordering information for such a system may be found under the SUPPLEMENTS in the back of this book.

## MECHANICAL DESCRIPTION

The six transmitter cubicles have welded steel frames and aluminum panels. Each cubicle has four leveling screws. A detachable wiring trough is built into the lower rear of each cubicle, thus providing a full length wiring trough for the interconnection cables. Full length, full width front and rear doors are provided, and each door has a large, unobstructed window. Four large scale meters are mounted on an inclined panel on the top front of each cubicle. Instrument and control panels are illuminated, and each cubicle is equipped with a convenience outlet and a service light. All controls and indicators are completely identified. Details of particular cubicles are listed below:

## 1. Power Control Cubicle

This cubicle functions as the basic power control center for the entire transmitter, and contains the following:

1500-3000 volt supply
De-ion switches
Bus regulator controls Supervisory control relays and lamps
Outage time clock

Outage duration clock
Blower controls
Bias supply controls
Miscellaneous relays

The four large meters at the top of the cubicle indicate Line Current, Line Voltage, Bus Current, and Bus Voltage. Line and Bus Phase Selector switches are provided for the meters. These switches also have an off position. The drop-down panel in the front door provides access to the supervisory control indicators and switches, the two outage clocks, the blower control switches and lamps, and the bias supply switches and indicators.

The front door provides access to all De-ion switches, the bus regulator controls, the meter switches and the elapsed hour meter, all of which are mounted just above the control panel. This door is not interlocked. The rear doors are electrically interlocked and a grounding switch automatically grounds the output of the 1500 volt and 3000 volt supplies.
2. Exciter Cubicle

This cubicle contains the driver sections for the modulator and the power amplifier stages. It also contains the following:

400 volt supply
Exciter RF bias supply
Both audio 5736 bias supplies
Both modulator bias supplies

> Both type FA crystal oscillators
> First, second and driver audio stages
> RF buffer, amplifier, and driver stages

The four large scale meters at the top of the cubicle indicate Left 5736 Audio Cathode Current, Right 5736 Audio Cathode Current, 3000 Volt Rectifier volts and 5736 RF Total Plate Current.

The drop-down panel in the front door allows access to the control panel. This panel, which is hinged to facilitate servicing, mounts the switches and lamps for the 400 volt supply, the 1500-3000 volt supply, and the crystal heater circuits. It also mounts the audio 5736 bias controls, the modulator bias controls, the 813 tank tuning motor drive control, the 5736 tank tuning motor drive control, and the crystal oscillator selector switch. In addition to the position indicating meters associated with the motor driven tuning elements, the following meters are mounted on this panel:

400 Volt Rectifier Voltage
1500 Volt Rectifier Voltage
Left 5736 Audio Driver Bias
Right 5736 Audio Driver Bias
807 Audio Cathode Current
Left 813 Audio Power Amplifier
Cathode Current
Right 813 Audio Power Amplifier
Cathode Current
Left 5736 Driver Grid Current
Right 5736 Driver Grid Current

Left Modulator Bias
Right Modulator Bias
Oscillator Cathode Current
807 RF Buffer Cathode Current
813 RF Amplifier Total Grid Current
813 RF Amplifier Total Cathode
Current
5736 RF Driver Total Grid Current
Left 5736 RF Driver Plate Current
Right 5736 RF Driver Plate Current

The audio circuits are contained in the left side of the cubicle and the radio frequency circuits in the right side, viewed from the front. The controls and indicators on the control panel are correspondingly grouped. When the front door is opened, two smaller doors below the control panel and two tube compartments above the control panel are exposed. The low level audio stages are mounted on the inside of the lefthand door, and the low level RF stages are mounted on the inside of the righthand door. Components and wiring are accessible when these doors are open. The crystal oscillators are individual plug-in units.

The left compartment above the control panel houses the audio 5736 stage, and the right compartment houses the RF 5736 stage.

Audio and RF components mount at the rear on the side walls of the cubicle. A partial partition divides the left and right sides of the cubicle to isolate the audio circuits from the radio frequency circuits. All doors are interlocked, except the drop-down panel.

## 3. Modulator Cubicle

This cubicle contains four tube sockets and four filament transformers (two of each are spares), transfer switches, two feedback dividers, and two gas surge suppressor resistors. The four large scale meters at the top of the cubicle indicate Left Modulator Plate Current, Modulator Filament Volts, Modulator Plate Volts, and Right Modulator Plate Current.

The panel in the front door is fixed in position as there are no controls on this cubicle. On the upper part of this panel are mounted four indicator lamps and a switch. The lamps are "ON" indicators for Left Filament, Bias, Plate, and Right Filament. The switch is used to connect any one of the four filament transformers to the filament voltmeter at the top of the cubicle.

The lower part of the cubicle is used as the plenum chamber for the cooling air. The four filament transformers are mounted from the top of the cubicle, each one directly above its associated tube socket. The plate suppressor resistors and the plate transfer switches are mounted between each front and rear tube. The grid transfer switches are mounted on the side walls between each front and rear tube.

The plenum chamber is equipped with removable metal panels in the front and rear and these panels are interlocked with the air supply. The front and rear cubicle doors are interlocked. The electrical interlocks remove the modulator and driver plate voltage and bias voltages. The mechanical switch grounds the modulator plate supply.
4. Left Power Amplifier Cubicle

This cubicle encloses one side of the push-pull amplifier circuit. It contains one of the power amplifier tubes with provisions for mounting and switching a spare tube, two filament transformers, bias supply, plate choke, neutralizing coil, plate tank capacitor, grid tank circuit, grid leak, overload and under-voltage relays.

The four large scale meters mounted at the top of the cubicle indicate Left PA Filament Volts, Left PA Grid Volts, Left PA Grid Current and Left PA Plate Current.

The basic construction of the cubicle is identical to that of the Modulator Cubicle previously described.

The panel in the front door is fixed and mounts four indicator lamps and a filament voltmeter selector switch. The lower part of the cubicle is used as the air plenum chamber. It has two removable metal access panels which are interlocked with the air supply.

The filament transformers are mounted from the top of the cubicle directly above the tube sockets. The compressed gas plate tank capacitors are mounted in the plenum chamber with their tops protruding for connection to the tuning motor drive. The plate selector switch is mounted between the two tube sockets. A grid parasitic suppressor and a switch are mounted on both side walls near the grid connections to the tubes. The grid tank inductor and capacitor are mounted from the top of the cubicle. The plate choke is mounted in the plenum chamber and the neutralizing coil and its associated capacitors are mounted on the top of the plenum chamber.

The front and rear doors are both interlocked. The electrical interlocks remove the power amplifier and driver plate voltage and bias voltages when either door is opened. The mechanical switch grounds the plate supply.
5. Center Power Amplifier Cubicle

This cubicle is similar in general construction to the Power Control and Exciter cubicles previously described. It contains the power amplifier circuit controls, the plate tank inductor, and the output coupling inductor assembly with the Faraday shield. It also contains the Antenna Arc Interrupter control panel, current transformer-rectifier, the thermo-couple output ammeter and the remote output ammeter and its current transformer-rectifier.

The four large scale meters at the top of the cubicle indicate PA Plate Volts, Total PA Plate Current, RF Output Current, and Total Transmitter Input Power. The drop-down panel in the front door covers the control panel which mounts the following controls and indicators:

> Antenna Arc Protector Control Switch and Indicators Main Rectifier Control Switch and Indicators
> Main Rectifier Regulator Selector Switch
> Main Rectifier Regulator Automatic Voltage Control
> Main Rectifier Regulator Manual-Raise-Lower Switch Main Rectifier Regulator Indicators

The front door, which is not interlocked, provides access to the tuning controls and indicators mounted above the control panel. They are:

> Left Grid Tuning
> Right Grid Tuning
> Ganged Grid Tuning
> Left Plate Tuning

Right Plate Tuning

> Ganged Plate Tuning
> Driver Coupling
> Output Coupling

The indicating instruments are:

```
Left Grid Current
Right Grid Current
Left Plate Current
Right Plate Current
Left Grid Tuning Position
```

> Right Grid Tuning Position
> Driver Coupling Position
> Left Plate Tuning Position
> Right Plate Tuning Position
> Output Coupling Position

On the left, below the center control panel, is the plug-in Antenna Arc Interrupter Unit. To the right is a glass window behind which is mounted the output thermocouple RF ammeter. Near the window is a handle which operates a make-before-break shorting switch for the ammeter.

The interior of the cubicle is partitioned into three sections. The lower half houses the tank inductor, the output coupling inductor, and the output coupling motor drive. The current transformer-rectifier for the output ammeter and the current transformer-rectifier used in the antenna arc interrupter system are also mounted in this section. The upper half of the cubicle is divided into two sections by a vertical partition. These two sections are provided for housing optional antenna phasing components. Cutouts are provided on either side of the upper front panel for bringing out controls for these components.

The rear doors, which are electrically interlocked, provide immediate access to the upper two sections. In addition, removable panels in the lower front and rear of the cubicle allow access to the tank inductor compartment.
6. Right Power Amplifier Cubicle

This cubicle contains the other side of the push-pull amplifier circuit. It is identical to the Left Power Amplifier Cubicle in construction and contents except that the arrangement is reversed for symmetry.
7. Equipment External to the Cubicles

The equipment external to the transmitter cubicles consists of the Switchgear Cubicle, the Power Amplifier and Modulator Rectox Rectifier, the Filter Capacitors and Reactor, the Main Rectifier Induction Regulator if used, the two Bus Induction Regulators, the Main Rectifier Plate Transformer, the three Distribution Bus Transformers, the Modulation Transformer and Reactor, the Blower and Control Box, the Auxiliary Audio Choke, the Modulation Coupling Capacitor, and the

Arc Interrupter Current Transformer-Rectifier. The design of the transmitter provides for control of this equipment from the transmitter cubicles or from a console in the transmitter room. No oil-cooled components are used, making it unnecessary to provide a fire-proof vault.

The Switchgear Cubicle houses the two DB-25 air breakers and associated control system. The cubicle is standard Westinghouse Metal-Enclosed Switchgear and will match other switchgear the purchaser might obtain from Westinghouse for other purposes. This cubicle is intended for installation near the power room, preferably in the wall of the room with the front panel exposed so that manual operation or inspection is possible without entering the room.

The main Rectifier Filter Capacitors and Reactor are intended for installation in the power room.

The Auxiliary Audio Choke is an air core inductor intended for mounting on the wall of the power room.

The Blower is a Sturtevant Silentvane horizontal bottom discharge unit, clockwise rotation. The blower is equipped with a $7-1 / 2$ horsepower motor. Adjustable-pitch sheaves are provided to allow adjustment of blower speed to suit the particular air duct installation. The Blower is intended for installation outside the power room, discharging into the room through the two Rectox units. A Wall Mounting Control Box is supplied for the Blower.

The Current transformer-rectifier used in connection with the Antenna Arc Interrupter system is intended for connection in series with the lead to the antenna in the antenna tuning equipment. It may be wall or bracket mounted.

## RECEIVING, HANDLING, AND STORAGE

Any obvious shortages or damage should be noted by the customer on the waybill and claim made to the transporation company immediately. It is imperative that when unpacked, the equip. ment be inspected mechanically and electrically and a concealed damage claim submitted within the time limit set by the carrier.

## INSPECTION OF THE SHIPMENT

To assist in inspecting and identifying the equipment, the 50HG-2 Transmitter Packing List, which follows, should be used. Note that some of the master items, such as the transmitter cubicles, are shipped with the more fragile components removed. These components will be found separately boxed.

All boxes of the shipment will have stencilled on the outside surface the following information:

1. The box number.
2. Westinghouse style numbers, if applicable.
3. Description and assigned symbol number of units and separately packed components.

Uncrating should proceed as follows:

1. Begin by selecting box No. 1 .
a. Place it in a position near the selected permanent location for this unit.
b. Unpack carefully.
c. Move the unit into place using the section on Handling Procedure as a guide.
2. Select box No. 2, etc.

To further assist in the inventory, identification and assembly of all units and component parts, the following references are submitted:

1. Units of the complete transmitter listed in the INTRODUCTION.
2. Photographs.
3. Wiring Diagrams.

## HANDLING PROCEDURE

1. Lifting and Skidding

Each of the $50 \mathrm{HG}-2$ transmitter cubicles is separately crated and is provided with a standard skid base. This skid base permits the use of rollers and fork lift.

Eye bolts are provided in the top of each cubicle permitting the use of an "A" frame or other hoisting device for lifting. Care should be used to insure that the pull on the eye bolts is largely vertical and that there is little horizontal strain because of the danger of breaking the bolts or bending the cubicle frame. Never use a short sling.

## 2. Uncrating the Cubicles

After the crated cubicle has been rolled into place, remove the crating from the cubicle, leaving the skid base intact. Use care in the removal of the crating to prevent scratching the finish. Next remove the lag screws from the clamps which secure the cubicle to the skid base. From this point the procedure for installation is described in the section on INSTALLATION.

## STORAGE

The 50HG-2 transmitter may be stored in a clean, dry, well ventilated room for an indefinite period provided that the gas pressure is maintained in gas filled capacitors.

## PACKING LIST

This list only includes units of a standard 50HG-2 Transmitter. Any accessory units ordered such as Antenna Phasing Cubicle, Console, etc., will appear on the packing lists included with the shipment.

## 1. Method of Packing

Some of the components within the cubicles such astransformers, chokes, capacitors, and resistors are tied down or supported by bracing or blocking. The interlocks are tied down or removed from their mountings and tied down. The contactors and relays are tied down and their moving contacts secured firmly with tape or blocked with paper. The fluorescent lamps are removed from their sockets, packed separately and placed within the cubicle. The ceramic lead-in bowls are removed, packed separately and placed within the cubicle. Sets of door keys are tied to the front doors, door keepers are removed, packed separately, and placed in the cubicle.

The fragile components which cannot be properly supported within the cubicle are removed from the cubicle and packaged separately as indicated in the packing list below.

Box \#1 Power Control Cubicle - style 1475118
Box \#2 Exciter Cubicle - style 1474773
Box \#3 Exciter Cubicle components
a. Six Metal Rectifier units

| $R X-101$ | $R X-104$ |
| :--- | :--- |
| $R X-102$ | $R X-105$ |
| $R X-103$ | $R X-106$ |

b. Two RF coils

L-109 - WL-813 RF plate tank coil
L-112 - WL-5736 RF plate tank coil
c. Three Capacitors

C-122 - WL-5736 neutralizing capacitor
C-127 - WL-5736 plate coupling
C-129 - WL-5736 plate tank capacitor
Box \#4 Exciter Cubicle components
a. Two crystal oscillator units - style 1472593
b. Two oscillator crystals - the resonant frequency to be specified by the customer

Box \#5 Modulator Cubicle - style 1474774
Box \#6 Modulator Cubicle components
a. Two feedback divider assemblies consisting of 4 resistors in each assembly.

R-210-1 to R-210-4
R-212-1 to R-212-4
b. Two voltage feedback capacitors, C-207 and C-209.
c. Two parasitic chokes, RL-201 and RL-202
d. Four micarta air ducts

Box \#7 Left Power Amplifier Cubicle - style 1475119
Box \#8 Left Power Amplifier components
a. One metal rectifier unit - RX-301
b. One WL-5671 plate RF choke - L-304
c. One WL-5671 plate blocking capacitor - C-319
d. One WL-5671 grid blocking capacitor - C-316
e. One WL-5671 grid tank coil - L-301
f. One WL-5671 neutralizing blocking capacitor - C-318
g. Two WL-5671 grid parasitic suppressors - RL-302 and RL-303
h. Two micarta air ducts

Box \#9 One WL-5671 Neutralizing Coil - L-303
Box \#10 Center Power Amplifier Cubicle - style 1474775
Box \#11 Center Power Amplifier components
a. One WL-5671 plate tank coil - L-401
b. One Load current ammeter - M-415

Box \#12 Right Power Amplifier Cubicle - style 1475120
Box \#13 Right Power Amplifier components
a. One metal rectifier unit - RX-501
b. One WL-5671 plate RF choke - L-504
c. One WL-5671 plate blocking capacitor - C-519
d. One WL- 5671 grid blocking capacitor - C-516
e. One WL-5671 grid tank coil - L-501
f. One WL-5671 neutralizing blocking capacitor - C-518
g. Two WL-5671 grid parasitic suppressors - RL-502 and RL-503
h. Two micarta air ducts.

Box \#14 One WL-5671 neutralizing coil - L-503
Box \#15 Switchgear cubicle - style 1474865, including levering mechanism and 2 instruction books
Box \#16 Switchgear Cubicle component - Type DB-25 breaker - S-2001
Box \#17 Switchgear Cubicle component - Type DB-25 breaker - S-2002
Box \#18 Filter Reactor - Dwg. 7822469
Box \#19 One PA Rectox Rectifier - style 1474566
Box \#20 One Modulator Rectox Rectifier - style 1474565
Box \#21 One Auxiliary Audio Choke - style 1472317, symbol L-1502
Box \#22 One set of Lefthand End Radius
Box \#23 One set of Righthand End Radius
Bqx \#24 One installation kit per Dwg. 7427705
Box \#25 One audio coupling capacitor - style 1081020, symbol C-1502
Box \#26 One RF current transformer-rectifier for antenna arc interrupterstyle 1471694A
Box \#27 One set of vacuum tubes consisting of:

| Qty. |  | Type |
| :---: | :--- | :--- |
| 4 |  | WL-5736 |
| 4 |  | WL-813 |
| 3 |  | WL-807 |
| 2 |  | WL-802 |
| 2 |  | WL-VR-150 |
| 3 |  | RCA 1V |

Box \#28, 29, 30, 31, Contain one each of the WL-5671 thoriated tungsten tubes
Box \#36, 37, 38 One each of the three distribution bus transformers - style
1483783, symbols T-1502A, B, C
Box \#39 One main rectifier plate transformer - Dwg. 50-D-5771, symbol T-1501
Box \#40 One modulation transformer - style 1483785, symbol T-1503
Box \#41 Filter Capacitor - style 1474519, symbol C-1503
Box \#42 Filter Capacitor - style 1474519, symbol C-1504
Box \#43 One each of two Distribution Bus Regulators, style 1486439, symbol YR-1301
Box \#44 One each of two Distribution Bus Regulators, style 1486439, symbol YR-1302
Box \#45 One modulation reactor - style 1453629, symbol L-1501
Box \#46 One blower fan and housing assembly per Dwg. 7426385, symbol BM \#1
Box \#47 Line Starter - Dwg. 7426385, Pt. 10
Box \#48 One 7-1/2 HP motor - S\#1442202 Two R-150 Belts - Dwg. 7426385, Pt. 8
Box \#49 One Vari-pitch Texrope drive - Dwg. 7426385, Pt. 6
Box \#50 One Sheave "Magic-Grip" - Dwg. 7426385, Pt. 7
Box \#51 One Motor Base "Texslide \#3" - Dwg. 7426385, Pt. 9
Box \#52 One each of the items listed below:
a. Station call letters
b. Nameplate S\#1472812
c. RG-17/U cable - 60 ft .
d. RG-62/U cable - 70 ft .
e. One Audio Filter Capacitor S\#1471665, symbol C-1501

## INSTALLATION PLANNING

The 50HG-2 Transmitter has been designed for maximum installation flexibility to fit various situations. This section on installation planning is intended to assist the architect, station engineers and consultants, in planning the building layout and should NOT be considered an exact specification.

## BUILDING LAYOUT

The building plans must include provisions for:
The Transmitter Cubicles
The External Components
The Cooling System
Cables and Conduits
These items are discussed below.

1. Transmitter Cubicles

A suggested equipment layout for a single floor installation appears on figure 27, and for a two floor installation in figure 28.

These figures illustrate the installation of the six transmitter cubicles and their related external equipment.

The cubicle construction of the transmitter provides adaptability to meet individual installation requirements, but it is preferable to install the cubicles in line. If it is necessary to install the cubicles in a different arrangement, however, Westinghouse will assist the purchaser in planning the installation.

Figure 36 and figure 37 illustrate in-line layouts for the six cubicles. The first figure shows the cubicles built into the wall, and the other shows the cubicles installed free-standing. In either case, appropriate end radii are supplied to provide a finished appearance to the transmitter. The installed length of the six cubicles is $289-1 / 2$ inches and the end radii add 12 inches, making a total of 301-1/2 inches. The cubicles are all $54-1 / 4$ inches deep and a minimum clearance of 60 inches should be allowed in front of and behind the cubicles.

A typical $50 \mathrm{HG}-2$ Transmitter cubicle is shown on figure 35. All six cubicles are identical in general construction and the basic installation requirements are the same. The transmitter room floor should be designed to carry a minimum dead load of approximately 4000 pounds per cubicle, although none of the transmitter cubicles actually weigh that much. The floor should include two parallel "I" beams, 50 inches apart, with top faces level with the floor. The cubicles are set on these beams. After all the cubicles are in place and leveled, they are bolted together and the two end cubicles are bolted down to the "I" beams to prevent creepage. Note that the wooden blocks shown on figure 35 are to prevent either: the drill or the tap from contacting concrete.

## 2. The External Components

The equipment external to the six transmitter cubicles is illustrated on figure 33. All of the items on this figure are individual units and installation is mostly a matter of placement and electrical interconnection. However, it is necessary to install the Rectox Units directly in the main air stream.

The remaining power components should be installed in the power room, with the Switchgear Cubicle built into the wall and its front panel available from outside the room.

A suggested layout for these components is shown on figure 27 and figure 28.

## 3. The Cooling System

The basic air supply system is illustrated on figure 39. For a two floor layout, the supply air duct is the power room and for a single floor layout, it is a concrete trench built into the floor. A 26 by 26 inch hole in the floor beneath each cubicle allows the air to flow into the cubicles. See the Transmitter Floor Plan, figure 29.

The cubicles are constructed to direct the cooling air properly through the cubicles and out through the exhaust grills. An exhaust air duct with a cross-section area of at least 12 square feet is required above the cubicles. This duct should be equipped to allow for direct exhaust or for recirculation of air. A Typical Air Exhaust Duct is shown in figure 38. Recirculation of the air may be provided to assist in heating of the building in cool weather.

Two Blowers are installed so that either may be used to supply the cooling air in case a spare blower is purchased. Air Filters for use with these blowers may be installed directly at the intake to the blowers or in the walls of the building, depending on the situation. If desired, a Precipitron electronic air cleaner may also be used in connection with the air supply system. The Blower Outline showing overall dimensions appears on figure 34.

The Rectox Units must be installed in the air stream from the Blowers. These units are constructed to facilitate such installation, the frames themselves actually forming part of the air duct. It is not necessary to provide any direct cooling for the other components in the power room, but allowance should be made for convection air circulation as in the single floor installation.
4. Cables and Conduits

The cable and conduit runs appear on the Power Room Layout figure 31 (Two Floor) and figure 30 (One Floor). These figures illustrate in a general way the cross wiring of the external power equipment. In a two floor plan, two floor openings, in addition to those provided for the cooling system should be provided, directly beneath the transmitter proper. Other openings are required when a control desk and an audio rack are used with the transmitter; see the Transmitter Floor Plan and Power Room Layout on figure 29 and figure 31.

In a single floor installation, two troughs for high voltage conductors and one trough for power and control wires are required. See Power Room Layout (one floor) on figure 30.

## INSTALLATION

The basic installation plan for the $50 \mathrm{HG}-2$ Transmitter includes two centers of placement of the transmitter components. One is the transmitter room, where the transmitter cubicles are installed, and the other is the power room where the equipment external to the transmitter cubicles is installed.

## TRANSMITTER INTERCONNECTIONS

1. The complete interconnection wiring information appears on figures 42 and 43 . Figure 42 lists point-to-point wiring between cubicles and between cubicles and the power room. Figure 43 shows point-to-point wiring for power room components.
2. The types of wires and lugs and their electrical ratings appear on the last sheet of figure 42. Only items so marked in the figure are supplied as part of the transmitter.
a. The wires and lugs shown on figure 42 are suggested types only. If these are not available or not convenient to use, a satisfactory equivalent may be substituted.
b. Other materials, not listed on figure 42 but required for installation are:
(1) Cable clamps and brackets
(2) Conduit and conduit brackets
(3) House breaker box
(4) Hardware

## TRANSMITTER CUBICLES

The transmitter proper consists of six cubicles. Additional cubicles may be added when necessary for directional antenna arrays. Figure 35 (Typical Cubicle) shows all important dimensions and general constructional details of the cubicles. It should, however, only be used to supplement the layout drawings. These cubicles house the major electronic elements of the transmitter as well as all the low voltage supplies, supervisory control circuits and transmitter controls.

The transmitter is generally installed in conjunction with an operating console, as well as racks containing the audio frequency and measuring equipment. For suggested arrangement of the cubicles with the transmitter room, please turn to Building Layout of this instruction book. Proceed to install the transmitter as follows:

1. Place each cubicle in its permanent position by carefully following instructions under Handling Procedure of this instruction book.
2. Align and level all cubicles on the floor rails.
3. Bolt all cubicles together securely by means of $1 / 2^{\prime \prime}-13$ studs, washers and nuts supplied in the Installation Kit. Make sure of good electrical contact between cubicles.
4. Mark hold-down bolt holes in first and last cubicle.
5. Move first and last cubicles back after removing bolts from sides. Drill and tap $1 / 2^{\prime \prime} \mathbf{x}$ 13 holes in the floor rail.
6. Replace cubicles; align and level and bolt cubicles together tightly, making sure of good electrical contact between cubicles. Bolt end cubicles down with two inch $1 / 2^{\prime \prime}-13$ bolts and washers.

At this time the caulking should be done to prevent air leakage. With a caulking gun, apply compound around all the inside and accessible outside edges of the base of each cubicle. The inside may be reached through the air opening in the floor beneath cubicles. This completes the cubicle installation.
7. Install two RG-17/U coaxial cables to connect the RF driver terminals located on the Exciter Cubicle with the RF input terminals on the Power Amplifier cubicles. The four cable plugs for the RG-17/U cable are shipped assembled to the panel terminations mounted on the top of the cubicles. Figure 44 and figure 45 show RG-17/U wiring and termination respectively. In order to preserve circuit balance, the RG-17/U cables must be cut to the same length.
8. Install two . 375 OD hard-drawn copper tube leads to connect the audio driver terminals (two porcelain feed-through bowls) located on top of the Exciter Cubicle with the audio input terminals (located on top of the Modulator Cubicle). Figure 44 shows the audio driver connection between Exciter and Modulator.

## EXTERNAL POWER EQUIPMENT

The Auxiliary Power Equipment shown on figure 33 is installed in the power room adjacent to the transmitter room.

For suggested arrangements of the Auxiliary Power Equipment within the power room, refer to the Auxiliary Components under INSTALLATION PLANNING.

Proceed to install the Auxiliary Power Equipment as follows:

1. The Switchgear Cubicle houses the two DB-25 Air Breakers and associated control system This cubicle is intended for installation near the power room, preferably in the wall of the roon with the front panel exposed and accessible from outside.
2. The two Rectox Frames house the metal rectifiers for the power amplifier and modulatod supplies. They are intended for installation in the air stream, serving as part of the air duct Clearance shall be provided for the spark gaps mounted on top of the frame.
3. The two filter capacitors and the filter reactor should be mounted adjacent to the rector frames and with at least one foot of clearance on all sides.
4. The Main Rectifier Induction Voltage Regulator, if used, should be installed with clear ances of at least two feet from the top and the sides which mount the primary relay, De-ionswitch and potential transformer.
5. The Distribution Bus Induction Voltage Regulators should be installed with clearances of al least one foot on all sides.
6. The Main Rectifier Plate Transformer, and the Modulation Transformer and Modulatior Reactor are floor-mounted. Access to these units is through the front and rear panels and clear ances should be provided accordingly.
7. The three Distribution Bus Transformers are floor-mounted adjacent to the bus regulators. At least $1^{\prime \prime}$ of clearance should be provided about these units.
8. The Auxiliary Audio Choke is an air core inductor intended for wall mounting adjacent to the Modulation Reactor.
9. The Modulation Coupling Capacitor may be floor-mounted (terminals up) near the Modula. tion Transformer, or wall-mounted on a special bracket (bracket is not supplied).
10. The Audio Filter Capacitor is mounted on top of the Modulation Transformer. It is connected to and mounted on secondary terminal $\mathrm{X}-1$ and a ceramic standoff insulator supplied in the Installation Kit.
11. Install all copper tubing conductors using figure 43 as a reference.
a. The Power Room Layout, figure 30 for a one floor building, and figure 31 for a two floor building, may be used as a reference for the copper tubing conduction layout.

## GROUND SYSTEM

Install the transmitter ground strap using figure 43 as a reference.

1. The transmitter cubicle ground strap is placed in the wire trough and runs from cubicle \#1 to cubicle \#6.

This ground strap runs along the inside surface of the rear " I " beam. It is fastened to the center of the "I" beam in each cubicle base using a $1 / 2$ " -13 bolt. The Exciter Cubicle base is then grounded to the transmitter ground system.
2. Each unit of external equipment is grounded to the cubicle ground strap and thus returned to the transmitter ground system.

## INTERLOCKS

## 1. Electrical

Each cubicle is equipped with interlock switches. Additional switches in the air duct, power room, doors to vaults, etc., should be connected into the transmitter control circuit as shown on figure 49, so that any interruption of the interlocking series will remove power from the transmitter.

## 2. Mechanical

In addition to electrical interlocking, the power room can be protected from entry by a mechanical key interlocking system. Inspection of the Switchgear will disclose two keys marked \#RE-1130. These keys, removable only after the switches are locked in their "off" position, can be used to gain entry into the power room, which should be provided with two identical locks so that both switchgear keys are required to gain admittance.

It would be desirable for the air tunnel trap door to be included in this interlock system. See attached copy of "R. and I. E. Kirk Catalog" for suggestions. All door locks other than the two on the Switchgear should be supplied by the customer. To obtain locks using the keys supplied in the Switchgear, it is necessary to supply R. and I. E. Co. with three items of information: (1) Neg. \#4708179, (2) Key \#1130, (3) Type of locks selected as listed in the Kirk Catalogue. A duplicate set of keys is necessary in case the first set is misplaced, but it is recommended that the duplicate set be kept behind non-removable glass so that breakage is necessary to obtain them. A word of warning at this time: Defeating the key interlock or electrical interlock system is dangerous. THE PURPOSE OF THESE SYSTEMS IS TO PROTECT LIFE.

## COOLING SYSTEM

1. Ducts

After the transmitter is bolted down in its final location, the exhaust air duct can be installed. A typical installation is shown on figure 38. If sound-proof duct lining is used, it must be of fire-proof material. The duct work should be extended to all locations requiring heat and should be equipped with automatic or manually controlled registers. See figure 39, Basic Air Supply System.

For discharge of the heated air to the outside, a ventilator in the roof or ventilators on two sides of the building should be provided to take advantage of the prevailing winds. Self-closing shutters to prevent back-draft are extremely important to prevent back pressure from reducing the flow of cooling air to a dangerous level. Screening should be provided to prevent entry of small animals and birds.

## 2. Air Returns

An unrestricted air return circuit to the blowers should be planned for normal recirculation. This may be in the form of gratings in the floor, doors, walls or a combination of gratings and filters so arranged as to disperse the flow of air and reduce the velocity. Care should be taken to see that the total back resistance pressure of the return circuit is not excessive for the volume of air handled, (approximately 12,000 CFM). The exhaust duct should not present more than $1 / 4$ " water gauge pressure drop.
3. Air Requirements

Normal air requirement for the $50 \mathrm{HG}-2$ Transmitter at sea level in the ambient range $+5^{\circ}$ to $+45^{\circ} \mathrm{C}$, is approximately $12,000 \mathrm{CFM}$ at a resistance pressure of $2^{\prime \prime}$ water gauge. The fan speed for this delivery is $570 \mathrm{RPM}(4.6 \mathrm{HP})$. If necessary, the fan speed can be regulated between 460 RPM and 875 RPM by means of the "Vari-Pitch" sheave. The oil level indicators on the bearings should be installed and the bearings filled to proper level with a good quality oil (SAE 10). Check frequently for the first week after filling to be sure that the fan bearing cups maintain a safe oil level.
4. Blower

The Blower supplied with the transmitter is a Sturtevant "Silentvane," size 90 shown on figure 34. Make certain the Blower is mounted on a level surface.
5. Motor

The motor supplied is Westinghouse Type CPS "Life-line" with standard NEMA frame No. 284. The electrical characteristics are $7-1 / 2 \mathrm{HP}$, three phase, $50 / 60$ cycles, $220 / 440$ volts with medium starting torque. The slide base is an Allis-Chalmers "Texslide No. 3." Some slipping of the belts will be noticed upon starting. This is a normal condition and helps to limit the motor starting current.
6. Sheaves and Belts

The motor is equipped with an Allis-Chalmers "Vari-Pitch" wide-range, two groove sheave allowing a variation from $5-1 / 4$ inch pitch diameter to 10 inch pitch diameter. The Blower has a fixed, two groove sheave of 20 inch pitch diameter. Belts for the above are of a special section to allow for the wide range of speed variation and are known as R-150 "Texrope." A word of caution when replacing belts; always replace both belts, since a new belt will have a shorter circumference than a used one.

## 7. Starter

The motor starter is a combination switch (with magnetic trip overload protection) and contactor (with thermal trip overload protection). Connections to the starter should be made as shown on figure 43. It is recommended that the starter be installed within sight of the blower motor.

## 8. Filters

Some means of cleaning the circulated air should be employed. This may be in the form of spun glass filters or the highly efficient Westinghouse Precipitron. In many cases both are used. The Precipitron is used to clean air brought in from the outside and the spun glass filters are used to clean the recirculated air.

The recommendation of Owens-Corning to filter $12,000 \mathrm{cfm}$ of air is to use 15 of their \#2, $20^{\prime \prime} \times 20^{\prime \prime}$ "Dust Stop" filters. This allows each filter to pass 800 cfm and thus maintain maximum cleaning efficiency. The average resistance of the \#2 filter when clean is . $13^{\prime \prime}$ water gauge. (This drop doubles when they are stacked double.) A loss of more than . $15^{\prime \prime}$ water gauge for the inlet is not recommended.

The Westinghouse District Office has among its personnel a specialist in Precipitron installation and filter problems. He will be glad to give assistance and make recommendations.

## HEATING FACILITIES

Approximately 50 kw is available for use in heating the transmitter building, when the transmitter is in full power operation.

## INITIAL ADJUSTMENT AND TESTS

Before proceeding with these tests, the following should be observed:

1. Transmitter installation should have been completed according to the section on RECEIVING, HANDLING, AND STORAGE and the section on INSTALLATION of this book.
2. Make a thorough mechanical inspection of the transmitter installation, noting particularly that good wiring practice is used throughout. Check all wires to make sure that the lugs have been properly applied. Burndy-type lugs depend entirely upon the success of the clamping operation for electrical continuity, therefore it is imperative that the proper size lug is properly installed.
3. Check mechanical operation of all doors to make sure that the latches are functioning properly, and that the mechanical and electrical interlocks which depend upon door operation have been installed in their proper places and have been adjusted for positive action.
4. Check the mechanical operation of all relays and make sure that all traces of packing, plocks, twine, tape, wires, etc., have been removed.
5. Remove VR-150, 802, 807, and 813 tubes from their sockets. Disconnect filament leads from the 5736 and 5671 tubes.
6. Make sure that all switches and breakers are off and that the 460 volt, three phase, incoming line is deenergized.

## GROUNDS AND SHORT CIRCUITS

1. Open fuses F-2001, F-2002, F-2003, F-2006, F-2007 in Switchgear Cubicle and test 460 volt lines for short circuits and grounds. Use megger ( 500 volts d-c).
2. Replace fuses, check 460 volt line for grounds.
3. Remove two primary line wires from Distribution Bus Transformers, T-1502, A, B, C. Check for short circuits and grounds. Replace wires.
4. If a Main Rectifier Regulator has been purchased, disconnect leads No. 1 and No. 3 from Main Regulator YR-1201, two leads from primary of Main Rectifier Plate Transformer T-1501, and one fuse from potential transformer on Regulator YR-1201. Check lines for short circuits and grounds. Replace connections.
5. Remove ground from secondary of Distribution Transformer T-1502-B and remove two incoming bus wires from TS-20 in the Power Control Cubicle. Remove fuse F-1C from tube hour meter M-7. Check both ways for shorts and grounds on all wires of bus. Check only for grounds in Distribution Transformer direction.
6. Replace fuse and wires in Power Control Cubicle, but do not replace ground on Distribution Transformer secondary.
7. a. Connect an ohmmeter between ground and a distribution bus wire, then close in sequence the power control De-ion switches shown below:
```
S-1, LEFT PA FILAMENT NO. 1
S-2, LEFT PA FILAMENT NO. 2
S-3, RIGHT PA FILAMENT NO. 1
S-4, RIGHT PA FILAMENT NO. 2
S-5, LEFT MODULATOR FILAMENT NO. 1
S-6, RIGHT MODULATOR FILAMENT NO.2
S-7, LEFT MODULATOR FILAMENT NO. }
S-8, RIGHT MODULATOR FILAMENT NO. 4
```

S-10, PANEL LIGHTS
$\times$ S-11, TRANSMITTER CONTROL BUS
S-12, EXCITER FILAMENTS
S-13, AUDIO BIAS
S-14, RF BIAS
S-15, 400 VOLT SUPPLY
S-16, 1500 VOLT - 3000 VOLT SUPPLY
S-22, BUS REGULATOR

No ground should appear.
7. b. If a Main Rectifier Regulator has been purchased, turn on VRS-1201 on the Main Regulator. Operate AUTO/MANUAL, LOWER/RAISE switches S-19 and S-20 in the Power Control Cubicle and VOLTAGE CONTROL SELECTOR and MANUAL VOLTAGE CONTROL switches S-411 and S-412 in the Center Power Amplifier Cubicle. No ground should appear.
8. Close manually, in sequence, the DN magnetic contactors $\mathrm{K}-37$ to $\mathrm{K}-40$ in the Power Control Cubicle. No ground should appear.
9. Remove ground from secondary of switchgear control transformer (T-2005) and check for grounds. No ground should appear. Replace lead.
10. Open TRANSMITTER CONTROL BUS switch and observe 27.5 ohms d-c resistance between Power Control terminals No. 61 and No. 73 with all cubicle doors open.
11. Measure (with ohmmeter or bridge using less than 10 volt battery) the resistance at terminals of the following Rectox units. (Do not remove Rectox from circuit, since this is primarily a check of the associated circuit and not of the Rectox Units.) The resistance should be approximately as indicated.

| Unit | Term. | Res. |  |  | Term. |
| :---: | :---: | :---: | :---: | :---: | :---: |

12. Measure insulation resistance, using potential not less than 500 volts d-c, of high voltage conductors in power room.
a. Conductors from T-1501 to both high voltage rectox units.
b. Conductors from high voltage rectox units to filter capacitors and reactor.
c. Conductors from filter units to Modulation Transformer and Modulation Reactor.
d. Conductors from Modulator and Power Amplifier to Modulation Transformer and to Audio Auxiliary Choke. Do not disconnect leads from transmitter: Doors to Modulator and Power Amplifier cubicles must be closed.
e. Investigate any of above, a to d readings, if less than 50 megohms.
f. Connect automatic capacitor shorting switches on the three filter capacitors to the voltage bus with No. 28 bare copper wire. Bend the springs up so ends are level with the high voltage terminals. (Note: This fuse wire is supplied in the Installation Kit.)

## SWITCHGEAR ADJUSTMENTS

Before application of power the two type DB-25 circuit breakers S-2001 and S-2002, mounted in the Switchgear Enclosure should be withdrawn part way out of the enclosure using the extension rails and levering handle.

Inspect the two breakers with the aid of the inspection list furnished on page 7 of $1 . \mathrm{B} .35-225-1$, Check the overcurrent tripping devices for proper settings as follows:

1. Long time delay setting

| S-2001 | $100 \%$ of rated current |
| :--- | ---: |
| S-2002 | $80 \%$ of rated current |

2. Instantaneous settings
$\begin{array}{ll}\text { S-2001 } & 1000 \% \text { of rated current } \\ \text { S-2002 } & 1000 \% \text { of rated current }\end{array}$
The above adjustments are normally accomplished at the factory but should be checked prior to the application of power to the equipment. For details of adjustment, consult I.B. 35-225-1 pages 15 through 18.

## RELAY SETTINGS

1. Set overload relays as follows, and using battery, rheostat, and ammeter, check operating point by application of test leads to relay coil terminals. Do not remove shunting resistors.

| Symbol | Description | Scale Setting | Operating Point |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\times \mathrm{K}-9$ | 1500/3000 Volt | 5.5 amp 6.7 | 4.5 | to | 5.5 |  |
| $\times \mathrm{K}-11$ | Modulator Rectifier | $9.5 \mathrm{amp} / / 4$ | 8.5 | to | 9.5 |  |
| 入K-12 | Power Amplifier Rectifier | 11.5 amp 14 | 11.0 | to | 12.0 |  |
| $\times \mathrm{K}-105$ | 400 Volt | 0.4 amp 6 | 0.45 | to | 0.65 | amp |
| $\times \mathbf{K}-106$ | 813 RF | 0.6 amp 75 | 0.5 | to | 0.7 | al |
| $\times K-107$ $\times K-108$ | Left 5736 RF | $1.4 \mathrm{amp} / .6$ | 1.05 | to | 1.35 | m |
| Y K-108 | Right 5736 RF | 1.4 amp | 1.05 | to | 1.35 | amp |
| K-110 | Left 813 Audio | 0.15 amp | 0.14 | to | 0.16 | amp |
| K-111 | Right 813 Audio | 0.15 amp .16 | 0.14 | to | 0.16 | amp |
| K-114 | Left 5736 Audio | $0.25 \mathrm{amp}, 3$ | 0.5 | to | 0.7 | amp |
| $\mathrm{K}-115$ $\times \mathbf{K}-201$ | Right 5736 Audio | 0.25 amp , 3 | 0.5 | to | 0.7 | amp |
| $\times$ K-202 | Right Modulat | 3.5 amp | 4.2 | to | 4.8 | amp |
| K-301 | Left Power Amplifier | 3.5 amp | 4.2 | to | 4.8 | amp |
| $\times \mathbf{K}-501$ | Right Power Amplifier | 3.0 amp | 4.4 4.4 | to | 4.8 4.8 | amp |

2. Set bias undervoltage relays:

| Symbol | Description | Scale Setting |
| :---: | :---: | :---: |
| X K-109 | Exciter | 90 volts |
| $\chi_{\times} \mathrm{K}-112$ | Left Audio Driver | 50 volts |
| K-113 | Right Audio Driver | 50 volts |
| X K-203 | Left Modulator | 90 volts |
| $\times \mathrm{K}-204$ | Right Modulator | 90 volts |
| $\times \mathrm{K}-302$ | Left Power Amplifier | 60 volts |
| $\times \mathrm{K}-502$ | Right Power Amplifier | 60 volts |

I. B. $81-120-2 \mathrm{~A}$

## GAS FILLED CAPACITORS

Capacitors which are identified with symbols C-129, C-320, C-517 and C-520 are Lapp gasfilled, variable capacitors.

Observe the following precautions when handling these capacitors, (also refer to Lapp Bulletin 266 in the SUPPLEMENT section of this instruction book):

1. When first received:
a. Check for possible damages.
b. Check gauge pressure. This should be between 50 and 65 psi .
c. Measure safety gap spacing and record for future reference.
d. Check gauge pressure frequently to make no leaks.
2. Before installation:
a. If gauge pressure is between 50 and 65 , add oil pumped dry nitrogen to 150 .
b. If gauge pressure is below 50, add Freon gas ( $\mathrm{F}-12$ ) to 65 and then add oil pumped dry nitrogen to 150 .
c. Check safety gap spacing.
3. After installation:
a. Inspect periodically to see that the proper gauge pressure $(150 \pm 20)$ is maintained.
b. If gauge pressure is less than 85 , drain to 2.5 and refill to 65 with Freon ( $\mathrm{F}-12$ ) and then to 150 with oil pumped dry nitrogen.
c. If $\mathrm{g}_{\mathrm{g}} \mathrm{gauge}$ pressure is 85 or more, refill to 150 with oil pumped dry nitrogen.
d. Keep ceramic bowl clean and dry.

## 4. Storage

a. See that the gauge pressure is between 100 and 150 so that the gaskets will be held in proper position to prevent leakage.

## RF COMPONENT SETTINGS

The following information is to be used as a guide in adjusting the Type 50HG-2 Transmitter for operation on a specific carrier frequency. At frequencies for which a choice of adjustments exists, either will be suitable.

1. Crystal Oscillator, Type FA
a. L-102

540 to 650 KC - connect tap 6 to tap 5
650 to 840 KC - connect tap 6 to tap 4
840 to 1300 KC - connect tap 6 to tap 3
1300 to 1600 KC - connect tap 6 to tap 2
b. L-103

540 to 650 KC - connect plate to 1 , output to 2
650 to 840 KC - connect plate to 2, output to 3
840 to 1000 KC -connect plate to 2, output to 4
1000 to 1300 KC - connect plate to 3, output to 4
1300 to 1600 KC - connect plate to 4 , output to 4
2. 807 Buffer Amplifier
a. L-105

540 to 660 KC - use all sections
660 to 808 KC - short out one section (nearest panel)
808 to 985 KC - short out two sections (nearest panel)
985 to 1300 KC - short out two sections (nearest panel)
1300 to 1600 KC - short out three sections (nearest panel)
3. 813 RF Plate Tank
a. L-109

540 to 660 KC - use all (62) turns


X 660 to 800 KC - short out 7 turns on each end
800 to 900 KC - short out 11 turns on each end
900 to 1020 KC - short out 15 turns on each end
1020 to 1300 KC - short out 19 turns on each end
1300 to 1600 KC - short out 23 turns on each end
b. L-109-Grid tap and neutralizing tap

540 to $660 \mathrm{KC}-17$ turns above and below center tap
660 to $800 \mathrm{KC}-15$ turns above and below center tap
800 to $900 \mathrm{KC}-13$ turns above and below center tap
900 to $1000 \mathrm{KC}-11$ turns above and below center tap
1000 to $1100 \mathrm{KC}-9$ turns above and below center tap
1100 to $1300 \mathrm{KC}-7$ turns above and below center tap
1300 to $1400 \mathrm{KC}-6$ turns above and below center tap
1400 to $1600 \mathrm{KC}-5$ turns above and below center tap
4. 5736 Plate Tank
a. L-112 - Tap location

540 to 600 KC - 13-3/4 turns from ground
600 to $660 \mathrm{KC}-12-3 / 4$ turns from ground
660 to $800 \mathrm{KC}-12-3 / 4$ turns from ground
800 to $1000 \mathrm{KC}-12-3 / 4$ turns from ground 1000 to $1300 \mathrm{KC}-11-3 / 4$ turns from ground 1300 to $1500 \mathrm{KC}-10-3 / 4$ turns from ground 1500 to $1600 \mathrm{KC}-8-3 / 4$ turns from ground
b. $\mathrm{C}-129$ - A

540 to 600 KC - use 4 adders $560 \mu \mu \mathrm{f}$ each
600 to 660 KC - use 3 adders $560 \mu \mu \mathrm{f}$ each
660 to 800 KC - use 2 adders $560 \mu \mu \mathrm{f}$ each
800 to 1000 KC - use 1 badder $560 \mu \mu \mathrm{f}$ each
1000 to 1600 KC - none
5. Left and Right Power Amplifier Grid Circuit
a. L-301 or L-501

540 to 600 KC - use all turns
600 to 660 KC - short out 2 turns
660 to 800 KC - short out 7 turns
800 to 1000 KC - short out 13 turns
1000 to 1300 KC - short out 15 turns
1300 to 1600 KC - short out 18 turns
6. Left and Right Power Amplifier Neutralizing Circuit
a. L-303 and L-503 - See Power Amplifier Neutralization

540 to 660 KC - total turns 196
660 to 1000 KC - total turns 156
1000 to 1600 KC - total turns 96
7. Power Amplifier Plate Tank
a. $\mathrm{L}-401-\mathrm{A}$

540 to 750 KC - use all turns
750 to 800 KC - short out one turn each end of coil
800 to 1000 KC - short out two turns each end of coil
1000 to 1200 KC - short out three turns each end of coil
1200 to 1500 KC - short out four turns each end of coil
1500 to 1600 KC - short out five turns each end of coil
b. C-320-A and C-520-A

540 to 800 KC - one $450 \mu \mu \mathrm{f}, 45 \mathrm{KV}$ Capacitor

## POWER-ON ADJUSTMENTS

## WARNING

THE USE OF HIGH VOLTAGES IS NECESSARY FOR THE OPERATION OF THE ELECTRONIC EQUIPMENT COVERED BY THESE INSTRUCTIONS. WHILE ALL PRACTICAL SAFETY PRECAUTIONS HAVE BEEN INCORPORATED IN THE DESIGN OF THIS EQUIPMENT, THEY ARE NOT INFALLIBLE; THEREFORE, ALL PRECAUTIONARY MEASURES MUST BE CAREFULLY OBSERVED BY THE OPERATING PERSONNEL DURING THE OPERATION, INSPECTION AND MAINTENANCE OF THE EQUIPMENT. SEE WARNING IN THE FRONT OF THIS BOOK.

## POWER LINE VOLTAGE

Apply 460 volts a-c to Switchgear. All De-ion switches should be off and all control switches turned to left (if no duplicate controls have been connected). Observe that the line voltage meter reads 460 volts, and the line current meters reads zero.

## BLOWERS

Turn on as follows:

1. Turn S-30 (BLOWER CONTROL) to BLOWER ONLY position.
2. Turn S-29 (BLOWER SELECTOR) to No. 1 position.
3. Close S-9 (SWITCHGEAR CONTROL BUS).
4. Turn S-28 (BUS BREAKER) on. Observe:
a. Indicator I-40 (BUS BREAKER SWITCH ON) lights.
b. Blower No. 1 starts; check direction of rotation.

If not same as arrow on blower housing, reverse two leads on blower motor.
c. After Blower No. 1 comes up to normal speed, S-515 (air flow interlock) operates allowing I-36 (BLOWER NO. 1 ON) to light.
5. If a spare blower has been purchased, turn BLOWER SELECTOR to NO. 2 position. Observe: Blower No. 2 starts; check direction of rotation. I-41 (BLOWER NO. 2) lights.

## AIR VELOCITY

1. Measure air velocity at following points using an integrating vane-type anemomett * such as the four-inch diameter "CENCO" anemometer, (Central Scientific Co., Chicago, Ill. Cat. No. 78605).

Measurements on the power tubes should be the average of maximum readings around the tube with the instrument held horizontal just above the radiator fins and midway between the glass bulb and the outside edge of the radiator. The Rectox units must be installed, all tubes in tube sockets, all cubicle doors must be closed, and exhaust ducts in normal condition when measurements are taken.

| Location | Component | Minimum Velocity, Fpm |
| :---: | :---: | :---: |
| Power Control | RX-1 | 1000 |
| Exciter | RX-104 | 800 |
| Modulator | Each WL-5671 | 1000 l/w |
| Left Power Amplifier | Each WL-5671 | 1000 |
| Left Power Amplifier | RX-301 | 800 |
| Right Power Amplifier | Each WL-5671 | 1000 |
| Right Power Amplifier | RX-501 | 800 800 |

2. Remove one 5736 tube from its socket on the left side of the Exciter and measure air velocity to be 800 fpm minimum. Replace tube and remove one 5736 from right side and measure air velocity to be 800 fpm minimum.
3. Orient the air nozzles in the Modulator, Left Power Amplifier and Right Power Amplifier cubicles so that air is directed on the 5671 tube filament seals.
4. If necessary, change speed of Blowers by adjusting "Vari-Pitch" sheave or install baffles to meet above minimum air requirements.

## DISTRIBUTION BUS

Check that primary switch positions on T-1502-A, B, C are all on position 3. Positions 1 and under top cover plates.

1. Turn BLOWER CONTROL to TRANSMITTER AND BLOWER position. Observe:
a. The Distribution Bus Breaker closes. (Do not allow breaker to "pump." If abnormal operation is encountered, see Switchgear Instruction Book I.B. 35-225-1 in SUPPLEMENT Section.)
b. I-35 (BUS BREAKER ON) lights.
c. M-4 (BUS VOLTAGE) indicates 230 volts on each of the three phases selected by S-18 (BUS METERS PHASE SELECTOR). Note that if the phase voltages are not inbalance, throw S-19 (BUS REGULATOR SELECTOR CONTROL) to MANUAL position; throw S-22 (BUS REGULATOR) to its ON position; hold S-20 (BUS REGULATOR MANUAL CONTROL) in its LOWER position until both regulators have reached their lower limit positions and all three phases are balanced. Next, hold S-20 in its RAISE position until all three phases show 230 volts.
d. With S-19 in AUTOMATIC position, note that the bus voltages on each of the three phases are equal ( 230 volts). See Regulator Instruction Book 5521-A for adjustment of regulator relays in case the three phases are unbalanced or not 230 volts.

## FILAMENT VOLTAGES

1. Throw S-12 (EXCITER FILAMENTS) to ON position. Observe:
a. K-8 (Exciter filament undervoltage) timing relay begins to operate and should close after a 22 -second delay, lighting I-42 (EXCITER FILAMENT NORMAL VOLTAGE) indicator. Note that K-8 should be adjusted to close in 22 seconds and drop out in 5 seconds. See Instruction Leaflet 41-291D in SUPPLEMENTS Section of this book.
b. The Exciter filament transformers should be energized.
2. Voltages at the filament terminals of the following tube sockets: (bus voltage 230 volts)

3. Voltages at all 5736 filament connectors:

|  | Filaments Not <br> Connected | Filaments <br> Connected |
| :--- | :---: | :---: |
| Audio WL-5736 | 5.9 to 6.5 volts |  |
| RF WL-5736 | 5.9 to 6.5 volts |  |
|  | 5.7 to 6.3 volts 5.8 |  |
|  |  |  |

4. Modulator and Power Amplifier filament voltages.
a. Make sure that filament connectors are not touching filament terminals of 5671 tubes in Modulator, Left Power Amplifier, Right Power Amplifier.
(1) Turn ON all filaments in Modulator, Left Power Amplifier and Right Power Amplifier.
(2) Observe, using filament voltmeter selector switch on each cubicle, that each voltage is 10 to 11 volts.
(3) Try combinations of Power Amplifier Filament Switches, S-1, 2, 3, 4. Check voltages to be same as above.
(4) Turn Bus Breaker OFF and connect all 5671 filaments.
(5) Repeat (1), (2), (3) above, and observe each filament voltage to be between 9.6 and 10.2 volts. (Bus voltage 230 volts on all three phases.) Using an accurate laboratory-type voltmeter, measure voltage at filaments of the 5671 tubes. Adjust the indication on M-202, M-301, M-501 to be the same as the laboratorytype voltmeter (adjust zero set screw). Do this after the set has been checked and operated long enough for voltmeters to have reached operating temperature.

## EXCITER BLAS AND PLATE VOLTAGES

Adjust Bus Voltage to be 230 volts.

## 1. Audio Bias

Close S-13 (AUDIO BIAS). Turn on S-31 (AUDIO BIAS). Observe:
a. I-43 (AUDIO BIAS SWITCH ON) lights, (amber).
b. K-37 (audio bias contactor) operates.
c. M-111 (LEFT 5736 AUDIO DRIVER BIAS), 130 volts - adjusted by R-119.
d. M-112 (RIGHT 5736 AUDIO DRIVER BIAS), 130 volts - adjusted by R-120.
e. M-116 (LEFT MODULATOR BIAS), 330 volts - adjusted by S-108.
f. M-117 (RIGHT MODULATOR BIAS), 330 volts - adjusted by S-109.
g. The following undervoltage relays operated, and bias ON indicators light.

K-112, I-38, Power Control AUDIO BIAS ON (red)
K-113, I-403, Center Power Amplifier AUDIO BIASES ON (green)
K-203, K-204, I-202, Modulator BIAS (green)
2. RF Bias

Close S-14 (RF BIAS). Turn on S-32 (RF BIAS). Observe:
a. I-44 (RF BIAS SWITCH ON), (amber).
b. K-38, RF bias contactor operates.
c. M-302 (LEFT PA GRID VOLTS), 340 to 360 volts.
d. M-502 (RIGHT PA GRID VOLTS), 340 to 360 volts.
e. K-109 (exciter bias undervoltage) closes, I-39 (RF BIAS ON), (red) and I-404 (RF BIASES ON), (green) light.
f. K-302 (left power amplifier bias undervoltage) closes, I-302 (BIAS), (green) lights.
g. K-502 (right power amplifier bias undervoltage) closes,I-502 (BIAS), (green) lights.
h. Using a d-c voltmeter, observe 300 to 400 volts negative from RF 5736 tube grids to ground.
3. 400 Volt Supply

Close S-15 ( 400 VOLT SUPPLY) on Power Control Panel. Turn on S-103, ( 400 VOLT SUPPLY) switch on Exciter Control Panel. Observe:
a. I-105 (amber) lights. (SWITCH ON).
b. K-39 closes - contactor, 400-volt supply.
c. I-106 (red) lights - (POWER ON).
d. M-118 (400 VOLT RECTIFIER) indicates between 440 and 460 volts.

14 mae . M-101 (OSCILLATOR CATHODE CURRENT) indicates between 10 and 14 milliamperes. Note that as the oscillator is tuned through resonance by adjusting C-105, that the 802 cathode current goes through a sharp dip, a gradual rise and then a sharp rise.
f. M-102 ( 807 RF BUFFER CATHODE CURRENT) indicates between 35 and 55 ma . Tune to minimum with $\mathrm{C}-112$ (plate tank capacitor).
g. M-103 (813 RF AMPLIFIER TOTAL GRID CURRENT) indicates between 14 and 18 ma .
4. 1500 Volt Supply

Put S-110 in OPERATE and S-111 in TUNE and put S-113 in OPEN position. Close S-16 ( 1500 VOLT - 3000 VOLT SUPPLY) in Power Control. Turn on S-104 (1500-3000 VOLT RECTIFIER) on Exciter Control Panel. Observe:
a. I-107 (green) lights (SWITCH ON).
b. K-40 closes - contactor, 1500-3000 volt supply.
c. I-108 (red) lights - (POWER ON) and K-104 operates 807 and 813 screen interlock relay).
d. Using S-106 (813 RF AMPLIFIER PLATE TUNING), tune for maximum reading on M-108 (1500 VOLT RECTIFIER).

## RF DRIVER NEUTRALIZATION

1. Turn off 1500-3000 VOLT RECTIFIER and couple a wavemeter, or some other RF indicating device to the RF 5736 plate tank ( $L-112$ ). A suggested method is to use link coupling, with one $6^{\prime \prime}$ turn on each end of link, and place the wavemeter outside the cubicle.
2. Remove cable plugs (RG-17/U from sockets on top of cubicle.
3. Turn on 1500-3000 VOLT RECTIFIER and adjust S-107 (5736 RF DRIVER PLATE TUNING) for maximum indication on wavemeter.
4. Readjust 813 RF AMPLIFIER PLATE TUNING for maximum indication on wavemeter.
5. Adjust neutralizing capacitor ( $\mathrm{C}-122$ ) for minimum indication on wavemeter. (A piece of cord may be wrapped around the sleeve of C-122 to permit adjustment from outside the cubicle.)
6. Place S-111 in OPERATE position and repeat 3, 4, and 5 above.

## MAIN RECTIFIER REGULATOR OPERATION

When a Main Rectifier Regulator (YR-1201) is supplied with $50 \mathrm{HG}-2$ equipment, power wiring should be according to figure 43 and control circuit wiring according to figure 42.

1. With S-421 (MAIN RECTIFIER CONTROL) in the off position, YR-1201 has run down to minimum position and the DELTA-WYE contactors are deenergized. No power is applied through the switchgear breaker, S-2002.
2. With switch S-421 in the "TUNE" position, power is applied to the primary of T-1501 through the WYE contactor. The regulator will automatically run up to a predetermined voltage when S-411 (REGULATOR CONTROL SELECTOR) is in the "AUTOMATIC" position.

With S-411 in the "MANUAL" position, the regulator is controlled by S-412 (MANUAL VOLTAGE CONTROL) and any desired voltage in the range 6 to 10 kv approx. may be obtained.
3. With switch S-421 in the "ON" position, power is applied to the primary of T-1501 through the "DELTA" contactors. If S-411 is in the "AUTOMATIC" position when going from "TUNE" to "ON", the regulator will have reached its "HIGH LIMIT" and the increase in voltage is brought about by the change in transformer primary connections from WYE to DELTA. If S-411 is in the "MANUAL" position when S-421 is placed in the "ON" position, any desired voltage in the range 9 kv to 12 kv approx. may be obtained.

## MAIN RECTIFIER REGULATOR ADJUSTMENTS (IF USED)

1. Remove conductors from primary terminals of T-1501 (Main Rectifier Plate Transformer).
2. Connect secondary links on Main Rectifier Plate Transformer from No. 4 to No. 6 on all three phases.
3. Place S-411 (REGULATOR CONTROL SELECTOR) in MANUAL position.
4. Release brake on YR-1201 (Main Rectifier Induction Voltage Regulator).
5. By hand, rotate regulator to full LOWER position (full counterclockwise on regulator LOWER-RAISE dial). Observe:

> I-407 (LOW LIMIT) indicator on Center Power Amplifier Control Panel lights.
6. Rotate regulator to full RAISE position (full clockwise on regulator LOWER-RAISE dial). Observe:

> I-408 (HIGH LIMIT) indicator on Center Power Amplifier Control Panel lights.
7. Rotate regulator to mid-range (zero on LOWER-RAISE dial).
8. Set brake on regulator.
9. Block the undervoltage relay on the primary relay panel of regulator in the closed position. This can be done by inserting insulating material between the righthand contact (as seen from the front) and the movable contact, and then screwing up the adjustments on the contacts until the movable contact is firmly against the lefthand contact of the undervoltage relay.
10. Close VRS-1201 (De-ion breaker mounted on side of regulator).
a. If motor runs the regulator toward RAISE, immediately open breaker and interchange two leads from the regulator motor. (Terminals for the motor are under the limit switch cover.)
b. Close breaker and allow motor to run regulator down to lower limit and stop.
11. Turn S-421 (MAIN RECTIFIER CONTROL) ON. Observe:
a. I-406 (green) lights - (SWITCH ON).
b. K-1601 and K-1602 (Modulator bleeder contactors on Rectox Frame) operate.
c. S-2002 (Main Rectifier Breaker in Switchgear) closes.
d. I-203 (PLATE), I-303 (PLATE), I-405 (MAIN RECTIFIER POWER ON), I-503 (PLATE) (all red) light on Modulator, Left Power Amplifier, Center Power Amplifier, and Right Power Amplifier, respectively.
e. Determine that three phase output voltage of Main Rectifier Regulator is between 350 and 380 and that all three phase voltages are equal.
12. Operate S-412 (MANUAL VOLTAGE CONTROL) and determine that regulator runs in proper direction.
13. Turn MAIN RECTIFIER CONTROL off and observe that regulator runs downto lower limit stops.
14. Turn MAIN RECTIFIER CONTROL on and S-411 (VOLTAGE CONTROL SELECTOR) to AUTOMATIC and observe that regulator setting is under control of R-417 (AUTOMATIC VOLTAGE CONTROL).

## MAIN RECTIFIER POWER ADJUSTMENTS

1. Remove conductors from primary terminals of T-1501 (Main Rectifier Plate Transformer).
2. Connect secondary links of Main Rectifier Plate Transformer from No. 4 to No. 6 on all three phases.
3. Turn S-421 (Main Rectifier Control) to the TUNE position. Observe:
a. I-406 (green) lights - (SWITCH ON).
b. K-1601, K-1602 (bleeder contactors in Rectox Frame) operate.
c. K-1503 in High Voltage Transformer operates connecting primaries in Wye.
d. S-2002 (Main Rectifier Breaker in switchgear) closes.
e. I- 203 (PLATE), I-303 (PLATE), I-405 (MAIN RECTIFIER POWER ON), I-503 (PLATE), (all red) light on Modulator, Left Power Amplifier, Center Power Amplifier, and Right Power Amplifier, respectively.
4. Repeat 3 above except turn S-421 to the ON position and in (c) K-1501 and K-1502 should close in sequence connecting the Transformer primaries in Delta.

## FINAL TUNE-UP

1. Replace primary leads on Main Rectifier Plate Transformer.
2. Protective gap settings:
a. Set the protective gap on the Modulator Reactor to 0.2 inch. A number 8 or 13/64 straight shank twist drill may be used as a gauge. Set the protective gaps on the Modulation Transformer to 0.15 inch each. A No. 25 or $5 / 32$ straight shank twist drill may be used as a gauge. These are initial settings. If sparking of the gaps occurs during program operation, each gap may be opened up an additional .05 inch.
b. Set the two protective ball gap assemblies in the Rectox Frame to $1 / 16$ inch each
3. Set up for audio input level, response, distortion and modulation measurements as follows: a. Obtain sample of carrier for modulation monitor and distortion analyzer from two separate lines each connected across a portion of the end ring on the PA inductor L-401.
b. Using a Western Electric Type 111-C (or equivalent) repeat coil for isolation between a 500 ohm attenuator and the input of the transmitter, read level in dbm with volume indicator meter on the audio oscillator side of the attenuator. This applies to all audio input level and audio response measurements.
4. Turn MAIN RECTIFIER CONTROL to tune. Power Amplifier plate volts should be approximately 8.1 kv . Tune Power Amplifier for minimum plate current indicated on M-402 (TOTAL PA PLATE CURRENT).
a. Observe:
(1) M-415 (LOAD CURRENT) 10.6 to 11.0 amperes RF (230 ohm load).
(2) M-304, M-413 (LEFT POWER AMPLIFIER PLATE CURRENT) 1.7 to 1.8 amperes.
(3) M-504, M-414 (RIGHT POWER AMPLIFIER PLATE CURRENT) 1.7 to 1.8 amperes
(4) M-203 (MODULATOR PLATE VOLTS) 9.7 to 10 kv .
b. Adjust C-101 in the Type FA Crystal Oscillators for correct carrier operating frequency. The shaft of $\mathbf{C - 1 0 1}$ (screwdriver adjustment) is accessible through holes in the RF door of the Exciter. The range of $\mathrm{C}-101$ is approximately $\pm 30$ cycles.
c. Reduce MODULATOR BIAS until the tubes draw 0.1 amperes plate current each.
d. Apply 1000 cycle tone to transmitter input at a level of about -14 dbm in order to produce 50 percent modulation of the carrier.
e. Allow transmitter to run at this level for 15 minutes. During this period an occasional Modulator or Power Amplifier plate overload may occur with no apparent reason. If no other abnormal indications are encountered, it may be assumed that the interruptions are "gas flashes" in the WL-5671 tubes.
f. At the end of the 15 minute run, shut down the transmitter completely, including blowers. Inspect and feel all components for indications of abnormal operation or heating. Inspect and feel metal rectifiers, including all stacks of the Modulator and Power Amplifier Rectox Units.
5. If no overloads occurred in e. above, switch main rectifier control to ON and readjust MODULATOR BIAS so that tubes draw 0.2 amperes each with modulation.
a. Modulate 50 percent with 100 cycle tone for 15 minutes. Repeat f . above. If more than one gas flash occurs in a 10 minute period, the run must be extended until the gas "cleans up." Note that with all feedback disconnected, the carrier envelope as seen on an oscilloscope will be considerably distorted. At 11.5 kv on M-401 (POWER AMPLIFIER PLATE VOLTS), observe:
(1) LOAD CURRENT 14.7 amp . RF (230 ohm load). Operate $\mathrm{S}-405$ (OUTPUT COUPLING) as required to give 50 kw output.
(2) LEFT POWER AMPLIFIER PLATE CURRENT 2.55 amp maximum, and equal to Right Power Amplifier plate current.
(3) RIGHT POWER AMPLIFIER PLATE CURRENT equal to Left Power Amplifier plate current.
Note: The plate currents for (2), (3) above must be obtained with equal (or within 3 percent of average) capacitance in C-320 and C-520. Check capacities after tuning to maximum plate efficiency.
(4) M-402 (TOTAL PLATE CURRENT) 5.1 amp maximum.
(5) M-203 (MODULATOR PLATE VOLTS) 13.4 to 13.8 kv .
(6) M-201 (LEFT MODULATOR PLATE CURRENT), M-204 (RIGHT MODULATOR PLATE CURRENT) 0.2 amp each. Operate $\mathrm{S}-108$ and S-109 (LEFT AND RIGHT MODULATOR BIAS) switches on Exciter control panel to give 0.2 amp Modulator plate current each.
(7) M-404 (TOTAL TRANSMITTER INPUT POWER) 98.5 to 103.5 kw .
b. Apply 1000 cps sine tone to the input of the transmitter to give 85 percent modulation. Observe:
(1) Modulator plate currents do not differ from each other by more than 0.2 amps .
c. Repeat (b) except use 50 cps sine tone modulation.
d. Repeat (b) except use 7500 cps sine tone modulation.
e. Input level for 50 percent modulation at 1000 cps should be between -12 and -14 dbm .
6. Shut down all power and bias supplies and:
a. Reconnect wire to TS-125 terminal 325 (audio relay removed in Low Level Audio Adjustments, 807 Stage).
b. Reconnect wires TS-126, terminal 340, and terminal 342. Remove grounds from terminals 340 and 342.
7. Turn on transmitter, observe same conditions as in 5 a above.
a. Apply 1000 cycle sine tone to the input of the transmitter at an input level of +8.6 dbm . Adjust voltage feedback potentiometers R-1117 and R-1118 until Modulator plate currents are equal at 85 percent modulation. Observe that:
(1) The noise level is better than 60 db below 100 percent modulation.
(2) The modulation capability is at least one hundred percent from 50 to 7500 cycles.
(3) The frequency response from 30 to 10,000 cycles is uniform within $\pm 1 \mathrm{db}$.
(4) The distortion is less than 3 percent up to 95 percent modulation from 50 to 7500 cycles.
(5) The carrier shift is less than 5 percent for 100 percent modulation at 1000 cycles.

## ANTENNA ARC INTERRUPTER ADJUSTMENTS

1. Disconnect lead from Center Power Amplifier TS-408, terminal 114 and from the tower tuning RF Current Transformer-Rectifier Unit.
a. Measure capacitance to ground of the above lead.
b. Obtain fixed paper or mica capacitor, 600 volt rating, within 10 percent of above measured value and connect the capacitor between terminals 359 and 362 on TS-414 in the Center Power Amplifier.
2. Replace leads removed in 1 above. Note: If station does not employ pattern change, place permanent jumper between terminals 111 and 112 of TS-408.
3. Remove Antenna Arc Interrupter Unit from Center Power Amplifier.
a. Turn ARRAY BALANCE, ANTENNA BALANCE, and LINE BALANCE controls full counterclockwise.
b. Connect Interrupter Unit to Center Power Amplifier by means of the extension cable supplied.
c. Turn on transmitter ( 50 kw carrier).
d. Turn S-409 (OFF-CALIBRATE-OPERATE) to CALIBRATE.
4. With d-c voltmeter of $1 / 4$ megohm or more resistance, observe 75 to 100 volts icross R-1405 (LINE BALANCE) and across R-1403 (ANTENNA BALANCE). The two voltages must be of same polarity. If not, reverse output leads on tower tuning RF Current transformer-rectifier. If voltages are not between 75 and 100 volts, adjust tap switches on RF Current transformer-rectifier Units to bring them within the above range.
5. Observe:
a. Clockwise rotation of $\mathrm{R}-1405$ (LINE BALANCE CONTROL) causes M-1401 (BALANCE INDICATOR) to deflect, and that with S-1401 (METER SHUNT) button depressed, a deflection of 300 microamperes causes K-1401 (sensitive relay) to close, which closes K-1402 and lights J-401 (ANTENNA SYSTEM UNBALANCE).
b. Similarly, deflecting the BALANCE INDICATOR 300 microamperes in the opposite direction by turning ANTENNA BALANCE CONTROL, should cause the same operations as in a. above.
c. If station employs pattern change, switch ANTENNA ARRAY to DIRECTIONAL, and note action similar to above with R-1404 (ARRAY BALANCE).
d. Increase sensitivity by turning all controls clockwise, keeping BALANCE INDICATOR near zero.
6. Turn OFF-CALIBRATE-OPERATE switch to OPERATE and observe that a 300 microampere unbalance causes momentary interruption of the carrier and lights I-26 (ANTENNA ARC-OVER). Note that if the unbalance is done deliberately by turning one of the controls, the transmitter will be keyed on and off at a rapid rate which may cause one or more overloads to operate if allowed to continue for more than about one second. In normal operation, the cause of an unbalance is removed by momentary interruption of the carrier.

## NOISE, FEEDBACK, DISTORTION, AND RESPONSE

## NOISE

## 1. Power Amplifier

Carrier noise is caused mainly by a-c heating of the Power Amplifier filaments. It is minimized in the 50HG-2 by:
a. Operating the Left Power Amplifier filaments and Right Power Amplifier filaments iquadrature.
b. Current feedback.
c. Adequate grid drive.
d. Symmetry of the Power Amplifier - (circuit balance).

With normal meter indications as listed in the Section on MAINTENANCE, Normal Meter Readings with the Modulator tube plates connected together, the carrier hum should be better than 60 db below 100 percent modulation. With Modulator tubes darkened and with the plates not connected together, the carrier hum should be better than 60 db below 100 percent modulation.

## 2. Modulator

Modulator noise is caused by a-c heating of the tube filaments, and is minimized $k$
a. In-phase operation of filaments and out-of-phase operation of plates (push-pull).
b. Symmetry of Modulator circuit (plate current balance, uniformity of tubes).
c. Voltage feedback.

With Modulator grids connected together, the carrier noise should be better than 54 dbb low 100 percent modulation.
3. Exciter
a. RF Amplifier: The RF amplifiers in the Exciter operate Class C, and do not contribute appreciable hum.
b. 5736 Cathode Follower Audio Stage: The large amount of inherent inverse feedback ? vided by the cathode follower circuit suppresses hum originating within this si
c. 813 Audio Stage: Filament hum is reduced by negative feedback within the stage by the use of a cathode resistor. The hum measured between an 813 plate and ground with the modulator tubes dark, should be less than 3 volts rms.
d. 807 Audio Stage: Very little carrier noise should be contributed by this stage. the tubes, however, must have no loose elements or heater-cathode leakage. A cathode resistor provides negative feedback.

## POWER SUPPLY RIPPLE VOLTAGES

With a 60 cycle supply and normal operating loads, the ripple voltages should be approximately as shown below:

Left 5736 Audio Bias<br>Right 5736 Audio Bias<br>Left Modulator Bias<br>Right Modulator Bias<br>400 Volt Supply<br>Exciter RF Bias<br>1500 Volt Supply<br>3000 Volt Supply<br>Left Power Amplifier Bias Supply<br>Right Power Amplifier Bias Supply<br>Modulator Plate Supply ( 0.4 amp load)<br>Power Amplifier Plate Supply (5.0 amp load)

0.02 volts rms
0.02 volts rms
0.03 volts rms
0.03 volts rms
0.04 volts rms
0.12 volts rms
0.70 volts rms
1.2 volts rms
0.10 volts rms
0.10 volts rms

10 volts rms
100 volts rms
(out of rectifier)

## VOLTAGE FEEDBACK

Voltage feedback is most effective at frequencies greater than 400 cycles. Voltage feedback is used to reduce noise and distortion appearing at the plates of the modulator tubes.

Enough feedback is used at the hum frequencies to bring the hum output of the Modulators well below the power amplifier filament hum.

## CURRENT FEEDBACK

Current feedback is most effective at frequencies below 400 cycles. The change from voltage to current feedback in the feedback loop is accomplished by a cross-over network such that flat overall frequency response within the audio system is maintained, eliminating the need for equalizing.

Current feedback also eliminates instability in the audio system such as may be caused by heavy low frequency modulation (below 30 cps ).

Turntable rumble, program amplifier "thumps," antenna arcs are familiar examples of low frequency phenomena which cause audio instability and overloads.

This audio stability is accomplished by taking the sample of current feedback from the primary side of the modulation transformer. Then in the event of heavy low frequency modulation, the magnetizing current which tends to saturate the transformer and cause overloads is limited by the "eedback loop.

## ISTORTION

1. In a correctly adjusted transmitter, the chief reasons for distortion are:
a. Shift of Modulator plate supply voltage with modulation level. The effect of the Modula tor plate voltage change is minimized by utilizing the increase in driver cathode current to change the operating bias on the modulator tubes.
b. Modulator driver regulation.

Each of the above reasons cause "symmetrical" or even-order harmonic distortion since תe same effect occurs during each half cycle. The first (a) may be seen at medium audio frequencies on the modulation envelope as a slight departure from a sine wave at the abscissa. The econd (b) is evidenced as a slight flattening of sine wave peaks.
2. If the two sides of the audio system do not have the same gain, "non-symmetrical" distortion will be produced as evidenced by inequality between positive and negative modulation peaks. Distortion from this source is minimized by symmetry of circuit components and by proper set-up of the audio system to compensate for non-uniformity of tubes.
3. Insufficient emission capability of the Power Amplifier tubes can cause distortion due to flattening of positive modulation peaks.

## FREQUENCY RESPONSE

The frequency response between 30 and 10,000 cycles is controlled mainly (1) by the characteristics of the voltage and current feedback divided networks, (2) by the "step circuit" network consisting of C-163 and R-143 or C-164 and R-144 for high frequencies and R-145 and C-1105 or R-146 and C-1106 for low frequencies of the grid of the second audio stage.

The input level in dbm required to produce 50 percent modulation in a representative $50 \mathrm{HG}-2$
is as follows:
Frequency
30 cycles
50 cycles
100 cycles
200 cycles
400 cycles
1000 cycles
2000 cycles
4000 cycles
5000 cycles
7500 cycles
10000 cycles

Feedback Connected
$+5.9 \mathrm{dbm}$
$+5.4 \mathrm{dbm}$
$+5.5 \mathrm{dbm}$
$+5.8 \mathrm{dbm}$
$+5.4 \mathrm{dbm}$
$+4.8 \mathrm{dbm}$
$+4.4 \mathrm{dbm}$
$+4.0 \mathrm{dbm}$
$+4.0 \mathrm{dbm}$
$+4.0 \mathrm{dbm}$
$+5.0 \mathrm{dbm}$

Current and
Voltage Feedback Disconnected

- 3.8 dbm
- 7.8 dbm
$-10.5 \mathrm{dbm}$
$-12 \mathrm{dbm}$
$-12.1 \mathrm{dbm}$
$-12.1 \mathrm{dbm}$
$-11.6 \mathrm{dbm}$
$-10 \mathrm{dbm}$
- 9 dbm
- 6.5 dbm
- 4.2 dbm


## CONTROL CIRCUITS

## FUNDAMENTAL CONTROL SCHEMATIC DIAGRAM

The Fundamental Control Schematic, figure 47, should be used as a reference in following the operation of the control circuits. Information pertinent to this diagram follows:

1. All switches are shown in the OFF position. All power is off.
2. All relays and contactors are shown deenergized. A normally closed contact is designated by a diagonal line through the contact.
3. All door and enclosure interlock switches are shown in the "door open," or "enclosure open" position.
4. The air interlock switch, S-515, is open.
5. Reference numbers that appear on coils, contacts, switches, etc., also appear on the same component terminals or are terminal board numbers in the wiring diagrams. This makes it possible to correlate points on the control schematic with terminals or terminal board connections in the transmitter cubicles themselves.

## THE TURN-ON SEQUENCE

With all switches on the upper Power Control Panel turned ON except SWITCHGEARCONTROL BUS, TRANSMITTER CONTROL BUS, and the filament switches for the spare Modulator and Power Amplifier Tubes, the turn-on sequence is as follows:

| S-9 | SWITCHGEAR CONTROL BUS | S-11 | TRANSMITTER CONTROL BUS |
| :--- | :--- | :--- | :--- |
| S-30 | BLOWER CONTROL (This will | S-31 | AUDIO BIAS |
|  | normally be left in the | S-32 | RF BIAS |
|  | TRANSMITTER AND BLOWER | S-103 | 400 VOLT RECTIFIER |
| position) | S-104 | $1500-3000$ VOLT RECTIFIER |  |
| S-28 | BUS BREAKER | S-410 | MAIN RECTIFIER CONTROL |

The manner in which the above sequence is maintained can be followed on the Fundamental Control Schematic, figure 47. This is facilitated by the dotted lines which connect each relay or contactor coil to all of its contacts.

ACTION ON SUSTAINED FAULT
The sequence is as follows:
With S-27 in AUTOMATIC position, assume that K-301, L PA overload has operated due to excessive plate current.

1. K-16, Main Master overload operates.
2. K-7, Main Rectifier Breaker Auxiliary, is deenergized.
3. K-7 normally closed contacts energize trip coil of S-2002, the Main Rectifier Breaker.
4. S-2002 opens.
5. S-2002 normally closed contact energizes K-2014 (MG-6 in Switchgear Cubicle).
6. K-2014 normally open contact energizes K-47, Stepping Switch Auxiliary No. 1.
7. K-47 normally open contact energizes step coil of $K-13$, stepping switch and $K-13$ advances one step.
8. K-13 normally open contact closes.
9. K-4, Time Delay, starts.
10. Removal of power by S-2002 will remove the overload and allow K-301 to drop out.
11. K-16 opens, closing K-7, energizing the breaker pull-in coil "CC" in the Switchgear. When breaker is nearly closed, a normally open breaker auxiliary contact energizes the "anti-pump" relay K-2008, which in turn opens the circuit to the pull-in coil "CC" which no longer needs to be energized since the breaker latches in mechanically. With the breaker closed, the Main Rectifier is again connected and the transmitter is returned to operation. The function of switches S-2010 and S-2011 is to allow the breaker toggle mechanism to reset before the closing coil is re-energized. This is accomplished by keeping K-2008 energized through switch S-2013 until the closing coil plunger reaches the bottom of its travel, thus opening switch S-2012 and allowing the closing coil to be energized.
12. Application of power again operates overload relay $\mathrm{K}-301$ if the fault condition is still present and the above sequence ( 1 to 11) is repeated ( $\mathrm{K}-13$ advancing one step each time) until the arms on $\mathrm{K}-13$ reach the fourth contact. Then:
13. K-16 is locked in by its own normally open contact, thus holding the Main Rectifier off.
14. K-4 continues to run until it closes, energizing K-5.
15. K-5, Time Delay Auxiliary, normally closed contact opens K-13 step coil, and K-5 normally open contact energizes $\mathrm{K}-13$ release coil.
16. $\mathrm{K}-13$ resets and the entire sequence listed above is repeated until stopped by the operator.
17. The operator may stop the sequence by turning off the Main Rectifier, or any switch ahead of it in the turn-on sequence, or by switching S-27 to MANUAL.

## NOTE

A sustained fault in the $1500 / 3000$ Volt Supply causes a similar performance, with the supply held off when the stepping relay reaches the fourth contact. (S-410 must be closed and S-27 in AUTOMATIC for the $1500 / 3000$ Volt Supply to operate the step sequence.) Note that an overload on the 400 Volt Supply will cause K-13 to step up, but will not shut down the supply. That must be done with S-103 or some switch ahead of it in turn-on seauence.

## SUPERVISORY RELAY TEST POSITION

Socket $\mathbf{X}$-20 is provided in the Power Control Cubicle for use as a test position for the supervisory system relays. As can be seen from the Fundamental Control Schematic, figure 47, a relay plugged into X-20 will be energized, closing both normally open contacts and causing 1-32 (SUPERVISORY RELAY TEST) to light, the relay is working properly.

## SUPERVISORY SEARCH RELAY

As a special supervisory search relay, K-1 may be employed to detect erratic operation of enclosure interlocks, air switch, undervoltage relays or other circuits not equipped with supervisory relays and indicator lights. Terminals of K-1 and I-31 (SEARCH RELAY) appear on TS-2, terminals 13 to 20, at the rear of the Power Control Cubicle where they are conveniently accessible and may be connected to other circuits as desired by the station engineer.

## OUTAGE CLOCKS

The OUTAGE TIME and OUTAGE DURATION clocks on the Power Control Panel are set as follows:

1. With Transmitter in operation, set the OUTAGE TIME clock to correct time and start it by pressing the RESET button below it.
2. Set the OUTAGE DURATION clock at 12. The clock will run with the transmitter in operation as long as the RESET button is pressed, thus making it possible to set the second hand accurately.

Operation of the clocks can be followed on the Control Schematic, figure 47. Briefly, whenever the Main Rectifier Breaker S-2002 trips, the OUTAGE TIME clock stops, the OUTAGE DURATION clock starts and I-25 (CARRIER INTERRUPTION) lights.

## FILAMENT UNDERVOLTAGE RELAY K-8

The operation of $\mathrm{K}-8$ is as follows:

1. K-8 begins a timing cycle when the exciter filament circuit is turned on.
2. After approximately 22 seconds, depending on the voltage slider setting, (see I. L. 41-291D in the Supplement Section) the normally open contact closes, lighting I-42 (EXCITER FILAMENTS NORMAL VOLTAGE) and "latching-in" relay K-46, the Filament Delay Auxiliary.
3. An interruption in supply voltage will cause the normally open contact to open and after a delay of approximately 8 seconds (depending on the time lever setting of $K-8$ ) the normally closed contact to close.

Note that reapplication of power before the 8 seconds have expired will return the transmitter to the air without delay.

BUS BREAKER S-2001
The operation of the Bus Breaker is as follows:

1. With switches S-28 and S-30 closed and series interlocks closed, relay K-3, Bus Breaker Auxiliary, is energized.
2. The normally open contacts of $\mathrm{K}-3$ close, energizing the "pull-in" coil "CC."
3. When the breaker is nearly closed, a normally open breaker auxiliary contact energizes and seals in the "anti-pump" relay K-2004 which in turn opens the circuit to the "pull-in" coil "CC" which no longer needs to be energized since the breaker latches in mechanically. Switches S-2010 and S-2011 function the same as switches S-2012 and S-2013 in the high voltage breaker S-2002.
4. With the breaker closed, the normally open contact in series with the trip coil " T " of S-2001 closes, but the trip coil receives no energy until K-3 becomes deenergized. When this occurs, the breaker is returned to its original "off" position.
5. Note that the breaker will follow relay K-3 off and on; however, the presence of K-2004 in the circuit prevents "pumping" of the breaker due to tripping from a-c overloads or undervoltage. It also prevents the breaker from coming back on automatically if it is manually tripped.

## MAINTENANCE

## SUGGESTED SCHEDULES

1. Daily
a. Check pressure in all gas filled capacitors.
b. Check and polish, if necessary, protective gaps on gas filled capacitors, on 5736 audio driver cathode chokes, on Modulation Transformer, on Modulation Reactor, and on Rectox units.
c. Inspect fuse wires on high voltage capacitors in Filter.
2. Weekly
a. Check operation of all control circuit devices, door interlocks, and other protective devices.
b. Check air interlock as follows: With the distribution bus on, but with filaments off, open the Blower line starter breaker (shutting down blower). This should cause I-36 or 1-41 light to go out and the distribution bus to be deenergized.
c. Thoroughly clean interior and exterior of transmitter cubicles. Clean power equipment external parts with special attention to insulators.
d. Inspect and oil Blower bearings. Use light machine oil, (SAE No. 10).
3. Monthly
a. Inspect and, if necessary, clean contactors and relays in the transmitter cubicles. Take particular care to keep the contacts clean on K-3, K-7, and K-13 in the Power Control. Abrasives should not be used on silver contacts, because particles of the abrasives may become embedded in the contact surface. Cleaning the contact fingers and contact arcs of relay $\mathrm{K}-13$ should be done with a soft rag saturated in carbon tetrachloride. After cleaning, remove all lint, and lubricate the contact fingers, bearing pins, and ratchets sparingly with a light mineral oil.
b. Inspect and, if necessary, clean Main Rectifier and Distribution Bus Switchgear, Type DB-25. Refer to I.B. 35-225-1.
c. Inspect, clean and lubricate Bus Regulators, also Main Rectifier Regulator if used. Refer to I. B. 5521-A.
d. Inspect and, if necessary, tighten all electrical connections.
e. Operate the spare Modulator and Power Amplifier tubes with reduced plate voltage and increase to full power in approximately 15 minutes. Check modulation capability with tone or program material.

## 4. Quarterly Schedule

a. Lubricate the exposed parts of the motor operated tuning controls. The reductiongears are packed in grease and with normal usage will require no attention during the life of the equipment. Put a drop of light machine oll on the motor bearings once or twice a year.
b. Metal rectifiers age slightly during the first several thousand hours of use resulting in a small decrease of output voltage. This decrease may be cancelled by changing the transformer primary taps of the 400 volt and RF bias supplies and by adjusting the controls of the audio bias supplies. Following this initial period, the rectifiers should be closely inspected regularly for evidence of overheating or corrosion. A casual inspection is usually unsatisfactory, because in practice first evidence of these effects usually shows up in individual cells rather than a general deterioration.
c. The dry type power transformers may require cleaning to prevent clogging of the ventilating ducts if the air contains an excessive amount of dust or lint. If a dry typetransformer gets wet, it must be removed from service and thoroughly dried.
d. The air inlet filter cleaning schedule will depend on local air conditions. The condition of the filters may be determined by inspection or by checking the air flow through the transmitter as specified in the section on Air Velocity under the main heading POWERON ADJUSTMENTS. Any indication of a reduction in the normal flow of air should call for replacement or cleaning at once.

If a Precipitron, the Westinghouse Electronic Air Cleaner is used, little maintenance is required besides periodic washings according to instructions furnished with the equipment.

## RECTOX RECTIFIERS

The following is a general discussion of the characteristics of rectox rectifiers.

1. Forward Aging
a. A small increase in resistance to the flow of load current is normal. The resulting reduction in output voltage should not be more than about 5 percent over a period of years. Most rectifier transformers are provided with "aging" taps whereby the voltage can be increased after a year or so of operation. Thereafter no further adjustments should be necessary. A further indication of normal forward aging is a slight increase in output hum of three-phase full-wave rectifiers.
2. Reverse Aging
a. Normal aging: The reverse resistance will decrease somewhat with age. This is normal and will have no appreciable effect on the rectifier operation.
b. Effects of excessive reverse aging: If the aging in the reverse direction becomes excessive, the rectifier will overheat. The overheating may damage the cells, or may accelerate forward aging. An abnormal increase in reverse current may overload and damage the rectifier transformer.
c. Indication of reverse aging: Excessive reverse aging may be detected from any of the effects listed in b. above. In addition, it is possible to measure directly the reverse current in any stack by following the procedure as set forth in paragraph 3 "Replacement of Rectifier Stacks."
d. Allowable limits of reverse current: It is not possible to give the exact limits of reverse current which may be considered normal. The following general statements apply, however:
(1) Using the original reverse current measurements supplied by the manufacturer as a standard, the current should not increase over four times this value as aging takes place.
(2) The reverse current will increase with increasing temperature.
(3) The reverse aging rate will be less with selenium than with copper oxide.

## 3. Replacement of Rectifier Stacks

The condition of selenium or copper oxide rectifiers can usually be determined by checking output d-c voltage and rms ripple voltage. A sudden increase in normal ripple with a simultaneous decrease in the output may be the fault of the rectifier and would warrant further investigation. A gradual decrease of approximately 5 percent in the output d-c voltage is to be expected from the normal aging of the rectifier. This also may result in some increase in hum due to some of the rectifiers aging more rapidly than others. If it is decided that the rectifier may be at fault, the following test should be made.

Ordinarily a faulty rectifier stack can be located by running the unit at full load for a short time and then immediately after shutting off the power, checking the temperature of the various rectifier stacks with a thermometer or with the hand. A faulty stack will usually be hotter than the rest. This stack should be disconnected and checked as follows:

Use a d-c power supply capable of supplying the current and voltage shown in the following chart. To check the forward rectifier resistance, connect the positive terminal of the d-c test supply to the negative terminal on the rectifier and the negative terminal of the test supply to the opposite end of the rectifier stack or center tap as noted in some cases. Adjust the test voltage to the proper value. The resulting forward current should be approximately as shown in the table. In checking the back resistance of the rectifier, connect the positive lead of the test supply to the positive rectifier stack terminal.

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I.B. $81-120-2 \mathrm{~A}$


I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \dot{2}$

I. B. 81-120-2A


I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

1.B. 81-120-2A

I. B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

| ORAWIN | $\begin{aligned} & \text { NG NO. } \frac{50-B-8600^{\circ}}{} \text { PHE } \\ & \text { PARTS } \\ & \text { ATUS } 50 \mathrm{HG}-2 \quad \text { A. } \mathrm{M} . \end{aligned}$ | ET 19 OF <br> AND RECOMMENDED SPARE <br> BROADCAST TRANSMITTER |  | $\begin{aligned} & \text { ST } \\ & \text { נT- } \\ & \text { No } \end{aligned}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CIRCUIT SYMBOL | FUnction | DESCRIPTION | STYLE OR CAT. NO. | MFR | WESTINGHOUSE DRAWING NO. |  |  |  |
|  |  |  |  |  |  | QUANTITY |  |  |
|  |  | P.C. (CONTINUED) |  |  |  |  |  |  |
| K-33 | Relay, R.P.A., O.L. Aux. | Same as K-17 |  |  | 7619418 P7. 153 |  |  |  |
| K-34 | Relay, garrier inter. Aux. | Sakc as K-17 |  |  | 7619418 Pt. 154 |  |  |  |
| K-35 | Relay, sparg | Same as K-17 |  |  | 7619418 Pt. 155 |  |  |  |
| K-36 | Relay, spare | Same as K-17 |  | . | 7619418 Pt. 156 |  |  |  |
| K-37* | Contactor, audio Blas | TYPE DN-00 10 AMP. CONTACTOR, 3 POLE N. O., 230 V., 60 crGLES. | $\begin{aligned} & \text { STYLE } \\ & 1301694 \end{aligned}$ | 1 | 7619418 Pr. 157 | 1 |  |  |
| K-38 | Contactor, R.f. bias | TYPE DN-00 10 AMP. CONTACTOR, 4 POLE N. O., 230 V., 60 creles | Strle 1190560 | 1 | 7619418 Pr. 158 | 1 |  |  |
| K-39 | Contactor, 400 V . SUPPLY | Samz as K-37 |  |  | 7619418 PT. 159 |  |  |  |
| K-40 |  | CLASS 15 . 825 N 2 SIZE2., <br> TYPE N-24O 45 AMP. CONTACTTOR. 4 POLE <br> N. O., 230 V., 60 creles (SEE NOTE FOR 50 CYCLE OPERATION ON PAGE 59 ). | Strle tratit69 1614216 | 1 | 7619418 Pr. 160 | 1 |  |  |
| K-41* | Relay, aux. frames | trpe Sg aux. relay, $230 \mathrm{~V} ., 50 / 60 \mathrm{cr}$. | $\begin{aligned} & \text { STYLE } \\ & 1008540 \end{aligned}$ | 1 | 7619418 Pr. 161 | 10 | 1 |  |
| K-42 | Relay, p.C. intla. | Same as K-41 |  |  | 7619418 PT. 162 |  |  |  |
| k-43 | Relay, Exc. \& MOD. Intlk. | Same as $\mathrm{K}-41$ |  |  | 7619418 Pr. 163 |  |  |  |
| $x-44$ | Relay, L.p.a. Intlk. | Same as K-41 |  |  | 7619418 Pr. 164 |  |  |  |
| K-45 | RELAY, C.P.A. \& R.P.A INTLK, | Same as K-41 |  |  | 7619418 Pr. 165 |  |  |  |
| k-46 | Relay, fil. delay Aux. | Trpe MG-6 aux. relay, 230 V., 60 cy . (SEE NOTE TOR 50 CYCLE OPERATION ON page 58). | Sirle <br> 1163957 | 1 | 7619418 Pr. 166 | i |  |  |
| K-47 | Relay, aux. No. 1 STEPPING | Same as K-41 |  |  | 7619418 Pr. 167 |  |  |  |
| K-48 | Relay, Aux. No. 2 STEPPINQ | SAME As K-41 |  |  | 7619418 Pr. 168 |  |  |  |
| K-49 | Relay, gus breaker time delay | Same as K-41 | . |  | 7619418 Pr. 169 |  |  |  |
| K-50 | Rglay, HV brcaker rime dilay | Same as K-41 |  |  | 7619418 PT. 174 |  |  |  |
|  |  | EXCITER |  |  |  |  |  |  |
| K-101 | Relay, audo inpuy SHORTING | SAME AS K-41 |  |  | 7619373 Pr. 172 |  |  |  |
| K-102 | Relay, osc. selector | D.P.D.t. latching relay, 24 V., D.C. COIL | Similar TO 2759 | 37 | 7619373 Pr. 173 | 1 |  |  |
| K-103 | Relat, carrier inter. | Same as K-41. |  |  | 7619373 Pr. 174 |  |  |  |
| K-104 | Relay, 807 \& 813 AVOIO SCREEN INTLK. | Samt as k-41 |  |  | 7619373 Pr. 175 |  |  |  |
| K-105* | REl.AY, 400 V., D.C. O. L. | TYPE SC CURRENT rELAY, 0.25-1.0 amp. RANGC | $\begin{aligned} & \text { STYLE } \\ & \text { 1096937- } \\ & (\text { MODIFIED } \end{aligned}$ | 1 | 7619373 PT. 176 | 2 |  |  |
| K-106 | felay, 813 k.f., Pl. (). L. | Same as k-105 |  |  | 7619373 P7. 177 |  |  | , |
| k-107* | Relay, L.5736, R.F. B.L. | Type sC current relay 0.5-2.0 amp. range | $\begin{aligned} & \text { STYLE } \\ & 1096937 \end{aligned}$ | 1 | 7619373 Pt. 178 | 4 |  |  |
| n. 108 | $\begin{aligned} & \text { RELAY, R.S736, R.F. } \\ & \text { FI. O. L. } \end{aligned}$ | Same as K-107 | - |  | 7619373 PT. 179 |  |  |  |
| 0.109 | kitar, Exc. Bias, U. V. | Trpe SV voltage relay, 50-150 V.D.C. | $\begin{aligned} & \text { STYLE } \\ & 1096958 \end{aligned}$ | 1 | 7619373 Pr. 180 | 7 |  |  |
| -110* | helay, l. Audio blz fi. O. I. | Type SC current relay, 0.1-0.4 amp. range | $\begin{aligned} & \text { STYLE } \\ & 1096937- \\ & (\text { Mooirico }) \end{aligned}$ | 1 | 7619374 PT. 181 | 4 |  |  |
| 11 | Sutay, R. Auble 813 | Sami as K-110 |  |  | 7619374 Pt. 182 |  |  |  |
| , | (1A1) … AUGIO BTAS | Same as K. 109 |  |  | 7619374 Pr. 183 |  |  |  |

I.B. $81-120-2 \mathrm{~A}$

I. B 81-120-2A

I. B. 81-120-2A


1. B. $81-120-2 \mathrm{~A}$


| DRAWING NO. 50.B.8600 SHEET 2 OF_SHEETS |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PARTS AND RECOMMENDED SPARE PARTS LIST <br> APPARATUS $\qquad$ $50 \mathrm{HG}-2$ <br> A. M. BRDADCAST TRANSMITTER <br> INPUT STYLE NO. $\qquad$ $\qquad$ |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |
| CIRCUIT SYMBOL | FUNCTION | DESCRIPTION | STYLE OR CAT. NO. | MFR | WESTINGHOUSE DRAWING NO. |  |  |  |
|  |  |  |  |  |  | QUANTITY |  |  |
|  |  | EXCITER (CONTINUED) |  |  |  |  |  |  |
| L-131 | Choke, R. audio 5736 CATHODE | Same as L-130 |  |  | Pr. 224 |  |  |  |
| L-132 | Choke low level AUDIO BIAS | Same as L-115 |  |  | Pr. 225 |  |  |  |
| L-133 | Same as L-132 | Same as L-115 |  |  | Рт.226 |  |  |  |
| L-134 | Coil, static drain | 7 turns each side of C. T. on ceramic COIS FORM | $\begin{gathered} G-1 \\ 7724079 \end{gathered}$ | 1 | 7619374 PT. 227 | 1 |  |  |
|  |  | MODUATOR |  |  |  |  |  |  |
| L-201* | Choke, r. F. folter | 2.5 MH., R.f. Choke | $\operatorname{TVPE}_{R-100}$ | 56 | 7617688 PT. 33 | 5 |  | 2 |
| L-202 | Same as L-201 |  |  |  | 7617688 Pr. 34 |  |  |  |
|  |  | L.P.A. |  |  |  |  |  |  |
| L-301* | COIL, 5736 ORID tank | Air cort | $\begin{gathered} \text { G-4 } \\ 7606741 \end{gathered}$ | 1 | 7619014 Pr. 69 | 2 |  |  |
| L-302 | Choke, R.f. grio | Same as L-110 |  |  | Pt. 70 |  |  |  |
| L-303* | coil, neutine | Freg. sensitive | SELECT FROM 7427628 |  | Pr. 71 | 2 | 1 |  |
| L-304* | Choke, R.f. plate | Ceramic wound | $\begin{gathered} 7427628 \\ \text { G-5 } \\ 7707576 \end{gathered}$ | 1 | Pr. 72 | 2. | 1 | 1 |
| L-305 R | Reagtor, bias supply | Same as L-113 |  |  |  |  |  |  |
| L-306 | Same as L-305 | Same as L-113 |  |  | Pr. 73 |  |  |  |
| L-308 S | Same as L-201 | Same as L-201 |  |  | Pr. 74 |  |  |  |
| L-309 S | Sahe as L-201 | Same as L-201 |  |  | $\begin{array}{rr}\text { Pr. } 76 \\ 7619014 & \text { Pr. } 77\end{array}$ |  |  |  |
|  |  | C.P.A. |  |  |  |  |  |  |
| L-401A C | Coil, plate tank | air core variable coil | $\begin{gathered} \mathrm{G}-1 \\ 7426170 \end{gathered}$ | 1 | 7619389 PT. 69 | 1 |  |  |
| L-4018 | COIL, COUPLING | Part of L-401A |  |  | Pт. 70 |  |  |  |
|  |  | R.P.A. |  |  |  |  |  |  |
| L-501 | COIL, 5736 QRIO TANK | Same as L-301 |  |  | 7619054 Pr. 69 |  |  |  |
| L-502 | Choke, R.f. ario | Same as L-110 | . |  | Pr. 70 |  |  |  |
| L-503 | Coil, meutralizing | Same as L-303 |  |  | Pr. 71 |  |  |  |
| L-504 | Chore, R.f. plate | Same as L-304 | . |  | PT. 72 |  |  |  |
| L-505 | REACTOR, R.P.A. BIAS SUPPLY | Same as L-113 |  |  | Pt. 73 |  |  |  |
| -506 | REACTOR, R.P.A. BIAS SUPPLY | Same as l-113 |  |  | Pr. 74 |  |  |  |

1.B. $81-120-2 \mathrm{~A}$

I. B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 \mathrm{~A}$

I.B. $81-120-2 A$

| CRAWIN <br> APPARA | ( NO 50.8.8600 SHEE PARTE <br> rus <br> 56) 46-2 | $T$ $\qquad$ OF $\qquad$ SHEETS <br> ND RECOMMENDED SPARE <br> 1. BROAI)C.AST TRANSMITTER | $\begin{array}{r} \text { ARTS LIS } \\ \text { INPUT } \\ \text { STYLE NO } \end{array}$ | ST | WESTIN |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CIRCUIT <br> SYMEOU | gUNCTION | DESCRIPTION | STYLE OR GAT. NO. | MFR | WESTINGHOUSE DRAWING NO. |  |  |  |  |
|  |  |  |  |  |  |  | QUANTITY |  |  |
|  |  | EXCITER |  |  |  |  |  |  |  |
| R-101 | Res., osc. grio | . 22 megonm, 1 W. | S-1471204 | 1 | 7720527 | PT. 17 | 1 | 5 | 2 |
| R-102 | Res., osc. catmode | 400 оНलs, 10 W. | 10F | 44 |  | Pr. 18 | 1 |  |  |
| R-103 | Res., osc. volts DIVIOES | 6000 оняs, 20 W. | 20K | 44 |  | PT. 19 | 1 |  |  |
| R-104 | $\begin{aligned} & \text { Regio osc. yoty } \\ & \text { Diviór } \end{aligned}$ | 20,000 омms, 10 W. | 10F | 44 |  | Pr. 20 | 1 |  |  |
| R-105 | Res.it ind. currcht ${ }_{\text {linit }}$ | 47,000 оннs, $1 / 2 \mathrm{~W}$. | S-1471167 | 1 | 7720527 | Pr. 21 | 1 | 5 | 2 |
| R-106 | RES., R.F. 807 GRID | 15,000 OHMS, 2 W . | S-1471266 | 1 | 7619375 | Pt. 271 | 1 | 5 | 2 |
| R-107 | RLS., R.F. 807 CATHODS | 200 OHms, 13 W . | JAN-R-26 RW20J201 |  |  | Pr. 272 | 1 |  |  |
| R-108 | Res., R.f. 807 screen | 0.i meg., 2 W. . | S-1471276 |  |  | Pr. 273 | 1 | 5 | 2 |
| R-109 |  | 5,000 ONMS. 6 W. ${ }^{\prime}$ | JAN -R-26 RW15E502 |  |  | Pr. 274 | 1 |  |  |
| R-110* | RES., R.F. 813 GRIO SUPPRESSOR | 56 Ohms, 1 W . | S-1471012 |  |  | Pr. 275 | 2 | 5 | 2 |
| R-111 | Same as R-110 |  |  |  |  | Pt. 276 |  |  |  |
| R-112* | Res., R.F. 813 CATHODE | 500 omms, 86 W. | JAN-R-26 2W12G501 |  |  | Pr. 277 | 2 | 2 | 1 |
| R-113 | REs., R. F., B13SCREEN DIVIOER | 40,000 OHMS, $20^{6} \mathrm{~W}$. | $20 \%$ | 46 |  | Рт. 278 | 1 |  |  |
| R-114 | Res., R.F. 813 SCREEN DIVIDER | 25,000 Ohms, 120 W . | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RWI 1G253 } \end{aligned}$ |  |  | Pr. 279 | 1 | 2 | 1 |
| R-115* | Res., grio balancing | 100 OMms, 50 W . | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RWI 3G } 101 \end{aligned}$ |  |  | Pr. 280 | 3 | 2 | 1 |
| R-116 | Res., grid oalancing | Same as R-115 |  |  |  | Pt. 281 |  |  |  |
| R-117A | Res., R.f. Exc. blas | Same as R-112 |  |  |  | Pr. 282 |  |  |  |
| R-1178 | Res., R.f. Exc. blas | 310 omus, 86 W . | JAN -R-2 6 RW12G311 |  |  | Pr. 283 | 1 | 2 | 1 |
| R-119* | Роt., L. AUQio 5736 BIAS | 10,000 ohns, 50 Wo | 1106-22 | 46 |  | Pr. 285 | 2 | 2 | 1 |
| R-120 | $\begin{aligned} & \text { POT., R. AUDIO } 5736 \\ & \text { BIAS } \end{aligned}$ | Sane as R-119 |  |  |  | Pt. 286 |  |  |  |
| R-121* | Reg., L. Mod. bias | 200 omms, 90 W . | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RW12G2O } \end{aligned}$ |  |  | Pr. 287 | 2 | 2 | 1 |
| R-122 A* | Res., L. Mod. bias | 2500 OHMS, 90 W. | $\begin{aligned} & \text { JAN-R-26 } \\ & \text { RW12G252 } \end{aligned}$ |  |  | Pr. 288 | 4 | 2 | 1 |
| R-1228 | Same as R-122a | Same as R-122a |  |  |  | Pr. 289 |  |  |  |
| R-124 | Res., R. MOD. bias | Same as R-121 |  |  |  | Pr. 291 |  |  |  |
| R-125A | Res., R. MOD. aias | Same as R-122A |  |  |  | Pr. 292 |  |  |  |
| R-12sfi | SAme as R-125A | Same as R-122A |  |  |  | Pr. 293 |  | - |  |
| R-126* | Res., M-123 shunt | . 47 megorm, 1 W . | S-1471200 | 1 |  | Pr. 294 | 2 | 5 | 2 |
| R-127 | Res., M-108 shunt | Sahe as R-126 |  |  |  | Pr. 295 |  |  |  |
| R-128* | pot., R.f. 813 plate TUNING CAL. | 7500 ohms, 2 W. . Linear taper pot. | $\begin{aligned} & \text { HAN-R=19 } \\ & \text { FA1SA1SA- } \\ & \text { TSRAKK } 43 \end{aligned}$ | 44 |  | Pt. 296 | 8 | 2 | 1 |
| R-1?9 | POT., R. F. 5736 pLATE tuning cal. | jame aspioz | TYPEA3 |  |  | Рт. 297 |  |  |  |
| R-1.30 | Pot., R. F. 81.3 plate tuning ino. | 300 Ohms, $\pm 10 \%, 2 \mathrm{~W}$. | $\begin{gathered} \text { Pr. } 3 \\ 7422247 \end{gathered}$ | 1 | 7619375 | Pt. 298 | 1 | 2 | 1 |
| (R-131* | FIt., R.F. 5736 plate TUNING IND. | 250 omms | JAN $=R=19$ RAS5AFFG- | 44 | 7619375 | Fr. 299 | 7 | 2 | 1 |
| R-132 | fot., R.F. 5736 plate COUPLING IND. | Same as R-131 |  |  | 7619375 | Pr. 300 |  |  |  |
| R-134." | KRES., AUD. INPUT trans. load | Nominal regigtance 33,000 ohms, 2 W. USED ONLY IN MATCHED PAIR WITM R-185. | $\begin{aligned} & 29,700 \\ & \text { ro } \\ & 36,300 \text { OHm } \\ & \text { SELECR } \operatorname{FRO} \\ & \text { S\#1471270 } \end{aligned}$ |  | 7619376 | Pt. 302 | ONE MATKE PAIR |  | ONE |
| R-1 35 | SAME AS R-134 | Nominal resistance 33,000 ohms, 2 W. (USEO ONLY IN MATCHED PAIR VITM R-134) | Matched WITHIM 660 ohms of R1: BELECT ERAO | $\begin{aligned} & 1 \\ & 132 \\ & 5 \# 2 \end{aligned}$ | 17619376 | Pr. 303 |  |  |  |

I. B. $81-120-2 \mathrm{~A}$

I.B. 81-120-2A

I. B. $81-120-2 \mathrm{~A}$


fig. 1. Power Control Cubicle, Front View (Photo C.12107)

I.B. $81-120-2 A$


I.B. 81-120-2


FIG. 6. Exciter Cubicle. Front View (Photo C-12115)

I.B. 81-120-2


FIG. 8. Exciter Cubicle, Radio Door (Pholo C-12118)





FIG. 13. Modulator Cubicle, Front View (Photo C-12123)



FIG. 15. Modulator Cubicle Interior (Photo C-20276)
I.B. 81-120-2


I.B. 81-120-2





FIG. 21. Antenna Arc Interrupter Unit (Photo C-12104)



FIG. 23. Right Power Amplifier Cubicle. Front View (Photo C.12139)

## I.B. 81-120-2



FIG. 24. Right Power Amplifier Cubicle, Interior, Front View (Photo C-12140)


FIG. 25. Right Power Amplifier Cubicle, Interior View (Photo C-12141)



(15)

(12)





- $25^{\prime}-1 \frac{1}{2}$ "WHEN END RADII ARE USED




general notes
(1) PROVIDE 7 RECTANGULAR HOLES THROUGH FLOOR AS SHOWN.

(2) OESIGN FLOOR TO CARRY $4000 \angle B S ~ P E R ~ C U B I C L E ~(6 . C U B I C L E S) ~$
(3) EACH CUBICLE IS 4! $/ 4^{\prime \prime}$ WIOE $\times 4^{.6} 6^{1 / 4}$ OEEP $\times 7^{\prime} \cdot 0^{\circ} H I G H$.






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NyTd 3sva







 BotTOM OF Duct open entiee Length of transuitter

aLL OMENSIONS ARE IN NCHES
CAULKING: INSIDE SHOUUD OE OONE BY REACHING THRU AIR HOLE,




Yat whe wow


FIG. 38. Typical Air Exhaust Duct (Dwg. 7621270)




 Rell


3. BOX ORANFRS CLEAR $13 \frac{9}{16} \times 5 \frac{27}{32} \times 24 \frac{1}{9}$
4. FINISH PEF PRCCESS SPEC. 332-B

CHAIR-ORDER FROM YARRINGTON $\ddagger$ UOHNS,INC.,





FIG. 61. Type FA Crystal Oscillator. Schematic Diagram (Dwg. 7425857)



NOTE- TO INEREASE THE SENSITIVITY, THE PICKUP COIL CAN BE
TRANSFERRED TO THE PRIMARY' SIDE OF THE ELECTROSTATIC SHIELD.

$$
\begin{aligned}
& \text { Chanqe in resistor } \\
& \text { made to use ima metor } \\
& \text { Ba. }
\end{aligned}
$$





TOP VIEW OF REGULATOR
I.B. $81-120-2 \mathrm{~A}$


FIG. 59. Main Rectifier Regulator, Schematic Diagram (If Used) (Dwg. 7718452)



```
A - POWER CONTROL
B-EXCITER
C. MODULATOR
D-IEFT POWER AMPLIFIER
E-CENTER POWER AMPLIFIER
F RIGHT POWER AMPLIFIER
    SPACE FOR PHASING CUBICLE IS NOT SHOWN.
    IF PHASING CUBICLE IS USED, DUE ALLOWANCE
    SHOULD BE MADE.
G- FILTER REACTOR
H-MODULATION REACTCR
\(J\)-AUXILIARY AUDIO CHOKE
\(K\) - MODULATION TRANSFORMER.
L. COUPLING CAPACITOR
M-OISTRIBUTION TRANSFORMER
N-DISTRIBUTION TRANSFORMER
P. DISTRIBUTION TRANSFORMER
Q-DISTRIBUTION REQULATOR
R. DISTRIBUTION REGULATOR
\(S\) - RECTIFIER REGULATOR (OPTIONAL EQUIPMENT)
T- PLATE TRANSFORMER
U. RECTIFIER
V. FILTER CAPACITOR
W-SWITCH GEAR
\(X\)-AUXILIARY POWER SUPPLY
```


[^0]:    * Weight does not include tubes. $\quad$ Includes $4-3 / 8$ inch shaft dimension.

[^1]:    * Weight does not include tubes. $\quad$ Includes $4-3 / 8$ inch shaft dimension.

